June 15, 2020

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: Notice of Exempt Modification for T-Mobile: <br> 876321 - T-Mobile Site ID: CTNH107A <br> 150 North Main Street, Branford, CT 06450 <br> Latitude: $\mathbf{4 1}^{\circ} \mathbf{1 7}^{\prime} \mathbf{1 9 . 0 0 \prime \prime}$ / Longitude: $\mathbf{- 7 2}^{\circ} \mathbf{4 8} \mathbf{~ 4 9 . 9 0 ' ~}^{\prime \prime}$

Dear Ms. Bachman:
T-Mobile currently maintains nine (9) total antennas at the 121 -foot mount on the existing 147 -foot monopole tower, located at 150 North Main Street, Branford, CT. The structure is owned by Crown Castle and the property is owned by Premier Realty Holdings LLC. T-Mobile now intends to replace three (3) existing antennas with three (3) new $600 / 700 \mathrm{MHz}$ antennas on a replacement mount. Additional mount modification details as shown on the enclosed mount analysis.

## Planned Modifications:

Tower:

Remove and Replace:
(3) ANDREW LNX-6515DS-A1M (REMOVE) - (3) RFS-APXVAARR24_43U-NA20 Antenna 600/700 MHz (REPLACE)
(3) $1-5 / 8 "$ coax (REMOVE) - (3) $1-5 / 8 " 6 \times 12$ HCS Hybrid Fiber Trunk (REPLACE)
(3) 11 - B12 RRUs (REMOVE) - (3) 4449 B12/B71 RRUs (REPLACE)

## Existing to Remain:

(3) AIR21 KRC118023-1_B2P_B4A Antenna 2100 MHz
(3) AIR21 KRC118023-1_B2A_B4P Antenna 1900/2100 MHz

## Ground:

Existing RBS 6201 Cabinet to be removed and replaced with new RBS 6131. Internal upgrades to existing cabinet.
Upgrade existing breakers.

This facility was approved by the Town of Brandord Planning and Zoning Commission on September 18, 1997. The approval was given with conditions which this exempt modification comply with.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16$50 \mathrm{j}-73$, for construction that constitutes an exempt modification pursuant to R.C.S.J. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to James B. Cosgrove, First Selectman for the Town of Branford, Harry Smith, Town Planner, as well as the property owner and Crown Castle is the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Anne Marie Zsamba.

Page 3

Sincerely,

Anne Marie Zsamba
Site Acquisition Specialist
3 Corporate Park Drive, Suite 101 Clifton Park, NY 12065
201-236-9224
annemarie.zsamba@crowncastle.com

Attachments
cc:
James Cosgrove, First Selectman (via email only to jcosgrove@branford-ct.gov)
Branford Town Hall
1019 Main Street, P.O. Box 150, Branford, CT 06405
(203) 488-8394

Harry Smith, Town Planner (via email only to p-z@branford-ct.gov)
Branford Town Hall
1019 Main Street, P.O. Box 150,
Branford, CT 06405
(203) 488-8394

Premier Realty Holdings LLC
155 North Main St (via email only to nancyanderson3@comcast.net)
Branford, CT 06405
(303) 359-5537

| From: | $\underline{Z s a m b a, ~ A n n e ~ M a r i e ~}$ |
| :--- | :--- |
| To: | icosgrove@branford-ct.gov |
| Subject: | Notice of Exempt Modification - 150 North Main Street, Branford - TMobile |
| Date: | Monday, June 15, 2020 10:48:00 AM |
| Attachments: | T-Mobile -CTNH107A - 876321 Exempt Modification App CT Siting Council Town of Branford notice.pdf |

Dear First Selectman Cosgrove:

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today June 15, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best,
Anne Marie Zsamba

ANNE MARIE ZSAMBA
Site Acquisition Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112

## CROWN CASTLE

3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

| From: | Zsamba, Anne Marie |
| :--- | :--- |
| To: | $\underline{\text { nancyanderson3@comcast.net }}$ |
| Subject: | Notice of Exempt Modification - 150 North Main Street, Branford - TMobile |
| Date: | Monday, June 15, 2020 10:48:00 AM |
| Attachments: | T-Mobile -CTNH107A - 876321 Exempt Modification App CT Siting Council Town of Branford notice.pdf. |

Dear Premier Realty Holdings LLC:

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today June 15, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best,
Anne Marie Zsamba

ANNE MARIE ZSAMBA
Site Acquisition Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112

## CROWN CASTLE

3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

| From: | $\underline{\text { Zsamba, Anne Marie }}$ |
| :--- | :--- |
| To: | $\underline{\text { p-z@branford-ct.gov }}$ |
| Subject: | Notice of Exempt Modification - 150 North Main Street, Branford - TMobile |
| Date: | Monday, June 15, 2020 10:48:00 AM |
| Attachments: | T-Mobile -CTNH107A - 876321 Exempt Modification App CT Siting Council Town of Branford notice.pdf |

Dear Town Planner Smith:

Attached please find T-Mobile's exempt modification application that is being submitted to the Connecticut Siting Council, today June 15, 2020.

In light of the present circumstances with Covid-19, The Council has advised that electronic notification of this filing is acceptable. If you could kindly confirm receipt. Thank you.

Best,
Anne Marie Zsamba

ANNE MARIE ZSAMBA
Site Acquisition Specialist
T: (201) 236-9224
M: (518) 350-3639
F: (724) 416-6112
CROWN CASTLE
3 Corporate Park Drive, Suite 101
Clifton Park, NY 12065
CrownCastle.com

## Exhibit A

## Original Facility Approval

TOWN OF BRANFORD TOWN HALL DRIVE P.O. BOX 150<br>Branford, Connecticut 06405 488-1255

## NOTICE OF DECISION

September 22, 1997
Sprint PCS
\% Attorney John Knuff
Harris Beach \& Wilcox, L.L.P
147 North Broad Street
Milford, Connecticut 06460
SUBJECT: Special Exception
APPLICATION \# 97-6.5
LOCATION: 150 North Main Street
OWNER OF RECORD: Irene Maculaitis
Dear Sir:
At a meeting of the Branford Planning \& Zoning Commission held on Thursday, September 18, 1997, the Commission voted to:

X Approve your above subject application with the conditions noted below.


NOTE: This Special Exception shall become effective only after it is filed on the Land Records in the office of the Town Clerk.

1. Prior to issuance of a building permit, revise plan to show the following:
a. Revise width of eastern-most curb cut to 30 feet (Sect. 25.10a) by creating new landscaped island extending 15 feet back from streetline (Sect. 25.8.2) with new sidewalk (Sect. 31.5.3(b)).
b. Relocate proposed utility pole so that it is not in the access drive.
2. Provide for co-location of communications equipment to be operated by the Town of Branford Sewage Treatment Plant.
3. Change plantings around tower yard to 6' to 7' dark American Arborvitae and rearrange to screen parking area from street.
4. All users of the telecommunications facility must demonstrate compliance with current FCC regulations for electromagnetic frequency emissions and any future changes in these standards.
5. The owner of the telecommunication facility shall provide for and encourage co-location of other antennae on the facility.

NOTE: Special Exception shall become null and void in the event the applicant fails to obtain a building permit within one (1) year of date of approval.
(Per Section 31.7 of the Branford Zoning Regulations)

CC: Scott M. Thomas Sprint PCS Irene Maculaitis

# SITE PLAN \ND SPECIAL `XCEPTION 

## APPLICATION FOR CERTIFICATE OF ZONING COMPLIANCE TOWN OF BRANFORD

ADDRESS OF SUBJECT PROPERTY<br>$\qquad$<br>150 N. MAI iv Street Branford, CT 06405

ASSESSOR'S MAP DG BLOCK 13

LOT
13 ZONE: $\qquad$ APPLICANT'S NAME Sprint PCS

TELEPHONE (203) 237-1737 ext. 17
ADDRESS 300 RESEARCH Parkway 3rd fl. Meriden, CT 06450
Briefly describe the building, structure or use for which Zoning Compliance Application is made:

The erection of a monopole telecommunications facility and
placement of the associated equipment cabinets on property located
at 150 N. MAIN Street within the IG-1/ Industrial District.

PLEASE SUBMIT THE FOLLOWING WITH YOUR COMPLETED APPLICATION:

1. $\$ 125.00$ (which includes $\$ 100.00$ application fee, $\$ 15.00$ Zoning Compliance fee, and $\$ 10.00$ State surcharge)
2. Application materials described in Sect. 31.4 of the Brantford

Zoning Regulations including:
(1) Statement of Use
(6) Building Plans
(2) Site Plan Map
(3) Erosion Control Plan
(4) Tabulation of Standards
(5) Staging Plan
(7) Traffic Report
(8) Drainage Report
(9) Flood Requirements
(10) Agency Reports
3. Sufficient information to determine compliance with special standards listed on attached sheet.
4. Copy of any variance or Wetlands Commission approval pertinent to this application.
5. Additional information which may be necessary to determine compliance, as specified by the Brantford Planning \& Zoning Commission.

The undersigned states that information submitted with this application is correct and acknowledges that any approval based on erroneous or incomplete information shall be null and void.

SIGNATURE OF APPLICANT
DATE


## Exhibit B

## Property Card

Town of Branford
Property Listing Report

## Property Information

| Owner | PREMIER REALTY HOLDINGS LLC |
| :--- | :--- |
| Address | $148-160$ NO MAIN ST |
| Mailing Address | 150 NORTH MAIN ST <br> BRANFORD , CT $\quad 06405$ |
| Land Use | $\quad$ AUTO S S\&S MDL96 |
| Land Class | C |


| Census Tract |  |
| :--- | :--- |
| Neighborhood | 500 |
| Zoning | IG-1 |
| Acreage | 2.05 |
| Utilities | Public Water,Public Sewer |
| Lot Setting/ Desc | / Level |

## Photo



PARCEL VALUATIONS (Assessed value $=70 \%$ of Appraised Value)

| Appraised |  | Assessed |
| :--- | :--- | :--- |
| Buildings | 61400 | 43000 |
| Outbuildings | 77800 | 54400 |
| Improvements | 142500 | 99700 |
| Extras | 3300 | 2300 |
| Land | 1007000 | 704900 |
| Total | 1149500 | 804600 |
| Previous |  |  |

## Construction Details

| Year Built | 1965 |
| :--- | :--- |
| Stories | 1 |
| Building Style | Car Dealrshp |
| Building Use | Ind/Comm |
| Building Condition | 03 |
| Total Rooms |  |
| Bedrooms |  |
| Full Bathrooms |  |
| Half Bathrooms |  |
| Bath Style |  |
| Kitchen Style |  |
| Roof Style | Flat |
| Roof Cover | Metal/Tin |

EXTERIOR WALLS:

| Primary | MASONRY |
| :--- | :--- |
| Secondary | Pre-finsh MetI |
| INTERIOR WALLS: |  |
| Primary | Minim/Masonry |
| Secondary | Drywall |
| FLOORS: |  |
| Primary | Concr-Finished |
| Secondary | Carpet |
| HEATING/AC: |  |
| Heating Type | Forced Air-Duc |
| Heating Fuel | Oil |
| AC Type | None |

BUILDING AREA:

| Effective Building Area |  |
| :--- | :--- |
| Gross Building Area | 23192 |
| Total Living Area | 13144 |

SALES HISTORY:

| Sale Date | $7 / 6 / 2004$ |
| :--- | :--- |
| Sale Price |  |
| Book/ Page | $0877 / 0469$ |



Approximate Scale: 1 inch : 100 feet
Grand List Date October 2019

This map is for informational purposes only.
All information is subject to verification by any user. The Town of Branford and its mapping contractors assume no legal responsibility for the information contained herein.

## Exhibit C

## Construction Drawings



## -мовіL <br> TOWER OWNER: CROWN CASTLE INTERNATONAL <br> A-MOBLLE <br> STLLVAR WAY LIMTED LABBLITY compair PARSIPPANY, NEW (973) 397-4800

tower owner:

- THE APPLCANT IS TO UPDATE THEIR NETWORK BY INSTALLING SIX ( 6 )
NEW PANEL ANTENNAS, THREE (3) RRUS, AND THREE (3) ADOIIINAL NEW PANEL ANTENNAS, THREE (3) RRUS, AND
CABLES MOUTED ON AN EXISTING MONOPLE.
$\therefore$ CROWN
CROWN
CASTLE

3. THIS FACILITY SHALL BE VIITED ON THE AVERAGE OF ONCE A MONTH
FOR MAITENANCE AND SHALL BE MONTTORED FROM A REMOTE解保
4. THE EXISTING SITE IS LOCATED AT LATTUDE OF 41.28850801 1. N $\pm$

5. THII SET OF PPANS HAS BEEN PREPARED FOR THE PURPOSES OF SHALL NOT BE UTLIZED AS CONSTRUCTION DOCUMENTS UNTLL ALL DRAWINGS HAVE BEEN REVISED TO INICATED "ISSUED FOR
DRAWNGG AVEV
6. ALL MATERALS, WORKMANSHP, AND CONSTRUCTION FOR THE SITE
IMPROVEMENTS' SHOWN HEREON SHALL BE IN ACCORDANCE WITH: 6.A. CURRENT PREVALING MUNICIPAL AND/OR COUNTY S.A. SECIFCATIONS, STANAROS, AND REQUREMENTS.
6.B. CURRENT PREVALING UTLITY COMPANY AUTHORIT.
7. THE CONTRACTOR SHALL NOTIFY B+T GROUP, P.A. IMMEDIATELY IF ANY FIELD-CONDITIONS ENCOUNTERED DIFFER RROM THOSE
REPESENTED HERON AND/OR IF SUCH CONTIONS WOLD OR REPRESENTED
COUD $\begin{aligned} & \text { INEED } \\ & \text { INEFECTVE. }\end{aligned}$.
8. THE CONTRACTOR IS RESPONSIBLE TO PROTECT, REPAIR AND/OR REPLACE ANY DAMAGED STRUCTURES, UTLITIES OR LANDSCAPED ARE
WHICH MAY BE DISTURBED DURING THE CONSTRUCTION OF THIS FACILITY.
9. THE CONSTRUCTION CONTRACTOR IS SOLELY RESPONSIBLE FOR CONSTRUCTION CONTRACTOR IS ALSO RESPONSIBLE FOR ALL JOB SITE
10. SITE INFORMATION SHOWN TAKEN FROM CROWN CASTLE SITE PLANS
11. NO GUARANTEE IS MADE NOR SHOULD BE ASSUMED AS TO THE
COMPLETENESS OR ACCURACY OF THE HORIZONAL OR VERTICAL LOCATIONS. ALL PARTES UTLIZING THIS INFORMATON SHALL FIELD SHOWN PRIOR TO CONSTRUCTON ACTVTIES.
12. ALL IMPROVEMENTS SHALL BE SUBJECT TO INSPECTION AND ALL IMPROVEMENTS SHALL BE SUBJECT TO INSPECTION AND
APPROVA EM THE TOWNSHE ENGINER WHO WEL BE GUNEN PROPER
NOTFICATION PRHOR TO THE START OF ANY CONSTRUCTION.

SCALE: E.

| LEGEND |  |  |  |
| :---: | :---: | :---: | :---: |
|  | ExIStingidemolition notes |  | installation notes |
| (A) | EXISTING ERICSSON <br> AIR21 KRC118023-1B2A B4P <br> ANTENNA TO REMAIN (TOTAL OF 3) | (1) | INSTALL RFS APXVAARR24-43-U-NA2O (8 FT) ANTENNAS ON NEW MOUNT. <br> (TYP. OF 1 PER SECTOR, TOTAL OF 3) |
| (B) | EXISTING ERICSSON AIR21 KRC118023-1B2P_B4A ANTENNA TO REMAIN (TOTAL OF 3) | (2) | INSTALL RADIO 4449 B12/B71 (TYP. OF 1 PER SECTOR, TOTAL OF 3) |
| (c) | EXISTING ANDREW LNX6515DS-A1M ANTENNA TO BE REMOVED (TOTAL OF 3) | (3) | INSTALL (3) $6 \times 12$ HCS FIBER RUN FROM EQUIPMENT TO ANTENNAS FOLLOWING EXISTING ROUTING |
| (0) | EXISTING RRUS11 B12 RADIO TO BE REMOVED (TOTAL OF 3) | (4) | INSTALL NEW RBS 6131 MU AC |
| (E) | EXISTING 1 5/8" COAX TO BE REMOVED (TOTAL OF 3) | (5) | INSTALL (2) NEW BB 6630 BASEBANDS $\operatorname{IN}$ NEW RBS 6131 CABINET |
| (F) | EXISTING RBS 3106 CABINET TO BE REMOVED (TOTAL OF 1) | (6) | INSTALL (6) NEW RU22 RADIOS IN NEW RBS 6131 CABINET |
| (6) | EXISTING DUW30 TO BE RELOCATED TO NEW RBS 6131 CABINET (total OF 2) |  |  |
| - | EXISTING DUG20 TO be relocated TO NEW RBS 6131 CABINET (TOTAL OF 1) |  |  |


| ANTENNA AND CABLE SCHEDULE |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| SECTOR | Position | PROPOSED ANTENNAS | PROPOSED ANTENNA CONFIGURATION |  | E-TIL | M-TLT | $\begin{aligned} & \text { ANTENNA } \\ & \text { CENTERLINE } \end{aligned}$ | TMARRU | CAbles | JUMPER TYPE | $\begin{gathered} \text { CABLE } \\ \text { LENGTH } \end{gathered}$ |
| $60^{\circ}$ - ALPHA | A1 | $\begin{aligned} & \text { ERICSSON AIR21 } \\ & \text { KRC } 118023-1 \text { _B2A_B4P } \end{aligned}$ | $\begin{aligned} & \mathrm{U} 1900 \\ & G 1900 \\ & \mathrm{U} 2100 \end{aligned}$ | - | $2 \cdot / 2^{*}$ | $0 \cdot$ | $125^{\prime}-0$ " | 1/0 | (2) $15 / 8^{\prime \prime} \operatorname{COAX}$ (1) $9 \times 18$ HCS FIBER | $\begin{gathered} \text { DC/FIBER \& } \\ 1 / 2^{\prime \prime} \text { COAX } \end{gathered}$ | 171'-0" |
|  | A2 | $\begin{gathered} \text { RFS } \\ \text { APXVAAR24_43-U-NA2O } \end{gathered}$ | $\begin{aligned} & L 700 \\ & \hline 1000 \end{aligned}$ | $\begin{aligned} & 871 \\ & 812 \end{aligned}$ | 2 | $0 \cdot$ |  | 0/1 | (1) $6 \times 12$ HCS FIBER | DC/FIBER | 171'-0" |
|  | A3 | $\begin{gathered} \text { ERICSSON AIR21 } \\ \text { KRC118023-1_B2P_B4A } \end{gathered}$ | L2100 | - | $2 \cdot$ | $0^{\circ}$ |  | 0/0 | (1) $6 \times 12$ HCS FIBER (SHARED) | DC/FIBER | 171'-0" |
| 200 - beta | B1 | ERICSSON AIR21 KRC118023-1_B2A_B4P | $\begin{aligned} & \mathrm{U} 1900 \\ & \text { G1900 } \\ & \text { U2100 } \end{aligned}$ | - | $2 \cdot / 2^{*}$ | ${ }^{\circ}$ | $125^{\prime}-0^{\prime \prime}$ | 1/0 | $\begin{aligned} & \text { (2) } 15 / 8^{\prime \prime} \text { COAAX } \\ & \text { (1) } 9 \times 18 \text { HCS FIBER } \\ & \text { (SHARED) } \end{aligned}$ | $\begin{aligned} & \text { DC/FIBER \& } \\ & 1 / 2^{\prime \prime} \text { COAX } \end{aligned}$ | 171'-0" |
|  | ${ }^{82}$ | $\begin{gathered} \text { RFS } \\ \text { APXVAARR24_43-U-NA2O } \end{gathered}$ | $\begin{aligned} & \mathrm{L} 700 \\ & \mathrm{~L} 00 \end{aligned}$ | $\begin{aligned} & 871 \\ & 812 \\ & 812 \end{aligned}$ | 2 | $0 \cdot$ |  | 0/1 | (1) $6 \times 12$ HCS FIBER | DC/FIBER | 171'-0" |
|  | B3 | $\begin{gathered} \text { ERICSSON AIR21 } \\ \text { KRC118023-1_B2P_B4A } \end{gathered}$ | L2100 | - | 2. | $0 \cdot$ |  | 0/0 | $\begin{gathered} \text { (1) } 6 \times 12 \text { HCS FIBER } \\ \text { (SHARED) } \end{gathered}$ | DC/FIBER | 171'-0" |
| 290\% - GAMMA | 61 | $\begin{aligned} & \text { ERICSSON AIR21 } \\ & \text { KRC118023-1_B2A_B4P } \end{aligned}$ | $\begin{aligned} & \text { U1900 } \\ & \text { G1900 } \\ & \text { U2100 } \end{aligned}$ | - | $2 \cdot / 2^{*}$ | $0 \cdot$ | $125^{\prime}-0^{\prime \prime}$ | 1/0 | $\begin{aligned} & \text { (2) } 15 / 8^{\prime \prime} \text { COAX } \\ & \text { (1) } 9 \times 18 \mathrm{HCS} \text { FIBER } \\ & \text { (SHARED) } \end{aligned}$ |  <br> 1/2" COAX | 171'-0" |
|  | 62 | $\begin{aligned} & \text { APXVAARR24_43-U-NA2O } \end{aligned}$ | $\begin{gathered} L 700 \\ \hline 600 \\ \hline 60 \end{gathered}$ | $\begin{aligned} & 871871 \\ & 812 \end{aligned}$ | 2 | 0 |  | 0/1 | (1) $6 \times 12$ HCS FIBER | DC/FIBER | 171'-0" |
|  | 63 | $\begin{gathered} \text { ERICSSON AIR21 } \\ \text { KRC118023-1_B2P_B4A } \end{gathered}$ | L2100 | - | $2 \cdot$ | $0 \cdot$ |  | 0/0 | (1) $6 \times 12$ HCS FIBER (SHARED) | DC/FIBER | 171'-0" |

## $\Sigma_{P}$ orree

 $\backsim$ CROWN-T- .- Mobile

|  |  |  | $\begin{aligned} & \text { 11 } \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & 0 \\ & \vdots \\ & 0 \\ & 0 \\ & 1 \\ & 10 \\ & 0 \\ & 0 \end{aligned}$ |
| :---: | :---: | :---: | :---: |



(2) EXISTING ANTENNA ORIENTATION

mstran naw nimwa mour

(3)

PROPOSED ANTENNA ORIENTATION


$\square$ Existing
[- $^{-}$future




## Exhibit D

## Structural Analysis Report

Date: August 22, 2019

Darcy Tarr
Crown Castle
3530 Toringdon Way Suite 300
Charlotte, NC 28277

## Subject:

Carrier Designation:

Engineering Firm Designation:
Site Data:

## Structural Analysis Report

T-Mobile Co-Locate Carrier Site Number: Carrier Site Name:

Paul J. Ford and Company<br>250 E. Broad St., Ste 600<br>Columbus, OH 43215<br>614-221-6679

Crown Castle BU Number:
Crown Castle Site Name:
Crown Castle JDE Job Number:
BRANFORD BANM TOWER
Crown Castle Work Order Number: 1783335
Crown Castle Order Number:
479853 Rev. 0
Paul J. Ford and Company Project Number: 37519-2435.002.7805
150 North Main Street, BRANFORD, New Haven County, CT Latitude $41^{\circ} 17^{\prime} 19$ ", Longitude $-72^{\circ} 48^{\prime} 49.9^{\prime \prime}$
147 Foot - Monopole Tower
Dear Darcy Tarr,
Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC5: Proposed Equipment Configuration
Sufficient Capacity - 89.6\%
This analysis utilizes an ultimate 3 -second gust wind speed of 130 mph as required by the 2018 Connecticut State Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 Analysis Criteria.

Respectfully submitted by:


Udaykiran Yerra Structural Designer uyerra@pauljford.com


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tnxTower Output

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## 1) INTRODUCTION

This tower is a 147 ft Monopole tower designed by SUMMIT Manufacturing in March of 1999.
The tower has been modified multiple times to accommodate additional loading.

## 2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Service Wind Speed:

TIA-222-H
II
130 mph
C
1
1.5 in

50 mph
60 mph

Table 1 - Proposed Equipment Configuration

| Mounting <br> Level (ft) | Center <br> Line <br> Elevation <br> (ft) | Number <br> of <br> Antennas | Antenna <br> Manufacturer | Antenna Model | Number <br> of Feed <br> Lines | Feed <br> Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 121.0 | 125.0 | 3 | ericsson | RADIO 4449 B12/B71 |  |  |
|  |  | 3 | rfs celwave | APXVAARR24_43-U- <br> NA20 w/ Mount Pipe |  | 10 |

Table 2-Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{array}{\|l} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 147.0 | 149.0 | 1 | andrew | VHLP2-18 | $\begin{aligned} & 3 \\ & 6 \end{aligned}$ | $\begin{gathered} 1-1 / 4 \\ 1 / 2 \end{gathered}$ |
|  |  | 2 | dragonwave | A-ANT-23G-2-C |  |  |
|  | 147.0 | 3 | alcatel lucent | TD-RRH8x20-25 |  |  |
|  |  | 1 | powerwave technologies | P40-16-XLPP-RR-A w/ Mount Pipe |  |  |
|  |  | 9 | rfs celwave | ACU-A20-N |  |  |
|  |  | 2 | rfs celwave | APXVSPP18-C-A20 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVTM14-C-120 w/ Mount Pipe |  |  |
|  |  | 1 | tower mounts | Platform Mount [LP 1201- |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 145.0 | 146.0 | 3 | alcatel lucent | 800 EXTERNAL NOTCH FILTER | -- | -- |
|  |  | 3 | alcatel lucent | TME-800MHZ RRH |  |  |
|  | 145.0 | 1 | tower mounts | Side Arm Mount [SO 1023] |  |  |
|  | 143.0 | 3 | alcatel lucent | TME-1900MHz RRH (65 $\mathrm{MHz})$ |  |  |
| 110.0 | 112.0 | 9 | andrew | SBNHH-1D65A w/ Mount Pipe | $\begin{gathered} 2 \\ 12 \\ 2 \\ 4 \end{gathered}$ | $\begin{gathered} 2 " \text { Cond } \\ 1-1 / 4 \\ 3 / 8 \\ 3 / 4 \end{gathered}$ |
|  |  | 3 | ericsson | RRUS 32 |  |  |
|  |  | 3 | ericsson | RRUS 32 B2 |  |  |
|  |  | 3 | ericsson | RRUS 32 B66 |  |  |
|  |  | 6 | powerwave technologies | 7020.00 |  |  |
|  |  | 3 | powerwave technologies | 7770.00 w/ Mount Pipe |  |  |
|  |  | 6 | powerwave technologies | LGP2140X |  |  |
|  |  | 2 | raycap | DC6-48-60-18-8F |  |  |
|  | 110.0 | 1 | SitePro1 | MT-195-14 (Hand Rail) |  |  |
|  |  | 1 | SitePro1 | PRK-1245(Kickers) |  |  |
|  |  | 1 | tower mounts | Platform Mount [LP 12011] |  |  |
| 53.0 | 54.0 | 1 | gps | GPS_A | 1 | 1/2 |
|  | 53.0 | 1 | tower mounts | Side Arm Mount [SO 7011] |  |  |
| 49.0 | 50.0 | 1 | lucent | KS24019-L112A | 1 | 1/2 |
|  | 49.0 | 1 | tower mounts | Side Arm Mount [SO 7011] |  |  |

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | Dr. Clarence Welti, P.E., P.C., <br> $10 / 08 / 96$ | 2135657 | CCISITES |
| 4-TOWER FOUNDATION <br> DRAWINGS/DESIGN/SPECS | Summit/PJF, 29299-111, 03/15/99 | 1613620 | CCISITES |
| 4-TOWER MANUFACTURER <br> DRAWINGS | Summit/PJF, 29299-111, 03/15/99 | 1614568 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | PJF, A41709-0058, 05/08/2009 | 2431042 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | PJF, 41709-0058, 06/15/09 | 2448190 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | PJF, A37512-1607, 09/04/2012 | 3316256 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | TEP, 128359, 03/06/13 | 3890848 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | Aero Solutions, 7/23/2013 | 4988798 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | SGS, 130357, 12/9/13 | 4699667 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically and must be replaced if damaged or cracked. Refer to Crown Castle document ENG-PRC-10012, Base Plate Grout Repair.
5) Monopole was modified in conformance with the referenced modification drawings.
6) The shaft reinforcement and transition stiffeners from reference document \#2431042 \& document \#3316256 has been found to be ineffective and therefore, has not been considered in this analysis.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J.
Ford and Company should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

| Section <br> No. | Elevation (ft) | Component <br> Type | Size | Critical <br> Element | P (K) | SF*P_allow <br> (K) | \% <br> Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $147-99.5$ | Pole | TP30.313x22x0.25 | 1 | -14.87 | 1342.23 | 60.2 | Pass |
| L2 | $99.5-59$ | Pole | TP36.9x29.1567x0.3125 | 2 | -22.73 | 2210.06 | 88.3 | Pass |
| L3 | $59-29.25$ | Pole | TP41.481x35.4438x0.375 | 3 | -30.79 | 2980.72 | 89.6 | Pass |
| L4 | $29.25-0$ | Pole | TP45.85x39.8123x0.4375 | 4 | -42.64 | 3929.66 | 89.4 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L3) | 89.6 | Pass |
|  |  |  |  |  |  | Rating $=$ | 89.6 | Pass |

Table 5 - Tower Component Stresses vs. Capacity - LC5

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 76.9 | Pass |
| 1 | Base Plate | 0 | 55.1 | Pass |
| 1 | Base Foundation <br> Steel | 0 | 87.3 | Pass |
| 1 | Base Foundation <br> Soil Interaction | 0 | 84.9 | Pass |
| Structure Rating (max from all components) = |  |  |  |  |

Notes:

- All structural ratings are per TIA-222-H Section 15.5

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

TNXTOWER OUTPUT


## MATERIAL STRENGTH

| GRADE | Fy |  | Fu |  | GRADE |
| :---: | :---: | :---: | :---: | :--- | :--- |
| A607-60 | 60 ksi | 75 ksi | A607-65 | 65 ksi |  |

## TOWER DESIGN NOTES

1. Tower is located in New Haven County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-H Standard.

Tower designed for a 130 mph basic wind in accordance with the TIA-222-H Standard
4. Tower is also designed for a 50 mph basic wind with 1.50 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Risk Category II.
7. Topographic Category 1 with Crest Height of 0.0000 ft
8. TIA-222H Annex S
9. TOWER RATING: 89.6\%

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

1) Tower is located in New Haven County, Connecticut.
2) Tower base elevation above sea level: 57.0000 ft .
3) Basic wind speed of 130 mph .
4) Risk Category II.
5) Exposure Category C.
6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
7) Topographic Category: 1.
8) Crest Height: 0.0000 ft .
9) Nominal ice thickness of 1.5000 in.
10) Ice thickness is considered to increase with height.
11) Ice density of 56.00 pcf.
12) A wind speed of 50 mph is used in combination with ice.
13) Temperature drop of $50^{\circ} \mathrm{F}$.
14) Deflections calculated using a wind speed of 60 mph .
15) TIA-222H Annex S.
16) A non-linear (P-delta) analysis was used.
17) Pressures are calculated at each section.
18) $\quad$ Stress ratio used in pole design is 1.05 .
19) Tower analysis based on target reliabilities in accordance with Annex S.
20) Load Modification Factors used: $\mathrm{K}_{\mathrm{es}}\left(\mathrm{F}_{\mathrm{w}}\right)=0.95$, $\mathrm{K}_{\mathrm{es}}\left(\mathrm{t}_{\mathrm{i}}\right)=0.85$.
21) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

| Consider Moments - Legs | Distribute Leg Loads As Uniform | Use ASCE 10 X-Brace Ly Rules |
| :---: | :---: | :---: |
| Consider Moments - Horizontals | Assume Legs Pinned | Calculate Redundant Bracing Forces |
| Consider Moments - Diagonals | $\checkmark$ Assume Rigid Index Plate | Ignore Redundant Members in FEA |
| Use Moment Magnification | $\checkmark$ Use Clear Spans For Wind Area | SR Leg Bolts Resist Compression |
| Use Code Stress Ratios | Use Clear Spans For KL/r | All Leg Panels Have Same Allowable |
| $\checkmark$ Use Code Safety Factors - Guys | Retension Guys To Initial Tension | Offset Girt At Foundation |
| Escalate Ice | $\checkmark$ Bypass Mast Stability Checks | $\checkmark$ Consider Feed Line Torque |
| Always Use Max Kz | $\checkmark$ Use Azimuth Dish Coefficients | Include Angle Block Shear Check |
| Use Special Wind Profile | $\sqrt{ }$ Project Wind Area of Appurt. | Use TIA-222-H Bracing Resist. Exemption |
| Include Bolts In Member Capacity | Autocalc Torque Arm Areas | Use TIA-222-H Tension Splice Exemption |
| Leg Bolts Are At Top Of Section | Add IBC . $6 \mathrm{D}+\mathrm{W}$ Combination | Poles |
| Secondary Horizontal Braces Leg | Sort Capacity Reports By Component | $\checkmark$ Include Shear-Torsion Interaction |
| Use Diamond Inner Bracing (4 Sided) | Triangulate Diamond Inner Bracing | Always Use Sub-Critical Flow |
| SR Members Have Cut Ends | Treat Feed Line Bundles As Cylinder | Use Top Mounted Sockets |
| SR Members Are Concentric | Ignore KL/ry For 60 Deg. Angle Legs | Pole Without Linear Attachments Pole With Shroud Or No |
|  |  | Appurtenances |
|  |  | Outside and Inside Corner Radii Are |

## Tapered Pole Section Geometry

| Section | Elevation | Section | Splice | Number | Top | Bottom | Wall | Bend | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | Length | Length | of | Diameter | Diameter | Thickness | Radius |  |
|  | ft | ft | Sides | in | in | in | in |  |  |


| Section | Elevation ft | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall <br> Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $\begin{gathered} 147.0000 \\ 99.5000 \end{gathered}$ | 47.5000 | 3.75 | 12 | 22.0000 | 30.3130 | 0.2500 | 1.0000 | $\begin{gathered} \text { A607-60 } \\ (60 \mathrm{ksi}) \end{gathered}$ |
| L2 | $\begin{aligned} & 99.5000- \\ & 59.0000 \end{aligned}$ | 44.2500 | 4.75 | 12 | 29.1567 | 36.9000 | 0.3125 | 1.2500 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | $\begin{aligned} & 59.0000- \\ & 29.2500 \end{aligned}$ | 34.5000 | 5.25 | 12 | 35.4438 | 41.4810 | 0.3750 | 1.5000 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | $\begin{gathered} 29.2500- \\ 0.0000 \end{gathered}$ | 34.5000 |  | 12 | 39.8123 | 45.8500 | 0.4375 | 1.7500 | $\begin{gathered} \text { A607-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |

Tapered Pole Properties

| Section | Tip Dia. in | Area $i n^{2}$ | $\stackrel{I}{i n^{4}}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & \text { C } \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & \text { w } \\ & \text { in } \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 22.6879 | 17.5087 | 1057.2060 | 7.7865 | 11.3960 | 92.7699 | 2142.1860 | 8.6173 | 5.2260 | 20.904 |
|  | 31.2941 | 24.2007 | 2791.7645 | 10.7626 | 15.7021 | 177.7952 | 5656.8718 | 11.9109 | 7.4539 | 29.816 |
| L2 | 30.7544 | 29.0245 | 3082.2498 | 10.3262 | 15.1032 | 204.0796 | 6245.4738 | 14.2850 | 6.9765 | 22.325 |
|  | 38.0915 | 36.8162 | 6290.5707 | 13.0983 | 19.1142 | 329.1046 | $\begin{gathered} 12746.401 \\ 8 \end{gathered}$ | 18.1198 | 9.0517 | 28.965 |
| L3 | 37.4224 | 42.3456 | 6647.1544 | 12.5546 | 18.3599 | 362.0477 | $\begin{gathered} 13468.937 \\ 0 \end{gathered}$ | 20.8412 | 8.4939 | 22.651 |
|  | 42.8120 | 49.6355 | $\begin{gathered} 10705.051 \\ 1 \end{gathered}$ | 14.7159 | 21.4872 | 498.2069 | $\begin{gathered} 21691.335 \\ 7 \end{gathered}$ | 24.4291 | 10.1119 | 26.965 |
| L4 | 42.0136 | 55.4692 | $\begin{gathered} 10976.776 \\ 7 \end{gathered}$ | 14.0962 | 20.6228 | 532.2649 | $\begin{gathered} 22241.925 \\ 5 \end{gathered}$ | 27.3003 | 9.4972 | 21.708 |
|  | 47.3131 | 63.9749 | $\begin{gathered} 16840.156 \\ 1 \end{gathered}$ | 16.2577 | 23.7503 | 709.0502 | $\begin{gathered} 34122.721 \\ 8 \end{gathered}$ | 31.4865 | 11.1153 | 25.406 |


| Tower | Gusset | Gusset | Gusset GradeAdjust. Factor | Adjust. | Weight Mult. Double Angle Double Angle Double Angle |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation | Area | Thickness | $A_{f}$ | Factor | Stitch Bolt | Stitch Bolt |
|  | (perface) |  |  | $A_{r}$ | Stitch Bolt |  |
|  |  |  |  |  | Spacing | Spacing |
|  |  |  |  | Spacing |  |  |
|  |  |  |  |  | Diagonals Horizontals Redundants |  |


| $f t$ | $f t^{2}$ |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| L1 $147.0000-$ | 1 | 1 | 1 | in |
| 99.5000 |  | 1 | 1 | 1 |
| L2 $99.5000-$ | 1 | 1 | 1 |  |
| 59.0000 |  | 1 | 1 | 1 |

0.0000

# Feed Line/Linear Appurtenances - Entered As Round Or Flat 

| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | Start/En $d$ Position | Width or Diamete $r$ in | Perimete <br> $r$ <br> in | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| **** |  |  |  |  |  |  |  |  |  |  |
| 7983A(ELLIPTICAL) | C | No | Surface Ar (CaAa) | $\begin{gathered} 147.0000- \\ 0.0000 \end{gathered}$ | 6 | 2 | $\begin{aligned} & 0.192 \\ & 0.225 \end{aligned}$ | 0.5730 |  | 0.08 |
| HB158-1-08U8S8F18(15/8") | B | No | Surface Ar (CaAa) | $\begin{gathered} 121.0000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.208 \\ & -0.158 \end{aligned}$ | 1.9800 |  | 1.70 |
| LDF4-50A(1/2) | A | No | Surface Ar (CaAa) | $\begin{array}{r} 53.0000- \\ 0.0000 \end{array}$ | 1 | 1 | $\begin{aligned} & 0.242 \\ & 0.258 \end{aligned}$ | 0.6250 |  | 0.15 |
| LDF4-50A(1/2) | A | No | Surface Ar (CaAa) | $\begin{gathered} 49.0000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.242 \\ & 0.258 \end{aligned}$ | 0.6250 |  | 0.15 |
| MP3-04 (L) | B | No | Surface Af (CaAa) | $\begin{gathered} 25.5000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.267 \\ & -0.267 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |

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| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number | Number Per Row | $\begin{aligned} & \text { Start/En } \\ & d \\ & \text { Position } \end{aligned}$ | Width or Diamete $r$ in | Perimete $r$ in | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP3-04 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 25.5000 \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.267 \\ & -0.267 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | C | No | Surface Af (CaAa) | $\begin{gathered} 25.5000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.267 \\ & -0.267 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 52.0000- \\ 32.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | C | No | Surface Af (CaAa) | $\begin{gathered} 52.0000- \\ 32.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | B | No | Surface Af (CaAa) | $\begin{gathered} 52.0000- \\ 32.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 71.0000- \\ 61.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | C | No | Surface Af (CaAa) | $\begin{gathered} 71.0000- \\ 61.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | B | No | Surface Af (CaAa) | $\begin{gathered} 71.0000- \\ 61.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.483 \\ & 0.483 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 35.5000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.017 \\ & -0.017 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | C | No | Surface Af (CaAa) | $\begin{gathered} 35.5000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.233 \\ & 0.233 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-04 (L) | B | No | Surface Af (CaAa) | $\begin{gathered} 35.5000- \\ 0.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.233 \\ & 0.233 \end{aligned}$ | 4.7800 | 12.7800 | 0.00 |
| MP3-03 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 59.0000- \\ 49.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.233 \\ & 0.233 \end{aligned}$ | 4.0600 | 11.2600 | 0.00 |
| MP3-03 (L) | C | No | Surface Af (CaAa) | $\begin{gathered} 59.0000- \\ 49.0000 \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.233 \\ & 0.233 \end{aligned}$ | 4.0600 | 11.2600 | 0.00 |
| MP3-03 (L) | B | No | Surface Af (CaAa) | $\begin{gathered} 59.0000- \\ 49.0000 \\ \hline \end{gathered}$ | 1 | 1 | $\begin{aligned} & 0.233 \\ & 0.233 \\ & \hline \end{aligned}$ | 4.0600 | 11.2600 | 0.00 |

## Feed Line/Linear Appurtenances - Entered As Area

| Description | Face or Leg | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number |  | $\begin{aligned} & C_{A} A_{A} \\ & f t^{2} / f t \end{aligned}$ | Weight <br> plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { HB114-1-0813U4- } \\ \text { M5J(1-1/4) } \end{gathered}$ | C | No | No | Inside Pole | $\begin{gathered} 147.0000- \\ 0.0000 \end{gathered}$ | 3 | $\begin{gathered} \text { No Ice } \\ \text { 1/2" Ice } \\ \text { 1" Ice } \\ \text { 2" Ice } \end{gathered}$ | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 1.20 \\ & 1.20 \\ & 1.20 \\ & 1.20 \end{aligned}$ |
| LDF7-50A(1-5/8) | B | No | No | Inside Pole | $\begin{gathered} 119.0000- \\ 0.0000 \end{gathered}$ | 6 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 0.82 \\ & 0.82 \\ & 0.82 \end{aligned}$ |
| $\begin{gathered} \text { HCS 6X12 } \\ \text { 4AWG(1-5/8) } \end{gathered}$ | B | No | No | Inside Pole | $\begin{gathered} 119.0000- \\ 0.0000 \end{gathered}$ | 3 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 2.40 \\ & 2.40 \\ & 2.40 \\ & 2.40 \end{aligned}$ |
| LDF6-5** ${ }_{\text {** }}(1-1 / 4)$ | B | No | No | Inside Pole | $\begin{gathered} 110.0000- \\ 0.0000 \end{gathered}$ | 12 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 0.60 \\ & 0.60 \\ & 0.60 \\ & 0.60 \end{aligned}$ |
| $\begin{gathered} \text { FB-L98B-034- } \\ \text { XXX(3/8) } \end{gathered}$ | B | No | No | Inside Pole | $\begin{gathered} 110.0000- \\ 0.0000 \end{gathered}$ | 2 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 0.06 \\ & 0.06 \\ & 0.06 \\ & 0.06 \end{aligned}$ |
| WR-VG86STBRD(3/4) | B | No | No | Inside Pole | $\begin{gathered} 110.0000- \\ 0.0000 \end{gathered}$ | 4 | No Ice 1/2" Ice 1 " Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 0.58 \\ & 0.58 \\ & 0.58 \\ & 0.58 \end{aligned}$ |
| 2" (Nominal) Conduit | B | No | No | Inside Pole | $\begin{gathered} 110.0000- \\ 0.0000 \end{gathered}$ | 2 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 0.0000 \\ & 0.0000 \\ & 0.0000 \\ & 0.0000 \end{aligned}$ | $\begin{aligned} & 0.72 \\ & 0.72 \\ & 0.72 \\ & 0.72 \end{aligned}$ |

Feed Line/Linear Appurtenances Section Areas

\begin{tabular}{|c|c|c|c|c|c|c|c|}
\hline Tower Sectio n \& Tower Elevation ft \& Face \& $A_{R}$

$f t^{2}$ \& AF

$f t^{2}$ \& $C_{A} A_{A}$ In Face $f t^{2}$ \& $$
\begin{gathered}
C_{A} A_{A} \\
\text { Out Face } \\
{f t^{2}}^{2} \\
\hline
\end{gathered}
$$ \& Weight

K <br>
\hline \multirow[t]{3}{*}{L1} \& 147.0000- \& A \& 0.000 \& 0.000 \& 0.000 \& 0.000 \& 0.00 <br>
\hline \& 99.5000 \& B \& 0.000 \& 0.000 \& 4.257 \& 0.000 \& 0.39 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 5.444 \& 0.000 \& 0.19 <br>
\hline \multirow[t]{3}{*}{L2} \& 99.5000-59.0000 \& A \& 0.000 \& 0.000 \& 7.806 \& 0.000 \& 0.00 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 15.825 \& 0.000 \& 1.01 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 12.447 \& 0.000 \& 0.17 <br>
\hline \multirow[t]{3}{*}{L3} \& 59.0000-29.2500 \& A \& 0.000 \& 0.000 \& 30.398 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 33.570 \& 0.000 \& 0.74 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 31.089 \& 0.000 \& 0.12 <br>
\hline \multirow[t]{3}{*}{L4} \& 29.2500-0.0000 \& A \& 0.000 \& 0.000 \& 47.274 \& 0.000 \& 0.01 <br>
\hline \& \& B \& 0.000 \& 0.000 \& 49.409 \& 0.000 \& 0.73 <br>
\hline \& \& C \& 0.000 \& 0.000 \& 46.970 \& 0.000 \& 0.12 <br>
\hline
\end{tabular}

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Sectio n | Tower Elevation ft | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Ice Thickness in | $A_{R}$ $f t^{2}$ | $\begin{aligned} & A_{F} \\ & f t^{2} \end{aligned}$ | $C_{A} A_{A}$ In Face $f t^{2}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ \text { ft }^{2} \end{gathered}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $\begin{gathered} 147.0000- \\ 99.5000 \end{gathered}$ | A | 1.453 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 10.506 | 0.000 | 0.52 |
|  |  | C |  | 0.000 | 0.000 | 24.063 | 0.000 | 0.46 |
| L2 | 99.5000-59.0000 | A | 1.391 | 0.000 | 0.000 | 9.398 | 0.000 | 0.10 |
|  |  | B |  | 0.000 | 0.000 | 29.189 | 0.000 | 1.36 |
|  |  | C |  | 0.000 | 0.000 | 29.915 | 0.000 | 0.50 |
| L3 | 59.0000-29.2500 | A | 1.312 | 0.000 | 0.000 | 51.632 | 0.000 | 0.50 |
|  |  | B |  | 0.000 | 0.000 | 50.979 | 0.000 | 1.26 |
|  |  | C |  | 0.000 | 0.000 | 51.419 | 0.000 | 0.63 |
| L4 | 29.2500-0.0000 | A | 1.173 | 0.000 | 0.000 | 76.981 | 0.000 | 0.69 |
|  |  | B |  | 0.000 | 0.000 | 71.444 | 0.000 | 1.38 |
|  |  | C |  | 0.000 | 0.000 | 71.761 | 0.000 | 0.76 |

Feed Line Center of Pressure

| Section | Elevation | $C P_{X}$ | $C P_{z}$ | $C P_{X}$ <br> $I c e$ <br>  | ft |
| :---: | :---: | :---: | :---: | :---: | :---: |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

## Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} \hline K_{a} \\ \text { No lce } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & I c e \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 6 | 7983A(ELLIPTICAL) | $\begin{aligned} & 99.50- \\ & 147.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L1 | 10 | HB158-1-08U8-S8F18(1 $\left.5 / 8^{\prime \prime}\right)$ | $\begin{aligned} & 99.50- \\ & 121.00 \end{aligned}$ | 1.0000 | 1.0000 |
| L1 | 28 | MP3-04 (L) | $\begin{array}{r} 99.50- \\ 71.00 \end{array}$ | 1.0000 | 1.0000 |
| L1 | 29 | MP3-04 (L) | $\begin{array}{r} 99.50 \\ 71.00 \end{array}$ | 1.0000 | 1.0000 |
| L1 | 30 | MP3-04 (L) | $99.50-$ | 1.0000 | 1.0000 |
| L2 | 6 | 7983A(ELLIPTICAL) | $\begin{array}{r} 59.00- \\ 99.50 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 10 | HB158-1-08U8-S8F18(1 $\left.5 / 8^{\prime \prime}\right)$ | $59.00-$ 99.50 | 1.0000 | 1.0000 |
| L2 | 19 | LDF4-50A(1/2) | $\begin{array}{r} 59.00- \\ 53.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 20 | LDF4-50A(1/2) | $\begin{array}{r} 59.00- \\ 49.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 25 | MP3-04 (L) | $\begin{array}{r} 59.00- \\ 52.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 26 | MP3-04 (L) | $\begin{array}{r} 59.00- \\ 52.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 27 | MP3-04 (L) | $\begin{array}{r} 59.00- \\ 52.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 31 | MP3-04 (L) | $\begin{array}{r} 59.00- \\ 35.50 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 32 | MP3-04 (L) | $\begin{array}{r} 59.00 \\ 35.50 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 33 | MP3-04 (L) | $59.00-$ 35.50 | 1.0000 | 1.0000 |
| L2 | 34 | MP3-03 (L) | $\begin{array}{r} 59.00- \\ 59.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 35 | MP3-03 (L) | $\begin{array}{r} 59.00- \\ 59.00 \end{array}$ | 1.0000 | 1.0000 |
| L2 | 36 | MP3-03 (L) | $\begin{array}{r} 59.00- \\ 59.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 6 | 7983A(ELLIPTICAL) | $\begin{array}{r} 29.25- \\ 59.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 10 | HB158-1-08U8-S8F18(1 5/8") | $\begin{array}{r} 29.25- \\ 59.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 19 | LDF4-50A(1/2) | $\begin{array}{r} 29.25- \\ 53.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 20 | LDF4-50A(1/2) | $\begin{array}{r} 29.25- \\ 49.00 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 22 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 25.50 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 23 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 25.50 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 24 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 25.50 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 31 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 35.50 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 32 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 35.50 \end{array}$ | 1.0000 | 1.0000 |
| L3 | 33 | MP3-04 (L) | $\begin{array}{r} 29.25- \\ 35.50 \end{array}$ | 1.0000 | 1.0000 |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\) Side \(f t^{2}\) \& Weight

K <br>

\hline $$
\begin{gathered}
\text { Top Hat 10" Diameter } \times 4 \text { ' } \\
\text { 6" Tall }
\end{gathered}
$$ \& C \& None \& \& 0.00 \& 147.0000 \& \[

$$
\begin{gathered}
\text { No Ice } \\
\text { 1/2" } \\
\text { Ice } \\
1 " \text { Ice } \\
2 " \text { Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 2.1167 \\
& 3.1744 \\
& 3.4914 \\
& 4.1531
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.1167 \\
& 3.1744 \\
& 3.4914 \\
& 4.1531
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.20 \\
& 0.23 \\
& 0.27 \\
& 0.35
\end{aligned}
$$
\] <br>

\hline APXVSPP18-C-A20 w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 4.6000 \\
& 5.0500 \\
& 5.5000 \\
& 6.4400
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.0100 \\
& 4.4500 \\
& 4.8900 \\
& 5.8200
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.10 \\
& 0.16 \\
& 0.23 \\
& 0.42
\end{aligned}
$$
\] <br>

\hline APXVSPP18-C-A20 w/ Mount Pipe \& B \& From Leg \& \[
$$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$

\] \& 0.00 \& 147.0000 \& | No Ice |
| :--- |
| 1/2" |
| Ice |
| 1" Ice |
| 2" Ice | \& \[

$$
\begin{aligned}
& 4.6000 \\
& 5.0500 \\
& 5.5000 \\
& 6.4400
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.0100 \\
& 4.4500 \\
& 4.8900 \\
& 5.8200
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.10 \\
& 0.16 \\
& 0.23 \\
& 0.42
\end{aligned}
$$
\] <br>

\hline APXVTM14-C-120 w/ Mount Pipe \& A \& From Leg \& \[
$$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$

\] \& 0.00 \& 147.0000 \& | No Ice |
| :--- |
| 1/2" |
| Ice |
| 1" Ice |
| 2" Ice | \& \[

$$
\begin{aligned}
& 4.0900 \\
& 4.4800 \\
& 4.8800 \\
& 5.7100
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.8600 \\
& 3.2300 \\
& 3.6100 \\
& 4.4000
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.13 \\
& 0.19 \\
& 0.33
\end{aligned}
$$
\] <br>

\hline APXVTM14-C-120 w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 4.0900 \\
& 4.4800 \\
& 4.8800 \\
& 5.7100
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.8600 \\
& 3.2300 \\
& 3.6100 \\
& 4.4000
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.13 \\
& 0.19 \\
& 0.33
\end{aligned}
$$
\] <br>

\hline APXVTM14-C-120 w/ Mount Pipe \& C \& From Leg \& \[
$$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$

\] \& 0.00 \& 147.0000 \& | No Ice |
| :--- |
| 1/2" |
| Ice |
| 1" Ice |
| 2" Ice | \& \[

$$
\begin{aligned}
& 4.0900 \\
& 4.4800 \\
& 4.8800 \\
& 5.7100
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 2.8600 \\
& 3.2300 \\
& 3.6100 \\
& 4.4000
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.08 \\
& 0.13 \\
& 0.19 \\
& 0.33
\end{aligned}
$$
\] <br>

\hline TD-RRH8x20-25 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 4.0455 \\
& 4.2975 \\
& 4.5570 \\
& 5.0981
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.5345 \\
& 1.7142 \\
& 1.9008 \\
& 2.2951
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.10 \\
& 0.13 \\
& 0.20
\end{aligned}
$$
\] <br>

\hline TD-RRH8x20-25 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 4.0455 \\
& 4.2975 \\
& 4.5570 \\
& 5.0981
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.5345 \\
& 1.7142 \\
& 1.9008 \\
& 2.2951
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.10 \\
& 0.13 \\
& 0.20
\end{aligned}
$$
\] <br>

\hline TD-RRH8x20-25 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 4.0455 \\
& 4.2975 \\
& 4.5570 \\
& 5.0981
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.5345 \\
& 1.7142 \\
& 1.9008 \\
& 2.2951
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.10 \\
& 0.13 \\
& 0.20
\end{aligned}
$$
\] <br>

\hline (3) ACU-A20-N \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.0667 \\
& 0.1037 \\
& 0.1481 \\
& 0.2593
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1167 \\
& 0.1620 \\
& 0.2148 \\
& 0.3426
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00 \\
& 0.01
\end{aligned}
$$
\] <br>

\hline (3) ACU-A20-N \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.0667 \\
& 0.1037 \\
& 0.1481 \\
& 0.2593
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1167 \\
& 0.1620 \\
& 0.2148 \\
& 0.3426
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00 \\
& 0.01
\end{aligned}
$$
\] <br>

\hline (3) ACU-A20-N \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.0667 \\
& 0.1037 \\
& 0.1481 \\
& 0.2593
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1167 \\
& 0.1620 \\
& 0.2148 \\
& 0.3426
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.00 \\
& 0.00 \\
& 0.00 \\
& 0.01
\end{aligned}
$$
\] <br>

\hline P40-16-XLPP-RR-A w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 147.0000 \& \[

$$
\begin{gathered}
\text { No Ice } \\
\text { 1/2" } \\
\text { Ice } \\
1 \text { " Ice }
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
8.2425 \\
8.7006 \\
9.1551 \\
10.0902
\end{gathered}
$$

\] \& \[

$$
\begin{aligned}
& 4.8250 \\
& 5.5706 \\
& 6.2654 \\
& 7.6723
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.14 \\
& 0.21 \\
& 0.37
\end{aligned}
$$
\] <br>

\hline
\end{tabular}



\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen \(t\) \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{A} A_{A}\) Side
\[
f t^{2}
\] \& Weight

K <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 2.9201 \& 2.5100 \& 0.16 <br>

\hline Side Arm Mount [SO 1023] \& B \& None \& \& 0.00 \& 145.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& $$
\begin{aligned}
& 3.6000 \\
& 4.1800 \\
& 4.7500 \\
& 5.9000
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 3.6000 \\
& 4.1800 \\
& 4.7500 \\
& 5.9000
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.07 \\
& 0.11 \\
& 0.14 \\
& 0.20
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A \& A \& \& \& 0.00 \& 121.0000 \& \& \& \& 0.11 <br>

\hline B4P w/ Mount Pipe \& A \& From Leg \& $$
\begin{aligned}
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.00 \& 121.0000 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& \text { 1/2" } \\
& \text { Ice } \\
& \text { 1" Ice } \\
& 2 " \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.3292 \\
& 6.7751 \\
& 7.2137 \\
& 8.1168
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6424 \\
& 6.4259 \\
& 7.1313 \\
& 8.5907
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A B4P w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.3292 \\
& 6.7751 \\
& 7.2137 \\
& 8.1168
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6424 \\
& 6.4259 \\
& 7.1313 \\
& 8.5907
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B2A B4P w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.3292 \\
& 6.7751 \\
& 7.2137 \\
& 8.1168
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6424 \\
& 6.4259 \\
& 7.1313 \\
& 8.5907
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B4A B2P w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.3186 \\
& 6.7646 \\
& 7.2032 \\
& 8.1062
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6334 \\
& 6.4160 \\
& 7.1208 \\
& 8.5791
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B4A B2P w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.3186 \\
& 6.7646 \\
& 7.2032 \\
& 8.1062
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6334 \\
& 6.4160 \\
& 7.1208 \\
& 8.5791
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline ERICSSON AIR 21 B4A B2P w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 6.3186 \\
& 6.7646 \\
& 7.2032 \\
& 8.1062
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 5.6334 \\
& 6.4160 \\
& 7.1208 \\
& 8.5791
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.11 \\
& 0.17 \\
& 0.23 \\
& 0.38
\end{aligned}
$$
\] <br>

\hline APXVAARR24_43-U-NA20 w/ Mount Pipe \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
4.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 14.6900 \\
& 15.4600 \\
& 16.2300 \\
& 17.8200
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.8700 \\
& 7.5500 \\
& 8.2500 \\
& 9.6700
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.19 \\
& 0.31 \\
& 0.46 \\
& 0.79
\end{aligned}
$$
\] <br>

\hline APXVAARR24_43-U-NA20 w/ Mount Pipe \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
4.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 14.6900 \\
& 15.4600 \\
& 16.2300 \\
& 17.8200
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.8700 \\
& 7.5500 \\
& 8.2500 \\
& 9.6700
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.19 \\
& 0.31 \\
& 0.46 \\
& 0.79
\end{aligned}
$$
\] <br>

\hline APXVAARR24_43-U-NA20 w/ Mount Pipe \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
4.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 14.6900 \\
& 15.4600 \\
& 16.2300 \\
& 17.8200
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.8700 \\
& 7.5500 \\
& 8.2500 \\
& 9.6700
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.19 \\
& 0.31 \\
& 0.46 \\
& 0.79
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& A \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.3500 \\
& 0.4259 \\
& 0.5093 \\
& 0.6981
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1750 \\
& 0.2343 \\
& 0.3009 \\
& 0.4565
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01 \\
& 0.02 \\
& 0.03
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& B \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" Ice 1" Ice 2" Ice \& \[

$$
\begin{aligned}
& 0.3500 \\
& 0.4259 \\
& 0.5093 \\
& 0.6981
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1750 \\
& 0.2343 \\
& 0.3009 \\
& 0.4565
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01 \\
& 0.02 \\
& 0.03
\end{aligned}
$$
\] <br>

\hline KRY 112 144/1 \& C \& From Leg \& $$
\begin{gathered}
4.0000 \\
0.00
\end{gathered}
$$ \& 0.00 \& 121.0000 \& No Ice 1/2" \& \[

$$
\begin{aligned}
& 0.3500 \\
& 0.4259
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.1750 \\
& 0.2343
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.01 \\
& 0.01
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& Offsets: Horz Lateral Vert ft ft ft \& \begin{tabular}{l}
Azimuth Adjustmen \(t\) \\
0
\end{tabular} \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
f t^{2}
$$ \& $C_{A} A_{A}$ Side

$$
f t^{2}
$$ \& Weight <br>

\hline \multirow{5}{*}{RADIO 4449 B12/B71} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& 0.00 \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{121.0000} \& Ice \& 0.5093 \& 0.3009 \& 0.02 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 0.6981 \& 0.4565 \& 0.03 <br>

\hline \& \& \& 4.0000 \& \& \& No Ice \& 1.6500 \& 1.1625 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.8104 \& 1.3012 \& 0.09 <br>
\hline \& \& \& 4.00 \& \& \& Ice \& 1.9781 \& 1.4473 \& 0.11 <br>
\hline \multirow{6}{*}{RADIO 4449 B12/B71} \& \multirow{6}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{121.0000} \& 1" Ice \& 2.3359 \& 1.7618 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 1.6500 \& 1.1625 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.8104 \& 1.3012 \& 0.09 <br>
\hline \& \& \& 4.00 \& \& \& Ice \& 1.9781 \& 1.4473 \& 0.11 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{121.0000} \& 1 " Ice \& 2.3359 \& 1.7618 \& 0.16 <br>
\hline \multirow{5}{*}{RADIO 4449 B12/B71} \& \multirow{4}{*}{C} \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 1.6500 \& 1.1625 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.8104 \& 1.3012 \& 0.09 <br>
\hline \& \& \& 4.00 \& \& \& Ice \& 1.9781 \& 1.4473 \& 0.11 <br>
\hline \& \multirow{7}{*}{C} \& \multirow{7}{*}{None} \& \& \multirow{6}{*}{0.00} \& \multirow{6}{*}{121.0000} \& 1" Ice \& 2.3359 \& 1.7618 \& 0.16 <br>
\hline \multirow{5}{*}{Platform Mount [LP 3011_KCKR]} \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& \& \& \& No Ice \& 35.0300 \& 35.0300 \& 1.86 <br>
\hline \& \& \& \& \& \& 1/2" \& 44.4600 \& 44.4600 \& 2.52 <br>
\hline \& \& \& \& \& \& Ice \& 53.7200 \& 53.7200 \& 3.33 <br>
\hline \& \& \& \& \& \& 1" Ice \& 72.2900 \& 72.2900 \& 5.42 <br>
\hline \multirow{5}{*}{7770.00 w/ Mount Pipe} \& \& \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{110.0000} \& 2" Ice \& \& \& <br>
\hline \& \multirow{4}{*}{A} \& \multirow{4}{*}{From Leg} \& \& \& \& \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 5.7460 \& 4.2543 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.1791 \& 5.0137 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 6.6067 \& 5.7109 \& 0.16 <br>
\hline \multirow{5}{*}{7770.00 w/ Mount Pipe} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{110.0000} \& 1" Ice \& 7.4880 \& 7.1553 \& 0.29 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 5.7460 \& 4.2543 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.1791 \& 5.0137 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 6.6067 \& 5.7109 \& 0.16 <br>
\hline \multirow{5}{*}{7770.00 w/ Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{110.0000} \& 1" Ice \& 7.4880 \& 7.1553 \& 0.29 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 5.7460 \& 4.2543 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 6.1791 \& 5.0137 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 6.6067 \& 5.7109 \& 0.16 <br>
\hline \multirow{5}{*}{(3) SBNHH-1D65A w/ Mount Pipe} \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{5}{*}{110.0000} \& 1" Ice \& 7.4880 \& 7.1553 \& 0.29 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 3.0400 \& 2.4500 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.3400 \& 2.7500 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.6500 \& 3.0500 \& 0.16 <br>
\hline \multirow{5}{*}{(3) SBNHH-1D65A w/ Mount Pipe} \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \multirow{6}{*}{110.0000} \& 1 " Ice \& 4.3100 \& 3.6800 \& 0.31 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 3.0400 \& 2.4500 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.3400 \& 2.7500 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.6500 \& 3.0500 \& 0.16 <br>
\hline \multirow{6}{*}{(3) SBNHH-1D65A w/ Mount Pipe} \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \& 1" Ice \& 4.3100 \& 3.6800 \& 0.31 <br>
\hline \& \& \& \& \& \multirow{5}{*}{110.0000} \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 3.0400 \& 2.4500 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 3.3400 \& 2.7500 \& 0.10 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 3.6500 \& 3.0500 \& 0.16 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.00} \& \& 1" Ice \& 4.3100 \& 3.6800 \& 0.31 <br>
\hline \multirow{4}{*}{(2) LGP2140X} \& \& \& \& \& \multirow{4}{*}{110.0000} \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 1.0800 \& 0.3580 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.2137 \& 0.4536 \& 0.02 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 1.3548 \& 0.5563 \& 0.03 <br>
\hline \multirow{6}{*}{(2) LGP2140X} \& \multirow{6}{*}{B} \& \multirow{6}{*}{From Leg} \& \& \multirow{6}{*}{0.00} \& \multirow{6}{*}{110.0000} \& 1" Ice \& 1.6593 \& 0.7825 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline \& \& \& 4.0000 \& \& \& No Ice \& 1.0800 \& 0.3580 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" \& 1.2137 \& 0.4536 \& 0.02 <br>
\hline \& \& \& 2.00 \& \& \& Ice \& 1.3548 \& 0.5563 \& 0.03 <br>
\hline \& \& \& \& \& \& 1" Ice \& 1.6593 \& 0.7825 \& 0.05 <br>
\hline \& \& \& \& \& \& 2" Ice \& \& \& <br>
\hline (2) LGP2140X \& C \& From Leg \& 4.0000 \& 0.00 \& 110.0000 \& No Ice \& 1.0800 \& 0.3580 \& 0.01 <br>
\hline
\end{tabular}




\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& $$
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
$$ \& Offset Type \& Offsets: Horz Lateral Vert ft ft ft \& Azimuth Adjustmen $t$ \& Placement

ft \& \& $C_{A} A_{A}$ Front

$$
f t^{2}
$$ \& $C_{A} A_{A}$ Side $f t^{2}$ \& Weight <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& \text { 1" Ice } \\
& \text { 2" Ice }
\end{aligned}
$$ \& 2.0100 \& 4.3500 \& 0.12 <br>

\hline
\end{tabular}

| Dishes |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Dish <br> Type | Offset Type | Offsets: Horz Lateral Vert ft | Azimuth Adjustment | $3 d B$ <br> Beam <br> Width | Elevation | Outside Diameter |  | Aperture Area <br> $f t^{2}$ | Weight |
| A-ANT-23G-2-C | A | Paraboloid w/o Radome | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 |  | 147.0000 | 2.1750 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 3.7200 \\ & 4.0100 \\ & 4.3000 \\ & 4.8800 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \\ & 0.03 \\ & 0.04 \end{aligned}$ |
| A-ANT-23G-2-C | B | Paraboloid w/o Radome | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | 0.00 |  | 147.0000 | 2.1750 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 3.7200 \\ & 4.0100 \\ & 4.3000 \\ & 4.8800 \end{aligned}$ | $\begin{aligned} & 0.01 \\ & 0.02 \\ & 0.03 \\ & 0.04 \end{aligned}$ |
| VHLP2-18 | C | Paraboloid w/o Radome | From Leg | $\begin{gathered} 4.0000 \\ 0.00 \\ 2.00 \end{gathered}$ | -60.00 |  | 147.0000 | 2.1750 | No Ice 1/2" Ice 1" Ice 2" Ice | $\begin{aligned} & 3.7200 \\ & 4.0100 \\ & 4.3000 \\ & 4.8800 \end{aligned}$ | $\begin{aligned} & 0.03 \\ & 0.05 \\ & 0.07 \\ & 0.11 \end{aligned}$ |

## Tower Pressures - No Ice

$G_{H}=1.100$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation ft \& \(z\)
ft \& \(K_{z}\) \& \begin{tabular}{l}
\(q_{z}\) \\
psf
\end{tabular} \& A \& F
\(a\)
\(c\)
\(e\) \& \(A_{F}\)

$f t^{2}$ \& $A_{R}$

$f t^{2}$ \& $A_{\text {leg }}$

$f t^{2}$ \& \[
$$
\begin{gathered}
\mathrm{Leg} \\
\%
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\ln \\
\text { Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& $C_{A} A_{A}$ Out Face $f t^{2}$ <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\hline \text { L1 } 147.0000- \\
99.5000
\end{array}
$$} \& \multirow[t]{3}{*}{122.2279} \& \multirow[t]{3}{*}{1.32} \& \multirow[t]{3}{*}{51.38} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{r}
106.83 \\
9
\end{array}
$$
\]} \& A \& 0.000 \& 106.839 \& 106.839 \& 100.00 \& 0.000 \& 0.000 <br>

\hline \& \& \& \& \& B \& 0.000 \& 106.839 \& \& 100.00 \& 4.257 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 106.839 \& \& 100.00 \& 5.444 \& 0.000 <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\text { L2 99.5000- } \\
59.0000
\end{array}
$$} \& \multirow[t]{3}{*}{78.8041} \& \multirow[t]{3}{*}{1.204} \& \multirow[t]{3}{*}{46.80} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{r}
116.17 \\
7
\end{array}
$$
\]} \& A \& 0.000 \& 116.177 \& 116.177 \& 100.00 \& 7.806 \& 0.000 <br>

\hline \& \& \& \& \& B \& 0.000 \& 116.177 \& \& 100.00 \& 15.825 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 116.177 \& \& 100.00 \& 12.447 \& 0.000 <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\text { L3 59.0000- } \\
29.2500
\end{array}
$$} \& \multirow[t]{3}{*}{43.7930} \& \multirow[t]{3}{*}{1.064} \& \multirow[t]{3}{*}{41.45} \& \multirow[t]{3}{*}{99.457} \& A \& 0.000 \& 99.457 \& 99.457 \& 100.00 \& 30.398 \& 0.000 <br>

\hline \& \& \& \& \& B \& 0.000 \& 99.457 \& \& 100.00 \& 33.570 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 99.457 \& \& 100.00 \& 31.089 \& 0.000 <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\text { L4 } 29.2500- \\
0.0000
\end{array}
$$} \& \multirow[t]{3}{*}{14.3368} \& \multirow[t]{3}{*}{0.85} \& \multirow[t]{3}{*}{33.12} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{r}
108.86 \\
7
\end{array}
$$
\]} \& A \& 0.000 \& 108.867 \& 108.867 \& 100.00 \& 47.274 \& 0.000 <br>

\hline \& \& \& \& \& B \& 0.000 \& 108.867 \& \& 100.00 \& 49.409 \& 0.000 <br>
\hline \& \& \& \& \& C \& 0.000 \& 108.867 \& \& 100.00 \& 46.970 \& 0.000 <br>
\hline
\end{tabular}

## Tower Pressure - With Ice

$G_{H}=1.100$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation ft \& $Z$
$f t$ \& $K_{z}$ \& $q_{z}$

$p s f$ \& $t_{z}$
in \& AG

$f t^{2}$ \& F
$a$
$c$
$e$ \& $A_{F}$

$f t^{2}$ \& $A_{R}$

$f t^{2}$ \& $A_{l e g}$

$f t^{2}$ \& \[
$$
\begin{gathered}
\mathrm{Leg} \\
\%
\end{gathered}
$$

\] \& \[

$$
\begin{gathered}
C_{A} A_{A} \\
\operatorname{In} \\
\text { Face } \\
{f t^{2}}^{2}
\end{gathered}
$$
\] \& $C_{A} A_{A}$ Out Face $f t^{2}$ <br>

\hline L1 147.0000- \& \multirow[t]{3}{*}{122.2279} \& \multirow[t]{3}{*}{1.32} \& \multirow[t]{3}{*}{7.60} \& \multirow[t]{3}{*}{1.4534} \& \multirow[t]{3}{*}{118.345} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \mathrm{A} \\
& \mathrm{~B} \\
& \mathrm{C}
\end{aligned}
$$} \& 0.000 \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 118.345 \\
& 118.345
\end{aligned}
$$
\]} \& \multirow[t]{2}{*}{118.345} \& 100.00 \& 0.000 \& 0.000 <br>

\hline 99.5000 \& \& \& \& \& \& \& 0.000 \& \& \& 100.00 \& 10.506 \& 0.000 <br>
\hline \& \& \& \& \& \& \& 0.000 \& 118.345 \& \& 100.00 \& 24.063 \& 0.000 <br>
\hline L2 99.5000- \& \multirow[t]{3}{*}{78.8041} \& \multirow[t]{3}{*}{1.204} \& \multirow[t]{3}{*}{6.92} \& \multirow[t]{3}{*}{1.3910} \& \multirow[t]{3}{*}{125.988} \& A \& 0.000 \& 125.988 \& \& 100.00 \& 9.398 \& 0.000 <br>
\hline 59.0000 \& \& \& \& \& \& B \& 0.000 \& 125.988 \& 125.988 \& 100.00 \& 29.189 \& 0.000 <br>

\hline \& \& \& \& \& \& C \& 0.000 \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 125.988 \\
& 106.354
\end{aligned}
$$} \& \& \multirow[t]{2}{*}{\[

100.00
\]} \& 29.915 \& 0.000 <br>

\hline L3 59.0000- \& \multirow[t]{3}{*}{43.7930} \& \multirow[t]{3}{*}{1.064} \& \multirow[t]{3}{*}{6.13} \& \multirow[t]{3}{*}{1.3116} \& \multirow[t]{3}{*}{106.354} \& A \& 0.000 \& \& \multirow[t]{2}{*}{106.354} \& \& 51.632 \& 0.000 <br>

\hline 29.2500 \& \& \& \& \& \& B \& 0.000 \& 106.354 \& \& $$
\begin{aligned}
& 100.00 \\
& 100.00
\end{aligned}
$$ \& 50.979 \& 0.000 <br>

\hline \& \& \& \& \& \& C \& 0.000 \& 106.354 \& \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 100.00 \\
& 100.00
\end{aligned}
$$} \& 51.419 \& \multirow[t]{2}{*}{0.000} <br>

\hline L4 29.2500- \& \multirow[t]{3}{*}{14.3368} \& \multirow[t]{3}{*}{0.85} \& \multirow[t]{3}{*}{4.90} \& \multirow[t]{3}{*}{1.1730} \& \multirow[t]{3}{*}{115.261} \& A \& 0.000 \& 115.261 \& \multirow[t]{3}{*}{115.261} \& \& 76.981 \& <br>

\hline 0.0000 \& \& \& \& \& \& B \& 0.000 \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 115.261 \\
& 115.261
\end{aligned}
$$} \& \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 100.00 \\
& 100.00
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 71.444 \\
& 71.761
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 0.000 \\
& 0.000
\end{aligned}
$$
\]} <br>

\hline \& \& \& \& \& \& C \& 0.000 \& \& \& \& \& <br>
\hline
\end{tabular}

## Tower Pressure - Service

$G_{H}=1.100$

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|c|c|}
\hline Section Elevation ft \& z \& $K_{z}$ \& $q_{z}$
psf \& AG

$f t^{2}$ \& F
a
$c$
$c$
$e$ \& $A_{F}$

$f t^{2}$ \& $A_{R}$

$f t^{2}$ \& $A_{\text {leg }}$

$f t^{2}$ \& \[
$$
\begin{gathered}
\mathrm{Leg} \\
\%
\end{gathered}
$$

\] \& | $C_{A} A_{A}$ In |
| :--- |
| Face |
| $f t^{2}$ | \& | $C_{A} A_{A}$ Out |
| :--- |
| Face |
| $\mathrm{ft}^{2}$ | <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\hline \text { L1 } 147.0000- \\
99.5000
\end{array}
$$} \& \multirow[t]{3}{*}{122.2279} \& \multirow[t]{3}{*}{1.32} \& \multirow[t]{3}{*}{10.31} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{r}
\hline 106.83 \\
9
\end{array}
$$
\]} \& \multirow[t]{2}{*}{A} \& 0.000 \& 106.839 \& \multirow[t]{2}{*}{106.839} \& 100.00 \& 0.000 \& 0.000 <br>

\hline \& \& \& \& \& \& 0.000 \& 106.839 \& \& 100.00 \& 4.257 \& 0.000 <br>

\hline \& \& \& \& \& C \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 0.000 \\
& 0.000
\end{aligned}
$$} \& 106.839 \& \multirow{3}{*}{116.177} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 100.00 \\
& 100.00
\end{aligned}
$$
\]} \& 5.444 \& 0.000 <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\text { L2 99.5000- } \\
59.0000
\end{array}
$$} \& \multirow[t]{3}{*}{78.8041} \& \multirow[t]{3}{*}{1.204} \& \multirow[t]{3}{*}{9.39} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{r}
116.17 \\
7
\end{array}
$$
\]} \& \multirow[t]{2}{*}{A} \& \& 116.177 \& \& \& 7.806 \& 0.000 <br>

\hline \& \& \& \& \& \& $$
\begin{aligned}
& 0.000 \\
& 0.000
\end{aligned}
$$ \& 116.177 \& \& 100.00 \& 15.825 \& 0.000 <br>

\hline \& \& \& \& \& B
C
A \& 0.000 \& 116.177 \& \& 100.00 \& 12.447 \& 0.000 <br>

\hline \multirow[t]{3}{*}{$$
\begin{array}{r}
\text { L3 59.0000- } \\
29.2500
\end{array}
$$} \& \multirow[t]{3}{*}{43.7930} \& \multirow[t]{3}{*}{1.064} \& \multirow[t]{3}{*}{8.32} \& \multirow[t]{3}{*}{99.457} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{0.000

0.000} \& 99.457 \& \multirow[t]{2}{*}{$$
99.457
$$} \& 100.00 \& 30.398 \& 0.000 <br>

\hline \& \& \& \& \& \& \& 99.457 \& \& \multirow[t]{2}{*}{$$
\begin{aligned}
& 100.00 \\
& 100.00
\end{aligned}
$$} \& 33.570 \& 0.000 <br>

\hline \& \& \& \& \& B \& $$
\begin{aligned}
& 0.000 \\
& 0.000
\end{aligned}
$$ \& 99.457 \& \multirow[t]{4}{*}{\[

108.867
\]} \& \& 31.089 \& 0.000 <br>

\hline L4 29.2500- \& \multirow[t]{3}{*}{14.3368} \& \multirow[t]{3}{*}{0.85} \& \multirow[t]{3}{*}{6.64} \& \multirow[t]{3}{*}{$$
\begin{array}{r}
108.86 \\
7
\end{array}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{array}{|l|}
\mathrm{A} \\
\mathrm{~B} \\
\mathrm{C} \\
\hline
\end{array}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 0.000 \\
& 0.000 \\
& 0.000
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{108.867 108.867 108.867} \& \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 100.00 \\
& 100.00 \\
& 100.00
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 47.274 \\
& 49.409 \\
& 46.970
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 0.000 \\
& 0.000 \\
& 0.000
\end{aligned}
$$
\]} <br>

\hline 0.0000 \& \& \& \& \& \& \& \& \& \& \& <br>
\hline \& \& \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}

## Load Combinations

| Comb No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Dead+1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |


| Comb. No. | Description |
| :---: | :---: |
| 24 | 1.2 Dead+1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 29 | 1.2 Dead+1.0 Wind $60 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp |
| 32 | 1.2 Dead+1.0 Wind $150 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 33 | 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind $210 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 35 | 1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp |
| 38 | 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg - Service |

## Maximum Member Forces

| Sectio | Elevation |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $n$ | ft | Component | Type |
| :---: |
| No. |

## Maximum Reactions

| Location | Condition | Gov. <br> Load <br> Comb. | Vertical <br> $K$ | Horizontal, $X$ <br>  <br> Pole | Max. Vert |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 26 | 21 | 72.34 | Horizontal, $Z$ <br> K |
|  | ${\text { Max. } \mathrm{H}_{\mathrm{z}}}^{\text {Max. } \mathrm{M}_{\mathrm{x}}}$ | 3 | 32.01 | -0.00 |  |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 2 | 32.01 | 36.96 | -0.00 |
|  | Max. Torsion | 5 | 3719.31 | 0.21 | 0.10 |
|  | Min. Vert | 15 | 3664.93 | 0.21 | 38.40 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 9 | 1.48 | -38.14 | 38.40 |
|  | Min. $\mathrm{H}_{\mathrm{z}}$ | 15 | 32.01 | -18.52 | 0.06 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | 32.01 | 0.04 | 32.30 |
|  | Min. $\mathrm{M}_{\mathrm{z}}$ | 20 | -32.01 | -38.14 | -37.16 |
|  | Min. Torsion | 11 | -3623.09 | 0.04 | 0.06 |
|  |  | -0.56 | -37.16 |  |  |
|  |  |  | 36.96 | -37.16 |  |
|  |  |  | -33.02 | 0.10 |  |
|  |  |  |  | -19.35 |  |
|  |  |  |  |  |  |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> K | Shear $_{x}$ K | Shear $_{z}$ K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 35.56 | 0.00 | -0.00 | -0.15 | -0.40 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg No Ice | 42.68 | -0.21 | -38.40 | -3719.31 | 33.66 | -1.21 |
| 0.9 Dead+1.0 Wind 0 deg No Ice | 32.01 | -0.21 | -38.40 | -3669.60 | 33.23 | -1.21 |
| 1.2 Dead+1.0 Wind 30 deg No Ice | 42.68 | 18.52 | -32.30 | -3165.33 | -1807.15 | -1.48 |
| 0.9 Dead+1.0 Wind 30 deg No Ice | 32.01 | 18.52 | -32.30 | -3122.68 | -1782.75 | -1.48 |
| 1.2 Dead+1.0 Wind 60 deg No Ice | 42.68 | 31.97 | -18.79 | -1859.54 | -3130.11 | -1.46 |
| 0.9 Dead+1.0 Wind 60 deg No Ice | 32.01 | 31.97 | -18.79 | -1834.34 | -3087.93 | -1.46 |
| 1.2 Dead+1.0 Wind 90 deg No Ice | 42.68 | 38.14 | -0.06 | -9.77 | -3664.93 | 0.30 |
| 0.9 Dead+1.0 Wind 90 deg No Ice | 32.01 | 38.14 | -0.06 | -9.56 | -3616.19 | 0.30 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice | 42.68 | 33.02 | 19.35 | 1881.22 | -3179.17 | 0.56 |
| 0.9 Dead+1.0 Wind 120 deg <br> - No Ice | 32.01 | 33.02 | 19.35 | 1856.06 | -3136.70 | 0.56 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No Ice | 42.68 | 18.38 | 32.19 | 3166.79 | -1796.66 | 0.54 |
| 0.9 Dead+1.0 Wind 150 deg <br> - No Ice | 32.01 | 18.38 | 32.19 | 3124.17 | -1772.42 | 0.54 |
| 1.2 Dead+1.0 Wind 180 deg <br> - No Ice | 42.68 | -0.04 | 37.16 | 3652.67 | 4.91 | 0.34 |
| 0.9 Dead+1.0 Wind 180 deg <br> - No Ice | 32.01 | -0.04 | 37.16 | 3603.69 | 4.96 | 0.34 |
| 1.2 Dead+1.0 Wind 210 deg <br> - No Ice | 42.68 | -18.98 | 33.11 | 3209.03 | 1830.58 | -0.14 |
| 0.9 Dead+1.0 Wind 210 deg <br> - No Ice | 32.01 | -18.98 | 33.11 | 3166.19 | 1806.33 | -0.13 |
| 1.2 Dead+1.0 Wind 240 deg <br> - No Ice | 42.68 | -33.17 | 19.19 | 1857.84 | 3206.03 | 0.06 |
| 0.9 Dead+1.0 Wind 240 deg <br> - No Ice | 32.01 | -33.17 | 19.19 | 1833.05 | 3163.33 | 0.06 |
| 1.2 Dead+1.0 Wind 270 deg <br> - No Ice | 42.68 | -36.96 | -0.10 | -16.92 | 3623.09 | 0.29 |
| 0.9 Dead+1.0 Wind 270 deg <br> - No Ice | 32.01 | -36.96 | -0.10 | -16.59 | 3574.68 | 0.28 |
| 1.2 Dead+1.0 Wind 300 deg <br> - No Ice | 42.68 | -32.25 | -18.91 | -1867.47 | 3153.61 | -0.93 |
| 0.9 Dead+1.0 Wind 300 deg <br> - No Ice | 32.01 | -32.25 | -18.91 | -1842.19 | 3111.40 | -0.94 |
| 1.2 Dead+1.0 Wind 330 deg - No Ice | 42.68 | -19.22 | -33.31 | -3217.24 | 1854.88 | -0.91 |


| Load Combination | Vertical $\qquad$ <br> K | Shear $_{x}$ $K$ | Shear $_{z}$ K | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { 0.9 Dead+1.0 Wind } 330 \mathrm{deg} \\ & \text { - No Ice } \end{aligned}$ | 32.01 | -19.22 | -33.31 | -3174.23 | 1830.25 | -0.92 |
| 1.2 Dead+1.0 Ice+1.0 Temp | 72.34 | 0.00 | 0.00 | 0.31 | -1.08 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp | 72.34 | -0.04 | -7.64 | -822.46 | 6.29 | -0.21 |
| $\begin{aligned} & \text { 1.2 Dead+1.0 Wind } 30 \\ & \text { deg+1.0 Ice+1.0 Temp } \end{aligned}$ | 72.34 | 3.79 | -6.61 | -709.37 | -405.93 | -0.26 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp | 72.34 | 6.55 | -3.84 | -415.16 | -703.21 | -0.26 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 72.34 | 7.58 | -0.01 | -0.63 | -812.18 | 0.05 |
| 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 72.34 | 6.56 | 3.84 | 416.13 | -704.04 | 0.09 |
| 1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp | 72.34 | 3.77 | 6.60 | 711.38 | -405.50 | 0.09 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp | 72.34 | -0.00 | 7.62 | 820.16 | -1.13 | 0.06 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp | 72.34 | -3.77 | 6.59 | 710.10 | 403.22 | -0.02 |
| $\begin{aligned} & \text { 1.2 Dead+1.0 Wind } 240 \\ & \text { deg+1.0 Ice+1.0 Temp } \end{aligned}$ | 72.34 | -6.59 | 3.81 | 410.62 | 707.08 | 0.01 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp | 72.34 | -7.58 | -0.02 | -3.83 | 811.77 | 0.05 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp | 72.34 | -6.57 | -3.85 | -417.05 | 704.23 | -0.18 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp | 72.34 | -3.82 | -6.62 | -711.75 | 409.46 | -0.17 |
| Dead+Wind 0 deg - Service | 35.56 | -0.04 | -7.70 | -741.48 | 6.38 | -0.24 |
| Dead+Wind 30 deg - Service | 35.56 | 3.72 | -6.48 | -630.96 | -360.48 | -0.30 |
| Dead+Wind 60 deg - Service | 35.56 | 6.41 | -3.77 | -370.71 | -624.14 | -0.29 |
| Dead+Wind 90 deg - Service | 35.56 | 7.65 | -0.01 | -2.06 | -730.84 | 0.06 |
| Dead+Wind 120 deg Service | 35.56 | 6.62 | 3.88 | 374.82 | -633.96 | 0.10 |
| Dead+Wind 150 deg Service | 35.56 | 3.69 | 6.46 | 631.00 | -358.39 | 0.10 |
| Dead+Wind 180 deg Service | 35.56 | -0.01 | 7.46 | 727.95 | 0.65 | 0.07 |
| Dead+Wind 210 deg Service | 35.56 | -3.81 | 6.64 | 639.47 | 364.53 | -0.02 |
| Dead+Wind 240 deg Service | 35.56 | -6.65 | 3.85 | 370.17 | 638.68 | 0.01 |
| Dead+Wind 270 deg Service | 35.56 | -7.41 | -0.02 | -3.49 | 721.81 | 0.05 |
| Dead+Wind 300 deg Service | 35.56 | -6.47 | -3.79 | -372.30 | 628.20 | -0.20 |
| Dead+Wind 330 deg Service | 35.56 | -3.86 | -6.68 | -641.36 | 369.38 | -0.19 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.00 | -35.56 | 0.00 | -0.00 | 35.56 | 0.00 | $0.000 \%$ |
| 2 | -0.21 | -42.68 | -38.40 | 0.21 | 42.68 | 38.40 | $0.003 \%$ |
| 3 | -0.21 | -32.01 | -38.40 | 0.21 | 32.01 | 38.40 | $0.002 \%$ |
| 4 | 18.52 | -42.68 | -3.30 | -18.52 | 42.68 | 32.30 | $0.000 \%$ |
| 5 | 18.52 | -32.01 | -32.30 | -18.52 | 32.01 | 32.30 | $0.000 \%$ |
| 6 | 31.97 | -42.68 | -18.79 | -31.97 | 42.68 | 18.79 | $0.000 \%$ |
| 7 | 31.97 | -32.01 | -18.79 | -31.97 | 32.01 | 18.79 | $0.000 \%$ |
| 8 | 38.15 | -42.68 | -0.06 | -38.14 | 42.68 | 0.06 | $0.007 \%$ |
| 9 | 38.15 | -32.01 | -0.06 | -38.14 | 32.01 | 0.06 | $0.005 \%$ |
| 10 | 33.02 | -42.68 | 19.35 | -33.02 | 42.68 | -19.35 | $0.000 \%$ |
| 11 | 33.02 | -32.01 | 19.35 | -33.02 | 32.01 | -19.35 | $0.000 \%$ |
| 12 | 18.38 | -42.68 | 32.19 | -18.38 | 42.68 | -32.19 | $0.000 \%$ |
| 13 | 18.38 | -32.01 | 32.19 | -18.38 | 32.01 | -32.19 | $0.000 \%$ |

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|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ | PY | PZ |  |
| Comb. | K | K | K | K | K | K |  |
| 14 | -0.04 | -42.68 | 37.17 | 0.04 | 42.68 | -37.16 | 0.007\% |
| 15 | -0.04 | -32.01 | 37.17 | 0.04 | 32.01 | -37.16 | 0.005\% |
| 16 | -18.98 | -42.68 | 33.11 | 18.98 | 42.68 | -33.11 | 0.000\% |
| 17 | -18.98 | -32.01 | 33.11 | 18.98 | 32.01 | -33.11 | 0.000\% |
| 18 | -33.17 | -42.68 | 19.19 | 33.17 | 42.68 | -19.19 | 0.000\% |
| 19 | -33.17 | -32.01 | 19.19 | 33.17 | 32.01 | -19.19 | 0.000\% |
| 20 | -36.96 | -42.68 | -0.10 | 36.96 | 42.68 | 0.10 | 0.007\% |
| 21 | -36.96 | -32.01 | -0.10 | 36.96 | 32.01 | 0.10 | 0.005\% |
| 22 | -32.25 | -42.68 | -18.91 | 32.25 | 42.68 | 18.91 | 0.000\% |
| 23 | -32.25 | -32.01 | -18.91 | 32.25 | 32.01 | 18.91 | 0.000\% |
| 24 | -19.22 | -42.68 | -33.31 | 19.22 | 42.68 | 33.31 | 0.000\% |
| 25 | -19.22 | -32.01 | -33.31 | 19.22 | 32.01 | 33.31 | 0.000\% |
| 26 | 0.00 | -72.34 | 0.00 | -0.00 | 72.34 | -0.00 | 0.000\% |
| 27 | -0.04 | -72.34 | -7.64 | 0.04 | 72.34 | 7.64 | 0.001\% |
| 28 | 3.79 | -72.34 | -6.62 | -3.79 | 72.34 | 6.61 | 0.001\% |
| 29 | 6.55 | -72.34 | -3.84 | -6.55 | 72.34 | 3.84 | 0.001\% |
| 30 | 7.58 | -72.34 | -0.01 | -7.58 | 72.34 | 0.01 | 0.001\% |
| 31 | 6.56 | -72.34 | 3.85 | -6.56 | 72.34 | -3.84 | 0.001\% |
| 32 | 3.78 | -72.34 | 6.60 | -3.77 | 72.34 | -6.60 | 0.001\% |
| 33 | -0.00 | -72.34 | 7.62 | 0.00 | 72.34 | -7.62 | 0.001\% |
| 34 | -3.77 | -72.34 | 6.59 | 3.77 | 72.34 | -6.59 | 0.001\% |
| 35 | -6.59 | -72.34 | 3.81 | 6.59 | 72.34 | -3.81 | 0.001\% |
| 36 | -7.58 | -72.34 | -0.02 | 7.58 | 72.34 | 0.02 | 0.001\% |
| 37 | -6.57 | -72.34 | -3.85 | 6.57 | 72.34 | 3.85 | 0.001\% |
| 38 | -3.82 | -72.34 | -6.63 | 3.82 | 72.34 | 6.62 | 0.001\% |
| 39 | -0.04 | -35.56 | -7.70 | 0.04 | 35.56 | 7.70 | 0.002\% |
| 40 | 3.72 | -35.56 | -6.48 | -3.72 | 35.56 | 6.48 | 0.002\% |
| 41 | 6.41 | -35.56 | -3.77 | -6.41 | 35.56 | 3.77 | 0.002\% |
| 42 | 7.65 | -35.56 | -0.01 | -7.65 | 35.56 | 0.01 | 0.002\% |
| 43 | 6.62 | -35.56 | 3.88 | -6.62 | 35.56 | -3.88 | 0.002\% |
| 44 | 3.69 | -35.56 | 6.46 | -3.69 | 35.56 | -6.46 | 0.002\% |
| 45 | -0.01 | -35.56 | 7.46 | 0.01 | 35.56 | -7.46 | 0.002\% |
| 46 | -3.81 | -35.56 | 6.64 | 3.81 | 35.56 | -6.64 | 0.002\% |
| 47 | -6.65 | -35.56 | 3.85 | 6.65 | 35.56 | -3.85 | 0.002\% |
| 48 | -7.42 | -35.56 | -0.02 | 7.41 | 35.56 | 0.02 | 0.002\% |
| 49 | -6.47 | -35.56 | -3.79 | 6.47 | 35.56 | 3.79 | 0.002\% |
| 50 | -3.86 | -35.56 | -6.68 | 3.86 | 35.56 | 6.68 | 0.002\% |

## Non-Linear Convergence Results

| Load <br> Combination | Converged? | Number <br> of Cycles | Displacement <br> Tolerance | Force <br> Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 6 | 0.00000001 | 0.00000001 |
| 2 | Yes | 15 | 0.00003487 | 0.00010404 |
| 3 | Yes | 15 | 0.00002186 | 0.00007748 |
| 4 | Yes | 18 | 0.00000001 | 0.00012914 |
| 5 | Yes | 18 | 0.00000001 | 0.00008542 |
| 6 | Yes | 18 | 0.00000001 | 0.00013581 |
| 7 | Yes | 18 | 0.00000001 | 0.00008997 |
| 8 | Yes | 14 | 0.00008553 | 0.00010041 |
| 9 | Yes | 14 | 0.00005510 | 0.00008143 |
| 10 | Yes | 18 | 0.00000001 | 0.00013477 |
| 11 | Yes | 18 | 0.00000001 | 0.00008900 |
| 12 | Yes | 18 | 0.00000001 | 0.00012994 |
| 13 | Yes | 18 | 0.00000001 | 0.00008602 |
| 14 | Yes | 14 | 0.00008535 | 0.00011208 |
| 15 | Yes | 14 | 0.00005497 | 0.00009027 |
| 16 | Yes | 18 | 0.00000001 | 0.00013174 |
| 17 | Yes | 18 | 0.00000001 | 0.00008702 |
| 18 | Yes | 18 | 0.00000001 | 0.00013402 |
| 19 | Yes | 18 | 0.00000001 | 0.00008846 |
| 20 | Yes | 14 | 0.00008554 | 0.00012696 |
| 21 | Yes | 14 | 0.00005510 | 0.00010018 |
| 22 | Yes | 18 | 0.00000001 | 0.00013392 |
| 23 | Yes | 18 | 0.00008851 |  |

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| 24 | Yes | 18 | 0.00000001 | 0.00013567 |
| :--- | :--- | :---: | :--- | :--- |
| 25 | Yes | 18 | 0.00000001 | 0.00008958 |
| 26 | Yes | 6 | 0.00000001 | 0.00000001 |
| 27 | Yes | 16 | 0.00000001 | 0.00007528 |
| 28 | Yes | 16 | 0.00000001 | 0.00009248 |
| 29 | Yes | 16 | 0.00000001 | 0.00009371 |
| 30 | Yes | 16 | 0.00000001 | 0.00007402 |
| 31 | Yes | 16 | 0.00000001 | 0.00009369 |
| 32 | Yes | 16 | 0.00000001 | 0.00009295 |
| 33 | Yes | 16 | 0.00000001 | 0.00007495 |
| 34 | Yes | 16 | 0.00000001 | 0.00009236 |
| 35 | Yes | 16 | 0.00000001 | 0.00009302 |
| 36 | Yes | 16 | 0.00000001 | 0.00007396 |
| 37 | Yes | 16 | 0.00000001 | 0.00009343 |
| 38 | Yes | 16 | 0.00000001 | 0.00009373 |
| 39 | Yes | 14 | 0.00000001 | 0.00002984 |
| 40 | Yes | 14 | 0.00000001 | 0.00003282 |
| 41 | Yes | 14 | 0.00000001 | 0.00004153 |
| 42 | Yes | 14 | 0.00000001 | 0.00002850 |
| 43 | Yes | 14 | 0.00000001 | 0.00003903 |
| 44 | Yes | 14 | 0.00000001 | 0.00003517 |
| 45 | Yes | 14 | 0.00000001 | 0.00002884 |
| 46 | Yes | 14 | 0.00000001 | 0.00003707 |
| 47 | Yes | 14 | 0.00000001 | 0.00003753 |
| 48 | Yes | 14 | 0.00000001 | 0.00002851 |
| 49 | Yes | 14 | 0.00003488 |  |
| 50 | Yes | 14 | 0.00004111 |  |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 。 |
| :---: | :---: | :---: | :---: | :---: | :---: | | Ttwist |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | ft | $147-99.5$ | 27.10 | 39 |
| L1 | $103.25-59$ | 13.97 | 39 | 1.51 |
| L3 | $63.75-29.25$ | 5.27 | 39 | 0.27 |
| L4 | $34.5-0$ | 1.56 | 39 | 0.78 |

Critical Deflections and Radius of Curvature - Service Wind
$\left.\begin{array}{ccccccc}\hline \text { Elevation } & \text { Appurtenance } & \begin{array}{c}\text { Gov. } \\ \text { Load } \\ \text { Comb. }\end{array} & \text { Deflection } & \text { Tilt } & \begin{array}{c}\text { Twist }\end{array} \\ \text { ft } & & 39 & 27.10 & 1.51 & 0 & 0.00 \\ \text { Curvature } \\ \text { ft }\end{array}\right]$

## Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | ft | $147-99.5$ | 135.92 | 2 | $\circ$ |

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| Section <br> No. | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | 。 |
| :---: | :---: | :---: | :---: | :---: | :---: |


| Critical Deflections and Radius of Curvature - Design Wind |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature ft |
| 149.0000 | A-ANT-23G-2-C | 2 | 135.92 | 7.61 | 0.02 | 9647 |
| 147.0000 | Top Hat 10" Diameter x 4' 6" Tall | 2 | 135.92 | 7.61 | 0.02 | 9647 |
| 145.0000 | TME-1900MHz RRH ( 65 MHz ) | 2 | 132.75 | 7.57 | 0.02 | 9647 |
| 121.0000 | ERICSSON AIR 21 B2A B4P w/ Mount Pipe | 2 | 95.43 | 7.06 | 0.01 | 1850 |
| 110.0000 | 7770.00 w/ Mount Pipe | 2 | 79.39 | 6.69 | 0.01 | 1297 |
| 100.0000 | APXV18-206517S-C w/ Mount Pipe | 2 | 65.79 | 6.24 | 0.01 | 1074 |
| 53.0000 | GPS_A | 2 | 18.15 | 3.20 | 0.00 | 825 |
| 49.0000 | KS24019-L112A | 2 | 15.47 | 2.94 | 0.00 | 806 |

## Compression Checks

## Pole Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | KI/r | $A$ | $P_{u}$ | $\phi P_{n}$ | Ratio $P_{u}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  |  | ft | ft |  | $i n^{2}$ | K | K | $\phi P_{n}$ |
| L1 | 147-99.5 (1) | TP30.313x22x0.25 | $\begin{gathered} 47.500 \\ 0 \end{gathered}$ | 0.0000 | 0.0 | $\begin{gathered} 23.672 \\ 4 \end{gathered}$ | -14.88 | 1278.31 | 0.012 |
| L2 | 99.5-59 (2) | TP36.9x29.1567x0.3125 | $\begin{gathered} 44.250 \\ 0 \end{gathered}$ | 0.0000 | 0.0 | $\begin{gathered} 35.979 \\ 8 \end{gathered}$ | -22.73 | 2104.82 | 0.011 |
| L3 | 59-29.25 (3) | TP41.481×35.4438x0.375 | $\begin{gathered} 34.500 \\ 0 \end{gathered}$ | 0.0000 | 0.0 | $\begin{gathered} 48.526 \\ 2 \end{gathered}$ | -30.79 | 2838.78 | 0.011 |
| L4 | 29.25-0 (4) | TP45.85x39.8123x0.4375 | $\begin{gathered} 34.500 \\ 0 \end{gathered}$ | 0.0000 | 0.0 | $\begin{gathered} 63.974 \\ 9 \end{gathered}$ | -42.64 | 3742.53 | 0.011 |


| Pole Bending Design Data |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | Size | $M_{u x}$ | $\phi M_{n x}$ | Ratio $M_{u x}$ | $M_{u y}$ | $\phi M_{n y}$ | Ratio $M_{u y}$ |
|  | ft |  | kip-ft | kip-ft | ${ }_{\phi} M_{n x}$ | kip-ft | kip-ft | $\phi M_{n y}$ |
| L1 | 147-99.5 (1) | TP30.313x22x0.25 | 529.12 | 857.29 | 0.617 | 0.00 | 857.29 | 0.000 |
| L2 | 99.5-59 (2) | TP36.9x29.1567x0.3125 | 1560.78 | 1707.36 | 0.914 | 0.00 | 1707.36 | 0.000 |
| L3 | 59-29.25 (3) | TP41.481x35.4438x0.375 | 2472.84 | 2662.28 | 0.929 | 0.00 | 2662.28 | 0.000 |
| L4 | 29.25-0 (4) | TP45.85x39.8123x0.4375 | 3719.47 | 4017.32 | 0.926 | 0.00 | 4017.32 | 0.000 |

## Pole Shear Design Data

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Section No. \& Elevation \& Size \& Actual $V_{u}$ \& $\phi V_{n}$

$K$ \& Ratio $V_{u}$ \& Actual $T_{u}$ \& $\phi T_{n}$ \& Ratio $T_{u}$ <br>
\hline \multicolumn{3}{|c|}{$f t$} \& K \& K \& $\phi V_{n}$ \& kip-ft \& kip-ft \& $\phi T_{n}$ <br>
\hline L1 \& 147-99.5 (1) \& TP30.313x22x0.25 \& 22.75 \& 383.49 \& 0.059 \& 1.24 \& 991.98 \& 0.001 <br>
\hline L2 \& 99.5-59 (2) \& TP36.9x29.1567x0.3125 \& 28.80 \& 631.45 \& 0.046 \& 1.23 \& 1986.04 \& 0.001 <br>
\hline L3 \& 59-29.25 (3) \& TP41.481×35.4438x0.375 \& 33.63 \& 851.63 \& 0.039 \& 1.21 \& 3010.53 \& 0.000 <br>
\hline L4 \& 29.25-0 (4) \& TP45.85x39.8123x0.4375 \& 38.44 \& 1122.76 \& 0.034 \& 1.21 \& 4484.99 \& 0.000 <br>
\hline
\end{tabular}

| Pole Interaction Design Data |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | Elevation | $\begin{gathered} \text { Ratio } \\ P_{u} \\ \hline \end{gathered}$ | Ratio $M_{u x}$ | Ratio $M_{u y}$ | Ratio $V_{u}$ | $\begin{gathered} \text { Ratio } \\ T_{u} \\ \hline \end{gathered}$ | Comb. Stress | Allow. Stress | Criteria |
|  | $f t$ | $\phi P_{n}$ | $\phi M_{n \times}$ | $\phi M_{n y}$ | $\phi V_{n}$ | $\phi T_{n}$ | Ratio | Ratio |  |
| L1 | 147-99.5 (1) | 0.012 | 0.617 | 0.000 | 0.059 | 0.001 | 0.633 | 1.050 | 4.8.2 |
| L2 | 99.5-59 (2) | 0.011 | 0.914 | 0.000 | 0.046 | 0.001 | 0.927 | 1.050 | 4.8.2 |
| L3 | 59-29.25 (3) | 0.011 | 0.929 | 0.000 | 0.039 | 0.000 | 0.941 | 1.050 | 4.8.2 |
| L4 | 29.25-0 (4) | 0.011 | 0.926 | 0.000 | 0.034 | 0.000 | 0.938 | 1.050 | 4.8.2 |

## Section Capacity Table

| Section No. | $\begin{aligned} & \text { Elevation } \\ & \mathrm{ft} \end{aligned}$ | Component Type | Size | Critical Element | $\begin{aligned} & P \\ & K \end{aligned}$ | $\begin{gathered} \varnothing P_{\text {allow }} \\ K \end{gathered}$ | \% Capacity | $\begin{aligned} & \text { Pass } \\ & \text { Fail } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 147-99.5 | Pole | TP30.313×22×0.25 | 1 | -14.88 | 1342.23 | 60.2 | Pass |
| L2 | 99.5-59 | Pole | TP36.9x29.1567x0.3125 | 2 | -22.73 | 2210.06 | 88.3 | Pass |
| L3 | 59-29.25 | Pole | TP41.481×35.4438×0.375 | 3 | -30.79 | 2980.72 | 89.6 | Pass |
| L4 | 29.25-0 | Pole | TP45.85x39.8123x0.4375 | 4 | -42.64 | 3929.66 | 89.4 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L3) | 89.6 | Pass |
|  |  |  |  |  |  | RATING = | 89.6 | Pass |

## APPENDIX B

## BASE LEVEL DRAWING



## APPENDIX C

## ADDITIONAL CALCULATIONS

| Site Info |  |
| ---: | ---: |
| BU \# |  |
| Site Name |  |
| Order \# |  |


| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{I}_{\mathrm{ar}}$ (in) | 0 |


| Applied Loads |  |
| :--- | :---: |
| Moment (kip-ft) | 3719.43 |
| Axial Force (kips) | 42.64 |
| Shear Force (kips) | 38.44 |



## Connection Properties

Analysis Results

Anchor Rod Data
GROUP 1: (16) 2-1/4" $\varnothing$ bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 54" BC Anchor Spacing: 6 in
GROUP 2: (3) 1-3/4" $\varnothing$ bolts (A193 Gr. B7 N; Fy=105 ksi, Fu=125 ksi) on 61.85" BC pos. (deg): 18, 149, 226

Base Plate Data
54" OD x 3.5" Plate (A572-50; Fy=50 ksi, Fu=65 ksi)

Stiffener Data
N/A

Pole Data
45.85 " $\times 0.4375$ " 12-sided pole (A607-65; Fy=65 ksi, Fu=80 ksi)

Anchor Rod Summary
(units of kips, kip-in) GROUP 1:

| Pu_c = 196.49 | $\phi P n \_c=243.75$ | Stress Rating |
| :--- | :--- | :---: |
| $\mathrm{Vu}=2.4$ | $\phi \mathrm{Vn}=73.13$ | $76.9 \%$ |
| $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |

GROUP 2:

$$
\begin{aligned}
& \mathrm{Pu} u_{-}=119.79 \\
& \mathrm{Vu}=0 \\
& \mathrm{Mu}=\mathrm{n} / \mathrm{a}
\end{aligned}
$$

$$
\begin{aligned}
& \phi P n \_c=199.5 \\
& \phi V n=59.85 \\
& \phi M n=n / a
\end{aligned}
$$

Stress Rating 57.2\% Pass

| Base Plate Summary |  |  |
| :--- | :--- | :---: |
| Max Stress (ksi): | 26.05 | (Flexural) |
| Allowable Stress (ksi): | $\mathbf{4 5}$ |  |
| Stress Rating: | $\mathbf{5 5 . 1 \%}$ | Pass |

Pier and Pad Foundation

| BU \# : 876321 |  |
| ---: | :--- |
| Site Name: |  |
| App. Number: | $\square$ |


| TIA-222 Revision: | H |
| ---: | :---: |
| Tower Type: | Monopole |
|  |  |


| Top \& Bot. Pad Rein. Different?: | $\Gamma$ |
| ---: | :---: |
| Block Foundation?: | $\Gamma$ |


| Superstructure Analysis Reactions |  |  |
| ---: | :---: | :--- |
| Compression, $\mathbf{P}_{\text {comp }}:$ | 43 | kips |
| Base Shear, Vu_comp: | 38 | kips |
|  |  |  |
|  |  |  |
| ${\text { Moment, } \mathbf{M}_{\mathbf{u}}:}^{\|c\|} 3719$ | ft-kips |  |
| Tower Height, H: | 147 | ft |
|  |  |  |
| BP Dist. Above Fdn, bp dist: | 2.5 | in |


| Foundation Analysis Checks |  |  |  |  |
| ---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating* | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 346.43 | 38.00 | $\mathbf{1 0 . 4 \%}$ | Pass |
| Bearing Pressure (ksff | 6.00 | 4.16 | $\mathbf{6 9 . 3 \%}$ | Pass |
| Overturning (kip*ft) | 4904.30 | 4163.92 | $\mathbf{8 4 . 9 \%}$ | Pass |
| Pier Flexure (Comp.) (kip*ft) | 4076.63 | 4042.00 | $\mathbf{9 4 . 4 \%}$ | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 23390.64 | 105.13 | $\mathbf{0 . 4 \%}$ | Pass |
| Pad Flexure (kip*ft) | 4322.10 | 2187.06 | $\mathbf{4 8 . 2 \%}$ | Pass |
| Pad Shear -1-way (kips) | 624.22 | 358.92 | $\mathbf{5 4 . 8 \%}$ | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.164 | 0.000 | $\mathbf{0 . 0 \%}$ | Pass |
| Flexural 2-way (Comp) (kip*ft) | 6631.37 | 2425.20 | $\mathbf{3 4 . 8 \%}$ | Pass |

*Rating per TIA-222-H Section 15.5

| Soil Rating*: | $\mathbf{8 4 . 9 \%}$ |
| ---: | :---: |
| Structural Rating $^{*}:$ | $*$ |

*See SP Column for steel calculations

| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 11 | ft |
| Pad Width, W: | 20.5 | ft |
| Pad Thickness, T: | 3 | ft |
| Pad Rebar Size (Bottom), Sp: | 11 |  |
| Pad Rebar Quantity (Bottom), mp: | 21 |  |
| Pad Clear Cover, $\mathbf{c c}_{\text {pad }}:$ | 3 | in |


| Material Properties |  |  |  |
| ---: | :---: | :--- | :---: |
| Rebar Grade, Fy: | 60 | ksi |  |
| Concrete Compressive Strength, F'c: | 3 | ksi |  |
| Dry Concrete Density, $\delta \mathbf{c}:$ | 150 | pcf |  |

Soil Properties

| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 125 | pcf |
| Ultimate Gross Bearing, Qult: | 8.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 35 | degrees |
| SPT Blow Count, N | blows: | 34 |
|  |  |  |
| Base Friction, $\mu:$ |  |  |
| Neglected Depth, $\mathbf{N}:$ | 3.50 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | 4.5 | ft |

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Computer program for the Strength Design of Reinforced Concrete Sections
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## 1. General Information

| File Name | g:Itowerl375_crown_....foundati <br> on steel check.col |
| :--- | :--- |
| Project | $37519-2435.001 .7805$ |
| Column | BU 876321 |
| Engineer | GP |
| Code | ACI 318-14 |
| Bar Set | ASTM A615 |
| Units | English |
| Run Option | Investigation |
| Run Axis | X -axis |
| Slenderness | Not Considered |
| Column Type | Architectural |

## 2. Material Properties

### 2.1. Concrete

| Type | Standard |
| :--- | :---: |
| $f_{c}$ | 3 ksi |
| $E_{c}$ | 3122.02 ksi |
| $f_{c}$ | 2.55 ksi |
| $\varepsilon_{u}$ | $0.003 \mathrm{in} / \mathrm{in}$ |
| $\beta_{1}$ | 0.85 |

### 2.2. Steel

| Type | Standard |
| :--- | ---: |
| $\mathrm{f}_{\mathrm{y}}$ | 60 ksi |
| $\mathrm{E}_{\mathrm{s}}$ | 29000 ksi |
| $\varepsilon_{y t}$ | $0.00206897 \mathrm{in} / \mathrm{in}$ |

## 3. Section

### 3.1. Shape and Properties

| Type | Rectangular |
| :--- | ---: |
| Width | 84 in |
| Depth | 84 in |
| $A_{g}$ | 7056 in $^{2}$ |
| $I_{x}$ | $4.14893 \mathrm{e}+006$ in $^{4}$ |
| $\mathrm{I}_{y}$ | $4.14893 \mathrm{e}+006$ in $^{4}$ |
| $\mathrm{r}_{\mathrm{x}}$ | 24.2487 in |
| $\mathrm{r}_{y}$ | 24.2487 in |
| $X_{0}$ | 0 in |
| $Y_{0}$ | 0 in |

### 3.2. Section Figure



## Figure 1: Column section

## 4. Reinforcement

4.1. Bar Set: ASTM A615

| Bar | Diameter <br> in | Area <br> $\mathrm{in}^{2}$ | Bar | Diameter <br> in | Area <br> in $^{2}$ | Bar | Diameter <br> in | Area <br> in $^{2}$ |
| ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: | ---: |
| $\# 3$ | 0.38 | 0.11 | $\# 4$ | 0.20 | 0.31 |  |  |  |
| $\# 6$ | 0.75 | 0.44 | $\# 7$ | 0.50 | $\# 5$ | 0.63 |  |  |
| $\# 9$ | 1.13 | 1.00 | $\# 10$ | 1.27 | 0.60 | 1.27 | \#8 | 1.00 |
| $\# 14$ | 1.69 | 2.25 | $\# 18$ | 2.26 | 4.00 | 1.41 |  |  |

### 4.2. Confinement and Factors

| Confinement type | Tied |
| :--- | ---: |
| For \#10 bars or less | \#3 ties |
| For larger bars | \#4 ties |
|  |  |
| Capacity Reduction Factors |  |
| Axial compression, (a) | 0.8 |
| Tension controlled $\phi$, (b) | 0.9 |
| Compression controlled $\phi,(c)$ | 0.65 |

### 4.3. Arrangement

| Pattern | Irregular |
| :--- | :---: |
| Bar layout | --- |
| Cover to | --- |
| Clear cover | --- |
| Bars | --- |


| STRUCTUREPOINT - spColumn v6.00 | Page 5 |
| :--- | ---: | ---: |
| Licensed to: Paul J. Ford and Company. License ID: 68668-1061816-4-1E6CD-227E3 | $8 / 22 / 2019$ |

g:ltowerl375_crown_castle\2019\37519-2435_876321_branford banm towerl...lfoundation steel check.col
8/22/2019
11:30 AM

|  |  |
| :--- | :---: |
| Total steel area, $\mathrm{A}_{\mathrm{s}}$ | $30.66 \mathrm{in}^{2}$ |
| Rho | $0.43 \%$ |
| Minimum clear spacing | 5.95 in |
| Note: Rho $<0.50 \%$ ) |  |

### 4.4. Bars Provided

| Area |  | Y |  | X | Y | Area | X | Y |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{in}^{2}$ | in | in | in ${ }^{2}$ | in | in | in ${ }^{2}$ | in | in |
| 1.56 | 0.0 | 38.3 | 1.56 | 14.7 | 35.4 | 1.56 | 27.1 | 27.1 |
| 1.56 | 35.4 | 14.7 | 1.56 | 38.3 | 0.0 | 1.56 | 35.4 | -14.7 |
| 1.56 | 27.1 | -27.1 | 1.56 | 14.7 | -35.4 | 1.56 | 0.0 | -38.3 |
| 1.56 | -14.7 | -35.4 | 1.56 | -27.1 | -27.1 | 1.56 | -35.4 | -14.7 |
| 1.56 | -38.3 | 0.0 | 1.56 | -35.4 | 14.7 | 1.56 | -27.1 | 27.1 |
| 1.56 | -14.7 | 35.4 | 1.90 | 9.5 | -29.4 | 1.90 | 15.7 | 26.7 |
| 1.90 | -22.5 | 21.3 |  |  |  |  |  |  |

## 5. Factored Loads and Moments with Corresponding Capacities

| No | $\mathrm{P}_{\mathbf{u}}$ | $M_{u x}$ | $\boldsymbol{\phi} \mathrm{M}_{\mathrm{nx}}$ | $\boldsymbol{\phi} \mathrm{M}_{\mathrm{n}} / \mathrm{M}_{\mathrm{u}}$ | NA Depth | $d_{\text {t }}$ Depth | $\varepsilon_{\text {t }}$ | ф |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | kip | k-ft | k-ft |  | in | in |  |  |
| 1 | -91.37 | 4163.62 | 4771.41 | 1.146 | 12.53 | 80.29 | 0.01622 | 0.900 |

## Address:

No Address at This Location

## ASCE 7 Hazards Report



## Wind

## Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

127 Vmph
78 Vmph
88 Vmph
95 Vmph
103 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Mon Jun 032019

Date Accessed:


## Seismic

Site Soil Class: D-Stiff Soil

Results:

| $\mathrm{S}_{\mathrm{S}}:$ | 0.18 |
| :--- | :--- |
| $\mathrm{~S}_{1}:$ | 0.061 |
| $\mathrm{~F}_{\mathrm{a}}:$ | 1.6 |
| $\mathrm{~F}_{\mathrm{V}}:$ | 2.4 |
| $\mathrm{~S}_{\mathrm{Ms}}:$ | 0.288 |
| $\mathrm{~S}_{\mathrm{M} 1}:$ | 0.147 |


| $\mathrm{S}_{\mathrm{DS}}:$ | 0.192 |
| :--- | :--- |
| $\mathrm{~S}_{\mathrm{D} 1}:$ | 0.098 |
| $\mathrm{~T}_{\mathrm{L}}:$ | 6 |
| $\mathrm{PGA}:$ | 0.093 |
| $\mathrm{PGA}:$ | 0.149 |
| $\mathrm{~F}_{\mathrm{PGA}}:$ | 1.6 |
| $\mathrm{I}_{\mathrm{e}}:$ | 1 |

## Seismic Design Category <br> B




## Data Accessed:

Date Source:

Mon Jun 032019
USGS Seismic Design Maps based on ASCE/SEI 7-10, incorporating
Supplement 1 and errata of March 31, 2013, and ASCE/SEI 7-10 Table 1.5-2. Additional data for site-specific ground motion procedures in accordance with ASCE/SEI 7-10 Ch. 21 are available from USGS.

AMERICAN SOCIETY OF CIVIL ENGINEERS
Ice

Results:

Ice Thickness:
Concurrent Temperature:
Gust Speed:
Data Source:
Date Accessed:
0.75 in.

15 F
50 mph
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Mon Jun 032019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.
Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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## Exhibit E

## Mount Analysis

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Crown Castle
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Charlotte, NC 28277
(704) 405-6619

CLS $\operatorname{ENGINEERING}^{\text {and }}$
CLS Engineering PLLC
319 Chapanoke Road, Suite 118
Raleigh, NC 27603
(405) 348-5460
Engineering@clsengineeringpllc.com
Mount Replacement Report
T-Mobile Equipment Change-Out Carrier Site Number: Carrier Site Name:

Crown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number: Crown Castle Order Number:

CLS Engineering PLLC Project \#:

CTNH107A
NH107/Global/Cherry Hill
876321
Branford Banm Tower
559323
479853 Rev. 0
42284-CTNH107A-02-MR

150 North Main Street, Branford, CT 06405, New Haven County Latitude: $41^{\circ} 17$ ' $19.00^{\prime \prime}$ Longitude: $-72^{\circ} 48^{\prime} 49.90^{\prime \prime}$

Tower Height \& Type:
Mount Elevation:
Mount Width \& Type:
147 ft Monopole
121 ft
12.5 ft Site Pro 1 RMQP-4096-HK

## Dear Kevin Morrow,

CLS Engineering PLLC is pleased to submit this "Mount Replacement Report" to determine the structural integrity of TMobile's antenna mounting system with the proposed appurtenance and equipment addition on the above mentioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

Site Pro 1 RMQP-4096-HK
Sufficient*
*Sufficient upon completion of the changes listed in the 'Conclusion and Recommendations' section of this report.
This analysis utilizes an ultimate 3 -second gust wind speed of 130 mph as required by the 2018 Connecticut State Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: Michelle Lin

Respectfully Submitted by:

Tyler M. Barker, P.E.
Director of Engineering


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## 1. INTRODUCTION

The proposed equipment is to be mounted to the existing Site Pro 1 RMQP-4096-HK. This proposed mounting configuration was analyzed using RISA-3D, a commercially available finite element analysis software package. A selection of input and output from our analysis is attached to the end of this report.

## 2. ANALYSIS CRITERIA

| STANDARD | 2015 IBC / 2018 Connecticut State Building Code / TIA-222-H |
| :--- | :--- |
| BASIC WIND SPEED | $130 \mathrm{mph}, \mathrm{V}_{\mathrm{ult}}$ (3-Second Gust) |
| BASIC WIND SPEED W/ ICE | 50 mph (3-Second Gust) w/ 1.5" Radial Ice (Escalating) |
| EXPOSURE CATEGORY | C |
| MAX. TOPOGRAPHIC FACTOR, | 1.00 |
| RISK CATEGORY | II |
| MAINTENANCE LIVE LOAD | $\mathrm{L}_{\mathrm{m}}: 500 \mathrm{lb}$ |

Table 1 - Final Equipment Configuration

| ELEVATION (ft) |  | ANTENNAS |  |
| :---: | :---: | :---: | :---: |
| MOUNT | RAD. | $\#$ | NAME |
| 121.0 |  | 121.0 | 3 |
|  |  | 3 | RFS Celwave APXVAARR24_43-U-NA20 |
|  |  | 3 | Ericsson AIR 21 B2A/B4P |
|  |  | 3 | Ericsson AIR 21 B4A/B2P |
|  |  | 3 | Ericsson RADIO 4449 B12/B71 |

## 3. ANALYSIS PROCEDURE

Table 2 - Documents Provided

| STRUCTURAL DATA | Assembly Drawings by Site Pro 1, Part No. RMQP-4096-HK, Rev. A, dated July 14, 2014 |
| :--- | :--- |
| PREVIOUS ANALYSES | Mount Analysis by CLS Group, Project No. 42284-CTNH107A-01-MA, dated April 29, <br> 2019 <br> Tower SA by Tower Engineering Professionals, Project \#25579.155918, dated January <br> 31,2018 |
| LOADING DATA | Crown Castle Order ID \#479853 Rev. 0, dated April 22, 2019 |

### 3.1. Analysis Method

RISA-3D, a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases. This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 Tower Mount Analysis (Revision B).

## 4. ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity

| COMPONENT | PEAK USAGE | RESULT |
| :---: | :---: | :---: |
| Connection Plate | $84 \%$ | Pass |
| Support Rail | $43 \%$ | Pass |
| Mount Pipes | $36 \%$ | Pass |
| Collar Reactions | $30 \%$ | Pass |
| Connections | $18 \%$ | Pass |
| Platform Base | $11 \%$ | Pass |


| Structure Rating (max from all components) $=$ |  |  | $84 \%$ |
| :--- | :--- | :---: | :---: |
| Notes: <br> 1) | See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the \% capacity <br> consumed. |  |  |

### 4.1 Conclusion and Recommendations

According to our structural analysis, the mounts have been found to PASS PENDING REPLACEMENT. The mounting configuration considered in this analysis will be capable of supporting the referenced loading pursuant to referenced standards once the following scope is executed:

- Replace existing T-Arms with (1) proposed Site Pro 1 RMQP-4096-HK platform mount.
- All mount pipes are to be installed equidistant from each other as shown in the following sketches.
- Install existing and proposed antennas such that they are centered vertically on the platform base. Install existing and proposed RRUS and TMAs behind antennas.

See "Appendix E: Installation Sketches and Mount Assembly Drawings" for additional details.

## 5. ASSUMPTIONS AND CONDITIONS

This analysis is inclusive of the antenna supporting frames/mounts and all recorded connections that will support the equipment listed in this report. It considers only the theoretical capacity of structural components and it is not a condition assessment. The validity of the analysis may be dependent on the accuracy of structural information supplied by others. The client is responsible for verifying this information. If any provided information is revised after completion of this analysis, CLS Engineering PLLC should be notified immediately to revise results.

This analysis assumes the following:

1. The tower or other superstructure and mounts (if existing) were properly constructed as per the original design and have been properly maintained in accordance with applicable code standards.
2. Member sizes and strengths are accurate as supplied or are assumed as stated in the calculations.
3. In the absence of sufficient design information, all welds and connections are assumed to develop at least the capacity of the connected member, unless otherwise stated in this analysis.
4. All prior structural modifications, if any, are assumed to be correctly installed and fully effective.
5. The loading configuration is complete and accurate as supplied and/or as modeled in the previous analysis. All appurtenances are assumed to be properly installed and supported as per manufacturer requirements.
6. Some conservative assumptions may be used regarding appurtenances and their projected areas based on careful interpretation of data supplied, previous experience and standard industry practice.

All opinions and conclusions are considered accurate to a reasonable degree of engineering certainty based upon the evidence available at the time of the report. All opinions and conclusions contained herein are subject to revision based upon receipt of new or updated information. All services are provided exercising a level of care and diligence equivalent to the standard of our profession. No warranty or guarantee, either expressed or implied, is offered. All services are confidential in nature and this report will not be released to any other party without the client's consent. The use of this analysis is limited to the expressed purpose for which it was commissioned and it may not be reused, copied or disseminated for any other purpose without consent from CLS Engineering PLLC.

All services were performed, results obtained and recommendations made in accordance with generally accepted engineering principles and practices. CLS Engineering PLLC is not responsible for the conclusions, opinions or recommendations made by others based on the information supplied in this analysis.

It is not possible to have the fully detailed information necessary to perform a complete and thorough analysis of every structural sub-component of an existing structure. The structural analysis by CLS Engineering PLLC verifies the adequacy of the primary members of the structure. CLS Engineering PLLC provides a limited scope of service in that we cannot verify the adequacy of every weld, bolt, gusset, etc.

## APPENDIX A

SOFTWARE INPUT CALCULATIONS

| Wind \& Ice Loading |  |  |  |
| :---: | :---: | :---: | :---: |
| Nominal Mount Elevation (AGL), $\boldsymbol{z}_{\text {mount }}$ | 121 ft | $\mathrm{K}_{\mathrm{a}}$ | 0.90 |
| Nominal Rad Elevation (AGL), $\mathrm{z}_{\text {rad }}$ | 121 ft | $\mathrm{K}_{\mathrm{d}}$ | 0.95 |
| TIA Standard | H | $\mathrm{K}_{\mathrm{z}}$ | 1.32 |
| Basic Wind Speed, $\mathrm{v}_{\text {ult }}$ (bare) | 130 mph | $\mathrm{K}_{\mathrm{zt}}$ | 1.00 |
| Basic Wind Speed, V (ice) | 50 mph | $\mathrm{Ks}_{\mathrm{s}}$ | 1.00 |
| Design Ice Thickness, $\mathrm{t}_{\mathrm{i}}$ | $11 / 2 \mathrm{in}$ | $\mathrm{t}_{\mathrm{i}}$ | 1.71 in |
| Exposure Category | C | $\mathrm{G}_{\mathrm{h}}$ | 1.00 |
| Risk Category | II | $\mathrm{q}_{\mathbf{z}}$ (bare) | 54.0 psf |
| Seismic Response Coeff., $\mathrm{C}_{\mathrm{s}}$ | - | $\mathrm{q}_{\mathbf{z}}$ (ice) | 8.0 psf |


| Live Loading |  | Member Distributed Loading |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| At Mount Pipes, $L_{M}$ | 500 lb | Section Set Label | Shape Label | $\mathrm{F}_{\mathrm{A}}$ | b/ft) | Ice Wt. |
| Joint Labels Considered | M1 | PRK-1245 | L2.5x2.5x3 | 20.26 | 2.68 | 9.96 |
|  |  | Offset Tube | HSS4X4X4 | 32.42 | 2.82 | 14.19 |
|  |  | Offset End Plate | $0.5 \times 6$ Plate | 48.63 | 6.79 | 12.20 |
|  |  | Offset Side Plate | $0.38 \times 6$ Plate | 48.63 | 6.78 | 12.04 |
|  | мз | Platform Horzontal Pipe | PIPE_3.0 | 17.02 | 4.98 | 10.87 |
|  |  | Grating Angle | L2×2x ${ }^{\text {a }}$ | 16.21 | 2.64 | 8.64 |
|  | M4 | HRKAngle | L2.5×2.5x4 | 20.26 | 2.68 | 9.96 |
|  |  | HRK12-U | PIPE_2.0 | 11.55 | 4.17 | 8.52 |
|  |  | HRKPlate | $0.38 \times 6$ Plate | 48.63 | 6.78 | 12.04 |
|  |  | Mount Pipe | PIPE_2.5 | 13.98 | 4.53 | 9.56 |


| Appurtenances |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| AppurtenanceModel | Status | $\begin{array}{\|l\|} \hline \text { Azimuth } \\ \text { Offset } \\ (\circ, 0) \end{array}$ | Rad Elev. <br> Override <br> (ft) | Swap Width \& Depth | Area Factor |  | Qty. per Azimuth |  |  | $\begin{array}{\|c\|} \hline \text { Total } \\ \text { Qty. } \\ \text { Overide } \\ \hline \end{array}$ | $0^{\circ}$ Joints |  | $120^{\circ}$ Joints |  | $240^{\circ}$ Joints |  | Height <br> (in) | Width <br> (in) | Depth (in) | Weight <br> (Bare) <br> (Ib) | Shape | $\begin{array}{\|c\|} \hline \text { Weight } \\ \text { of (le } \\ \text { (lb) } \end{array}$ | EPA ${ }_{\text {( }}$ (Bare) (ttr ${ }^{\text {a }}$ |  | $\mathrm{EPA}_{A}(\mathrm{lcee})\left(\mathrm{ft}^{2}\right)$ |  | $\mathrm{F}_{\mathrm{A}}$ (Bare) ( lb ) |  | $\mathrm{F}_{\mathrm{A}}(\mathrm{lcee})(\mathrm{lb})$ |  |
|  |  |  |  |  | Front | Side | $0^{\circ}$ | $120^{\circ}$ | $240^{\circ}$ |  | 1 | 2 | 1 | 2 | 1 | 2 |  |  |  |  |  |  | N | T | N | T | N | T | N | T |
| AIR 21 B2A/B4P |  |  |  | $\ulcorner$ |  |  | 1 | 1 | 1 |  | a1_t | a1_b | b1_t | b1_b | g1_t | g1_b | 55 | 12 | 7.9 | 83 | Flat | 140.07 | 5.92 | 4.22 | 7.86 | 6.05 | 288.12 | 205.19 | 56.57 | 43.54 |
| AIR 21 B4A/B2P |  |  |  | $\ulcorner$ |  |  | 1 | 1 | 1 |  | a4_t | a4_b | b4_t | b4_b | g4_t | g4_b | 55 | 12 | 7.9 | 83 | Flat | 140.07 | 5.92 | 4.22 | 7.86 | 6.05 | 288.12 | 205.19 | 56.57 | 43.54 |
| APXVAARR24_43-U-NA20 |  |  |  | $\ulcorner$ |  |  | 1 | 1 | 1 |  | a2_t | a2_b | b2_t | b2_b | g2_t | g2_b | 95.9 | 24 | 8.7 | 128 | Flat | 384.65 | 20.24 | 8.89 | 23.63 | 12.03 | 984.45 | 432.27 | 170.03 | 86.56 |
| KRY 112 144/1 |  |  |  | $\ulcorner$ | 0.5 |  | 1 | 1 | 1 |  | a1_-r1 |  | b1_r1 |  | g1_r1 |  | 7 | 6 | 3 | 11 | Flat | 10.85 | 0.18 | 0.18 | 0.41 | 0.56 | 8.51 | 8.51 | 2.94 | 4.01 |
| RADIO 4449 B12/B71 |  |  |  | $\ulcorner$ | 0.5 |  | 1 | 1 | 1 |  | a2_r1 |  | b2_r1 |  | g2_r1 |  | 15 | 13.2 | 10.4 | 75 | Flat | 58.77 | 0.83 | 1.30 | 1.28 | 2.12 | 40.12 | 63.22 | 9.17 | 15.25 |

## APPENDIX B

 WIRE FRAME AND RENDERED MODELS

Envelope Only Solution

| CLS | 42284-CTNH107A-NH107/Global/Cherry Hill Rendered | SK - 1 |
| :---: | :---: | :---: |
| ML |  | May 27, 2019 at 6:28 PM |
| 42284-CTNH107A-02-MR |  | 42284-CTNH107A-02-MR.r3d |




Envelope Only Solution

| CLS | 42284-CTNH107A-NH107/Global/Cherry Hill <br> Member Labels | SK - 3 |
| :---: | :---: | :---: |
| ML |  | May 27, 2019 at 6:30 PM |
| 42284-CTNH107A-02-MR |  | 42284-CTNH107A-02-MR.r3d |






 Envelope Only Solution

| CLS |  | SK - 9 |
| :--- | :---: | :--- | :--- |
| ML |  |  |
| 42284-CTNH107A-02-MR | 42284-CTNH107A-NH107/Global/Cherry Hill | May 27, 2019 at 6:34 PM |
|  | Envelope Member Check Results - Shear | 42284-CTNH107A-02-MR.r3d |

## APPENDIX C

SOFTWARE ANALYSIS OUTPUT

## Basic Load Cases

|  | BLC Description | Category | X Gravity | Y Gravity | Z Gravity | Joint | Point | Distribu... | Area(M. | Surface... |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Dead | DL |  |  | -1 | 24 |  |  |  |  |
| 2 | Ice Dead | RL |  |  |  | 24 |  | 72 |  |  |
| 4 | Structure Wind $0^{\circ}$ | None |  |  |  |  |  | 70 |  |  |
| 5 | Structure Wind $30^{\circ}$ | None |  |  |  |  |  | 115 |  |  |
| 6 | Structure Wind $45^{\circ}$ | None |  |  |  |  |  | 144 |  |  |
| 7 | Structure Wind $60^{\circ}$ | None |  |  |  |  |  | 140 |  |  |
| 8 | Structure Wind $90^{\circ}$ | None |  |  |  |  |  | 58 |  |  |
| 9 | Structure Wind $120^{\circ}$ | None |  |  |  |  |  | 140 |  |  |
| 10 | Structure Wind $135^{\circ}$ | None |  |  |  |  |  | 144 |  |  |
| 11 | Structure Wind $150^{\circ}$ | None |  |  |  |  |  | 115 |  |  |
| 12 | Structure Wind w/ Ice $0^{\circ}$ | None |  |  |  |  |  | 70 |  |  |
| 13 | Structure Wind w/ Ice $30^{\circ}$ | None |  |  |  |  |  | 118 |  |  |
| 14 | Structure Wind w/ Ice $45^{\circ}$ | None |  |  |  |  |  | 144 |  |  |
| 15 | Structure Wind w/ Ice $60^{\circ}$ | None |  |  |  |  |  | 140 |  |  |
| 16 | Structure Wind w/ Ice $90^{\circ}$ | None |  |  |  |  |  | 59 |  |  |
| 17 | Structure Wind w/ Ice $120^{\circ}$ | None |  |  |  |  |  | 140 |  |  |
| 18 | Structure Wind w/ Ice $135{ }^{\circ}$ | None |  |  |  |  |  | 144 |  |  |
| 19 | Structure Wind w/ Ice $150^{\circ}$ | None |  |  |  |  |  | 118 |  |  |
| 20 | Antenna Wind $0^{\circ}$ | None |  |  |  | 24 |  |  |  |  |
| 21 | Antenna Wind $30^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 22 | Antenna Wind $45^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 23 | Antenna Wind $60^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 24 | Antenna Wind $90^{\circ}$ | None |  |  |  | 24 |  |  |  |  |
| 25 | Antenna Wind $120^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 26 | Antenna Wind $135^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 27 | Antenna Wind $150^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 28 | Antenna Wind w/ Ice $0^{\circ}$ | None |  |  |  | 24 |  |  |  |  |
| 29 | Antenna Wind w/ Ice $30^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 30 | Antenna Wind w/ Ice $45^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 31 | Antenna Wind w/ Ice $60^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 32 | Antenna Wind w/ Ice $90^{\circ}$ | None |  |  |  | 24 |  |  |  |  |
| 33 | Antenna Wind w/ Ice $120^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 34 | Antenna Wind w/ Ice $135^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 35 | Antenna Wind w/ Ice $150^{\circ}$ | None |  |  |  | 48 |  |  |  |  |
| 39 | Maintenance Live 500 (1) | OL1 |  |  |  | 1 |  |  |  |  |
| 40 | Maintenance Live 500 (2) | OL2 |  |  |  | 1 |  |  |  |  |
| 41 | Maintenance Live 500 (3) | OL3 |  |  |  | 1 |  |  |  |  |
| 42 | Maintenance Live 500 (4) | OL4 |  |  |  | 1 |  |  |  |  |

## Load Combinations

## Description

S... P... S... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa... B... Fa.. | 1 | DISPLAY $\left(1.0 D+1.0 W \_0^{\circ}\right)$ Yes | $Y$ |  | $D L$ | 1 | 20 | 1 |
| :--- | :--- | :--- | :--- | :--- | :--- | :--- | :--- |



Company
Designer
Job Number Model Name

CLS
ML
42284-CTNH107A-02-MR
42284-CTNH107A-NH107/Global/Cherry Hill

May 27, 2019
6:34 PM
Checked By: CAR

## Load Combinations (Continued)



## Load Combinations (Continued)

|  | Description S |  |  | B... |  |  |  |  |  |  |  |  | a... |  | Fa... | B... | Fa... | B... Fa... | . B .. | Fa.. | B... |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 71 | 1.2D + 1.5Lm_3 + 1.0Wm...Y | Yes | Y | DL | 1.2 | 8 | . 056 | 24 | . 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 72 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm}$... Y | Yes | Y | DL | 1.2 | 9 | . 056 | 25 | . 056 | O. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 73 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm} \ldots . . \mathrm{Y}$ | Yes | Y | DL | 1.2 | 10 | 056 | 26 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 74 | 1.2D + 1.5Lm_3+1.0Wm... Y | Yes | Y | DL | 1.2 | 11 | . 056 | 27 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 75 | 1.2D + 1.5Lm_3 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 4 | -. 056 | 20 | - 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 76 | 1.2D + 1.5Lm_3+1.0Wm... Y | Yes | Y | DL | 1.2 | 5 | -. 056 | 21 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 77 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $3+1.0 \mathrm{Wm} . . . \mathrm{Y}$ | Yes | Y | DL | 1.2 | 6 | -. 056 | 22 | - 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 78 | 1.2D + 1.5Lm_3+1.0Wm... Y | Yes | Y | DL | 1.2 | 7 | -. 056 | 23 | - 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 79 | 1.2D + 1.5Lm_3 + 1.0Wm...Y | Yes | Y | DL | 1.2 | 8 | -. 056 | 24 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 80 | 1.2D + 1.5Lm_3 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 9 | -. 056 | 25 | -. 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 81 | 1.2D + 1.5Lm_3 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 10 | -. 056 | 26 | - 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 82 | 1.2D + 1.5Lm_3 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 11 | -. 056 | 27 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 83 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_4+1.0 \mathrm{Wm} . . . \mathrm{Y}$ | Yes | Y | DL | 1.2 | 4 | . 056 | 20 | . 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 84 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 5 | . 056 | 21 | . 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 85 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 6 | . 056 | 22 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 86 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_4+1.0 \mathrm{Wm}$... Y | Yes | Y | DL | 1.2 | 7 | . 056 | 23 | . 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 87 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 8 | . 056 | 24 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 88 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 9 | . 056 | 25 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 89 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $4+1.0 \mathrm{Wm} \ldots \mathrm{}$. Y | Yes | Y | DL | 1.2 | 10 | . 056 | 26 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 90 | $1.2 \mathrm{D}+1.5 \mathrm{Lm}$ _ $4+1.0 \mathrm{Wm}$... Y | Yes | Y | DL | 1.2 | 11 | . 056 | 27 | . 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 91 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 4 | -. 056 | 20 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 92 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 5 | -. 056 | 21 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 93 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 6 | -. 056 | 22 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 94 | 1.2D + 1.5Lm_4 + 1.0Wm... Y | Yes | Y | DL | 1.2 | 7 | -. 056 | 23 | -. 056 | O.. | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 95 | $1.2 \mathrm{D}+1.5 \mathrm{Lm} \_4+1.0 \mathrm{Wm} . . . \mathrm{Y}$ |  | Y | DL | 1.2 | 8 | -. 056 | 24 | -. 056 |  | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 96 | 1.2D + 1.5Lm_4 + 1.0Wm... Y |  | Y | DL | 1.2 | 9 | -. 056 | 25 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 97 | 1.2D + 1.5Lm_4 + 1.0Wm...Y | Yes | Y | DL | 1.2 | 10 | -. 056 | 26 | - 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |
| 98 | 1.2D + 1.5Lm_4 + 1.0Wm...Y | Yes | Y | DL | 1.2 |  | -. 056 | 27 | -. 056 | O... | 1.5 |  |  |  |  |  |  |  |  |  |  |  |

## Hot Rolled Steel Properties

| Label |  | E [ksi] | G [ksi] | Nu | Therm (11E...Density[k/ft... Yield[ksi] |  |  | Ry | Fu[ksi] Rt |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | . 49 | 36 | 1.5 | 58 | 1.2 |
| 2 | A572 Gr. 50 | 29000 | 11154 | . 3 | . 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 3 | A992 | 29000 | 11154 | . 3 | . 65 | 49 | 50 | 1.1 | 65 | 1.1 |
| 4 | A500 Gr.B RND | 29000 | 11154 | . 3 | 65 | . 527 | 42 | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | . 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | 3 | . 65 | 49 | 35 | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | . 3 | . 65 | 49 | 50 | 1.4 | 65 | 1.3 |

Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design | A [in | lyy [in | lzz [in4] J [in4] |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Platform Horzontal Pi.. | PIPE 3.0 | Beam | Pipe | A53 Gr.B | Typical | 2.07 | 2.85 | 2.85 | 5.69 |
| 2 | Offset Tube | HSS4X4X4 | Beam | SquareTube | A36 Gr. 36 | Typical | 3.37 | 7.8 | 7.8 | 12.8 |
| 3 | Offset Side Plate | 0.38 X 6 Plate | Beam | RECT | A36 Gr. 36 | Typical | 2.28 | 027 | 6.84 | 105 |
| 4 | Grating Angle | L2x2x3 | Beam | Single Angle | A36 Gr. 36 | Typical | 722 | . 271 | 271 | 009 |
| 5 | Mount Pipe | PIPE 2.5 | Beam | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 6 | Offset End Plate | $0.5 \times 6$ Plate | Beam | RECT | A36 Gr. 36 | Typical | 3 | 063 | 9 | 237 |
| 7 | HRK12-U | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | 627 | 1.25 |
| 8 | HRKPlate | $0.38 \times 6$ Plate | Beam | RECT | A36 Gr. 36 | Typical | 2.28 | 027 | 6.84 | 105 |
| 9 | HRKAngle | L2.5x2.5x4 | Beam | Single Angle | A36 Gr. 36 | Typical | 1.19 | . 692 | . 692 | 026 |
| 10 | PRK-1245 | L2.5x2.5x3 | Beam | Single Angle | A36 Gr. 36 | Typical | . 901 | . 535 | 535 | 011 |

## Hot Rolled Steel Design Parameters

|  | Label | Shape | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp top[in] | Lcomp bot[in] | L-torq... | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M16 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 2 | M18 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 3 | M19 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 4 | M21 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 5 | M22 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 6 | M24 | PRK-1245 | 47.94 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 7 | M25 | Offset Tube | 62.507 |  |  |  |  |  |  |  |  | Lateral |
| 8 | M26 | Offset End . | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 9 | M27 | Offset End ... | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 10 | M28 | Offset End ... | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 11 | M29 | Offset Side . | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 12 | M31 | Offset Side . | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 13 | M32 | Offset Side ... | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 14 | M33 | Offset Tube | 30.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 15 | M36 | Offset Tube | 30.687 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 16 | M38 | Offset Tube | 62.507 |  |  |  |  |  |  |  |  | Lateral |
| 17 | M39 | Offset End ... | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 18 | M40 | Offset End | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 19 | M41 | Offset End ... | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 20 | M42 | Offset Side | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 21 | M44 | Offset Side ... | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 22 | M45 | Offset Tube | 30.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 23 | M48 | Offset Tube | 30.687 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 24 | M50 | Offset Tube | 62.507 |  |  |  |  |  |  |  |  | Lateral |
| 25 | M51 | Offset End ... | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 26 | M52 | Offset End | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 27 | M53 | Offset End ... | 3.122 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 28 | M54 | Offset Side | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 29 | M56 | Offset Side . | . 875 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 30 | M57 | Offset Tube | 30.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 31 | M60 | Offset Tube | 30.687 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 32 | M62 | Platform Ho... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 33 | M65 | Platform Ho... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 34 | M68 | Platform Ho... | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 35 | M71 | Offset End ... | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 36 | M73 | Offset End | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 37 | M75 | Offset End | 4.688 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 38 | M87 | Offset Side | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 39 | M88 | Offset Side . | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 40 | M93 | Offset Side ... | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 41 | M94 | Offset Side ... | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 42 | M99 | Offset Side | 3 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 43 | M101 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 44 | M103 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 45 | M107 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 46 | M109 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 47 | M113 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 48 | M115 | Grating Angle | 50.542 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 49 | M139 | HRKAngle | 14.902 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 50 | M140 | HRKAngle | 14.902 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 51 | M141 | HRKAngle | 14.902 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 52 | M146 | HRK12-U | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 53 | M151 | HRK12-U | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 54 | M156 | HRK12-U | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 55 | M159 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 56 | M163 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |

Hot Rolled Steel Design Parameters (Continued)

|  | Label | Shape | Length[in] | Lbyy[in] | Lbzz[in] | Lcomp top[in] | Lcomp bot[in] | L-torq... | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 57 | M167 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 58 | M171 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 59 | M175 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 60 | M179 | HRKPlate | 6 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 61 | M196 | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 62 | M197 | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 63 | M198 | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 64 | M199 | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 65 | M155 | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 66 | M156A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 67 | M157A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 68 | M158A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 69 | M175A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 70 | M176A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 71 | M177A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 72 | M178A | Mount Pipe | 96 |  |  | Lbyy |  |  |  |  |  | Lateral |

## Envelope Joint Reactions

| Joint |  |  |
| :---: | :---: | :---: |
| 1 | N53 | m |
| 2 |  | m |
| 3 | N31 | m |
| 4 |  | m |
| 5 | N71 | m |
| 6 |  | m |
| 7 | N88 | m |
| 8 |  | m |
| 9 | N35 | m |
| 10 |  | m |
| 11 | N39 | m |
| 12 |  | max |
| 13 | Totals: | m |
| 14 |  | m |


|  | X [lb] | LC | Ib] | LC | Z [lb] | LC | MX | LC | M | C | ft] | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ax | 1763.059 | 6 | 5225.061 | 14 | 889.813 | 20 | -62.517 | 10 | 470.225 | 17 | 2436.388 | 18 |
| min | -2828.854 | 14 | -3389.274 | 6 | 299.188 | 12 | -1096.711 | 34 | -790.09 | 73 | -2431.551 | 10 |
| max | 1705.997 | 30 | 683.875 | 6 | 2099.251 | 30 | 202.968 | 6 | 119.256 | 6 | 158.025 | 18 |
| min | -394.738 | 6 | -2954.403 | 30 | -470.806 | 6 | -912.381 | 30 | -518.961 | 30 | -150.866 | 10 |
| max | 2213.146 | 3 | 3221.531 | 16 | 889.813 | 31 | 915.617 | 19 | 315.459 | 4 | 2436.244 | 12 |
| min | -3270.504 | 11 | -5062.431 | 8 | 295.718 | 1 | -65.093 | 11 | -908.075 | 60 | -2431.4 | 4 |
| max | 5939.584 | 3 | 1885.091 | 15 | 889.862 | 25 | 746.264 | 7 | 1096.341 | 27 | 2436.429 | 7 |
| min | -3816.84 | 11 | -1882.351 | 7 | 265.101 | 1 | -608.92 | 15 | 275.38 | 1 | -2431.588 | 15 |
| max | 1705.595 | 24 | 2954.646 | 24 | 2099.257 | 24 | 905.626 | 24 | 116.156 | 16 | 158.018 | 12 |
| min | -394.898 | 16 | -683.815 | 16 | -470.823 | 16 | -204.767 | 16 | -530.668 | 24 | -150.86 | 4 |
| max | 789.702 | 11 | 79.857 | 15 | 2099.269 | 19 | 71.553 | 7 | 1049.635 | 19 | 158.027 | 7 |
|  | -3411.617 | 19 | -79.843 | 7 | -470.853 | 11 | -67.146 | 15 | -235.427 | 11 | -150.868 | 15 |
| max | 6930.14 | 3 | 6930.007 | 15 | 8062.388 | 19 |  |  |  |  |  |  |
| min | -6930.146 | 11 | -6930.01 | 7 | 2644.218 | 1 |  |  |  |  |  |  |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

| Member |  |  | Code Che...Loc... |  | $\frac{\mathrm{LC}}{5}$ | Shear Che.$.843$ | $\begin{gathered} \text { Loc........ } \\ \hline 3 \text { y } 11 \end{gathered}$ |  | $\begin{aligned} & \text { phi*Pn...phi*Pn... } \\ & \hline 71019 \ldots 73872 \end{aligned}$ |  |  |  | Eqn |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M31 | $0.38 \times 6$ Plate |  |  |  |  |  |  | H1-1b |  |  |
| 2 | M94 | $0.38 \times 6$ Plate | . 299 | 1.5 |  | 10 | . 843 | 3 |  |  | y 16 | 71019... | 73872 | 584.82 | 9234 |  | H1-1b |
| 3 | M88 | $0.38 \times 6$ Plate | . 299 | 1.5 | 15 | . 843 | 3 | y 6 | 71019. | 73872 | 584.82 | 9234 |  | H1-1b |
| 4 | M87 | $0.38 \times 6$ Plate | . 311 | 1.5 | 18 | . 764 | 3 | y 11 | 171020. | 73872 | 584.82 | 9234 |  | H1-1b |
| 5 | M99 | $0.38 \times 6$ Plate | . 311 | 1.5 | 7 | . 764 | 3 | y 16 | 71020... | 73872 | 584.82 | 9234 |  | H1-1b |
| 6 | M93 | $0.38 \times 6$ Plate | . 311 | 1.5 | 12 | 764 | 3 | y 6 | 71020... | 73872 | 584.82 | 9234 |  | H1-1b |
| 7 | M32 | $0.38 \times 6$ Plate | . 310 | 875 | 5 | . 745 | . 875 | y 3 | 73624. | 73872 | 584.82 | 9234 |  | H1-1b |
| 8 | M56 | $0.38 \times 6$ Plate | . 296 | 875 | 10 | . 745 | . 875 | y 8 | 73624. | 73872 | 584.82 | 9234 |  | H1-1b |
| 9 | M44 | $0.38 \times 6$ Plate | . 296 | 875 | 15 | . 745 | . 875 | y 14 | 73624... | 73872 | 584.82 | 9234 |  | H1-1b |
| 10 | M42 | $0.38 \times 6$ Plate | . 251 | 875 | 12 | . 679 | . 875 | y 3 | 73624. | 73872 | 584.82 | 9234 |  | H1-1b |
| 11 | M29 | $0.38 \times 6$ Plate | . 251 | 875 | 18 | . 679 | . 875 | y 8 | 73624... | 73872 | 584.82 | 9234 |  | H1-1b |
| 12 | M54 | $0.38 \times 6$ Plate | . 251 | 875 | 7 | . 679 | . 875 | y 14 | 473624... | 73872 | 584.82 | 9234 |  | H1-1b |
| 13 | M41 | $0.5 \times 6$ Plate | . 095 | 1.479 | 8 | . 641 | 0 | y 5 | 94834... | 97200 | 1012.5 | 12150 |  | H1-1b |
| 14 | M28 | $0.5 \times 6$ Plate | . 095 | 1.479 | 14 | . 628 | 0 | y 11 | 94834. | 97200 | 1012.5 | 12150 |  | H1-1b |
| 15 | M53 | $0.5 \times 6$ Plate | . 095 | 1.479 | 3 | . 628 | 0 | y 16 | 94834. | 97200 | 1012.5 | 12150 |  | H1-1b |
| 16 | M39 | $0.5 \times 6$ Plate | . 091 | 1.479 | 8 | . 622 | 0 | y 11 | 194834. | 97200 | 1012.5 | 12150 |  | H1-1b |
| 17 | M26 | $0.5 \times 6$ Plate | . 091 | 1.479 | 14 | . 622 | 0 | y 16 | 94834. | 97200 | 1012.5 | 12150 |  | H1-1b |
| 18 | M51 | $0.5 \times 6$ Plate | . 091 | 1.479 | 3 | . 622 | 0 | y 6 | 94834. | 97200 | 1012.5 | 12150 |  | H1-1b |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

| Member |  |  | Code Che...Loc... <br> .431 94.... |  | $\begin{aligned} & \mathrm{LC} \\ & \hline 11 \\ & \hline \end{aligned}$ | $\begin{gathered} \text { Shear Che.....oc..... } \\ .299 \quad 11 \ldots . . \end{gathered}$ |  | ... phi*Pn...phi*Pn... |  | phi*Mn y-y [lb-ft] phi*M. |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 19 | M146 | PIPE 2.0 |  |  | 176295.... |  |  | $32130$ | 1871.625 | 1871.. | H3-6 |
| 20 | M151 | PIPE 2.0 | 431 | 94. |  | 6 | 296 | 11. | $116295 . .$. | 32130 | 1871.625 | 1871. | H3-6 |
| 21 | M156 | PIPE 2.0 | 431 | 94. | 16 | 296 | 11.. | 6 6295.... | 32130 | 1871.625 | 1871.... | H3-6 |
| 22 | M179 | $0.38 \times 6$ Plate | . 294 | 2.368 | 11 | 294 | 2.211 | y $1063107 .$. | 73872 | 584.82 | 9234 | H1-1b |
| 23 | M171 | $0.38 \times 6$ Plate | . 294 | 2.368 | 16 | . 294 | 2.211 | y 1563107... | 73872 | 584.82 | 9234 | H1-1b |
| 24 | M163 | $0.38 \times 6$ Plate | . 294 | 2.368 | 6 | 294 | 2.211 | y 463107. | 73872 | 584.82 | 9234 | H1-1b |
| 25 | M159 | $0.38 \times 6$ Plate | . 414 | 2.368 | 16 | 290 | 2.211 | y 1763107. | 73872 | 584.82 | 9234 | H |
| 26 | M175 | $0.38 \times 6$ Plate | . 414 | 2.368 | 6 | 280 | 2.211 | y 763107. | 73872 | 584.82 | 9234 | H1-1b |
| 27 | M167 | $0.38 \times 6$ Plate | 414 | 2.368 | 11 | 280 | 2.211 | y 1263107. | 73872 | 584.82 | 9234 | H1-1b |
| 28 | M40 | $0.5 \times 6$ Plate | . 264 | 4.688 | 8 | 268 | 4.688 | y 591950. | 97200 | 1012.5 | 12150 | H |
| 29 | M27 | $0.5 \times 6$ Plate | . 273 | 4.688 | 13 | 264 | 4.688 | y 1091950. | 97200 | 1012.5 | 12150.. | H1-1b |
| 30 | M52 | $0.5 \times 6$ Plate | 264 | 4.688 | 3 | 264 | 4.688 | y 1591950... | 97200 | 1012.5 | 12150 | H1-1b |
| 31 | M73 | $0.5 \times 6$ Plate | . 242 | 0 | 14 | 247 | 0 | y 9 91950... | 97200 | 1012.5 | 12150 | H1-1b |
| 32 | M75 | $0.5 \times 6$ Plate | 250 | 0 | 9 | 241 | 0 | y $491950 .$. | 97200 | 1012.5 | 12150 | H1-1b |
| 33 | M71 | $0.5 \times 6$ Plate | . 242 | 0 | 3 | 241 | 0 | y 1591950. | 97200 | 1012.5 | 12150 . | H1-1b |
| 34 | M198 | PIPE_2.5 | 228 | 70. | 7 | 189 | 30. | 1130038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 35 | M177A | PIPE 2.5 | . 229 | 70. | 13 | 189 | 30. | 1630038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 36 | M157A | PIPE 2.5 | 228 | 70 | 18 | 189 | 30 | 630038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 37 | M199 | PIPE 2.5 | 209 | 70. | 15 | 144 | 30. | 11 30038... | 50715 | 3596.25 | 3596.25. | H1-1b |
| 38 | M178A | PIPE 2.5 | 209 | 70. | 4 | 144 | 30. | 1630038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 39 | M158A | PIPE 2.5 | 209 | 70.. | 10 | 144 | 30. | 630038. | 50715 | 3596.25 | 3596.25. | ... H1-1b |
| 40 | M25 | HSS4X4X4 | 231 | 0 | 18 | 133 | 0 | z 1899903 | 109188 | 12663 | 12663. | H1-1b |
| 41 | M50 | HSS4X4X4 | 231 | 0 | 7 | 133 | 0 | z 799903. | 109188 | 12663 | 12663. | H1-1b |
| 42 | M38 | HSS4X4X4 | . 231 | 0 | 12 | 133 | 0 | z 1299903. | 109188 | 12663 | 12663. | H1-1b |
| 43 | M175A | PIPE 2.5 | . 270 | 70. | 6 | . 116 | 70. | 1730038. | 50715 | 3596.25 | 3596.25. | H1-1 |
| 44 | M196 | PIPE 2.5 | . 270 | 70. | 16 | 112 | 70. | 1130038. | 50715 | 3596.25 | 3596.25. | H1- |
| 45 | M155 | PIPE 2.5 | . 270 | 70 | 11 | 112 | 70 | 630038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 46 | M141 | L2.5x2.5x4 | . 357 | 14. | 16 | 107 | 14. | y 1736663.9 | 38556 | 1113.554 | 2537.... | H2-1 |
| 47 | M140 | L2.5x2.5x4 | . 362 | 14. | 5 | . 105 | 0 | y 736663.9 | 38556 | 1113.554 | 2537.... | ... H2-1 |
| 48 | M139 | L2.5x2.5x4 | . 357 | 14. | 11 | 105 | 0 | y 1236663.9 | 38556 | 1113.554 | 2537.... | ... H2-1 |
| 49 | M62 | PIPE 3.0 | . 104 | 59... | 15 | 102 | 134... | 11 28250... | 65205 | 5748.75 | 5748.75. | ... H1-1b |
| 50 | M68 | PIPE 3.0 | 104 | 59. | 4 | 102 | 134. | 1628250 | 65205 | 5748.75 | 5748.75. | H1-1b |
| 51 | M65 | PIPE 3.0 | . 105 | 59. | 9 | 102 | 134. | 628250 | 65205 | 5748.75 | 5748.75. | H1-1b |
| 52 | M197 | PIPE 2.5 | . 357 | 70. | 3 | 090 | 48 | 930038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 53 | M176A | PIPE 2.5 | . 357 | 70 | 8 | . 087 | 48 | 1430038. | 50715 | 3596.25 | 3596.25. | H1-1b |
| 54 | M156A | PIPE 2.5 | . 357 | 70 | 14 | . 087 | 48 | 330038. | 50715 | 3596.25 | 3596.25. | H1-1 |
| 55 | M60 | HSS4X] 4 | . 152 | 0 | 4 | . 063 | 27. | z 510687. | 109188 | 12663 | 12663 . | H1-1b |
| 56 | M48 | HSS4X4X4 | . 152 | 0 | 10 | . 062 | 27. | z $1010687 .$. | 109188 | 12663 | 12663. | H1-1 |
| 57 | M36 | HSS4X4X4 | . 152 | 0 | 15 | . 062 | 27. | z 1510687. | 109188 | 12663 | 12663 | H1-1b |
| 58 | M33 | HSS4X4X4 | . 129 | 30... | 29 | . 053 | 3.23 | z 1210687 ... | 109188 | 12663 | 12663. | H1-1b |
| 59 | M57 | HSS4X4X4 | . 128 | 30. | 34 | . 053 | 3.23 | z 1810687. | 109188 | 12663 | 12663 | H1-1b |
| 60 | M45 | HSS4X4X4 | . 128 | 30... | 23 | 053 | 3.23 | z $710687 .$. | 109188 | 12663 | 12663. | H1-1b |
| 61 | M101 | L2x2x3 | . 196 | 50.. | 14 | . 010 | 50... | y $339618 .$. | 23392.8 | 557.717 | 1232. | ... H2-1 |
| 62 | M113 | L2x2x3 | . 196 | 50. | 3 | . 010 | 50. | y 239618. | 23392.8 | 557.717 | 1232 | H2-1 |
| 63 | M107 | L2x2x ${ }^{\text {a }}$ | . 196 | 50... | 8 | . 010 | 50. | y 289618. | 23392.8 | 557.717 | 1232. | H2- |
| 64 | M103 | L2x2x | . 204 | 0 | 15 | . 009 | 50 | y 99618. | 23392.8 | 557.717 | 1192 | H2-1 |
| 65 | M115 | L2x2x | . 207 | 0 | 5 | . 009 | 50. | z 319618. | 23392.8 | 557.717 | 1217. | H2-1 |
| 66 | M109 | L2x2x | . 204 | 0 | 10 | . 009 | 50 | z 209618. | 23392.8 | 557.717 | 1192. | H2-1 |
| 67 | M19 | $\mathrm{L} 2.5 \times 2.5 \times 3$ | . 155 | 23.97 | 17 | . 008 | 0 | z $1817206 .$. | 29192.4 | 872.574 | 1753. | H2-1 |
| 68 | M21 | L2.5x2.5x3 | 140 | 23.97 | 27 | 008 | 0 | y $1817206 \ldots$ | 29192.4 | 872.574 | 1753. | H2-1 |
| 69 | M22 | L2.5x2.5×3 | . 153 | 23.97 | 27 | . 008 | 0 | z $1217206 .$. | 29192.4 | 872.574 | 1753. | H2-1 |
| 70 | M24 | L2.5x2.5x3 | . 146 | 23.97 | 5 | 008 | 0 | y $1217206 .$. | 29192.4 | 872.574 | 1753. | H2-1 |
| 71 | M16 | L2.5x2.5x3 | . 153 | 23.97 | 22 | . 008 | 47.94 | z $717206 .$. | 29192.4 | 872.574 | 1753. | H2-1 |
| 72 | M18 | L2.5×2.5x3 | 140 | 23.97 | 32 | 008 | 47.94 | y 717206. | 29192.4 | 872.574 | 1753. | H2-1 |

## APPENDIX D

## ADDITIONAL CALCULATIONS

CLS Group
Bolt Strength Check
AISC 14th Edition (360-10)

| Member/Node Number | Load Comb. | Tensile Load, $\mathrm{T}_{\mathrm{u}}$ (kips) | Shear Load, $\mathrm{V}_{\mathrm{u}}$ (kips) | $\begin{gathered} \text { Bolt } \\ \text { Diameter (in) } \end{gathered}$ | Number of Bolts | Shear <br> Planes <br> per Bolt | Bolt <br> Tensile Strength, $\mathrm{F}_{\mathrm{nt}}$ (ksi) | Bolt <br> Shear <br> Strength, <br> $\mathrm{F}_{\mathrm{nv}}$ (ksi) | Connected <br> Member <br> Thickness <br> (in) | Connected <br> Member <br> Edge Clear <br> Distance (in) | Connected <br> Member <br> Ultimate <br> Strength, $\mathrm{F}_{\mathrm{u}}$ <br> (ksi) | Bolt Tensile Usage | Bolt Shear Usage | Member Bearing Usage |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| M63 | Env. | 1.150 | 0.400 | 0.5 | 1 | 1 | 43.5 | 26.1 | 0.375 | 0.71875 | 58 | 18\% | 10\% | 3\% |
| M49 | Env. | 1.160 | 0.180 | 0.5 | 1 | 1 | 43.5 | 26.1 | 0.375 | 0.71875 | 58 | 18\% | 5\% | 1\% |

## APPENDIX E

## INSTALLATION SKETCHES AND MOUNT ASSEMBLY DRAWINGS

INSTALL ANTENNAS CENTERED ON THE PLATFORM BASE





| PARTS LIST |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ITEM | QTY | PART NO. | PART DESCRIPTION | LENGTH | UNIT WT. | NET WT. |
| 1 | 6 | X-LWRM | RING MOUNT WELDMENT |  | 68.16 | 408.95 |
| 2 | 66 | G58LW | 5/8" HDG LOCKWASHER |  | 0.03 | 1.72 |
| 3 | 60 | A58NUT | 5/8" HDG A325 HEX NUT |  | 0.13 | 7.78 |
| 4 | 18 | G58R-24 | 5/8" $\times 24$ " THREADED ROD (HDG.) |  | 0.55 | 9.88 |
| 5 | 18 | G58R-48 | $5 / 8{ }^{\prime \prime} \times 48^{\prime \prime}$ THREADED ROD (HDG.) |  | 0.55 | 9.88 |
| 6 | 24 | A58234 | 5/8" $\times 2$-3/4" HDG A325 HEX BOLT | $23 / 4$ in | 0.36 | 8.53 |
| 7 | 24 | A58FW | 5/8" HDG A325 FLATWASHER |  | 0.03 | 0.82 |
| 8 | 36 | X-UB1306 | 1/2" $\times 3-5 / 8$ " $\times 6$ " $\times 3$ " U-BOLT (HDG.) |  | 0.73 | 26.34 |
| 9 | 264 | G12FW | 1/2" HDG USS FLATWASHER |  | 0.03 | 8.99 |
| 10 | 252 | G12LW | 1/2" HDG LOCKWASHER |  | 0.01 | 3.50 |
| 11 | 252 | G12NUT | 1/2" HDG HEAVY 2H HEX NUT |  | 0.07 | 18.03 |
| 12 | 12 | P3096 | 2-7/8" OD X 96" Sch 40 Galvanized Pipe |  | 46.45 | 557.43 |
| 13 | 48 | X-UB1300 | 1/2" $\times 3$ " $\times 5$ " $\times 2$ " U-BOLT (HDG.) |  | 0.73 | 35.12 |
| 14 | 3 | P3150 | $3-1 / 2$ " $\times 150$ " SCH 40 GALVANIZED PIPE | 150 in | 94.80 | 284.40 |
| 15 | 3 | X-SV196 | LOW PROFILE PLATFORM CORNER |  | 212.10 | 636.31 |
| 16 | 3 | P2150 | 2-3/8" OD X 150" SCH 40 GALVANIZED PIPE | 150 in | 48.06 | 144.17 |
| 17 | 12 | SCX2 | CROSSOVER PLATE | 7 in | 4.80 | 57.56 |
| 18 | 36 | X-UB1212 | 1/2" $\times 2$-1/2" $\times 4-1 / 2^{\prime \prime} \times 2$ 2 U-BOLT (HDG.) |  | 0.73 | 26.34 |
| 19 | 15 | SCX4 | CROSSOVER PLATE | $81 / 2$ in | 6.02 | 90.32 |
| 20 | 6 | G58NUT | 5/8" HDG HEAVY 2H HEX NUT |  | 0.13 | 0.78 |
| 21 | 6 | X-253993 | PLATFORM REINFORCEMENT KIT ANGLE | $5225 / 32$ in | 14.33 | 85.99 |
| 22 | 6 | X-253992 | T-BRACKET FOR REINFORCEMENT KIT |  | 13.55 | 81.27 |
| 23 | 6 | G5802 | 5/8" $\times 2$ 2" HDG HEX BOLT GR5 |  | 0.27 | 1.62 |
| 24 | 12 | G12065 | 1/2" $\times 6$-1/2" HDG HEX BOLT GR5 FULL THREAD | $61 / 2$ in | 0.41 | 4.91 |
| 25 | 3 | X-AHCP | ANGLE HANDRAIL CORNER PLATE |  | 12.92 | 38.76 |
|  |  |  |  |  | TOTAL WT. \# | 2645.84 |

(11)
(118)
TOLERANCE NOTES
TOLERANCES ON DIMENSIONS, UNLESS OTHERWISE NOTED ARE: AWED, SHEARED AND GAS CUT EDGES $\left( \pm 0.030^{\prime \prime}\right)$ LASER CUT EDGES AND HOLES $\left( \pm 0.010^{\prime \prime}\right)$-NO CONING OF HOLES BENDS ARE $\pm 1 / 2$ DEGREE
ALL



RMQP-4096-HK


DETAIL E



## Exhibit F

## Power Density/RF Emissions Report

## Transcom Engineering, Inc.

# Radio Frequency Emissions Analysis Report 

T-MOBILE Existing Facility

## Site ID: CTNH107A

NH107/Global/Cherry Hill 150 North Main Street
Branford, CT 06405
August 13, 2019

Transcom Engineering Project Number: 737001-0043

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of FCC <br> general population <br> allowable limit: | $\mathbf{1 1 . 7 0} \%$ |

# Transcom Engineering, Inc. 

August 13, 2019

T-MOBILE
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 6009

## Emissions Analysis for Site: CTNH107A - NH107/Global/Cherry Hill

Transcom Engineering, Inc ("Transcom") was directed to analyze the proposed upgrades to the TMOBILE facility located at $\mathbf{1 5 0}$ North Main Street, Branford, CT, for the purpose of determining whether the emissions from the Proposed T-MOBILE Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limits for the $600 \& 700 \mathrm{MHz}$ bands are approximately $400 \mu \mathrm{~W} / \mathrm{cm}^{2}$ and $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$ respectively. The general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

## Transcom Engineering, Inc.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## Transcom Engineering, Inc.

## CALCULATIONS

Calculations were performed for the proposed upgrades to the T-MOBILE antenna facility located at $\mathbf{1 5 0}$ North Main Street, Branford, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65 . Since T-MOBILE is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was focused at the base of the tower. For this report the sample point is the top of a 6 -foot person standing at the base of the tower.

Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. All power values expressed and analyzed are maximum power levels expected to be used on all radios.

All emissions values for additional carriers were taken from the Connecticut Siting Council (CSC) active MPE database. Values in this database are provided by the individual carriers themselves

For each sector the following channel counts, frequency bands and power levels were utilized as shown in Table 1:

| Technology | Frequency Band | Channel Count | Transmit Power per <br> Channel (W) |
| :---: | :---: | :---: | :---: |
| UMTS | 1900 MHz (PCS) | 1 | 40 |
| GSM | 1900 MHz (PCS) | 1 | 15 |
| UMTS | $2100 \mathrm{MHz}($ AWS $)$ | 1 | 40 |
| LTE | $2100 \mathrm{MHz}($ AWS $)$ | 2 | 60 |
| LTE $/ 5 \mathrm{G}$ NR | 600 MHz | 2 | 40 |
| LTE | 700 MHz | 2 | 20 |

Table 1: Channel Data Table

## Transcom Engineering, Inc.

The following antennas listed in Table 2 were used in the modeling for transmission in the $600,700 \mathrm{MHz}$, 1900 MHz (PCS) and 2100 MHz (AWS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB for directional panel antennas, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.

| Sector | Antenna <br> Number | Antenna Make / Model | Antenna <br> Centerline <br> $(\mathrm{ft})$ |
| :---: | :---: | :---: | :---: |
| A | 1 | Ericsson AIR21 B2A/B4P | 121 |
| A | 2 | Ericsson AIR21 B4A/B2P | 121 |
| A | 3 | RFS APXVAARR24_43-U-NA20 | 121 |
| B | 1 | Ericsson AIR21 B2A/B4P | 121 |
| B | 2 | Ericsson AIR21 B4A/B2P | 121 |
| B | 3 | RFS APXVAARR24_43-U-NA20 | 121 |
| C | 1 | Ericsson AIR21 B2A/B4P | 121 |
| C | 2 | Ericsson AIR21 B4A/B2P | 121 |
| C | 3 | RFS APXVAARR24_43-U-NA20 | 121 |

Table 2: Antenna Data

All calculations were done with respect to uncontrolled / general population threshold limits.

Cable losses were factored in the calculations for this site. Since all $2100 \mathbf{M H z}$ (AWS) UMTS radios are ground mounted the following cable loss values were used. For each ground mounted $2100 \mathbf{M H z}$ (AWS) UMTS radio there was 1.83 dB of cable loss calculated into the system gains / losses for this site. These values were calculated based upon the manufacturers specifications for $\mathbf{1 7 3}$ feet of $\mathbf{1 - 5 / 8}$ " coax.

## Transcom Engineering, Inc.

## RESULTS

Per the calculations completed for the proposed T-MOBILE configurations Table 3 shows resulting emissions power levels and percentages of the FCC's allowable general population limit.

| Antenna ID | Antenna Make / Model | Frequency Bands | Antenna Gain (dBd) | Channel Count | $\qquad$ | ERP (W) | MPE \% |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna A1 | Ericsson AIR21 B2A/B4P | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | 15.9 | 3 | 95 | 3,160.83 | 0.86 |
| Antenna A2 | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B4A/B2P } \\ \hline \end{gathered}$ | 2100 MHz (AWS) | 15.9 | 2 | 120 | 4,668.54 | 1.27 |
| Antenna A3 | $\begin{gathered} \text { RFS } \\ \text { APXVAARR24_43-U-NA20 } \end{gathered}$ | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.57 |
| Sector A Composite MPE\% |  |  |  |  |  |  | 3.70 |
| Antenna B1 | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B2A/B4P } \end{gathered}$ | 1900 MHz (PCS) / <br> 2100 MHz (AWS) | 15.9 | 3 | 95 | 3,160.83 | 0.86 |
| $\begin{gathered} \text { Antenna } \\ \text { B2 } \\ \hline \end{gathered}$ | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B4A/B2P } \end{gathered}$ | 2100 MHz (AWS) | 15.9 | 2 | 120 | 4,668.54 | 1.27 |
| $\begin{gathered} \text { Antenna } \\ \text { B3 } \\ \hline \end{gathered}$ | $\begin{gathered} \text { RFS } \\ \text { APXVAARR24_43-U-NA20 } \end{gathered}$ | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.57 |
| Sector B Composite MPE\% |  |  |  |  |  |  | 3.70 |
| $\begin{aligned} & \text { Antenna } \\ & \mathrm{C} 1 \end{aligned}$ | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B2A/B4P } \end{gathered}$ | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | 15.9 | 3 | 95 | 3,160.83 | 0.86 |
| Antenna C2 | $\begin{gathered} \text { Ericsson } \\ \text { AIR21 B4A/B2P } \end{gathered}$ | 2100 MHz (AWS) | 15.9 | 2 | 120 | 4,668.54 | 1.27 |
| Antenna $\qquad$ <br> C3 | $\begin{gathered} \text { RFS } \\ \text { APXVAARR24_43-U-NA20 } \\ \hline \end{gathered}$ | $600 \mathrm{MHz} / 700 \mathrm{MHz}$ | 12.95 / 13.35 | 4 | 120 | 2,443.03 | 1.57 |
| Sector C Composite MPE\% |  |  |  |  |  |  | 3.70 |

Table 3: T-MOBILE Emissions Levels

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The Following table (table 4) shows all additional carriers on site and their MPE\% as recorded in the CSC active MPE database for this facility along with the newly calculated maximum T-MOBILE MPE contributions per this report. FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. For this site, all three sectors have the same configuration yielding the same results on all three sectors. Table 5 below shows a summary for each T-MOBILE Sector as well as the composite MPE value for the site.

| Site Composite MPE\% |  |
| :---: | :---: |
| Carrier | MPE \% |
| T-MOBILE - Max Per Sector Value | $\mathbf{3 . 7 0} \%$ |
| AT\&T / Cingular | $6.48 \%$ |
| MetroPCS | $0.53 \%$ |
| PageNet | $0.11 \%$ |
| Nextel | $0.46 \%$ |
| Clearwire | $0.10 \%$ |
| Sprint | $0.32 \%$ |
| Site Total MPE \%: | $\mathbf{1 1 . 7 0} \%$ |

Table 4: All Carrier MPE Contributions

| T-MOBILE Sector A Total: | $3.70 \%$ |
| ---: | :---: |
| T-MOBILE Sector B Total: | $3.70 \%$ |
| T-MOBILE Sector C Total: | $3.70 \%$ |
| Site Total: |  |

Table 5: Site MPE Summary

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FCC OET 65 specifies that for carriers utilizing directional antennas that the highest recorded sector value be used for composite site MPE values due to their greatly reduced emissions contributions in the directions of the adjacent sectors. Table 6 below details a breakdown by frequency band and technology for the MPE power values for the maximum calculated T-MOBILE sector(s). For this site, all three sectors have the same configuration yielding the same results on all three sectors.

| T-MOBILE _ Frequency Band/ Technology <br> Max Power Values (Per Sector) | \# <br> Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Frequency (MHz) | Allowable MPE ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ) | Calculated \% MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-Mobile 1900 MHz (PCS) UMTS | 1 | 1,556.18 | 121 | 4.23 | 1900 MHz (PCS) | 1000 | 0.42\% |
| T-Mobile 1900 MHz (PCS) GSM | 1 | 583.57 | 121 | 1.59 | 1900 MHz (PCS) | 1000 | 0.16\% |
| T-Mobile 2100 MHz (AWS) UMTS | 1 | 1,021.08 | 121 | 2.78 | 2100 MHz (AWS) | 1000 | 0.28\% |
| T-Mobile 2100 MHz (AWS) LTE | 2 | 2,334.27 | 121 | 12.69 | 2100 MHz (AWS) | 1000 | 1.27\% |
| T-Mobile 600 MHz LTE / 5G NR | 2 | 788.97 | 121 | 4.29 | 600 MHz | 400 | 1.07\% |
| T-Mobile 700 MHz LTE | 2 | 432.54 | 121 | 2.35 | 700 MHz | 467 | 0.50\% |
|  |  |  |  |  |  | Total: | 3.70\% |

Table 6: T-MOBILE Maximum Sector MPE Power Values

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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-MOBILE facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| T-MOBILE Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector A: | $3.70 \%$ |
| Sector B: | $3.70 \%$ |
| Sector C: | $3.70 \%$ |
| T-MOBILE Maximum | $3.70 \%$ |
| Total (per sector): |  |
| Site Total: | $11.70 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{1 1 . 7 0} \%$ of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


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