

10 INDUSTRIAL AVENUE, SUITE 3 MAHWAH, NJ 07430

PHONE: 201.684.0055 FAX: 201.684.0066

July 28, 2020

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Notice of Exempt Modification 623 Pine Street, Bridgeport, CT Latitude- 41.16567777 Longitude- -73.216627777 T-Mobile Site ID: CT11014B / Anchor

Dear Ms. Bachman,

T-Mobile currently maintains (9) existing antennas at the 180' level of the existing 250' selfsupport lattice at 623 Pine Street in Bridgeport, Connecticut. The tower and property is owned by Radio Communications Corp. T-Mobile now intends to replace (3) of its existing antennas with (3) new 2500 MHz antennas. The new antennas would be installed at the 180-foot level of the tower.

Planned Modifications:

Remove: (6) 1-5/8" coax cables

Install New: (3) Commscope -SDX 1926 Q-43(E14F05P86) Diplexers (3) 6x12 Hybrid cable

<u>Remove/Replace</u>:

Antennas: AIR21 KRC118023-1_B2A_B4P (Remove) - (3) Air6449 B41- 2500 MHz / 2500 MHz (Replace) RRUs: (3) RRUS32 B2 (Remove) - (3) Radio 4424 B25 (Replace)

Ground:

Remove (2) Nortel Cabinets, add (1) Battery cabinet, (1) enclosure to contain (3) BB6630 for L2500 and (1) BB6648 for N2500 on new slab

This facility was approved by the City of Bridgeport Zoning Board of Appeals in 1999, with no record of conditions that would restrict exempt modifications. Therefore this modification complies with the aforementioned approval.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. 16-50j-72(b)(2). In accordance with R.C.S.A. 16-50j-73, a copy of this letter is being sent to Joseph P. Ganim, Mayor of the City of Bridgeport, as well as the tower and property owner.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. 16-50j-72(b)(2).

1. The proposed modification will not result in an increase in the height of the existing structure

2. The proposed modifications will not require the extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.

5. The proposed modification will not cause a change or alteration in the physical or environmental characteristics of the site.

6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. 16-50j-72(b)(2).

Sincerely,

Elizabeth Jamieson Transcend Wireless 10 Industrial Ave., Suite 3 Mahwah, New Jersey 07430 860-605-7808 EJamieson@TranscendWireless.com

cc: Mayor Joseph P. Ganim- as elected official RCC Communications Corp/Bob Knapp - as tower and property owner Thomas F. Gill- Director of Office of Planning and Economic Development

Exhibit A Original Facility Approval

Exhibit B Property card

623 PINE ST

Location	623 PINE ST	Mblu	19/ 307/ 25/ /
Acct#	RK-0259405	Owner	KNAPP ANDREW & LILLIAN &
Assessment	\$224,850	Appraisal	\$321,210
PID	2504	Building Count	1

Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2017	\$251,840	\$69,370	\$321,210
	Assessment		
Valuation Year	Improvements	Land	Total
2017	\$176,290	\$48,560	\$224,850

Owner of Record

Owner	KNAPP ANDREW & LILLIAN &	Sale Price	\$90,000
Co-Owner	ROBERT KNAPP (SURV OF THEM)	Certificate	
Address	24 ROCKDALE RD	Book & Page	2838/ 116
	WEST HAVEN, CT 06516	Sale Date	09/24/1990

Ownership History

Ownership History					
Owner Sale Price Certificate Book & Page Sale Date					
KNAPP ANDREW & LILLIAN &	\$90,000		2838/ 116	09/24/1990	

Building Information

Building 1 : Section 1

Field	Description			
Building Attributes				
Less Depreciation:	\$201,840			
Replacement Cost				
Building Percent Good:	85			
Replacement Cost:	\$237,462			
Living Area:	2,625			
Year Built:	1964			

STYLE	Telephone Bldg
MODEL	Ind/Comm
Grade:	Above Ave
Stories:	1
Occupancy:	1
Exterior Wall 1:	Concr/CinderBl
Exterior Wall 2:	
Roof Struct:	Flat
Roof Cover:	T+G/Rubber
Interior Wall 1:	Minim/Masonry
Interior Wall 2:	
Interior Floor 1:	Concr-Finished
Interior Floor 2:	
Heating Fuel:	Gas
Heating Type:	Forced Air
АС Туре:	Central
Bldg Use:	Industrial Mdl 96
Ttl Rooms:	
Ttl Bedrms:	00
Ttl Baths:	0
Ttl Half Baths:	0
Ttl Xtra Fix:	0
1st Floor Use:	
Heat/AC:	Heat/Ac Pkgs
Frame Type:	Masonry
Baths/Plumbing:	Average
Ceiling/Wall:	Ceil & Walls
Rooms/Prtns:	Average
Wall Height:	14

Building Photo



(http://images.vgsi.com/photos2/BridgeportCTPhotos//\00\08\99

Building Layout



(http://images.vgsi.com/photos2/BridgeportCTPhotos//Sketches/

Building Sub-Areas (sq ft)			<u>Legend</u>
Code	Description	Gross Area	Living Area
BAS	First Floor	2,625	2,625
		2,625	2,625

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Extra Features

	Extra Features	Legend
No Data for Extra Features		
Land		
Land Use	Land Line Valuation	
Use Code 300	Size (Acres) 0.09	

DescriptionIndustrial Mdl 96ZoneILINeighborhoodINDAlt Land ApprNoCategoryIndustrial Mdl 96

Frontage	0
Depth	0
Assessed Value	\$48,560
Appraised Value	\$69,370

Outbuildings

	Outbuildings				Legend	
Code	Description	Sub Code	Sub Description	Size	Value	Bldg #
TWR	Tower			250 LF	\$50,000	1

Valuation History

Appraisal				
Valuation Year	Improvements	Land	Total	
2017	\$251,840	\$69,370	\$321,210	
2016	\$251,840	\$69,370	\$321,210	
2015	\$251,840	\$69,370	\$321,210	

Assessment				
Valuation Year	Improvements	Land	Total	
2017	\$176,290	\$48,560	\$224,850	
2016	\$176,290	\$48,560	\$224,850	
2015	\$176,290	\$48,560	\$224,850	

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Exhibit C Construction Drawings

PROJECT DESCRIPTION

T-MOBILE IS PROPOSING TO REMOVE (1) EXISTING AIR 21 PANEL ANTENNA AND REPLACE WITH (1) PROPOSED AIR6449 PANEL ANTENNA FOR POSITION 1 AT EACH SECTOR. (1) EXISTING RRUS 32 B2 TO BE REMOVED AND REPLACED WITH (1) RADIO 4424 B25 AT POSITION 4 FOR EACH SECTOR. (1) PROPOSED SDX1926Q-43 DIPLEXER TO BE INSTALLED AT POSITION 4 FOR EACH SECTOR. (1) EXISTING TWIN STYLE 1B AWS TMA TO BE RELOCATED TO POSITION 4 FOR EACH SECTOR.

(12) EXISTING T-MOBILE 1-5/8" COAX LINES TO BE REMAIN, (6) EXISTING 1-5/8" COAX LINES TO BE REMOVED. (4) EXISTING 6X12 HYBRIDS LINES TO REMAIN, (3) PROPOSED 6X12 HYBRID CABLES TO BE INSTALLED.

(2) EXISTING T-MOBILE NORTEL S12000 EQUIPMENT CABINETS TO BE REMOVED AND REPLACED WITH (1) B160 CABINET AND (1) 6160 CABINET.

A TOTAL OF (3) ANTENNAS REPLACED, (3) RRUS REPLACED, (3) DIPLEXERS INSTALLED, AND (3) TMAS RELOCATED.



_AST PLOTTED: Monday, 20-July-2020, 13:22 2: \Users\Engineer\Desktop\Bridgeport\CAD



623 PINE STREET BRIDGEPORT, CT 06605 SITE ID: CT11014B

DRAWING INDEX				
SHEET	SHEET TITLE			
T—1	TITLE SHEET			
S-1	EXISTING SITE PLAN			
S-2	PROPOSED SITE PLAN			
S-3	TOWER ELEVATION			
A-1	ANTENNA PLAN AND DETAILS			
A-2	ANTENNA AND EQUIPMENT DETAILS			
G-1	GROUNDING DETAILS			
GN-1	GENERAL NOTES			
	SITE INF	ORMATION		
PROPERTY OV	NER: RADIO COMMUNICATIONS SERVICES 24 ROCKDALE ROAD WEST HAVEN CT 06516	LATITUDE:	41°9'56.7"N	
	WEST HAVEN, CT 00010	LONGITUDE:	73°13'0.0"W	
APPLICANT:	T-MOBILE NORTHEAST LLC 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002	POWER COMPANY:	TBD	
ARCHITECT/ ENGINEER:	KM CONSULTING ENGINEERS 262 UPPER FERRY ROAD EWING, NJ 08628	T-MOBILE CONTACT:	TBD	
SITE ADDRESS	S: 623 PINE STREET BRIDGEPORT, CT 06605	EXISTING/PROPOSED USE:	UNMANNED TELECOMMUNICATIONS FACILITY	
COUNTY:	FAIRFIELD			
GROUND ELEV	ATION: 11'			

	APPROVALS
LANDLORD:	
CHAIRPERSON:	
BOARD SECRETARY:	
BOARD ENGINEER:	
	Governor John Da
	C. P. MCCON
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CLIENT: Transcend Wireless 10 INDUSTRIAL AVE TEL: (201) 684–0055 MAHWAH, NJ 07430 FAX: (201) 684-0066 KM Consulting Engineers, Inc. Wireless Engineering and Project Management 262 UPPER FERRY RD. EWING, NEW JERSEY 08628 PHONE: (609) 538-0400 WEB PAGE: http://www.kmengr.com UNAUTHORIZED ALTERATION OR ADDITIONS TO A PLAN BEARING THE SEAL OF A LICENSED ENGINEER, LAND SURVEYOR, OR ARCHITECT IS A VIOLATION OF STATE LAW. COPIES FROM THE ORIGINAL OF THIS DOCUMENT WITHOUT A FACSIMILE OF THE SIGNATURE AND AN ORIGINAL OF THE STAMP OR EMBOSSED SEAL OF THE PROFESSIONAL ENGINEER, LAND SURVEYOR, AND/OR ARCHITECT SHALL NOT BE CONSIDERED VALID COPIES. MICHAEL L. BOHLINGER, PE CONNECTICUT PROFESSIONAL ENGINEER _ICENSE 7/20/20 REVISIONS 1 7/20/20 JTH REVISED AS PER COMMENT 1 7/14/20 JTH REVISED AS PER COMMENT NO. DATE: DRN.: DESCRIPTION: PROJECT PARTICIPANTS SITE ACQUISITION: SIGN OFF INITL. _____DATE: _____ RF ENGINEER.: SIGN OFF INITL. _____DATE: _____ CONSTR. SUPV.: SIGN OFF INITL. _____DATE: _____ A & E: KM CONSULTING ENGR.'S INC. P.C.: CHKD.: DRN.: DATE: MLB || JTH || 6/11/20 PROJECT NAME: BRIDGEPORT SITE ADDRESS: 623 PINE STREET BRIDGEPORT, CT 06605 DRAWING TITLE: TITLE SHEET DRAWING #: REV. #: SITE ID #: CT11014B 1-7 PROJECT #.: 180416.02 Bridgeport (CT11014B) CDs.dwg FILE NAME:

PINE STREET



SIGNAGE: EXTERIOR SIGNS ARE NOT PROPOSED EXCEPT AS REQUIRED BY THE FCC.

STORM WATER CONTROL: THE PROPOSED FACILITY WILL RESULT IN AN INSIGNIFICANT INCREASE IN STORM WATER RUNOFF. CONSEQUENTLY, NO WATER QUALITY CONTROL DEVICES ARE PROPOSED.

EXCAVATING.

PUBLIC USE.

NOTE:

GENERAL CONTRACTOR TO REFER TO THE STRUCTURAL ANALYSIS BY KM CONSULTING ENGINEERS, INC. DATED 7/7/20 AND EQUIPMENT INSTALLATION RECOMMENDATIONS PRIÓR TO COMMENCING CONSTRUCTION.

GENERAL NOTES:

LIGHTING: EXISTING FACILITY WILL MEET OR EXCEED ALL FAA AND FCC REGULATORY REQUIREMENTS.

GRADE: EXISTING GRADE WILL BE MAINTAINED FOR PROPOSED CONSTRUCTION.

UTLITIES: SANITARY SEWER SERVICES AND POTABLE WATER ARE NOT APPLICABLE PER THE USE. IF APPLICABLE, SUBCONTRACTOR SHALL LOCATE ALL UTLITIES PRIOR TO

DRIVEWAY: A DRIVEWAY PERMIT IS NOT REQUIRED FOR THIS PROJECT. THE PROJECT WILL NOT REQUIRE RIGHT OF WAY OR PROPERTY TO BE DEDICATED FOR

MISC: NO NOISE, SMOKE, DUST, VAPORS OR ODOR WILL RESULT FROM THIS PROJECT.

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NOTE:

GENERAL CONTRACTOR TO REFER TO THE STRUCTURAL



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REPLACEMENT OF (2) T-MOBILE EQUIPMENT CABINETS. (1) EXISTING CABINETS TO REMAIN.

NOTE:

GENERAL CONTRACTOR TO REFER TO THE STRUCTURAL ANALYSIS BY KM CONSULTING ENGINEERS, INC. DATED 7/7/20 AND EQUIPMENT INSTALLATION RECOMMENDATIONS PRIOR TO COMMENCING CONSTRUCTION.



SCALE: 1/16" = 1'-0"

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·
RAWING TITLE:
TOWER FLEVATION
TE ID #· [DRAWING #·] [REV #·
CT11014B
ROJECT #.: S-3 2
180416.02
LE NAME: Bridgeport (CT11014B) CDs.dwg



NOTE:

EXISTING ANTENNA SC SECTOR POSITION | MANUFACTURER MODEL AIR 21 B2A/B4P ERICSSON 1 ERICSSON AIR 3246 B66 2 EMPTY MOUNT 1 - 3 APXVAARR24 43-U-NA 4 RFS AIR 21 B2A/B4P ERICSSON 1 ERICSSON AIR 3246 B66 2 2 EMPTY MOUNT - 3 APXVAARR24 43-U-NA RFS 4 AIR 21 B2A/B4P ERICSSON 1 ERICSSON 2 AIR 3246 B66 3 EMPTY MOUNT - 3 RFS APXVAARR24 43-U-NA 4

		PRO	POSED ANTENNA SCHED	ULE	
SECTOR	POSITION	MANUFACTURER	MODEL	TMA/RRH	SIZE (HxWxD)
	1	ERICSSON	AIR 6449 B41		33.1"x20.6"x8.6"
	2	ERICSSON	AIR 3246 B66		58.1"x15.75"x9.4"
	3	EMPTY MOUNT			
1	4	RFS	APXVAARR24 43-U-NA20	RADIO 4424 B25 RADIO 4449 B71/B85 TWIN STYLE 1BX TMA SDX1926Q-43 DIXPLEXER	95.9"x24"x8.7"
	1	ERICSSON	AIR 6449 B41		33.1"x20.6"x8.6"
	2	ERICSSON	AIR 3246 B66		58.1"x15.75"x9.4"
	3	EMPTY MOUNT			
2	4	RFS	APXVAARR24 43-U-NA20	RADIO 4424 B25 RADIO 4449 B71/B85 TWIN STYLE 1BX TMA SDX1926Q-43 DIXPLEXER	95.9"x24"x8.7"
	1	ERICSSON	AIR 6449 B41		33.1"x20.6"x8.6"
	2	ERICSSON	AIR 3246 B66		58.1"x15.75"x9.4"
_	3	EMPTY MOUNT			
3	4	RFS	APXVAARR24 43-U-NA20	RADIO 4424 B25 RADIO 4449 B71/B85 TWIN STYLE 1BX TMA SDX1926Q-43 DIXPLEXER	95.9"x24"x8.7"

3 ANTENNA SPECIFICATION TABLE A-1

EXISTING MOUNTING PIPE —— B41 ANTENNA MOUNTED TO EXISTING MOUNTING PIPE (TYP)

> PROPOSED ANTENNA MOUNTING BRACKET

4 ANTENNA MOUNTING DETAIL A-1

NOTE: REFER TO THE FINAL RF DATA SHEET FOR FINAL ANTENNA CONFIGURATION

— EXISTING RFS APXVAARR24 43-U-NA20 ANTENNA, (1) PER SECTOR (TYP.), (3) TOTAL

- PROPOSED ERICSSON RRUS 4424 B25, (1) PER SECTOR

- EXISTING ERICSSON RADIO 4449 B71/B85 (1) PER SECTOR (TYP.), (3) TOTAL

GENERAL CONTRACTOR TO REFER TO THE STRUCTURAL ANALYSIS BY KM CONSULTING ENGINEERS, INC. DATED 7/7/20 AND EQUIPMENT INSTALLATION RECOMMENDATIONS PRIOR TO COMMENCING CONSTRUCTION.

HEDL	JLE	
	TMA/RRH	SIZE (HxWxD)
	TWIN STYLE 1B AWS TMA	55"x12"x7.9"
		58.1"x15.75"x9.4"
A20	RRUS 32 B2 RADIO 4449 B71/B85	95.9"X24"X8.7"
	TWIN STYLE 1B AWS TMA	55"x12"x7.9"
		58.1"x15.75"x9.4"
A20	RRUS 32 B2 RADIO 4449 B71/B85	95.9"X24"X8.7"
	TWIN STYLE 1B AWS TMA	55"x12"x7.9"
		58.1"x15.75"x9.4"
A20	RRUS 32 B2 RADIO 4449 B71/B85	95.9"X24"X8.7"
HEDI	JLE	
	TMA /RRH	SIZE (HxWxD)

SCALE:







Bridgeport (CT11014B) CDs.dwg FILE NAME:





Numbers of power pairs / fiber pairs		6/12
Material		plastic PPE black
Pulling force	radio end	2000 N (short-term during installation)
Temperature range	operation	–40 ℃ to +75 ℃
	installtion	–25 ℃ to +65℃
	fiber break-out cable	500 N
Cable retention force at	power break-out cable	500 N
enclosure	hybrid cable	2000 N
In average investigation	radio end	IP 68
ingress protection	base station	IP 65 (with protection tube)
IK class		IK 10
Flammability		UL94-V0
UV resistant		ISO 4892-2
Salt mist, IEC 61300-2- 26		96 h
Vibration, IEC 61300-2-1		10 – 500 Hz / 10 g
Shock, IEC 61300-2-9		100 g

Hybrid cable spe	cification
Jacket material	Heat, moisture, a
Temperature range	
Operating voltage	
Rated voltage	
Cable shielding	
Fiber optic	4.8 mm loo
Flame retardant	
UV resistant	
UL approved	

ERICSSON 6x12 HYBRID CABLE SPECS A-2 NOT TO SCALE



A-2 NOT TO SCALE



COLOR: GREY DIMENSIONS (HxWxD): 4.173" X 6.929" X 2.913" WEIGHT: 6.173 Ibs WITHOUT MOUNTING HARDWARE CONNECTOR: 4.3-10 FEMALE CONNECTORS

SDX1926Q-43 DIPLEXER DETAIL A-2 NOT TO SCALE





ERICSSON RBS6160 EQUIPMENT CABINET

ENCLOSURE: ALUMINUM DIMENSIONS (HxWxD): 63" X 25.6" X 25.6" WEIGHT: 188 Ibs (EXCLUDES EQUIPMENT) WEATHER TIGHTNESS: NEMA TYPE 3R ERICSSON RBS6160 EQUIPMENT CABINET

A-2 NOT TO SCALE

standard cable) and sunlight resistant polyvinyl chloride (PVC) jacket -40°F to + 158°F (-40°C to + 75°C) 48VDC 0,6kV/1kV (1.2kV) copper foil > 100% coverage ose-tube cable with up to 24 fibers single mode

IEC 60332-1-2:2004 Yes, according IEC 68-2-5 Yes

SDX1926Q-43 DIPLEXER



ERICSSON B160 EQUIPMENT CABINET

ENCLOSURE: ALUMINUM DIMENSIONS (HxWxD): 63" X 25.6" X 25.6" WEIGHT: 188 Ibs (EXCLUDES EQUIPMENT) WEATHER TIGHTNESS: NEMA TYPE 3R

6 ERICSSON B160 EQUIPMENT CABINET

A-2 NOT TO SCALE









SCALE: N.T.S.

6 AN G-1

ITENNA	CABLE	GROUI	NDING
	SC	ALE:	N.T.S.



GROUNDING NOTES

- 1. THE SUBCONTRACTOR SHALL REVIEW AND INSPECT THE EXISTING FACILITY GROUNDING SYSTEM AND LIGHTNING PROTECTION SYSTEM (AS DESIGNED AND INSTALLED) FOR STRICT COMPLIANCE WITH THE NEC (AS ADOPTED BY THE AHJ), THE SITE-SPECIFIC (UL, LPI, OR NFPA) LIGHTING PROTECTION CODE, AND GENERAL COMPLIANCE WITH TELCORDIA AND TIA GROUNDING STANDARDS. THE SUBCONTRACTOR SHALL REPORT ANY VIOLATIONS OR ADVERSE FINDINGS TO THE CONTRACTOR FOR RESOLUTION.
- 2. ALL GROUNDING ELECTRODE SYSTEMS (INCLUDING TELECOMMUNICATIONS, RADIO, LIGHTNING PROTECTION, AND AC POWER GEC"S) SHALL BE BONDED TOGETHER, AT OR BELOW GRADE, BY TWO OR MORE COPPER BONDING CONDUCTORS IN ACCORDANCE WITH THE NEC.
- 3. THE SUBCONTRACTOR SHALL PERFORM IEEE FALL-OF-POTENTIAL RESISTANCE TO EARTH TESTING (PER IEEE 1100 AND 81) FOR NEW GROUND ELECTRODE SYSTEMS. THE SUBCONTRACTOR SHALL FURNISH AND INSTALL SUPPLEMENTAL GROUND ELECTRODES AS NEEDED TO ACHIEVE A TEST RESULT OF 5 OHMS OR LESS.
- 4. METAL RACEWAY SHALL NOT BE USED AS THE NEC REQUIRED EQUIPMENT GROUND CONDUCTOR. STRANDED COPPER CONDUCTORS WITH GREEN INSULATION, SIZED IN ACCORDANCE WITH THE NEC, SHALL BE FURNISHED AND INSTALLED WITH THE POWER CIRCUITS TO BTS EQUIPMENT.
- 5. EACH BTS CABINET FRAME SHALL BE DIRECTLY CONNECTED TO THE MASTER GROUND BAR WITH GREEN INSULATED SUPPLEMENTAL EQUIPMENT GROUND WIRES, 6 AWG STRANDED COPPER OR LARGER FOR INDOOR BTS, 2 AWG STRANDED COPPER FOR OUTDOOR BTS.
- 6. EXOTHERMIC WELDS SHALL BE USED FOR ALL GROUNDING CONNECTIONS BELOW GRADE.
- 7. APPROVED ANTIOXIDANT COATINGS (I.E. CONDUCTIVE GEL OR PASTE) SHALL BE USED ON ALL COMPRESSION AND BOLTED GROUND CONNECTIONS.
- 8. ICE BRIDGE BONDING CONDUCTORS SHALL BE EXOTHERMICALLY BONDED OR BOLTED TO THE BRIDGE AND THE TOWER GROUND BAR.
- 9. ALUMINUM CONDUCTOR OR COPPER CLAD STEEL CONDUCTOR SHALL NOT BE USED FOR GROUNDING CONNECTIONS.
- 10. MISCELLANEOUS ELECTRICAL AND NON-ELECTRICAL METAL BOXES, FRAMES AND SUPPORTS SHALL BE BONDED TO THE GROUND RUNG, IN ACCORDANCE WITH THE NEC.
- 11. METAL CONDUIT SHALL BE MADE ELECTRICALLY CONTINUOUS WITH LISTED BONDING FITTING OR BY BONDING ACROSS THE DISCONTINUITY WITH 6 AWS COPPER WIRE UL APPROVED GROUNDING TYPE CONDUIT CLAMPS.

ELECTRICAL AND GROUNDING NOTES

- 1. CONNECTIONS TO MGB SHALL BE ARRANGED IN THREE MAIN GROUPS: SURGE PRODUCERS (COAXIAL CABLE GROUND KITS, TELCO AND POWER PANEL GROUNDS); GROUNDING ELECTRODE OR BUILDING STEEL; NON-SURGING OBJECTS (EGB GROUND IN BTS UNIT).
- 2. CONNECTIONS TO GROUND BARS SHALL BE MADE WITH TWO HOLE COMPRESSION TYPE COPPER LUGS. APPLY OXIDE INHIBITING COMPOUND TO ALL LOCATIONS.
- 3. APPLY OXIDE INHIBITING COMPOUND TO ALL COMPRESSION TYPE GROUND CONNECTIONS.
- 4. BOND ANTENNA MOUNTING BRACKETS, COAXIAL CABLE GROUND KITS, AND ALNA TO EGB PLACED NEAR THE ANTENNA LOCATION.
- 5. BOND ANTENNA EGB'S AND MGB TO WATER MAIN
- 6. TEST COMPLETED GROUND SYSTEM AND RECORD RESULTS FOR PROJECT CLOSE-OUT DOCUMENTATION.
- 7. BOND ANY METAL OBJECTS WITHIN 7 FEET OF PROPOSED EQUIPMENT OR CABINET TO MASTER GROUND BAR.
- 8. VERIFY PROPOSED SERVICE UPGRADE WITH LOCATION UTILITY COMPANY PRIOR TO CONSTRUCTION.

GENERAL NOTES

1. FOR THE PURPOSE OF CONSTRUCTION DRAWINGS, THE FOLLOWING DEFINITIONS SHALL APPLY.

CONTRACTOR - TRANSCEND WIRELESS SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) owner – t-mobile

2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.

3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL JURISDICTIONAL CODES, ORDINANCES, AND APPLICABLE REGULATIONS.

4. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.

5. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.

6. "KITTING LIST" SUPPLIED WITH THE BID PACKAGE IDENTIFIES ITEMS THAT WILL BE SUPPLIED BY THE CONTRACTOR. ITEMS NOT INCLUDED IN THE BILL OF MATERIALS AND KITTING LIST SHALL BE SUPPLIED BY THE SUBCONTRACTOR.

7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.

8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSED AN ALTERNATIVE INSTALLATION SPACE FOR APPROVAL BY THE CONTRACTOR.

9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER AND TI CABLES, GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWINGS. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY. SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR.

10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF OWNER.

11. SUBCONTRACTORS SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY. ANTENNAS REMOVED SHALL BE RETURNED TO THE OWNER'S DESIGNATED LOCATION.

12. SUBCONTRACTOR SHALL LEAVE PREMISED IN CLEAN CONDITION.

13. ALL CONCRETE REPAIR WORK SHALL BE DONE IN ACCORDANCE WITH AMERICAN CONCRETE INSTITUTE (ACI) 301.

14. ANY NEW CONCRETE NEEDED FOR THE CONSTRUCTION SHALL BE AIR-ENTRAINED AND SHALL HAVE 4000PSI STRENGTH AT 28 DAYS. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH ACI 318 CODE REQUIREMENTS.

- USING A COMPATIBLE ZINC RICH PAINT.
- SITES."
- CONSTRUCTION.
- PERIODS AFTER MIDNIGHT.
- DANGEROUS EXPOSURE LEVELS.
- 20. APPLICABLE BUILDING CODES:

BUILDING CODE: 2018 CONNECTICUT STATE BUILDING CODE. ELECTRICAL CODE: REFER TO ELECTRICAL DRAWINGS LIGHTNING CODE: REFER TO ELECTRICAL DRAWINGS

SUBCONTRACTOR'S WORK SHALL COMPLY WITH THE LATEST EDITION OF THE FOLLOWING STANDARDS:

AMERICAN CONCRETE INSTITUTE (ACI) 318: BUILDING CODE REQUIREMENTS FOR STRUCTURAL CONCRETE

AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC)

MANUAL OF STEEL CONSTRUCTION, ASD, 14TH EDITION

ANSI/TIA-222-G, STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND ANTENNA SUPPORTING STRUCTURES

FOR ANY CONFLICTS BETWEEN SECTIONS OF LISTED CODES AND STANDARDS REGARDING MATERIAL, METHOD OF CONSTRUCTION, OR OTHER REQUIREMENTS, THE MORE RESTRICTIVE REQUIREMENT SHALL GOVERN. WHERE THERE IS CONFLICT BETWEEN A GENERAL REQUIREMENT AND A SPECIFIC REQUIREMENT, THE SPECIFIC REQUIREMENT SHALL GOVERN.

15. ALL STRUCTURAL STEEL WORK SHALL BE DETAILED, FABRICATED, AND ERECTED IN ACCORDANCE WITH AISC SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE ASTM A36 (Fy = 36 ksi) UNLES OTHERWISE NOTED. PIPES SHALL BE ASTM A53 TYPE 3 (Fy = 36 ksi). ALL STEEL EXPOSED TO WEATHER SHALL BE HOT DIPPED GALVANIZED. TOUCHUP ALL SCRATCHES AND OTHER MARKS IN THE FIELD AFTER STEEL IS ERECTED

16. CONSTRUCTION SHALL COMPLY WITH UMTS SPECIFICATIONS AND "GENERAL CONSTRUCTION SERVICES FOR CONSTRUCTION OF T-MOBILE

17. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR WITH ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH

18. THE EXISTING CELL SITE IS IN FULL COMMERCIAL OPERATIONS. ANY CONSTRUCTIN WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR. ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE WINDOW USUALLY IN LOW TRAFFIC

19. SINCE THE CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE ADVISED TO BE WORN TO ALERT OF ANY

SUBCONTRACTOR'S WORK SHALL COMPLY WITH ALL APPLICABLE NATIONAL, STATE, AND LOCAL CODES AS ADOPTED BY THE LOCAL AUTHORITY HAVING JURISDICTION (AHJ) FOR THE LOCATION. THE EDITION OF THE AHJ ADOPTED CODES AND STANDARDS IN EFFECT ON THE DATE OF THE CONTRACT AWARD SHALL GOVERN THE DESIGN.



Exhibit D Structural Analysis Report

STRUCTURAL ANALYSIS REPORT

for

T • • Mobile •

Transcend Wireless 10 Industrial Ave., Suite 3 Mahwah, NJ 07430

Bridgeport (CT11014B) KM No. 180416.02

250' Self-Support Tower 623 Pine Street Bridgeport, CT 06605 41.16573, -73.21666

Prepared By:



KM CONSULTING ENGINEERS, INC.

262 Upper Ferry Road Ewing, NJ 08628 Ph: (609) 538-0400 www.kmengr.com

July 7, 2020

Prepared to ANSI/TIA-222-G-4 December 2014 Structural Standards for Antenna Supporting Structures and Antennas

TABLE OF CONTENTS

SECTION	PAGE
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2.0 TOWER INVENTORY	4
3.0 COMMENTARY	6
4.0 ANALYSIS PROCEDURE	7
5.0 TOWER ANALYSIS RESULTS	8
6.0 RECOMMENDATIONS	9
7.0 APPENDIX	10
Load Case No. 1: Existing tower superstructure with existing inventory an	d proposed T-

Mobile installation.

1.0 EXECUTIVE SUMMARY

Structure

Owner:	Radio Communications Tower
Location:	623 Pine Street Bridgeport, CT 06605 41.16573, -73.21666
Manufacturer:	Rohn Eng. File No. 37679AE dated 7/1/98

Equipment

Existing tower inventory plus the proposed installation are detailed in Section 2.0 "Tower Inventory."

Synopsis

<u>Load Case No. 1:</u> The existing tower superstructure with the current inventory and proposed T-Mobile installation.

The existing tower superstructure and base foundation have sufficient capacity and therefore meet the current ANSI/TIA-222-G design standards. The tower superstructure is rated at 95.0% and the foundation is rated at 64.5%.

2.0 TOWER INVENTORY

DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
yaggi in radom	256	mounting frames w/stable bar	138
Beacon	256	(MetroPCS)	
Omni antenna	256	mounting frames w/stable bar	138
Omni antenna	256	(MetroPCS)	
Omni antenna	256	VHLP1-23-2WH (Clearwire)	121
Omni antenna	256 - 239	VHLP1-23-2WH (Clearwire)	121
Top Platform	256	VHLP2.5-11-4WH (Clearwire)	121
Omni antenna	248 - 238	Panel Antenna w/mount pipe	118
mounting frames w/stable bar (T-Mobile)	180	Panel Antenna w/mount pipe (Clearwire)	118
mounting frames w/stable bar (T-Mobile)	180	Panel Antenna w/mount pipe (Clearwire)	118
mounting frames w/stable bar (T-Mobile)	180	800 10736V01 (Verizon)	110
AIR 3246 B66 (T-Mobile)	180	800 10736V01 (Verizon)	110
AIR 3246 B66 (T-Mobile)	180	800 10736V01 (Verizon)	110
AIR 3246 B66 (T-Mobile)	180	(2) APL-866513-42T9 (Verizon)	110
APXVAARR24 43-U-NA20 (T-Mobile)	180	(2) APL-866513-42T6 (Verizon)	110
APXVAARR24 43-U-NA20 (T-Mobile)	180	(2) APL-866513-42T9 (Verizon)	110
APXVAARR24 43-U-NA20 (T-Mobile)	180	Rohn 6'x15' Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Rohn 6'x15' Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Rohn 6'x15' Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Distribution Box (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	GPS antenna (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	(2) HBXX-6516DS-A2M (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	2x60 PCS RRH B25 (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	2x60 PCS RRH B25 (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	Distribution Box (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX19260-43 (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX1926Q-43 (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX1926Q-43 (T-Mobile)	180	(2) HBXX-6516DS-A2M (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	(2) HBXX-6516DS-A2M (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	2x60 PCS RRH B25 (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	TV 65 antenna	100
mounting frames w/stable bar	138	4' Side Arm	100
(MetroPCS)	150	TV 65 antenna	100

Proposed T-Mobile Installation:

*(3) AIR6449 B41 panel antennas @ 180' AGL

- *(3) Radio 4424 B25's @ 180' AGL *(3) SBX1926Q-43 diplexers @ 180' AGL
- *(3) 6x12 hybrid cables up to 180' AGL
- *removal of (3) AIR 21 B2A/B4P panel antennas @ 180' AGL
- *removal of (3) RRUS 32 B2's @ 180' AGL
- *removal of (6) 1-5/8" coax lines up to 180' AGL

3.0 COMMENTARY

Our scope of work is to determine if the existing structure is capable of withstanding the additional stresses/forces imposed by the installation of the proposed T-Mobile equipment noted in the tower inventory. The tower is a 250' tall Rohn self-support tower with a triangular platform located at the top.

Tower member sizes, layout and foundation information was taken from previous structural analysis by KM Consulting Engineers, Inc. (KMCE) dated 1/21/19. Existing antenna inventory and coax cable layout was also taken from the above mentioned analysis. Proposed equipment was obtained from a draft T-Mobile RFDS dated 6/2/20 and by correspondence with the client.

The following report will provide analytical calculations and commentary regarding the capacity of the proposed tower and subsequent recommendations.

4.0 ANALYSIS PROCEDURE

KM Consulting Engineers, Inc. carried out their structural analysis by correlating field inspection and tower member data into proprietary software designed specifically for communication tower analysis.

These programs run in conjunction with the guidelines set down in the ANSI/TIA-222-G Standard entitled "Structural Standards for Antenna Supporting Structures and Antennas."

The existing tower is analyzed by placing wind forces on the structure in 30° positional increments around the tower (i.e. wind pressure directly onto the tower corners, faces and parallel to the faces). This enables the user to "create" a three-dimensional representation, yielding results for worst case scenarios. In effect, the production of these results allows the user to study the structural integrity of the tower when influenced by wind forces from any direction.

The proceeding report includes analysis for the tower with the addition of antennas in the scenarios stated. For clarity, the analysis shall include worst case loadings and a typical elevation view with maximum foundation loads tabulated.

Should the client require to be furnished with a full copy of our analysis, we will gladly do so.

Codes and Standards

ACI - American Concrete Institute - Building Code Requirements for Structural Concrete (ACI 318-14), 2014

AISC - American Institute of Steel Construction - Manual of Steel Construction, 14th edition, 2011

TIA - Telecommunications Industry Association – ANSI/TIA-222-G-4 Structural Standards for Antenna Supporting Structures and Antennas, 2014

CSBC - Connecticut State Building Code 2018

5.0 TOWER ANALYSIS RESULTS

The tower was analyzed for the inventory detailed in Section 2.0 "Tower Inventory".

The basic wind speed of 97 MPH with no radial ice in accordance with ANSI/TIA-222-G is taken from Appendix N in the 2018 Connecticut State Building Code for the nominal design wind speed for the municipality of Bridgeport, CT. The basic wind speed of 50 MPH concurrent with ³/₄" design ice thickness is taken from the ANSI/TIA-222-G listing applicable for Fairfield County, CT. Additional criteria include Structure Class II, Exposure Category C, and Topographic Category 1.

Load Case No. 1: Existing inventory and the proposed T-Mobile installation includes the additions of (3) existing AIR6449 B41 panel antennas, (3) Radio 4424 B25's, (3) SBX1926Q-43 diplexers, and (3) 6x12 hybrid cables, and the removal of (3) AIR 21 B2A/B4P panel antennas, (3) RRUS 32 B2's, and (6) 1-5/8" coax lines.

The existing tower superstructure and base foundation have sufficient capacity and therefore meet the current ANSI/TIA-222-G design standards. The tower superstructure is rated at 95.0% and the foundation is rated at 64.5%.

Table 1. Base Foundation Rating

Force	Actual (kip.ft)	Allowable (kip-ft)	Capacity
Overturning Moment	11,290	17,504	64.5%

6.0 RECOMMENDATIONS

Further to our calculations, we conclude that the existing tower superstructure and base foundation have adequate capacity and therefore meet the current ANSI/TIA-222-G design standards. The tower and foundation are acceptable to support the proposed T-Mobile installation.

Please do not hesitate to contact our office with any questions or concerns regarding this report.

Sincerely, **KM CONSULTING ENGINEERS, INC.**

Domenic Aversa, PE Project Manager



7.0 APPENDIX

LOAD CASE 1



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
yaggi in radom	256	mounting frames w/stable bar	138
Beacon	256	(MetroPCS)	
Omni antenna	256	mounting frames w/stable bar	138
Omni antenna	256	(MetroPCS)	
Omni antenna	256	VHLP1-23-2WH (Clearwire)	121
Omni antenna	256 - 239	VHLP1-23-2WH (Clearwire)	121
Top Platform	256	VHLP2.5-11-4WH (Clearwire)	121
Omni antenna	248 - 238	Panel Antenna w/mount pipe	118
mounting frames w/stable bar (T-Mobile)	180	Panel Antenna w/mount pipe	118
mounting frames w/stable bar (T-Mobile)	180	Panel Antenna w/mount pipe	118
mounting frames w/stable bar	180	800 10736\/01 (\/erizon)	110
(T-Mobile)		800 10736\/01 (\/erizon)	110
AIR 3246 B66 (T-Mobile)	180	800 10736\/01 (Verizon)	110
AIR 3246 B66 (T-Mobile)	180	(2) API 966512 42T0 (Verizon)	110
AIR 3246 B66 (T-Mobile)	180	(2) APL 966512 42T6 (Verizon)	110
APXVAARR24_43-U-NA20 (T-Mobile)	180	(2) APL 966542 42T0 (Verizon)	110
APXVAARR24_43-U-NA20 (T-Mobile)	180	(2) APL-866513-4219 (Verizon)	110
APXVAARR24_43-U-NA20 (T-Mobile)	180	Ronn 6 x15 Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Ronn 6 x15 Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Rohn 6'x15' Boom Gate (Verizon)	110
AIR6449 B41 (T-Mobile)	180	Distribution Box (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4449 B71/B85 (T-Mobile)	180	2x60 700 RRH B13 (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	GPS antenna (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	(2) HBXX-6516DS-A2M (Verizon)	110
Radio 4424 B25 (T-Mobile)	180	2x60 PCS RRH B25 (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	2x60 PCS RRH B25 (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	Distribution Box (Verizon)	110
Twin style 1B TMA (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX1926Q-43 (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX1926Q-43 (T-Mobile)	180	2x60 AWS RRH (Verizon)	110
SBX1926Q-43 (T-Mobile)	180	(2) HBXX-6516DS-A2M (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	(2) HBXX-6516DS-A2M (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	2x60 PCS RRH B25 (Verizon)	110
(2) MetroPCS Antenna (MetroPCS)	138	TV 65 antenna	100
mounting frames w/stable bar	138	4' Side Arm	100
(MetroPCS)		TV 65 antenna	100

SYMBOL LIST							
MARK		SIZE		MARK		SIZE	1
A	ROHN 3 STD			С	L3x3x1/4		
В	L1 3/4x1 3/4x3/16						
	MATERIAL STRENGTH						
GRADE	E Fy		Fu	GRADE	E Fy		Fu
A572-50	50 ksi	65 k	si				



 \triangle

Bridgeport LC1		
Project: 250' Rohn Self Suppo	ort Tower	
Client: Transcend Wireless	Drawn by: DCA	App'd:
Code: TIA-222-G	Date: 07/07/20	Scale: NTS
Path:		Dwg No. F-1



	SYMBOL LIST						
MARK		SIZE		MARK		SIZ	E
A	ROHN 3 STD			С	L3x3x1/4		
В	L1 3/4x1 3/4x3/1	6					
	MATERIAL STRENGTH						
GRAD	E Fy		Fu	GRAD	E	Fy	Fu

TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.

2. Tower designed for Exposure C to the TIA-222-G Standard. 3.

65 ksi

Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard. 4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to

increase in thickness with height. Deflections are based upon a 60 mph wind.

5. Tower Structure Class II.

50 ksi

6. 7. Topographic Category 1 with Crest Height of 0.00 ft

8. TOWER RATING: 95%

A572-50



50 mph WIND - 0.7500 in ICE

ALL REACTIONS ARE FACTORED

AXIAL 78315 lb MOMENT 11291341 lb-ft

TORQUE 155391 lb-ft REACTIONS - 97 mph WIND



^{lob:} Bridgeport LC1					
Project: 250' Rohn Self Suppo	ort Tower				
Client: Transcend Wireless	Drawn by: DCA	App'd:			
^{Code:} TIA-222-G	Date: 07/07/20	Scale: NTS			
Path:		Dwg No. F-1			

Feed Line Distribution Chart

App In Face

Flat

Round

8' - 256'

App Out Face

Truss Leg





Bridgeport LC1		
Project: 250' Rohn Self Supp	ort Tower	
Client: Transcend Wireless	Drawn by: DCA	App'd:
^{Code:} TIA-222-G	Date: 07/07/20	Scale: NTS
Path:	4D))En nine enine al Dridene est I C4 es	Dwg No. E-7





^{ob:} Bridgeport LC1		
Project: 250' Rohn Self Suppo	ort Tower	
Client: Transcend Wireless	Drawn by: DCA	App'd:
Code: TIA-222-G	Date: 07/07/20	Scale: NTS
Path:		Dwg No. E-7

Stress Distribution Chart 8' - 256' > 100% 90%-100% 75%-90% 50%-75% < 50% Overstress</td>





^{Job:} Bridgeport LC1						
Project: 250' Rohn Self Support Tower						
Client: Transcend Wireless	Drawn by: DCA	App'd:				
^{Code:} TIA-222-G	Date: 07/07/20	Scale: NTS				
Path:		Dwg No. F-8				

tnxT o

KM Consulting Engineers, Inc 262 Upper Ferry Road Ewing, NJ 08628 Phone: (609) 538-0400 FAX:

	Job		Page
ower		43 of 44	
Engineers, Inc. Ferry Road	Project	250' Rohn Self Support Tower	Date 12:10:50 07/07/20
VJ 08628 9) 538-0400 X:	Client	Transcend Wireless	Designed by DCA

Section Capacity Table

Section	Elevation	Component	Size	Critical Florent	P	ϕP_{allow}	% Canacity	Pass Fail
No.	<u></u>	Type	DOMNA (TTD	Liemeni	10	10	cupacity 7.2	- T uii
TI	256 - 248	Leg	ROHN 3 STD	3	-4732.89	88543.60	5.3	Pass
		Diagonal	L1 3/4x1 3/4x3/16	8	-1856.19	/836.45	23.7	Pass
TO	249 229	Top Girt	L3x3x1/4	4	-6//.51	19/05.80	3.4	Pass
12	248 - 228	Leg	ROHN 3 EH	21	-2/5/5.00	11911/.00	23.1	Pass
		Diagonal	L2x2x1/4	23	-3461.67	15423.50	22.4 29.5 (b)	Pass
Т3	228 - 208	Leg	ROHN 4 EH	54	-62342.70	183589.00	34.0	Pass
10	220 200	Diagonal	$L_{2x}^{2x1/4}$	59	-5027.34	16011.80	31.4	Pass
		Diugonui	EEAEAT)	57	5027.51	10011.00	41.1 (b)	1 455
T4	208 - 188	Leg	ROHN 5 EH	87	-85982.10	254372.00	33.8	Pass
		Diagonal	L2x2x1/4	89	-3330.49	9442.17	35.3	Pass
T5	188 - 168	Leg	ROHN 6 EH	114	-112684.00	343100.00	32.8	Pass
		Diagonal	$L_2 \frac{1}{2x^2} \frac{1}{2x^{1/4}}$	116	-6283.06	11996.10	52.4	Pass
T6	168 - 148	Leg	ROHN 6 EH	135	-146112.00	343100.00	42.6	Pass
10	100 110	Diagonal	$L_{3x}_{3x}_{1/4}$	137	-7668.72	16173.10	47.4	Pass
		Diagonai		107		101/0110	53.6(h)	1 400
Т7	148 - 128	Leg	ROHN 6 EH	156	-182000.00	343092.00	53.0	Pass
17	110 120	Diagonal	I 3x3x1/4	158	-9395 99	12584 10	74 7	Pass
Т8	128 - 108	Lea	ROHN 8 EHS	177	-219205.00	386381.00	567	Pass
10	120 100	Diagonal	I AvAv3/8	179	-13060.00	30/186 60	12.8	Pass
		Diagonai	LHAHAJ/0	177	-15000.00	30480.00	60.7 (b)	1 435
Т9	108 - 88	Leg	ROHN 8 FH	192	-266591.00	505517.00	52 7	Pass
17	100 00	Diagonal	I 4x4x0 31	192	-16460.90	21205 70	77.6	Pass
		Diagonai	247470.51	174	10400.90	21203.70	78 9 (b)	1 435
т10	88 - 68	Leg	P10x 5	207	-319868.00	668659.00	17.8	Pass
110	00-00	Diagonal	I 5x5x3/8	207	10073 00	43484 70	45.0	Dass
		Diagonai	L3X3X3/8	209	-19975.90	43464.70	43.9 82.0 (b)	1 455
T11	68 18	Leg	P10x 5	222	376841.00	668663.00	56.4	Dase
111	08 - 48	Diagonal	I 10X.J	222	-370841.00	27204.00	50.4	Doce
		Diagonai	LJXJXJ/0	224	-22730.10	37294.00	90.1 (b)	F 888
T12	48 - 28	Leg	P10x.5	237	-434722.00	668640.00	65.0	Pass
	.0 20	Diagonal	L5x5x3/8	239	-25514.30	31978.80	79.8	Pass
T13	28 - 8	Leg	P10x 5	2.52	-452442.00	711505.00	63.6	Pass
	20 0	Diagonal	ROHN 3 STD	259	-36105.70	38509.50	93.8	Pass
		Top Girt	ROHN 3 STD	253	-21664.80	31030.70	69.8	Pass
		Redund Horz 1	ROHN 1.5 STD	233	-7851.80	13888.30	56.5	Pass
		Bracing		271	/ 00 1.00	10000.00	20.2	1 435
		Redund Diag 1	ROHN 1.5 STD	267	-6859.68	7217.78	95.0	Pass
		Bracing		207	0007.00	/21/./0	22.0	1 435
		Redund Hin 1	ROHN 1 5 STD	278	-115.66	12002.20	1.0	Pass
		Bracing	Rom 1.5 51D	270	115.00	12002.20	1.0	1 435
		Redund Hin Diagonal	ROHN 1.5 STD	279	-68 66	2211.89	3.1	Pase
		1 Bracing	KOIII I.J SID	21)	-00.00	2211.09	5.1	1 455
		Inner Bracing	ROHN 3 STD	280	-375 25	29213 70	17.6	Pass
		miler Dracing	KOIII J SID	200	-313.23	27213.70	Summary	1 435
						$L_{eq}(T12)$	65 0	Dage
						$1e\sigma(112)$	62.0	Pass

Leg (T12) Diagonal (T13) Top Girt (T13) 93.8 Pass 69.8 Pass Redund 56.5 Pass Horz 1 Bracing (T13) Redund 95.0 Pass Diag 1 Bracing

Arrest Tools on	Job		Page
<i>inx1ower</i>		44 of 44	
KM Consulting Engineers Inc	Project		Date
262 Upper Ferry Road		250' Rohn Self Support Tower	12:10:50 07/07/20
Ewing, NJ 08628	Client		Designed by
Phone: (609) 538-0400 FAX:		Transcend Wireless	DCA

Section	Elevation	Component	Size	Critical	Р	ϕP_{allow}	%	Pass
No.	ft	Type		Element	lb	lb	Capacity	Fail
						(T13)		
						Redund Hip	1.0	Pass
						1 Bracing		
						(T13)		
						Redund Hip	3.1	Pass
						Diagonal 1		
						Bracing		
						(T13)		
						Inner	17.6	Pass
						Bracing		
						(T13)		
						Bolt Checks	90.1	Pass
						RATING =	95.0	Pass

Program Version 8.0.7.4 - 5/11/2020 File:I:/Doug/Transcend Wireless/Bridgeport (CT11014B)/Engineering/Bridgeport LC1.eri


KM Consulting Engineers, Inc. 262 Upper Ferry Road Ewing, NJ 08628



Transcened Wireless Bridgeport (CT11014B) KM #181110.02

Exhibit E Mount Analysis



Centered on Solutions^{5M}

Structural Analysis Report

Antenna Mount Analysis

T-Mobile Site #: CT11014B

623 Pine Street Bridgeport, CT 06605

Centek Project No. 20074.32

Date: June 8, 2020

Max Stress Ratio = 65.0%

Prepared for:

T-Mobile USA 35 Griffin Road Bloomfield, CT 06002



CENTEK Engineering, Inc. Structural Analysis – Mount Analysis T-Mobile Site Ref. ~ CT11014B Bridgeport, CT June 8, 2020

Table of Contents

SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION

SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT

SECTION 3 - REFERENCE MATERIALS (NOT INCLUDED WITHIN REPORT)

• RF DATA SHEET, DATED 6/2/2020



June 8, 2020

Mr. Dan Reid Transcend Wireless 10 Industrial Ave Mahwah, NJ 07430

Re: Structural Letter ~ Antenna Mount T-Mobile – Site Ref: CT11014B 623 Pine Street Bridgeport, CT 06605

Centek Project No. 20074.32

Dear Mr. Reid,

Centek Engineering, Inc. has reviewed the T-Mobile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the existing mount, consisting of three (3) 14.5-ft sector frames to support the equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2012 International Building Code as modified by the 2016 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G *Structural Standards for Steel Antenna Towers and Supporting Structures*.

The loads considered in this analysis consist of the following:

T-Mobile:

<u>Sector Frame:</u> Three (3) Ericsson AIR6449 panel antennas, three (3) Ericsson AIR3246 B66 panel antennas, three (3) RFS APXVAARR24-43-NA20 panel antennas, three (3) KRY111-144/2 TMAs, three (3) Ericsson 4424 remote radio units, three (3) Ericsson 4449 B71_B12 remote radio units and three (3) Commscope SDX1926Q-43 diplexers mounted on three (3) sector frames with a RAD center elevation of 180-ft +/- AGL.

(NOTE: APXVAARR24-43 antenna must be mounted on the same side of the sector frame as the stabilizer arm)

The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering a nominal design wind speed of 97 mph for Bridgeport as required in Appendix N of the 2016 Connecticut State Building Code.

A structural analysis of tower and foundation needs to be completed prior to any work.

Based on our review of the installation, it is our opinion that the subject antenna mount has sufficient capacity to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.

Respectfully Submitted by:

Timothy J. Lynn, PE Structural Engineer



CENTEK Engineering, Inc. Structural Analysis – Mount Analysis T-Mobile Site Ref. ~ CT11014B Bridgeport, CT June 8, 2020

Section 2 - Calculations

CENTEK engineering Subject:	TIA-222-G Loads
Centered on Solutions www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 P: (203) 498-0580	Bridgeport, CT
Rev. 0: 6/6/2	Prepared by: T.J.L. Checked by: C.F.C. Job No. 20074.32
Development of Design Heights, Exposure Coefficients, and Velocity Pressures Per TIA-222-G	
Wind Speeds	
Basic Wind Speed Basic Wind Speed with Ice Input	V := 97 mph (User Input - 2016 CSBC Appendix N) V _i := 50 mph (User Input per Annex B of TIA-222-G)
Structure Type =	Structure_Type := Pole (User Input)
Structure Category =	SC := II (User Input)
Exposure Category =	Exp := D (User Input)
Structure Height =	h := 250 ft (User Input)
Height to Center of Antennas=	$z_{AT&T} \approx 180$ ft (User Input)
Radial Ice Thickness =	t _i := 0.75 in (User Input per Annex B of TIA-222-G)
Radial Ice Density=	Id := 56.00 pcf (User Input)
Topograpic Factor =	K _{zt} := 1.0 (User Input)
	K _a := 1.0 (User Input)
Gust Response Factor =	G _H = 1.1 (User Input)
Output	
Output Wind Direction Probability Factor =	$K_d :=$ 0.95 if Structure_Type = Pole= 0.95(Per Table 2-2 of TIA-222-G)0.85 if Structure_Type = LatticeTIA-222-G)
Output Wind Direction Probability Factor = Importance Factors =	$K_{d} := \begin{bmatrix} 0.95 & \text{if } Structure_Type = Pole \\ 0.85 & \text{if } Structure_Type = Lattice \\ \end{bmatrix} \begin{pmatrix} \text{Per Table 2-2 of } \\ \text{TIA-222-G} \end{pmatrix}$ $I_{Wind} := \begin{bmatrix} 0.87 & \text{if } SC = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.15 & \text{if } SC = 3 \\ \end{pmatrix}$
Output Wind Direction Probability Factor = Importance Factors =	$K_{d} := \begin{bmatrix} 0.95 & \text{if Structure_Type} = \text{Pole} \\ 0.85 & \text{if Structure_Type} = \text{Lattice} \end{bmatrix} = 0.95 & (\text{Per Table 2-2 of TIA-222-G}) \\ I_{Wind} := \begin{bmatrix} 0.87 & \text{if SC} = 1 & = 1 \\ 1.00 & \text{if SC} = 2 \\ 1.15 & \text{if SC} = 3 \end{bmatrix} & (\text{Per Table 2-3 of TIA-222-G}) \\ I_{Wind_w_Ice} := \begin{bmatrix} 0 & \text{if SC} = 1 & = 1 \\ 1.00 & \text{if SC} = 2 \\ 1.00 & \text{if SC} = 2 \\ 1.00 & \text{if SC} = 3 \end{bmatrix}$
Output Wind Direction Probability Factor = Importance Factors =	$K_{d} := \begin{bmatrix} 0.95 & \text{if } Structure_Type = Pole \\ 0.85 & \text{if } Structure_Type = Lattice} \end{bmatrix} = 0.95 \qquad (Per Table 2-2 \text{ of } TIA-222-G)$ $I_{Wind} := \begin{bmatrix} 0.87 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.15 & \text{if } SC = 3 \end{bmatrix} \qquad (Per Table 2-3 \text{ of } TIA-222-G)$ $I_{Wind_w_lce} := \begin{bmatrix} 0 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.00 & \text{if } SC = 3 \end{bmatrix}$ $I_{ice} := \begin{bmatrix} 0 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 3 \end{bmatrix}$ $I_{ice} := \begin{bmatrix} 0 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 3 \end{bmatrix}$
Wind Direction Probability Factor = Importance Factors = $K_{iz} := \left(\frac{z_{AT&T}}{33}\right)^{0.1} = 1.185$	$\begin{split} & K_{d} := \begin{bmatrix} 0.95 & \text{if } Structure_Type = Pole \\ 0.85 & \text{if } Structure_Type = Lattice} \end{bmatrix} = 0.95 & (Per Table 2.2 of TIA-222-G) \\ & I_{Wind} := \begin{bmatrix} 0.87 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.15 & \text{if } SC = 3 \end{bmatrix} & (Per Table 2.3 of TIA-222-G) \\ & I_{Vind}_w_Ice} := \begin{bmatrix} 0 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.00 & \text{if } SC = 2 \\ 1.00 & \text{if } SC = 3 \end{bmatrix} \\ & I_{ice} := \begin{bmatrix} 0 & \text{if } SC = 1 & = 1 \\ 1.00 & \text{if } SC = 2 \\ 1.25 & \text{if } SC = 3 \end{bmatrix} \\ & t_{iz} := 2.0 \cdot t_{i} \cdot I_{ice} \cdot K_{iz} \cdot K_{zt} \overset{0.35}{=} 1.777 \\ & \underline{2} \end{bmatrix} \end{split}$
Wind Direction Probability Factor = Importance Factors = $K_{iz} := \left(\frac{z_{AT&T}}{33}\right)^{0.1} = 1.185$ Velocity Pressure CoefficientAnternas=	$K_{d} := \begin{bmatrix} 0.95 & \text{if } \text{Structure_Type = Pole} \\ 0.85 & \text{if } \text{Structure_Type = Lattice} \end{bmatrix} = 0.95 \qquad (Per Table 2-2 \text{ of } TL-222-G)$ $Wind := \begin{bmatrix} 0.87 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.15 & \text{if } \text{SC} = 3 \end{bmatrix} \qquad (Per Table 2-3 \text{ of } TL-222-G)$ $Wind_w_lce := \begin{bmatrix} 0 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.00 & \text{if } \text{SC} = 3 \end{bmatrix}$ $V_{it} = \begin{bmatrix} 0 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.25 & \text{if } \text{SC} = 3 \end{bmatrix}$ $t_{iz} := 2.0 \cdot t_{i} \cdot I_{ic} e^{iK_{iz}} K_{zt}^{0.35} = 1.777$ $K_{ZAT&T} := 2.01 \left(\left(\frac{ZAT&T}{zg} \right) \right)^{\frac{2}{\alpha}} = 1.587$
OutputWind Direction Probability Factor =Importance Factors = $K_{iz} := \left(\frac{z_{AT&T}}{33} \right)^{0.1} = 1.185$ Velocity Pressure CoefficientAnternas =Velocity Pressure w/o Ice Antennas =	$K_{d} := \begin{bmatrix} 0.95 & \text{if } \text{Structure_Type = Pole} \\ 0.85 & \text{if } \text{Structure_Type = Lattice} \end{bmatrix} = 0.95 \qquad (Per Table 2-2 \text{ of } TA-222-G)$ $Wind := \begin{bmatrix} 0.87 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.15 & \text{if } \text{SC} = 3 \end{bmatrix}$ $Wind_w_lce := \begin{bmatrix} 0 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.00 & \text{if } \text{SC} = 3 \end{bmatrix}$ $I_{ice} := \begin{bmatrix} 0 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 3 \end{bmatrix}$ $I_{ice} := \begin{bmatrix} 0 & \text{if } \text{SC} = 1 & = 1 \\ 1.00 & \text{if } \text{SC} = 2 \\ 1.25 & \text{if } \text{SC} = 3 \end{bmatrix}$ $I_{iz} := 2.0 \cdot I_{i} \cdot I_{ice} \cdot K_{iz} \cdot K_{zt} \begin{bmatrix} 0.35 \\ -2 \\ -2 \end{bmatrix} = 1.777$ $Kz_{AT&T} := 2.01 \left(\left(\frac{z_{AT&T}}{zg} \right) \right)^{\frac{2}{\alpha}} = 1.587$ $qz_{AT&T} := 0.00256 \cdot K_{d} \cdot Kz_{AT&T} \cdot \sqrt{2} \cdot I_{Wind} = 36.318$



Location:

Rev. 0: 6/6/20

TIA-222-G Loads

Bridgeport, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 20074.32

Development of Wind & Ice Load on Antennas

Antenna Data:			
Antenna Model =	Ericsson AIR6449		
Antenna Shape =	Flat		(User Input)
Anterna Height=	L _{ant} := 33.1	in	(User Input)
Antenna Width =	W _{ant} := 20.5	in	(User Input)
Antenna Thickness =	T _{ant} := 8.3	in	(User Input)
Antenna Weight =	WT _{ant} := 103	lbs	(User Input)
Number of Antennas =	N _{ant} := 1		(User Input)
AntennaAspectRatio =	$Ar_{ant} := \frac{L_{ant}}{W_{ant}} = 1$.6	

Ca_{ant} = 1.2

 $SA_{antF} := \frac{L_{ant} W_{ant}}{144} = 4.7$

 $SA_{antS} := \frac{L_{ant} T_{ant}}{144} = 1.9$

 $F_{ant} := qz_{AT&T} \cdot G_{H} \cdot Ca_{ant} \cdot K_{a} \cdot SA_{antF} = 226$

 $F_{ant} := qz_{AT\&T} \cdot G_{H} \cdot Ca_{ant} \cdot K_a \cdot SA_{antS} = 91$

 $SA_{ICEantF} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(W_{ant} + 2 \cdot t_{iz}\right)}{144} = 6.1$

Fiant := qz_{ice.AT&T}·G_H·Ca_{ant}·K_a·SA_{ICEantF} = 78

Fiant := qzice.AT&T'GH'Caant'Ka'SAICEantS = 38

 $V_{ice} \coloneqq \left(L_{ant} + 2 \cdot t_{iz}\right) \left(W_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right) - V_{ant} = 4820$

 $SA_{ICEantS} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right)}{144} = 3$

Wind Load (without ice)	Wind Load	(without ice)	
-------------------------	-----------	---------------	--

Surface Area for One Antenna =

Antenna Force Coefficient =

Total Anten na Wind Force =

Surface Area for One Antenna =

TotalAnten na Wind Force =

Wind Load (with ice)

Surface Area for One Antenna w/ Ice =

Total Antenna Wind Forcew/lce =

Surface Area for One Antenna w/ Ice =

Total Antenna Wind Forcew/lce =

Gravity Load (without ice)

Weight of All Antennas=

Gravity Loads (ice only)

Volume of Each Antenna =

Volume of Ice on EachAntenna =

Weight of Ice on Each Antenna =

Weight of Ice on All Antennas =

 $V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 5632$

lbs

 $WT_{ant} \cdot N_{ant} = 103$

 $W_{ICEant} \cdot N_{ant} = 156$

cuin

sf Ibs

sf

lbs

sf

lbs

sf

lbs

lbs

cuin

lbs



Location:

Antenna Model =

Antenna Shape =

Antenna Height =

Antenna Width =

Antenna Thickness =

Number of Antennas =

AntennaAspectRato =

Wind Load (without ice)

Antenna Force Coefficient =

Surface Area for One Antenna =

Surface Area for One Antenna =

Surface Ar ea for One Antenna w/ Ice =

Surface Area for One Antenna w/ Ice =

Total Antenna Wind Forcew/Ice =

Total Antenna Wind Forcew/Ice =

Gravity Load (without ice) Weight of All Antennas=

Gravity Loads (ice only)

Volume of Each Antenna =

Volume of I ce on Each Antenna =

Weight of Ice on Each Antenna =

Weight of Ice on All Antennas =

Total Anten na Wind Force =

Total Anten na Wind Force=

Wind Load (with ice)

Antenna Weight =

Rev. 0: 6/6/20

TIA-222-G Loads

Bridgeport, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 20074.32

Development of Wind & Ice Load on Antennas

Antenna Data:			
tenna Model =	Ericsson AIR3246-B	66	
enna Shape =	Flat		(User Input)
erna Heicht=	L _{ant} := 58.1	in	(User Input)
ntenna Width =	W _{ant} := 15.7	in	(User Input)
a Thickness=	T _{ant} := 9.4	in	(User Input)
enna Weight =	WT _{ant} := 180	lbs	(User Input)
of Antennas =	N _{ant} := 1		(User Input)
	Lont		
spectRa í o=	$Ar_{ant} := \frac{ant}{W} = 3$	3.7	

 $Ca_{ant} = 1.25$

L _{ant} .W _{ant}	
$SA_{antF} := \frac{144}{144} = 6.3$	

 $F_{ant} := qz_{AT&T} \cdot G_{H} \cdot Ca_{ant} \cdot K_{a} \cdot SA_{antF} = 317$

$$SA_{antS} := \frac{L_{ant} T_{ant}}{144} = 3.8$$
 sf

$$SA_{ICEantF} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(W_{ant} + 2 \cdot t_{iz}\right)}{144} = 8.2$$

lbs $Fi_{ant} := qz_{ice,AT&T} \cdot G_{H} \cdot Ca_{ant} \cdot K_a \cdot SA_{ICEantF} = 110$

$$SA_{ICEantS} \coloneqq \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right)}{144} = 5.5$$
 sf

lbs

lbs

sf lbs

lbs

sf

$$V_{ant} := L_{ant} \cdot W_{ant} \cdot T_{ant} = 8574$$
 cu in

 $V_{ice} \coloneqq \left(L_{ant} + 2 \cdot t_{iz}\right) \left(W_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right) - V_{ant} = 6805$ cuin

$$W_{ICEant} := \frac{V_{ice}}{1728} \cdot Id = 221$$
 lbs

TIA RevG Load Calculations.xmcd.xmcd



Location:

Rev. 0: 6/6/20

TIA-222-G Loads

Bridgeport, CT

Prepared by: T.J.L. Checked by: C.F.C. Job No. 20074.32

Development of Wind & Ice Load on Antennas

Antenna Data:			
Antenna Model =	RFSAPXVAARR24-	43	
Antenna Shape =	Flat		(User Input)
Anterna Height=	L _{ant} := 95.9	in	(User Input)
Antenna Width =	W _{ant} := 24	in	(User Input)
Antenna Thickness =	T _{ant} := 8.7	in	(User Input)
Antenna Weight =	WT _{ant} := 153	lbs	(User Input)
Number of Antennas =	N _{ant} := 1		(User Input)
AntennaAspectRato =	$Ar_{ant} \coloneqq \frac{L_{ant}}{W_{ant}} = 4$	l.0	
Antenna Force Coefficient =	Ca _{ant} = 1.27		

Wind Load (without ice)

Surface Area for One Antenna =

Total Anten na Wind Force =

Surface Area for One Antenna =

Total Anten na Wind Force =

Wind Load (with ice)

Surface Ar ea for One Antenna w/ Ice =

Total Antenna Wind Forcew/lce=

Surface Area for One Antenna w/ Ice =

Total Antenna Wind Forcew/Ice =

Gravity Load (without ice)

- Weight of All Antennas=
- Gravity Loads (ice only)

Volume of Each Antenna =

Volume of Ice on EachAntenna =

Weight of Ice on Each Antenna =

Weight of Ice on All Antennas =

$SA_{antF} := \frac{L_{ant} \cdot W_{ant}}{144} = 16$	sf
	lbs

F_{ant} := qz_{AT&T}·G_H·Ca_{ant}·Ka·SA_{antF} = 809

$$SA_{antS} := \frac{L_{ant} T_{ant}}{144} = 5.8$$
 sf

F_{ant} := qz_{AT&T}·G_H·Ca_{ant}·K_a·SA_{antS} = 293

$$SA_{ICEantF} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(W_{ant} + 2 \cdot t_{iz}\right)}{144} = 19 \qquad \qquad \text{sf}$$

Fi_{ant} := qz_{ice.AT&T}·G_H·Ca_{ant}·Ka·SA_{ICEantF} = 256

$$SA_{ICEantS} := \frac{\left(L_{ant} + 2 \cdot t_{iz}\right) \cdot \left(T_{ant} + 2 \cdot t_{iz}\right)}{144} = 8.5$$
 sf

× /

$$WT_{ant} \cdot N_{ant} = 153$$

F

lbs

cuin

lbs

lbs

lbs

$$V_{ant} := L_{ant} W_{ant} T_{ant} = 2 \times 10^4$$

 $\mathsf{V}_{ice} \coloneqq \left(\mathsf{L}_{ant} + 2 \cdot \mathsf{t}_{iz}\right) \left(\mathsf{W}_{ant} + 2 \cdot \mathsf{t}_{iz}\right) \cdot \left(\mathsf{T}_{ant} + 2 \cdot \mathsf{t}_{iz}\right) - \mathsf{V}_{ant} = 1 \times 10^4 \qquad \qquad \mathsf{cu} \ \mathsf{in}$

$$W_{ICEant} := \frac{V_{ice}}{1728} \cdot Id = 439$$
 lbs

CENITER	Sub	ject:			TIA-222-G Loads	
	igineering					
Centered on Solutions [®] www 63-2 North Branford Road Branford, CT 06405	Loca (203) 488-0580 (203) 488-8587	ation:			Bridgeport, CT	
	Rev	. 0: 6/6/20			Prepared by: T.J.L. Checke Job No. 20074.32	d by: C.F.C.
Developmen	t of Wind & Ice Load on TMA	's				
	<u>TM</u>	A Data:				
	TMAMo	del =	Ericsson KRY11214	4/1 TM	A	
	TMASh	ape =	Flat		(User Input)	
	TMAHe	ight =	L _{TMA} := 7.7	in	(User Input)	
	TMAW	/idth =	W _{TMA} ≔ 7.5	in	(User Input)	
	TMAThick	ess =	T _{TMA} ≔ 3.4	in	(User Input)	
	TMAWe	eight =	WT _{TMA} := 11	lbs	(User Input)	
	Number of TM	A's=	N _{TMA} := 1		(User Input)	
	TMA Aspect Ra	atio =	$Ar_{TMA} \coloneqq \frac{L_{TMA}}{W_{TMA}}$	= 1		
	TMA Force Coefficie	nt =	Ca _{TMA} = 1.2			
	Wind Load (without	t ice)				
	Surface Area for One TM	4=	SA _{TMAF} :=	^{. W} ТМ 144	$\frac{1A}{2} = 0.4$	sf
	Total TMAWind For	ce =	F _{TMA} := qz _{AT&T}	·G _H ·Ca	TMA ^{·K} a ^{·SA} TMAF = 19	lbs
	Surface Area for One TM	4=	SA _{TMAS} :=	а ^{.⊤} тм/ 144	A - = 0.2	sf
	Total TMAWind For	ce =	F _{TMA} := qz _{AT&T}	G _H .Ca	TMA ^{.K} a ^{.SA} TMAS = 9	lbs
	Wind Load (wit	h ice)				
Su	rfaceArea for One TMA w Ice	=	SA _{ICETMAF} ≔ (LTMA -	$\frac{+2 \cdot t_{iz} \left(W_{TMA} + 2 \cdot t_{iz} \right)}{144} = 0.9$	sf
	Total TMAWind Force w/ lc	e =	Fi _{TMA} := qz _{ice.A1}	ſ&T [.] Gŀ	H ^{·Ca} TMA·Ka ^{·SA} ICETMAF = 11	lbs
Su	rfaceAræfor One TMA w/lce	=	SA _{ICETMAS} ≔ (LTMA -	$\frac{+2 \cdot t_{iz} \cdot \left(T_{TMA} + 2 \cdot t_{iz} \right)}{144} = 0.5$	sf
	Total TMAW ind Force w/ lc	e =	Fi _{TMA} := qz _{ice.A1}	г <mark>&Т[.]G</mark> Ь	H ^{·Ca} TMA·Ka·SAICETMAS = 7	lbs
	Gravity Load (without	ice)				
	Weight of All TM	As=	WT _{TMA} ·N _{TMA} =	11		lbs
	Gravity Loads (ice o	nly)				
	Volume of Each TM	IA=	V _{TMA} ≔ L _{TMA} ·W	/ _{TMA} .T	T _{TMA} = 196	cuin
	Volume of Ice on Each TMA	.=	$V_{ice} := (L_{TMA} + 2)$	2∙t _{iz})(W	$V_{TMA} + 2 \cdot t_{iz} \cdot (T_{TMA} + 2 \cdot t_{iz}) - V_{TMA} =$	= 669 cu in
	Weight of Ice on Each TM	\=	W _{ICETMA} ≔ V _{ic} 172	$\frac{e}{28} \cdot Id =$	22	lbs
	Weight of Ice on All TMA:	S=	WICETMA ^{. N} TMA	= 22		lbs

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CENTEK engineering Subject:	TIA-222-G Loads	
Centered on Solutions ^{**} www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 Exanford (206405	Bridgeport, CT	
Rev. 0: 6/6/20	Prepared by: T.J.L. Checke Job No. 20074.32	d by: C.F.C.
Development of Wind & Ice Load on RRUS's		
RRUS Data:	5. (110)77(2)0	
	Encsson 4449 B71B12	
RUS Shape =	riat (User input)	
	LRRUS = 14.9 in (User input)	
	$W_{\text{RRUS}} \coloneqq 13.2$ in (User input)	
DDI IS Weight -	$1_{\text{RRUS}} = 10.4 \text{in (User input)}$	
	W TRRUS = 74 ibs (User linput)	
RRUSAspect Ratio =	$Ar_{RRUS} = \frac{RRUS}{W_{RRUS}} = 1.1$	
RRUS Force Coefficient =	Ca _{RRUS} = 1.2	
Wind Load (without ice)		
Surface Area for One R RUS =	$SA_{RRUSF} \coloneqq \frac{L_{RRUS} W_{RRUS}}{144} = 1.4$	sf
Total RRUS Wind Force =	F _{RRUS} := qz _{AT&T} ·G _H ·Ca _{RRUS} ·K _a ·SA _{RRUSF} = 65	lbs
Surface Area for One R RUS =	$SA_{RRUSS} := \frac{L_{RRUS} \cdot T_{RRUS}}{144} = 1.1$	sf
Total RRUS Wind Force =	F _{RRUS} := qz _{AT&T} ·G _H ·Ca _{RRUS} ·K _a ·SA _{RRUSS} = 52	lbs
Wind Load (with ice)		
Surface Area for One RRUS w/Ice =	$SA_{ICERRUSF} \coloneqq \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(W_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 2.1$	sf
Total RRUS Wind Force w/ Ice =	Fi _{RRUS} := qz _{ice.AT&T} ·G _H ·Ca _{RRUS} ·Ka ^{·SA} ICERRUSF = 27	lbs
Surface Area for One RRUS w/ Ice =	$SA_{ICERRUSS} \coloneqq \frac{\left(L_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(T_{RRUS} + 2 \cdot t_{iz}\right)}{144} = 1.8$	sf
Total RRUS Wind Force w/ Ice =	Fi _{RRUS} := qz _{ice.AT&T} .G _H .Ca _{RRUS} .K _a .SA _{ICERRUSS} = 23	lbs
Gravity Load (without ice)		
Weight of All RRUSs=	WT _{RRUS} ·N _{RRUS} = 74	lbs
Gravity Loads (ice only)		
Volume of Each RRUS =	V _{RRUS} ^{:= L} RRUS ^{·W} RRUS ^{·T} RRUS ^{= 2045}	cuin
Volume of Ice on EachRRUS =	$V_{ice} \coloneqq \left(L_{RRUS} + 2 \cdot t_{iz}\right) \left(W_{RRUS} + 2 \cdot t_{iz}\right) \cdot \left(T_{RRUS} + 2 \cdot t_{iz}\right) - V_{RIS}$	RUS ^{= 2269}
Weight of Ice on Each RRUS =	$W_{\text{ICERRUS}} \coloneqq \frac{V_{\text{ice}}}{1728} \cdot \text{Id} = 74$	lbs
Weight of Ice on All RRUSs =	WICERRUS ^{·N} RRUS = 74	lbs

TIA-222-G Loads

CENITER	engineering	Subject:			TIA-222-G Loads	
63-2 North Branford Road Branford, CT 06405	P: (203) 488-0580 F: (203) 488-8587	Location:			Bridgeport, CT	
	,	Rev. 0: 6/6/20			Prepared by: T.J.L. Checke Job No. 20074.32	ed by: C.F.C.
Developm	ent of Wind & Ice Load or	n RRUS's				
		<u>RRUS Data:</u>				
	R	RUS Model =	4424			
	R	RUS Shape =	Flat		(User Input)	
	R	RUS Height =	L _{RRUS} := 17.1	in	(User Input)	
	F	RRUS Width =	W _{RRUS} ≔ 14.4	in	(User Input)	
	RRU	S Thickness =	T _{RRUS} ≔ 11.3	in	(User Input)	
	RI	RUSWeight=	WT _{RRUS} := 86	lbs	(User Input)	
	Number	r of RRUS's=	N _{RRUS} ≔ 1		(User Input)	
	RRUSA	spect Ratio =	$Ar_{RRUS} \coloneqq \frac{L_{RRI}}{W_{RR}}$	US =	1.2	
	RRUS Force	Coefficient=	Ca _{RRUS} = 1.2			
	Wind Load	(without ice)				
	Surface Area for Or	ne R RUS =	SA _{RRUSF} :=	RUS ^{. V} 14	$\frac{V_{RRUS}}{4} = 1.7$	st
	Total RRUS W	/ind Force =	F _{RRUS} := qz _{AT&}	T'GH'	Ca _{RRUS} ·K _a ·SA _{RRUSF} = 82	lbs
			Lp	DI IQ'T		
	Surface Area for Or	ne R RUS =	SA _{RRUSS} :=	144	$\frac{1}{4}$ = 1.3	sf
	Total RRUS W	/ind Force =	F _{RRUS} := qz _{AT&}	T'GH'	Ca _{RRUS} ·Ka ^{·SA} RRUSS = 64	lbs
	Wind Lo	oad (with ice)				
	Surface Area for One RRU	S w/ Ice =	SA _{ICERRUSF} :=	(L _{RR}	$\frac{\text{US} + 2 \cdot t_{iz} \cdot \left(\text{W}_{\text{RRUS}} + 2 \cdot t_{iz} \right)}{144} = 2.6$	sf
	Total RRUS Wind Fo	rce w/ lce =	Fi _{RRUS} := qz _{ice.} ,	AT&T	GH ^{.Ca} RRUS ^{.K} a ^{.SA} ICERRUSF ^{= 33}	lbs
	Surface Area for One RRU	S w/Ice =	SA _{ICERRUSS} :=		$\frac{\text{US} + 2 \cdot t_{iz}) \cdot \left(\text{T}_{\text{RRUS}} + 2 \cdot t_{iz}\right)}{144} = 2.1$	sf
	Total RRUS Wind Fo	rce w/ lce =	Firrus := qz _{ice.}	AT&T	G _H ·Ca _{RRUS} ·K _a ·SA _{ICERRUSS} = 27	lbs
	Gravity Load (v	vithout ice)				
	Weight of	All RRUSs=	WT _{RRUS} ·N _{RRUS}	s = 86	i	lbs
	Gravity Load	ls (ice only)				
	Volume of Ea	chRRUS=	V _{RRUS} := L _{RRUS}	s ^{.W} RI	rus ^{-T} rrus ^{= 2783}	cuin
	Volume of Ice on Eac	hRRUS=	V _{ice} := (L _{RRUS} +	· 2·t _{iz})	$(W_{RRUS} + 2 \cdot t_{iz}) \cdot (T_{RRUS} + 2 \cdot t_{iz}) - V_{F}$	RRUS ^{= 2726} cu in
	Weight of Ice on Eac	ch RRUS=	^W ICERRUS ^{:=} [−]	ice 728 Id	l = 88	lbs
	Weight of Ice on Al	IRRUSs=	WICERRUS ^{.N} RR	US ⁼	88	lbs

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(Global) Model Settings

Display Sections for Member Calcs	5
Max Internal Sections for Member Calcs	97
Include Shear Deformation?	Yes
Increase Nailing Capacity for Wind?	Yes
Include Warping?	Yes
Trans Load Btwn Intersecting Wood Wall?	Yes
Area Load Mesh (in^2)	144
Merge Tolerance (in)	.12
P-Delta Analysis Tolerance	0.50%
Include P-Delta for Walls?	Yes
Automatically Iterate Stiffness for Walls?	Yes
Max Iterations for Wall Stiffness	3
Gravity Acceleration (ft/sec^2)	32.2
Wall Mesh Size (in)	12
Eigensolution Convergence Tol. (1.E-)	4
Vertical Axis	Υ
Global Member Orientation Plane	XZ
Static Solver	Sparse Accelerated
Dynamic Solver	Accelerated Solver

Hot Rolled Steel Code	AISC 14th(360-10): LRFD
Adjust Stiffness?	Yes(Iterative)
RISAConnection Code	AISC 14th(360-10): ASD
Cold Formed Steel Code	AISI S100-10: ASD
Wood Code	AWC NDS-12: ASD
Wood Temperature	< 100F
Concrete Code	ACI 318-11
Masonry Code	ACI 530-11: ASD
Aluminum Code	AA ADM1-10: ASD - Building
Stainless Steel Code	AISC 14th(360-10): ASD
Adjust Stiffness?	Yes(Iterative)

Number of Shear Regions	4
Region Spacing Increment (in)	4
Biaxial Column Method	Exact Integration
Parme Beta Factor (PCA)	.65
Concrete Stress Block	Rectangular
Use Cracked Sections?	Yes
Use Cracked Sections Slab?	No
Bad Framing Warnings?	No
Unused Force Warnings?	Yes
Min 1 Bar Diam. Spacing?	No
Concrete Rebar Set	REBAR_SET_ASTMA615
Min % Steel for Column	1
Max % Steel for Column	8

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(Global) Model Settings, Continued

Seismic Code	ASCE 7-10
Seismic Base Elevation (ft)	Not Entered
Add Base Weight?	Yes
Ct X	.02
Ct Z	.02
T X (sec)	Not Entered
TZ (sec)	Not Entered
RX	3
RZ	3
Ct Exp. X	.75
Ct Exp. Z	.75
SD1	1
SDS	1
S1	1
TL (sec)	5
Risk Cat	l or ll
Drift Cat	Other
Om Z	1
Om X	1
Cd Z	4
Cd X	4
Rho Z	1
Rho X	1
Footing Overturning Safety Factor	1
Optimize for OTM/Sliding	No
Check Concrete Bearing	No
Footing Concrete Weight (k/ft^3)	150.001
Footing Concrete f'c (ksi)	4
Footing Concrete Ec (ksi)	3644
Lambda	1
Footing Steel fy (ksi)	60
Minimum Steel	0.0018
Maximum Steel	0.0075
Footing Top Bar	#3
Footing Top Bar Cover (in)	2
Footing Bottom Bar	#3
Footing Bottom Bar Cover (in)	3.5
Pedestal Bar	#3
Pedestal Bar Cover (in)	1.5
Pedestal Ties	#3

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nu	Therm (\1	Density[k/ft^3]	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	58	1.2
3	A992	29000	11154	.3	.65	.49	50	1.1	58	1.2
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.3	58	1.1
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.2	58	1.1
6	A53 Grade B	29000	11154	.3	.65	.49	35	1.5	58	1.2



Hot Rolled Steel Section Sets

	Label	Shape	Туре	Design List	Material	Design Rul	.A [in2]	lyy [in4]	lzz [in4]	J [in4]
1	Horz	PIPE_2.5	Beam	Pipe	A53 Grade B	Typical	1.61	1.45	1.45	2.89
2	Antenna Mast	PIPE_2.0	Column	Wide Flange	A53 Grade B	Typical	1.02	.627	.627	1.25
3	Vert	PIPE_2.5	Column	Wide Flange	A53 Grade B	Typical	1.61	1.45	1.45	2.89
4	Stablizer Arm	PIPE_2.0	Beam	Pipe	A53 Grade B	Typical	1.02	.627	.627	1.25

Hot Rolled Steel Design Parameters

	Label	Shape	Length[ft]	Lbyy[ft]	Lbzz[ft]	Lcomp top[.Lcomp bot[.L-torq	Куу	Kzz	Cb	Functi
1	M1	Horz	14.5			Lbyy						Lateral
2	M2	Horz	14.5			Lbyy						Lateral
3	M3	Antenna Mast	6			Lbyy						Lateral
4	M4	Antenna Mast	6			Lbyy						Lateral
5	M5	Antenna Mast	6			Lbyy						Lateral
6	M6	Antenna Mast	6			Lbyy						Lateral
7	M7	Vert	5			Lbyy						Lateral
8	M8	Antenna Mast	8			Lbyy						Lateral
9	M9	Stablizer Arm	8.382			Lbyy						Lateral

Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(d	Section/Shape	Туре	Design List	Material	Design Rul
1	M1	N1	N6			Horz	Beam	Pipe	A53 Gra	Typical
2	M2	N8	N13			Horz	Beam	Pipe	A53 Gra	Typical
3	M3	N23	N24			Antenna Mast	Column	Wide Flange	A53 Gra	Typical
4	M4	N17	N20			Antenna Mast	Column	Wide Flange	A53 Gra	Typical
5	M5	N18	N21			Antenna Mast	Column	Wide Flange	A53 Gra	Typical
6	M6	N19	N22			Antenna Mast	Column	Wide Flange	A53 Gra	Typical
7	M7	N15	N16			Vert	Column	Wide Flange	A53 Gra	Typical
8	M8	N27	N28			Antenna Mast	Column	Wide Flange	A53 Gra	Typical
9	M9	N29	N30			Stablizer Arm	Beam	Pipe	A53 Gra	Typical

Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia
1	N1	0	0	0	0	
2	N2	.5	0	0	0	
3	N3	5	0	0	0	
4	N4	9.5	0	0	0	
5	N5	14	0	0	0	
6	N6	14.5	0	0	0	
7	N7	7.25	0	0	0	
8	N8	0	-4	0	0	
9	N9	.5	-4	0	0	
10	N10	5	-4	0	0	
11	N11	9.5	-4	0	0	
12	N12	14	-4	0	0	
13	N13	14.5	-4	0	0	
14	N14	7.25	-4	0	0	
15	N15	7.25	.5	0	0	



Joint Coordinates and Temperatures (Continued)

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Dia
16	N16	7.25	-4.5	0	0	
17	N17	5	1	0	0	
18	N18	9.5	1	0	0	
19	N19	14	1	0	0	
20	N20	5	-5	0	0	
21	N21	9.5	-5	0	0	
22	N22	14	-5	0	0	
23	N23	.5	1	0	0	
24	N24	.5	-5	0	0	
25	N25	1	0	0	0	
26	N26	1	-4	0	0	
27	N27	1	2	0	0	
28	N28	1	-6	0	0	
29	N29	.5	-1	0	0	
30	N30	3	-1	-8	0	

Joint Boundary Conditions

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]
1	N15	Reaction	Reaction	Reaction			
2	N16	Reaction	Reaction	Reaction			
3	N30	Reaction	Reaction	Reaction			

Member Point Loads (BLC 2 : Dead Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Y	077	.5
2	M8	Y	077	7.5
3	M4	Y	09	.5
4	M4	Y	09	5.5
5	M5	Y	052	.5
6	M5	Y	052	3.5
7	M8	Y	074	1.5
8	M8	Y	086	%50

Member Point Loads (BLC 3 : Ice Load)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Y	22	.5
2	M8	Y	22	7.5
3	M4	Y	111	.5
4	M4	Y	111	5.5
5	M5	Y	078	.5
6	M5	Y	078	3.5
7	M8	Y	074	1.5
8	M8	Y	088	%50

Member Point Loads (BLC 4 : Wind with Ice X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Х	.057	.5
2	M8	Х	.057	7.5



Member Point Loads (BLC 4 : Wind with Ice X) (Continued)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
3	M4	Х	.037	.5
4	M4	Х	.037	5.5
5	M5	Х	.019	.5
6	M5	Х	.019	3.5
7	M8	Х	.023	1.5
8	M8	Х	.027	%50

Member Point Loads (BLC 5 : Wind X)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Х	.147	.5
2	M8	Х	.147	7.5
3	M4	Х	.095	.5
4	M4	Х	.095	5.5
5	M5	Х	.046	.5
6	M5	Х	.046	3.5
7	M8	Х	.052	1.5
8	M8	Х	.064	%50

Member Point Loads (BLC 6 : Wind with Ice Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Z	.128	.5
2	M8	Z	.128	7.5
3	M4	Z	.055	.5
4	M4	Z	.055	5.5
5	M5	Z	.039	.5
6	M5	Z	.039	3.5

Member Point Loads (BLC 7 : Wind Z)

	Member Label	Direction	Magnitude[k,k-ft]	Location[ft,%]
1	M8	Z	.405	.5
2	M8	Z	.405	7.5
3	M4	Z	.159	.5
4	M4	Z	.159	5.5
5	M5	Z	.113	.5
6	M5	Z	.113	3.5

Member Distributed Loads (BLC 4 : Wind with Ice X)

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft,%]
1	M9	Х	.003	.003	0	0
2	M3	Х	.003	.003	0	0
3	M8	Х	.003	.003	0	0
4	M4	Х	.003	.003	0	0
5	M7	Х	.003	.003	0	0
6	M5	Х	.003	.003	0	0
7	M6	Х	.003	.003	0	0

Member Distributed Loads (BLC 5 : Wind X)

Member Label Direction Start Magnitude[k/ft,... End Magnitude[k/ft,F... Start Location[ft,%] End Location[ft,%]



Member Distributed Loads (BLC 5 : Wind X) (Continued)

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft,%]
1	M9	Х	.009	.009	0	0
2	M3	Х	.009	.009	0	0
3	M8	Х	.009	.009	0	0
4	M4	Х	.009	.009	0	0
5	M7	Х	.009	.009	0	0
6	M5	Х	.009	.009	0	0
7	M6	Х	.009	.009	0	0

Member Distributed Loads (BLC 6 : Wind with Ice Z)

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft,%]
1	M9	Z	.003	.003	0	0
2	M1	Z	.003	.003	0	0
3	M2	Z	.003	.003	0	0
4	M7	Z	.003	.003	0	0
5	M8	Z	.003	.003	0	0
6	M3	Z	.003	.003	0	0

Member Distributed Loads (BLC 7 : Wind Z)

	Member Label	Direction	Start Magnitude[k/ft,	End Magnitude[k/ft,F	Start Location[ft,%]	End Location[ft,%]
1	M9	Z	.009	.009	0	0
2	M1	Z	.009	.009	0	0
3	M2	Z	.009	.009	0	0
4	M7	Z	.009	.009	0	0
5	M8	Z	.009	.009	0	0
6	M3	Z	.009	.009	0	0

Basic Load Cases

	BLC Description	Category	X GraY Gra	Z Gra	Joint	Point	Distrib.	.Area(Surfa
1	Self Weight	DL	-1						
2	Dead Load	None				8			
3	Ice Load	None				8			
4	Wind with Ice X	None				8	7		
5	Wind X	None				8	7		
6	Wind with Ice Z	None				6	6		
7	Wind Z	None				6	6		

Load Combinations

	Description	Solve	P	S	BLC	Fac	BLC	Fac.	BLC	Fac	BLC	Fac.	BLC	Fac.	.BLC	Fac								
1	1.2D + 1.6W (X-direc	Yes	Υ		1	1.2	2	1.2	5	1.6														
2	0.9D + 1.6W (X-direc	Yes	Y		1	.9	2	.9	5	1.6														
3	1.2D + 1.0Di + 1.0Wi	Yes	Y		1	1.2	2	1.2	3	1	4	1												
4	1.2D + 1.6W (Z-direc	Yes	Y		1	1.2	2	1.2	7	1.6														
5	0.9D + 1.6W (Z-direc	Yes	Y		1	.9	2	.9	7	1.6														
6	1.2D + 1.0Di + 1.0Wi	Yes	Y		1	1.2	2	1.2	3	1	6	1												



June 8, 2020 11:45 AM Checked By:___

Envelope Joint Reactions

	Joint		X [k]	LC	Y [k]	LC	Z [k]	LC	MX [k-ft]	LC	MY [k-ft]	LC	MZ [k-ft]	LC
1	N15	max	1.292	6	1.045	3	0	1	0	6	0	6	0	6
2		min	497	2	.41	5	489	5	0	1	0	1	0	1
3	N16	max	571	5	1.029	6	0	1	0	6	0	6	0	6
4		min	-1.54	3	.396	2	923	5	0	1	0	1	0	1
5	N30	max	.47	4	.022	4	0	3	0	6	0	6	0	6
6		min	06	2	.013	2	-1.567	4	0	1	0	1	0	1
7	Totals:	max	0	6	2.089	6	0	3						
8		min	-1.761	1	.832	2	-2.978	4						

Envelope Joint Displacements

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotatio LC Z Rotatio LC
1	N1	max	.008	1	226	2	.006	3	-6.765e-07	2	7.276e-05 3 3.683e-03 6
2		min	.002	6	659	6	055	5	-2.121e-03	4	-2.531e-03 5 1.154e-03 2
3	N2	max	.008	1	219	2	.006	3	-6.765e-07	2	7.276e-05 3 3.683e-03 6
4		min	.002	6	637	6	04	5	-2.121e-03	4	-2.532e-03 5 1.154e-03 2
5	N3	max	.008	1	057	2	.027	4	-2.354e-07	2	1.093e-03 4 7.636e-03 6
6		min	.003	6	161	3	.001	2	-9.625e-04	4	5.471e-05 2 2.48e-03 2
7	N4	max	.008	1	005	6	.068	5	1.143e-03	4	7.301e-05 3 -5.397e-04 5
8		min	.003	5	009	1	002	3	1.375e-07	2	-3.433e-03 5 -8.887e-04 1
9	N5	max	.008	1	039	5	.269	5	2.187e-03	4	7.312e-05 3 -3.247e-04 2
10		min	.003	5	057	1	006	3	2.18e-07	2	-3.76e-03 5 -5.964e-04 6
11	N6	max	.008	1	041	5	.291	5	2.187e-03	4	7.312e-05 3 -3.251e-04 2
12		min	.003	5	059	1	006	3	2.18e-07	2	-3.762e-03 5 -5.97e-04 6
13	N7	max	.008	1	0	5	.004	5	4.423e-08	2	7.275e-05 3 1.324e-03 3
14		min	.003	5	0	3	0	1	-4.879e-04	5	-2.252e-04 5 6.064e-04 5
15	N8	max	.006	2	227	2	.753	4	-9.706e-07	2	5.84e-03 4 3.61e-03 3
16		min	001	6	658	6	.005	2	-2.383e-02	4	5.513e-05 2 1.243e-03 5
17	N9	max	.006	2	219	2	.718	4	-9.706e-07	2	5.839e-03 4 3.609e-03 3
18		min	001	6	636	6	.004	2	-2.383e-02	4	5.513e-05 2 1.242e-03 5
19	N10	max	.005	2	057	2	.226	4	-3.711e-07	2	1.013e-02 4 7.694e-03 3
20		min	002	6	161	3	.001	2	-7.946e-03	4	5.531e-05 2 2.744e-03 5
21	N11	max	.004	2	005	6	001	2	1.793e-03	4	7.334e-05 3 -4.469e-04 5
22		min	003	6	009	1	025	4	5.785e-08	2	-1.513e-03 5 -7.703e-04 3
23	N12	max	.004	2	039	5	.142	5	2.509e-03	4	7.316e-05 3 -4.211e-04 5
24		min	003	6	057	1	006	3	1.785e-07	2	-3.751e-03 5 -6.467e-04 1
25	N13	max	.004	2	041	5	.165	5	2.509e-03	4	7.316e-05 3 -4.215e-04 5
26		min	003	6	061	1	006	3	1.785e-07	2	-3.752e-03 5 -6.473e-04 1
27	N14	max	.004	2	0	2	.002	5	-9.59e-08	2	4.475e-03 4 1.168e-03 6
28		min	003	6	0	6	0	1	-1.387e-04	4	5.504e-05 2 -1.282e-04 2
29	N15	max	0	6	0	6	0	6	6.132e-08	2	7.275e-05 3 1.3e-03 1
30		min	0	1	0	1	0	1	-7.482e-04	5	-2.252e-04 5 5.331e-04 6
31	N16	max	0	6	0	6	0	6	3.557e-04	5	4.475e-03 4 4.27e-04 6
32		min	0	1	0	1	0	1	-1.257e-07	1	5.504e-05 2 -7.711e-04 2
33	N17	max	02	2	057	2	.019	4	-2.354e-07	2	1.093e-03 4 7.64e-03 6
34		min	089	6	161	3	.001	2	-6.479e-04	4	5.471e-05 2 2.269e-03 2
35	N18	max	.02	1	005	6	.084	5	1.367e-03	4	7.301e-05 3 -5.398e-04 5
36		min	.01	5	009	1	002	3	1.375e-07	2	-3.433e-03 5 -1.004e-03 1
37	N19	max	.014	1	039	5	.295	5	2.187e-03	4	7.312e-05 3 -3.485e-04 2
38		min	.008	5	057	1	006	3	2.18e-07	2	-3.76e-03 5 -5.964e-04 6

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Envelope Joint Displacements (Continued)

	Joint		X [in]	LC	Y [in]	LC	Z [in]	LC	X Rotation [rad]	LC	Y Rotatio	LC	Z Rotatio	LC
39	N20	max	.092	3	057	2	.325	4	-3.711e-07	2	1.013e-02	4	7.741e-03	3
40		min	.033	5	161	3	.001	2	-8.258e-03	4	5.531e-05	2	2.743e-03	5
41	N21	max	001	2	005	6	001	2	1.793e-03	4	7.334e-05	3	-4.341e-04	2
42		min	012	6	009	1	046	4	5.785e-08	2	-1.513e-03	5	-7.676e-04	6
43	N22	max	002	2	039	5	.112	5	2.509e-03	4	7.316e-05	3	-4.211e-04	5
44		min	011	6	057	1	006	3	1.785e-07	2	-3.751e-03	5	-6.254e-04	3
45	N23	max	006	2	219	2	.006	3	-6.765e-07	2	7.276e-05	3	3.683e-03	6
46		min	042	6	637	6	065	5	-2.097e-03	4	-2.532e-03	5	1.13e-03	2
47	N24	max	.043	3	219	2	1.005	4	-9.706e-07	2	5.839e-03	4	3.614e-03	3
48		min	.015	5	636	6	.004	2	-2.386e-02	4	5.513e-05	2	1.242e-03	5
49	N25	max	.008	1	211	2	.005	3	-6.718e-07	2	7.272e-05	3	4.786e-03	6
50		min	.002	6	611	6	024	5	-1.745e-03	4	-2.455e-03	5	1.247e-03	2
51	N26	max	.006	2	21	2	.682	4	-9.228e-07	2	6.471e-03	4	4.822e-03	3
52		min	001	6	611	6	.004	2	-2.353e-02	4	5.516e-05	2	1.731e-03	5
53	N27	max	.032	2	211	2	.07	5	5.685e-03	5	7.272e-05	3	4.809e-03	6
54		min	113	6	612	6	.004	2	-2.061e-06	3	-2.455e-03	5	-1.667e-03	2
55	N28	max	.128	3	21	2	1.382	4	-9.221e-07	2	6.471e-03	4	5.48e-03	3
56		min	.042	5	611	6	.004	2	-3.091e-02	4	5.516e-05	2	1.73e-03	5
57	N29	max	.022	4	219	2	.014	4	-8.373e-07	2	7.299e-05	3	5.38e-04	5
58		min	.014	2	637	6	.004	2	-8.749e-03	4	-4.427e-04	5	-4.598e-04	3
59	N30	max	0	6	0	6	0	6	7.133e-03	3	3.509e-03	1	4.121e-03	4
60		min	0	1	0	1	0	1	1.942e-03	5	4.29e-04	6	8.22e-04	2

Envelope AISC 14th(360-10): LRFD Steel Code Checks

	Member	Shape	Code Check	Lo	LC	She	Lo		.phi*P	phi*P	phi*	phi*	Cb	Eqn
1	M1	PIPE_2.5	.447	7.25	6	.119	.604	5	10.82	50.715	3.596	3.596	1.8	.H1
2	M2	PIPE_2.5	.536	7.25	4	.298	4	4	10.82	50.715	3.596	3.596	1.8	H3-6
3	M3	PIPE_2.0	.650	2	4	.229	2	5	20.867	32.13	1.872	1.872	1.8	.H1
4	M4	PIPE_2.0	.627	5	3	.160	1	4	20.867	32.13	1.872	1.872	1.7	.H1
5	M5	PIPE_2.0	.096	5	4	.047	1	4	20.867	32.13	1.872	1.872	1.7	.H1
6	M6	PIPE_2.0	.045	1	1	.007	1	1	20.867	32.13	1.872	1.872	1.8	.H1
7	M7	PIPE_2.5	.213	4	3	.101	5	3	41.332	50.715	3.596	3.596	2.5	.H1
8	M8	PIPE_2.0	.574	2	4	.200	2	4	14.916	32.13	1.872	1.872	1.4	.H1
9	M9	PIPE_2.0	.067	4	1	.006	8	1	13.839	32.13	1.872	1.872	1.1	.H1



Exhibit F Power Density/RF Emissions Report



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11014B

CT014/ I-95/ X24/ Bla 645 Pine Street Bridgeport, Connecticut 06605

July 24, 2020

EBI Project Number: 6220003389

Site Compliance Summary							
Compliance Status:	COMPLIANT						
Site total MPE% of FCC general population allowable limit:	19.63%						



July 24, 2020

T-Mobile Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, Connecticut 06002

Emissions Analysis for Site: CT11014B - CT014/ I-95/ X24/ Bla

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **645 Pine Street** in **Bridgeport, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm²). The number of μ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

<u>General population/uncontrolled exposure</u> limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400 μ W/cm² and 467 μ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



<u>Occupational/controlled exposure</u> limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over the potential for exposure and can exercise control over the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 645 Pine Street in Bridgeport, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) I NR channel (600 MHz Band) was considered for each sector of the proposed installation. This Channel has a transmit power of 80 Watts.
- 3) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 4 GSM channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 2 LTE channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.



- 6) 2 UMTS channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 7) 4 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 8) 2 LTE channels (BRS Band 2500 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 9) 2 NR channels (BRS Band 2500 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 10) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 11) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 12) The antennas used in this modeling are the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s) in Sector A, the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz channel(s) in Sector B, the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s) in Sector B, the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s), the Ericsson AIR 3246 for the 2500 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz / 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 3246 for the 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz / 2100 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative



estimate as gain reductions for these particular antennas are typically much higher in this direction.

- 13) The antenna mounting height centerline of the proposed antennas is 180 feet above ground level (AGL).
- 14) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 15) All calculations were done with respect to uncontrolled / general population threshold limits.



T-Mobile Site Inventory and Power Data

Sector	^	Sector	D	Sectory	C
Sector:	A	Sector:	D	Sector:	C
Antenna #:	I	Antenna #:	Ι	Antenna #:	
Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449	Make / Model:	Ericsson AIR 6449
Frequency Bands:	2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz	Frequency Bands:	2500 MHz / 2500 MHz
Gain:	22.05 dBd / 22.05 dBd	Gain:	22.05 dBd / 22.05 dBd	Gain:	22.05 dBd / 22.05 dBd
Height (AGL):	180 feet	Height (AGL):	180 feet	Height (AGL):	180 feet
Channel Count:	4	Channel Count:	4	Channel Count:	4
Total TX Power (W):	160 Watts	Total TX Power (W):	160 Watts	Total TX Power (W):	160 Watts
ERP (VV):	25,651.93	ERP (VV):	25,651.93	ERP (VV):	25,651.93
Antenna AI MPE %:	2.85%	Antenna BI MPE %:	2.85%	Antenna CI MPE %:	2.85%
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Ericsson AIR 3246	Make / Model:	Ericsson AIR 3246	Make / Model:	Ericsson AIR 3246
Frequency Bands:	2100 MHz	Frequency Bands:	2100 MHz	Frequency Bands:	2100 MHz
Gain:	15.85 dBd	Gain:	15.85 dBd	Gain:	15.85 dBd
Height (AGL):	180 feet	Height (AGL):	180 feet	Height (AGL):	180 feet
Channel Count:	4	Channel Count:	4	Channel Count:	4
Total TX Power (W):	160 Watts	Total TX Power (W):	160 Watts	Total TX Power (W):	160 Watts
ERP (VV):	6,153.47	ERP (VV):	6,153.47	ERP (VV):	6,153.47
Antenna A2 MPE %:	0.68%	Antenna B2 MPE %:	0.68%	Antenna C2 MPE %:	0.68%
Antenna #:	4	Antenna #:	4	Antenna #:	4
Make / Model:	RFS APXVAARR24_43-U- NA20	Make / Model:	RFS APXVAARR24_43-U- NA20	Make / Model:	RFS APXVAARR24_43-U- NA20
Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz	Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz / 1900 MHz / 2100 MHz
Gain:	12.95 dBd / 12.95 dBd / 13.35 dBd / 15.65 dBd / 15.65 dBd / 16.35 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.35 dBd / 15.65 dBd / 15.65 dBd / 16.35 dBd	Gain:	12.95 dBd / 12.95 dBd / 13.35 dBd / 15.65 dBd / 15.65 dBd / 16.35 dBd
Height (AGL):	180 feet	Height (AGL):	180 feet	Height (AGL):	180 feet
Channel Count:	13	Channel Count:	13	Channel Count:	13
Total TX Power (W):	500 Watts	Total TX Power (W):	500 Watts	Total TX Power (W):	500 Watts
ERP (W):	15,462.91	ERP (W):	15,462.91	ERP (W):	5,462.9
Antenna A4 MPE %:	2.34%	Antenna B4 MPE %:	2.34%	Antenna C4 MPE %:	2.34%



environmental | engineering | due diligence

Site Composite MPE %							
Carrier	MPE %						
T-Mobile (Max at Sector A):	5.87%						
Sprint	4.49%						
Verizon	6.41%						
Unknown	I.58%						
Metro PCS	I.28%						
Site Total MPE % :	19.63%						

T-Mobile MPE % Per Sector							
T-Mobile Sector A Total:	5.87%						
T-Mobile Sector B Total:	5.87%						
T-Mobile Sector C Total:	5.87%						
Site Total MPE % :	19.63%						

T-Mobile Maximum MPE Power Values (Sector A)

T-Mobile Frequency Band / Technology (Sector A)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm ²)	Frequency (MHz)	Allowable MPE (µW/cm²)	Calculated % MPE
T-Mobile 2500 MHz LTE	2	6412.98	180.0	14.23	2500 MHz LTE	1000	1.42%
T-Mobile 2500 MHz NR	2	6412.98	180.0	14.23	2500 MHz NR	1000	1.42%
T-Mobile 2100 MHz LTE	4	1538.37	180.0	6.83	2100 MHz LTE	1000	0.68%
T-Mobile 600 MHz LTE	2	591.73	180.0	1.31	600 MHz LTE	400	0.33%
T-Mobile 600 MHz NR	I	1577.94	180.0	1.75	600 MHz NR	400	0.44%
T-Mobile 700 MHz LTE	2	648.82	180.0	1.44	700 MHz LTE	467	0.31%
T-Mobile 1900 MHz GSM	4	1101.85	180.0	4.89	1900 MHz GSM	1000	0.49%
T-Mobile 1900 MHz LTE	2	2203.69	180.0	4.89	1900 MHz LTE	1000	0.49%
T-Mobile 2100 MHz UMTS	2	1294.56	180.0	2.87	2100 MHz UMTS	1000	0.29%
	•	•	•	•	•	Total:	5.87%

• NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	5.87%
Sector B:	5.87%
Sector C:	5.87%
T-Mobile Maximum	5 97%
MPE % (Sector A):	J.07 /6
Site Total:	19.63%
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **19.63%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Exhibit G Mailing Receipts/Proof of Notice

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