



Crown Castle
12 Gill Street, Suite 5800
Woburn, MA 01801

February 10, 2017

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

RE: Notice of Exempt Modification for Sprint / 2016-207 Crown Site BU: 822779
Sprint Site ID: CT54XC747
Located at: 1875 Nobel Avenue, Bridgeport, CT 06610
Latitude: 41° 12' 37.271" / Longitude: -73° 10' 52.259"

Dear Ms. Bachman,

Sprint currently maintains three (3) antennas at the 96-foot level of the existing 120-foot monopole at 1875 Nobel Avenue, Bridgeport, CT. The tower is owned by Crown Castle. The property is owned by The Connecticut Zoological Society. Sprint now intends to remove and replace the three (3) existing antennas with three (3) new antennas at the same 96-foot level and add: three (3) Nokia FWHR RRHs, three (3) diplexers, four (4) Belden fiber lines and one (1) Corning Ethernet line inside of 1" conduit, one (1) Southwire Power line inside of 1" conduit, and one (1) junction box.

This facility was approved by the Town of Bridgeport Zoning Department, File Number 2K-07 on March 31, 2000. This approval included the condition(s) that:

1. Stockade fencing not less than 6' high shall be installed to encompass & enclose the proposed equipment area.
2. No equipment shall exceed the height of the fencing required in condition No. 1 above.
3. Arborvitae trees no less than 6' high shall be planted at 6' intervals around the perimeter of the equipment enclosure area.
4. All required fencing & landscape trees are to be maintained at all times.

5. A "Removal Bond" as determined by the City Attorney's Office shall be filed with the Bridgeport Zoning Department prior to the Certificate of an Application for Zoning Compliance.

This modification complies with the aforementioned condition(s).

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16-50j-72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to the Honorable Joseph P. Ganim, Mayor for the Town of Bridgeport, the Planning & Economic Department for the Town of Bridgeport, the property owner and the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modification will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Amanda Goodall.

Melanie A. Bachman

February 10, 2017

Page 3

Sincerely,

Amanda Goodall

Real Estate Specialist

12 Gill Street, Suite 5800, Woburn, MA 01801

339-205-7017

Amanda.Goodall@crowncastle.com

Attachments:

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table report (RF Emissions Analysis Report)

cc: Joseph P. Ganim, Mayor
Town of Bridgeport
999 Broad Street
Bridgeport, CT 06604

Thomas F. Gill, Director of OPED
Office of Planning and Economic Development
999 Broad Street
Bridgeport, CT 06604

Crown Castle (Tower Owner)
12 Gill Street, Suite 5800
Woburn, Ma 01801

Connecticut Zoological Society (Property Owner)
1875 Nobel Ave
Bridgeport, CT 06610

ZONING DEPARTMENT
DEVELOPMENT ADMINISTRATION

City of Bridgeport



34

DATE: March 31, 2000

OUR FILE: # 2K-07

Attorney J. Brendan Sharkey
100 Filley Street
Bloomfield, CT 06002

RE: Site Plan Review
1875 Noble Avenue
Bridgeport, CT

Dear Attorney Sharkey:

At its meeting held on Monday, March 27, 2000, the Planning & Zoning Commission voted to approve conditionally the application submitted by you which sought a Site Plan Review under Sec. 14-2 of the Bridgeport Zoning Regulations to permit the installation of a 120' high flagpole which will house telecommunications antennas & associated equipment within the Beardsley Zoo pavilion in a ZOOLOGICAL PARK ZONE.

The Commission stipulated the following conditions for its approval:

1. Stockade fencing not less than 6' high shall be installed to encompass & enclose the proposed equipment area.
2. No equipment shall exceed the height of the fencing required in condition No. 1 above.
3. Arborvitae trees no less than 6' high shall be planted at 6' intervals around the perimeter of the equipment enclosure area.
4. All required fencing & landscape trees are to be maintained at all times.
5. A "Removal Bond" as determined by the City Attorney's Office shall be filed with the Bridgeport Zoning Department prior to the Certification Of An Application For Zoning Compliance.

The Commission assigned the following reason for its action:

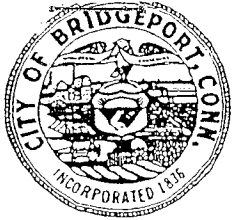
1. As to the Site Plan Review, the project, as approved, complies with the standards of Sec. 14-2-5 of the Bridgeport Zoning Regulations.

Very truly yours,

A handwritten signature in black ink that reads "William A. Shaw". The signature is written in a cursive style with a large, prominent initial "W".

William A. Shaw, Clerk
Planning & Zoning Commission

WAS:map



NO.
APPLICATION FOR CERTIFICATE OF ZONING COMPLIANCE
ZONING COMMISSION
CITY OF BRIDGEPORT, CONN.

CT11-240A
CITY HALL
 45 Lyon Terrace
 Room No. 206
 Bridgeport, Conn.

Applicant Omnipoint Communications, Inc. Date 5/17/00 19.....

Address of Work 1875 Noble Ave ^{Owner or Tenant Only}
45 Lyons Terrace
 Number

on the corner of Noble & East main St side of the above street about feet

from Beardsley Zoo Lot No. 9-9A-9-B-9C
 North, South, East, West Street

Block No. 3000 as shown on Tax Assessor's Maps. C.A.M. Area NO Wetlands NO
 Yes - No Yes - No

Dimension of Lot: Entire city block

Size of Proposed Building or Addition No. Stories

Wood Frame Brick Veneer Masonry

Other Work (Describe in Detail) Installation of telecommunication antennas and associated equipment. (flagpole)

Proposed Use of Above (Describe in Detail) Telecommunication antenna for cell phones. as approved by Z.B.P. 1/11/00 P.Z. approval 3/27/00

Presently Existing Use 200 Zone ZP

Previous use and date discontinued (if applicable)

Is pre-existing right claimed yes
 Yes - No

Signature J. Brendan Sharkey Print Name J. Brendan Sharkey, Esq.

If signed by agent state capacity (attorney, builder, etc.) Attorney for Omnipoint Communications (The Applicant)

Mailing Address 100 Filley Street, Bloomfield, CT 06002 Phone No. 860/692-7100

INSTRUCTIONS

Fill Out This Application In Ink or Type

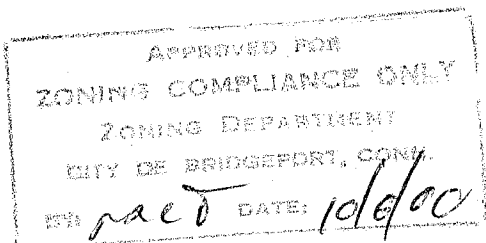
A detailed plot plan must be submitted with this application showing the proposed or existing lot and building dimensions and the location of all buildings in relation to the street line, side lot lines and rear lot line. NOTE: The occupancy and use of land, buildings and structures prior to the issuance of a Certificate of Zoning Compliance is prohibited. This is not the said certificate. Fees, payable at the time of making application, are not returnable and, are in an amount established by the Zoning Commission.

Fee received 100 Date 5/17/00 19..... By paid

PLAN AND APPLICATION

C.A.M. APPROVAL

FINAL INSPECTION



Certificate Issued Date 19.....

1875 Noble Ave



Map data ©2017 Google 200 ft



SPRINT SITE NUMBER:
SPRINT SITE NAME:
SITE TYPE:
TOWER HEIGHT:

CT54XC747

FLAGPOLE
120'-0"

CROWN CASTLE BU #: 822779
SITE ADDRESS:
COUNTY:
JURISDICTION:

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610
FAIRFIELD
CITY OF BRIDGEPORT

SPRINT 2016-2017 LOCAL ASK INITIATIVE



SPRINT SITE NUMBER:
CT54XC747
BU #: 822779
BRIDGEPORT/ RT 8
1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

SITE INFORMATION

CROWN CASTLE SITE NAME: BRIDGEPORT/ RT 8
 SITE ADDRESS: 1875 NOBLE AVENUE BRIDGEPORT, CT 06610
 COUNTY: FAIRFIELD
 MAP/PARCEL #: BRID-003000-000009A
 AREA OF CONSTRUCTION: EXISTING
 LATITUDE: 41° 12' 37.271"
 LONGITUDE: -73° 10' 52.259"
 LAT/LONG TYPE: NAD83
 GROUND ELEVATION: 102.0 FT.
 CURRENT ZONING: Z-P
 JURISDICTION: CITY OF BRIDGEPORT
 OCCUPANCY CLASSIFICATION: U
 TYPE OF CONSTRUCTION: VB
 A.D.A. COMPLIANCE: FACILITY IS UNMANNED AND NOT FOR HUMAN HABITATION
 PROPERTY OWNER: CONNECTICUT ZOOLOGICAL SOCIETY 1875 NOBLE AVE C/O BEARDSLEY ZOO BRIDGEPORT, CT 16610-1646
 TOWER OWNER: CCTMO LLC 2000 CORPORATE DRIVE CANONSBURG, PA 15317
 CARRIER/APPLICANT: SPRINT 6391 SPRINT PARKWAY OVERLAND PARK, KS 66251-2650
 CROWN CASTLE APPLICATION ID: 368093
 ELECTRIC PROVIDER: CPL (800) 788-5456
 TELCO PROVIDER: AT&T (866) 620-6900

DRAWING INDEX

SHEET #	SHEET DESCRIPTION
T-1	TITLE SHEET
T-2	GENERAL NOTES
T-3	GENERAL NOTES
C-1	ENLARGED SITE PLAN
C-2	EXISTING AND NEW ELEVATION
C-3	ANTENNA PLANS AND SCHEMATIC
C-4	CONDUIT ROUTING SCHEMATIC
C-5	INSTALLATION SPECS AND DETAILS
C-6	EQUIPMENT SPECIFICATIONS
E-1	ELECTRICAL SPECIFICATIONS
G-1	GROUNDING DETAILS
G-2	GROUNDING DETAILS

ALL DRAWINGS CONTAINED HEREIN ARE FORMATTED FOR FULL SIZE. CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

PROJECT DESCRIPTION

THE PURPOSE OF THIS PROJECT IS TO ENHANCE BROADBAND CONNECTIVITY AND CAPACITY TO THE EXISTING ELIGIBLE WIRELESS FACILITY.

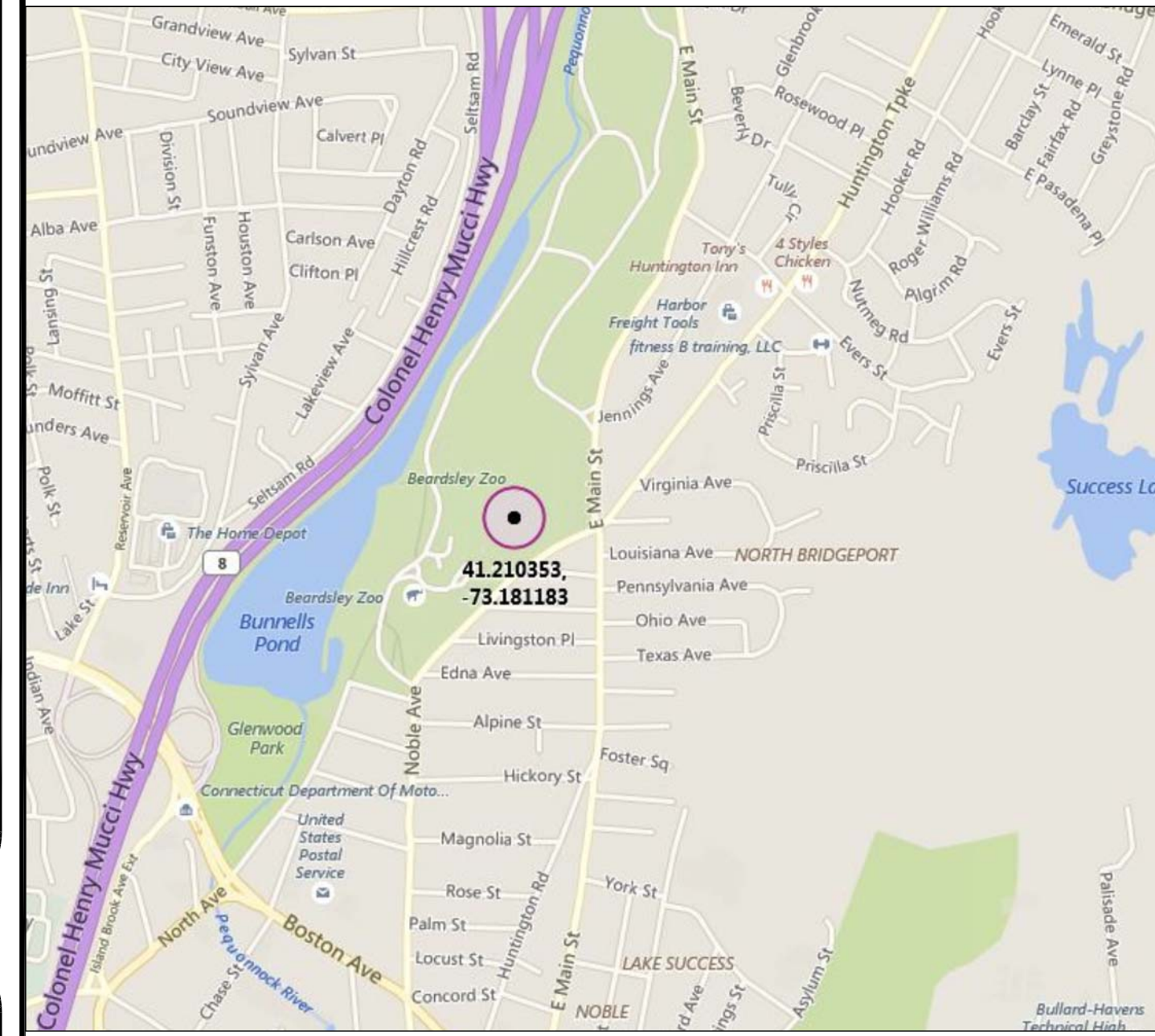
- REMOVE (3) ANTENNAS
- INSTALL (3) ANTENNAS
- INSTALL (3) RRHS
- INSTALL (3) DIPLEXERS
- INSTALL (1) JUNCTION BOX
- INSTALL (4) 17/64" FIBER LINES AND (1) 1/8" ETHERNET CABLE INSIDE 1" CONDUIT
- INSTALL (1) 7/8" POWER LINE INSIDE 1" CONDUIT

DESIGN PACKAGE BASED ON THE APPLICATION ID: 368093
 REVISION: 5

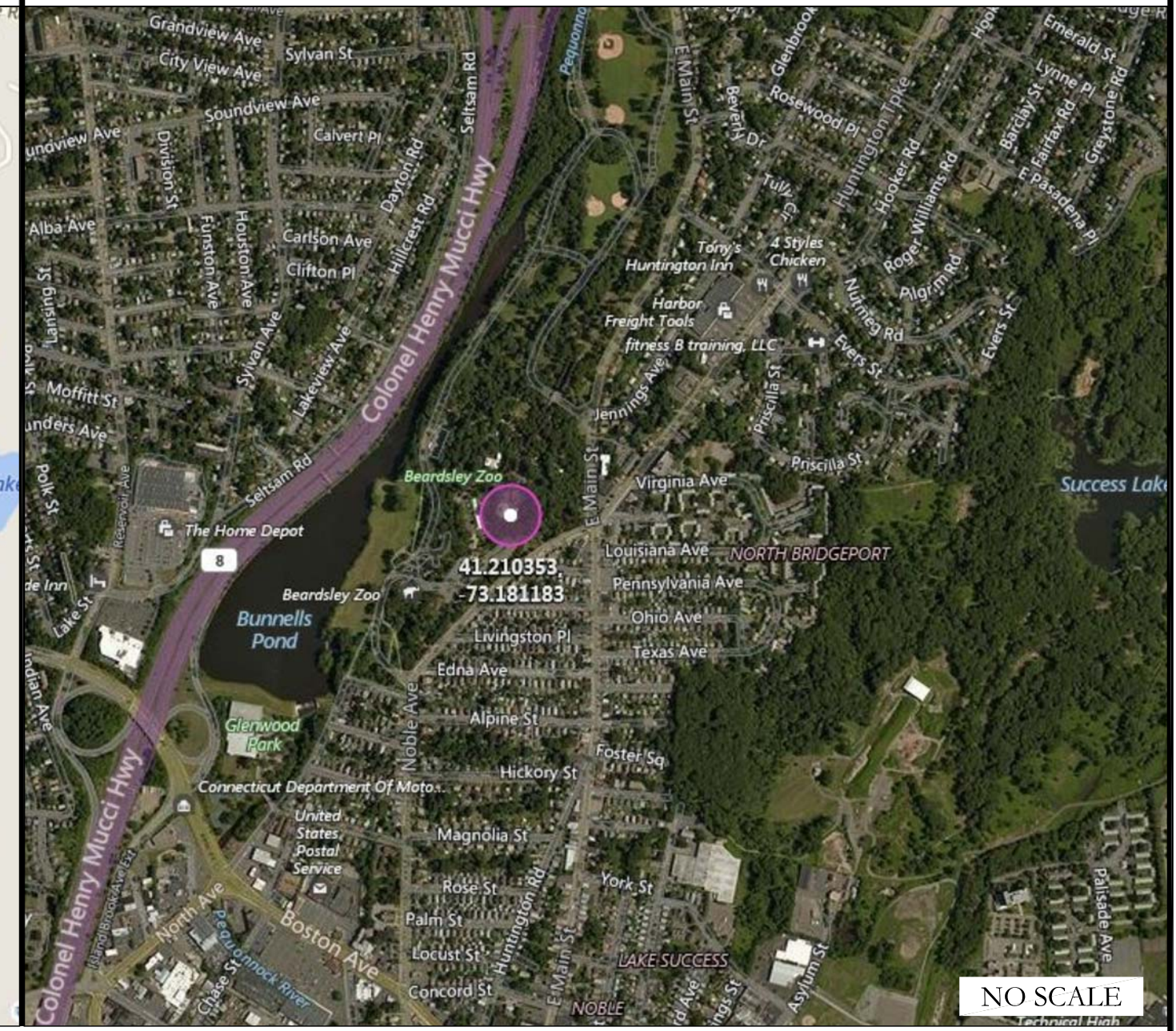
INSTALLER NOTE:
 TOWER DOES NOT HAVE CLIMBING FACILITIES - MANLIFT REQUIRED FOR ELEVATED WORK.

THE PARTIES ABOVE HEREBY APPROVE AND ACCEPT THESE DOCUMENTS AND AUTHORIZE THE CONTRACTOR TO PROCEED WITH THE CONSTRUCTION DESCRIBED HEREIN. ALL CONSTRUCTION DOCUMENTS ARE SUBJECT TO REVIEW BY THE LOCAL BUILDING DEPARTMENT AND ANY CHANGES AND MODIFICATIONS THEY MAY IMPOSE.

VICINITY MAP



AERIAL MAP



DRIVING DIRECTIONS FROM BRADLEY INTERNATIONAL AIRPORT:

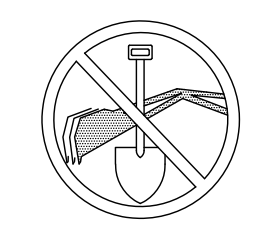
EXIT BRADLEY INTERNATIONAL AIRPORT VIA SCHOEPHOESTER RD TOWARD CT-20 E. CONTINUE ONTO CT-20 E/BRADLEY INTERNATIONAL AIRPORT CON, THEN USE THE RIGHT TWO LANES TO TAKE THE I-91S EXIT TOWARD HARTFORD. TAKE EXIT 17 FOR CT-155/WILBUR CROSS PKWY. TAKE EXIT 52 FOR STATE ROUTE 108S/STATE ROUTE 8S TOWARD BRIDGEPORT. TAKE EXIT 7 FOR CT-127/WHITE PLAINS ROAD. TURN LEFT ONTO CT-127S/WHITE PLAINS ROAD. TURN RIGHT ONTO NOBLE AVE. TURN RIGHT TO ENTER BEARDSLEY ZOO PARKING LOT. UPON ENTERING, INFORM TICKET WINDOW OPERATOR THAT ACCESS TO FLAGPOLE IS REQUIRED.

APPLICABLE CODES/REFERENCE DOCUMENTS

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES:

CODE TYPE	CODE
BUILDING	2016 CONNECTICUT STATE BUILDING CODE/2012 IBC W/ CT AMENDMENTS
MECHANICAL	2016 CONNECTICUT STATE BUILDING CODE/2012 IMC W/ CT AMENDMENTS
ELECTRICAL	2016 CONNECTICUT STATE BUILDING CODE/2014 NEC W/ CT AMENDMENTS

REFERENCE DOCUMENTS:
 STRUCTURAL ANALYSIS: BY OTHERS



CALL CONNECTICUT ONE CALL
 (800) 922-4455
 CALL 3 WORKING DAYS BEFORE YOU DIG!



APPROVALS

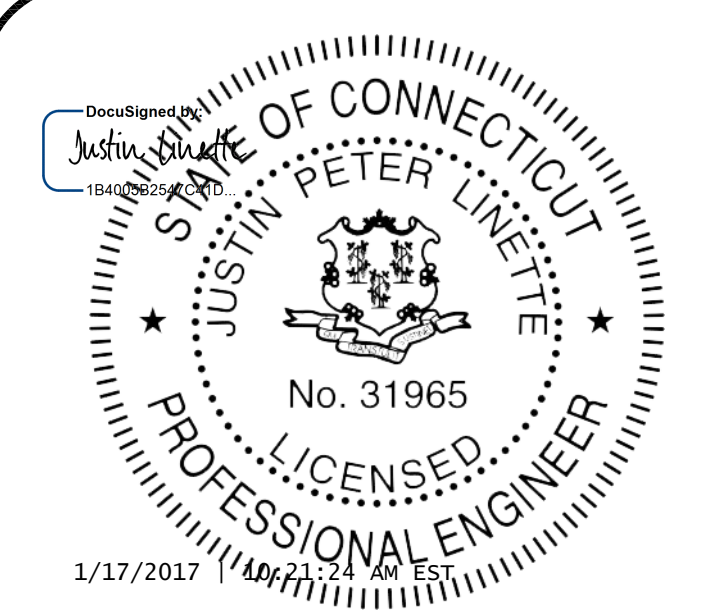
APPROVAL	SIGNATURE	DATE
SITE ACQ. & ZONING	_____	_____
CONSTRUCTION MGR	_____	_____
A&E MGR	_____	_____
PLANNING CONSULTANT	_____	_____
RF MGR	_____	_____
PROPERTY OWNER	_____	_____
SPRINT REP.	_____	_____

PROJECT TEAM

CROWN CASTLE A&E FIRM:
 CROWN CASTLE
 2000 CORPORATE DRIVE
 CANONSBURG, PA 15317
 CROWNAE.APPROVAL@CROWNCastle.COM
 CROWN CASTLE CONTACTS:
 3 CORPORATE PARK DRIVE, SUITE 101
 CLIFTON PARK, NY 12065
 MARYELLEN PERROTTA - PROJECT MANAGER (781) 970-0057
 JASON D'AMICO - CONSTRUCTION MANAGER (860) 209-0104
 WILLIAM STONE - A&E PROJECT MANAGER
 WILLIAM.STONE.CONTRACTOR@CROWNCastle.COM (518) 373-3543
 SPRINT CONTACT:
 MICHELLE HISERT
 MICHELLE.HISERT@SPRINT.COM

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



Justin Peter Linette, P.E.
 Professional Engineer License: 31965
 Crown Castle USA, Inc. Firm Registration #PEC.0001101
 IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER, TO ALTER THIS DOCUMENT.

SHEET NUMBER:
T-1
REVISION:
0

CROWN CASTLE SITE WORK GENERAL NOTES:

1. THE SUBCONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
2. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY CONTRACTOR. EXTREME CAUTION SHOULD BE USED BY THE SUBCONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES, SUBCONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING AND EXCAVATION.
3. ALL SITE WORK TO COMPLY WITH QAS--STD--10068 "INSTALLATION STANDARDS FOR CONSTRUCTION ACTIVITIES ON CROWN CASTLE TOWER SITE" AND LATEST VERSION OF TIA 1019 "STANDARD FOR INSTALLATION, ALTERATION, AND MAINTENANCE OF ANTENNA SUPPORTING STRUCTURES AND ANTENNAS."
4. ALL SITE WORK SHALL BE AS INDICATED ON THE STAMPED CONSTRUCTION DRAWINGS AND PROJECT SPECIFICATIONS.
5. IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
6. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF CONTRACTOR, OWNER AND/OR LOCAL UTILITIES.
7. THE SUBCONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE TECHNICAL SPECIFICATION FOR SITE SIGNAGE.
8. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE BTS EQUIPMENT AND TOWER AREAS.
9. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
10. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
11. THE AREAS OF THE OWNERS PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER, EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE, AND STABILIZED TO PREVENT EROSION AS SPECIFIED ON THE PROJECT SPECIFICATIONS.
12. SUBCONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
13. NOTICE TO PROCEED-- NO WORK TO COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE OF A PURCHASE ORDER.
14. ALL CONSTRUCTION MEANS AND METHODS; INCLUDING BUT NOT LIMITED TO, ERECTION PLANS, RIGGING PLANS, CLIMBING PLANS, AND RESCUE PLANS SHALL BE THE RESPONSIBILITY OF THE GENERAL CONTRACTOR RESPONSIBLE FOR THE EXECUTION OF THE WORK CONTAINED HEREIN AND SHALL MEET ANSI/TIA 1019 (LATEST EDITION), OSHA, AND GENERAL INDUSTRY STANDARDS. ALL RIGGING PLANS SHALL ADHERE TO ANSI/TIA-1019 (LATEST EDITION) INCLUDING THE REQUIRED INVOLVEMENT OF A QUALIFIED ENGINEER FOR CLASS IV CONSTRUCTION.

SPRINT CONSTRUCTION NOTES

SECTION 01 100 -- SCOPE OF WORK

THE WORK:

MUST COMPLY WITH ALL APPLICABLE ADOPTED CODES AND STANDARDS, AND PORTIONS THEREOF. SPRINT METHOD OF PROCEDURE (MOP) AND SPRINT STANDARDS AT THE TIME OF CONSTRUCTION START.

PRECEDENCE:

SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES INCLUDING THE STANDARD DETAILS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. ALONG WITH SPRINT CONSTRUCTION MANAGER APPROVAL.

SITE FAMILIARITY:

CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING THEMSELVES WITH ALL CONTRACT DOCUMENTS, FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION.

ON-SITE SUPERVISION:

THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.

DRAWINGS, SPECIFICATIONS AND DETAILS REQUIRED AT JOBSITE:

THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.

A. DETAILS ARE INTENDED TO SHOW DESIGN INTENT. PROVIDE ALL MATERIALS AND LABOR AS REQUIRED TO PROVIDE A COMPLETE FUNCTIONING SYSTEM. MODIFICATIONS MAY BE REQUIRED TO SUITE JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK.

B. CONTRACTOR SHALL NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY VARIATIONS PRIOR TO PROCEEDING WITH THE WORK. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. MODIFICATIONS MAY BE REQUIRED TO SUIT JOB DIMENSIONS OR CONDITIONS, AND SUCH MODIFICATIONS SHALL BE INCLUDED AS PART OF THE WORK.

C. MARK THE FIELD SET OF DRAWINGS IN RED, DOCUMENTING ANY CHANGES FROM THE CONSTRUCTION DOCUMENTS.

METHODS OF PROCEDURE (MOPS) FOR CONSTRUCTION:

CONTRACTOR SHALL PERFORM WORK AS DESCRIBED IN THE FOLLOWING INSTALLATION AND COMMISSIONING MOPS. CONTRACTOR IS RESPONSIBLE FOR DISTRIBUTION OF LATEST MOPS.

- A. TOP HAT
- B. HOW TO INSTALL A NEW CABINET
- C. BASE BAND UNIT IN EXISTING UNIT
- D. INSTALLATION OF BATTERIES
- E. INSTALLATION OF FIBER CABLE
- F. INSTALLATION OF RRU'S
- G. CABLING
- H. TS-0200 REV 5 -- ANTENNA LINE ACCEPTANCE STANDARDS
- I. SPRINT CELL SITE ENGINEERING NOTICE -- EN 2012-001, REV 1.
- J. COMMISSIONING MOPS

SECTION 01 200 -- COMPANY FURNISHED MATERIAL AND EQUIPMENT

- A. COMPANY FURNISHED MATERIAL AND EQUIPMENT IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DRAWINGS.
- B. CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT TO ENSURE IT IS PROTECTED AND HANDLED PROPERLY THROUGHOUT THE CONSTRUCTION DURATION.
- C. CONTRACTOR IS RESPONSIBLE FOR RECEIPT OF SPRINT FURNISHED EQUIPMENT AT CELL SITE OR CONTRACTORS LOCATION. CONTRACTOR TO COMPLETE SHIPPING AND RECEIPT DOCUMENTATION

IN ACCORDANCE WITH COMPANY PRACTICE. CONTRACTOR MAY BE REQUIRED TO PICK UP MATERIAL AT LOCATION PRESCRIBED BY SPRINT.

SECTION 01 300 -- CELL SITE CONSTRUCTION

NOTICE TO PROCEED:

NO WORK SHALL COMMENCE PRIOR TO COMPANY'S WRITTEN NOTICE TO PROCEED AND THE ISSUANCE OF WORK ORDER.

SITE CLEANLINESS:

CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.

SECTION 01 400 -- SUBMITTALS AND TESTS

ALTERNATIVES:

AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED.

TESTS AND INSPECTIONS:

A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.

B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:

1. COAX SWEEPS AND FIBER TESTS PER TS-200 REV 5 ANTENNA LINE ACCEPTANCE STANDARDS.
2. AGL, AZIMUTH AND DOWNTILT: PROVIDE AN AUTOMATED REPORT UPLOADED TO SITERRA USING A COMMERCIAL MADE-FOR PURPOSE ELECTRONIC ANTENNA ALIGNMENT TOOL (AAT). INSTALLED AZIMUTH, CENTERLINE AND DOWNTILT MUST CONFORM WITH RF CONFIGURATION DATA.
3. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
4. ALL TESTING REQUIRED BY APPLICABLE INSTALLATION MOPS.

C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING:

1. AZIMUTH, DOWNTILT, AGL FROM SUNSIGHT INSTRUMENTS -- ANTENNA ALIGNMENT TOOL (AAT)
2. SWEEP AND FIBER TESTS.
3. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT.
4. ALL AVAILABLE JURISDICTIONAL PERMIT AND OCCUPANCY INFORMATION.
5. PDF SCAN OF REDLINES PRODUCED IN FIELD.
6. A PDF SCAN OF REDLINE MARK-UPS SUITABLE FOR USE IN ELECTRONIC AS-BUILT DRAWING PRODUCTION.
7. LIEN WAIVERS.
8. FINAL PAYMENT APPLICATION.
9. REQUIRED FINAL CONSTRUCTION PHOTOS.
10. CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS.
11. APPLICABLE POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLETED IN SITERRA (SPRINT'S DOCUMENT REPOSITORY OF RECORD).
12. CLOSEOUT PHOTOGRAPHS AND CLOSEOUT CHECKLIST: SPRINT WILL PROVIDE SEPARATE GUIDANCE.

a. PROVIDE PHOTOGRAPHS OF FINAL PROJECT PER THE FOLLOWING LIST. ADDITIONAL PHOTOS MAY BE REQUIRED TO SUPPORT ACCEPTANCE PROCESSES

- (i) BACK MAIN FIBER CABLE ROUTE (MINIMUM TWO PHOTOS)
 - (ii) OF EACH ANTENNA AND RRU
 - (iii) MANUFACTURERS NAME TAG FOR ALL SERIALIZED EQUIPMENT
 - (iv) PULL AND DISTRIBUTION BOXES INTERMEDIATE BETWEEN RRU'S AND RBS (DOOR OPEN)
 - (v) RBS CABINET WITH DOOR OPEN SHOWING MODIFICATIONS
 - (vi) POWER CABINET, DOORS OPEN, BATTERIES INSTALLED
 - (vii) BREAK OUT CYLINDERS
 - (viii) ASR SIGNAGE FOR SPRINT OWNED TOWERS
 - (ix) RADIATION EXPOSURE WARNING SIGNS
 - (x) PHOTOGRAPH FROM EACH SECTOR FROM APPROXIMATELY RAD CENTER OF ANY NEW ANTENNA AT HORIZON.
- b. LOAD PHOTOS TO SITERRA PROJECT LIBRARY 15. IN 15 CREATE NEW CATEGORY: 2.5 DEPLOYMENT, AND SECTION: PERMANENT CONSTRUCTION. LABEL PHOTOS WITH SITE CASCADE AND VIEW BEING DEPICTED. CAMERAS USED TO TAKE PHOTOS SHALL BE GPS ENABLED SUCH THAT THE GPS COORDINATES ARE INCLUDED IN THE PHOTO MEDIA-FILE INFORMATION.

COMMISSIONING:

PERFORM ALL COMMISSIONING AS REQUIRED BY APPLICABLE MOPS

INTEGRATION:

PERFORM ALL INTEGRATION ACTIVITIES AS REQUIRED BY APPLICABLE MOPS

SECTION 09 900 -- PAINTING

QUALITY ASSURANCE:

A. COMPLY WITH GOVERNING CODES AND REGULATIONS. PROVIDE PRODUCTS OF ACCEPTABLE MANUFACTURERS WHICH HAVE BEEN IN SATISFACTORY USE IN SIMILAR SERVICE FOR THREE YEARS. USE EXPERIENCED INSTALLERS. DELIVER, HANDLE, AND STORE MATERIALS IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS.

B. COMPLY WITH ALL ENVIRONMENTAL REGULATIONS FOR VOLATILE ORGANIC COMPOUNDS.

MATERIALS:

A. MANUFACTURERS: BENJAMIN MOORE, ICI DEVOE COATINGS, PPG, SHERWIN WILLIAMS OR APPROVED PROVIDE PREMIUM GRADE, PROFESSIONAL-QUALITY PRODUCTS FOR COATING SYSTEMS.

PAINT SCHEDULE:

A. EXTERIOR ANTENNAE AND ANTENNA MOUNTING HARDWARE: ONE COAT OF PRIMER AND TWO FINISH COATS. PAINT FOR ANTENNAE SHALL BE NON-METALLIC BASED AND CONTAIN NO METALLIC PARTICLES. PROVIDE COLORS AND PATTERNS AS REQUIRED TO MASK APPEARANCE OF ANTENNAE ON ADJACENT BUILDING SURFACES AND AS ACCEPTABLE TO THE OWNER. REFER TO ANTENNA MANUFACTURER'S INSTRUCTION WHENEVER POSSIBLE.

B. WATER TANKS: TOUCH UP -- PREPARE SURFACES TO BE REPAIRED. FOLLOW INDUSTRY STANDARDS AND REQUIREMENTS OF OWNER TO MATCH EXISTING COATING AND FINISH.

PAINTING APPLICATION:

1. INSPECT SURFACES, REPORT UNSATISFACTORY CONDITIONS IN WRITING; BEGINNING WORK MEANS ACCEPTANCE OF SUBSTRATE.
2. COMPLY WITH MANUFACTURER'S INSTRUCTIONS AND RECOMMENDATIONS FOR PREPARATION, PRIMING AND COATING WORK. COORDINATE WITH WORK OF OTHER SECTIONS.
3. MATCH APPROVED MOCK-UPS FOR COLOR, TEXTURE, AND PATTERN. RE-COAT OR REMOVE AND REPLACE WORK WHICH DOES NOT MATCH OR SHOWS LOSS OF ADHESION.
4. CLEAN UP, TOUCH UP AND PROTECT WORK.

TOUCHUP PAINTING:

1. GALVANIZING DAMAGE AND ALL BOLTS AND NUTS SHALL BE TOUCHED UP AFTER TOWER ERECTION WITH "GALVANOX," "DRY GALV," OR "ZINC-IT".
2. FIELD TOUCHUP PAINT SHALL BE DONE IN ACCORDANCE WITH THE MANUFACTURER'S WRITTEN INSTRUCTIONS.
3. ALL METAL COMPONENTS SHALL BE HANDLED WITH CARE TO PREVENT DAMAGE TO THE COMPONENTS, THEIR PRESERVATIVE TREATMENT, OR THEIR PROTECTIVE COATINGS.

SECTION 11 700 -- ANTENNA ASSEMBLY, REMOTE RADIO UNITS AND CABLE INSTALLATION

SUMMARY:

THIS SECTION SPECIFIES INSTALLATION OF ANTENNAS, RRU'S, AND CABLE EQUIPMENT, INSTALLATION, AND TESTING OF COAXIAL FIBER CABLE.

ANTENNAS AND RRU'S:

THE NUMBER AND TYPE OF ANTENNAS AND RRU'S TO BE INSTALLED IS DETAILED ON THE CONSTRUCTION DRAWINGS.

NV FIBER CABLE:

EXISTING NV FIBER CABLE WILL BE USED AT EACH SITE. CABLE SHALL BE USED PER THE CONSTRUCTION DRAWINGS AND THE APPLICABLE MANUFACTURER'S REQUIREMENTS.

JUMPERS AND CONNECTIONS:

FURNISH AND INSTALL 1/2" COAX JUMPER CABLES BETWEEN THE RRU'S AND ANTENNAS. JUMPERS SHALL BE TYPE LDF 4, FLC 12-50, CR 540, OR FXL 540. SUPER-FLEX CABLES ARE NOT ACCEPTABLE JUMPERS BETWEEN THE RRU'S AND ANTENNAS OR TOWER TOP AMPLIFIERS SHALL CONSIST OF 1/2" FOAM DIELECTRIC, OUTDOOR RATED COAXIAL CABLE, MINIMUM LENGTH FOR JUMPER SHALL BE SO AS TO ALLOW FOR THE PROPER BEND RADIUS PER MANUFACTURER OR SPRINT SPECIFICATIONS.

REMOTE ELECTRICAL TILT (RET) CABLES:

MISCELLANEOUS:

INSTALL SPLITTERS, COMBINERS, FILTERS PER RF DATA SHEET, FURNISHED BY SPRINT.

ANTENNA INSTALLATION:

THE CONTRACTOR SHALL ASSEMBLE ALL ANTENNAS ONSITE IN ACCORDANCE WITH THE INSTRUCTIONS SUPPLIED BY THE MANUFACTURER. ANTENNA HEIGHT, AZIMUTH AND FEED ORIENTATION INFORMATION SHALL BE AS DESIGNATED ON THE CONSTRUCTION DRAWINGS.

A. THE CONTRACTOR SHALL POSITION THE ANTENNA ON TOWER PIPE MOUNTS SO THAT THE BOTTOM STRUT IS LEVEL. THE PIPE MOUNTS SHALL BE PLUMB TO WITHIN 1 DEGREE.

B. ANTENNA MOUNTING REQUIREMENTS: PROVIDE ANTENNA MOUNTING HARDWARE AS INDICATED ON THE CONSTRUCTION DRAWINGS.

FIBER CABLE INSTALLATION:

A. THE CONTRACTOR SHALL ROUTE, TEST AND INSTALL ALL CABLES AS INDICATED ON THE CONSTRUCTION DRAWINGS AND IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.

B. THE INSTALLED RADIUS OF THE CABLES SHALL NOT BE LESS THAT THE MANUFACTURER'S SPECIFICATIONS FOR BENDING RADI.

C. EXTREME CARE SHALL BE TAKEN TO AVOID DAMAGE TO THE CABLES DURING HANDLING AND INSTALLATION.

1. FASTENING MAIN FIBER CABLES:

LATTICE AND GUYED TOWERS:

ALL CABLES SHALL BE PERMANENTLY FASTENED TO THE COAX LADDER AT 4'-0" OC USING NON-MAGNETIC STAINLESS STEEL CLIPS. HOISTING GRIPS SHOULD BE INSTALLED AT MID-POINT IF CABLE RUN EXCEEDS 200' AS WELL AS TOP SIDE.

MONOPOLE:

ALL CABLES SHALL BE PERMANENTLY SUPPORTED WITH HOISTING GRIPS AT INTERVALS OF NO MORE THAN 200' (ONE HOISTING GRIP PER COAX).

1. FASTENING INDIVIDUAL FIBER AND DC CABLES ABOVE BREAKOUT ENCLOSURE (MEDUSA). WITHIN THE MMBS CABINET AND ANY INTERMEDIATE DISTRIBUTION BOXES.

a. FIBER: SUPPORT FIBER BUNDLES USING 1/2" VELCRO STRAPS OF THE REQUIRED LENGTH AT 18" O.C. STRAPS SHALL BE UV, OIL AND WATER RESISTANT AND SUITABLE FOR INDUSTRIAL INSTALLATIONS AS MANUFACTURED BY TEXTOL OR APPROVED EQUAL.

b. DC: SUPPORT DC BUNDLES WITH ZIP TIES OF THE ADEQUATE LENGTH. ZIP TIES TO BE UV STABILIZED, BLACK NYLON, WITH TENSILE STRENGTH AT 12,000 PSI AS MANUFACTURED BY NELCO PRODUCTS OR EQUAL.

2. FASTENING OR SECURING JUMPERS SHOULD CONSIST OF STAINLESS STEEL CLIPS, 18" FROM REAR OF CONNECTOR AND 24" THEREAFTER AND AT NO TIME SHALL THEY CONTACT TOWER OR STRUCTURAL STEEL.

3. CABLE INSTALLATION:

a. INSPECT CABLE PRIOR TO USE FOR SHIPPING DAMAGE. NOTIFY THE CONSTRUCTION MANAGER.

b. CABLE ROUTING CABLE INSTALLATION SHALL BE PLANNED TO ENSURE THAT THE LINES WILL BE PROPERLY ROUTED IN THE CABLE ENVELOPE AS INDICATED ON THE DRAWINGS. AVOID TWISTING AND CROSSOVERS.

c. HOIST CABLE USING PROPER HOISTING GRIPS. DO NOT EXCEED MANUFACTURER'S RECOMMENDED MAXIMUM BEND RADIUS.

5. GROUNDING OF TRANSMISSION LINES: ALL TRANSMISSION LINES SHALL BE GROUNDED AS INDICATED ON DRAWINGS.

6. HYBRID CABLE COLOR CODING: ALL COLOR CODING SHALL BE AS REQUIRED IN TS 0200 REV 5.

7. HYBRID CABLE LABELING: INDIVIDUAL HYBRID AND DC BUNDLES SHALL BE LABELED ALPHA-NUMERICALLY A ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE -- EN 2012-001, REV 1.



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

**SPRINT SITE NUMBER:
CT54XC747**

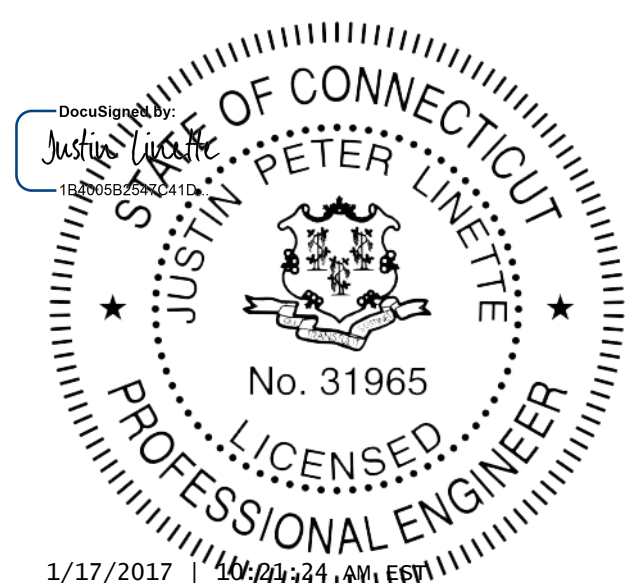
**BU #: 822779
BRIDGEPORT/ RT 8**

**1875 NOBLE AVENUE
BRIDGEPORT, CT 06610**

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



1/17/2017 1:40:44 PM EST

Justin Peter Linette, P.E.
Professional Engineer License: 31965
Crown Castle USA, Inc. Firm Registration #PEC.0001101

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SHEET NUMBER:

T-2

REVISION:

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WEATHERPROOFING EXTERIOR CONNECTORS AND HYBRID CABLE GROUND KITS:

- A. ALL FIBER AND COAX CONNECTORS AND GROUND KITS SHALL BE WEATHERPROOFED.
- B. WEATHERPROOFED USING ONE OF THE FOLLOWING METHODS. ALL INSTALLATIONS MUST BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND INDUSTRY BEST PRACTICES.

1. SELF-AMALGAMATING TAPE: CLEAN SURFACES. APPLY A DOUBLE WRAP OF SELF AMALGAMATING TAPE 2" BEYOND CONNECTOR. APPLY A SECOND WRAP OF SELF-AMALGAMATING TAPE IN OPPOSITE DIRECTION. APPLY DOUBLE WRAP OF 2" WIDE ELECTRICAL TAPE EXTENDING 2" BEYOND THE SELF AMALGAMATING TAPE.
2. 3M SLIM LOCK CLOSURE 716: SUBSTITUTIONS WILL NOT BE ALLOWED.
3. JMA-WPS SERIES ENCLOSURE.
4. BUTYL AND TAPE, 1 COMPLETE WRAP OF 3/4" PRE-TAPE, BUTYL WRAPPED IN HALF INCH LAP LAYERS, ENDED WITH SHINGLED DOWNWARD 3 WRAPS OF 2" TAPE, 3 WRAPS OF 3/4" TAPE SHINGLED DOWNWARD, FREE OF WRINKLES, BUCKLES AND FLAGGING.
5. OPEN FLAME ON JOB SITE IS NOT ACCEPTABLE

- C. ANTENNA MOUNTING REQUIREMENTS: PROVIDE ANTENNA MOUNTING HARDWARE AS INDICATED ON THE CONSTRUCTION DRAWINGS.

FIBER CABLE INSTALLATION:

- A. THE CONTRACTOR SHALL ROUTE, TEST AND INSTALL ALL CABLES AS INDICATED ON THE CONSTRUCTION DRAWINGS AND IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS.

- B. THE INSTALLED RADIUS OF THE CABLES SHALL NOT BE LESS THAT THE MANUFACTURER'S SPECIFICATIONS FOR BENDING RADII.

- C. EXTREME CARE SHALL BE TAKEN TO AVOID DAMAGE TO THE CABLES DURING HANDLING AND INSTALLATION.

- 1. FASTENING MAIN FIBER CABLES:

a. LATTICE AND GUYED TOWERS:

ALL CABLES SHALL BE PERMANENTLY FASTENED TO THE COAX LADDER AT 4'-0" OC USING NON-MAGNETIC STAINLESS STEEL CLIPS. HOISTING GRIPS SHOULD BE INSTALLED AT MID-POINT IF CABLE RUN EXCEEDS 200' AS WELL AS TOP SIDE.

b. MONOPOLE:

ALL CABLES SHALL BE PERMANENTLY SUPPORTED WITH HOISTING GRIPS AT INTERVALS OF NO MORE THAN 200' (ONE HOISTING GRIP PER COAX).

- 2. FASTENING INDIVIDUAL FIBER AND DC CABLES ABOVE BREAKOUT ENCLOSURE (MEDUSA). WITHIN THE MMBS CABINET AND ANY INTERMEDIATE DISTRIBUTION BOXES.

a. FIBER: SUPPORT FIBER BUNDLES USING 1/2" VELCRO STRAPS OF THE REQUIRED LENGTH AT 18" O.C. STRAPS SHALL BE UV, OIL AND WATER RESISTANT AND SUITABLE FOR INDUSTRIAL INSTALLATIONS AS MANUFACTURED BY TEXTOL OR APPROVED EQUAL.

b. DC: SUPPORT DC BUNDLES WITH ZIP TIES OF THE ADEQUATE LENGTH. ZIP TIES TO BE UV STABILIZED, BLACK NYLON, WITH TENSILE STRENGTH AT 12,000 PSI AS MANUFACTURED BY NELCO PRODUCTS OR EQUAL.

- 3. FASTENING OR SECURING JUMPERS SHOULD CONSIST OF STAINLESS STEEL CLIPS, 18" FROM REAR OF CONNECTOR AND 24" THEREAFTER AND AT NO TIME SHALL THEY CONTACT TOWER OR STRUCTURAL STEEL.

- 4. CABLE INSTALLATION:

- a. INSPECT CABLE PRIOR TO USE FOR SHIPPING DAMAGE. NOTIFY THE CONSTRUCTION MANAGER.

b. CABLE ROUTING CABLE INSTALLATION SHALL BE PLANNED TO ENSURE THAT THE LINES WILL BE PROPERLY ROUTED IN THE CABLE ENVELOPE AS INDICATED ON THE DRAWINGS. AVOID TWISTING AND CROSSEOVERS.

c. HOIST CABLE USING PROPER HOISTING GRIPS. DO NOT EXCEED MANUFACTURER'S RECOMMENDED MAXIMUM BEND RADIUS.

- 5. GROUNDING OF TRANSMISSION LINES: ALL TRANSMISSION LINES SHALL BE GROUNDED AS INDICATED ON DRAWINGS.

- 6. HYBRID CABLE COLOR CODING: ALL COLOR CODING SHALL BE AS REQUIRED IN TS 0200 REV 5.

- 7. HYBRID CABLE LABELING: INDIVIDUAL HYBRID AND DC BUNDLES SHALL BE LABELED ALPHA-NUMERICALLY ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE – EN 2012-001, REV 1.

WEATHERPROOFING EXTERIOR CONNECTORS AND HYBRID CABLE GROUND KITS:

- A. ALL FIBER AND COAX CONNECTORS AND GROUND KITS SHALL BE WEATHERPROOFED.

- B. WEATHERPROOFED USING ONE OF THE FOLLOWING METHODS. ALL INSTALLATIONS MUST BE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND INDUSTRY BEST PRACTICES.

1. SELF-AMALGAMATING TAPE: CLEAN SURFACES. APPLY A DOUBLE WRAP OF SELF AMALGAMATING TAPE 2" BEYOND CONNECTOR. APPLY A SECOND WRAP OF SELF-AMALGAMATING TAPE IN OPPOSITE DIRECTION. APPLY DOUBLE WRAP OF 2" WIDE ELECTRICAL TAPE EXTENDING 2" BEYOND THE SELF AMALGAMATING TAPE.
2. 3M SLIM LOCK CLOSURE 716: SUBSTITUTIONS WILL NOT BE ALLOWED.
3. JMA-WPS SERIES ENCLOSURE.
4. BUTYL AND TAPE, 1 COMPLETE WRAP OF 3/4" PRE-TAPE, BUTYL WRAPPED IN HALF INCH LAP LAYERS, ENDED WITH SHINGLED DOWNWARD 3 WRAPS OF 2" TAPE, 3 WRAPS OF 3/4" TAPE SHINGLED DOWNWARD, FREE OF WRINKLES, BUCKLES AND FLAGGING.
5. OPEN FLAME ON JOB SITE IS NOT ACCEPTABLE

SECTION 11 800 – INSTALLATION OF MULTIMODAL BASE STATIONS (MMBS) AND RELATED EQUIPMENT

SUMMARY:

A. THIS SECTION SPECIFIES MMBS CABINETS, POWER CABINETS, AND INTERNAL EQUIPMENT INCLUDING BUT NOT LIMITED TO RECTIFIERS, POWER DISTRIBUTION UNITS, BASE BAND UNITS, SURGE ARRESTORS, BATTERIES, AND SIMILAR EQUIPMENT FURNISHED BY THE COMPANY FOR INSTALLATION BY THE CONTRACTOR (OFC).

B. CONTRACTOR SHALL PROVIDE AND INSTALL ALL MISCELLANEOUS MATERIALS AND PROVIDE ALL LABOR REQUIRED FOR INSTALLATION EQUIPMENT IN EXISTING CABINET OR NEW CABINET AS SHOWN ON DRAWINGS AND AS REQUIRED

BY THE APPLICABLE INSTALLATION MOPS.

- C. COMPLY WITH MANUFACTURER'S INSTALLATION AND START-UP REQUIREMENTS.

DC CIRCUIT BREAKER LABELING:

- A. LABEL CIRCUIT BREAKERS ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE – EN 2012-001, REV 1. SECTION 26 100 – BASIC ELECTRICAL REQUIREMENTS

SUMMARY:

THIS SECTION SPECIFIES BASIC ELECTRICAL REQUIREMENTS FOR SYSTEMS AND COMPONENTS.

QUALITY ASSURANCE:

A. ALL EQUIPMENT FURNISHED UNDER DIVISION 26 SHALL CARRY UL LABELS AND LISTINGS WHERE SUCH LABELS AND LISTING ARE AVAILABLE IN THE INDUSTRY.

B. MANUFACTURERS OF EQUIPMENT SHALL HAVE A MINIMUM OF THREE YEARS EXPERIENCE WITH THEIR EQUIPMENT INSTALLED AND OPERATING IN THE FIELD IN A USE SIMILAR TO THE NEW USE FOR THIS PROJECT.

C. MATERIALS AND EQUIPMENT: ALL MATERIALS AND EQUIPMENT SPECIFIED IN DIVISION 26 OF THE SAME TYPE SHALL BE OF THE SAME MANUFACTURER AND SHALL BE NEW, OF THE BEST QUALITY AND DESIGN, AND FREE FROM DEFECTS.

SUPPORTING DEVICES:

A. MANUFACTURED STRUCTURAL SUPPORT MATERIALS: SUBJECT TO COMPLIANCE WITH REQUIREMENTS. PROVIDE PRODUCTS BY THE FOLLOWING:

1. ALLIED TUBE AND CONDUIT.
2. B-LINE SYSTEM.
3. UNISTRUT DIVERSIFIED PRODUCTS.
4. THOMAS & BETTS

B. FASTENERS: TYPES, MATERIALS AND CONSTRUCTION FEATURES AS FOLLOWS:

1. EXPANSION ANCHORS: CARBON STEEL WEDGE OR SLEEVE TYPE.
2. POWER-DRIVEN THREADED STUDS: HEAT-TREATED STEEL. DESIGNED SPECIFICALLY FOR THE INTENDED SERVICE.
3. FASTEN BY MEANS OF WOOD SCREWS IN WOOD.
4. TOGGLE BOLTS ON HOLLOW MASONRY UNITS.
5. CONCRETE INSERTS OR EXPANSION BOLTS ON CONCRETE OR SOLID MASONRY.
6. MACHINE SCREWS, WELDED THREADED STUDS, OR SPRING-TENSION CLAMPS ON STEEL.
7. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE SHALL NOT BE PERMITTED.
8. DO NOT WELD CONDUIT, PIPE STRAPS, OR ITEMS OTHER THAN THREADED STUDS TO STEEL STRUCTURES.
9. IN PARTITIONS OF LIGHT STEEL CONSTRUCTION, USE SHEET METAL SCREWS.

SUPPORTING DEVICES:

A. INSTALL SUPPORTING DEVICES TO FASTEN ELECTRICAL COMPONENTS SECURELY AND PERMANENTLY IN ACCORDANCE WITH NEC.

B. COORDINATE WITH THE BUILDING STRUCTURAL SYSTEM AND WITH OTHER TRADES.

C. UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FASTEN ELECTRICAL ITEMS AND THEIR SUPPORTING HARDWARE SECURELY TO THE STRUCTURE IN ACCORDANCE WITH THE FOLLOWING:

1. ENSURE THAT THE LOAD APPLIED BY ANY FASTENER DOES NOT EXCEED 25 PERCENT OF THE PROOF TEST LOAD.
2. USE VIBRATION AND SHOCK-RESISTANT FASTNERS FOR ATTACHMENTS TO CONCRETE SLABS.

ELECTRICAL IDENTIFICATION:

A. UPDATE AND PROVIDE TYPED CIRCUIT BREAKER SCHEDULES IN THE MOUNTING BRACKET, INSIDE DOORS OF AC PANEL BOARDS WITH ANY CHANGES MADE TO THE AC SYSTEM.

B. BRANCH CIRCUITS FEEDING AVIATION OBSTRUCTION LIGHTING EQUIPMENT SHALL BE CLEARLY IDENTIFIED AS SUCH AT THE BRANCH CIRCUIT PANELBOARD.

SECTION 26 200 – ELECTRICAL MATERIALS AND EQUIPMENT

CONDUIT:

A. RIGID GALVANIZED STEEL (RGS) CONDUIT SHALL BE USED FOR EXTERIOR LOCATIONS ABOVE GROUND AND IN UNFINISHED INTERIOR LOCATIONS AND FOR UNDERGROUND RUNS. RIGID CONDUIT AND FITTINGS SHALL BE STEEL, COATED WITH ZINC EXTERIOR AND INTERIOR BY THE HOT DIP GALVANIZING PROCESS. CONDUIT SHALL BE PRODUCED TO ANSI SPECIFICATIONS C80.1, FEDERAL SPECIFICATION WW-C-581 AND SHALL BE LISTED WITH THE UNDERWRITERS' LABORATORIES. FITTINGS SHALL BE THREADED – SET SCREW OR COMPRESSION FITTINGS WILL NOT BE ACCEPTABLE. RGS CONDUITS SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND.

B. UNDERGROUND CONDUIT IN CONCRETE SHALL BE POLYVINYLCHLORIDE (PVC) SUITABLE FOR DIRECT BURIAL AS APPLICABLE. JOINTS SHALL BE BELLED, AND FLUSH SOLVENT WELDED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. CONDUIT SHALL BE CARLON ELECTRICAL PRODUCTS OR APPROVED EQUAL.

C. TRANSITIONS BETWEEN PVC AND RIGID (RGS) SHALL BE MADE WITH PVC COATED METALLIC LONG SWEEP RADIUS ELBOWS.

D. ALL UNDERGROUND CONDUIT OR CONDUIT IN CONCRETE SHOULD BE PVC. EMT OR RIGID GALVANIZED STEEL CONDUIT MAY BE USED IN FINISHED SPACES CONCEALED IN WALLS AND CEILINGS. EMT SHALL BE MILD STEEL, ELECTRICALLY WELDED, ELECTRO-GALVANIZED OR HOT-DIPPED GALVANIZED AND PRODUCED TO ANSI SPECIFICATIONS C80.3, FEDERAL SPECIFICATION WW-C-563, AND SHALL BE UL LISTED. EMT SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND, OR APPROVED EQUAL. FITTINGS SHALL BE METALLIC COMPRESSION. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE.

E. LIQUID TIGHT FLEXIBLE METALLIC CONDUIT SHALL BE USED FOR FINAL CONNECTION TO EQUIPMENT FITTINGS SHALL BE METALLIC GLAND TYPE COMPRESSION FITTINGS, MAINTAINING THE INTEGRITY OF CONDUIT SYSTEM. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE. MAXIMUM LENGTH OF FLEXIBLE CONDUIT SHALL NOT EXCEED 6- FEET. LPMC SHALL BE PROTECTED AND SUPPORTED AS REQUIRED BY NEC. MANUFACTURERS OF FLEXIBLE CONDUITS SHALL BE CAROL, ANACONDA METAL HOSE OR UNIVERSAL METAL HOSE, OR APPROVED EQUAL.

F. MINIMUM SIZE CONDUIT SHALL BE 3/4 INCH (21MM).

HUBS AND BOXES:

A. AT ENTRANCES TO CABINETS OR OTHER EQUIPMENT NOT HAVING INTEGRAL THREADED HUBS PROVIDE METALLIC THREADED HUBS OF THE SIZE AND CONFIGURATION REQUIRED HUB SHALL INCLUDE LOCK NUT AND NEOPRENE O-RING SEAL. PROVIDE IMPACT RESISTANT 105 DEGREE C PLASTIC BUSHINGS TO PROTECT CABLE INSULATION

- B. CABLE TERMINATION FITTINGS FOR CONDUIT

- 1. CABLE TERMINATORS FOR RGS CONDUITS SHALL BE TYPE CRC BY O-Z/GEDNEY OR EQUAL BY ROXTEC.

- 2. CABLE TERMINATORS FOR LPMC SHALL BE ETCO – CL2075, OR MADE FOR THE PURPOSE PRODUCTS BY ROXTEC.

C. EXTERIOR PULL BOXES AND PULL BOXES IN INTERIOR INDUSTRIAL AREAS SHALL BE PLATED CAST ALLOY, HEAVY DUTY, WEATHERPROOF, DUST PROOF, WITH GASKET, PLATED IRON ALLOY COVER AND STAINLESS STEEL COVER SCREWS, CROUSE-HINDS WAB SERIES OR EQUAL.

D. CONDUIT OUTLET BODIES SHALL BE PLATED CAST ALLOY WITH SIMILAR GASKET COVERS. OUTLET BODIES SHALL BE OF THE CONFIGURATION AND SIZE SUITABLE FOR THE APPLICATION, PROVIDE CROUSE-HINDS FORM 8 OR EQUAL.

E. MANUFACTURER FOR BOXES AND COVERS SHALL BE HOFFMAN, SQUARE "D", CROUSE-HINDS, COOPER, ADALET, APPLETON, O-Z GEDNEY, RACO, OR APPROVED EQUAL.

SUPPLEMENTAL GROUNDING SYSTEM:

A. FURNISH AND INSTALL A SUPPLEMENTAL GROUNDING SYSTEM TO THE EXTENT INDICATED ON THE DRAWINGS. SUPPORT SYSTEM WITH NON-MAGNETIC STAINLESS STEEL CLIPS WITH RUBBER GROMMET. GROUNDING CONNECTORS SHALL BE TINNED COPPER WIRE, SIZES AS INDICATED ON THE DRAWINGS. PROVIDE STRANDED OR SOLID BARE OR INSULATED CONDUCTORS EXCEPT AS OTHERWISE NOTED.

B. SUPPLEMENTAL GROUNDING SYSTEM: ALL CONNECTIONS TO BE MADE WITH CAD WELDS, EXCEPT AT EQUIPMENT USE LUGS OR OTHER AVAILABLE GROUNDING MEANS AS REQUIRED BY MANUFACTURER; AT GROUND BARS USE TWO-HOLE SPADES WITH NO-OX.

C. STOLEN GROUND-BARS: IN THE EVENT OF STOLEN GROUND BARS, CONTACT SPRINT CONSTRUCTION MANAGER FOR REPLACEMENT INSTRUCTION USING THREADED ROD KITS.

EXISTING STRUCTURE:

A. EXISTING EXPOSED WIRING AND ALL EXPOSED OUTLETS, RECEPTACLES, SWITCHES, DEVICES, BOXES, AND OTHER EQUIPMENT THAT ARE NOT TO BE UTILIZED IN THE COMPLETED PROJECT SHALL BE REMOVED OR DE-ENERGIZED AND CAPPED IN THE WALL, CEILING, OR FLOOR SO THAT THEY ARE CONCEALED AND SAFE. WALL, CEILING, OR FLOOR SHALL BE PATCHED TO MATCH THE ADJACENT CONSTRUCTION.

CONDUIT AND CONDUCTOR INSTALLATION:

A. CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED STRAPS AND HANGERS. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED. CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUITS IN TIGHT ENVELOPES. CHANGES IN DIRECTION TO ROUTE AROUND OBSTACLES SHALL BE MADE WITH CONDUIT OUTLET BODIES. CONDUIT SHALL BE INSTALLED IN A NEAT AND WORKMANLIKE MANNER, PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES. ALL CONDUIT SHALL BE FISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED TO PREVENT CONCRETE, PLASTER OR DIRT FROM ENTERING. CONDUITS SHALL BE RIGIDLY CLAMPED TO BOXES BY GALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCKNUT ON OUTSIDE AND INSIDE.

B. CONDUCTORS SHALL BE PULLED IN ACCORDANCE WITH ACCEPTED GOOD PRACTICE.

ADDITIONAL REQUIRED NOTES:

- GC IS RESPONSIBLE FOR HIRING ALL 3RD PARTY SPECIAL INSPECTIONS AS REQUIRED PER MUNICIPALITY
- GC IS RESPONSIBLE FOR VERIFYING ALL FIELD MEASUREMENTS PRIOR TO STARTING CONSTRUCTION
- DO NOT OPEN RRU PACKAGES IN THE RAIN
- NO OPEN FLAME ON SITE
- GC TO ENSURE HYBRIDS ARE SUPPORTED EVERY 3'-0" ON HORIZONTAL AND 4'-0" ON VERTICAL RUNS



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

**SPRINT SITE NUMBER:
CT54XC747**

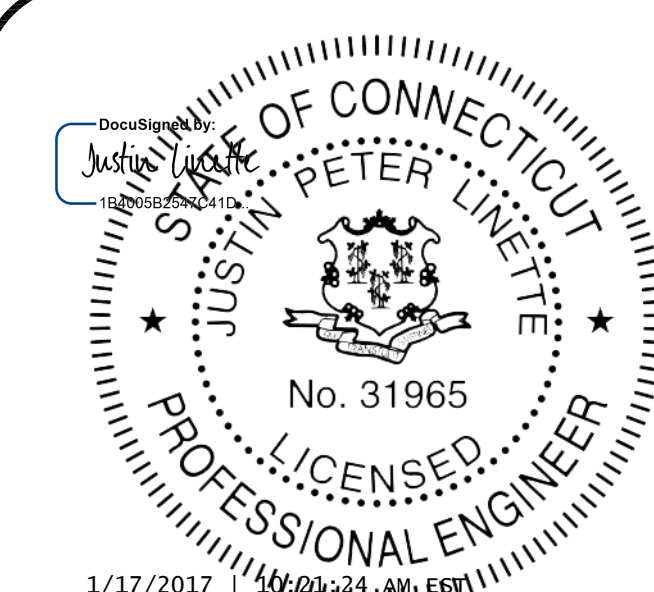
**BU #: 822779
BRIDGEPORT/ RT 8**

**1875 NOBLE AVENUE
BRIDGEPORT, CT 06610**

EXISTING 120'-0" FLAGPOLE

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1/17/2017 10:44:34 AM EST

Justin Peter Linette, P.E.
Professional Engineer License: 31965
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 CLIFTON PARK, NY 12065

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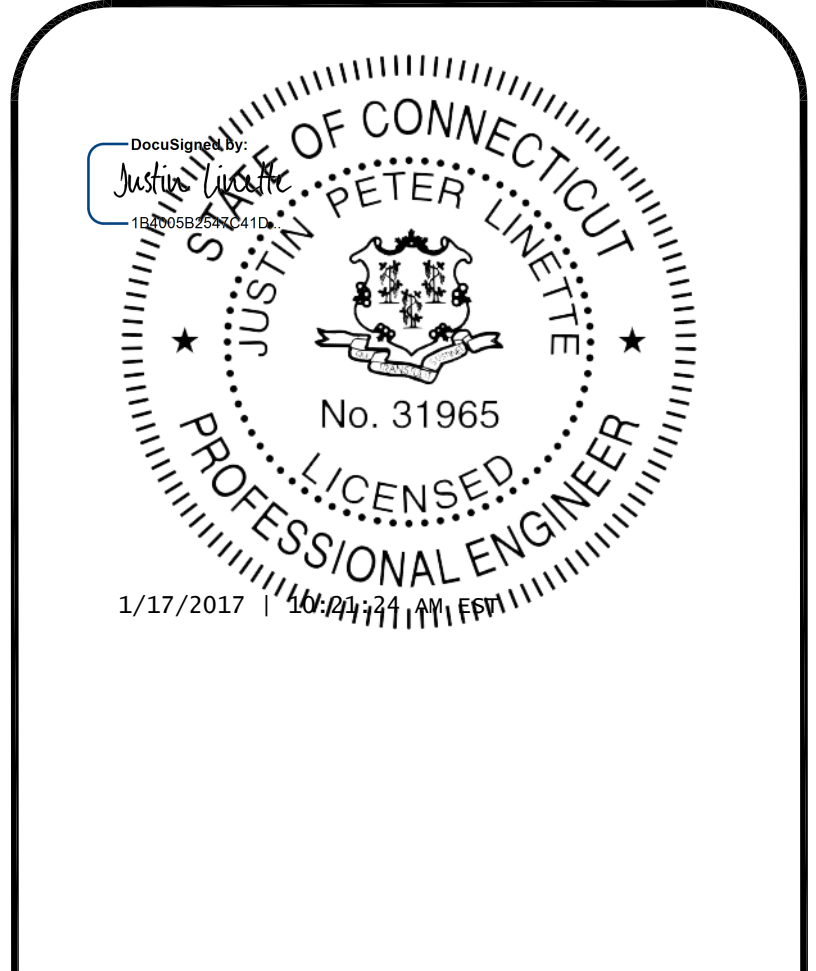
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REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



Justin Peter Linette, P.E.
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 Crown Castle USA, Inc. Firm Registration #PEC.0001101

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SHEET NUMBER: C-1 **REVISION: 0**



1 ENLARGED SITE PLAN

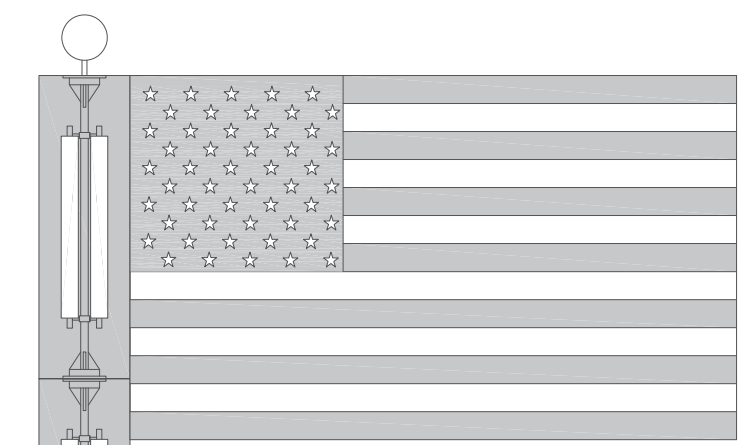
SCALE: 3/8"=1'-0" (FULL SIZE)
 3/16"=1'-0" (11x17)

STRUCTURE W/ APPURTENANCE
ELEV. = 122'-0"
HEIGHT OF STRUCTURE
ELEV. = 120'-0"

TIP OF ANTENNA
ELEV. = 98'-6"

(E) SPRINT EQUIPMENT TO BE REMOVED
(3) ANTENNAS
MOUNTED TO EXISTING MOUNT

SPRINT EQUIPMENT
ANTENNA CL: 96'-0"
MOUNT CL: 95'-0"



EXISTING RAD. CENTER
ELEV. = 115'-0"

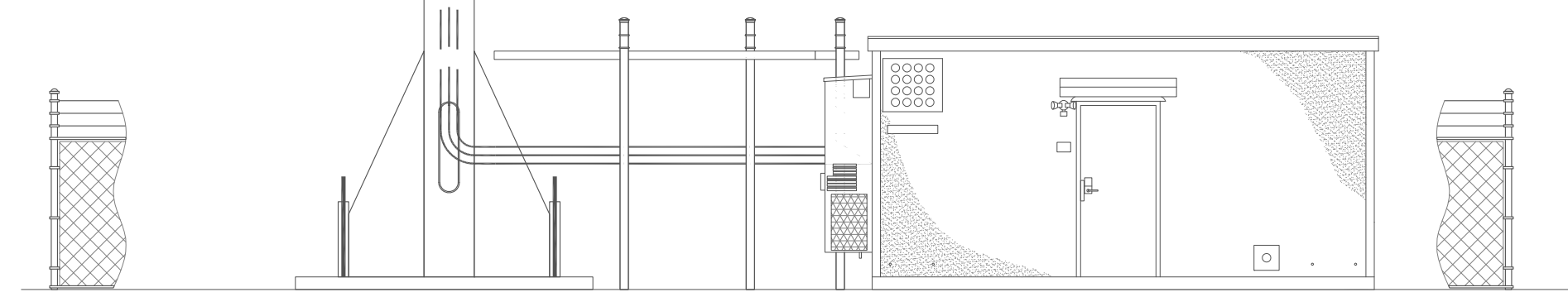
EXISTING RAD. CENTER
ELEV. = 105'-0"

EXISTING SPRINT RAD. CENTER
ELEV. = 96'-0"

EXISTING MCL
ELEV. = 86'-0"

(E) 120'-0" FLAGPOLE

(E) SPRINT FEEDLINES TO REMAIN
(6) ANDREW - LDF6-50A (1-1/4")
(2) BELDEN - 9833 (3/8")



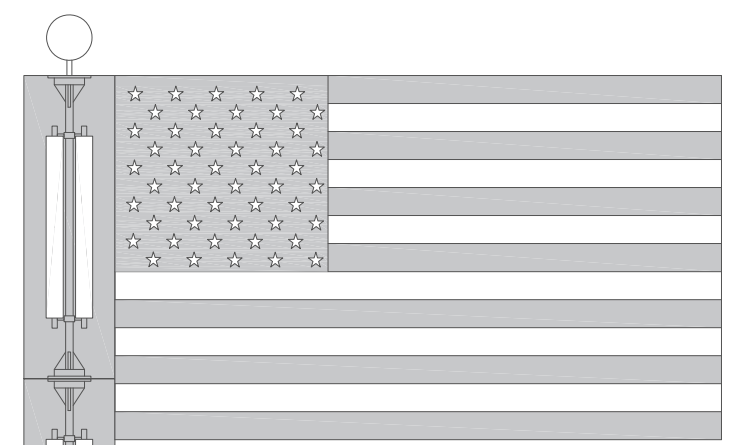
1 EXISTING ELEVATION
SCALE: NOT TO SCALE

STRUCTURE W/ APPURTENANCE
ELEV. = 122'-0"
HEIGHT OF STRUCTURE
ELEV. = 120'-0"

TIP OF ANTENNA
ELEV. = 99'-0"

NEW SPRINT EQUIPMENT
(3) ANTENNAS
(3) RRHs
(3) DIPLEXERS
(1) JUNCTION BOX
MOUNTED TO EXISTING MOUNT

SPRINT EQUIPMENT
ANTENNA CL: 96'-0"
MOUNT CL: 95'-0"



EXISTING RAD. CENTER
ELEV. = 115'-0"

EXISTING RAD. CENTER
ELEV. = 105'-0"

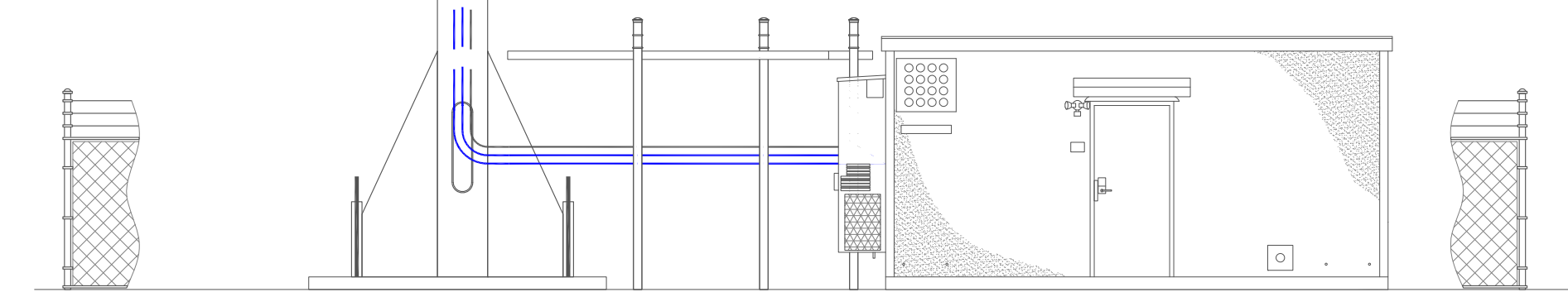
NEW SPRINT RAD. CENTER
ELEV. = 96'-0"

EXISTING MCL
ELEV. = 86'-0"

(E) 120'-0" FLAGPOLE

(E) SPRINT FEEDLINES
(6) ANDREW - LDF6-50A (1-1/4")
(2) BELDEN - 9833 (3/8")

NEW SPRINT FEEDLINE IN (1) 1" CONDUIT
(1) SOUTHWIRE - TYPE SOOW 12/9 (7/8")
NEW SPRINT FEEDLINES IN (1) 1" CONDUIT
(1) CORNING CABLE SYSTEMS - 004U8X-32125E2G (1/8")
(4) BELDEN - 7919A (17/64")



2 FINAL ELEVATION
SCALE: NOT TO SCALE

INSTALLER NOTE:
TOWER DOES NOT HAVE CLIMBING FACILITIES - MANLIFT REQUIRED FOR ELEVATED WORK.



SPRINT SITE NUMBER:
CT54XC747

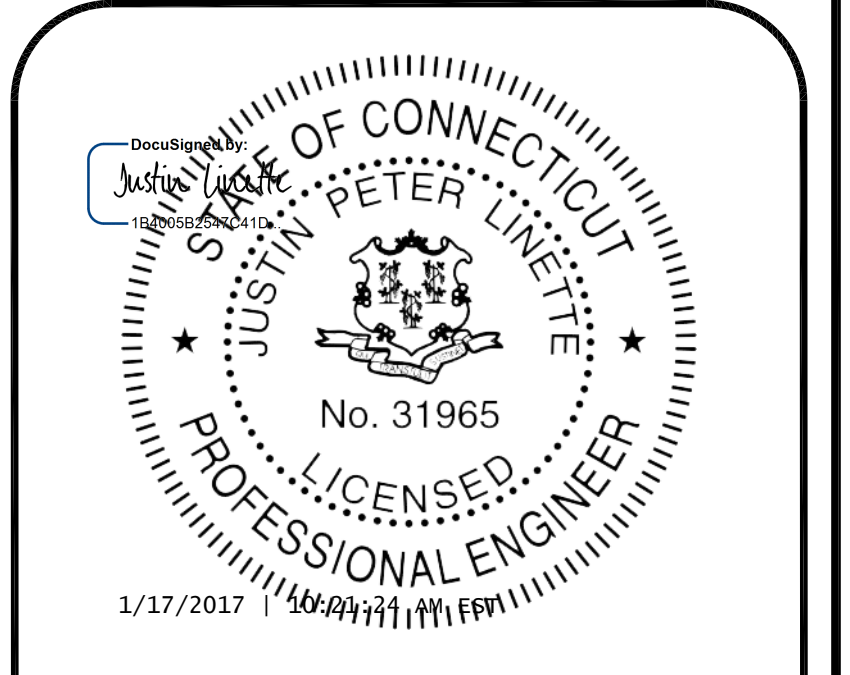
BU #: 822779
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR

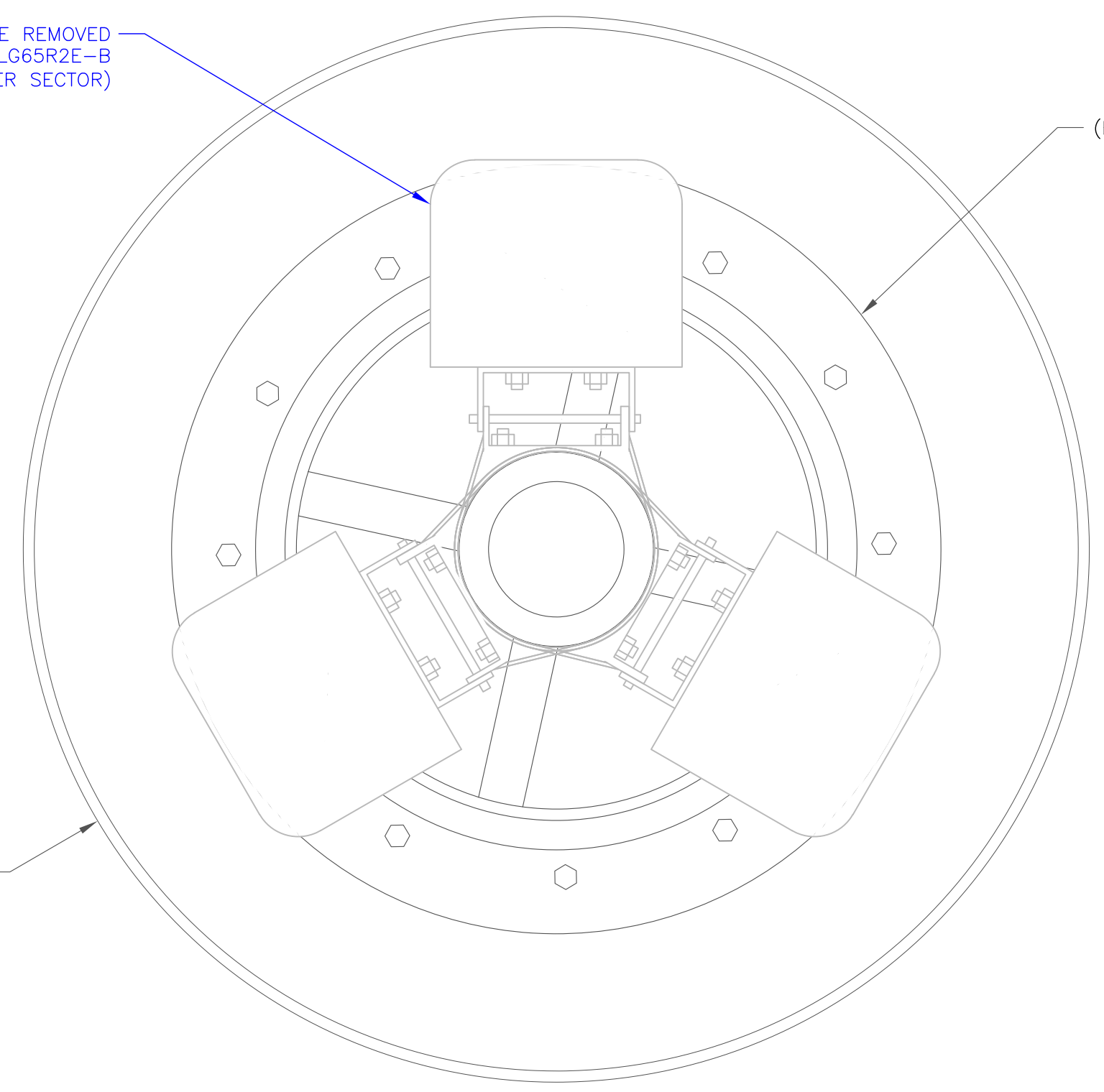


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SHEET NUMBER: **C-2** REVISION: **0**

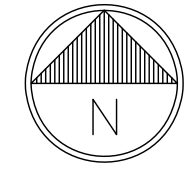
(E) SPRINT ANTENNA TO BE REMOVED
DECIBEL - 932LG65R2E-B
(3 TOTAL, 1 PER SECTOR)



(E) 120'-0" FLAGPOLE

(E) 3'-0" x 10'-0" CONCEALMENT SHROUD

1 EXISTING ANTENNA LAYOUT
SCALE: NOT TO SCALE



INSTALLER NOTE:
CONTRACTOR TO REFERENCE LATEST RFDS
FOR CORRECT AZIMUTHS.

NEW SPRINT JUNCTION BOX
ENCLOSURES AND ASSEMBLY -
BEN-92P
(1 TOTAL)

NEW SPRINT ANTENNA
COMMSCOPE - DHHTT65B3XR
(3 TOTAL, 1 PER SECTOR)

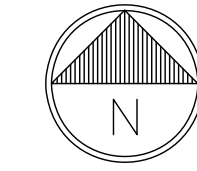
(E) 3'-0" x 10'-0" CONCEALMENT SHROUD

2 FINAL ANTENNA LAYOUT
SCALE: NOT TO SCALE

(E) 120'-0" FLAGPOLE

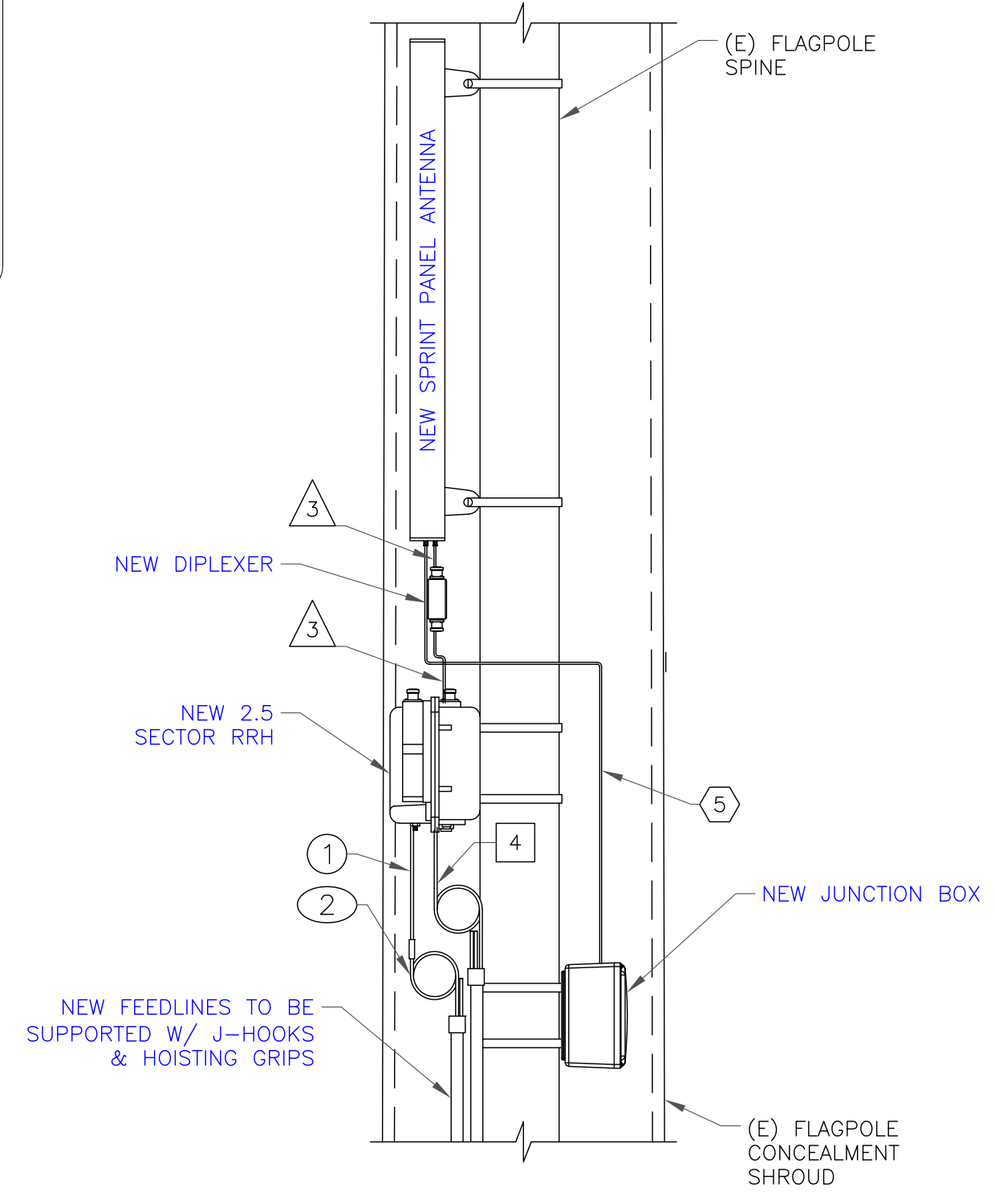
NEW SPRINT DIPLEXER
RFS/GELWAVE - FD9R6004/1C-3L
(3 TOTAL, 1 PER SECTOR)

NEW SPRINT RRH
NOKIA - FWHR
(3 TOTAL, 1 PER SECTOR)



KEYED CABLE LEGEND

- 1 OEM PROPRIETARY
- 2 SOOW
- 3 1/2" RF JUMPERS
- 4 ETHERNET/FIBER
- 5 RET



NEW FEEDLINES TO BE SUPPORTED W/ J-HOOKS & HOISTING GRIPS

(E) FLAGPOLE SPINE

NEW JUNCTION BOX

(E) FLAGPOLE CONCEALMENT SHROUD

4 ANTENNA SCHEMATIC
SCALE: NOT TO SCALE

3 NOT USED
SCALE: NOT TO SCALE



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

SPRINT SITE NUMBER:
CT54XC747

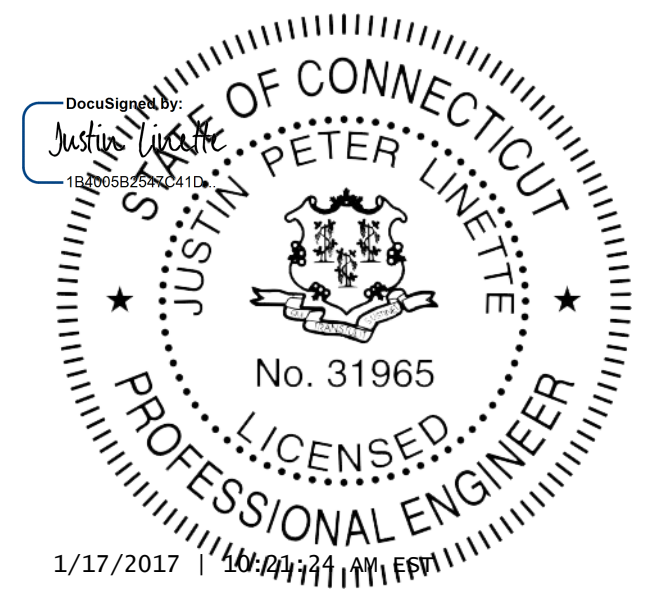
BU #: **822779**
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



1/17/2017

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SHEET NUMBER:
C-3

REVISION:
0



SPRINT SITE NUMBER:
CT54XC747

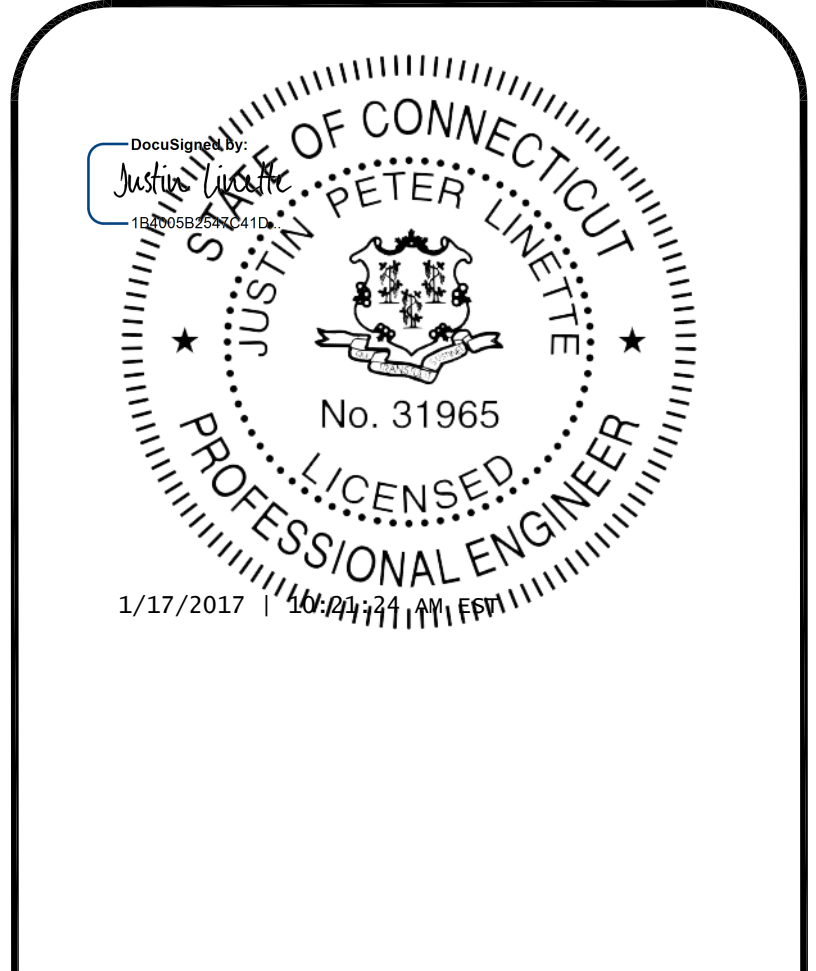
BU #: **822779**
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

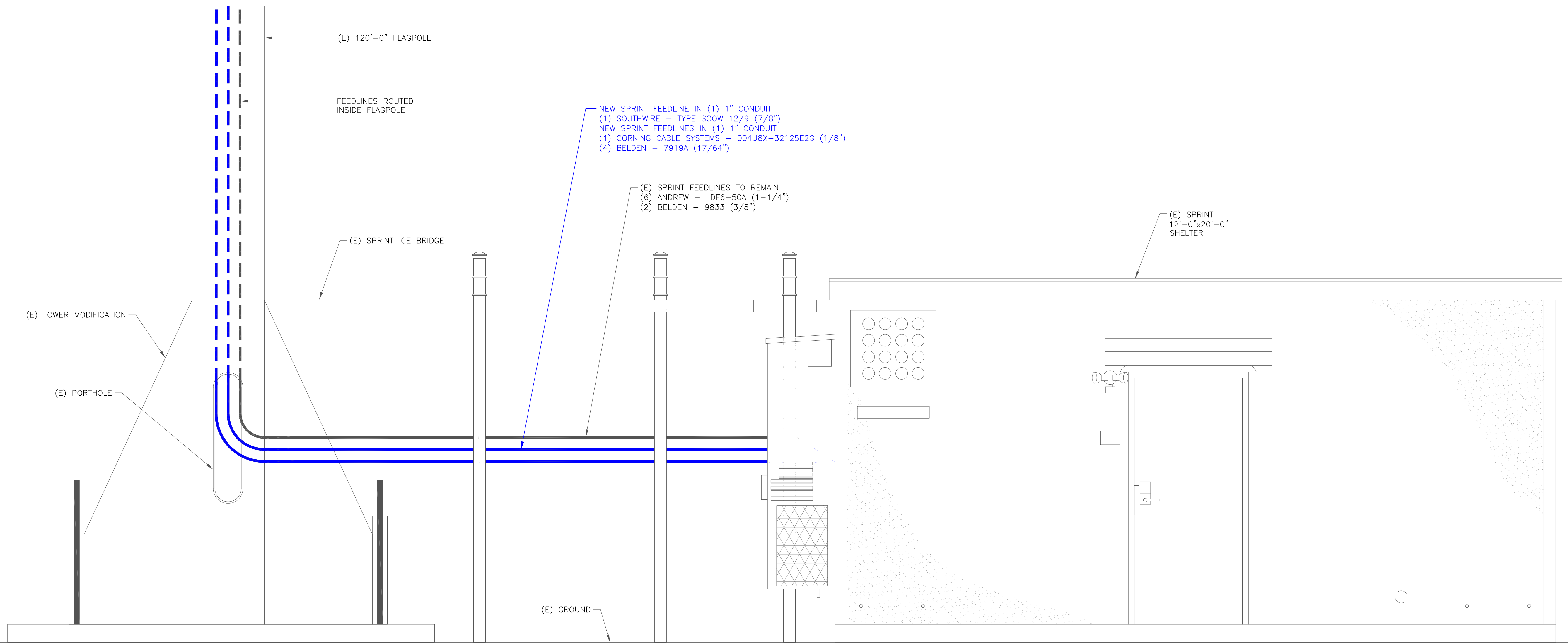
REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



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SHEET NUMBER: **C-4** REVISION: **0**



1 CONDUIT ROUTING SCHEMATIC
SCALE: NOT TO SCALE

REV. 0 7/25/16

SPRINT CONSTRUCTION SPECIFICATIONS
MINI-MACRO CELL SITES

1) BASIC REQUIREMENTS

- a) MEET ALL REQUIREMENTS OF JURISDICTIONS.
- b) IF EQUIPMENT FURNISHED BY THE COMPANY DOES NOT MATCH THE EQUIPMENT LISTED ON THE RFDS AND SHOWN ON THE PERMITTING DRAWINGS, RESOLVE DISCREPANCY THROUGH INSTALLER'S CONSTRUCTION MANAGER AND COMPANY'S POINT OF CONTACT
- c) CABLE INSTALLATIONS
 - i) ALL CABLES MUST BE OUTDOOR RATED AND HAVE UV RESISTANT OUTER JACKETS
 - ii) CABLE BENDS MUST NOT EXCEED MANUFACTURER'S ALLOWABLE CABLE BEND RADII
 - iii) AT RADIOS INSTALL SERVICE LOOPS FOR POWER, FIBER, AND ETHERNET SECURED AT LEAST TWICE 180° TO THE STRUCTURE
 - iv) SPARE FIBERS MUST BE ENCASED IN A LOW PROFILE WEATHERTIGHT ASSEMBLY
- d) FIBERS MUST BE FIELD-TERMINATED WITH LC TYPE CONNECTORS
- e) CONDUITS IN EARTH: PROVIDE PVC. CONDUITS EXPOSED IN FACILITIES: PROVIDE RGS. HAND DIG TRENCHES IN COMPOUNDS
- f) SECURE AND SUPPORT CONDUITS AND CABLES ON NO MORE THAN 48" INTERVALS
- g) ON TOWER SITES RGS CONDUITS MAY BE SURFACE MOUNTED AWAY FROM WALKWAYS AND ACCESS/EGRESS PATHS. IF INSTALLATIONS IN WALKWAYS AND ACCESS/EGRESS PATHS CANNOT BE AVOIDED, IDENTIFY THE CONDUIT ENVELOPE/TRIP HAZARD BY ALTERNATING YELLOW AND BLACK STRIPES PAINTED ON CONCRETE AND CONDUIT.

2) SPRINT – FURNISHED EQUIPMENT

- a) INSTALL THE FOLLOWING EQUIPMENT AT LOCATIONS AND AZIMUTHS SHOWN ON THE CONSTRUCTION DRAWINGS.
 - i) PANEL ANTENNAS
 - ii) RADIOS
 - iii) GPS ANTENNAS
 - iv) FILTERS
 - v) 120 VOLT DIN-RAIL CIRCUIT BREAKER ASSEMBLY

3) TOWER INSTALLATIONS

- a) MEET ALL REQUIREMENTS OF THE TOWER OWNER
- b) INSTALL CORRUGATED FLEXIBLE CONDUIT UP THE TOWER TO COMPANY'S RAD CENTER
- c) PROVIDE HANGING GRIPS OR CONDUIT CLAMPS AND ENSURE CONDUITS AS WELL AS INNER CABLES ARE SUPPORTED
- d) CONDUIT RISERS: AT THE TOP OF THE TOWER TURN CONDUIT DOWN AND PROVIDE CABLE TERMINATION FITTINGS. EXTEND CABLES TO RADIOS EXPOSED AND SECURED TO THE STRUCTURE, AT CONDUIT EXIT FROM TOWER, PROVIDE DRIP LOOPS AND WEEP HOLES.
- e) AT THE ICE BRIDGE RUN CABLES IN RGS CONDUIT. UTILIZE CONDULETS TO MAKE COMPACT 90 DEGREE TURNS

4) AC POWER TIE-IN

- a) INSTALL SPRINT'S 120 VOLT DIN-RAIL CIRCUIT BREAKER ASSEMBLY IN THE EXISTING POWER PROTECTION CABINET TELCO SECTION
- b) INSTALL A 20 AMPERE MOLDED CASE CIRCUIT BREAKER IN AVAILABLE SPACE IN THE ADJACENT PPC POWER SECTION LOAD CENTER

5) GROUNDING

- a) 120 VOLT CIRCUITS: POWER CABLES MUST BE 3-WIRE WITH EQUIPMENT GROUNDING CONDUCTOR
- b) SUPPLEMENTAL GROUNDING: ALL GROUNDING HARDWARE MUST BE UL STAMPED AS SUITABLE FOR GROUNDING HARDWARE
- c) RADIOS: BOND RADIO TO THE TOWER TOP OR SECTOR GROUND BAR WITH #6 BARE TINNED COPPER WIRE (GREEN INSULATED ON ROOFTOPS)
- d) DIN-RAIL CIRCUIT BREAKER ASSEMBLY: BOND SURGE ARRESTOR TO PPC TELCO BOARD GROUND BAR

6) MINOR MATERIALS

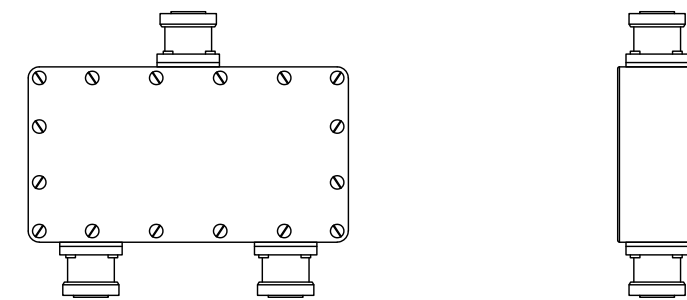
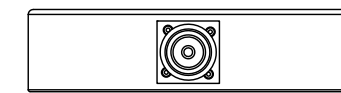
- a) CONDUIT
 - i) RIGID GALVANIZED STEEL CONDUIT (RGS): UL LISTED, COMPLIANT WITH ANSI STANDARD C80, HOT-DIP GALVANIZED, WITH THREADED FITTINGS. MANUFACTURERS: ALLIED, REPUBLIC, WHEATLAND, OR EQUAL.
 - ii) CORRUGATED FLEXIBLE CONDUIT: DURALINE OR EQUAL.
 - iii) LIQUID-TIGHT FLEXIBLE METALLIC CONDUIT (LFMC): UL LABELED, UC RESISTANT, FLAME RETARDANT PVC JACKET, HOT-DIP GALVANIZED, GREY. MANUFACTURERS: AFC, ANACONDA, SOUTHWIRE, OR EQUAL.
 - iv) PVC CONDUIT: SCHEDULE 40. CARLON OR EQUAL
 - v) CABINET HUBS AND CABLE TERMINATION FITTINGS: OZ GEDNEY OR ROXTEC
- b) COAXIAL CABLE JUMPERS: ½" LDF-4 MANUFACTURERS: COMMSCOPE, RFS OR FCT.
- c) FASTENERS AND HARDWARE
 - i) TO SECURE RACEWAYS, UTILIZE NON CORRODING NON-MAGNETS METALLIC FASTENERS AND HARDWARE SUITABLE FOR THE PURPOSE
- d) POWER CABLES – 3/C #12 SOOW BY SOUTHWIRE OR EQUAL
- e) ETHERNET CABLES AND CONNECTORS: OUTDOOR RATED, CAT 5E, BELDEN OR EQUAL
- f) FIBER CABLES: CORNING "FREEDOM FAN OUT" OUTDOOR RISER CABLE, 4F, SINGLE MODE, OR EQUAL
- g) RF TRANSPARENT PAINT FOR ANTENNA CONCEALMENT: SELECT NO/LOW CARBON PAINTS, WITH NO/LOW TITANIUM DIOXIDE, AND WITHOUT SUSPENDED METAL PARTICLES (ALUMINUM, ZINC, COPPER, ETC)

7) COLOR CODING

- a) COLOR CODE CABLES AND CONDUITS AS REQUIRED BY SPRINT STANDARD TS-0200

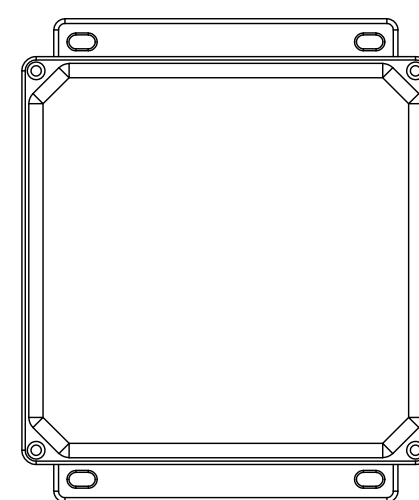
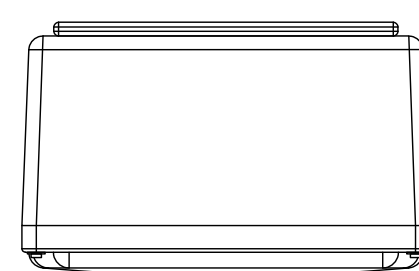
8) TESTING AND CONSTRUCTION COMPLETE

- a) SWEEP ALL COAXIAL CABLES ACCORDING TO SPRINT STANDARD TS-0200
- b) PANEL ANTENNA ALIGNMENT – USING ELECTRONIC ALIGNMENT TOOL. AZIMUTH/DOWNTILT +/- 1 DEGREE
- c) LEAVE EQUIPMENT DE-ENERGIZED UNTIL INSTRUCTED BY THE COMMISSIONING AND INTEGRATION TEAM TO ENERGIZE
- d) OTHER REQUIREMENTS AND DELIVERABLES MAY BE REQUIRED BEFORE THE CONSTRUCTION COMPLETE MILESTONE CAN BE ACTUALIZED IN SITERRA (SPRINT'S DATABASE-OF-RECORD).



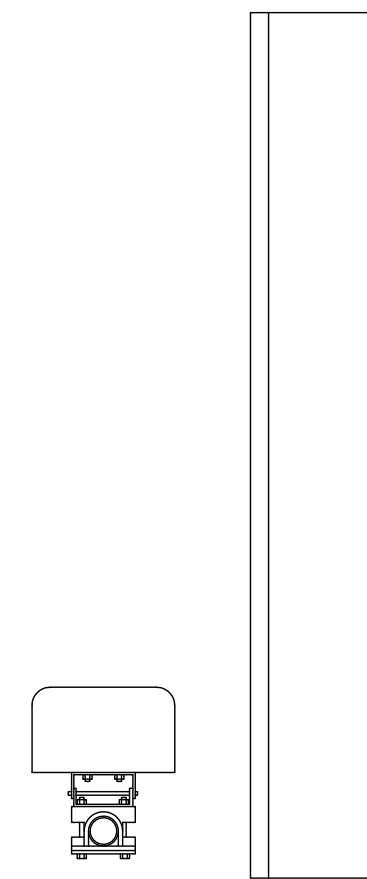
RFS/CELWAVE – FD9R6004/1C-3L
WEIGHT (WITHOUT MOUNTING HARDWARE): 2.6LBS
SIZE (HxWxD): 5.8x6.5x1.5 IN.

1 RFS/CELWAVE – FD9R6004/1C-3L
SCALE: NOT TO SCALE



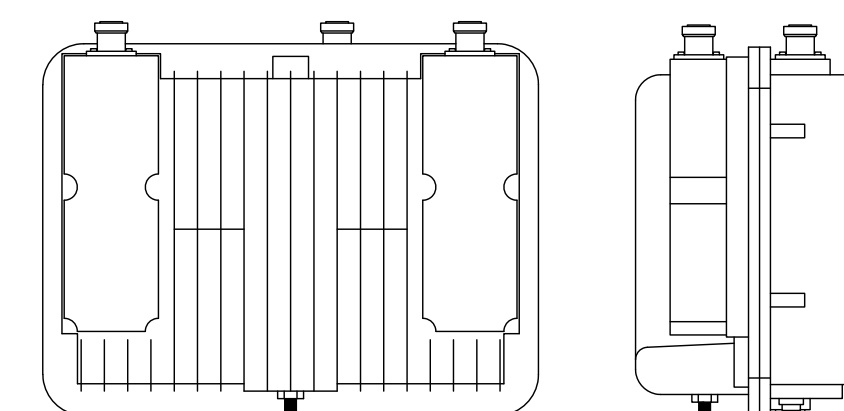
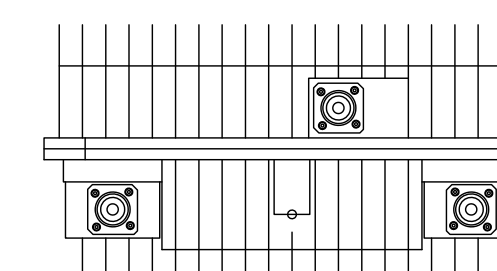
BOX ENCLOSURES AND ASSEMBLY – BEN-92P
WEIGHT (WITHOUT MOUNTING HARDWARE): 2.2 LBS
SIZE (HxWxD): 9.7x12.8"x6.3 IN.

3 BOX ENCLOSURES AND ASSEMBLY – BEN-92P
SCALE: NOT TO SCALE



COMMSCOPE – DHHTT65B-3XR
WEIGHT (WITHOUT MOUNTING HARDWARE): 45.4 LBS
SIZE (HxWxD): 72.10x11.90x7.10 IN.
RATED WIND VELOCITY: 149.8 MPH

2 COMMSCOPE – DHHTT65B-3XR
SCALE: NOT TO SCALE



NOKIA – FWHR
WEIGHT: 24.7 LBS
SIZE (HxWxD): 9.7x12.9x6.3 IN.

4 NOKIA – FWHR
SCALE: NOT TO SCALE



3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

SPRINT SITE NUMBER:
CT54XC747

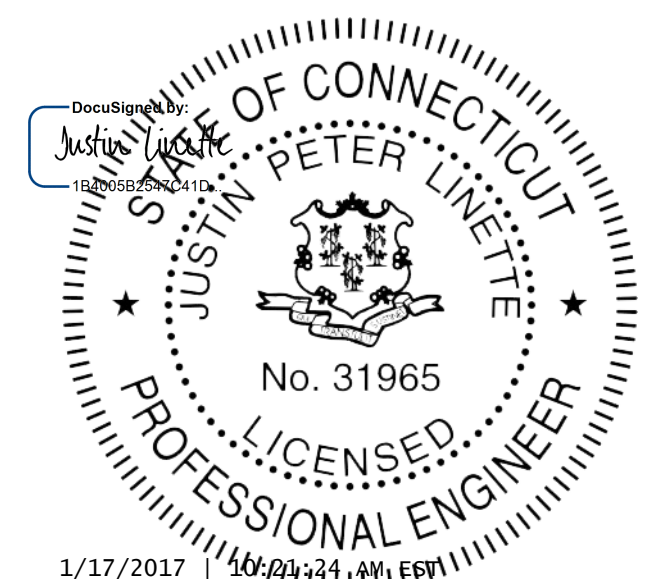
BU #: 822779
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



1/17/2017

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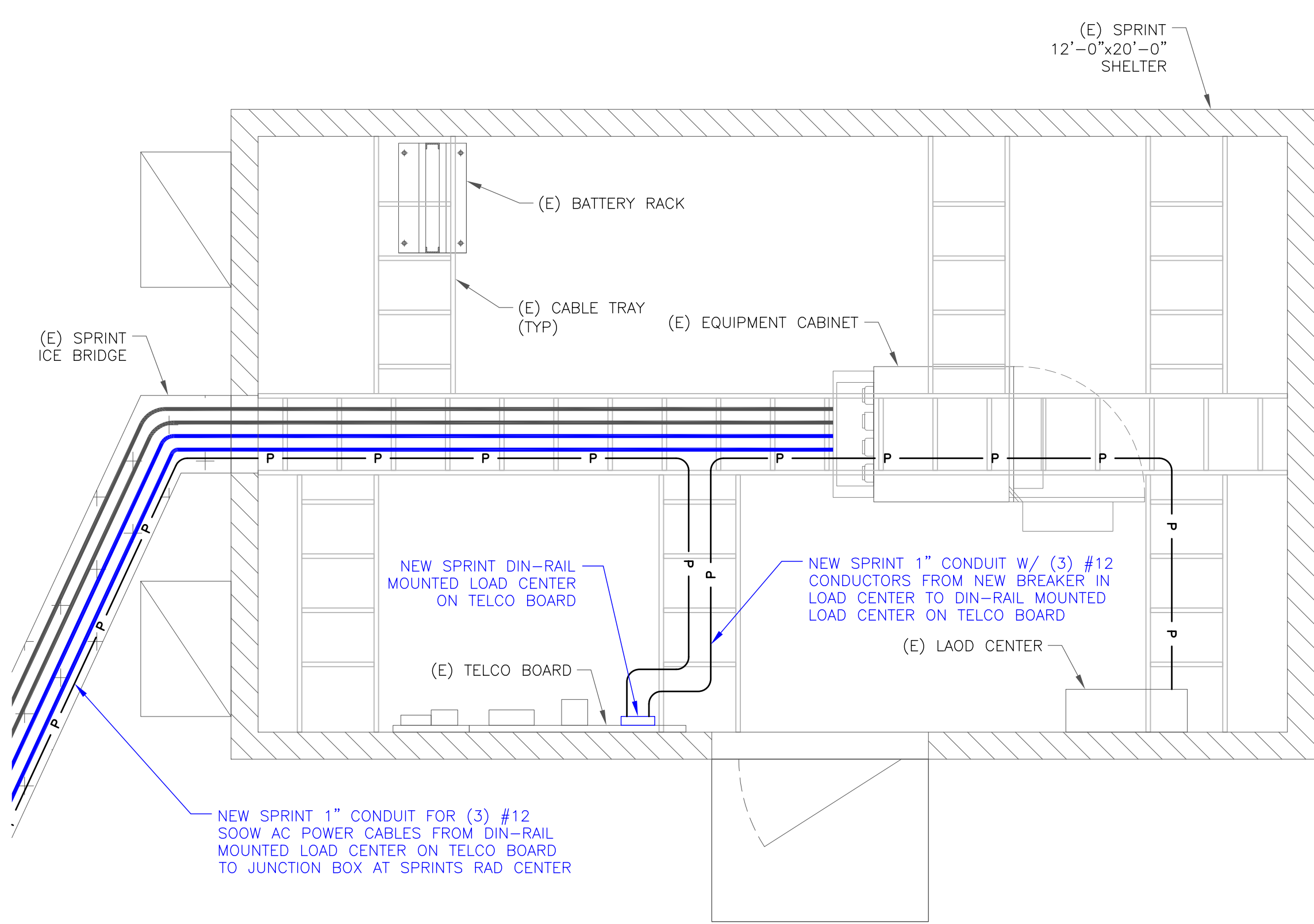
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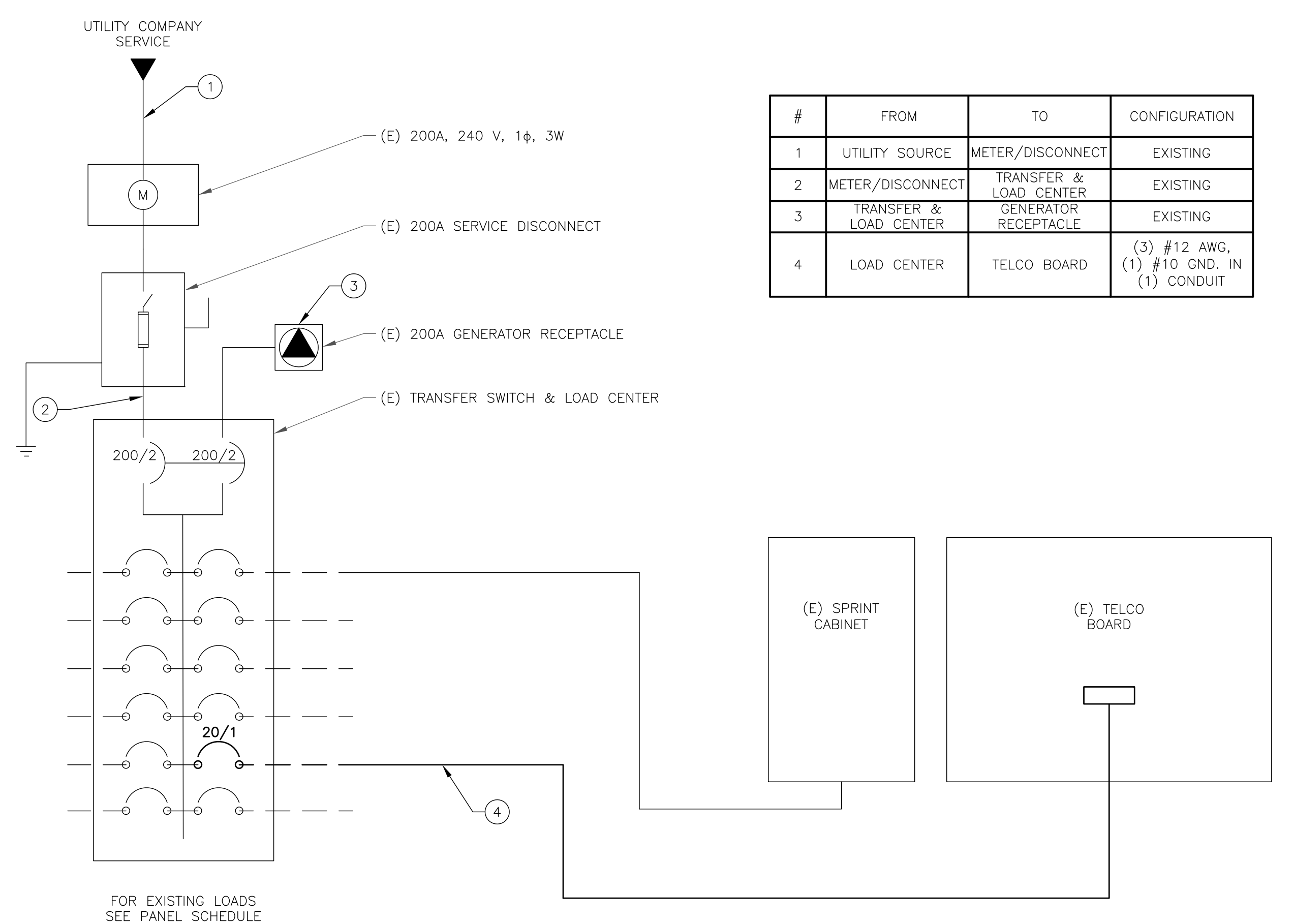
C-5

REVISION:

0



1 ELECTRICAL AND GROUNDING PLAN
SCALE: NOT TO SCALE



2 ELECTRICAL ONE-LINE DIAGRAM
SCALE: NOT TO SCALE

#	FROM	TO	CONFIGURATION
1	UTILITY SOURCE	METER/DISCONNECT	EXISTING
2	METER/DISCONNECT	TRANSFER & LOAD CENTER	EXISTING
3	TRANSFER & LOAD CENTER	GENERATOR RECEPTACLE	EXISTING
4	LOAD CENTER	TELCO BOARD	(3) #12 AWG, (1) #10 GND. IN (1) CONDUIT

EXISTING PANEL PANEL											
MAIN: 200 AMP MAIN BREAKER			VOLTAGE/PHASE: 120/240V, 1-PHASE, 3-WIRE				SHORT CIRCUIT CURRENT RATING: 22,000 AMPS				
MOUNTING: SURFACE			ENCLOSURE: NEMA 1				SURGE PROTECTION DEVICE: YES				
SERVICE FROM: NA			MANUFACTURER: NORTHERN TECHNOLOGIES, INC (SQUARE D)				MODEL NUMBER: QO142M200				
DESCRIPTION	LOAD (VA)	C or NC	C/B	CIR No.	LOAD (VA)		CIR No.	C/B	C or NC	LOAD (VA)	DESCRIPTION
					A-PHASE	B-PHASE					
RECTIFIER CKT #1	1924	C	30	1	3848		2	30	C	1924	RECTIFIER CKT #2
RECTIFIER CKT #1	1924	C	-	3		3848	4	-	C	1924	RECTIFIER CKT #2
RECTIFIER CKT #3	1924	C	30	5	3848		6	30	C	1924	RECTIFIER CKT #4
RECTIFIER CKT #3	1924	C	-	7		3848	8	-	C	1924	RECTIFIER CKT #4
RECTIFIER CKT #5	1924	C	30	9	3848		10	30	C	1924	RECTIFIER CKT #6
RECTIFIER CKT #5	1924	C	-	11		3848	12	-	C	1924	RECTIFIER CKT #6
RECTIFIER CKT #7	1924	C	30	13	3848		14	30	C	1924	RECTIFIER CKT #8
RECTIFIER CKT #7	1924	C	-	15		3848	16	-	C	1924	RECTIFIER CKT #8
SPARE		NC	30	17	0		18	30	NC		SPARE
SPARE		NC	-	19		0	20	-	NC		SPARE
HVAC UNIT #1	1060	C	60	21	2120		22	60	C	1060	HVAC UNIT #2
HVAC UNIT #1	1060	C	-	23		2120	24	-	C	1060	HVAC UNIT #2
SPARE		NC	15	25	0		26	60	NC		SPARE
VENT FAN	150	NC	15	27		150	28	-	NC		SPARE
RECEPTACLE	180	C	20	29	500		30	20	NC	320	LIGHTING
RECEPTACLE	180	C	20	31		360	32	20	C	180	SMOKE DETECTOR
RECEPTACLE	180	C	20	33	180		34	60	NC		SPARE
RECEPTACLE	180	C	20	35		180	36	-	NC		SPARE
SURGE ARRESTOR	0	C	60	37	180		38	20	C	180	EXT. RECEPTABLE
SURGE ARRESTOR	0	C	-	39		180	40	20	NC	180	GAS DETECTOR
BASE LOAD (VA) =					18372	18382	*C* DESIGNATION IDENTIFIES CONTINUOUS LOADS AND MOTOR LOADS AS REQUIRED BY SECTIONS 230.42 AND 430.24 OF THE NEC				
25% OF CONTINUOUS LOAD (VA) =					4513	4513					
TOTAL LOAD (VA) =					22885	22895					
TOTAL LOAD (A) =					191	191					

PROPOSED PANEL PANEL											
MAIN: 200 AMP MAIN BREAKER			VOLTAGE/PHASE: 120/240V, 1-PHASE, 3-WIRE				SHORT CIRCUIT CURRENT RATING: 22,000 AMPS				
MOUNTING: SURFACE			ENCLOSURE: NEMA 1				SURGE PROTECTION DEVICE: YES				
SERVICE FROM: NA			MANUFACTURER: NORTHERN TECHNOLOGIES, INC (SQUARE D)				MODEL NUMBER: QO142M200				
DESCRIPTION	LOAD (VA)	C or NC	C/B	CIR No.	LOAD (VA)		CIR No.	C/B	C or NC	LOAD (VA)	DESCRIPTION
					A-PHASE	B-PHASE					
RECTIFIER CKT #1	1924	C	30	1	3848		2	30	C	1924	RECTIFIER CKT #2
RECTIFIER CKT #1	1924	C	-	3		3848	4	-	C	1924	RECTIFIER CKT #2
RECTIFIER CKT #3	1924	C	30	5	3848		6	30	C	1924	RECTIFIER CKT #4
RECTIFIER CKT #3	1924	C	-	7		3848	8	-	C	1924	RECTIFIER CKT #4
RECTIFIER CKT #5	1924	C	30	9	3848		10	30	C	1924	RECTIFIER CKT #6
RECTIFIER CKT #5	1924	C	-	11		3848	12	-	C	1924	RECTIFIER CKT #6
RECTIFIER CKT #7	1924	C	30	13	3848		14	30	C	1924	RECTIFIER CKT #8
RECTIFIER CKT #7	1924	C	-	15		3848	16	-	C	1924	RECTIFIER CKT #8
SPARE		NC	30	17	0		18	30	NC		SPARE
SPARE		NC	-	19		0	20	-	NC		SPARE
HVAC UNIT #1	1060	C	60	21	2120		22	60	C	1060	HVAC UNIT #2
HVAC UNIT #1	1060	C	-	23		2120	24	-	C	1060	HVAC UNIT #2
DIN-RAIL MOUNTED LOAD CENTER	1200	C	20	25	1200		26	60	NC		SPARE
VENT FAN	150	NC	15	27		150	28	-	NC		SPARE
RECEPTACLE	180	C	20	29	500		30	20	NC	320	LIGHTING
RECEPTACLE	180	C	20	31		360	32	20	C	180	SMOKE DETECTOR
RECEPTACLE	180	C	20	33	180		34	60	NC		SPARE
RECEPTACLE	180	C	20	35		180	36	-	NC		SPARE
SURGE ARRESTOR	0	C	60	37	180		38	20	C	180	EXT. RECEPTABLE
SURGE ARRESTOR	0	C	-	39		180	40	20	NC	180	GAS DETECTOR
BASE LOAD (VA) =					19572	18382	*C* DESIGNATION IDENTIFIES CONTINUOUS LOADS AND MOTOR LOADS AS REQUIRED BY SECTIONS 230.42 AND 430.24 OF THE NEC				
25% OF CONTINUOUS LOAD (VA) =					4813	4513					
TOTAL LOAD (VA) =					24385	22895					
TOTAL LOAD (A) =					204	191					

3 EXISTING/NEW PANEL SCHEDULE AND NOTES
SCALE: NOT TO SCALE

3 CORPORATE PARK DRIVE, SUITE 101
CLIFTON PARK, NY 12065

SPRINT SITE NUMBER:
CT54XC747

BU #: 822779
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

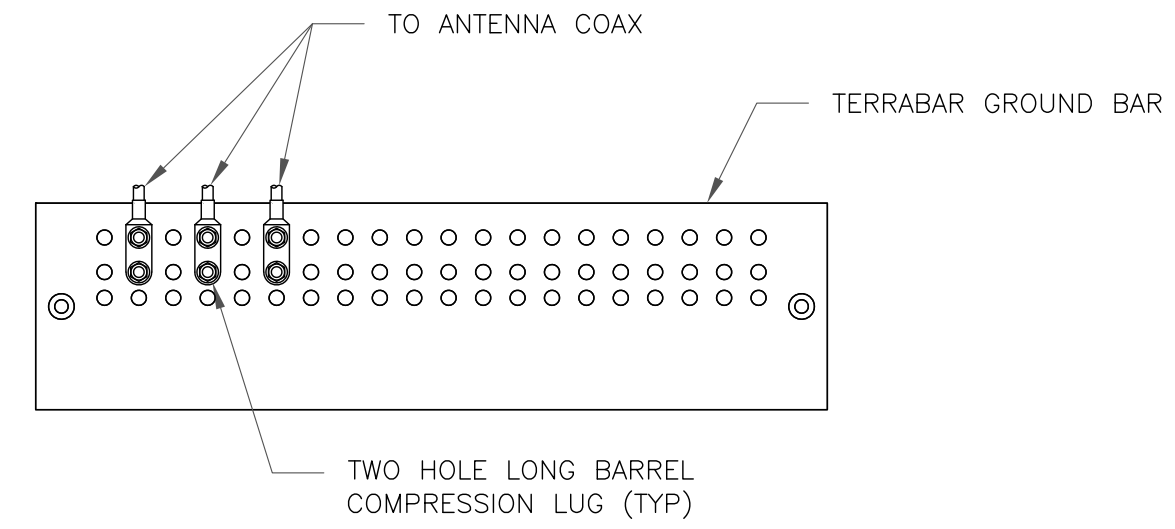
ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR

Justin Peter Linette, P.E.
Professional Engineer License: 31965
Crown Castle USA, Inc. Firm Registration #PEC.0001101

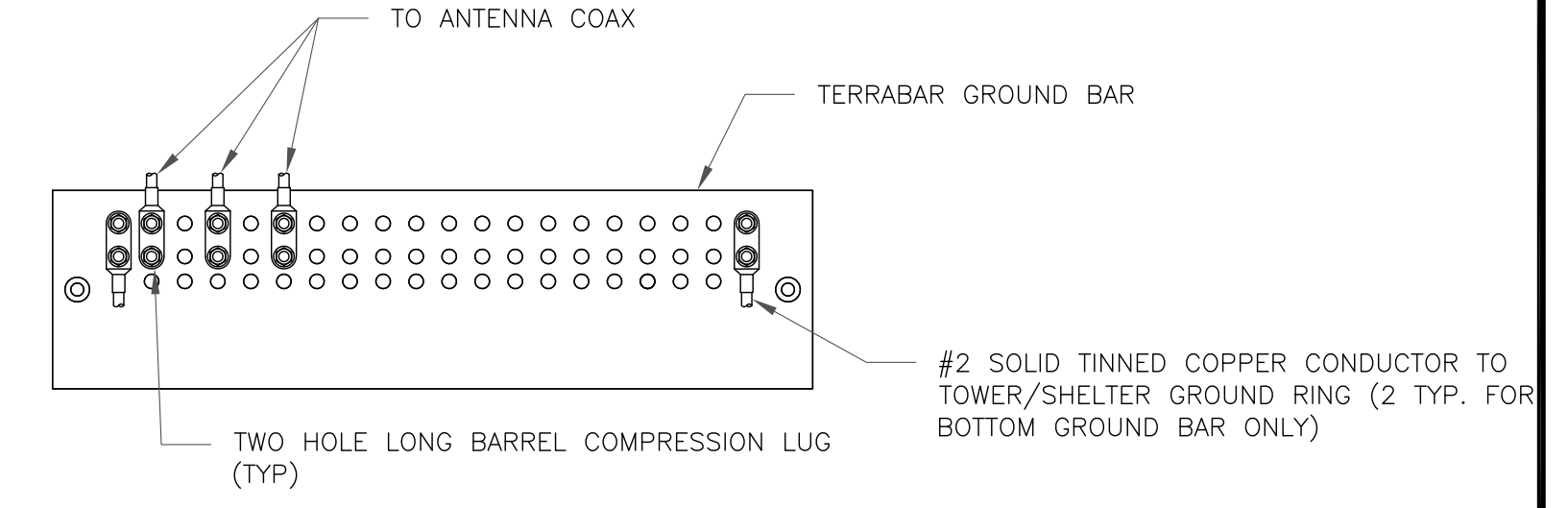
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SHEET NUMBER: **E-1** REVISION: **0**



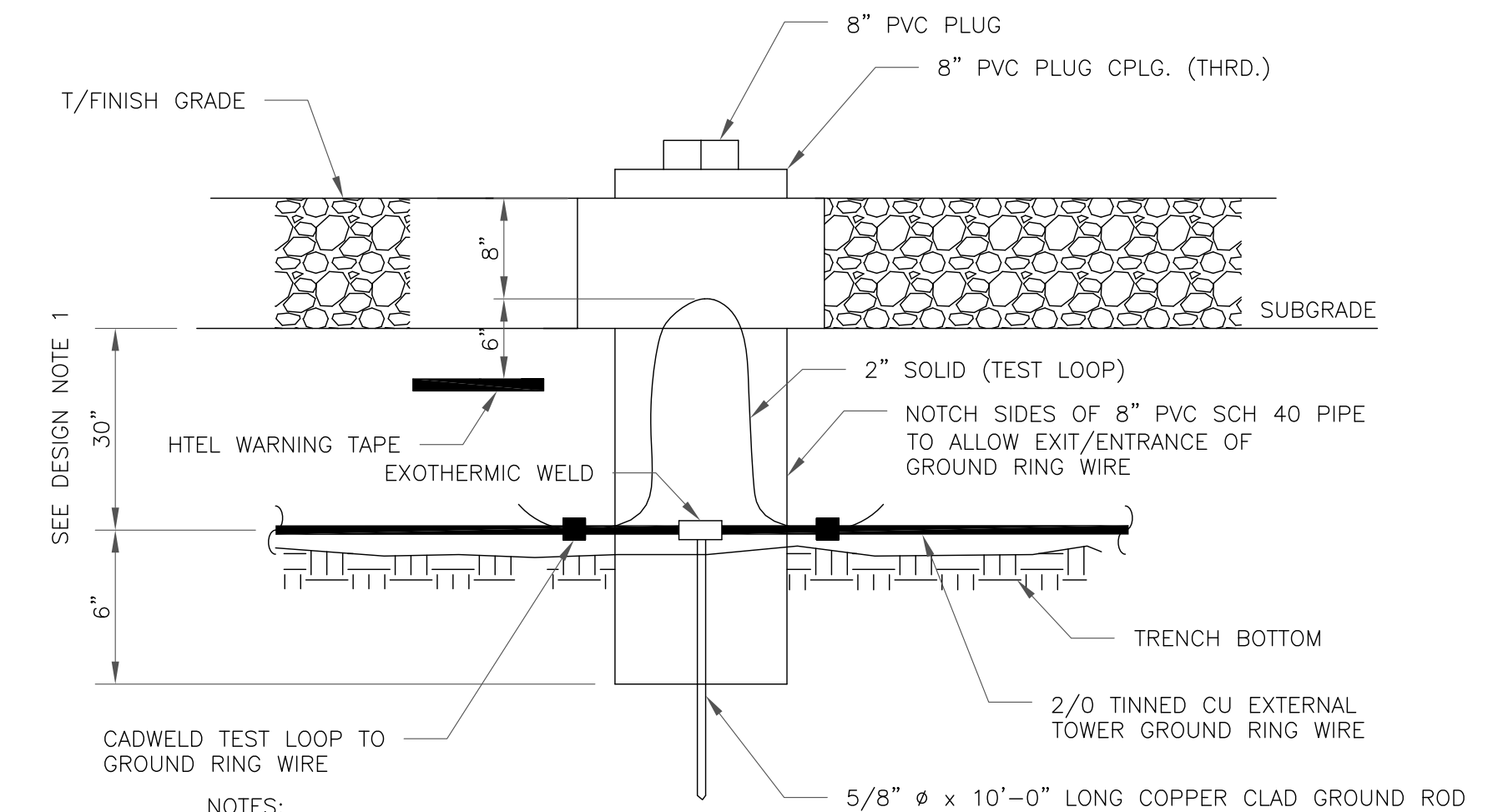
- NOTES:**
1. DOUBLING UP "OR STACKING" OF CONNECTIONS IS NOT PERMITTED.
 2. EXTERIOR ANTIOXIDANT JOINT COMPOUND TO BE USED ON ALL EXTERIOR CONNECTIONS.
 3. GROUND BAR SHALL NOT BE ISOLATED FROM TOWER. MOUNT DIRECTLY TO TOWER STEEL.

1 ANTENNA GROUND BAR DETAIL
SCALE: NOT TO SCALE



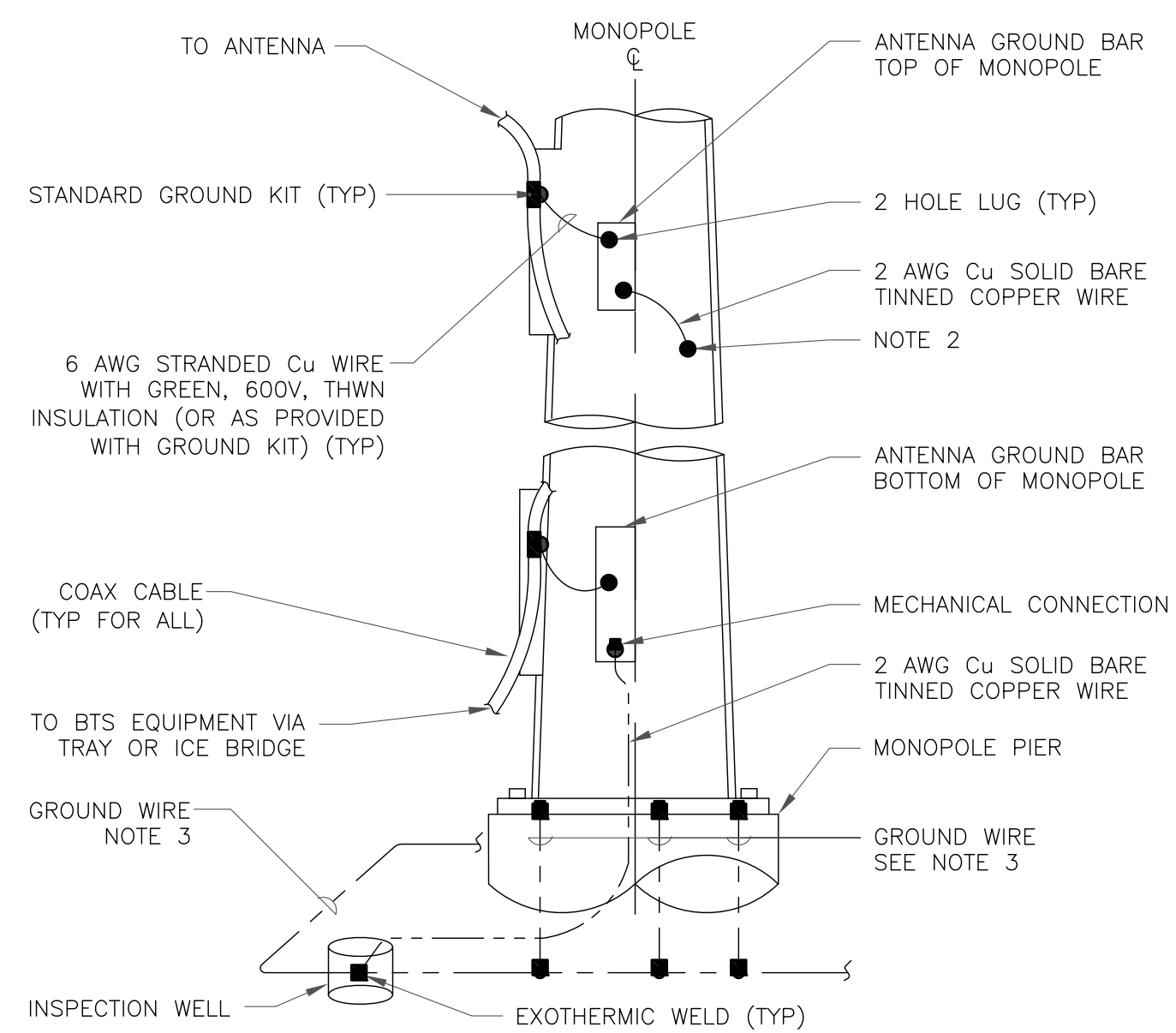
- NOTES:**
1. EXTERIOR ANTIOXIDANT JOINT COMPOUND TO BE USED ON ALL EXTERIOR CONNECTIONS.
 2. GROUND BAR SHALL NOT BE ISOLATED FROM TOWER. MOUNT DIRECTLY TO TOWER STEEL (TOWER ONLY).
 3. INSTALL GROUND BARS AT 75 FT. INTERVAL MAXIMUM.
 4. GROUND BAR SHALL BE ISOLATED FROM BUILDING OR SHELTER.

2 TOWER/SHELTER GROUND BAR DETAIL
SCALE: NOT TO SCALE



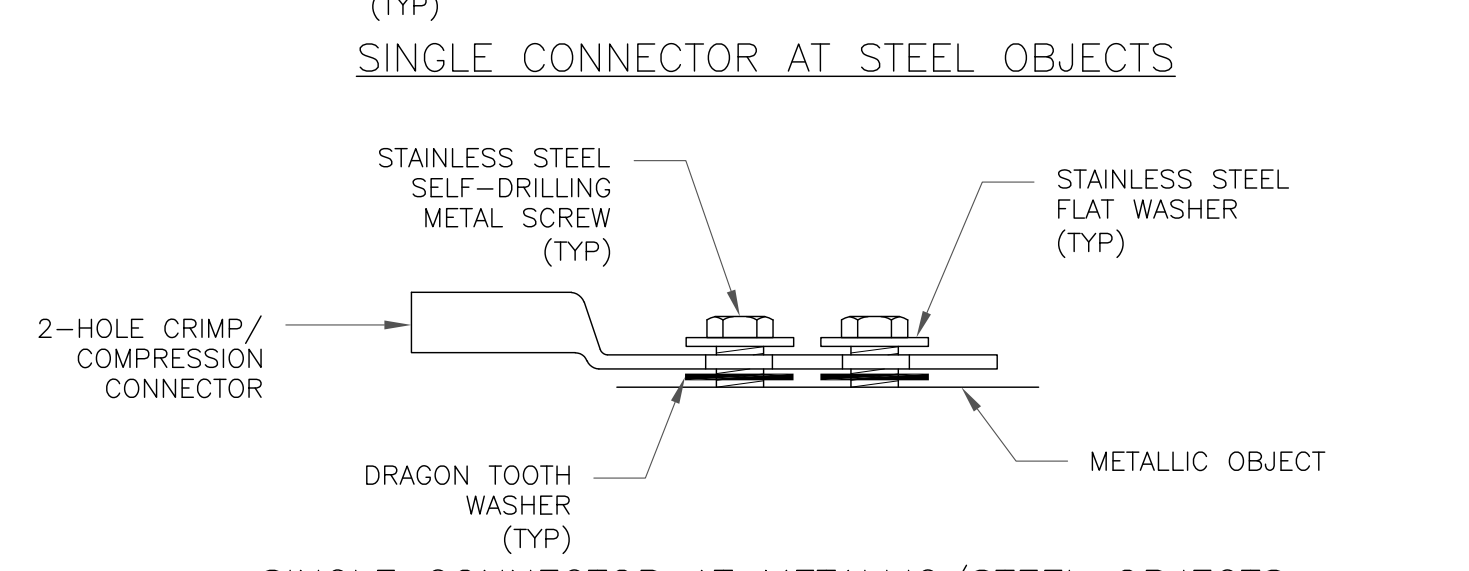
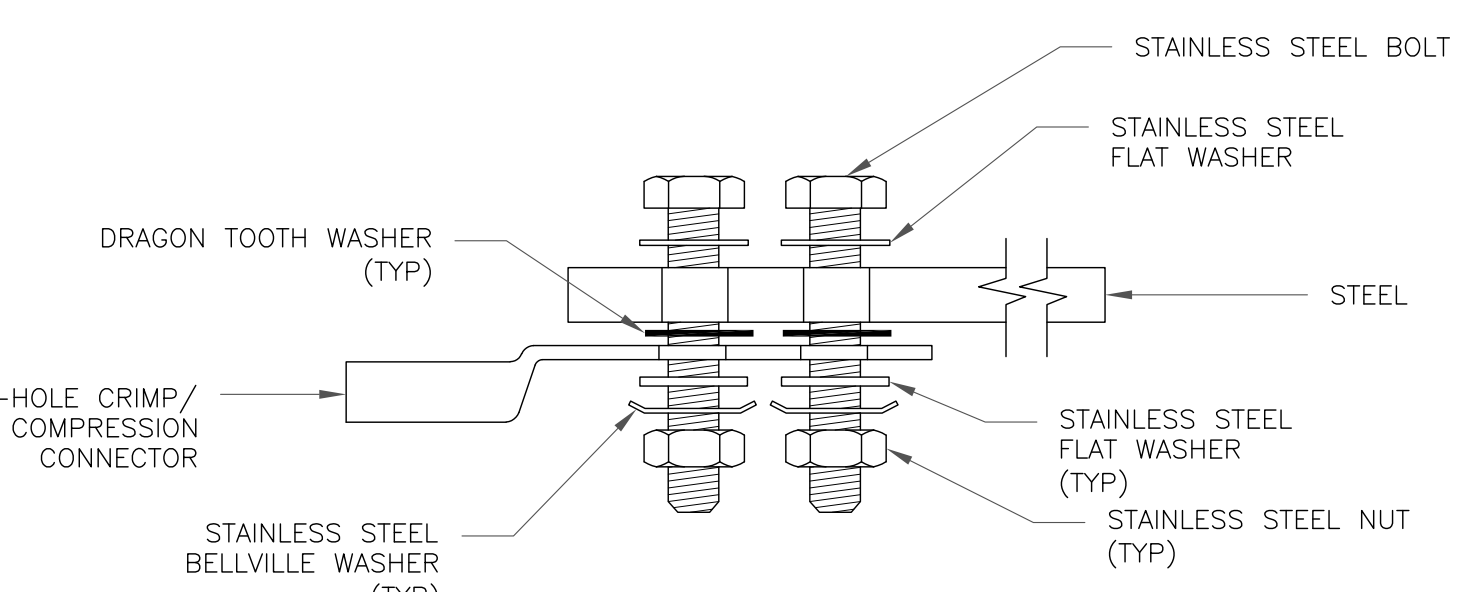
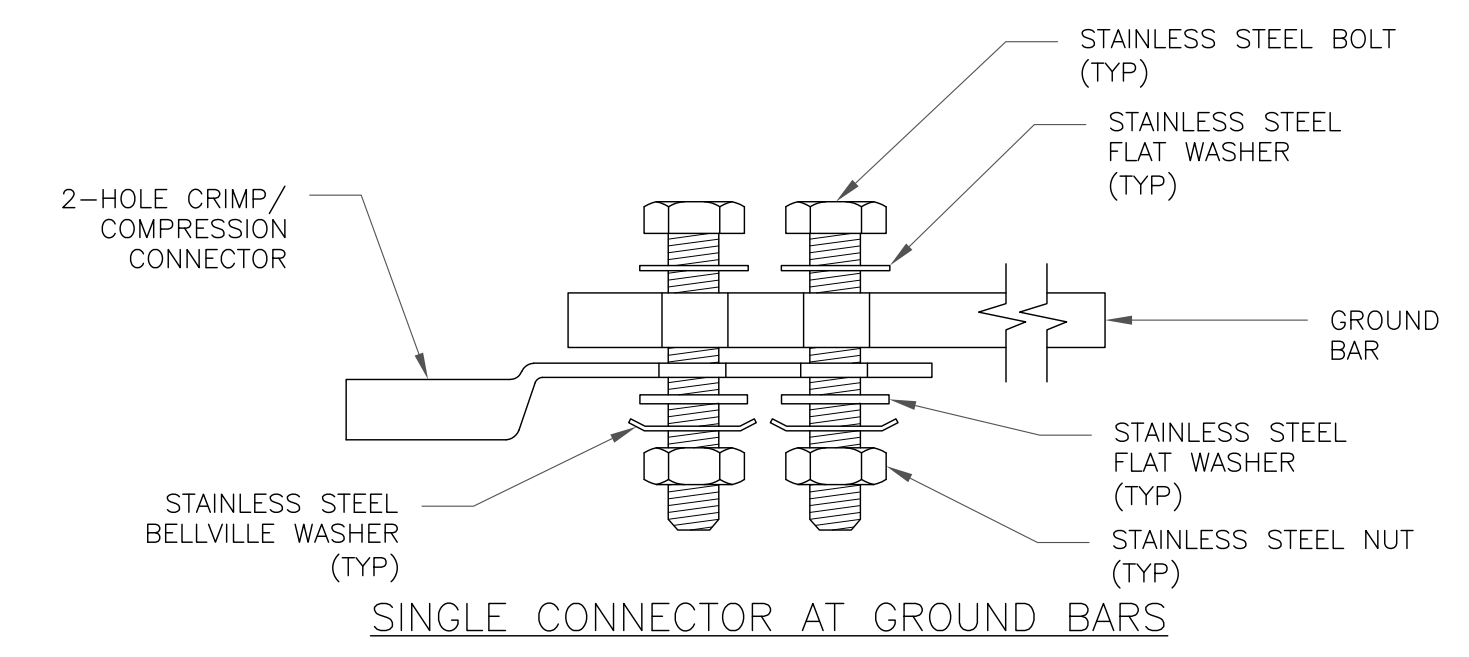
- NOTES:**
1. GROUND ROD SHALL BE DRIVEN VERTICALLY, NOT TO EXCEED 45 DEGREES FROM THE VERTICAL.
 2. GROUND WIRE SHALL BE MIN. 30" BELOW GRADE OR 6" BELOW FROST LINE. (WHICH EVER IS GREATER) AS PER N.E.C. ARTICLE 250-50(D)

3 INSPECTION PORT DETAIL
SCALE: NOT TO SCALE

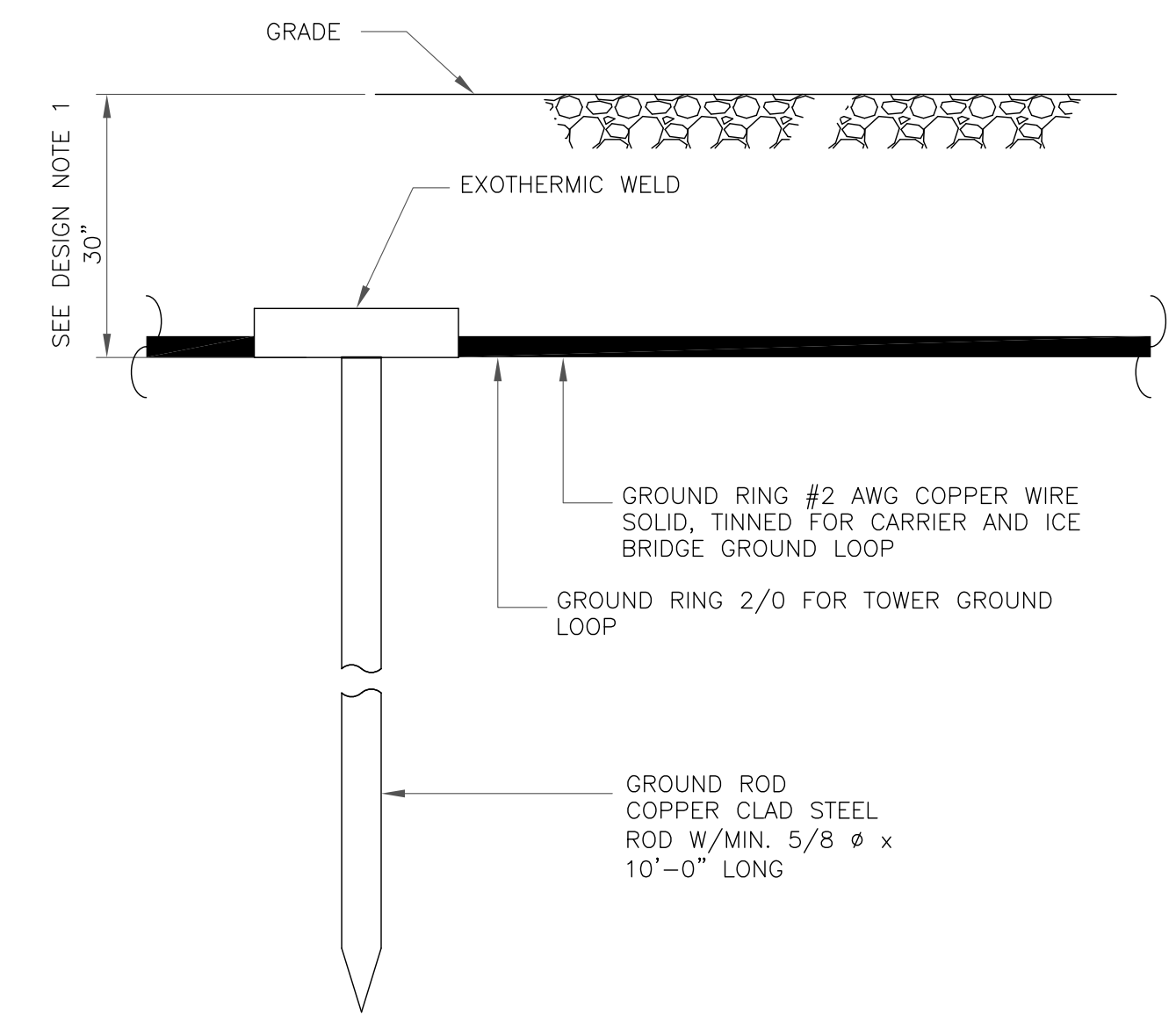


- NOTES:**
1. NUMBER OF GROUND BARS MAY VARY DEPENDING ON THE TYPE OF MONOPOLE, ANTENNA LOCATION AND CONNECTION ORIENTATION. COAXIAL CABLES EXCEEDING 200 FEET IN/ON THE POLE SHALL HAVE GROUND KITS AT THE MIDPOINT. PROVIDE AS REQUIRED.
 2. ONLY MECHANICAL CONNECTIONS ARE ALLOWED TO BE MADE TO CROWN CASTLE TOWERS. ALL MECHANICAL CONNECTIONS SHALL BE TREATED WITH AN ANTI-OXIDANT COATING.
 3. ALL TOWER GROUNDING SYSTEMS SHALL COMPLY WITH THE REQUIREMENTS OF ANSI/TIA 222. FOR TOWERS BEING BUILT TO REV G OF THE STANDARD, THE WIRE SIZE OF THE BURIED GROUND RING AND CONNECTIONS BETWEEN THE TOWER AND THE BURIED GROUND RING SHALL BE 2/0 AWG. STRANDED IN ADDITION, THE MINIMUM LENGTH OF THE GROUND RODS SHALL BE INCREASED FROM 8 FEET TO 10 FEET.

4 TYPICAL ANTENNA CABLE GROUNDING
SCALE: NOT TO SCALE



5 HARDWARE DETAIL FOR EXTERIOR CONNECTIONS
SCALE: NOT TO SCALE



- NOTES:**
1. GROUND ROD SHALL BE DRIVEN VERTICALLY, NOT TO EXCEED 45 DEGREES FROM THE VERTICAL.
 2. GROUND WIRE SHALL BE MIN. 30" BELOW GRADE OR 6" BELOW FROST LINE. (WHICH EVER IS GREATER) AS PER N.E.C. ARTICLE 250-50(D)

6 GROUND ROD DETAIL
SCALE: NOT TO SCALE



SPRINT SITE NUMBER:
CT54XC747

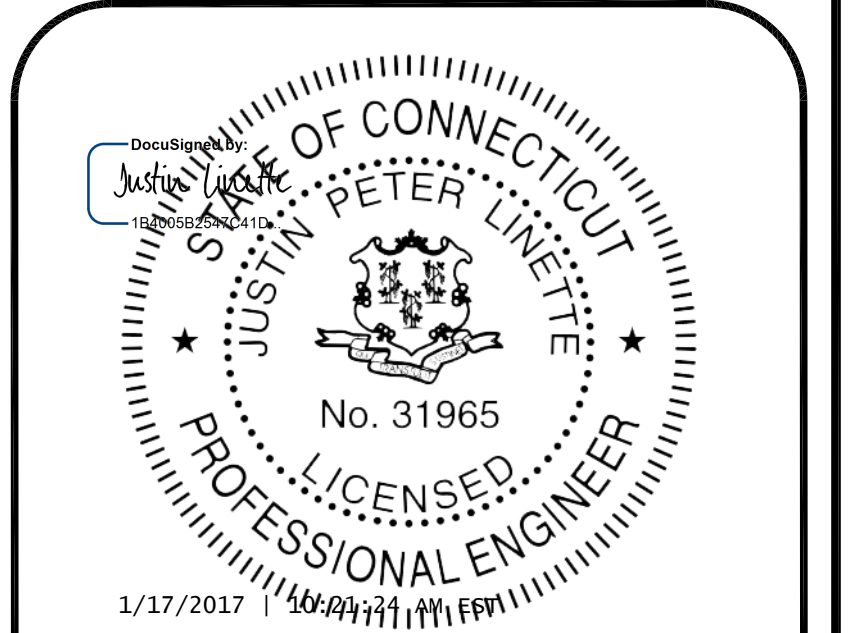
BU #: **822779**
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

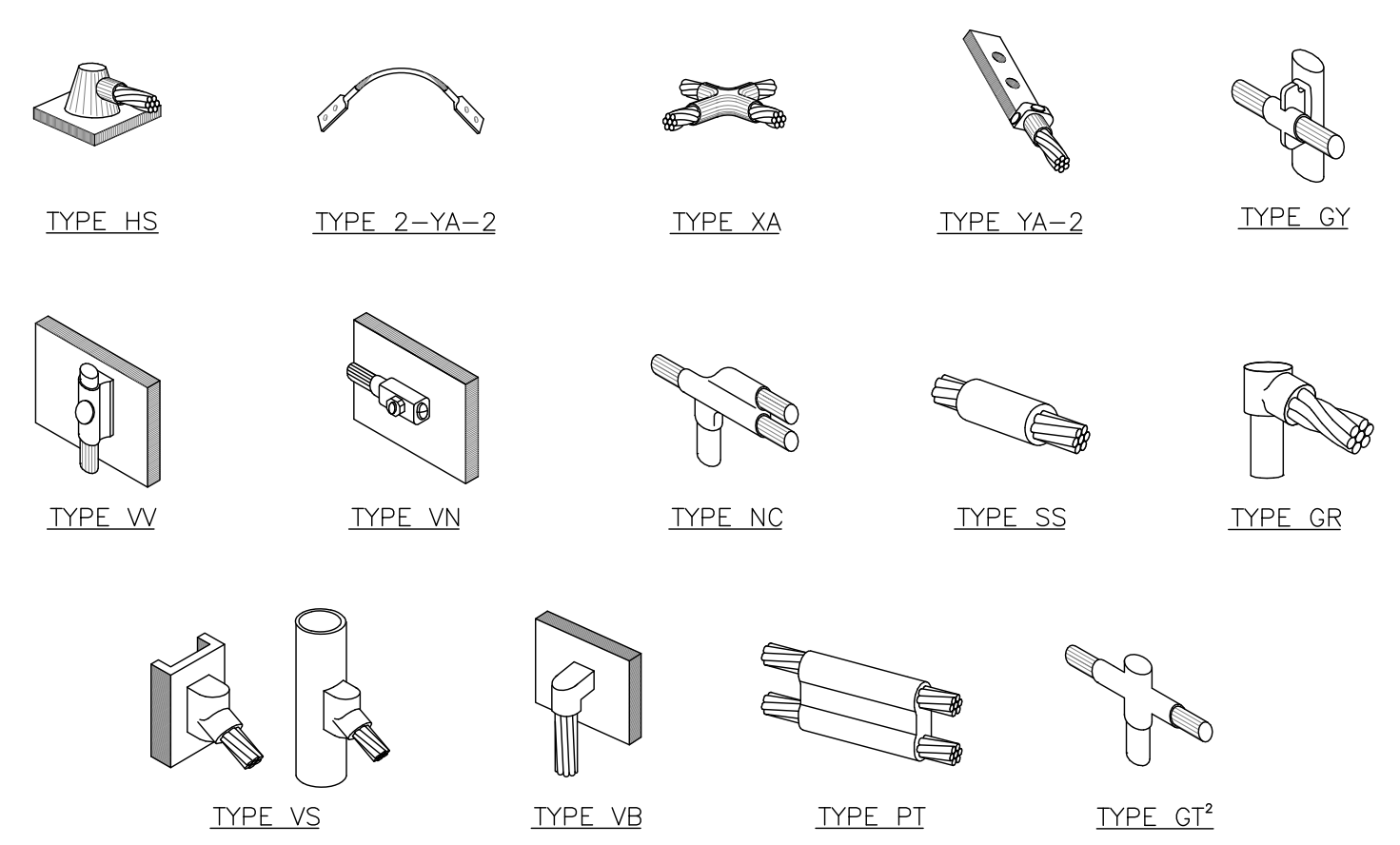
ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
B	01/12/17	JRM	PRELIMINARY	LMR
0	01/17/17	JRM	CONSTRUCTION	LMR



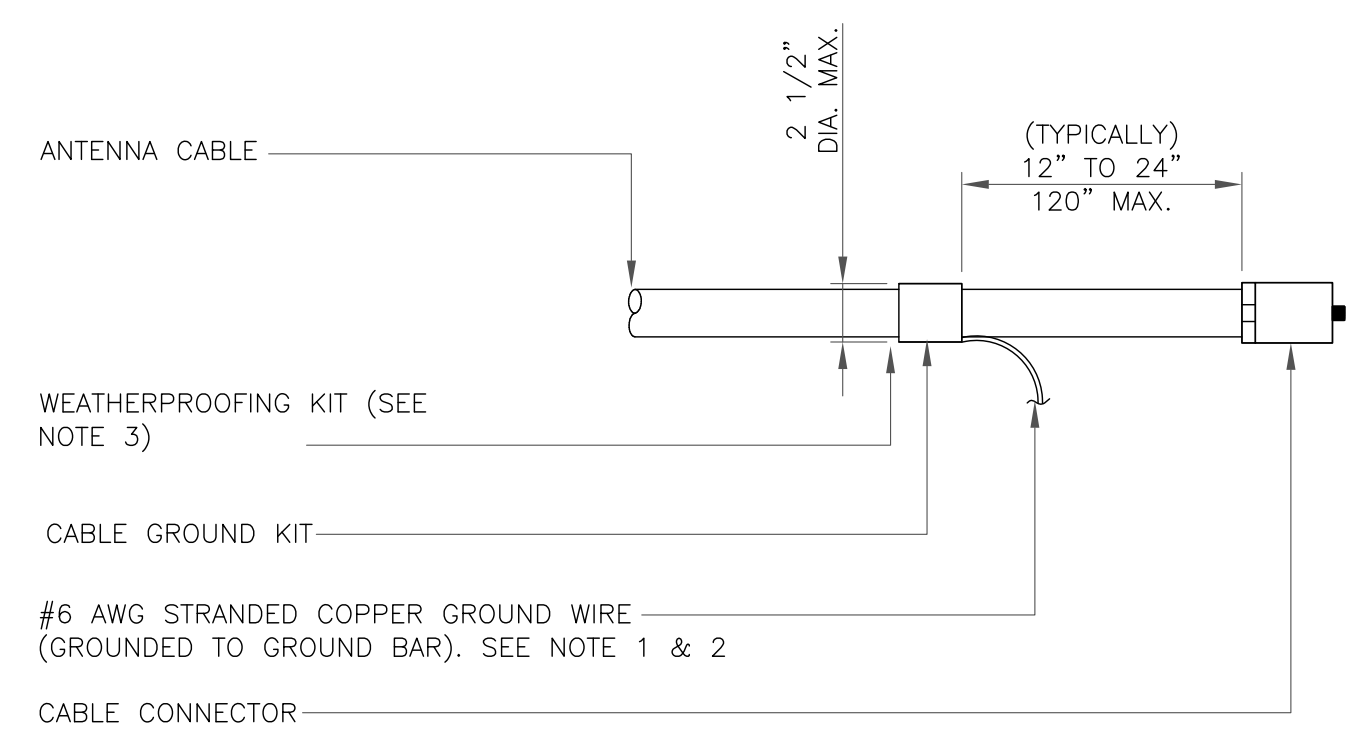
Justin Peter Linette, P.E.
Professional Engineer License: 31965
Crown Castle USA, Inc. Firm Registration #PEC.0001101
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SHEET NUMBER: **G-1** REVISION: **0**



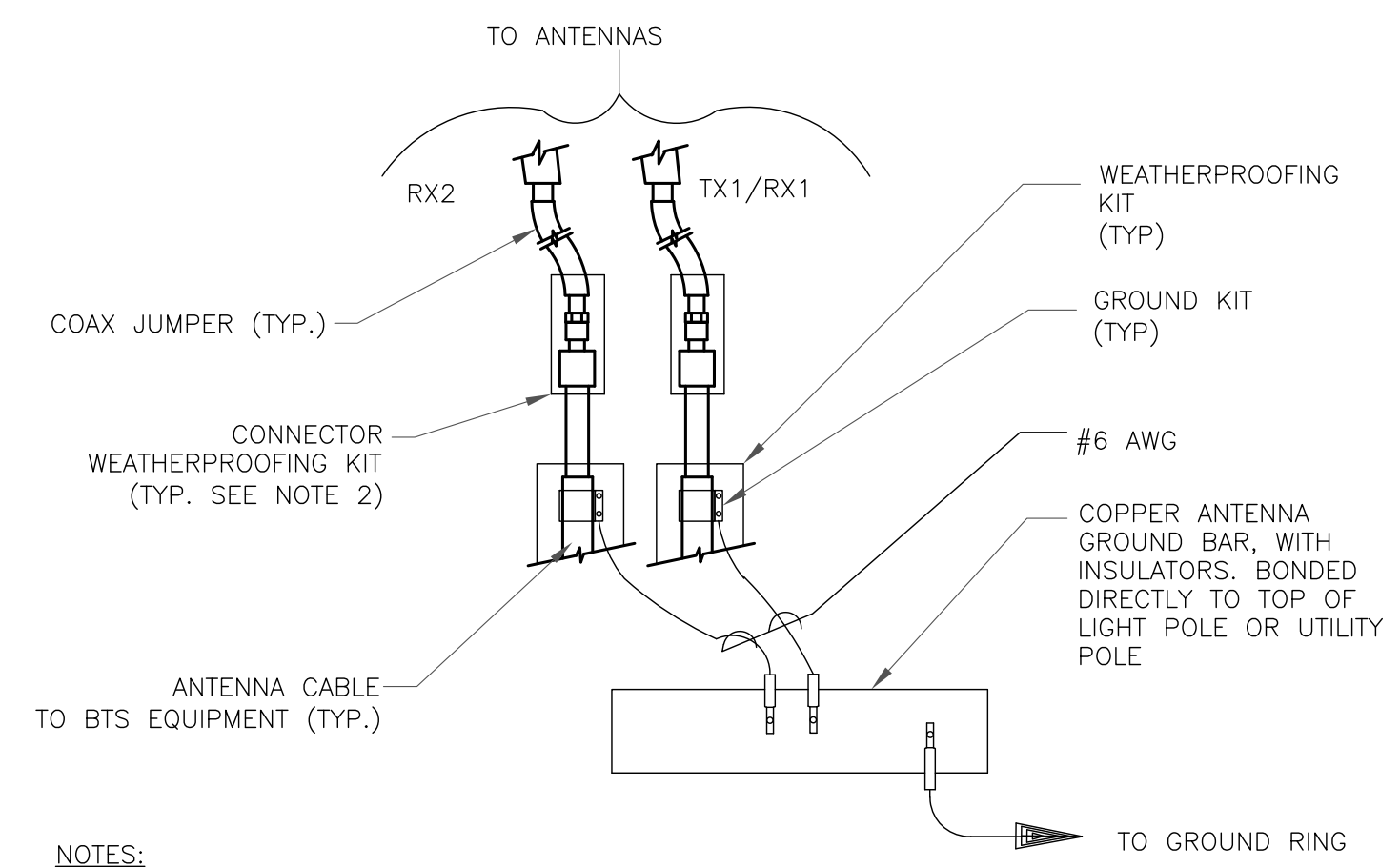
NOTE:
 1. ERICO EXOTHERMIC "MOLD TYPES" SHOWN HERE ARE EXAMPLES. CONSULT WITH CONSTRUCTION MANAGER FOR SPECIFIC MOLDS TO BE USED FOR THIS PROJECT.
 2. MOLD TYPE ONLY TO BE USED BELOW GRADE WHEN CONNECTING GROUND RING TO GROUND ROD.

1 CADWELD GROUNDING CONNECTIONS
 SCALE: NOT TO SCALE



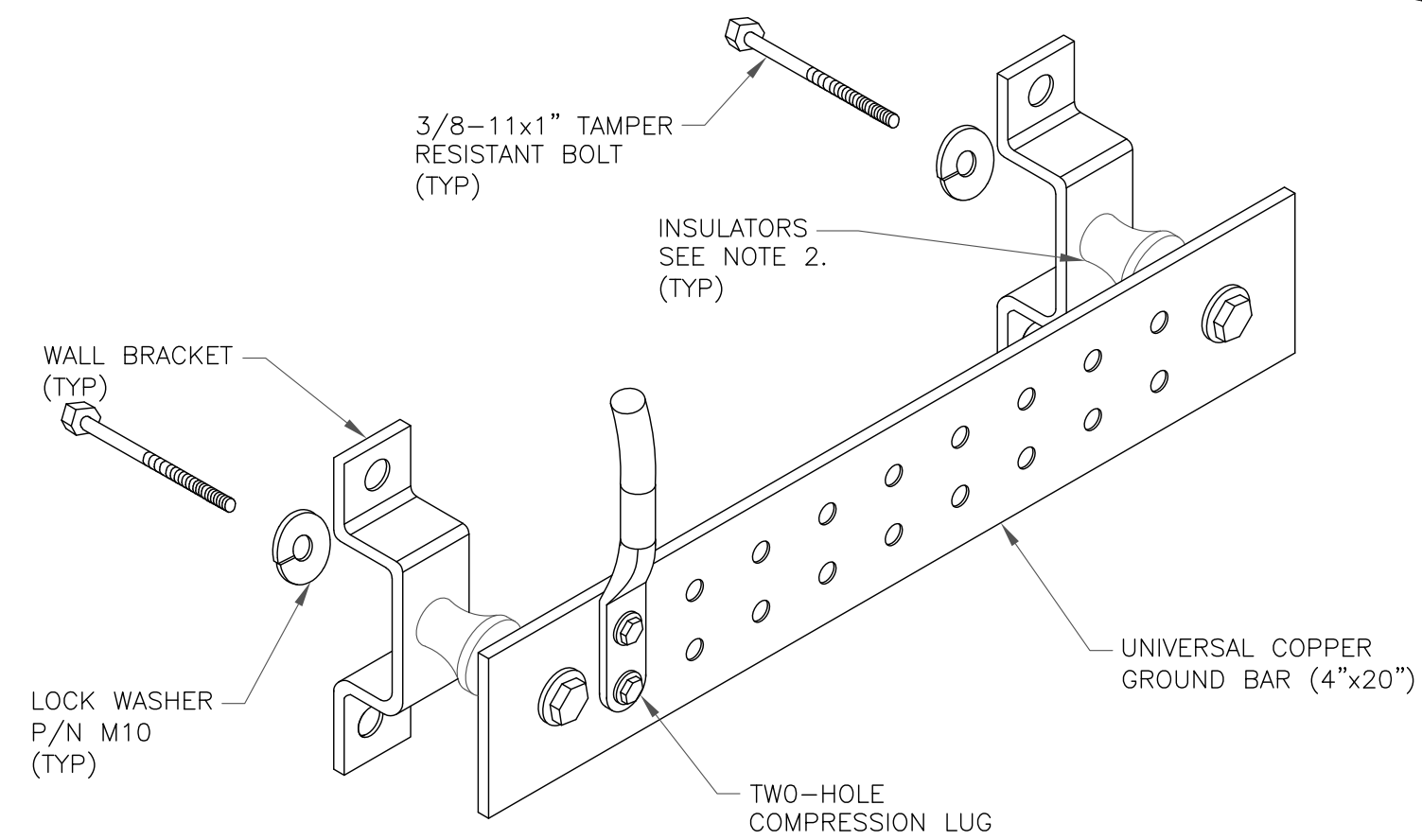
NOTES:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO GROUND BAR.
 2. GROUNDING KIT SHALL BE TYPE AND PART NUMBER AS SUPPLIED OR RECOMMENDED BY CABLE MANUFACTURER.
 3. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT. COLD SHRINK SHALL NOT BE USED.

3 CABLE GROUND KIT CONNECTION
 SCALE: NOT TO SCALE



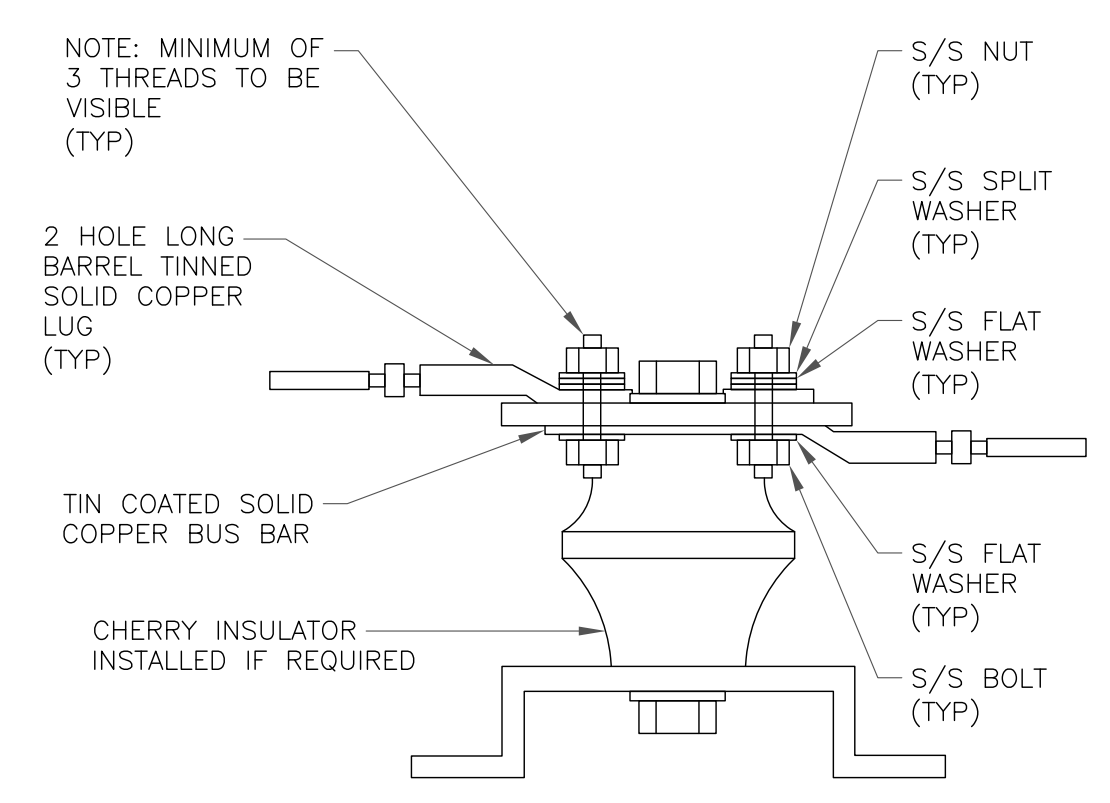
NOTES:
 1. DO NOT INSTALL CABLE GROUND KIT AT A BEND AND ALWAYS DIRECT GROUND WIRE DOWN TO ANTENNA GROUND BAR.
 2. WEATHER PROOFING SHALL BE TWO-PART TAPE KIT. COLD SHRINK SHALL NOT BE USED.

4 GROUND CABLE CONNECTION
 SCALE: NOT TO SCALE



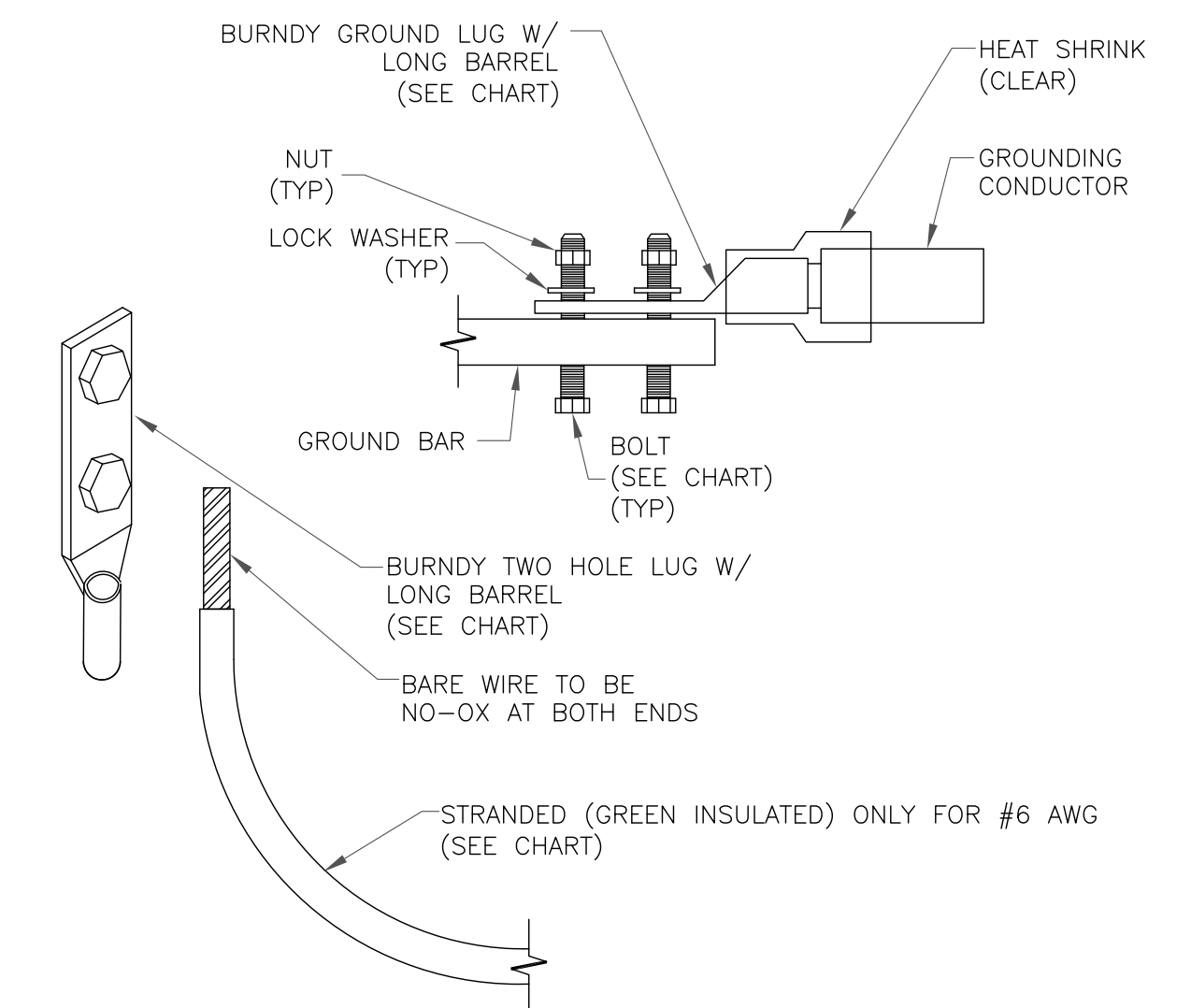
NOTES:
 1. DOWN LEAD (HOME RUN) CONDUCTORS ARE NOT TO BE INSTALLED ON CROWN CASTLE TOWER, PER THE GROUNDING DOWN CONDUCTOR POLICY GAS-STD-10091. NO MODIFICATION OR DRILLING TO TOWER STEEL IS ALLOWED IN ANY FORM OR FASHION, CAD-WELDING ON THE TOWER AND/OR IN THE AIR ARE NOT PERMITTED.
 2. OMIT INSULATOR WHEN MOUNTING TO TOWER STEEL OR PLATFORM STEEL. USE INSULATORS WHEN ATTACHING TO BUILDING OR SHELTERS.

6 GROUND BAR DETAIL
 SCALE: NOT TO SCALE



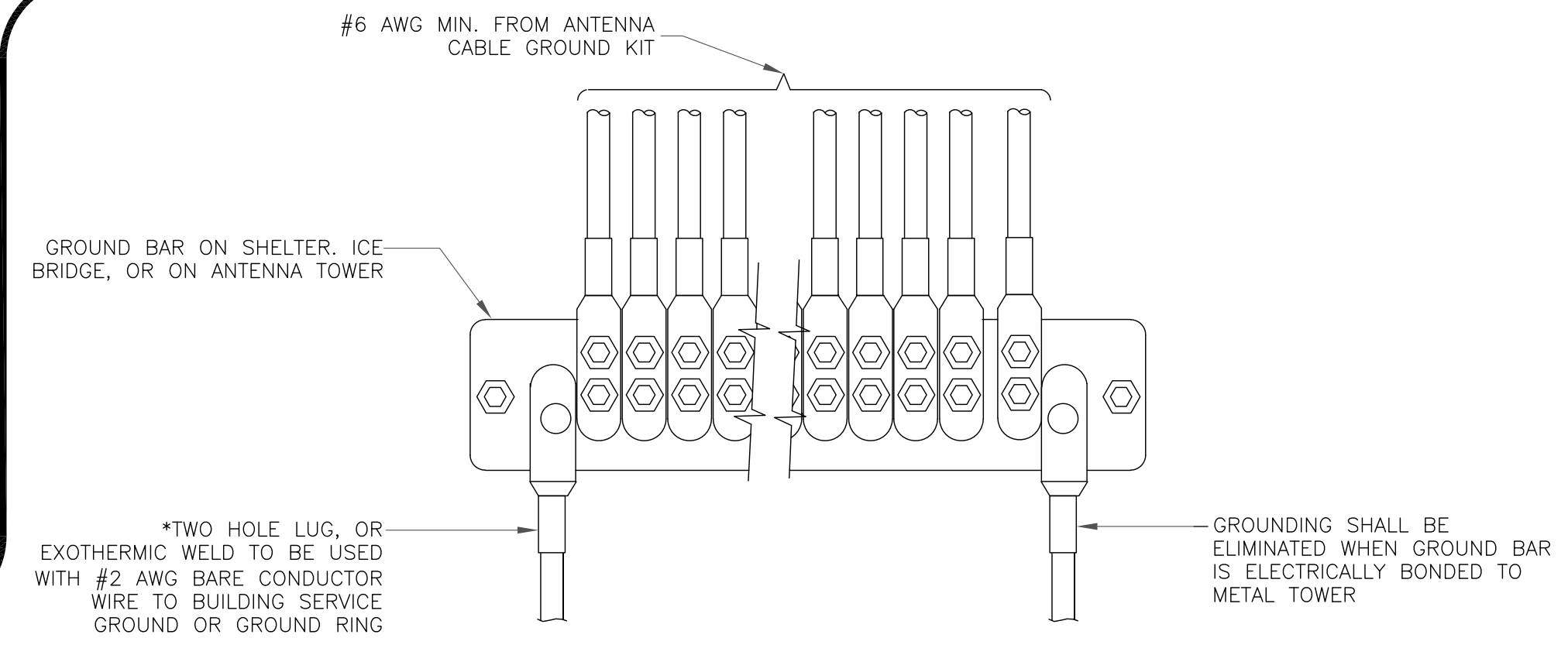
7 LUG DETAIL
 SCALE: NOT TO SCALE

WIRE SIZE	BURNDY LUG	BOLT SIZE
#6 AWG GREEN INSULATED	YA6C-2TC38	3/8" - 16 NC S 2 BOLT
#2 AWG SOLID TINNED	YA3C-2TC38	3/8" - 16 NC S 2 BOLT
#2 AWG STRANDED	YA2C-2TC38	3/8" - 16 NC S 2 BOLT
#2/0 AWG STRANDED	YA26-2TC38	3/8" - 16 NC S 2 BOLT
#4/0 AWG STRANDED	YA28-2N	1/2" - 16 NC S 2 BOLT

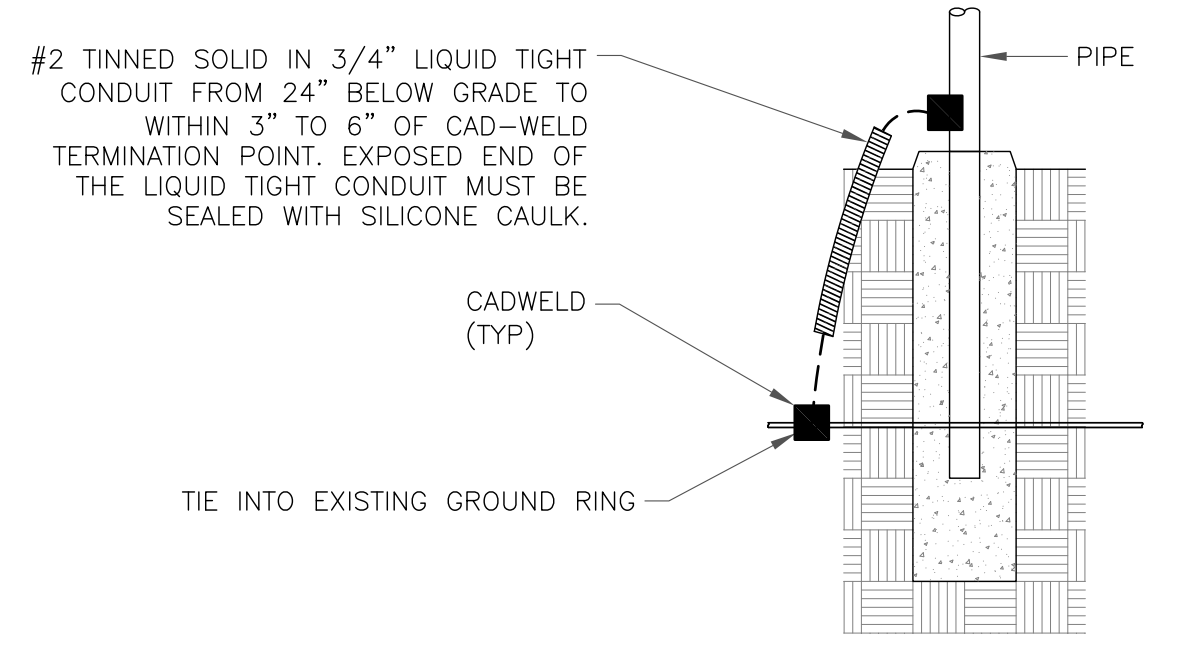


NOTES:
 1. ALL GROUNDING LUGS ARE TO BE INSTALLED PER MANUFACTURER'S SPECIFICATIONS. ALL HARDWARE BOLTS, NUTS, LOCK WASHERS SHALL BE STAINLESS STEEL. ALL HARDWARE ARE TO BE AS FOLLOWS: BOLT, FLAT WASHER, GROUND BAR, GROUND LUG, FLAT WASHER AND NUT.
 STRANDED (GREEN INSULATED) ONLY FOR #6 AWG (SEE CHART)

2 MECHANICAL LUG CONNECTION
 SCALE: NOT TO SCALE



5 GROUNDWIRE INSTALLATION
 SCALE: NOT TO SCALE



8 TRANSITIONING GROUND DETAIL
 SCALE: NOT TO SCALE



SPRINT SITE NUMBER:
CT54XC747

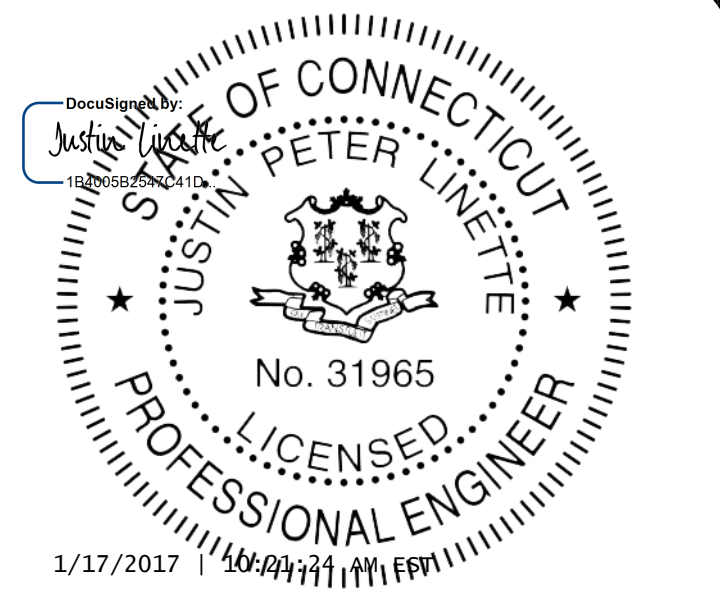
BU #: 822779
BRIDGEPORT/ RT 8

1875 NOBLE AVENUE
BRIDGEPORT, CT 06610

EXISTING 120'-0" FLAGPOLE

ISSUED FOR:

REV	DATE	DRWN	DESCRIPTION	DES./QA
A	12/23/16	CJ	PRELIMINARY	LMR
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SHEET NUMBER:
G-2

REVISION:
0



Date: November 21, 2016

Andrew Bazinet
Crown Castle
3 Corporate Park Drive Suite 101
Clifton Park, NY 12065
585.370.4766

Paul J Ford and Company
250 E. Broad Street, Suite 600
Columbus, OH 43215
614.221.6679
stschanen@pjfweb.com

Subject: Structural Analysis Report

Carrier Designation: Sprint PCS Co-Locate
Carrier Site Number: CT54XC747
Carrier Site Name: N/A

Crown Castle Designation: Crown Castle BU Number: 822779
Crown Castle Site Name: Bridgeport/ Rt 8
Crown Castle JDE Job Number: 408063
Crown Castle Work Order Number: 1327701
Crown Castle Application Number: 368093 Rev. 1

Engineering Firm Designation: Paul J Ford and Company Project Number: 37516-3608.001.7805

Site Data: 1875 Noble Avenue, Bridgeport, Fairfield County, CT
Latitude 41° 12' 37.271", Longitude -73° 10' 52.259"
120 Foot - Monopole Tower

Dear Andrew Bazinet,

Paul J Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 972394, in accordance with application 368093, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

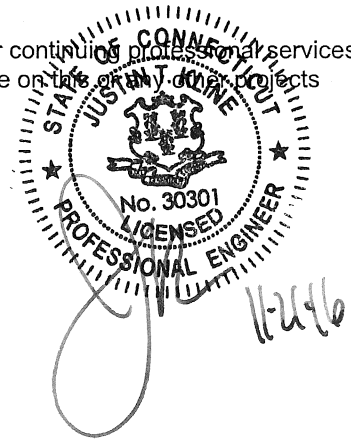
LC5: Existing + Proposed Equipment **Sufficient Capacity**
Note: See Table I and Table II for the proposed and existing loading, respectively.

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 125 mph converted to a nominal 3-second gust wind speed of 97 mph per Section 1609.3 and Appendix N as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1. Risk Category II, Exposure Category C and Topographic Category 1 were used in this analysis.

We at Paul J Ford and Company appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on any of our projects please give us a call.

Respectfully submitted by:

Seth Tschanen, E.I. *TS*
Structural Designer



Date: **November 21, 2016**

Andrew Bazinet
Crown Castle
3 Corporate Park Drive Suite 101
Clifton Park, NY 12065
585.370.4766

Paul J Ford and Company
250 E. Broad Street, Suite 600
Columbus, OH 43215
614.221.6679
stschanen@pjfweb.com

Subject: Structural Analysis Report

Carrier Designation: **Sprint PCS Co-Locate**
Carrier Site Number: CT54XC747
Carrier Site Name: N/A

Crown Castle Designation: **Crown Castle BU Number:** 822779
Crown Castle Site Name: Bridgeport/ Rt 8
Crown Castle JDE Job Number: 408063
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Sufficient Capacity

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Respectfully submitted by:

Seth Tschanen, E.I.
Structural Designer

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3.2) Assumptions

4) ANALYSIS RESULTS

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7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 120 ft Monopole tower designed by PIROD MANUFACTURES INC. in June of 2000. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

2) ANALYSIS CRITERIA

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3-second gust wind speed of 125 mph converted to a nominal 3-second gust wind speed of 97 mph per Section 1609.3 and Appendix N as required for use in the ANSI/TIA-222-G-2005 Standard, "Structural Standard for Antenna Supporting Structures and Antennas", with ANSI/TIA-222-G-1-2007 and ANSI/TIA-222-G-2-2009 Addenda per Exception #5 of Section 1609.1.1. Risk Category II, Exposure Category C and Topographic Category 1 were used in this analysis.

Table 1 - Proposed Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
95.0	96.0	3	commscope	DHHTT65B-3XR	1	1/8	--
	92.0	3	nokia	FWHR		4	
	91.0	1	box enclosures and assembly	BEN-92P	1	7/8	

Table 2 - Existing Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
115.0	117.0	3	ericsson	KRY 112 144/1	6	1 5/8	1
		3	rfs celwave	APXV18-206517S-C-ACU			
		3	rfs celwave	ATMAA1412D-1A20			
105.0	107.0	3	ericsson	KRY 112 144/1	6	1 5/8	1
		3	rfs celwave	APXV18-206517S-C-ACU			
95.0	95.0	--	--	--	2	3/8	1
		3	decibel	932LG65R2E-B	6	1 1/4	
					--	--	2

Notes:

- 1) Existing Equipment
- 2) Equipment To Be Removed

Table 3 - Design Antenna and Cable Information

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
--	--	--	--	--	--	--

3) ANALYSIS PROCEDURE

Table 4 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH Velocitel, 15BZKS1600, 10/7/15	3584592	CCISITES
4-POST-MODIFICATION INSPECTION	TEP, 61158.32797, 4/29/16	6261360	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	Pirod, A-116835, 6/1/00	3914232	CCISITES
4-TOWER MANUFACTURER DRAWINGS	Pirod, A-116835, 6/1/00	3584593	CCISITES

3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Monopole was modified in conformance with the referenced modification drawings.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	120 - 110	Pole	P10.75x0.349	1	-0.71	431.06	11.6	Pass
L2	110 - 100	Pole	P10.75x0.349	2	-1.79	431.06	32.1	Pass
L3	100 - 90	Pole	P10.75x0.349	3	-3.13	431.06	61.4	Pass
L4	90 - 82	Pole	P10.75x0.349	4	-4.12	431.06	90.5	Pass
L5	82 - 60	Pole	P24x0.375	5	-7.29	1052.07	36.6	Pass
L6	60 - 30	Pole	P24x0.375	6	-11.30	1052.07	69.8	Pass
L7	30 - 8.5	Pole	P24x0.375	7	-14.32	1052.07	97.3	Pass
L8	8.5 - 0	Pole	P24x0.5	8	-15.84	1313.94	82.9	Pass
							Summary	
						Pole (L7)	97.3	Pass
						Rating =	97.3	Pass

Table 6 - Tower Component Stresses vs. Capacity – LC5

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	17.5	Pass
1	Base Plate	0	19.9	Pass
1	Base Foundation	0	60.2	Pass
1	Flange Connection	110	9.9	Pass
1	Flange Connection	100	27.7	Pass
1	Flange Connection	90	53.1	Pass
1	Flange Connection	82	92.4	Pass
1	Flange Connection	60	63.2	Pass
1	Flange Connection	30	96.9	Pass

Structure Rating (max from all components) =	97.3%
---	--------------

Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

4.1) Recommendations

The monopole and its foundation have sufficient capacity to carry the proposed loading configuration. No modifications are required at this time.

APPENDIX A
TNXTOWER OUTPUT

Tower Input Data

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

- 1) Tower is located in Fairfield County, Connecticut.
- 2) ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).
- 3) Basic wind speed of 97 mph.
- 4) Structure Class II.
- 5) Exposure Category C.
- 6) Topographic Category 1.
- 7) Crest Height 0.0000 ft.
- 8) Nominal ice thickness of 0.7500 in.
- 9) Ice thickness is considered to increase with height.
- 10) Ice density of 56.00 pcf.
- 11) A wind speed of 50 mph is used in combination with ice.
- 12) Temperature drop of 50 °F.
- 13) Deflections calculated using a wind speed of 60 mph.
- 14) A non-linear (P-delta) analysis was used.
- 15) Pressures are calculated at each section.
- 16) Stress ratio used in pole design is 1.
- 17) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification ✓ Use Code Stress Ratios ✓ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile Include Bolts In Member Capacity Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric	Distribute Leg Loads As Uniform Assume Legs Pinned ✓ Assume Rigid Index Plate ✓ Use Clear Spans For Wind Area Use Clear Spans For KL/r Retension Guys To Initial Tension ✓ Bypass Mast Stability Checks ✓ Use Azimuth Dish Coefficients ✓ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder	Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation ✓ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption <div style="text-align: center; background-color: #e0e0e0; padding: 2px;">Poles</div> ✓ Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets
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Pole Section Geometry

Section	Elevation <i>ft</i>	Section Length <i>ft</i>	Pole Size	Pole Grade	Socket Length <i>ft</i>
L1	120.0000- 110.0000	10.0000	P10.75x0.349	A500-42 (42 ksi)	
L2	110.0000- 100.0000	10.0000	P10.75x0.349	A500-42 (42 ksi)	
L3	100.0000- 90.0000	10.0000	P10.75x0.349	A500-42 (42 ksi)	
L4	90.0000-82.0000	8.0000	P10.75x0.349	A500-42 (42 ksi)	
L5	82.0000-60.0000	22.0000	P24x0.375	A53-B-42 (42 ksi)	
L6	60.0000-30.0000	30.0000	P24x0.375	A53-B-42 (42 ksi)	
L7	30.0000-8.5000	21.5000	P24x0.375	A53-B-42	

Section	Elevation ft	Section Length ft	Pole Size	Pole Grade	Socket Length ft
L8	8.5000-0.0000	8.5000	P24x0.5	(42 ksi) Reinf 39.55 ksi (40 ksi)	

Tower Elevation ft	Gusset Area (per face) ft ²	Gusset Thickness in	Gusset Grade	Adjust. Factor A _r	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L1 120.0000- 110.0000				1	0	1			
L2 110.0000- 100.0000				1	0	1			
L3 100.0000- 90.0000				1	0	1			
L4 90.0000- 82.0000				1	0	1			
L5 82.0000- 60.0000				1	1	1			
L6 60.0000- 30.0000				1	1	1			
L7 30.0000- 8.5000				1	1	1			
L8 8.5000- 0.0000				1	1	1			

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C _A A _A ft ² /ft	Weight plf
LDF7-50A(1-5/8")	C	No	Inside Pole	115.0000 - 0.0000	6	No Ice	0.0000	0.82
						1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82

LDF7-50A(1-5/8")	C	No	Inside Pole	105.0000 - 0.0000	6	No Ice	0.0000	0.82
						1/2" Ice	0.0000	0.82
						1" Ice	0.0000	0.82

LDF6-50A(1-1/4")	C	No	Inside Pole	95.0000 - 0.0000	6	No Ice	0.0000	0.66
						1/2" Ice	0.0000	0.66
						1" Ice	0.0000	0.66
9833(3/8")	C	No	Inside Pole	95.0000 - 0.0000	2	No Ice	0.0000	0.07
						1/2" Ice	0.0000	0.07
						1" Ice	0.0000	0.07
7919A(17/64")	C	No	Inside Pole	95.0000 - 0.0000	4	No Ice	0.0000	0.03
						1/2" Ice	0.0000	0.03
						1" Ice	0.0000	0.03
004U8X- 32125E2G(1/8)	C	No	Inside Pole	95.0000 - 0.0000	1	No Ice	0.0000	0.01
						1/2" Ice	0.0000	0.01
						1" Ice	0.0000	0.01
TYPE SOOW 12/9(7/8")	C	No	Inside Pole	95.0000 - 0.0000	1	No Ice	0.0000	0.51
						1/2" Ice	0.0000	0.51
						1" Ice	0.0000	0.51

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
L1	120.0000- 110.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.02
L2	110.0000-	A	0.000	0.000	0.000	0.000	0.00

Tower Section n	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
	100.0000	B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.07
L3	100.0000-90.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.12
L4	90.0000-82.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.12
L5	82.0000-60.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.32
L6	60.0000-30.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.44
L7	30.0000-8.5000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.31
L8	8.5000-0.0000	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.12

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section n	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
L1	120.0000-110.0000	A	1.699	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.02
L2	110.0000-100.0000	A	1.684	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.07
L3	100.0000-90.0000	A	1.667	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.12
L4	90.0000-82.0000	A	1.651	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.12
L5	82.0000-60.0000	A	1.619	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.32
L6	60.0000-30.0000	A	1.547	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.44
L7	30.0000-8.5000	A	1.421	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.31
L8	8.5000-0.0000	A	1.222	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	0.000	0.000	0.12

Feed Line Center of Pressure

Section	Elevation ft	CP _X in	CP _Z in	CP _X Ice in	CP _Z Ice in
L1	120.0000-110.0000	0.0000	0.0000	0.0000	0.0000
L2	110.0000-100.0000	0.0000	0.0000	0.0000	0.0000
L3	100.0000-90.0000	0.0000	0.0000	0.0000	0.0000
L4	90.0000-82.0000	0.0000	0.0000	0.0000	0.0000
L5	82.0000-60.0000	0.0000	0.0000	0.0000	0.0000
L6	60.0000-30.0000	0.0000	0.0000	0.0000	0.0000
L7	30.0000-8.5000	0.0000	0.0000	0.0000	0.0000
L8	8.5000-0.0000	0.0000	0.0000	0.0000	0.0000

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _s No Ice	K _s Ice
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User Defined Loads

Description	Elevation	Offset From Centroid	Azimuth Angle	Weight	F _x	F _z	Wind Force	C _A A _C	
	ft	ft	°	K	K	K	K	ft ²	
Flag	120.0000	0.00	0.00	No Ice	0.02	0.00	0.00	0.48	14.5606
				Ice	0.25	0.00	0.00	0.08	8.8835
				Service	0.02	0.00	0.00	0.11	9.7996

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement	C _A A _A Front	C _A A _A Side	Weight
			ft ft ft	°	ft	ft ²	ft ²	K

APXV18-206517S-C-ACU	A	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.03 0.05 0.09
APXV18-206517S-C-ACU	B	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.03 0.05 0.09
APXV18-206517S-C-ACU	C	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.03 0.05 0.09
KRY 112 144/1	A	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.01 0.02
KRY 112 144/1	B	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.01 0.02
KRY 112 144/1	C	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.01 0.02
ATMAA1412D-1A20	A	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.02 0.03
ATMAA1412D-1A20	B	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.02 0.03
ATMAA1412D-1A20	C	From Leg	0.5000 0.00 2.00	0.00	115.0000	No Ice 1/2" Ice 1" Ice	0.0000 0.0000 0.0000 0.0000	0.01 0.02 0.03

APXV18-206517S-C-ACU	A	From Leg	0.5000 0.00	0.00	105.0000	No Ice 1/2"	0.0000 0.0000	0.03 0.05

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft		C _{AA} Front ft ²	C _{AA} Side ft ²	Weight K
			2.00			Ice	0.0000	0.0000	0.09
APXV18-206517S-C-ACU	B	From Leg	0.5000	0.00	105.0000	1" Ice	0.0000	0.0000	0.03
			0.00			No Ice	0.0000	0.0000	0.05
			2.00			1/2"	0.0000	0.0000	0.09
						Ice	0.0000	0.0000	0.09
APXV18-206517S-C-ACU	C	From Leg	0.5000	0.00	105.0000	1" Ice	0.0000	0.0000	0.03
			0.00			No Ice	0.0000	0.0000	0.05
			2.00			1/2"	0.0000	0.0000	0.09
						Ice	0.0000	0.0000	0.09
KRY 112 144/1	A	From Leg	0.5000	0.00	105.0000	1" Ice	0.0000	0.0000	0.01
			0.00			No Ice	0.0000	0.0000	0.01
			2.00			1/2"	0.0000	0.0000	0.02
						Ice	0.0000	0.0000	0.02
KRY 112 144/1	B	From Leg	0.5000	0.00	105.0000	1" Ice	0.0000	0.0000	0.01
			0.00			No Ice	0.0000	0.0000	0.01
			2.00			1/2"	0.0000	0.0000	0.01
						Ice	0.0000	0.0000	0.02
KRY 112 144/1	C	From Leg	0.5000	0.00	105.0000	1" Ice	0.0000	0.0000	0.01
			0.00			No Ice	0.0000	0.0000	0.01
			2.00			1/2"	0.0000	0.0000	0.01
						Ice	0.0000	0.0000	0.02
***						1" Ice			
DHHTT65B-3XR	A	From Leg	0.5000	0.00	95.0000	No Ice	0.0000	0.0000	0.05
			0.00			1/2"	0.0000	0.0000	0.10
			1.00			Ice	0.0000	0.0000	0.16
DHHTT65B-3XR	B	From Leg	0.5000	0.00	95.0000	1" Ice	0.0000	0.0000	0.05
			0.00			No Ice	0.0000	0.0000	0.10
			1.00			1/2"	0.0000	0.0000	0.16
						Ice	0.0000	0.0000	0.16
DHHTT65B-3XR	C	From Leg	0.5000	0.00	95.0000	1" Ice	0.0000	0.0000	0.05
			0.00			No Ice	0.0000	0.0000	0.10
			1.00			1/2"	0.0000	0.0000	0.16
						Ice	0.0000	0.0000	0.16
FWHR	A	From Leg	0.5000	0.00	95.0000	1" Ice	0.0000	0.0000	0.03
			0.00			No Ice	0.0000	0.0000	0.04
			-3.00			1/2"	0.0000	0.0000	0.04
						Ice	0.0000	0.0000	0.05
FWHR	B	From Leg	0.5000	0.00	95.0000	1" Ice	0.0000	0.0000	0.03
			0.00			No Ice	0.0000	0.0000	0.04
			-3.00			1/2"	0.0000	0.0000	0.04
						Ice	0.0000	0.0000	0.05
FWHR	C	From Leg	0.5000	0.00	95.0000	1" Ice	0.0000	0.0000	0.03
			0.00			No Ice	0.0000	0.0000	0.04
			-3.00			1/2"	0.0000	0.0000	0.04
						Ice	0.0000	0.0000	0.05
BEN-92P	C	From Leg	4.0000	0.00	95.0000	1" Ice	0.0000	0.0000	0.00
			0.00			No Ice	0.0000	0.0000	0.01
			-4.00			1/2"	0.0000	0.0000	0.01
						Ice	0.0000	0.0000	0.02
***						1" Ice			
Canister Load1	C	None		0.00	120.0000	No Ice	9.0000	9.0000	0.09
						1/2"	18.5000	18.5000	0.21
						Ice	19.0000	19.0000	0.32
Canister Load2	C	None		0.00	110.0000	1" Ice	18.0000	18.0000	0.40
						No Ice	37.0000	37.0000	0.63
						1/2"	38.0000	38.0000	0.86
						Ice	38.0000	38.0000	0.86
Canister Load3	C	None		0.00	100.0000	1" Ice	18.0000	18.0000	0.40
						No Ice	37.0000	37.0000	0.63
						1/2"	38.0000	38.0000	0.86
						Ice	38.0000	38.0000	0.86
Canister Load4	C	None		0.00	90.0000	1" Ice	16.2000	16.2000	0.39
						No Ice	16.2000	16.2000	0.39

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment t °	Placement ft	C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K	
Canister Load5	C	None		0.00	82.0000	1/2" Ice	33.3000	33.3000	0.59
						1" Ice	34.2000	34.2000	0.79
						No Ice	7.2000	7.2000	0.29
						1/2" Ice	14.8000	14.8000	0.38
						1" Ice	15.2000	15.2000	0.47
Truck Ball	C	None		0.00	120.7500	No Ice	0.8836	0.8836	0.05
						1/2" Ice	1.3783	1.3783	0.07
						1" Ice	1.5272	1.5272	0.09
						1" Ice			

Tower Pressures - No Ice

$G_H = 1.100$

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L1 120.0000-110.0000	115.0000	1.303	29.826	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000	0.00	0.000	0.000	
					C	0.000	0.000	0.00	0.000	0.000	
L2 110.0000-100.0000	105.0000	1.279	29.260	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000	0.00	0.000	0.000	
					C	0.000	0.000	0.00	0.000	0.000	
L3 100.0000-90.0000	95.0000	1.252	28.650	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000	0.00	0.000	0.000	
					C	0.000	0.000	0.00	0.000	0.000	
L4 90.0000-82.0000	86.0000	1.226	28.056	7.167	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000	0.00	0.000	0.000	
					C	0.000	0.000	0.00	0.000	0.000	
L5 82.0000-60.0000	71.0000	1.178	26.946	44.000	A	0.000	44.000	44.000	100.00	0.000	0.000
					B	0.000	44.000	100.00	0.000	0.000	
					C	0.000	44.000	100.00	0.000	0.000	
L6 60.0000-30.0000	45.0000	1.07	24.479	60.000	A	0.000	60.000	60.000	100.00	0.000	0.000
					B	0.000	60.000	100.00	0.000	0.000	
					C	0.000	60.000	100.00	0.000	0.000	
L7 30.0000-8.5000	19.2500	0.895	20.472	43.000	A	0.000	43.000	43.000	100.00	0.000	0.000
					B	0.000	43.000	100.00	0.000	0.000	
					C	0.000	43.000	100.00	0.000	0.000	
L8 8.5000-0.0000	4.2500	0.85	19.450	17.000	A	0.000	17.000	17.000	100.00	0.000	0.000
					B	0.000	17.000	100.00	0.000	0.000	
					C	0.000	17.000	100.00	0.000	0.000	

Tower Pressure - With Ice

$G_H = 1.100$

Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L1 120.0000-110.0000	115.0000	1.303	7.925	1.6995	11.791	A	0.000	0.000	0.000	0.00	0.000	0.000
						B	0.000	0.000	0.00	0.000	0.000	
						C	0.000	0.000	0.00	0.000	0.000	
L2 110.0000-100.0000	105.0000	1.279	7.774	1.6841	11.765	A	0.000	0.000	0.000	0.00	0.000	0.000
						B	0.000	0.000	0.00	0.000	0.000	
						C	0.000	0.000	0.00	0.000	0.000	
L3 100.0000-90.0000	95.0000	1.252	7.612	1.6673	11.737	A	0.000	0.000	0.000	0.00	0.000	0.000
						B	0.000	0.000	0.00	0.000	0.000	
						C	0.000	0.000	0.00	0.000	0.000	

Section Elevation ft	z ft	K _Z	q _z psf	t _z in	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L4 90.0000-82.0000	86.0000	1.226	7.454	1.6508	9.368	C	0.000	0.000	0.000	0.00	0.000	0.000
						A	0.000	0.000				
						B	0.000	0.000				
L5 82.0000-60.0000	71.0000	1.178	7.160	1.6194	49.938	C	0.000	0.000	49.938	100.00	0.000	0.000
						A	0.000	49.938				
						B	0.000	49.938				
L6 60.0000-30.0000	45.0000	1.07	6.504	1.5473	67.736	C	0.000	0.000	67.736	100.00	0.000	0.000
						A	0.000	67.736				
						B	0.000	67.736				
L7 30.0000-8.5000	19.2500	0.895	5.440	1.4213	48.093	C	0.000	0.000	48.093	100.00	0.000	0.000
						A	0.000	48.093				
						B	0.000	48.093				
L8 8.5000-0.0000	4.2500	0.85	5.168	1.2220	18.731	C	0.000	0.000	18.731	100.00	0.000	0.000
						A	0.000	18.731				
						B	0.000	18.731				

Tower Pressure - Service

$G_H = 1.100$

Section Elevation ft	z ft	K _Z	q _z psf	A _G ft ²	F a c e	A _F ft ²	A _R ft ²	A _{leg} ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L1 120.0000-110.0000	115.0000	1.303	10.210	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000				
					C	0.000	0.000				
L2 110.0000-100.0000	105.0000	1.279	10.017	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000				
					C	0.000	0.000				
L3 100.0000-90.0000	95.0000	1.252	9.808	8.958	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000				
					C	0.000	0.000				
L4 90.0000-82.0000	86.0000	1.226	9.604	7.167	A	0.000	0.000	0.000	0.00	0.000	0.000
					B	0.000	0.000				
					C	0.000	0.000				
L5 82.0000-60.0000	71.0000	1.178	9.225	44.000	A	0.000	44.000	44.000	100.00	0.000	0.000
					B	0.000	44.000				
					C	0.000	44.000				
L6 60.0000-30.0000	45.0000	1.07	8.380	60.000	A	0.000	60.000	60.000	100.00	0.000	0.000
					B	0.000	60.000				
					C	0.000	60.000				
L7 30.0000-8.5000	19.2500	0.895	7.008	43.000	A	0.000	43.000	43.000	100.00	0.000	0.000
					B	0.000	43.000				
					C	0.000	43.000				
L8 8.5000-0.0000	4.2500	0.85	6.659	17.000	A	0.000	17.000	17.000	100.00	0.000	0.000
					B	0.000	17.000				
					C	0.000	17.000				

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice

Comb. No.	Description
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	120 - 110	Pole	Max Tension	20	0.00	-0.00	0.00
			Max. Compression	26	-2.33	0.00	-0.00
			Max. Mx	20	-0.71	13.54	-0.00
			Max. My	14	-0.71	0.00	-13.54
			Max. Vy	20	-1.39	13.54	-0.00
			Max. Vx	14	1.39	0.00	-13.54
			Max. Torque	32			0.00
L2	110 - 100	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-4.94	0.00	-0.00
			Max. Mx	20	-1.79	37.69	-0.00
			Max. My	14	-1.79	0.00	-37.69
			Max. Vy	20	-2.45	37.69	-0.00
			Max. Vx	14	2.45	0.00	-37.69
			Max. Torque	32			0.00
L3	100 - 90	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-8.08	0.12	-0.07
			Max. Mx	20	-3.13	72.12	-0.01
			Max. My	14	-3.13	0.01	-72.11
			Max. Vy	20	-3.47	65.20	-0.01
			Max. Vx	14	3.47	0.01	-65.19
			Max. Torque	38			0.00
L4	90 - 82	Pole	Max Tension	1	0.00	0.00	0.00

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L5	82 - 60	Pole	Max. Compression	26	-9.94	0.12	-0.07
			Max. Mx	20	-4.12	106.45	-0.01
			Max. My	14	-4.12	0.01	-106.44
			Max. Vy	20	-4.31	76.43	-0.01
			Max. Vx	14	4.31	0.01	-76.42
			Max. Torque	38			0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-14.60	0.12	-0.07
			Max. Mx	20	-7.29	223.99	-0.01
			Max. My	14	-7.29	0.01	-223.99
L6	60 - 30	Pole	Max. Vy	20	-6.03	223.99	-0.01
			Max. Vx	14	6.03	0.01	-223.99
			Max. Torque	38			0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-19.98	0.12	-0.07
			Max. Mx	20	-11.30	428.55	-0.01
			Max. My	14	-11.30	0.01	-428.55
			Max. Vy	20	-7.56	428.55	-0.01
			Max. Vx	14	7.56	0.01	-428.55
			Max. Torque	38			0.00
L7	30 - 8.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-23.75	0.12	-0.07
			Max. Mx	20	-14.32	598.24	-0.01
			Max. My	14	-14.32	0.01	-598.24
			Max. Vy	20	-8.20	598.24	-0.01
			Max. Vx	14	8.20	0.01	-598.24
			Max. Torque	38			0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-25.50	0.12	-0.07
			Max. Mx	20	-15.84	668.72	-0.01
L8	8.5 - 0	Pole	Max. My	14	-15.84	0.01	-668.71
			Max. Vy	20	-8.40	668.72	-0.01
			Max. Vx	14	8.40	0.01	-668.71
			Max. Torque	38			0.00
			Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-25.50	0.12	-0.07
			Max. Mx	20	-15.84	668.72	-0.01
			Max. My	14	-15.84	0.01	-668.71
			Max. Vy	20	-8.40	668.72	-0.01
			Max. Vx	14	8.40	0.01	-668.71

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Pole	Max. Vert	26	25.50	0.00	-0.00
	Max. H _x	21	11.88	8.39	0.00
	Max. H _z	3	11.88	-0.00	8.39
	Max. M _x	2	668.70	-0.00	8.39
	Max. M _z	8	668.69	-8.39	0.00
	Max. Torsion	38	0.00	1.44	2.50
	Min. Vert	21	11.88	8.39	0.00
	Min. H _x	9	11.88	-8.39	0.00
	Min. H _z	15	11.88	-0.00	-8.39
	Min. M _x	14	-668.71	-0.00	-8.39
	Min. M _z	20	-668.72	8.39	0.00
	Min. Torsion	32	-0.00	-1.44	-2.50

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overtuning Moment, M _x kip-ft	Overtuning Moment, M _z kip-ft	Torque kip-ft
Dead Only	13.20	0.00	0.00	0.00	0.01	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	15.84	0.00	-8.39	-668.70	0.01	-0.00
0.9 Dead+1.6 Wind 0 deg - No Ice	11.88	0.00	-8.39	-658.10	0.01	-0.00
1.2 Dead+1.6 Wind 30 deg -	15.84	4.19	-7.27	-579.39	-334.50	-0.00

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M _z kip-ft	Torque kip-ft
No Ice						
0.9 Dead+1.6 Wind 30 deg - No Ice	11.88	4.19	-7.27	-570.18	-329.19	-0.00
1.2 Dead+1.6 Wind 60 deg - No Ice	15.84	7.27	-4.19	-334.51	-579.38	-0.00
0.9 Dead+1.6 Wind 60 deg - No Ice	11.88	7.27	-4.19	-329.19	-570.18	-0.00
1.2 Dead+1.6 Wind 90 deg - No Ice	15.84	8.39	-0.00	0.01	-668.69	0.00
0.9 Dead+1.6 Wind 90 deg - No Ice	11.88	8.39	-0.00	0.00	-658.10	0.00
1.2 Dead+1.6 Wind 120 deg - No Ice	15.84	7.27	4.19	334.52	-579.38	0.00
0.9 Dead+1.6 Wind 120 deg - No Ice	11.88	7.27	4.19	329.20	-570.18	0.00
1.2 Dead+1.6 Wind 150 deg - No Ice	15.84	4.19	7.27	579.40	-334.50	0.00
0.9 Dead+1.6 Wind 150 deg - No Ice	11.88	4.19	7.27	570.19	-329.19	0.00
1.2 Dead+1.6 Wind 180 deg - No Ice	15.84	0.00	8.39	668.71	0.01	0.00
0.9 Dead+1.6 Wind 180 deg - No Ice	11.88	0.00	8.39	658.11	0.01	0.00
1.2 Dead+1.6 Wind 210 deg - No Ice	15.84	-4.19	7.27	579.40	334.52	0.00
0.9 Dead+1.6 Wind 210 deg - No Ice	11.88	-4.19	7.27	570.19	329.20	0.00
1.2 Dead+1.6 Wind 240 deg - No Ice	15.84	-7.27	4.19	334.52	579.40	-0.00
0.9 Dead+1.6 Wind 240 deg - No Ice	11.88	-7.27	4.19	329.20	570.19	-0.00
1.2 Dead+1.6 Wind 270 deg - No Ice	15.84	-8.39	-0.00	0.01	668.72	-0.00
0.9 Dead+1.6 Wind 270 deg - No Ice	11.88	-8.39	-0.00	0.00	658.11	-0.00
1.2 Dead+1.6 Wind 300 deg - No Ice	15.84	-7.27	-4.19	-334.51	579.40	-0.00
0.9 Dead+1.6 Wind 300 deg - No Ice	11.88	-7.27	-4.19	-329.19	570.19	-0.00
1.2 Dead+1.6 Wind 330 deg - No Ice	15.84	-4.19	-7.27	-579.39	334.52	-0.00
0.9 Dead+1.6 Wind 330 deg - No Ice	11.88	-4.19	-7.27	-570.18	329.20	-0.00
1.2 Dead+1.0 Ice+1.0 Temp	25.50	-0.00	0.00	0.07	0.12	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	25.50	0.00	-2.89	-233.80	0.15	-0.00
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp	25.50	1.44	-2.50	-202.47	-116.79	-0.00
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp	25.50	2.50	-1.44	-116.86	-202.40	-0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	25.50	2.89	-0.00	0.09	-233.74	0.00
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp	25.50	2.50	1.44	117.03	-202.40	0.00
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp	25.50	1.44	2.50	202.64	-116.79	0.00
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	25.50	0.00	2.89	233.98	0.15	0.00
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp	25.50	-1.44	2.50	202.64	117.10	0.00
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp	25.50	-2.50	1.44	117.03	202.71	-0.00
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp	25.50	-2.89	-0.00	0.09	234.04	-0.00
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	25.50	-2.50	-1.44	-116.86	202.71	-0.00
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp	25.50	-1.44	-2.50	-202.47	117.10	-0.00
Dead+Wind 0 deg - Service	13.20	0.00	-1.74	-134.91	0.01	-0.00

Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	K	K	kip-ft	kip-ft	kip-ft
Dead+Wind 30 deg - Service	13.20	0.87	-1.51	-116.84	-67.45	-0.00
Dead+Wind 60 deg - Service	13.20	1.51	-0.87	-67.45	-116.83	-0.00
Dead+Wind 90 deg - Service	13.20	1.74	-0.00	0.01	-134.91	0.00
Dead+Wind 120 deg - Service	13.20	1.51	0.87	67.47	-116.83	0.00
Dead+Wind 150 deg - Service	13.20	0.87	1.51	116.85	-67.45	0.00
Dead+Wind 180 deg - Service	13.20	0.00	1.74	134.92	0.01	0.00
Dead+Wind 210 deg - Service	13.20	-0.87	1.51	116.85	67.47	0.00
Dead+Wind 240 deg - Service	13.20	-1.51	0.87	67.47	116.85	-0.00
Dead+Wind 270 deg - Service	13.20	-1.74	-0.00	0.01	134.93	-0.00
Dead+Wind 300 deg - Service	13.20	-1.51	-0.87	-67.45	116.85	-0.00
Dead+Wind 330 deg - Service	13.20	-0.87	-1.51	-116.84	67.47	-0.00

Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.00	-13.20	0.00	0.00	13.20	0.00	0.000%
2	0.00	-15.84	-8.39	-0.00	15.84	8.39	0.019%
3	0.00	-11.88	-8.39	-0.00	11.88	8.39	0.022%
4	4.19	-15.84	-7.27	-4.19	15.84	7.27	0.001%
5	4.19	-11.88	-7.27	-4.19	11.88	7.27	0.001%
6	7.27	-15.84	-4.19	-7.27	15.84	4.19	0.001%
7	7.27	-11.88	-4.19	-7.27	11.88	4.19	0.001%
8	8.39	-15.84	0.00	-8.39	15.84	0.00	0.019%
9	8.39	-11.88	0.00	-8.39	11.88	0.00	0.022%
10	7.27	-15.84	4.19	-7.27	15.84	-4.19	0.001%
11	7.27	-11.88	4.19	-7.27	11.88	-4.19	0.001%
12	4.19	-15.84	7.27	-4.19	15.84	-7.27	0.001%
13	4.19	-11.88	7.27	-4.19	11.88	-7.27	0.001%
14	0.00	-15.84	8.39	-0.00	15.84	-8.39	0.019%
15	0.00	-11.88	8.39	-0.00	11.88	-8.39	0.022%
16	-4.19	-15.84	7.27	4.19	15.84	-7.27	0.001%
17	-4.19	-11.88	7.27	4.19	11.88	-7.27	0.001%
18	-7.27	-15.84	4.19	7.27	15.84	-4.19	0.001%
19	-7.27	-11.88	4.19	7.27	11.88	-4.19	0.001%
20	-8.39	-15.84	0.00	8.39	15.84	0.00	0.019%
21	-8.39	-11.88	0.00	8.39	11.88	0.00	0.022%
22	-7.27	-15.84	-4.19	7.27	15.84	4.19	0.001%
23	-7.27	-11.88	-4.19	7.27	11.88	4.19	0.001%
24	-4.19	-15.84	-7.27	4.19	15.84	7.27	0.001%
25	-4.19	-11.88	-7.27	4.19	11.88	7.27	0.001%
26	0.00	-25.50	0.00	0.00	25.50	-0.00	0.000%
27	0.00	-25.50	-2.89	-0.00	25.50	2.89	0.004%
28	1.44	-25.50	-2.50	-1.44	25.50	2.50	0.004%
29	2.50	-25.50	-1.44	-2.50	25.50	1.44	0.004%
30	2.89	-25.50	0.00	-2.89	25.50	0.00	0.004%
31	2.50	-25.50	1.44	-2.50	25.50	-1.44	0.004%
32	1.44	-25.50	2.50	-1.44	25.50	-2.50	0.004%
33	0.00	-25.50	2.89	-0.00	25.50	-2.89	0.004%
34	-1.44	-25.50	2.50	1.44	25.50	-2.50	0.004%
35	-2.50	-25.50	1.44	2.50	25.50	-1.44	0.004%
36	-2.89	-25.50	0.00	2.89	25.50	0.00	0.004%
37	-2.50	-25.50	-1.44	2.50	25.50	1.44	0.004%
38	-1.44	-25.50	-2.50	1.44	25.50	2.50	0.004%
39	0.00	-13.20	-1.74	-0.00	13.20	1.74	0.004%
40	0.87	-13.20	-1.51	-0.87	13.20	1.51	0.004%
41	1.51	-13.20	-0.87	-1.51	13.20	0.87	0.004%
42	1.74	-13.20	0.00	-1.74	13.20	0.00	0.004%

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
43	1.51	-13.20	0.87	-1.51	13.20	-0.87	0.004%
44	0.87	-13.20	1.51	-0.87	13.20	-1.51	0.004%
45	0.00	-13.20	1.74	-0.00	13.20	-1.74	0.004%
46	-0.87	-13.20	1.51	0.87	13.20	-1.51	0.004%
47	-1.51	-13.20	0.87	1.51	13.20	-0.87	0.004%
48	-1.74	-13.20	0.00	1.74	13.20	0.00	0.004%
49	-1.51	-13.20	-0.87	1.51	13.20	0.87	0.004%
50	-0.87	-13.20	-1.51	0.87	13.20	1.51	0.004%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	6	0.00000001	0.00000001
2	Yes	26	0.00013715	0.00009074
3	Yes	25	0.00012571	0.00010109
4	Yes	35	0.00000001	0.00011798
5	Yes	34	0.00000001	0.00011991
6	Yes	35	0.00000001	0.00011798
7	Yes	34	0.00000001	0.00011991
8	Yes	26	0.00013715	0.00009074
9	Yes	25	0.00012571	0.00010109
10	Yes	35	0.00000001	0.00011800
11	Yes	34	0.00000001	0.00011993
12	Yes	35	0.00000001	0.00011798
13	Yes	34	0.00000001	0.00011991
14	Yes	26	0.00013715	0.00009075
15	Yes	25	0.00012571	0.00010109
16	Yes	35	0.00000001	0.00011802
17	Yes	34	0.00000001	0.00011994
18	Yes	35	0.00000001	0.00011801
19	Yes	34	0.00000001	0.00011993
20	Yes	26	0.00013715	0.00009075
21	Yes	25	0.00012571	0.00010109
22	Yes	35	0.00000001	0.00011799
23	Yes	34	0.00000001	0.00011992
24	Yes	35	0.00000001	0.00011801
25	Yes	34	0.00000001	0.00011993
26	Yes	6	0.00000001	0.00000001
27	Yes	31	0.00011749	0.00003419
28	Yes	31	0.00011727	0.00006478
29	Yes	31	0.00011727	0.00006482
30	Yes	31	0.00011748	0.00003417
31	Yes	31	0.00011727	0.00006502
32	Yes	31	0.00011728	0.00006490
33	Yes	31	0.00011750	0.00003425
34	Yes	31	0.00011729	0.00006525
35	Yes	31	0.00011730	0.00006521
36	Yes	31	0.00011751	0.00003427
37	Yes	31	0.00011729	0.00006501
38	Yes	31	0.00011728	0.00006513
39	Yes	26	0.00011282	0.00002103
40	Yes	26	0.00011273	0.00001804
41	Yes	26	0.00011273	0.00001804
42	Yes	26	0.00011282	0.00002103
43	Yes	26	0.00011273	0.00001804
44	Yes	26	0.00011273	0.00001804
45	Yes	26	0.00011282	0.00002103
46	Yes	26	0.00011273	0.00001805
47	Yes	26	0.00011273	0.00001805
48	Yes	26	0.00011282	0.00002103
49	Yes	26	0.00011273	0.00001804
50	Yes	26	0.00011273	0.00001805

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	120 - 110	18.51	48	1.37	0.00
L2	110 - 100	15.65	48	1.35	0.00
L3	100 - 90	12.89	48	1.27	0.00
L4	90 - 82	10.41	48	1.08	0.00
L5	82 - 60	8.80	48	0.83	0.00
L6	60 - 30	5.19	47	0.73	0.00
L7	30 - 8.5	1.42	47	0.44	0.00
L8	8.5 - 0	0.11	47	0.12	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
120.7500	Truck Ball	48	18.51	1.37	0.00	24383
120.0000	Canister Load1	48	18.51	1.37	0.00	24383
115.0000	APXV18-206517S-C-ACU	48	17.07	1.37	0.00	24383
110.0000	Canister Load2	48	15.65	1.35	0.00	11844
105.0000	APXV18-206517S-C-ACU	48	14.25	1.32	0.00	7273
100.0000	Canister Load3	48	12.89	1.27	0.00	4695
95.0000	DHHTT65B-3XR	48	11.59	1.19	0.00	2713
90.0000	Canister Load4	48	10.41	1.08	0.00	2081
82.0000	Canister Load5	48	8.80	0.83	0.00	4148

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	120 - 110	93.53	20	7.08	0.00
L2	110 - 100	78.83	20	6.96	0.00
L3	100 - 90	64.72	20	6.49	0.00
L4	90 - 82	52.11	20	5.47	0.00
L5	82 - 60	43.98	20	4.16	0.00
L6	60 - 30	25.91	18	3.63	0.00
L7	30 - 8.5	7.08	18	2.22	0.00
L8	8.5 - 0	0.54	18	0.60	0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
120.7500	Truck Ball	20	93.53	7.08	0.00	4382
120.0000	Canister Load1	20	93.53	7.08	0.00	4382
115.0000	APXV18-206517S-C-ACU	20	86.15	7.05	0.00	4382
110.0000	Canister Load2	20	78.83	6.96	0.00	2144
105.0000	APXV18-206517S-C-ACU	20	71.66	6.77	0.00	1343
100.0000	Canister Load3	20	64.72	6.49	0.00	882
95.0000	DHHTT65B-3XR	20	58.12	6.09	0.00	519
90.0000	Canister Load4	20	52.11	5.47	0.00	401
82.0000	Canister Load5	20	43.98	4.16	0.00	803

Compression Checks

Pole Design Data

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in^2	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
L1	120 - 110 (1)	P10.75x0.349	10.000	0.0000	0.0	11.403	-0.71	431.06	0.002
L2	110 - 100 (2)	P10.75x0.349	10.000	0.0000	0.0	11.403	-1.79	431.06	0.004
L3	100 - 90 (3)	P10.75x0.349	10.000	0.0000	0.0	11.403	-3.13	431.06	0.007
L4	90 - 82 (4)	P10.75x0.349	8.0000	0.0000	0.0	11.403	-4.12	431.06	0.010
L5	82 - 60 (5)	P24x0.375	22.000	0.0000	0.0	27.832	-7.29	1052.07	0.007
L6	60 - 30 (6)	P24x0.375	30.000	0.0000	0.0	27.832	-11.30	1052.07	0.011
L7	30 - 8.5 (7)	P24x0.375	21.500	0.0000	0.0	27.832	-14.32	1052.07	0.014
L8	8.5 - 0 (8)	P24x0.5	8.5000	0.0000	0.0	36.913	-15.84	1313.94	0.012

Pole Bending Design Data

Section No.	Elevation ft	Size	M_{ux} kip-ft	ϕM_{nx} kip-ft	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	M_{uy} kip-ft	ϕM_{ny} kip-ft	Ratio $\frac{M_{uy}}{\phi M_{ny}}$
L1	120 - 110 (1)	P10.75x0.349	13.54	118.97	0.114	0.00	118.97	0.000
L2	110 - 100 (2)	P10.75x0.349	37.70	118.97	0.317	0.00	118.97	0.000
L3	100 - 90 (3)	P10.75x0.349	72.16	118.97	0.607	0.00	118.97	0.000
L4	90 - 82 (4)	P10.75x0.349	106.51	118.97	0.895	0.00	118.97	0.000
L5	82 - 60 (5)	P24x0.375	224.11	623.72	0.359	0.00	623.72	0.000
L6	60 - 30 (6)	P24x0.375	428.77	623.72	0.687	0.00	623.72	0.000
L7	30 - 8.5 (7)	P24x0.375	598.54	623.72	0.960	0.00	623.72	0.000
L8	8.5 - 0 (8)	P24x0.5	669.04	819.18	0.817	0.00	819.18	0.000

Pole Shear Design Data

Section No.	Elevation ft	Size	Actual V_u K	ϕV_n K	Ratio $\frac{V_u}{\phi V_n}$	Actual T_u kip-ft	ϕT_n kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	120 - 110 (1)	P10.75x0.349	1.39	215.53	0.006	0.00	180.95	0.000
L2	110 - 100 (2)	P10.75x0.349	2.45	215.53	0.011	0.00	180.95	0.000
L3	100 - 90 (3)	P10.75x0.349	3.47	215.53	0.016	0.00	180.95	0.000
L4	90 - 82 (4)	P10.75x0.349	4.27	215.53	0.020	0.00	180.95	0.000
L5	82 - 60 (5)	P24x0.375	6.04	526.03	0.011	0.00	1019.71	0.000
L6	60 - 30 (6)	P24x0.375	7.56	526.03	0.014	0.00	1019.71	0.000
L7	30 - 8.5 (7)	P24x0.375	8.20	526.03	0.016	0.00	1019.71	0.000
L8	8.5 - 0 (8)	P24x0.5	8.40	656.97	0.013	0.00	1260.33	0.000

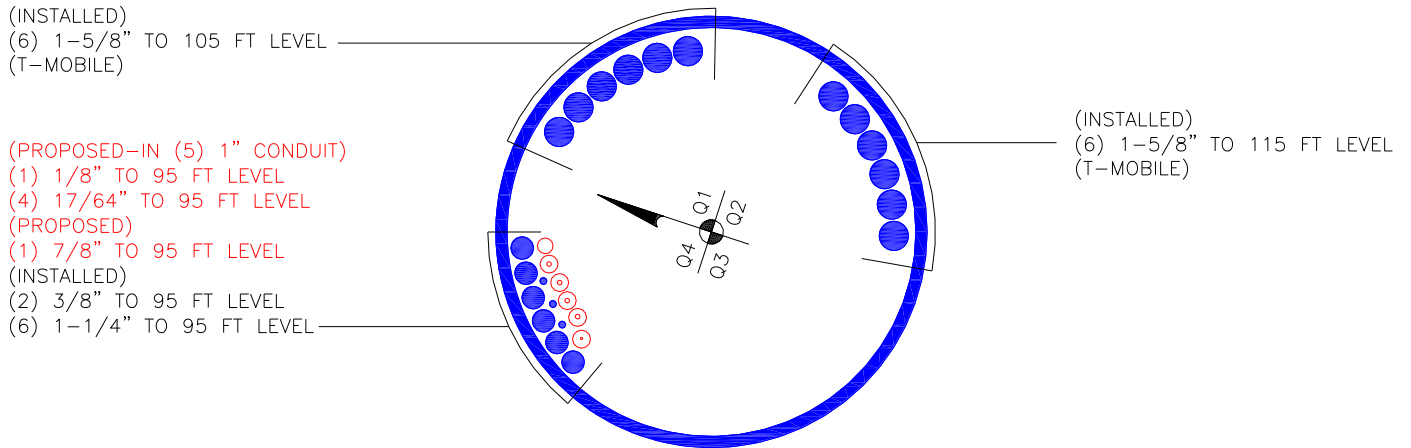
Pole Interaction Design Data

Section No.	Elevation ft	Ratio P_u	Ratio M_{ux}	Ratio M_{uy}	Ratio V_u	Ratio T_u	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
		ϕP_n	ϕM_{rx}	ϕM_{ry}	ϕV_n	ϕT_n			
L1	120 - 110 (1)	0.002	0.114	0.000	0.006	0.000	0.116 ✓	1.000	4.8.2 ✓
L2	110 - 100 (2)	0.004	0.317	0.000	0.011	0.000	0.321 ✓	1.000	4.8.2 ✓
L3	100 - 90 (3)	0.007	0.607	0.000	0.016	0.000	0.614 ✓	1.000	4.8.2 ✓
L4	90 - 82 (4)	0.010	0.895	0.000	0.020	0.000	0.905 ✓	1.000	4.8.2 ✓
L5	82 - 60 (5)	0.007	0.359	0.000	0.011	0.000	0.366 ✓	1.000	4.8.2 ✓
L6	60 - 30 (6)	0.011	0.687	0.000	0.014	0.000	0.698 ✓	1.000	4.8.2 ✓
L7	30 - 8.5 (7)	0.014	0.960	0.000	0.016	0.000	0.973 ✓	1.000	4.8.2 ✓
L8	8.5 - 0 (8)	0.012	0.817	0.000	0.013	0.000	0.829 ✓	1.000	4.8.2 ✓

Section Capacity Table

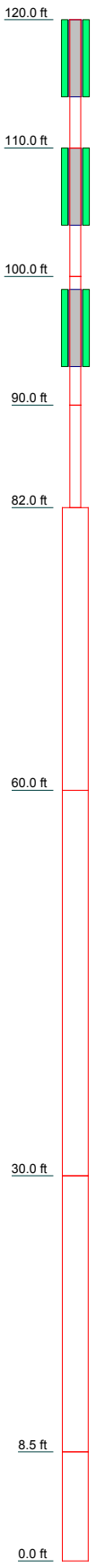
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
L1	120 - 110	Pole	P10.75x0.349	1	-0.71	431.06	11.6	Pass	
L2	110 - 100	Pole	P10.75x0.349	2	-1.79	431.06	32.1	Pass	
L3	100 - 90	Pole	P10.75x0.349	3	-3.13	431.06	61.4	Pass	
L4	90 - 82	Pole	P10.75x0.349	4	-4.12	431.06	90.5	Pass	
L5	82 - 60	Pole	P24x0.375	5	-7.29	1052.07	36.6	Pass	
L6	60 - 30	Pole	P24x0.375	6	-11.30	1052.07	69.8	Pass	
L7	30 - 8.5	Pole	P24x0.375	7	-14.32	1052.07	97.3	Pass	
L8	8.5 - 0	Pole	P24x0.5	8	-15.84	1313.94	82.9	Pass	
							Summary		
							Pole (L7)	97.3	Pass
							RATING =	97.3	Pass

APPENDIX B BASE LEVEL DRAWING



APPENDIX C
ADDITIONAL CALCULATIONS

Section	1								
Size	P10.75x0.349								
Length (ft)	10.0000								
Grade	A500-42								
Weight (K)	0.4								
Section	2								
Size	P10.75x0.349								
Length (ft)	10.0000								
Grade	A500-42								
Weight (K)	0.4								
Section	3								
Size	P10.75x0.349								
Length (ft)	10.0000								
Grade	A500-42								
Weight (K)	0.4								
Section	4								
Size	P10.75x0.349								
Length (ft)	8.0000								
Grade	A500-42								
Weight (K)	0.3								
Section	5								
Size	P24x0.375								
Length (ft)	22.0000								
Grade	A500-42								
Weight (K)	2.1								
Section	6								
Size	P24x0.375								
Length (ft)	30.0000								
Grade	A53-B-42								
Weight (K)	2.8								
Section	7								
Size	P24x0.375								
Length (ft)	21.5000								
Grade	Reinf 39.55 ksi								
Weight (K)	2.0								
Section	8								
Size	P24x0.5								
Length (ft)	8.5000								
Grade	Reinf 39.55 ksi								
Weight (K)	1.1								
Section	9.5								
Size									
Length (ft)									
Grade									
Weight (K)									



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Truck Ball	120.75	APXV18-206517S-C-ACU	105
Canister Load1	120	KRY 112 144/1	105
Flag	120	APXV18-206517S-C-ACU	105
KRY 112 144/1	115	APXV18-206517S-C-ACU	105
KRY 112 144/1	115	Canister Load3	100
KRY 112 144/1	115	FWHR	95
ATMAA1412D-1A20	115	BEN-92P	95
ATMAA1412D-1A20	115	DHHTT65B-3XR	95
ATMAA1412D-1A20	115	DHHTT65B-3XR	95
APXV18-206517S-C-ACU	115	FWHR	95
APXV18-206517S-C-ACU	115	DHHTT65B-3XR	95
APXV18-206517S-C-ACU	115	FWHR	95
Canister Load2	110	Canister Load4	90
KRY 112 144/1	105	Canister Load5	82
KRY 112 144/1	105		

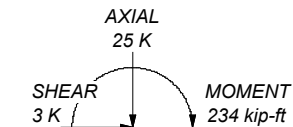
MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A500-42	42 ksi	58 ksi	Reinf 39.55 ksi	40 ksi	50 ksi
A53-B-42	42 ksi	63 ksi			

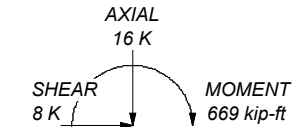
TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 97 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.0000 ft
8. TOWER RATING: 97.3%

ALL REACTIONS ARE FACTORED



TORQUE 0 kip-ft
50 mph WIND - 0.7500 in ICE



TORQUE 0 kip-ft
REACTIONS - 97 mph WIND

<p>Paul J Ford and Company 250 E. Broad Street, Suite 600 Columbus, OH 43215 Phone: 614.221.6679 FAX: 614.448.4105</p>	Job: 120' Monopole / Bridgeport, CT		
	Project: 37516-3608.001.7805 / BU 822779		
	Client: Crown Castle	Drawn by: Seth Tschanen	App'd:
	Code: TIA-222-G	Date: 11/21/16	Scale: NTS
	Path:		Dwg No. E-1

v4.4 - Effective 7-12-13

Asymmetric Anchor Rod Analysis

Moment =	669	k-ft	TIA Ref.	G	Location =	Base Plate
Axial =	16.0	kips	ASIF =	N/A	η =	0.50 for BP, Rev. G Sect. 4.9.9
Shear =	8.0	kips	Max Ratio =	100.0%	Threads =	N/A for FP, Rev. G
Anchor Qty =	24					

**** For Post Installed Anchors: Check anchors for embedment, epoxy/grout bond, and capacity based on proof load. ****

Item	Nominal Anchor Dia, in	Spec	Fy, ksi	Fu, ksi	Location, degrees	Anchor Circle, in	Area Override, in ²	Area, in ²	Max Net Compression, kips	Max Net Tension, kips	Load for Capacity Calc, kips	Capacity Override, kips	Capacity, kips	Capacity Ratio
1	1.000	A687	105	125	0.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
2	1.000	A687	105	125	18.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
3	1.000	A687	105	125	36.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
4	1.000	A687	105	125	54.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
5	1.000	A687	105	125	72.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
6	1.000	A687	105	125	90.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
7	1.000	A687	105	125	108.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
8	1.000	A687	105	125	126.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
9	1.000	A687	105	125	144.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
10	1.000	A687	105	125	162.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
11	1.000	A687	105	125	180.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
12	1.000	A687	105	125	198.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
13	1.000	A687	105	125	216.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
14	1.000	A687	105	125	234.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
15	1.000	A687	105	125	252.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
16	1.000	A687	105	125	270.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
17	1.000	A687	105	125	288.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
18	1.000	A687	105	125	306.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
19	1.000	A687	105	125	324.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
20	1.000	A687	105	125	342.0	27.00	0.00	0.79	10.03	8.91	10.60	0.00	60.60	17.5%
21		Other	0	0	0.0	96.00	1.64	1.64	71.49	69.13	71.49	118.72	118.72	60.2%
22		Other	0	0	90.0	96.00	1.64	1.64	71.49	69.13	71.49	118.72	118.72	60.2%
23		Other	0	0	180.0	96.00	1.64	1.64	71.49	69.13	71.49	118.72	118.72	60.2%
24		Other	0	0	270.0	96.00	1.64	1.64	71.49	69.13	71.49	118.72	118.72	60.2%

22.27

Stiffened or Unstiffened, UngROUTED, Circular Base Plate - Any Rod Material

TIA Rev G

Assumption: Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)*(Rod Diameter)

Site Data

BU#: 822779
Site Name: Bridgeport / Rt 8
App #:
Pole Manufacturer: Other

Anchor Rod Data

Qty:	20	
Diam:	1	in
Rod Material:	Other	
Strength (Fu):	125	ksi
Yield (Fy):	105	ksi
Bolt Circle:	27	in

Plate Data

Diam:	30.375	in
Thick:	1.25	in
Grade:	36	ksi
Single-Rod B-eff:	3.77	in

Stiffener Data (Welding at both sides)

Config:	2	*
Weld Type:	Both	
Groove Depth:	0.25	in **
Groove Angle:	45	degrees
Fillet H. Weld:	0.3125	in
Fillet V. Weld:	0.3125	in
Width:	3	in
Height:	5	in
Thick:	0.625	in
Notch:	0.5	in
Grade:	36	ksi
Weld str.:	70	ksi

Pole Data

Diam:	24	in
Thick:	0.375	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	63	ksi
Reinf. Fillet Weld	0	"0" if None

Reactions

Mu:	106.5	ft-kips
Axial, Pu:	11.3	kips
Shear, Vu:	5.6	kips
Eta Factor, η	0.5	TIA G (Fig. 4-4)

If No stiffeners, Criteria: **AISC LRFD** <-Only Applicable to Unstiffened Cases

Anchor Rod Results

Max Rod (Cu+ Vu/η): 10.6 Kips
 Allowable Axial, Φ*Fu*Anet: 60.6 Kips
 Anchor Rod Stress Ratio: 17.5% **Pass**

Rigid
AISC LRFD
φ*Tn

Base Plate Results

Base Plate Stress: 6.4 ksi
 Allowable Plate Stress: 32.4 ksi
 Base Plate Stress Ratio: 19.9% **Pass**

Flexural Check

Rigid
AISC LRFD
φ*Fy
Y.L. Length:
12.37

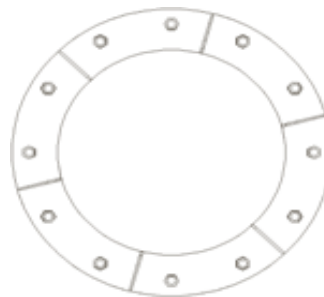
b/Le>2, Stiffeners are not fully effective

Stiffener Results

Horizontal Weld : n/a
 Vertical Weld: n/a
 Plate Flex+Shear, fb/Fb+(fv/Fv)^2: n/a
 Plate Tension+Shear, ft/Ft+(fv/Fv)^2: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Factored Foundation Loads:

	LC1	LC2	
Factored Axial Load (+Comp, -Ten) =	11.3	8.475	kips
Factored Horiz. Load at Top of Pier =	5.6	5.6	kips
Factored OTM at Top of Pier =	106.5	106.5	kips

LRFD Resistance and Load Factors:

	Φ	Dead Load Factors	
Soil Bearing =	0.75		
Soil Weight =	0.75	1.2	0.9
Concrete Weight =	0.75	1.2	0.9

Soil Properties:

Depth to Water Table =	99	ft
Uplift Cone from	Top	of footing

Layer Thk ft	Soil Density pcf	Cohesion ksf	Friction Angle degrees	Ult Bearing ksf	Depth ft
2	100	0	34		2.00
2	100	0	34		4.00
2	125	0	34	30	6.00

Dimensions:

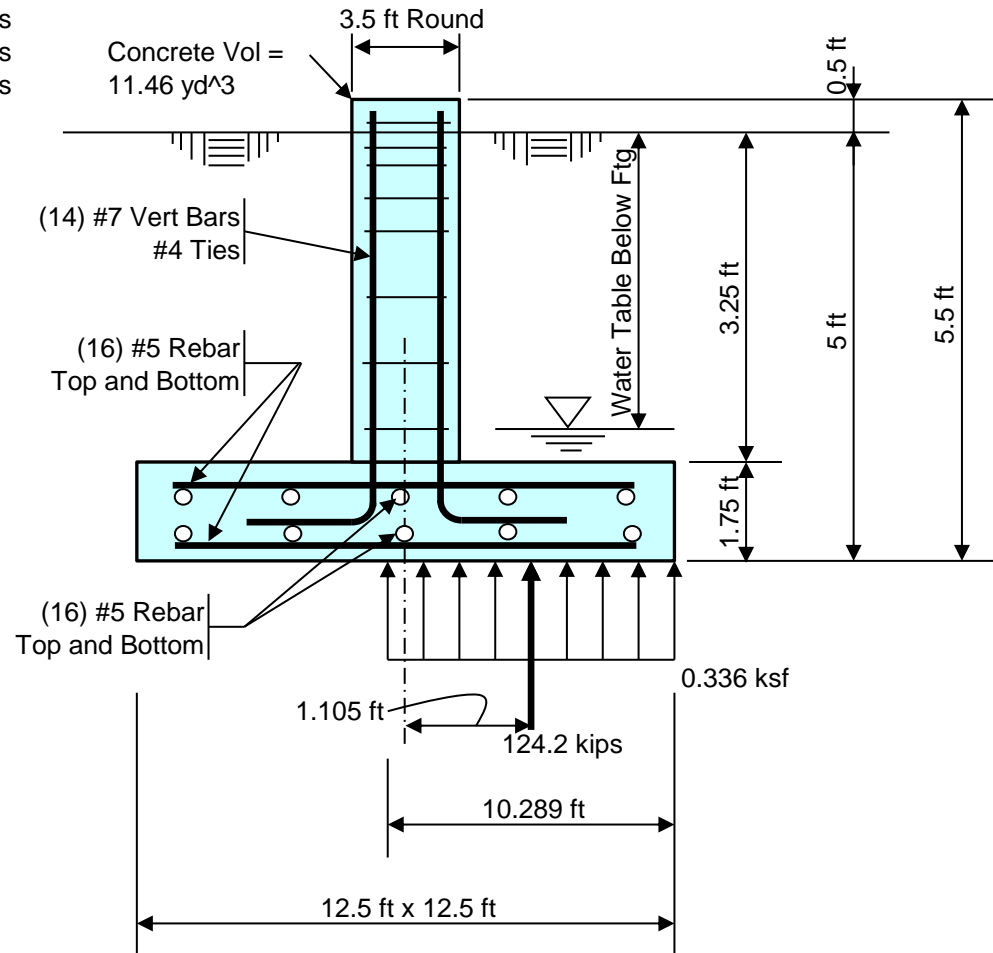
Pier Shape =	Round
Pier Width =	3.5 ft Diameter
Pier Height above Grade =	0.5 ft
Depth to Bottom of Footing =	5 ft
Footing Thickness =	1.75 ft
Footing Width, B =	12.5 ft
Footing Length, L =	12.5 ft

Concrete:

Concrete Strength =	3	ksi
Rebar Strength =	60	ksi

Summary Results:

	Required	Available
Maximum Net Soil Bearing =	0.336 ksf	22.500 ksf
Uplift =	0.0 kips	85.5 kips
Punching Shear Stress =	0.012 ksi	0.164 ksi
Bending Shear Stress =	15.7 kips	210.3 kips
Bending Moment =	51.945 k-ft	372.2 k-ft
Conc Pier Reinforcing Steel =	127.5 k-ft	641.5 k-ft



Total Pad Reinf Stl =	9.92	in ² >= 5.67 in ² = Min Stl, OK
Total Pier Reinf Stl =	8.40	in ² >= 6.93 in ² = Min Stl, OK
Footing Thickness =	1.75	ft >= 1.37 ft = Min Ftg Thk, OK

Stress Ratio =	1.5%	in Soil Bearing
Stress Ratio =	0.0%	in Uplift
Stress Ratio =	7.5%	in Punching Shear
Stress Ratio =	7.5%	in Bending Shear
Stress Ratio =	14.0%	in Bending Moment
Stress Ratio =	19.9%	in Pier Rebar

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	13.54	ft-kips
Axial, Pu:	0.71	kips
Shear, Vu:	1.39	kips
Elevation:	110	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results

Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B :	54.54 kips
Max Bolt directly applied T_u :	5.42 Kips
Min. PL "tc" for B cap. w/o Pry :	1.218 in
Min PL "treq" for actual T w/ Pry :	0.290 in
Min PL "t1" for actual T w/o Pry :	0.384 in
T allowable w/o Prying:	54.54 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = $T_u + q$:	5.42 kips
Non-Prying Bolt Stress Ratio, T_u/B :	9.9% Pass

Rigid
$\phi^* T_n$
$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$

Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results

Flexural Check	
Compression Side Plate Stress:	1.5 ksi
Allowable Plate Stress:	32.4 ksi
Compression Plate Stress Ratio:	4.6% Pass
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$:	2.1% Pass

Rigid
TIA G
$\phi^* F_y$
Comp. Y.L. Length:
10.10

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

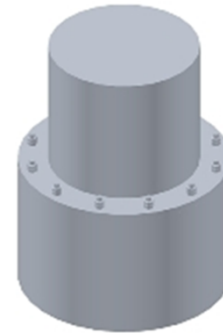
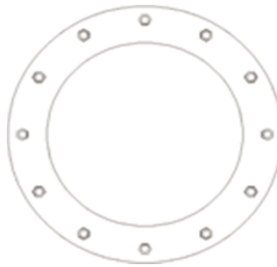
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Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$:	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$:	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check:	n/a
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Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None

* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	13.54	ft-kips
Axial, Pu:	0.71	kips
Shear, Vu:	1.39	kips
Elevation:	110	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results

Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B :	54.54 kips
Max Bolt directly applied T_u :	5.42 Kips
Min. PL "tc" for B cap. w/o Pry :	1.218 in
Min PL "treq" for actual T w/ Pry :	0.290 in
Min PL "t1" for actual T w/o Pry :	0.384 in
T allowable w/o Prying:	54.54 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = $T_u + q$:	5.42 kips
Non-Prying Bolt Stress Ratio, T_u/B :	9.9% Pass

Rigid
$\phi^* T_n$
$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$

Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results

Flexural Check	
Compression Side Plate Stress:	1.5 ksi
Allowable Plate Stress:	32.4 ksi
Compression Plate Stress Ratio:	4.6% Pass
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$:	2.1% Pass

Rigid
TIA G
$\phi^* F_y$
Comp. Y.L. Length:
10.10

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

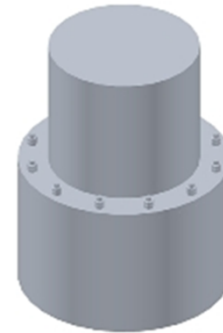
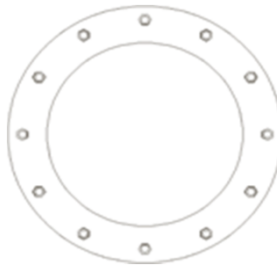
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Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$:	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$:	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check:	n/a
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Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None

* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	37.7	ft-kips
Axial, Pu:	1.79	kips
Shear, Vu:	2.45	kips
Elevation:	100	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results		Rigid
Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips	$\phi^* T_n$
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B :	54.54 kips	$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$
Max Bolt directly applied T_u :	15.11 Kips	
Min. PL "tc" for B cap. w/o Pry:	1.218 in	
Min PL "treq" for actual T w/ Pry:	0.485 in	
Min PL "t1" for actual T w/o Pry:	0.641 in	
T allowable w/o Prying:	54.54 kips	$\alpha' < 0$ case
Prying Force, q:	0.00 kips	
Total Bolt Tension = $T_u + q$:	15.11 kips	
Non-Prying Bolt Stress Ratio, T_u / B :	27.7% Pass	

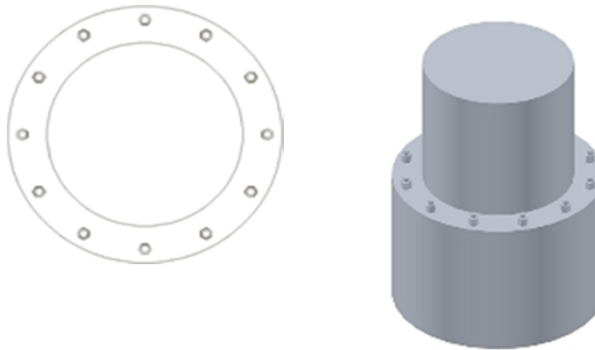
Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results		Flexural Check	Rigid
Compression Side Plate Stress:	4.1 ksi		TIA G
Allowable Plate Stress:	32.4 ksi		$\phi^* F_y$
Compression Plate Stress Ratio:	12.7% Pass		Comp. Y.L. Length: 10.10
No Prying			
Tension Side Stress Ratio, $(treq/t)^2$:	5.9% Pass		

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

Stiffener Results		n/a
Horizontal Weld :	n/a	
Vertical Weld:	n/a	
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$:	n/a	
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$:	n/a	
Plate Comp. (AISC Bracket):	n/a	
Pole Results		
Pole Punching Shear Check:	n/a	

Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	37.7	ft-kips
Axial, Pu:	1.79	kips
Shear, Vu:	2.45	kips
Elevation:	100	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results

Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B:	54.54 kips
Max Bolt directly applied T_u :	15.11 Kips
Min. PL "tc" for B cap. w/o Pry:	1.218 in
Min PL "treq" for actual T w/ Pry:	0.485 in
Min PL "t1" for actual T w/o Pry:	0.641 in
T allowable w/o Prying:	54.54 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = $T_u + q$:	15.11 kips
Non-Prying Bolt Stress Ratio, T_u / B :	27.7% Pass

Rigid
$\phi^* T_n$
$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$

Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results

Flexural Check	
Compression Side Plate Stress:	4.1 ksi
Allowable Plate Stress:	32.4 ksi
Compression Plate Stress Ratio:	12.7% Pass
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$:	5.9% Pass

Rigid
TIA G
$\phi^* F_y$
Comp. Y.L. Length:
10.10

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

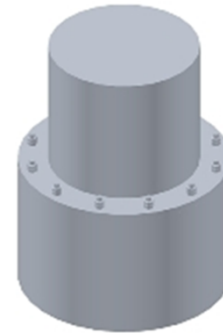
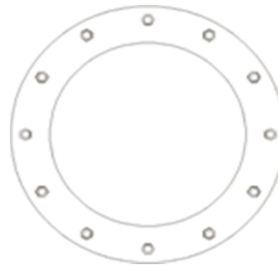
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Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$:	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$:	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check:	n/a
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Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None

* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	72.16	ft-kips
Axial, Pu:	3.13	kips
Shear, Vu:	3.47	kips
Elevation:	90	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results

Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B:	54.54 kips
Max Bolt directly applied T_u :	28.96 Kips
Min. PL "tc" for B cap. w/o Pry:	1.218 in
Min PL "treq" for actual T w/ Pry:	0.671 in
Min PL "t1" for actual T w/o Pry:	0.888 in
T allowable w/o Prying:	54.54 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = $T_u + q$:	28.96 kips
Non-Prying Bolt Stress Ratio, T_u/B :	53.1% Pass

Rigid
$\phi^* T_n$
$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$

Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results

Flexural Check	
Compression Side Plate Stress:	7.8 ksi
Allowable Plate Stress:	32.4 ksi
Compression Plate Stress Ratio:	24.2% Pass
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$:	11.3% Pass

Rigid
TIA G
$\phi^* F_y$
Comp. Y.L. Length:
10.10

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

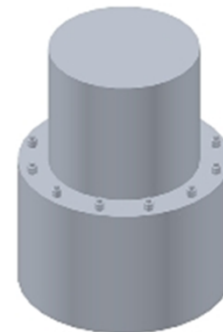
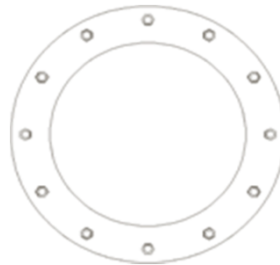
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Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b/F_b + (f_v/F_v)^2$:	n/a
Plate Tension+Shear, $f_t/F_t + (f_v/F_v)^2$:	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check:	n/a
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Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None

* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
Site Name: Bridgeport
App #:

Reactions		
Mu	72.16	ft-kips
Axial, Pu:	3.13	kips
Shear, Vu:	3.47	kips
Elevation:	90	feet

Bolt Threads:
X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Pole Manufacturer:	Other
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If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Bolt Data		
Qty:	8	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	0	<-- Disregard
N/A:	0	<-- Disregard
Circle (in.):	14.75	

Flange Bolt Results

Bolt Tension Capacity, $\phi^* T_n, B1$:	54.54 kips
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$), B :	54.54 kips
Max Bolt directly applied T_u :	28.96 Kips
Min. PL "tc" for B cap. w/o Pry :	1.218 in
Min PL "treq" for actual T w/ Pry :	0.671 in
Min PL "t1" for actual T w/o Pry :	0.888 in
T allowable w/o Prying:	54.54 kips $\alpha' < 0$ case
Prying Force, q:	0.00 kips
Total Bolt Tension = $T_u + q$:	28.96 kips
Non-Prying Bolt Stress Ratio, T_u / B :	53.1% Pass

Rigid
$\phi^* T_n$
$\phi T_n [1 - (V_u / \phi V_n)^2]^{0.5}$

Plate Data		
Diam:	17.75	in
Thick, t:	2	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	4.22	in

Exterior Flange Plate Results

Flexural Check	
Compression Side Plate Stress:	7.8 ksi
Allowable Plate Stress:	32.4 ksi
Compression Plate Stress Ratio:	24.2% Pass
No Prying	
Tension Side Stress Ratio, $(treq/t)^2$:	11.3% Pass

Rigid
TIA G
$\phi^* F_y$
Comp. Y.L. Length:
10.10

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

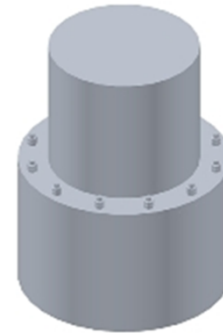
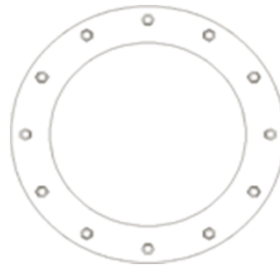
n/a

Stiffener Results

Horizontal Weld :	n/a
Vertical Weld:	n/a
Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$:	n/a
Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$:	n/a
Plate Comp. (AISC Bracket):	n/a

Pole Results

Pole Punching Shear Check:	n/a
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Pole Data		
Diam:	10.75	in
Thick:	0.349	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi
Reinf. Fillet Weld	0	"0" if None

* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

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CODE: **TIA-222-G**
 ASIF: 1.00

EEI FLANGE CONCEALMENT CALCULATIONS (82 Ft)

EEI Kit Number	Custom
Flange Elevation	82.00 ft

STIFFENER INFORMATION

Overrides

Stiffener Quantity	4	4
Width (in)	6.75	6.75
Height (in)	13.5	13.50
Thickness (in)	0.75	0.75
Horizontal Fillet Weld	0.375	0.375
Vertical Fillet Weld	0.375	0.375
Stiffener Grade (ksi)	36	36

RING PLATE INFORMATION

Thickness (in)	2.5	2.50
ID (in)	18	18.00
OD (in)	25	25.00
Ring Plate Grade (ksi)	36	36

BOLT INFORMATION

Bolt Quantity	8	8
Size (in)	1	1.00
Bolt Circle (in)	21	21.0
Bolt Specification	A325	A325

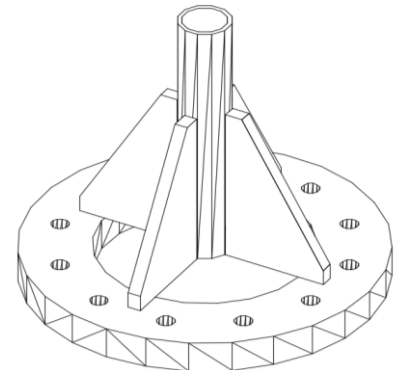
SPINE INFORMATION

Size	HSS10.75	HSS10.75
Pipe Grade	A500-42	A500-42
Fy (ksi)	42	42
Fu (ksi)	60	60
Pipe OD (in)	10.75	10.75
Pipe Thickness (in)	0.349	0.349

FLANGE CONNECTION REACTIONS

Moment	106.51	kip*ft
Shear	4.27	kips
Axial	4.12	kips

Max Allowable Capacity	105%
Electrode (ksi)	E70



FLANGE CONNECTION RESULTS

Bolts	54.9% Passing
Ring Plate	69.6% Passing
Weld - Stiffener & Ring Plate	92.4% Passing
Weld - Spine & Stiffener	44.5% Passing
Spine Wall Tear Out / Punching Shear	32.9% Passing
Max Tension In Stiffeners	59.8 kips
Max Compression in Stiffeners	61.9 kips
Stiffener Bending	38.6% Passing
Stiffener Shear	67.9% Passing
Stiffener Combined Shear & Bending	78.5% Passing

Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
 Site Name: Bridgeport
 App #:

Manufacturer: Other

Bolt Data

Qty:	8	Bolt Fu:	120
Diam:	1	Bolt Fy:	92
Bolt Material:	A325		
N/A:	0	<-- Disregard	
N/A:	0	<-- Disregard	
Circle:	21	in	

Reactions

Moment:	106.51	ft-kips
Axial:	4.12	kips
Shear:	4.27	kips
Exterior Flange Run, T+q:	0	kips

Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Elevation: 82 feet

Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 29.9 Kips, Ext. Tu=Interior Tu
 Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$): 54.5 Kips
 Bolt Stress Ratio: 54.9% **Pass**

Plate Data

Plate Outer Diam:	23.25	in
Plate Inner Diam:	18.25	in (Hole @ Ctr)
Thick:	1.25	in
Grade:	36	ksi
Effective Width:	5.50	in

Interior Flange Plate Results

Flexural Check
 Controlling Bolt Axial Force: 30.9 Kips, Ext. Cu=Interior Cu
 Plate Stress: 16.2 ksi
 Allowable Plate Stress, $\phi^* F_y$: 32.4 ksi
 Plate Stress Ratio: 50.0% **Pass**

Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

n/a

Stiffener Results

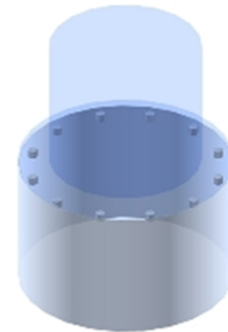
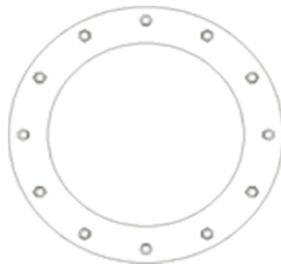
Horizontal Weld: n/a
 Vertical Weld: n/a
 Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$: n/a
 Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data

Pole OuterDiam:	24	in
Thick:	0.375	in
Pole Inner Diam:	23.25	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
 Site Name: Bridgeport
 App #:

Manufacturer: Other

Bolt Data

Qty:	21	Bolt Fu:	120
Diam:	1	Bolt Fy:	92
Bolt Material:	A325		
N/A:	0	<-- Disregard	
N/A:	0	<-- Disregard	
Circle:	21	in	

Reactions

Moment:	224.11	ft-kips
Axial:	7.29	kips
Shear:	6.04	kips
Exterior Flange Run, T+q:		kips

Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Elevation: 60 feet

Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 24.0 Kips, Ext. Tu=Interior Tu
 Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$): 54.5 Kips
 Bolt Stress Ratio: 44.1% **Pass**

Plate Data

Plate Outer Diam:	23.25	in
Plate Inner Diam:	18.25	in (Hole @ Ctr)
Thick:	1.25	in
Grade:	36	ksi
Effective Width:	3.48	in

Interior Flange Plate Results

Flexural Check
 Controlling Bolt Axial Force: 24.7 Kips, Ext. Cu=Interior Cu
 Plate Stress: 20.5 ksi
 Allowable Plate Stress, $\phi^* F_y$: 32.4 ksi
 Plate Stress Ratio: 63.2% **Pass**

Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

n/a

Stiffener Results

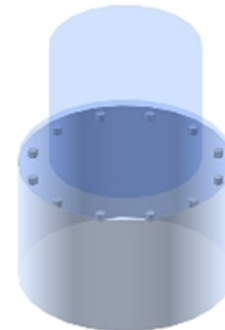
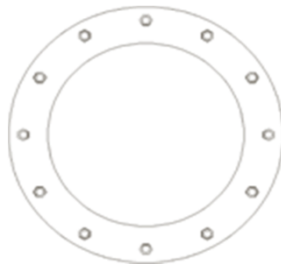
Horizontal Weld : n/a
 Vertical Weld: n/a
 Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$: n/a
 Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data

Pole OuterDiam:	24	in
Thick:	0.375	in
Pole Inner Diam:	23.25	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
 Site Name: Bridgeport
 App #:

Manufacturer: Other

Bolt Data

Qty:	21	Bolt Fu:	120
Diam:	1	Bolt Fy:	92
Bolt Material:	A325		
N/A:	0	<-- Disregard	
N/A:	0	<-- Disregard	
Circle:	21	in	

Reactions

Moment:	224.11	ft-kips
Axial:	7.29	kips
Shear:	6.04	kips
Exterior Flange Run, T+q:	0	kips

Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Elevation: 60 feet

Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 24.0 Kips, Ext. Tu=Interior Tu
 Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$): 54.5 Kips
 Bolt Stress Ratio: 44.1% **Pass**

Plate Data

Plate Outer Diam:	23.25	in
Plate Inner Diam:	18.25	in (Hole @ Ctr)
Thick:	1.25	in
Grade:	36	ksi
Effective Width:	3.48	in

Interior Flange Plate Results

Flexural Check
 Controlling Bolt Axial Force: 24.7 Kips, Ext. Cu=Interior Cu
 Plate Stress: 20.5 ksi
 Allowable Plate Stress, $\phi^* F_y$: 32.4 ksi
 Plate Stress Ratio: 63.2% **Pass**

Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

n/a

Stiffener Results

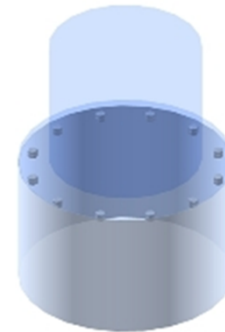
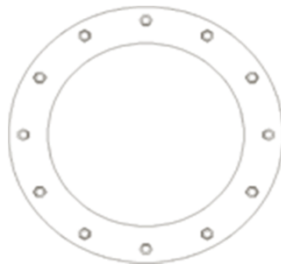
Horizontal Weld: n/a
 Vertical Weld: n/a
 Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$: n/a
 Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data

Pole OuterDiam:	24	in
Thick:	0.375	in
Pole Inner Diam:	23.25	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

v4.4 - Effective 7-12-13

Asymmetric Bolt Analysis

Moment = 429 k-ft
 Axial = 11.3 kips
 Shear = 7.6 kips
 Anchor Qty = 20

TIA Ref. = G
 ASIF = N/A
 Max Ratio = 100.0%

Location = Flange Plate
 η = N/A for BP, Rev. G Sect. 4.9.9
 Threads = X-Excluded for FP, Rev. G

**** For Flange Plates: Prying action is not considered in the bolt loads. ****

Item	Nominal Bolt Dia, in	Spec	Fy, ksi	Fu, ksi	Location, degrees	Bolt Circle, in	Area Override, in ²	Area, in ²	Max Net Compression, kips	Max Net Tension, kips	Load for Capacity Calc, kips	Capacity Override, kips	Capacity, kips	Capacity Ratio
1	1.000	A325	92	120	0.0	21.00	0.00	0.79	26.39	25.67	25.67	0.00	54.54	47.1%
2	1.000	A325	92	120	22.5	21.00	0.00	0.79	23.01	22.28	22.28	0.00	54.54	40.9%
3	1.000	A325	92	120	45.0	21.00	0.00	0.79	22.79	22.07	22.07	0.00	54.54	40.5%
4	1.000	A325	92	120	67.5	21.00	0.00	0.79	25.94	25.21	25.21	0.00	54.54	46.2%
5	1.000	A325	92	120	90.0	21.00	0.00	0.79	29.98	29.26	29.26	0.00	54.54	53.7%
6	1.000	A325	92	120	112.5	21.00	0.00	0.79	32.65	31.92	31.92	0.00	54.54	58.5%
7	1.000	A325	92	120	135.0	21.00	0.00	0.79	32.80	32.08	32.08	0.00	54.54	58.8%
8	1.000	A325	92	120	157.5	21.00	0.00	0.79	30.38	29.66	29.66	0.00	54.54	54.4%
9	1.000	A325	92	120	180.0	21.00	0.00	0.79	26.39	25.67	25.67	0.00	54.54	47.1%
10	1.000	A325	92	120	202.5	21.00	0.00	0.79	23.01	22.28	22.28	0.00	54.54	40.9%
11	1.000	A325	92	120	225.0	21.00	0.00	0.79	22.79	22.07	22.07	0.00	54.54	40.5%
12	1.000	A325	92	120	247.5	21.00	0.00	0.79	25.94	25.21	25.21	0.00	54.54	46.2%
13	1.000	A325	92	120	270.0	21.00	0.00	0.79	29.98	29.26	29.26	0.00	54.54	53.7%
14	1.000	A325	92	120	292.5	21.00	0.00	0.79	32.65	31.92	31.92	0.00	54.54	58.5%
15	1.000	A325	92	120	315.0	21.00	0.00	0.79	32.80	32.08	32.08	0.00	54.54	58.8%
16	1.000	A325	92	120	337.5	21.00	0.00	0.79	30.38	29.66	29.66	0.00	54.54	54.4%
17	0.000	CCI 4 x 0.75 (65 ksi)	65	80	0.0	24.75	3.00	3.00	118.57	115.81	118.57	122.34	122.34	96.9%
18	0.000	CCI 4 x 0.75 (65 ksi)	65	80	70.0	24.75	3.00	3.00	118.57	115.81	118.57	122.34	122.34	96.9%
19	0.000	CCI 4 x 0.75 (65 ksi)	65	80	180.0	24.75	3.00	3.00	118.57	115.81	118.57	122.34	122.34	96.9%
20	0.000	CCI 4 x 0.75 (65 ksi)	65	80	250.0	24.75	3.00	3.00	118.57	115.81	118.57	122.34	122.34	96.9%

24.57

Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
 Site Name: Bridgeport
 App #:

Manufacturer: Other

Bolt Data

Qty:	16		
Diam:	1	Bolt Fu:	120
Bolt Material:	A325	Bolt Fy:	92
N/A:	0	<-- Disregard	
N/A:	0	<-- Disregard	
Circle:	21	in	

Reactions

Moment:	227.1	ft-kips
Axial:	5.8	kips
Shear:	3.9	kips
Exterior Flange Run, T+q:		kips

Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Elevation: 30 feet

Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 32.1 Kips, Ext. Tu=Interior Tu
 Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$): 54.5 Kips
 Bolt Stress Ratio: 58.8% **Pass**

Plate Data

Plate Outer Diam:	23.25	in
Plate Inner Diam:	18.25	in (Hole @ Ctr)
Thick:	1.25	in
Grade:	36	ksi
Effective Width:	4.57	in

Interior Flange Plate Results

Flexural Check
 Controlling Bolt Axial Force: 32.8 Kips, Ext. Cu=Interior Cu
 Plate Stress: 20.7 ksi
 Allowable Plate Stress, $\phi^* F_y$: 32.4 ksi
 Plate Stress Ratio: 63.9% **Pass**

Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

n/a

Stiffener Results

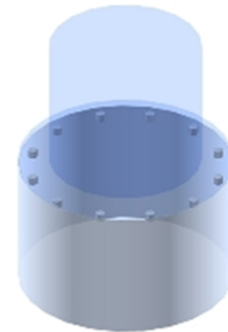
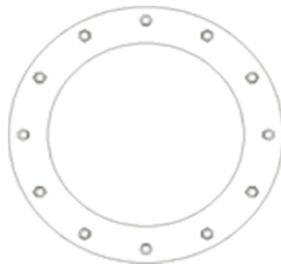
Horizontal Weld : n/a
 Vertical Weld: n/a
 Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$: n/a
 Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data

Pole OuterDiam:	24	in
Thick:	0.375	in
Pole Inner Diam:	23.25	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

Stiffened or Unstiffened, Interior Flange Plate - Any Bolt Material TIA Rev G

Site Data

BU#: 822779
 Site Name: *Bridgeport*
 App #:

Manufacturer: **Other**

Bolt Data

Qty:	16	Bolt Fu:	120
Diam:	1	Bolt Fy:	92
Bolt Material:	A325		
N/A:	0	<-- Disregard	
N/A:	0	<-- Disregard	
Circle:	21	in	

Reactions

Moment:	227.1	ft-kips
Axial:	5.8	kips
Shear:	3.9	kips
Exterior Flange Run, T+q:	0	kips

Bolt Threads:

X-Excluded
$\phi V_n = \phi(0.55 A_b F_u)$
$\phi = 0.75, \phi^* V_n$ (kips):
38.88

Elevation: **30** feet

Interior Flange Bolt Results

Maximum Bolt Tension, Tu: 32.1 Kips, Ext. Tu=Interior Tu
 Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$): 54.5 Kips
 Bolt Stress Ratio: 58.8% **Pass**

Plate Data

Plate Outer Diam:	23.25	in
Plate Inner Diam:	18.25	in (Hole @ Ctr)
Thick:	1.25	in
Grade:	36	ksi
Effective Width:	4.57	in

Interior Flange Plate Results

Flexural Check
 Controlling Bolt Axial Force: 32.8 Kips, Ext. Cu=Interior Cu
 Plate Stress: 20.7 ksi
 Allowable Plate Stress, $\phi^* F_y$: 32.4 ksi
 Plate Stress Ratio: 63.9% **Pass**

Stiffener Data (Welding at Both Sides)

Config:	0	*
Weld Type:	0	
Groove Depth:	0	in **
Groove Angle:	0	degrees
Fillet H. Weld:	0	<-- Disregard
Fillet V. Weld:	0	in
Width:	0	in
Height:	0	in
Thick:	0	in
Notch:	0	in
Grade:	0	ksi
Weld str.:	0	ksi

n/a

Stiffener Results

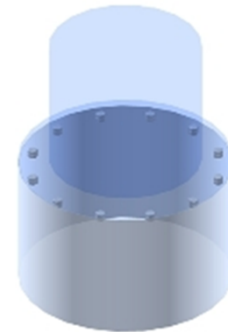
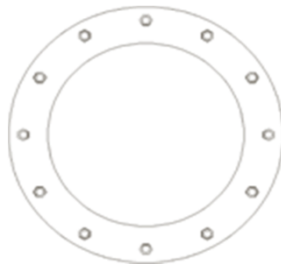
Horizontal Weld : n/a
 Vertical Weld: n/a
 Plate Flex+Shear, $f_b / F_b + (f_v / F_v)^2$: n/a
 Plate Tension+Shear, $f_t / F_t + (f_v / F_v)^2$: n/a
 Plate Comp. (AISC Bracket): n/a

Pole Results

Pole Punching Shear Check: n/a

Pole Data

Pole OuterDiam:	24	in
Thick:	0.375	in
Pole Inner Diam:	23.25	in
Grade:	42	ksi
# of Sides:	0	"0" IF Round
Fu	60	ksi



* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

** Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

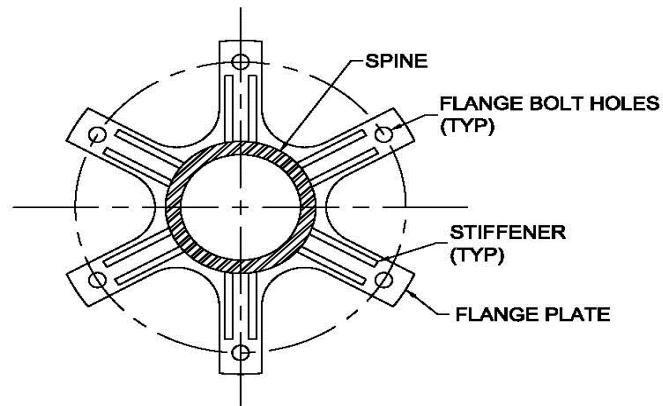
CCI Flagpole Tool



Site Data	
BU#:	822779
Site Name:	Bridgeport
App #:	

Code	
Code:	TIA-222-G
Ice Thickness:	0.5 in
Windspeed (V):	125 mph
Ice Wind Speed (V):	50 mph
Exposure Category:	C
Topographic Feature:	N/A
Structure Class:	II

Tower Information	
Total Tower Height:	120 ft
Base Tower Height:	82 ft
Total Canister Length:	38 ft
Number of Canister Assembly Sections:	4



FLANGE PLATE
(TYPE 3: SOLIDITY RATIO 0.5)

Canister Section Number *:	Canister Assembly Length (ft):	Canister Assembly Diameter (in):	Number of Sides Canister Section	Plate Type:	Mating Flange Plate Thickness (in)**:	Mating Flange Plate Diameter (in):	Solidity Ratio	Plate Weight (Kip):	Canister Weight (Kip)
1	10	36	Round	3	0.75	36	0.5	0.216	0.188
2	10	36	Round	3	0.75	36	0.5	0.216	0.188
3	10	36	Round	3	0.75	36	0.5	0.216	0.188
4	8	36	Round	3	0.75	36	0.5	0.216	0.151

* Sections are numbered from the top of the tower down

** Mating Flange Plate Thickness at the bottom of canister section

Flag on Tower:	Yes
Flag Width:	18 ft
Flag Height:	12 ft
Flag Elevation(z):	120 ft

Truck Ball on Tower:	Yes
Diameter of Ball:	18 in

Geometry : Base Tower + Spine

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Pole Height Above Base (ft)	Section Length (ft)	Lap Splice Length (ft)	Number of Sides	Top Diameter (in)	Bottom Diameter (in)	Wall Thickness (in)	Bend Radius (in)	Pole Material
120	10		0	10.75	10.75	0.349	n/a	A500-42
110	10		0	10.75	10.75	0.349	n/a	A500-42
100	10		0	10.75	10.75	0.349	n/a	A500-42
90	8		0	10.75	10.75	0.349	n/a	A500-42

Delete [x]
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Delete [x]
Delete [x]

82	22		0	24	24	0.375	n/a	A53-B-42
60	30		0	24	24	0.375	n/a	A53-B-42
30	30		0	24	24	0.375	n/a	A53-B-42

[x]
[x]
[x]

Discrete Loads: Truck Ball	Apply $C_a A_A$ at Elevation(z) (ft)	$C_a A_A$ No Ice (ft ²)	$C_a A_A$ 1/2" Ice (ft ²)	$C_a A_A$ 1" Ice (ft ²)	$C_a A_A$ 2" Ice (ft ²)	$C_a A_A$ 4" Ice (ft ²)	Weight No Ice (Kip)	Weight 1/2" Ice (Kip)
		120.75	0.884	1.378	1.527	1.848	2.581	0.05

Discrete Loads : $C_F A_F$ for Canister Assembly								
Canister Loading	Apply $C_F A_F$ at Elevation(z) (ft)	$C_F A_F$ No Ice (ft ²)	$C_F A_F$ 1/2" Ice (ft ²)	$C_F A_F$ 1" Ice (ft ²)	$C_F A_F$ 2" Ice (ft ²)	$C_F A_F$ 4" Ice (ft ²)	Canister Assembly Weight No Ice (Kip)	Canister Assembly Weight 1/2" Ice (Kip)
Canister Load 1	120	9.000	18.500	19.000	20.000	22.000	0.094	0.206
Canister Load 2	110	18.000	37.000	38.000	40.000	44.000	0.405	0.628
Canister Load 3	100	18.000	37.000	38.000	40.000	44.000	0.405	0.628
Canister Load 4	90	16.200	33.300	34.200	36.000	39.600	0.386	0.587
Canister Load 5	82	7.200	14.800	15.200	16.000	17.600	0.292	0.381

User Forces: Flag Force Calculation Per ANSI/NAAMM FP 1001-07	
Wind _{FORCE} =	0.482 Kip
Weight=	0.023 Kip
Wind _{FORCE, ICE} =	0.078 Kip
Weight _{ICE} =	0.252 Kip
W _{FORCE, SERVICE WIND} =	0.111 Kip
Weight=	0.023 Kip

← Flag force should be included at the top of the flag attachment elevation. If the attachment of the flag to the halyard distributes forces equally to the pole, apply flag forces accordingly in tnx file.

Deflection Check Required:	Yes	Import Deflection Results
3% Spine Deflection Check		
Allowable (3%) Horizontal Spine Deflection (inches)	Actual Deflection *** (inches)	Sufficient/ Insufficient
13.680	9.707	Sufficient

*** Relative deflection under service level wind speed



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

SPRINT Existing Facility

Site ID: CT54XC747

Bridgeport_Rt 8
1875 Noble Ave
Bridgeport, CT 06610

January 20, 2017

EBI Project Number: 6217000228

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general public allowable limit:	8.87 %



January 20, 2017

SPRINT

Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495

Emissions Analysis for Site: **CT54XC747 – Bridgeport_Rt 8**

EBI Consulting was directed to analyze the proposed SPRINT facility located at **1875 Noble Ave, Bridgeport, CT**, for the purpose of determining whether the emissions from the Proposed SPRINT Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 850 MHz Band is approximately $567 \mu\text{W}/\text{cm}^2$. The general population exposure limit for the 1900 MHz (PCS) and 2500 MHz bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed SPRINT Wireless antenna facility located at **1875 Noble Ave, Bridgeport, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since SPRINT is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 CDMA channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 2 LTE channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 3) 2 LTE channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 4) 2 LTE channels (2500 MHz (BRS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.



- 6) For the following calculations the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antennas used in this modeling are the **Commscope DHHTT65B-3XT** for transmission in the 850 MHz, 1900 MHz (PCS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antenna mounting height centerlines of the proposed antennas are **96 feet** above ground level (AGL) for **Sector A**, **96 feet** above ground level (AGL) for **Sector B** and **96 feet** above ground level (AGL) for Sector C.
- 9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.



SPRINT Site Inventory and Power Data by Antenna

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Commscope DHHTT65B-3XT	Make / Model:	Commscope DHHTT65B-3XT	Make / Model:	Commscope DHHTT65B-3XT
Gain:	13.35 / 15.25/15.05 dBd	Gain:	13.35 / 15.25/15.05 dBd	Gain:	13.35 / 15.25/15.05 dBd
Height (AGL):	96 feet	Height (AGL):	96 feet	Height (AGL):	96 feet
Frequency Bands	850 MHz / 1900 MHz (PCS) / 2500 MHz (BRS)	Frequency Bands	850 MHz / 1900 MHz (PCS) / 2500 MHz (BRS)	Frequency Bands	850 MHz / 1900 MHz (PCS) / 2500 MHz (BRS)
Channel Count	8	Channel Count	8	Channel Count	8
Total TX Power(W):	420 Watts	Total TX Power(W):	420 Watts	Total TX Power(W):	420 Watts
ERP (W):	11,751.15	ERP (W):	11,751.15	ERP (W):	11,751.15
Antenna A1 MPE%	6.54 %	Antenna B1 MPE%	6.54 %	Antenna C1 MPE%	6.54 %
Antenna A3 MPE%	0.00 %	Antenna B3 MPE%	0.00 %	Antenna C3 MPE%	0.00 %

Site Composite MPE%	
Carrier	MPE%
SPRINT – Max per sector	6.54 %
T-Mobile / Voicestream	0.86 %
Clearwire	0.24 %
Nextel	1.23 %
Site Total MPE %:	8.87 %

SPRINT Sector A Total:	6.54 %
SPRINT Sector B Total:	6.54 %
SPRINT Sector C Total:	6.54 %
Site Total:	8.87 %

SPRINT Max Values Per Sector:

SPRINT _ Frequency Band / Technology	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ($\mu\text{W}/\text{cm}^2$)	Frequency (MHz)	Allowable MPE ($\mu\text{W}/\text{cm}^2$)	Calculated % MPE
Sprint 850 MHz CDMA	2	648.82	96	5.76	850 MHz	567	1.02%
Sprint 850 MHz LTE	2	1,297.63	96	11.52	850 MHz	567	2.03%
Sprint 1900 MHz (PCS) LTE	2	2,009.79	96	17.84	1900 MHz (PCS)	1000	1.78%
Sprint 2500 MHz (BRS) LTE	2	1,919.34	96	17.04	2500 MHz (BRS)	1000	1.70%
						Total:	6.54%



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the SPRINT facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

SPRINT Sector	Power Density Value (%)
Sector A:	6.54 %
Sector B:	6.54 %
Sector C:	6.54 %
SPRINT Maximum Total (per sector):	6.54 %
Site Total:	8.87 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **8.87 %** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.