

10 INDUSTRIAL AVENUE, SUITE 3 MAHWAH, NJ 07430

PHONE: 201.684.0055 FAX: 201.684.0066

July 16, 2019

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: Notice of Exempt Modification 50 Maple Street, Branford CT Latitude 41.274244 Longitude -72.813566 T-Mobile site: CT11328F / L600

Dear Ms. Bachman:

T-Mobile currently maintains (6) antennas at the 96-foot level of the existing 100-foot smokestack. The smokestack and the property are owned by Marine Systems LLC. T-Mobile now intends to replace 3 of its existing antennas with (3) 600/700 MHz antennas. The new antennas would be installed at the 96 foot level of the tower.

Planned Modifications:

Tower: Remove: (6) coax

Remove and Replace:

(3) LNX 6515-A1M Antenna (REMOVE) - (3) RFS-APXVAARR24_43U-NA20 Antenna 600/700 MHz (REPLACE)
(3) Ericsson RRUS-11 B12 remote radio units (REMOVE) - Ericsson RADIO 4449 B71+B12 (REPLACE)

Install New: (3) 6x12 hybrid lines

Existing to Remain: (3) Ericsson AIR 21, 1.3M, B2P/B4A (3) TMAs

<u>Ground:</u> Remove and Replace: (1) DUS41 and (1) XMU with (1) BB6630 Install New: (1) BB6630 T-Mobile Previously received approvals from the Town of Branford on January 11, 2010 to install antennas and associated equipment on the existing brick chimney. A copy o the approval is attached, however the Siting Council indicated that brick chimney meets the regulatory definition of a "tower" as the chimney is no longer in use and here are cellular antennas affixed thereto. Accordingly, please accept this letter as notification pursuant to Regulations of Connecticut State Agencies 16-50ss, of T-Mobile's intent to share a telecommunications facility pursuant to R.C.SA. § 16-SOj-88.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies§ 16-SOj-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.SA. § 16-SOj-73, a copy of this letter is being sent to James B. Cosgrove, First Selectman of the Town of Branford, as well as Harry Smith, Town Planner for the Town of Branford and Marine Systems, Inc., property owner

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S;A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.

2. The proposed modifications will not require the extension of the site boundary.

3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.

5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.

6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Elizabeth Jamieson

Elizabeth Jamieson Transcend Wireless 10 Industrial Ave., Suite 3 Mahwah, New Jersey 07430 860-605-7808 EJamieson@TranscendWireless.com

Cc: James B. Cosgrove, First Selectman, Town of Branford Harry Smith, Town Planner, Town of Branford Maine Systems Inc, property and structure owner

Exhibit A Original Facility Approval

PLANNING AND ZONING COMMISSION TOWN OF BRANFORD TOWN HALL DRIVE P.O. BOX 150 Branford, Connecticut 06405 Telephone: (203) 488-1255 Fax: (203) 315-2188

NOTICE OF DECISION

January 11, 2010

Clearwire by Maxton Technology Attention: Thomas F. Flynn III 1296 Blue Hills Avenue Bloomfield, Connecticut 06002

SUBJECT: <u>Site Plan</u>

APPLICATION: <u>#09-12.4</u> ADDRESS: <u>50 Maple Street</u>

APPLICANT: <u>Clearwire Wireless LLC d/b/a Clearwire</u>

OWNER OF RECORD: Marine Systems, Inc.

Dear. Sir:

At a meeting of the Branford Planning & Zoning Commission held on <u>Thursday</u>, <u>January 7, 2010</u> the Commission voted to:

X Approve your above subject application.

Very truly yours,

Shirley Rasmussen Town Planner

NOTE: Site Plan shall become null and void in the event the applicant fails to obtain a building permit within one (1) year of date of approval. (Per Section 31.7 of the Branford Zoning Regulations)

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Exhibit B Property card

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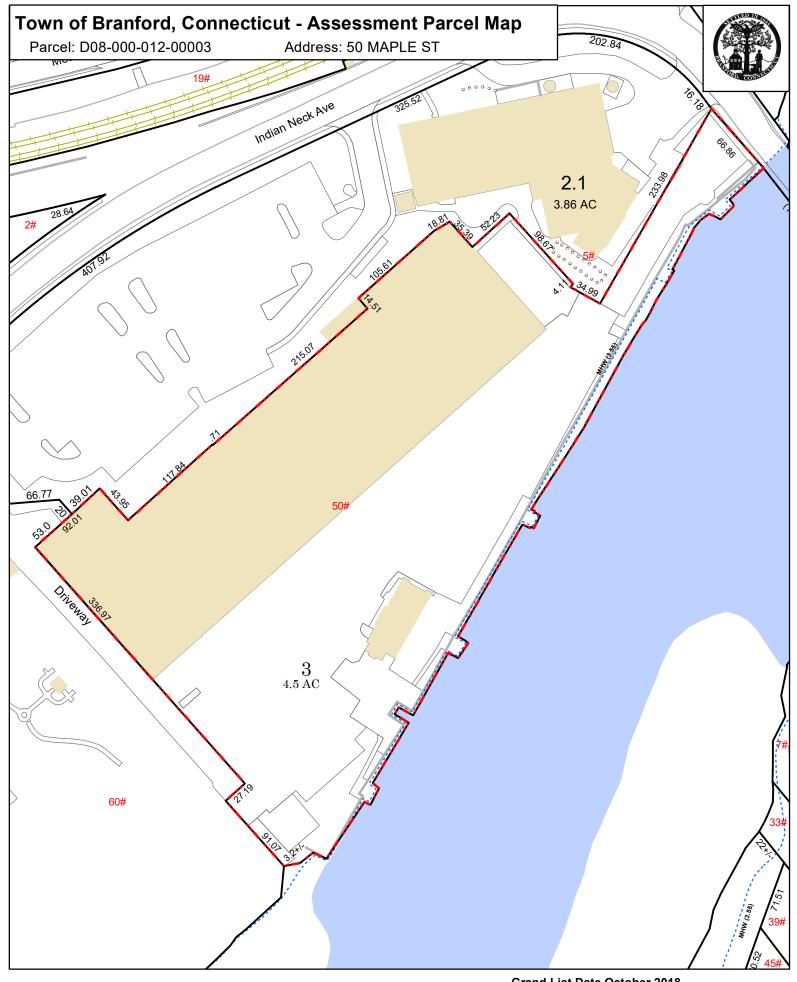
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| Interior Floo | | | Hardwood | | Adj. Bas | e Kate: | | | 103.66 | | | | | | | | |
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Approximate Scale: 1 inch : 100 feet

Grand List Date October 2018

Disclaimer: All information is subject to verification by any user. The Town of Branford and its mapping contractors assume no legal responsibility for the information contained herein.

Exhibit C Construction Drawings

- Mobile-WIRELESS COMMUNICATIONS FACILITY MARINE SYS. SMOKE STACK CT11328F 50 MAPLE STREET BRANFORD, CT 06405

GENERAL NOTES

- 1. ALL WORK SHALL BE IN ACCORDANCE WITH THE 2015 INTERNATIONAL BUILDING CODE AS MODIFIED BY THE 2018 CONNECTICUT SUPPLEMENT, INCLUDING THE TIA/EIA-222 REVISION "G" "STRUCTURAL STANDARDS FOR STEEL ANTENNA TOWERS AND SUPPORTING STRUCTURES." 2017 CONNECTICUT FIRE SAFETY CODE, 2017 NATIONAL ELECTRICAL CODE AND LOCAL CODES.
- CONTRACTOR SHALL REVIEW ALL DRAWINGS AND SPECIFICATIONS IN THE CONTRACT DOCUMENT SET. CONTRACTOR SHALL COORDINATE ALL WORK SHOWN IN THE SET OF DRAWINGS. THE CONTRACTOR SHALL PROVIDE A COMPLETE SET OF DRAWINGS TO ALL SUBCONTRACTORS AND ALL RELATED PARTIES. THE SUBCONTRACTORS SHALL EXAMINE ALL THE DRAWINGS AND SPECIFICATIONS FOR THE INFORMATION THAT AFFECTS THEIR WORK.
- CONTRACTOR SHALL PROVIDE A COMPLETE BUILD-OUT WITH ALL FINISHES, STRUCTURAL, MECHANICAL, AND ELECTRICAL COMPONENTS AND PROVIDE ALL ITEMS AS SHOWN OR INDICATED ON THE DRAWINGS OR IN THE WRITTEN SPECIFICATIONS.
- CONTRACTOR SHALL FURNISH ALL MATERIAL, LABOR AND EQUIPMENT TO COMPLETE THE WORK AND FURNISH A COMPLETED JOB ALL IN ACCORDANCE WITH LOCAL AND STATE GOVERNING AUTHORITIES AND OTHER AUTHORITIES HAVING LAWFUL JURISDICTION OVER THE WORK.
- CONTRACTOR SHALL SECURE AND PAY FOR ALL PERMITS AND ALL INSPECTIONS REQUIRED AND SHALL ALSO PAY FEES REQUIRED FOR THE GENERAL CONSTRUCTION, PLUMBING, ELECTRICAL AND HVAC. PERMITS SHALL BE PAID FOR BY THE RESPECTIVE SUBCONTRACTORS.
- CONTRACTOR SHALL MAINTAIN A CURRENT SET OF DRAWINGS AND SPECIFICATIONS ON SITE AT ALL TIMES AND INSURE DISTRIBUTION OF NEW DRAWINGS TO SUBCONTRACTORS AND OTHER RELEVANT PARTIES AS SOON AS THEY ARE MADE AVAILABLE. ALL OLD DRAWINGS SHALL BE MARKED VOID AND REMOVED FROM THE CONTRACT AREA. THE CONTRACTOR SHALL FURNISH AN 'AS-BUILT' SET OF DRAWINGS TO OWNER UPON COMPLETION OF PROJECT.
- LOCATION OF EQUIPMENT, AND WORK SUPPLIED BY OTHERS THAT IS DIAGRAMMATICALLY INDICATED ON THE DRAWINGS SHALL BE DETERMINED BY THE CONTRACTOR. THE CONTRACTOR SHALL DETERMINE LOCATIONS AND DIMENSIONS SUBJECT TO STRUCTURAL CONDITIONS AND WORK OF THE SUBCONTRACTORS.
- THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY.
- DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- 10. ALL UTILITY WORK SHALL BE IN ACCORDANCE WITH LOCAL UTILITY COMPANY REQUIREMENTS AND SPECIFICATIONS.

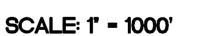
- 11. ALL EQUIPMENT AND PRODUCTS PURCHASED ARE TO BE REVIEWED BY CONTRACTOR AND ALL APPLICABLE SUBCONTRACTORS FOR ANY CONDITION PER MFR.'S RECOMMENDATIONS. CONTRACTOR TO SUPPLY THESE ITEMS AT NO COST TO OWNER OR CONSTRUCTION MANAGER.
- 12. ANY AND ALL ERRORS, DISCREPANCIES, AND 'MISSED" ITEMS ARE TO BE BROUGHT TO THE ATTENTION OF THE T-MOBILE CONSTRUCTION MANAGER DURING THE BIDDING PROCESS BY THE CONTRACTOR. ALL THESE ITEMS ARE TO BE INCLUDED IN THE BID. NO 'EXTRA' WILL BE ALLOWED FOR MISSED ITEMS.
- 13. CONTRACTOR SHALL BE RESPONSIBLE FOR ALL ON-SITE SAFETY FROM THE TIME THE JOB IS AWARDED UNTIL ALL WORK IS COMPLETE AND ACCEPTED BY THE OWNER.
- 14. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE CONSTRUCTION MANAGER FOR REVIEW.
- 15. THE CONTRACTOR SHALL FIELD VERIFY ALL DIMENSIONS, ELEVATIONS, ANGLES, AND EXISTING CONDITIONS AT THE SITE, PRIOR TO FABRICATION AND/OR INSTALLATION OF ANY WORK IN THE CONTRACT AREA.
- 16. COORDINATION, LAYOUT, FURNISHING AND INSTALLATION OF CONDUIT AND ALL APPURTENANCES REQUIRED FOR PROPER INSTALLATION OF ELECTRICAL AND TELECOMMUNICATION SERVICE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR.
- 17. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 18. THE CONTRACTOR SHALL CONTACT "CALL BEFORE YOU DIG" AT LEAST 48 HOURS PRIOR TO ANY EXCAVATIONS AT 1-800-922-4455. ALL UTILITIES SHALL BE IDENTIFIED AND CLEARLY MARKED. CONTRACTOR SHALL MAINTAIN AND PROTECT MARKED UTILITIES THROUGHOUT PROJECT COMPLETION.
- 19. CONTRACTOR SHALL COMPLY WITH OWNERS ENVIRONMENTAL ENGINEER ON ALL METHODS AND PROVISIONS FOR ALL EXCAVATION ACTIVITIES INCLUDING SOIL DISPOSAL. ALL BACKFILL MATERIALS TO BE PROVIDED BY THE CONTRACTOR.

SITE DIRECTIONS

FROM: 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002

- HEAD NORTH ON GRIFFIN ROAD S. TOWARD HARTMAN RD.
- TAKE THE 2ND RIGHT ONTO DAY HILL RD. MERGE ONTO I-91 S TOWARD HARTFORD
- TAKE CT-99 EXIT, EXIT 24 TOWARD WETHERSFIELD/ROCKY HILL
- TURN LEFT ONTO SILAS DEANE HWY/CT-99
- MERGE ONTO I-91 S via THE RAMP ON THE LEFT TOWARD NEW HAVEN MERGE ONTO 1-95 N via THE EXIT ON THE LEFT TOWARD NEW LONDON
- . TAKE THE US-1 EXIT. EXIT 53. TOWARD SHORT BEACH/CT-142/CT-146
- MERGE ONTO BRANFORD CONN. 10. TAKE THE 1ST RIGHT ONTO W MAIN ST/US-1 S
- 11. TAKE THE 1ST LEFT ONTO SHORT BEACH RD/CT-142
- 12. TURN LEFT ONTO MAPLE ST
- 13. TURN RIGHT ONTO INDIAN NECK AVE. 14. 50 MAPLE ST BRANFORD, CT 06405-3511, 50 MAPLE ST

VICINITY MAP



TO: 50 MAPLE STREET BRANFORD, CT 06405

0.30 MI.

3.64 MI

14.42 MI

0.28 MI

0.00 MI

4.55 MI

0.43 MI

0.62 MI.

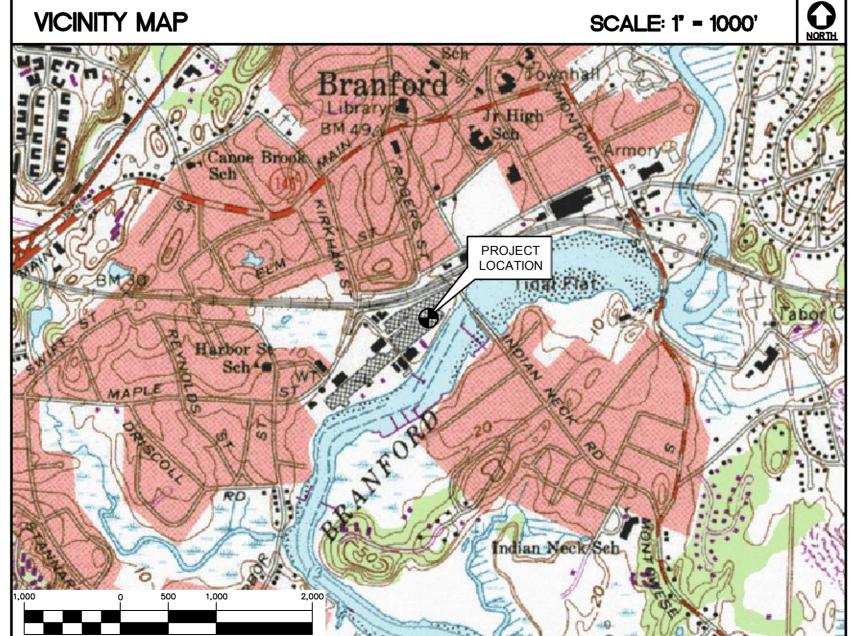
0.10 MI.

0.22 MI.

0.72 MI.

0.17 MI.

31.32 MI.



T-MOBILE RF CONFIGURATION

67D02C_2xAIR+10P

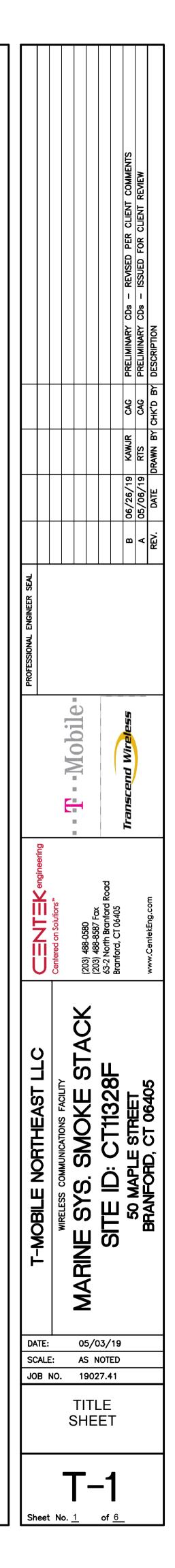
PROJECT SUMMARY

- 1. THE PROPOSED SCOPE OF WORK CONSISTS OF A MODIFICATION TO THE EXISTING UNMANNED TELECOMMUNICATIONS FACILITY INCLUDING THE FOLLOWING:
- A. REPLACE (1) DUS41 AND (1) XMU WITH (1) BB 6630
- B. INSTALL (1) ADDITIONAL BB 6630 C. INSTALL (3) NEW 6X12 HYBRID CABLES
- D. REMOVE (6) COAX CABLES
- E. REPLACE (3) LB DUAL ANTENNA WITH (3) LB/MB OCTA 8' ANTENNA . REMOVE (3) RRUS11 B12
- G. INSTALL (3) RADIO 4449 B71+B12

PROJECT INFORMATION

| SITE NAME: | MARINE SYS. SMOKE STACK |
|----------------------|--|
| SITE ID: | CT11328F |
| SITE ADDRESS: | 50 MAPLE STREET BRANFORD, CT 06405 |
| APPLICANT: | T—MOBILE NORTHEAST, LLC 35 GRIFFIN ROAD SOUTH BLOOMFIELD, CT 06002 |
| CONTACT PERSON: | DAN REID (PROJECT MANAGER) TRANSCEND WIRELESS, LLC (203) 592-8291 |
| ENGINEER: | CENTEK ENGINEERING, INC. 63–2 NORTH BRANFORD RD. BRANFORD, CT 06405 |
| PROJECT COORDINATES: | LATITUDE: 41°–16'–27.56" N LONGITUDE: 72°–48'–49.05" W GROUND ELEVATION: 08'± AMSL |
| | SITE COORDINATES AND GROUND ELEVATION REFERENCED FROM GOOGLE EARTH. |

| SHEET | INDEX | |
|----------|---------------------------------|------|
| SHT. NO. | DESCRIPTION | REV. |
| T-1 | TITLE SHEET | в |
| | | |
| N-1 | DESIGN BASIS AND SITE NOTES | В |
| | | |
| C-1 | SITE LOCATION PLAN | В |
| C-2 | COMPOUND PLAN AND ELEVATION | В |
| C-3 | ANTENNA MOUNTING AND ELEVATIONS | В |
| E-1 | TYPICAL ELECTRICAL DETAILS | В |



DESIGN BASIS:

GOVERNING CODE: 2015 INTERNATIONAL BUILDING (IBC) AS MODIFIED BY THE 2018 CT STATE BUILDING CODE AND AMENDMENTS.

- 1. DESIGN CRITERIA:
- WIND LOAD: PER TIA 222 G (ANTENNA MOUNTS): 90-105 MPH (3 SECOND GUST) •
- RISK CATEGORY: II (BASED ON IBC TABLE 1604.5)
- ULTIMATE DESIGN SPEED (OTHER STRUCTURE): 130 MPH (Vasd) (EXPOSURE B/IMPORTANCE FACTOR 1.0 BASED ON ASCE 7-10) PER 2015 INTERNATIONAL BUILDING CODE (IBC) AS MODIFIED BY THE 2018 CONNECTICUT STATE BUILDING CODE.
- SEISMIC LOAD (DOES NOT CONTROL): PER ASCE 7-10 MINIMUM DESIGN LOADS FOR ٠ BUILDING AND OTHER STRUCTURES.

GENERAL NOTES

- 1. ALL CONSTRUCTION SHALL BE IN COMPLIANCE WITH THE GOVERNING BUILDING CODE.
- 2. DRAWINGS INDICATE THE MINIMUM STANDARDS, BUT IF ANY WORK SHOULD BE INDICATED TO BE SUBSTANDARD TO ANY ORDINANCES, LAWS, CODES, RULES, OR REGULATIONS BEARING ON THE WORK, THE CONTRACTOR SHALL INCLUDE IN HIS WORK AND SHALL EXECUTE THE WORK CORRECTLY IN ACCORDANCE WITH SUCH ORDINANCES, LAWS, CODES, RULES OR REGULATIONS WITH NO INCREASE IN COSTS.
- 3. BEFORE BEGINNING THE WORK, THE CONTRACTOR IS RESPONSIBLE FOR MAKING SUCH INVESTIGATIONS CONCERNING PHYSICAL CONDITIONS (SURFACE AND SUBSURFACE) AT OR CONTIGUOUS TO THE SITE WHICH MAY AFFECT PERFORMANCE AND COST OF THE WORK.
- 4. DIMENSIONS AND DETAILS SHALL BE CHECKED AGAINST EXISTING FIELD CONDITIONS.
- 5. THE CONTRACTOR SHALL VERIFY AND COORDINATE THE SIZE AND LOCATION OF ALL OPENINGS, SLEEVES AND ANCHOR BOLTS AS REQUIRED BY ALL TRADES.
- 6. ALL DIMENSIONS, ELEVATIONS, AND OTHER REFERENCES TO EXISTING STRUCTURES, SURFACE, AND SUBSURFACE CONDITIONS ARE APPROXIMATE. NO GUARANTEE IS MADE FOR THE ACCURACY OR COMPLETENESS OF THE INFORMATION SHOWN. THE CONTRACTOR SHALL VERIFY AND COORDINATE ALL DIMENSIONS, ELEVATIONS, ANGLES WITH EXISTING CONDITIONS AND WITH ARCHITECTURAL AND SITE DRAWINGS BEFORE PROCEEDING WITH ANY WORK.
- 7. AS THE WORK PROGRESSES, THE CONTRACTOR SHALL NOTIFY THE OWNER OF ANY CONDITIONS WHICH ARE IN CONFLICT OR OTHERWISE NOT CONSISTENT WITH THE CONSTRUCTION DOCUMENTS AND SHALL NOT PROCEED WITH SUCH WORK UNTIL THE CONFLICT IS SATISFACTORILY RESOLVED.
- 8. THE CONTRACTOR SHALL COMPLY WITH ALL APPLICABLE SAFETY CODES AND REGULATIONS DURING ALL PHASES OF CONSTRUCTION. THE CONTRACTOR IS SOLELY RESPONSIBLE FOR PROVIDING AND MAINTAINING ADEQUATE SHORING, BRACING, AND BARRICADES AS MAY BE REQUIRED FOR THE PROTECTION OF EXISTING PROPERTY, CONSTRUCTION WORKERS, AND FOR PUBLIC SAFETY.
- 9. THE CONTRACTOR IS SOLELY RESPONSIBLE TO DETERMINE CONSTRUCTION PROCEDURE AND SEQUENCE, AND TO ENSURE THE SAFETY OF THE EXISTING STRUCTURES AND ITS COMPONENT PARTS DURING CONSTRUCTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, BRACING, UNDERPINNING, ETC. THAT MAY BE NECESSARY. MAINTAIN EXISTING SITE OPERATIONS, COORDINATE WORK WITH NORTHEAST UTILITIES
- 10. THE STRUCTURE IS DESIGNED TO BE SELF-SUPPORTING AND STABLE AFTER FOUNDATION REMEDIATION WORK IS COMPLETE. IT IS THE CONTRACTOR'S SOLE RESPONSIBILITY TO DETERMINE ERECTION PROCEDURE AND SEQUENCE AND TO ENSURE THE SAFETY OF THE STRUCTURE AND ITS COMPONENT PARTS DURING ERECTION. THIS INCLUDES THE ADDITION OF WHATEVER SHORING, TEMPORARY BRACING, GUYS OR TIEDOWNS, WHICH MIGHT BE NECESSARY.
- 11. ALL DAMAGE CAUSED TO ANY EXISTING STRUCTURE SHALL BE THE SOLE RESPONSIBILITY OF THE CONTRACTOR. THE CONTRACTOR WILL BE HELD LIABLE FOR ALL REPAIRS REQUIRED FOR EXISTING STRUCTURES IF DAMAGED DURING CONSTRUCTION ACTIVITIES.
- 12. SHOP DRAWINGS, CONCRETE MIX DESIGNS, TEST REPORTS, AND OTHER SUBMITTALS PERTAINING TO STRUCTURAL WORK SHALL BE FORWARDED TO THE OWNER FOR REVIEW BEFORE FABRICATION AND/OR INSTALLATION IS MADE. SHOP DRAWINGS SHALL INCLUDE ERECTION DRAWINGS AND COMPLETE DETAILS OF CONNECTIONS AS WELL AS MANUFACTURER'S SPECIFICATION DATA WHERE APPROPRIATE. SHOP DRAWINGS SHALL BE CHECKED BY THE CONTRACTOR AND BEAR THE CHECKER'S INITIALS BEFORE BEING SUBMITTED FOR REVIEW.
- 13. NO DRILLING WELDING OR TAPING ON EVERSOURCE OWNED EQUIPMENT.
- 14. REFER TO DRAWING T1 FOR ADDITIONAL NOTES AND REQUIREMENTS.

STRUCTURAL STEEL

- (FY = 46 KSI)
- (FY = 42 KSI)PIPE---ASTM A53 (FY = 35 KSI)
- CONNECTION BOLTS---ASTM A325-N G. U-BOLTS---ASTM A36
- ANCHOR RODS---ASTM F 1554 I. WELDING ELECTRODE---ASTM E 70XX
- ELEVATIONS AND DETAILS.
- 4. PROVIDE ALL PLATES, CLIP ANGLES, CLOSURE PIECES, STRAP ANCHORS,
- 5. FIT AND SHOP ASSEMBLE FABRICATIONS IN THE LARGEST PRACTICAL SECTIONS FOR
- DELIVERY TO SITE.
- DISTORTIONS OR DEFECTS.
- ACCORDANCE WITH ASTM 780.
- COATINGS" ON IRONS AND STEEL PRODUCTS.
- HARDWARE".
- REVIEW.
- UNLESS OTHERWISE ON THE DRAWINGS.
- 14. SHOP CONNECTIONS SHALL BE WELDED OR HIGH STRENGTH BOLTED.
- TRANSFER LOAD OVER ENTIRE CROSS SECTION.
- 16. FABRICATE BEAMS WITH MILL CAMBER UP.

- ENGINEER WITHIN TEN (10) WORKING DAYS OF THE DATE OF INSPECTION.

1. ALL STRUCTURAL STEEL IS DESIGNED BY ALLOWABLE STRESS DESIGN (ASD)

STRUCTURAL STEEL (W SHAPES) -- ASTM A992 (FY = 50 KSI) STRUCTURAL STEEL (OTHER SHAPES) -- ASTM A36 (FY = 36 KSI) C. STRUCTURAL HSS (RECTANGULAR SHAPES)---ASTM A500 GRADE B,

D. STRUCTURAL HSS (ROUND SHAPES)---ASTM A500 GRADE B,

2. CONTRACTOR TO REVIEW ALL SHOP DRAWINGS AND SUBMIT COPY TO ENGINEER FOR APPROVAL. DRAWINGS MUST BEAR THE CHECKER'S INITIALS BEFORE SUBMITTING TO THE ENGINEER FOR REVIEW. SHOP DRAWINGS SHALL INCLUDE THE FOLLOWING: SECTION PROFILES, SIZES, CONNECTION ATTACHMENTS, REINFORCING, ANCHORAGE, SIZE AND TYPE OF FASTENERS AND ACCESSORIES. INCLUDE ERECTION DRAWINGS,

3. STRUCTURAL STEEL SHALL BE DETAILED, FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST PROVISIONS OF AISC MANUAL OF STEEL CONSTRUCTION.

MISCELLANEOUS PIECES AND HOLES REQUIRED TO COMPLETE THE STRUCTURE.

6. INSTALL FABRICATIONS PLUMB AND LEVEL, ACCURATELY FITTED, AND FREE FROM

7. AFTER ERECTION OF STRUCTURES, TOUCHUP ALL WELDS, ABRASIONS AND NON-GALVANIZED SURFACES WITH A 95% ORGANIC ZINC RICH PAINT IN

8. ALL STEEL MATERIAL (EXPOSED TO WEATHER) SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT DIPPED GALVANIZED)

9. ALL BOLTS, ANCHORS AND MISCELLANEOUS HARDWARE SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL

10. THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER

11. CONNECTION ANGLES SHALL HAVE A MINIMUM THICKNESS OF 1/4 INCHES. 12. STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DIAMETER MINIMUM AND SHALL HAVE A MINIMUM OF TWO BOLTS,

13. LOCK WASHER ARE NOT PERMITTED FOR A325 STEEL ASSEMBLIES.

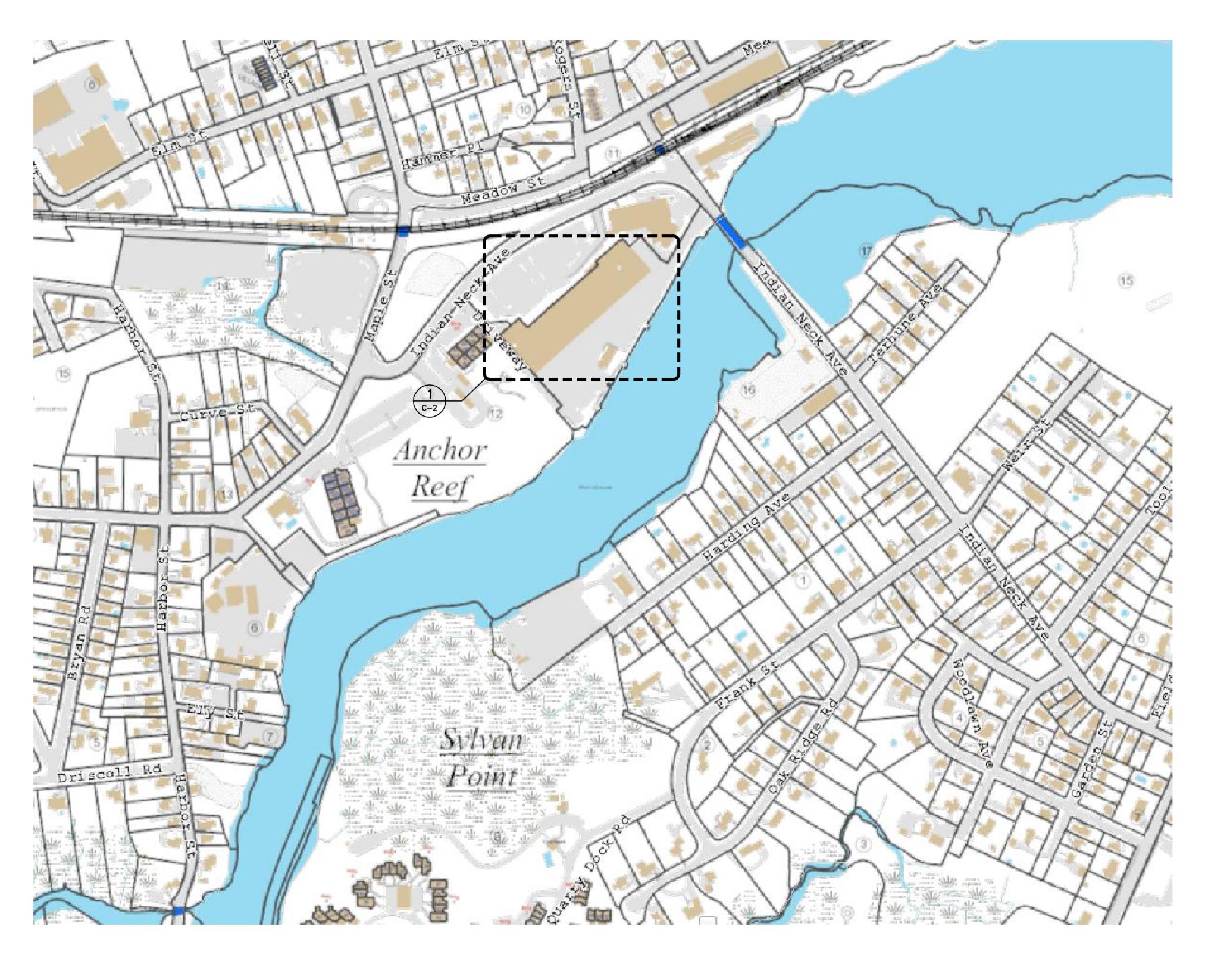
15. MILL BEARING ENDS OF COLUMNS, STIFFENERS, AND OTHER BEARING SURFACES TO

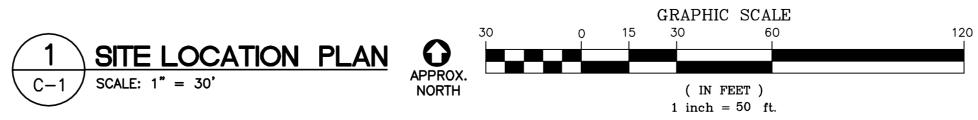
17. LEVEL AND PLUMB INDIVIDUAL MEMBERS OF THE STRUCTURE TO AN ACCURACY OF 1:500, BUT NOT TO EXCEED 1/4" IN THE FULL HEIGHT OF THE COLUMN.

18. COMMENCEMENT OF STRUCTURAL STEEL WORK WITHOUT NOTIFYING THE ENGINEER OF ANY DISCREPANCIES WILL BE CONSIDERED ACCEPTANCE OF PRECEDING WORK. 19. INSPECTION AND TESTING OF ALL WELDING AND HIGH STRENGTH BOLTING SHALL BE

PERFORMED BY AN INDEPENDENT TESTING LABORATORY. 20. FOUR COPIES OF ALL INSPECTION TEST REPORTS SHALL BE SUBMITTED TO THE

| L-NOBILE NORTHEAST LLC | | -olidoM T | PROFESSIONAL ENGINEER SEAL | | |
|-------------------------------|-------------------------------------|--------------------|----------------------------|--------------------|---|
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| 5/0 5 N | | | | | |
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| (19 ED H1 A(1) IC | Branford, CT 06405 | (| | | |
| | | Transcend Wireless | ш | B 06/26/19 KAWJR | CAG PRELIMINARY CDs – REVISED PER CLIENT COMMENTS |
| S | | | 4 | A 05/06/19 RTS | CAG PRELIMINARY CDs - ISSUED FOR CLIENT REVIEW |
| | www.CentekEng.com | | RE | REV. DATE DRAWN BY | SY CHK'D BY DESCRIPTION |



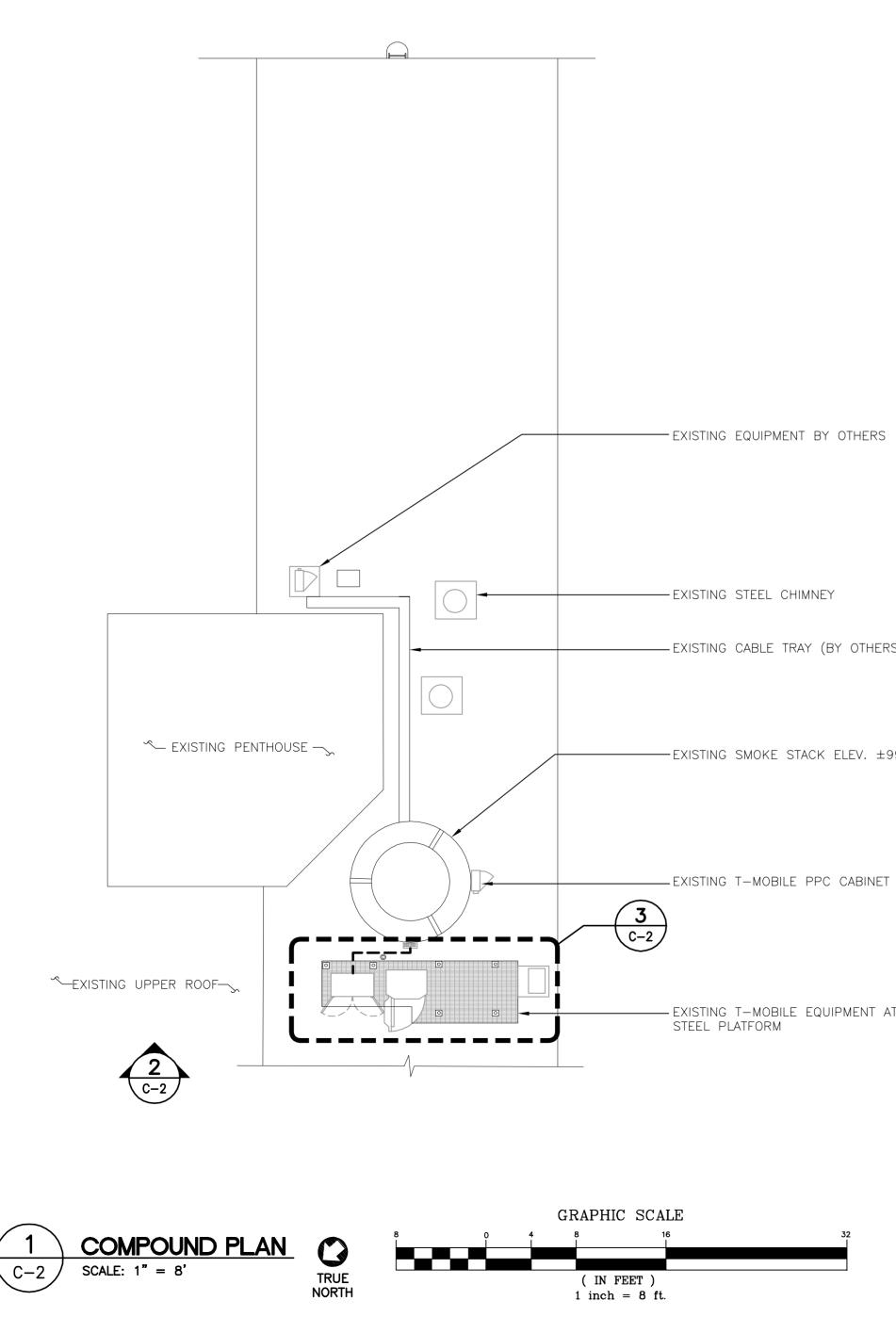


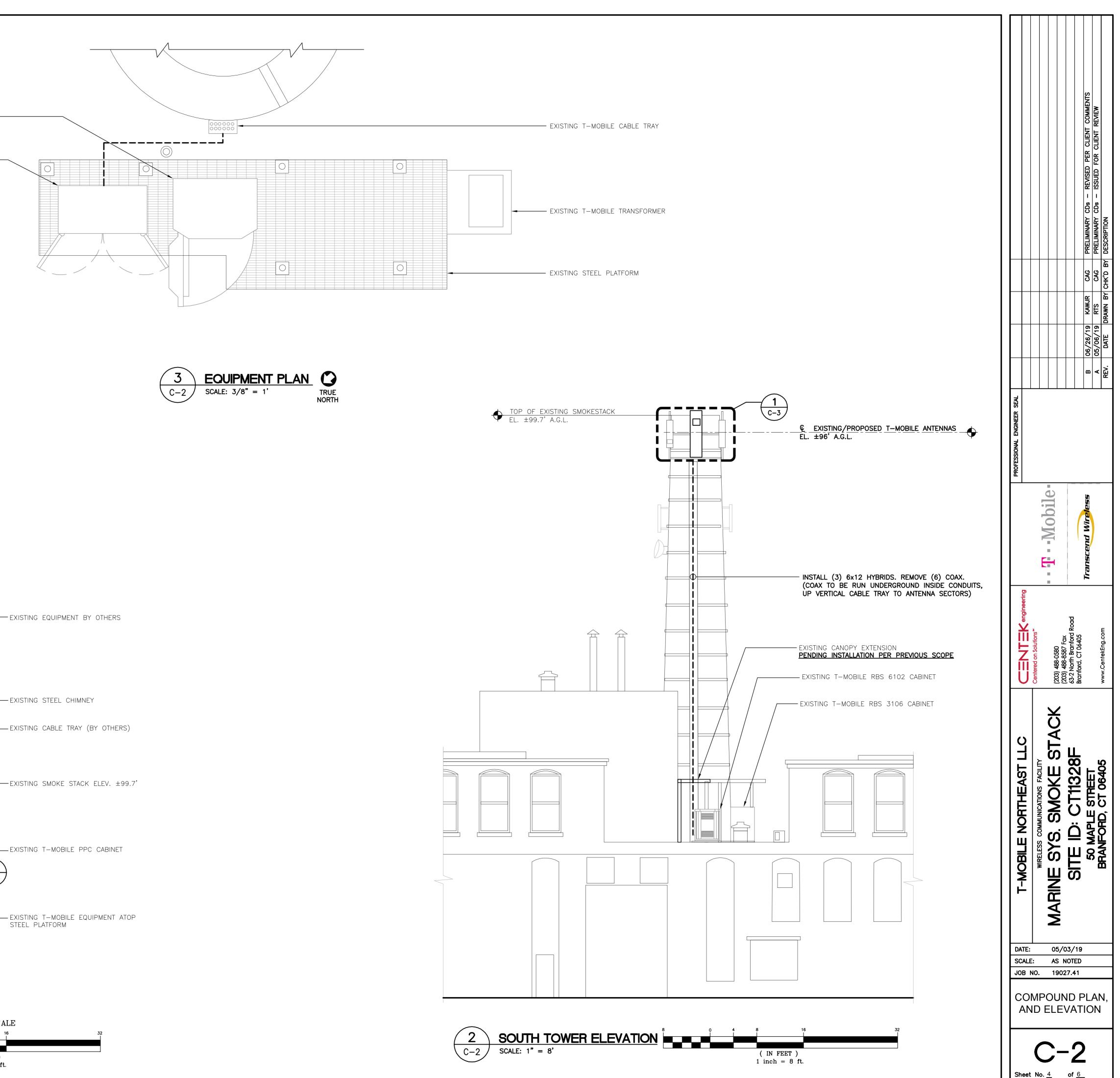
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| Na | 10. | WIRFLESS COMMUNICATIONS FACILITY | Centered on Solutions ^{**} | | 1 | | |
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| 3 | AS 19 | | (2013) 488-0580 | | | | |
| , - | 5 N 902 | | (203) 488-8587 Fox | | | | |
| of | | | 63-2 North Branford Road | | | | |
| 6 | ED F1 | | Branford, CT 06405 | (| | | |
| _ | IC | SO MAPI E STREET | | Transcend Wir <mark>el</mark> ess | | B 06/26/19 KAWJR | R CAG PRELIMINARY CDS - REVISED PER CLIENT COMMENTS |
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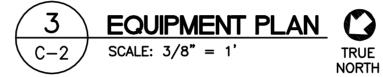


EXISTING T-MOBILE RBS 6102 CABINET ____

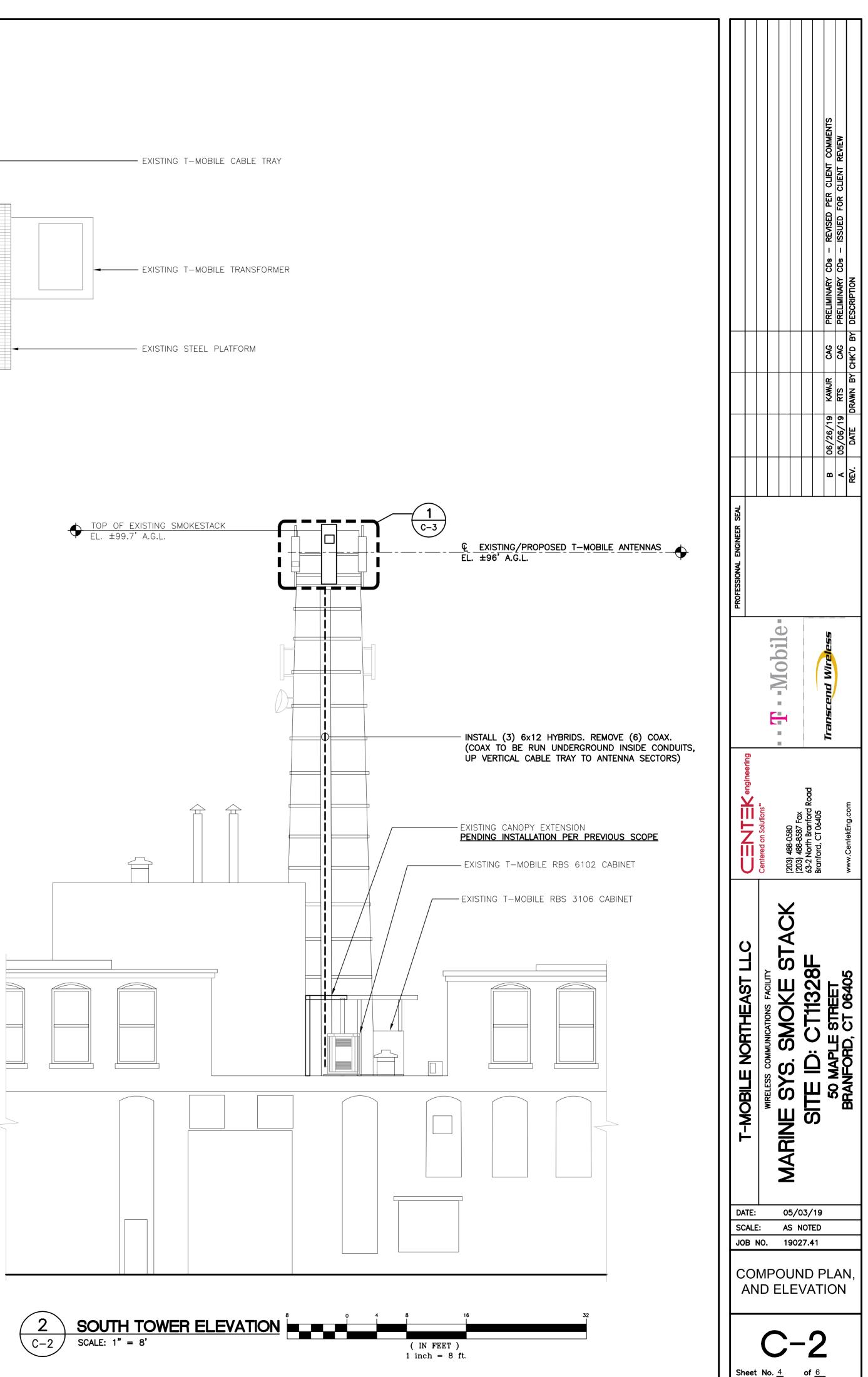


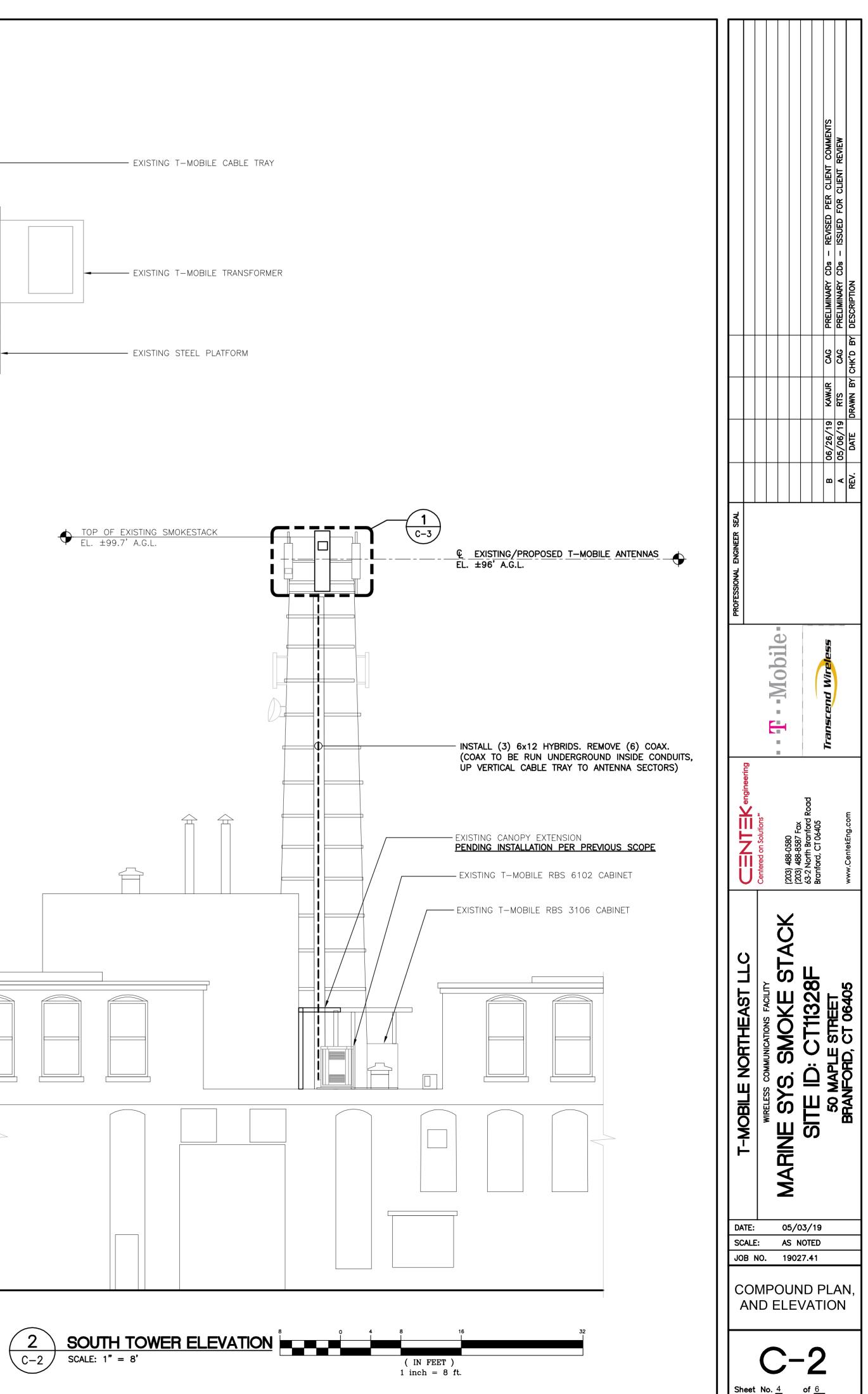


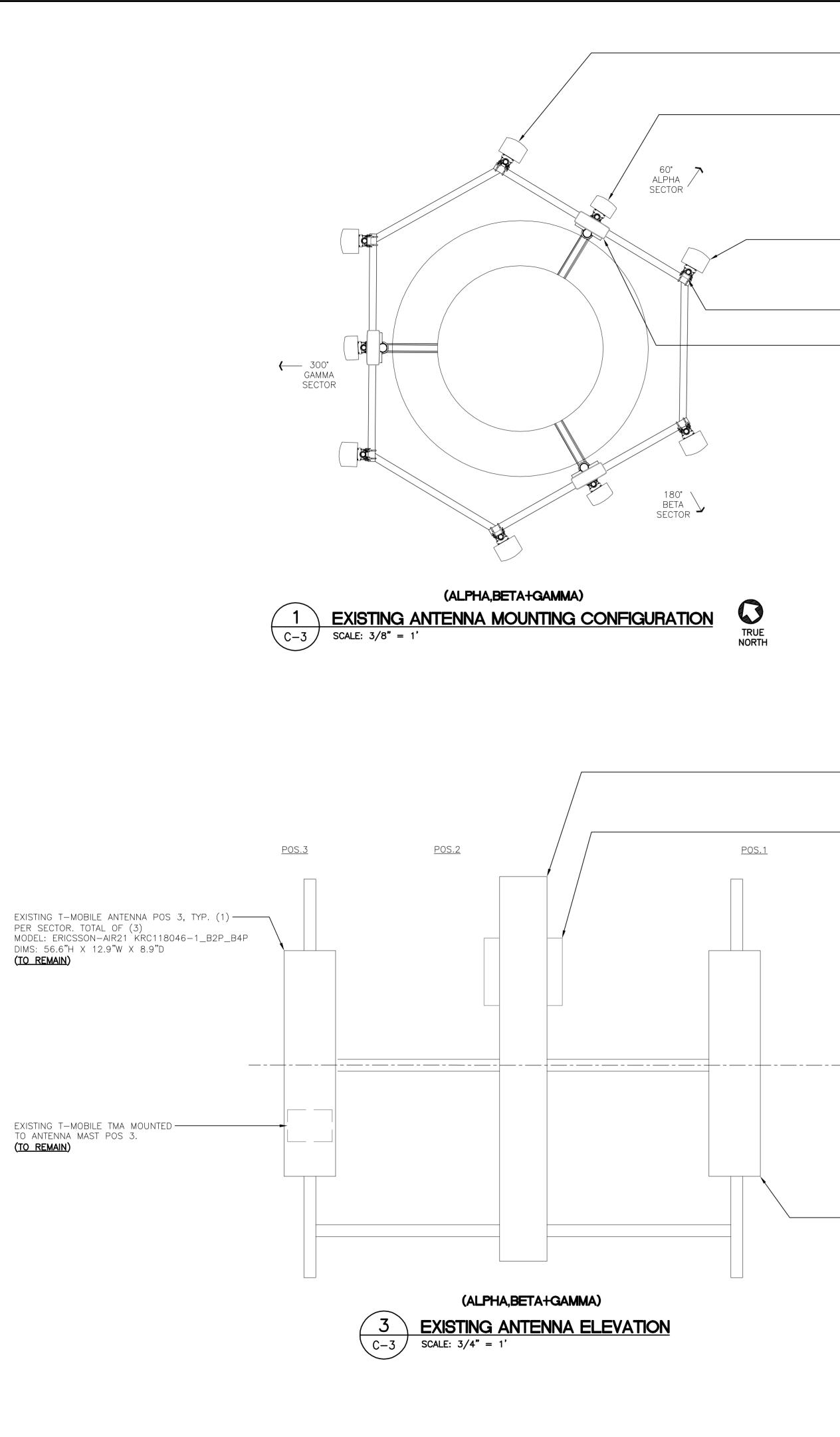




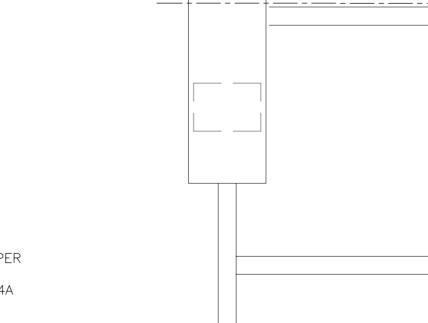
EXISTING CABLE TRAY (BY OTHERS)

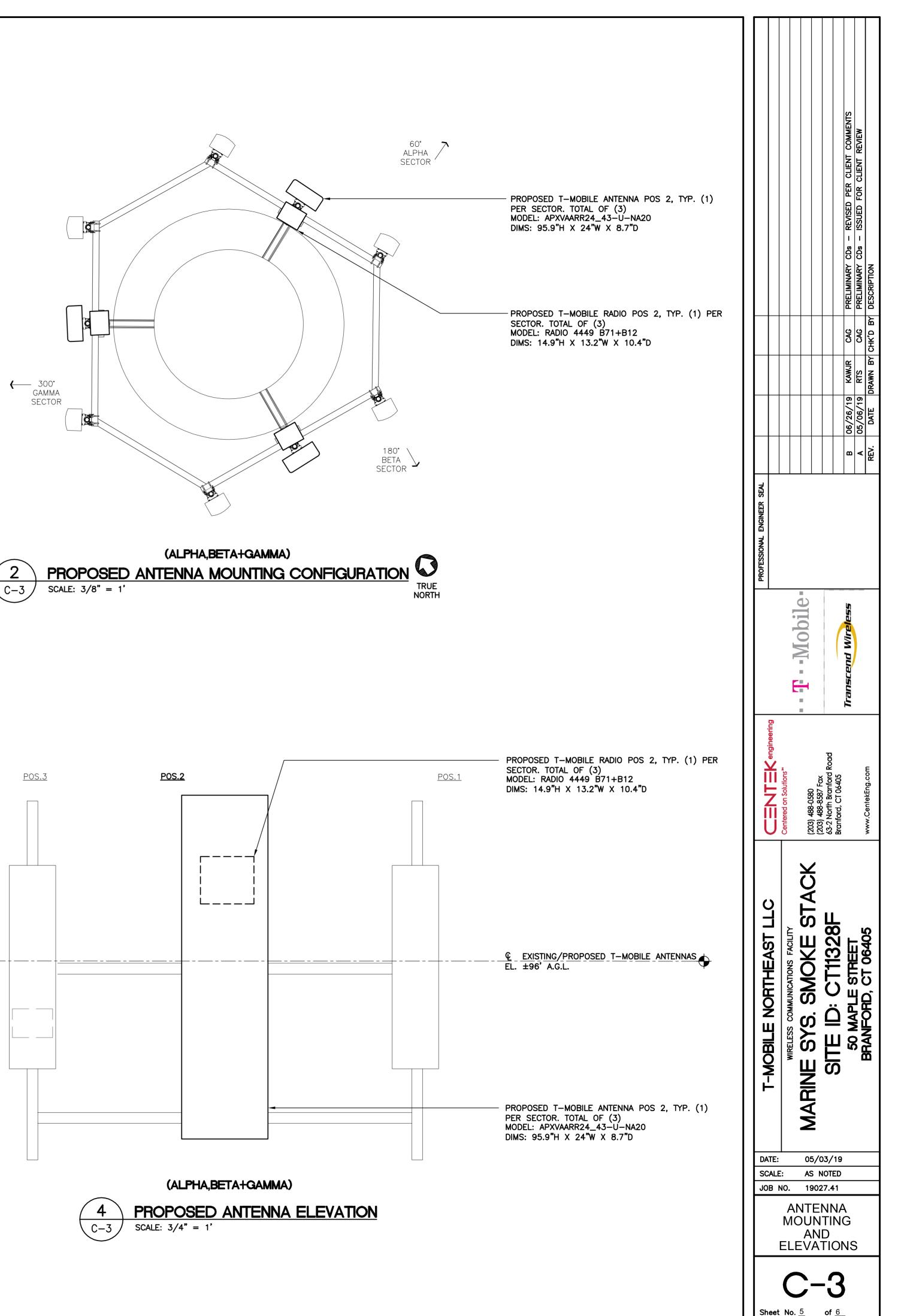










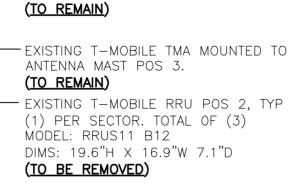








<u>POS.3</u>



- EXISTING T-MOBILE ANTENNA POS 2, TYP. (1) PER SECTOR. TOTAL OF (3) MODEL: ANDREW-LNX 6515DS-A1M DIMS" 96.9"H X 11.9"W X 7.1"D (TO BE REMOVED AND REPLACED)

- EXISTING T-MOBILE RRU POS 2. TYP

€ EXISTING T-MOBILE ANTENNAS EL. ±96' A.G.L.

(1) PER SECTOR. TOTAL OF (3)

DIMS: 19.6"H X 16.9"W 7.1"D

MÓDEL: RRUS11 B12

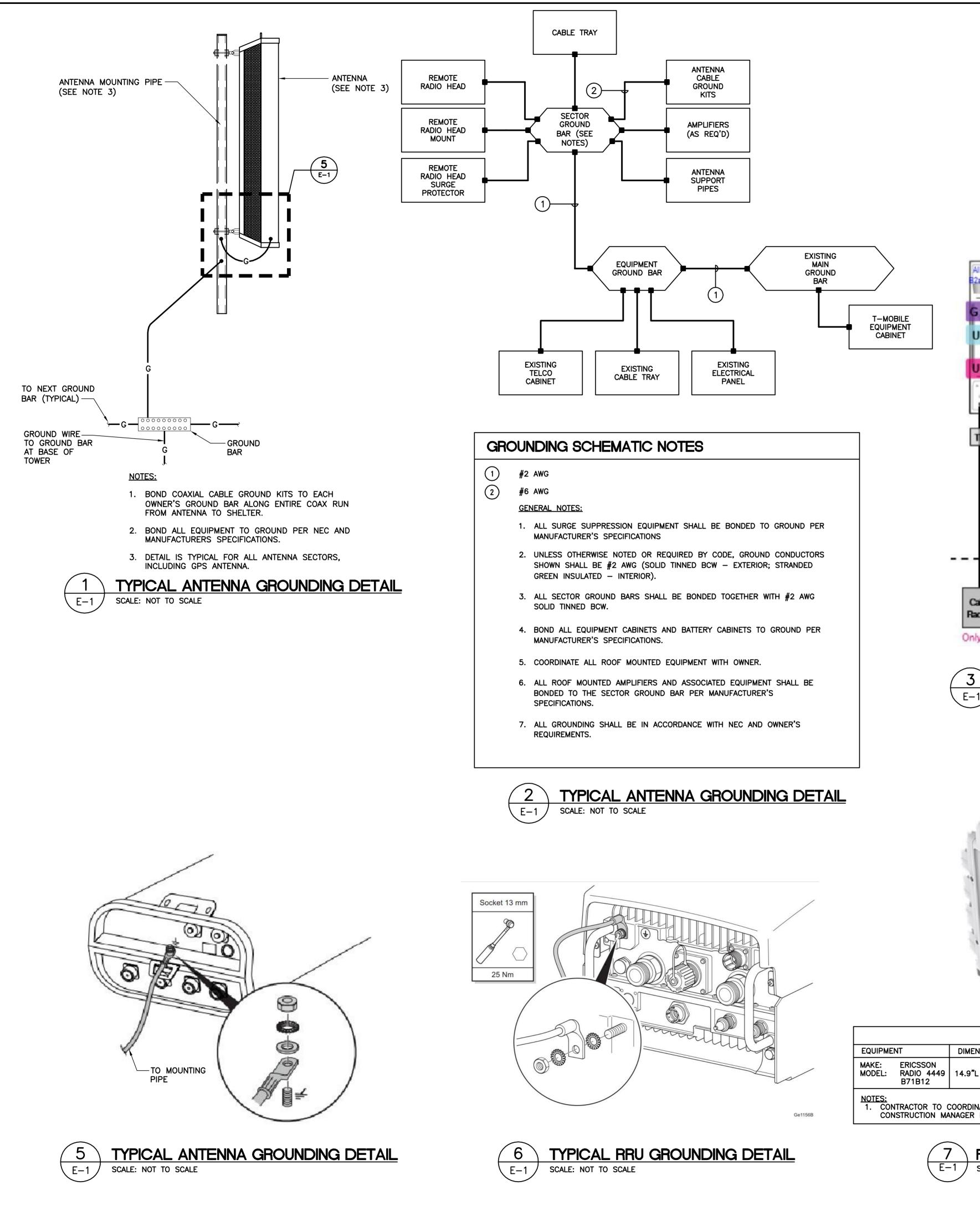
(TO BE REMOVED)

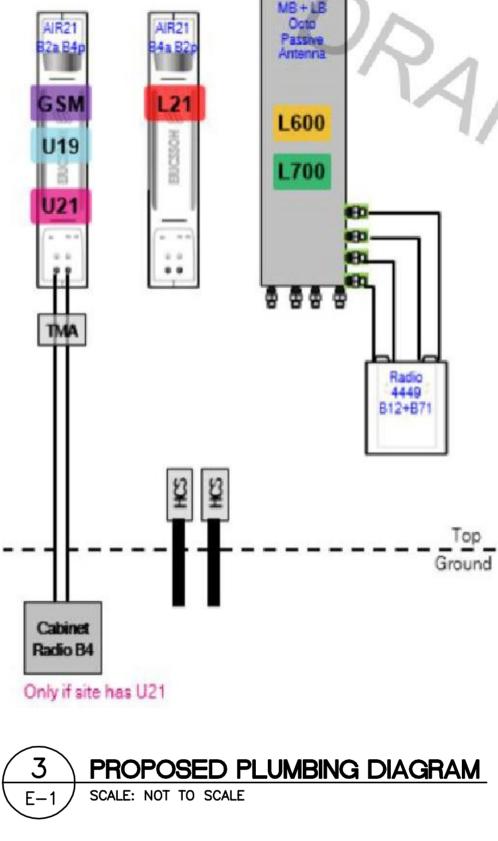
EXISTING T-MOBILE ANTENNA POS 2, TYP. (1) PER SECTOR. TOTAL OF (3) MODEL: ANDREW-LNX 6515DS-A1M DIMS" 96.9"H X 11.9"W X 7.1"D (TO BE REMOVED AND REPLACED)

- EXISTING T-MOBILE ANTENNA POS 1, TYP. (1) PER SECTOR. TOTAL OF (3) MODEL: ERICSSON-AIR21 KRC118023-1_B2P_B4A DIMS: 56.1"H X 12.08"W X 8.9"D (<u>TO_REMAIN</u>)

EXISTING T-MOBILE ANTENNA POS 3, TYP. (1)

PER SECTOR. TOTAL OF (3) MODEL: ERICSSON-AIR21 KRC118046-1_B2A_B4P DIMS: 56.6"H X 12.9"W X 8.9"D





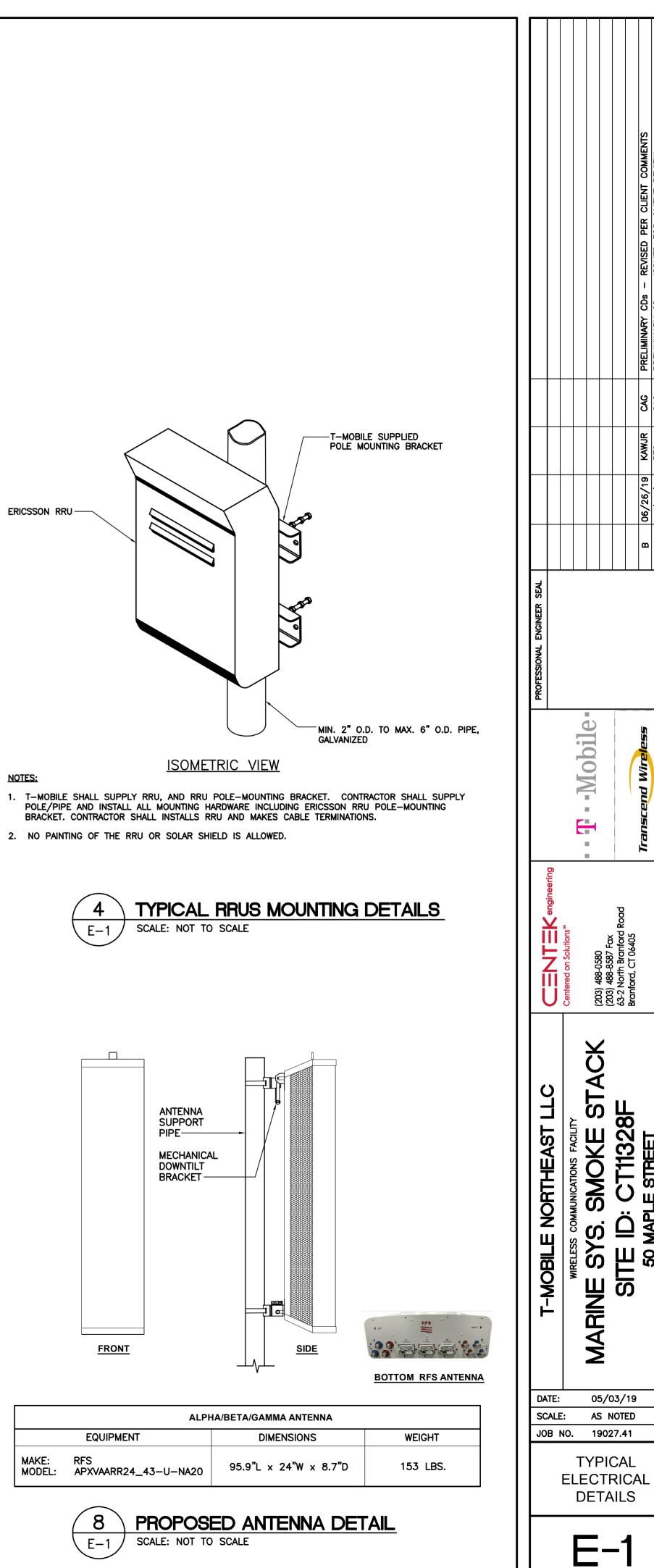


| | ISOMETRIC | VIEW |
|--|------------------|------|
|--|------------------|------|

| | | RRU (REMOTE RA | ADIO UNIT) | |
|-----------------|----------------------------------|--------------------------|------------|---|
| EQUIPME | NT | DIMENSIONS | WEIGHT | CLEARANCES |
| MAKE: MODEL: | ERICSSON RADIO 4449 B71B12 | 14.9"L x 13.2"W x 10.4"D | 74 LBS. | ABOVE: 16" MIN. BELOW: 12" MIN. FRONT: 36" MIN. |
| NOTES: | | | | |

1. CONTRACTOR TO COORDINATE FINAL EQUIPMENT MODEL SELECTION WITH T-MOBILE CONSTRUCTION MANAGER PRIOR TO ORDERING.

PROPOSED RRU DETAIL SCALE: NOT TO SCALE



Sheet No. 6 of 50 BA

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Exhibit D Structural Analysis Report



Structural Analysis Report

±99.7-ft Existing Masonry Smokestack

T-Mobile Site Ref: CT11328F

50 Maple Street Branford, CT 06405

Centek Project No. 19027.41

Date: June 18, 2019 Rev 1: July 16, 2019



Prepared for: T-Mobile USA 35 Griffin Road Bloomfield, CT 06002

Table of Contents

SECTION 1 - REPORT

- INTRODUCTION
- EQUIPMENT INSTALLATION SUMMARY
- DESIGN LOADING
- RESULTS
- CONCLUSION AND RECOMMENDATIONS

SECTION 2 - CONDITIONS & SOFTWARE

- STANDARD ENGINEERING CONDITIONS
- GENERAL DESCRIPTION OF STRUCTURAL ANALYSIS PROGRAM

SECTION 3 – CALCULATIONS

- WIND LOADING
- ANTENNA FRAME RISA 3D OUTPUT REPORT
- SMOKESTACK ANALYSIS

SECTION 4 – REFERENCES (NOT ATTACHED)

- RF DATA SHEET, DATED 4/17/2019
- STRUCTURAL ANLAYSIS REPORT AS PREPARED BY INTERNATIONAL CHMINEY CORP., DATED 08/08/2016.

Introduction

The purpose of this report is to summarize the results of the structural analysis of the equipment installation proposed by T-Mobile on the existing host masonry smokestack located in Branford, CT.

The host structure is a ± 99.7 -ft tall masonry smokestack. The smokestack geometry and structural information was obtained from a field investigation and inspection report prepared by International Chimney Corporation dated August 8, 2016.

Equipment Installation Summary

T-Mobile (Existing to Remove): Antennas: Three (3) Andrew LNX-6515DS-A1M panel antennas and three (3) Ericsson RRUS-11 B12 remote radio units mounted on custom sector mounts with RAD center elevations of ±96-ft AGL. Cables: Six (6) 1-5/8" \varnothing coax cables inside cable tray on exterior of smokestack.

T-Mobile (Final): Antennas: Three (3) RFS APXVAARR24 43-U-NA20 panel antennas mounted, three (3) Ericsson AIR21 KRC118023-1 B2A B4P panel antennas, three (3) Ericsson AIR21 KRC118046-1 B2P B4A panel antennas, three (3) Ericsson 4449 B71+B12 remote radio units and three (3) Ericsson KRY112 71 (TMAs) mounted on custom sector mounts with RAD center elevations of ±96-ft AGL.

Cables: Three (3) 6x12 fiber cables inside cable tray on exterior of smokestack.

Design Loading

Loading was determined per the requirements of the 2015 International Building Code as amended by the 2018 CT Building Code and ASCE 7-10 "Minimum Design Loads for Buildings and Other Structures".

| Wind Speed: | Vult = 140 mph | [Appendix N of the 2018 CT Building Code] |
|--------------------|----------------|--|
| Exposure Category: | C | |
| Risk Category | 111 | [ASCE 7-10, Table 1.5-1] |

<u>Results</u>

Smokestack:

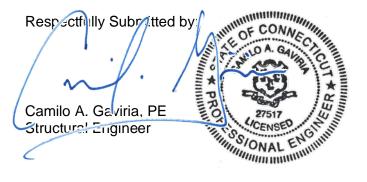
| Component | Stress Ratio (percentage of capacity) | Result |
|-------------------|---|--------|
| Compression | 25.0% | PASS |
| Tension of Mortar | 47.0% | PASS |

Conclusion and Recommendations

This analysis shows that the subject smokestack <u>is adequate</u> to support the proposed T-Mobile equipment installation.

The analysis is based, in part on the information provided to this office by T-Mobile. If the existing conditions are different than the information in this report, CENTEK engineering, Inc. must be contacted for resolution of any potential issues.

Please feel free to call with any questions or comments.



<u>Standard Conditions for Furnishing of</u> <u>Professional Engineering Services on</u> <u>Existing Structures</u>

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessarily limited to:

- Information supplied by the client regarding the structure itself, its foundations, the soil
 conditions, the antenna and feed line loading on the structure and its components, or
 other relevant information.
- Information from the field and/or drawings in the possession of Centek Engineering, Inc. or generated by field inspections or measurements of the structure.
- It is the responsibility of the client to ensure that the information provided to Centek Engineering, Inc. and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and are in an uncorroded condition and have not deteriorated. It is therefore assumed that its capacity has not significantly changed from the "as new" condition.
- All services will be performed to the codes specified by the client, and we do not imply to meet any other codes or requirements unless explicitly agreed in writing. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement. In the absence of information to the contrary, all work will be performed in accordance with the latest revision of ANSI/ASCE10 & ANSI/EIA-222
- All services performed, results obtained, and recommendations made are in accordance with generally accepted engineering principles and practices. Centek Engineering, Inc. is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

<u>GENERAL DESCRIPTION OF STRUCTURAL</u> <u>ANALYSIS PROGRAM~RISA-3D</u>

• RISA-3D Structural Analysis Program is an integrated structural analysis and design software package for buildings, bridges, tower structures, etc.

Modeling Features:

- Comprehensive CAD-like graphic drawing/editing capabilities that let you draw, modify and load elements as well as snap, move, rotate, copy, mirror, scale, split, merge, mesh, delete, apply, etc.
- Versatile drawing grids (orthogonal, radial, skewed)
- Universal snaps and object snaps allow drawing without grids
- Versatile general truss generator
- Powerful graphic select/unselect tools including box, line, polygon, invert, criteria, spreadsheet selection, with locking
- Saved selections to quickly recall desired selections
- Modification tools that modify single items or entire selections
- Real spreadsheets with cut, paste, fill, math, sort, find, etc.
- Dynamic synchronization between spreadsheets and views so you can edit or view any data in the plotted views or in the spreadsheets
- Simultaneous view of multiple spreadsheets
- Constant in-stream error checking and data validation
- Unlimited undo/redo capability
- Generation templates for grids, disks, cylinders, cones, arcs, trusses, tanks, hydrostatic loads, etc.
- Support for all units systems & conversions at any time
- Automatic interaction with RISASection libraries
- Import DXF, RISA-2D, STAAD and ProSteel 3D files
- Export DXF, SDNF and ProSteel 3D files

Analysis Features:

- Static analysis and P-Delta effects
- Multiple simultaneous dynamic and response spectra analysis using Gupta, CQC or SRSS mode combinations
- Automatic inclusion of mass offset (5% or user defined) for dynamic analysis
- Physical member modeling that does not require members to be broken up at intermediate joints
- State of the art 3 or 4 node plate/shell elements
- High-end automatic mesh generation draw a polygon with any number of sides to create a mesh of well-formed quadrilateral (NOT triangular) elements.
- Accurate analysis of tapered wide flanges web, top and bottom flanges may all taper independently
- Automatic rigid diaphragm modeling
- Area loads with one-way or two-way distributions
- Multiple simultaneous moving loads with standard AASHTO loads and custom moving loads for bridges, cranes, etc.
- Torsional warping calculations for stiffness, stress and design
- Automatic Top of Member offset modeling
- Member end releases & rigid end offsets
- Joint master-slave assignments
- Joints detachable from diaphragms
- Enforced joint displacements

- 1-Way members, for tension only bracing, slipping, etc.
- 1-Way springs, for modeling soils and other effects
- Euler members that take compression up to their buckling load, then turn off.
- Stress calculations on any arbitrary shape
- Inactive members, plates, and diaphragms allows you to quickly remove parts of structures from consideration
- Story drift calculations provide relative drift and ratio to height
- Automatic self-weight calculations for members and plates
- Automatic subgrade soil spring generator

Graphics Features:

- Unlimited simultaneous model view windows
- Extraordinary "true to scale" rendering, even when drawing
- High-speed redraw algorithm for instant refreshing
- Dynamic scrolling stops right where you want
- Plot & print virtually everything with color coding & labeling
- Rotate, zoom, pan, scroll and snap views
- Saved views to quickly restore frequent or desired views
- Full render or wire-frame animations of deflected model and dynamic mode shapes with frame and speed control
- Animation of moving loads with speed control
- High quality customizable graphics printing

Design Features:

- Designs concrete, hot rolled steel, cold formed steel and wood
- ACI 1999/2002, BS 8110-97, CSA A23.3-94, IS456:2000, EC 2-1992 with consistent bar sizes through adjacent spans
- Exact integration of concrete stress distributions using parabolic or rectangular stress blocks
- Concrete beam detailing (Rectangular, T and L)
- Concrete column interaction diagrams
- Steel Design Codes: AISC ASD 9th, LRFD 2nd & 3rd, HSS Specification, CAN/CSA-S16.1-1994 & 2004, BS 5950-1-2000, IS 800-1984, Euro 3-1993 including local shape databases
- AISI 1999 cold formed steel design
- NDS 1991/1997/2001 wood design, including Structural Composite Lumber, multi-ply, full sawn
- Automatic spectra generation for UBC 1997, IBC 2000/2003
- Generation of load combinations: ASCE, UBC, IBC, BOCA, SBC, ACI
- Unbraced lengths for physical members that recognize connecting elements and full lengths of members
- Automatic approximation of K factors
- Tapered wide flange design with either ASD or LRFD codes
- Optimization of member sizes for all materials and all design codes, controlled by standard or user-defined lists of available sizes and criteria such as maximum depths
- Automatic calculation of custom shape properties
- Steel Shapes: AISC, HSS, CAN, ARBED, British, Euro, Indian, Chilean
- Light Gage Shapes: AISI, SSMA, Dale / Incor, Dietrich, Marino\WARE
- Wood Shapes: Complete NDS species/grade database
- Full seamless integration with RISAFoot (Ver 2 or better) for advanced footing design and detailing
- Plate force summation tool

Results Features:

- Graphic presentation of color-coded results and plotted designs
- Color contours of plate stresses and forces with quadratic smoothing, the contours may also be animated
- Spreadsheet results with sorting and filtering of: reactions, member & joint deflections, beam & plate forces/stresses, optimized sizes, code designs, concrete reinforcing, material takeoffs, frequencies and mode shapes
- Standard and user-defined reports
- Graphic member detail reports with force/stress/deflection diagrams and detailed design calculations and expanded diagrams that display magnitudes at any dialed location
- Saved solutions quickly restore analysis and design results.

| | Subject: | | | Wind Load on | Equipmer | t per ASCE 7-10 |
|--|-------------------|--|--------------------------------|------------------------------|------------------|--------------------|
| Centered on Solutions [™] www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 Branford, CT 06405 F: (203) 488-8587 | Location: | | | Branford, CT | | |
| | Rev. 0: 6/10/2019 | | | Prepared by: Job No. 1902 | CAG Chec 7.41 | ked by: TJL |
| Design Wind Load on Other Str | uctures: | (Based on IBC 201 | 2, CSBC 20 ⁻ | 16 and ASCE 7-10) | | |
| Wi | nd Speed = | V := 140 | mph | (| (User Input) | (CSBC Appendix-N) |
| Ris | < Category = | BC := III | | (| (User Input) | (IBC Table 1604.5) |
| Exposure | Category = | Exp := C | | (| (User Input) | |
| Struc | ture Type = | Structuretype := | Round_Ch | imney | (User Input) | |
| Structu | re Height = | Height := 99.7 | ft | | (User Input) | |
| Horizontal Dimension of Str | ucture = | Width := 12.99 | ft | (| (User Input) | |
| <u>Terrain Exposure (</u> Nominal Height of the Atmospheric Boundary Lay | | zg := 1200 if | | 900 | | (Table 26.9-1) |
| | | 900 if E 700 if E | | | | |
| 3-Sec Gust Speed Power Law Exp | onent = | α:= 7 if Exp 9.5 if Exp | p = C | 9.5 | | (Table 26.9-1) |
| Integral Length Scale | Factor = | 11.5 if E I:= 320 if Exp 500 if Exp | p = B = 5 | 00 | | (Table 26.9-1) |
| | | 650 if Exp | p = D | | | |
| Integral Length Scale Power Law Expor | ient = | $E := \begin{bmatrix} \frac{1}{3} & \text{if } Exp \\ \frac{1}{3} & \frac{1}{3} \end{bmatrix}$ | $\mathbf{D} = \mathbf{B} = 0.$ | 2 | | (Table 26.9-1) |
| | | 1 | | | | |
| | | $\frac{1}{8}$ if Exp |) = D | | | |
| Turbulence Intensity | /Factor= | c:= 0.3 if Exp 0.2 if Exp 0.15 if E | p = C | 0.2 | | (Table 26.9-1) |
| Exposure | Constant = | Z _{min} := 30 if 15 if 7 if E | | 15 | | (Table 26.9-1) |
| | | | | | | |

| Topographic Factor = | K _{zt} := 1 | (Eq. 26.8-2) |
|---------------------------------------|-----------------------|----------------|
| Wind Directionality Factor = | $K_{d} = 0.95$ | (Table 26.6-1) |
| Peak Factor for Background Response = | g _Q := 3.4 | (Sec 26.9.4) |
| Peak Factor for Wind Response = | g _V := 3.4 | (Sec 26.9.4) |

| | Subject: | | Wind Load on Equipme | nt per ASCE 7-10 |
|--|-------------------|---|--|-----------------------|
| Centered on Solutions [™] www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 | Location: | | Branford, CT | |
| Branford, CT 06405 F: (203) 488-8587 | Rev. 0: 6/10/2019 | | Prepared by: CAG Che Job No. 19027.41 | cked by: TJL |
| Equivalent Height of Strue | oture = | z:= Z _{min} if Z _{min} > 0.6 0.6 Height otherwis | 6∙Height = 59.82 se | (Sec 26.9.4) |
| Intensity of Turbu | ilence = | $I_{z} := c \cdot \left(\frac{33}{z}\right)^{\left(\frac{1}{6}\right)} = 0.181$ | | (Eq. 26.9-7) |
| Integral Length Scale of Turbuler | ce = | $L_{Z} := I \left(\frac{z}{33} \right)^{E} = 563.166$ | | (Eq. 26.9-9) |
| Background Response | Factor = | $Q := \sqrt{\frac{1}{1 + 0.63 \left(\frac{\text{Width } + 1}{\frac{1}{2}}\right)}}$ | $\frac{1}{\frac{\text{Height}}{z}} = 0.902$ | (Eq. 26.9-8) |
| Gust Respons | e Factor = | $G := 0.925 \cdot \left[\frac{\left(1 + 1.7 \cdot g_{Q} \cdot I \right)}{1 + 1.7 \cdot g_{V}} \right]$ | $\left[\frac{\mathbf{z} \cdot \mathbf{Q}}{\mathbf{I}_{\mathbf{Z}}}\right] = 0.879$ | (Eq. 26.9-6) |
| Velocity P | ressure = | $q_{z} \coloneqq 0.00256 \cdot K_{zt} \cdot K_{d} \cdot V^{2}$ | = 47.67 | (Eq. 29.3-1) |
| Force Co | efficient = | C _f = 0.804 | | (Fig 29.5-1 - 29.5-3) |
| Ultimate Wind Pr | essure = | $F := q_{Z} \cdot G \cdot C_{f} = 33.7$ | psf | |
| HeightAbove | | Z := 115 ft $\left \begin{array}{c} 2\\ \alpha \end{array} \right ^{2} \left(\frac{2}{\alpha} \right) $ | (User Input) | (Table 29.3-1) |
| Exposure Co | emcient = | $K_{z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \\ \\ 2.01 \left(\frac{15}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \end{bmatrix}$ | 15 ≤ Z ≤ zg = 1.3 Z < 15 | |
| | | K _Z = 1.303 | | |
| HeightAbove | Grade = | Z := 90 ft | (User Input) | |
| Exposure Co | efficient = | $K_{z} := \begin{bmatrix} 2.01 \left(\frac{z}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \\ \\ 2.01 \left(\frac{15}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \end{bmatrix}$ | $15 \le Z \le zg = 1.24$ Z < 15 | (Table 29.3-1) |
| | | | | |



Wind Load on Equipment per ASCE 7-10

Branford, CT 06405 F: (203) 488-8587

Location:

Rev. 0: 6/10/2019

Branford, CT

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HeightAbove Grade = Z := 65 ft (User Input) $K_{Z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } 15 \le Z \le zg = 1.16 \\ \\ 2.01 \left(\frac{15}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } Z < 15 \end{bmatrix}$ (Table 29.3-1) Exposure Coefficient = K₇ = 1.156 HeightAbove Grade = Z := 40 ft (User Input) $K_{z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } 15 \le Z \le zg = 1.04 \\ \\ 2.01 \left(\frac{15}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } Z < 15 \end{bmatrix}$ (Table 29.3-1) Exposure Coefficient = K_z = 1.044

Wind on Other Stuctures (IBC 2012 ASCE 7-



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

sf

lbs

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

T-Mobile Loading:

| Development of Wind & Ice Load on Antennas | |
|--|--|
|--|--|

| Antenna Data: | | | |
|--------------------------------|--|---------------|--------------|
| Antenna Model = | RFSAPXVAA24_43 | -U-A20 | |
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 95.9 | in | (User Input) |
| Antenna Width = | W _{ant} := 24 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 8.7 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 128 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |
| Wind Load (Front) | | | |
| Surface Area for One Antenna = | SA _{ant} := $\frac{L_{ant} \cdot W_a}{144}$ | ant — = 16 | |

| Antenna Projected Surface Area = | $A_{ant} := SA_{ant} \cdot N_{ant} = 48$ | sf |
|----------------------------------|--|----|
| | | |

| $F_{ant} := F \cdot A_{ant} = 1614$ | lbs |
|-------------------------------------|-----|
|-------------------------------------|-----|

Wind Load (Side)

Surface Area for One Antenna =

Total Antenna Wind Force =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

 $SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 5.8$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 17.4$ sf

F_{ant} := F·A_{ant} = 585 lbs

WT_{ant}·N_{ant} = 384



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

Development of Wind & Ice Load on Antennas

| Antenna Model = | EricssonAIR21 (KRC118023-1) | | |
|----------------------|-----------------------------|-----|--------------|
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 56.3 | in | (User Input) |
| Antenna Width = | W _{ant} := 12.1 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 7.9 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 91.5 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |

Wind Load (Front)

| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} W_{ant}}{144} = 4.7$ | sf |
|--------------------------------|---|----|
|--------------------------------|---|----|

141

Antenna Projected Surface Area =

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

| $A_{ant} := SA_{ant} \cdot N_{ant} =$ | 14.2 | sf |
|---------------------------------------|------|-----|
| $F_{ant} := F \cdot A_{ant} = 478$ | | lbs |

 $SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 3.1$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 9.3$ sf

 $F_{ant} := F \cdot A_{ant} = 312$ lbs

lbs

 $WT_{ant} \cdot N_{ant} = 275$



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

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| Ericsson 4449 B12/B71 | |
|---|---|
| Flat (User Input) | |
| L _{RRH} := 15.0 in (User Input) | |
| W _{RRH} := 13.2 in (User Input) | |
| T _{RRH} ≔ 10.4 in <mark>(User Input)</mark> | |
| WT _{RRH} ≔ 75 lbs (User Input) | |
| N _{RRH} := 3 (User Input) | |
| | |
| $SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.4$ | sf |
| A _{RRH} := SA _{RRH} ·N _{RRH} = 4.1 | sf |
| F _{RRH} := F·A _{RRH} = 139 | lbs |
| | |
| $SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.1$ | sf |
| A _{RRH} := SA _{RRH} ·N _{RRH} = 3.3 | sf |
| F _{RRH} := F·A _{RRH} = 109 | lbs |
| | |
| WT _{RRH} ·N _{RRH} = 225 | lbs |
| | Flat(User Input) $L_{RRH} := 15.0$ in(User Input) $W_{RRH} := 13.2$ in(User Input) $T_{RRH} := 10.4$ in(User Input) $W_{RRH} := 75$ lbs(User Input) $W_{RRH} := 75$ lbs(User Input) $M_{RRH} := 3$ (User Input) $M_{RRH} := 3$ (User Input) $SA_{RRH} := 3$ (User Input) $SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.4$ $A_{RRH} := SA_{RRH} \cdot N_{RRH} = 4.1$ $F_{RRH} := F \cdot A_{RRH} = 139$ $SA_{RRH} := SA_{RRH} \cdot N_{RRH} = 3.3$ $F_{RRH} := F \cdot A_{RRH} = 109$ |



Location:

Rev. 0: 6/10/2019

_

Wind Load on Equipment per ASCE 7-10

sf

lbs

lbs

lbs

Branford, CT

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Sprint Loading:

Development of Wind & Ice Load on Antennas

| <u>Antenna Data:</u> | | | |
|----------------------|-------------------------|-----|--------------|
| Antenna Model = | Generic 6'Antenna | | |
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 72 | in | (User Input) |
| Antenna Width = | W _{ant} := 12 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 9.0 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 80 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |
| | | | |

Wind Load (Front)

| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} W_{ant}}{144} = 6$ | sf |
|--------------------------------|---|----|
|--------------------------------|---|----|

 $A_{ant} := SA_{ant} \cdot N_{ant} = 18$

 $F_{ant} := F \cdot A_{ant} = 606$

Antenna Projected Surface Area =

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

| $SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 4.5$ | sf |
|---|----|
| $A_{ant} := SA_{ant} \cdot N_{ant} = 13.5$ | sf |

 $F_{ant} \coloneqq F \cdot A_{ant} = 454$

WT_{ant}·N_{ant} = 240



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

lbs

lbs

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

Development of Wind & Ice Load on Antennas

Surface Area for

Antenna Projected

| Antenna Model = | Generic 4'Antenna | | |
|----------------------|---------------------------|-----|--------------|
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 56 | in | (User Input) |
| Antenna Width = | W _{ant} := 12 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 8.0 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 60.0 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |

Wind Load (Front)

| r One Antenna = | $SA_{ant} := \frac{L_{ant} W_{ant}}{144} = 4.7$ | sf |
|-----------------|---|----|
| SurfaceArea = | $A_{ant} := SA_{ant} \cdot N_{ant} = 14$ | sf |

 $F_{ant} := F \cdot A_{ant} = 471$

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

 $SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 3.1$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 9.3$ sf

F_{ant} := F·A_{ant} = 314 lbs

WT_{ant}·N_{ant} = 180



Subject:

Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

sf

sf

lbs

sf

sf

lbs

lbs

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

| Development of Wind & Ice Load on Antennas | | | |
|--|---|--------------------|--------------|
| Antenna Model = | Generic 3'MW Ante | enna | |
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 36 | in | (User Input) |
| Antenna Width = | W _{ant} := 32 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 12.0 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 60.0 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 1 | | (User Input) |
| | | | |
| Wind Load (Front) | | | |
| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} \cdot W}{144}$ | $\frac{1}{2}$ = 8 | |
| Antenna Projected Surface Area = | A _{ant} := SA _{ant} ·N | ant ⁼ 8 | |
| Total Antenna Wind Force = | F _{ant} := F·A _{ant} = | 269 | |
| Wind Load (Side) | | | |
| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} T_{ant}}{144}$ | ant = 3 | |
| Antenna Projected Surface Area = | A _{ant} := SA _{ant} ·N _a | ant ^{= 3} | |
| Total Antenna Wind Force = | F _{ant} := F·A _{ant} = | 101 | |
| Gravity Load (without ice) | | | |
| Weight of All Antennas = | $WT_{ant} \cdot N_{ant} = 60$ | 0 | |
| | | | |



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

| Development of Wind & Ice Load on RRHs |
|--|
| |

| RRH Data: | | | |
|------------------|---------------------------|-----|--------------|
| RRH Model = | Generic RRH 1 | | |
| RRH Shape = | Flat | | (User Input) |
| RRH Height = | L _{RRH} := 20.9 | in | (User Input) |
| RRH Width = | W _{RRH} := 12.2 | in | (User Input) |
| RRH Thickness = | T _{RRH} := 10.8 | in | (User Input) |
| RRH Weight = | WT _{RRH} := 50.7 | lbs | (User Input) |
| Number of RRHs = | N _{RRH} := 9 | | (User Input) |

Wind Load (Front)

| Surface Area for One RRH = | $SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.8$ | sf |
|------------------------------|--|-----|
| RRH Projected Surface Area = | A _{RRH} := SA _{RRH} ·N _{RRH} = 15.9 | sf |
| Total RRH Wind Force = | F _{RRH} := F·A _{RRH} = 537 | lbs |
| Wind Load (Side) | | |
| Surface Area for One RRH = | $SA_{RRH} := \frac{L_{RRH} T_{RRH}}{144} = 1.6$ | sf |
| RRH Projected Surface Area = | A _{RRH} := SA _{RRH} ·N _{RRH} = 14.1 | sf |
| Total RRH Wind Force = | F _{RRH} := F·A _{RRH} = 475 | lbs |
| Gravity Load (without ice) | | |
| Weight of All RRHs = | WT _{RRH} ·N _{RRH} = 456 | lbs |

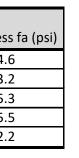
Wind on Other Stuctures (IBC 2012 ASCE 7-



| Centered on 63-2 North Branfor Branford, CT 06405 | d Road P: (203) 488-0580 | | | | |
|---|------------------------------------|-------------|----------|-------|---------|
| Job : | CT11328F | Project No. | 19027.41 | Sheet | 1 of 2 |
| Address: | 50 Maple Street Branford, CT 06405 | Computed by | LAA | Date | 6/10/19 |
| Description: | Smokestack Evaluation | Checked by | CAG | Date | |

| | Wind Force | | Height Above | |
|----------|------------|-------------|--------------|-------------|
| | (lb) | Weight (lb) | Base (ft) | Height (in) |
| T-Mobile | 2231 | 1200 | 96 | 1152 |
| Sprint | 1883 | 936 | 88 | 1056 |

| | | | | | Area At Base | Tot. Vol | Unit Weight | | | |
|---------|--------------|--------------|---------------|------------------|--------------|-----------|-------------|------------------------|-------------------|-----------------|
| Section | Top Dia (in) | Bot Dia (in) | Wall Thk (in) | Sect Height (in) | (in^2) | (ft^3) | (pcf) | Weight of Section (lb) | Total Weight (lb) | Axial Stress fa |
| 1 | 114 | 135.67 | 8 | 356.4 | 3207.0704 | 604.97204 | 127 | 76831.4485 | 78967.4485 | 24.6 |
| 2 | 135.67 | 161.4 | 8.5 | 360 | 4080.901 | 778.2026 | 125 | 97275.3249 | 176242.7734 | 43.2 |
| 3 | 161.4 | 169.92 | 9.5 | 120 | 4785.3286 | 323.30268 | 125 | 40412.83516 | 216655.6086 | 45.3 |
| 4 | 169.92 | 175.68 | 10.5 | 80 | 5445.9846 | 247.58964 | 125 | 30948.70445 | 247604.313 | 45.5 |
| 5 | 175.68 | 177.96 | 13 | 76 | 6733.6672 | 293.93989 | 125 | 36742.48571 | 284346.7987 | 42.2 |





| Cemere | Bu on Solohons www.centekeng.com | | | |
|-------------|-------------------------------------|-------------|----------|---------------------|
| 63-2 North | h Branford Road P: (203) 488-0580 | | | |
| Branford, C | CT 06405 F: (203) 488-8587 | | | |
| Job : | CT11328F | Project No. | 19027.41 | Sheet 2 of 2 |
| A d duo o o | 50 Marila Street Dranford, OT 06405 | • | | |
| Address | 50 Maple Street Branford, CT 06405 | Computed by | LAA | Date 6/10/19 |
| Descript | tion: Smokestack Evaluation | Checked by | CAG | Date |
| | | , | | |

| Ultimate Wind | ASD Wind | | | | | Section Modulus @ | Bending Stress fb | Allowable | Allowable Fb | | | | | | |
|----------------|----------------|------|----------------|-----------------|---------------|-------------------|-------------------|-----------|--------------|-------------|----|------|----|-------|----|
| Pressure (psf) | Pressure (psf) | KZ | Wind Area (sf) | Wind Force (lb) | Moment @ Base | Base | (psi) | Fa (psi) | (psi) | fa/Fa+fb/Fb | | ft | Ft | ft/Ft | |
| 33.7 | 20.22 | 1.23 | 309.0 | 7684.2 | 3311377.828 | 96703.96897 | 34.2 | 375 | 500 | 0.13 | ОК | 9.6 | 40 | 0.24 | ОК |
| 33.7 | 20.22 | 1.11 | 371.3 | 8334.4 | 9058911.713 | 148233.9248 | 61.1 | 375 | 500 | 0.24 | OK | 17.9 | 40 | 0.45 | ОК |
| 33.7 | 20.22 | 1.01 | 138.1 | 2819.3 | 11643975.81 | 181821.2694 | 64.0 | 375 | 500 | 0.25 | OK | 18.8 | 40 | 0.47 | ОК |
| 33.7 | 20.22 | 0.95 | 96.0 | 1844.1 | 13553885.82 | 212305.0695 | 63.8 | 375 | 500 | 0.25 | OK | 18.4 | 40 | 0.46 | OK |
| 33.7 | 20.22 | 0 | 93.3 | 0.0 | 15438374.77 | 259009.3359 | 59.6 | 375 | 500 | 0.23 | OK | 17.4 | 40 | 0.43 | OK |

Exhibit E Mount Analysis



Centered on Solutions[™]

Structural Analysis Report

Antenna Mount Analysis

T-Mobile Site #: CT11328F

50 Maple Street Branford, CT

Centek Project No. 19027.41

Date: June 19, 2019

Max Stress Ratio = 49.1%

Prepared for:

T-Mobile USA 35 Griffin Road Bloomfield, CT 06002



CENTEK Engineering, Inc. Structural Analysis – Mount Analysis T-Mobile Site Ref. ~ CT11328F Branford, CT June 19, 2019

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SECTION 1 - REPORT

- ANTENNA AND APPURTENANCE SUMMARY
- STRUCTURE LOADING
- CONCLUSION

SECTION 2 - CALCULATIONS

- WIND LOAD ON APPURTENANCES
- RISA3D OUTPUT REPORT

SECTION 3 - REFERENCE MATERIALS (NOT INCLUDED WITHIN REPORT)

• RF DATA SHEET, DATED 04/17/2019



June 19, 2019

Mr. Dan Reid Transcend Wireless 10 Industrial Ave Mahwah, NJ 07430

Re: Structural Letter ~ Antenna Mount T-Mobile – Site Ref: CT11328F 50 Maple Street Branford, CT 06405

Centek Project No. 19027.41

Dear Mr. Reid,

Centek Engineering, Inc. has reviewed the T-Mobile antenna installation at the above referenced site. The purpose of the review is to determine the structural adequacy of the existing mount, consisting three (3) T-frame sector to support the proposed/existing equipment configuration. The review considered the effects of wind load, dead load and ice load in accordance with the 2015 International Building Code as modified by the 2018 Connecticut State Building Code (CTBC) including ASCE 7-10 and ANSI/TIA-222-G *Structural Standards for Steel Antenna Towers and Supporting Structures*.

The loads considered in this analysis consist of the following:

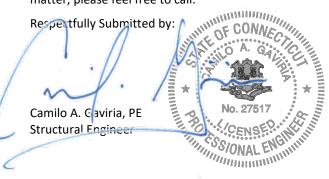
T-Mobile:

<u>T-Frames:</u> Three (3) RFS APXVAARR24_43-U-NA20 panel antennas, three (3) Ericsson AIR21 KRC118023-1_B2A_B4P panel antennas, three (3) Ericsson AIR21 KRC118046-1_B2P_B4A panel antennas, three (3) Ericsson 4449 B71+B12 remote radio units and three (3) Twin style AWS (TMAs) mounted on custom sector mounts with RAD center elevations of ±96-ft AGL

The antenna mount was analyzed per the requirements of the 2015 International Building Code as modified by the 2018 Connecticut State Building Code considering an ultimate design wind speed of 140 mph for Branford as required in Appendix N of the 2018 Connecticut State Building Code.

A structural analysis of tower and foundation needs to be completed prior to any work.

Based on our review of the installation, it is our opinion that the **subject antenna mount has sufficient capacity** to support the aforementioned antenna configuration. If there are any questions regarding this matter, please feel free to call.



Prepared by:

Fernando J. Palacios Engineer

CENTEK Engineering, Inc.

Structural Analysis – Mount Analysis T-Mobile Site Ref. ~ CT11328F Branford, CT June 19, 2019

Section 2 - Calculations

| | Subject: | | | Wind Load on | Equipmer | t per ASCE 7-10 |
|--|-------------------|--|--------------------------------|------------------------------|------------------|--------------------|
| Centered on Solutions [™] www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 Branford, CT 06405 F: (203) 488-8587 | Location: | | | Branford, CT | | |
| | Rev. 0: 6/10/2019 | | | Prepared by: Job No. 1902 | CAG Chec 7.41 | ked by: TJL |
| Design Wind Load on Other Str | uctures: | (Based on IBC 201 | 2, CSBC 20 ⁻ | 16 and ASCE 7-10) | | |
| Wi | nd Speed = | V := 140 | mph | (| (User Input) | (CSBC Appendix-N) |
| Ris | < Category = | BC := III | | (| (User Input) | (IBC Table 1604.5) |
| Exposure | Category = | Exp := C | | | (User Input) | |
| Struc | ture Type = | Structuretype := | Round_Ch | imney | (User Input) | |
| Structu | re Height = | Height := 99.7 | ft | | (User Input) | |
| Horizontal Dimension of Str | ucture = | Width := 12.99 | ft | (| (User Input) | |
| <u>Terrain Exposure (</u> Nominal Height of the Atmospheric Boundary Lay | | zg := 1200 if | | 900 | | (Table 26.9-1) |
| | | 900 if E 700 if E | | | | |
| 3-Sec Gust Speed Power Law Exp | onent = | α:= 7 if Exp 9.5 if Exp | p = C | 9.5 | | (Table 26.9-1) |
| Integral Length Scale | Factor = | 11.5 if E I:= 320 if Exp 500 if Exp | p = B = 5 | 00 | | (Table 26.9-1) |
| | | 650 if Exp | p = D | | | |
| Integral Length Scale Power Law Expor | ient = | $E := \begin{bmatrix} \frac{1}{3} & \text{if } Exp \\ \frac{1}{3} & \frac{1}{3} \end{bmatrix}$ | $\mathbf{D} = \mathbf{B} = 0.$ | 2 | | (Table 26.9-1) |
| | | 1 | | | | |
| | | $\frac{1}{8}$ if Exp |) = D | | | |
| Turbulence Intensity | /Factor= | c:= 0.3 if Exp 0.2 if Exp 0.15 if E | p = C | 0.2 | | (Table 26.9-1) |
| Exposure | Constant = | Z _{min} := 30 if 15 if 7 if E | | 15 | | (Table 26.9-1) |
| | | | | | | |

| Topographic Factor = | K _{zt} := 1 | (Eq. 26.8-2) |
|---------------------------------------|-----------------------|----------------|
| Wind Directionality Factor = | $K_{d} = 0.95$ | (Table 26.6-1) |
| Peak Factor for Background Response = | g _Q := 3.4 | (Sec 26.9.4) |
| Peak Factor for Wind Response = | g _V := 3.4 | (Sec 26.9.4) |

| | Subject: | | Wind Load on Equipme | nt per ASCE 7-10 |
|--|-------------------|---|--|-----------------------|
| Centered on Solutions [™] www.centekeng.com 63-2 North Branford Road P: (203) 488-0580 | Location: | | Branford, CT | |
| Branford, CT 06405 F: (203) 488-8587 | Rev. 0: 6/10/2019 | | Prepared by: CAG Che Job No. 19027.41 | cked by: TJL |
| Equivalent Height of Strue | oture = | z:= Z _{min} if Z _{min} > 0.6 0.6 Height otherwis | 6∙Height = 59.82 se | (Sec 26.9.4) |
| Intensity of Turbu | ilence = | $I_{z} := c \cdot \left(\frac{33}{z}\right)^{\left(\frac{1}{6}\right)} = 0.181$ | | (Eq. 26.9-7) |
| Integral Length Scale of Turbuler | ce = | $L_{Z} := I \left(\frac{z}{33} \right)^{E} = 563.166$ | | (Eq. 26.9-9) |
| Background Response | Factor = | $Q := \sqrt{\frac{1}{1 + 0.63 \left(\frac{\text{Width } + 1}{\frac{1}{2}}\right)}}$ | $\frac{1}{\frac{\text{Height}}{z}} = 0.902$ | (Eq. 26.9-8) |
| Gust Respons | e Factor = | $G := 0.925 \cdot \left[\frac{\left(1 + 1.7 \cdot g_{Q} \cdot I \right)}{1 + 1.7 \cdot g_{V}} \right]$ | $\left[\frac{\mathbf{z} \cdot \mathbf{Q}}{\mathbf{I}_{\mathbf{Z}}}\right] = 0.879$ | (Eq. 26.9-6) |
| Velocity P | ressure = | $q_{z} \coloneqq 0.00256 \cdot K_{zt} \cdot K_{d} \cdot V^{2}$ | = 47.67 | (Eq. 29.3-1) |
| Force Co | efficient = | C _f = 0.804 | | (Fig 29.5-1 - 29.5-3) |
| Ultimate Wind Pr | essure = | $F := q_{Z} \cdot G \cdot C_{f} = 33.7$ | psf | |
| HeightAbove | | Z := 115 ft $\left \begin{array}{c} 2\\ \alpha \end{array} \right ^{2} \left(\frac{2}{\alpha} \right) $ | (User Input) | (Table 29.3-1) |
| Exposure Co | emcient = | $K_{z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \\ \\ 2.01 \left(\frac{15}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \end{bmatrix}$ | 15 ≤ Z ≤ zg = 1.3 Z < 15 | |
| | | K _Z = 1.303 | | |
| HeightAbove | Grade = | Z := 90 ft | (User Input) | |
| Exposure Co | efficient = | $K_{z} := \begin{bmatrix} 2.01 \left(\frac{z}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \\ \\ 2.01 \left(\frac{15}{zg} \right)^{\left(\frac{2}{\alpha} \right)} & \text{if} \end{bmatrix}$ | $15 \le Z \le zg = 1.24$ Z < 15 | (Table 29.3-1) |
| | | | | |



Wind Load on Equipment per ASCE 7-10

Branford, CT 06405 F: (203) 488-8587

Location:

Rev. 0: 6/10/2019

Branford, CT

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HeightAbove Grade = Z := 65 ft (User Input) $K_{Z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } 15 \le Z \le zg = 1.16 \\ \\ 2.01 \left(\frac{15}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } Z < 15 \end{bmatrix}$ (Table 29.3-1) Exposure Coefficient = K₇ = 1.156 HeightAbove Grade = Z := 40 ft (User Input) $K_{z} := \begin{bmatrix} 2.01 \left(\frac{Z}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } 15 \le Z \le zg = 1.04 \\ \\ 2.01 \left(\frac{15}{zg}\right)^{\left(\frac{2}{\alpha}\right)} & \text{if } Z < 15 \end{bmatrix}$ (Table 29.3-1) Exposure Coefficient = K_z = 1.044

Wind on Other Stuctures (IBC 2012 ASCE 7-



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

sf

lbs

Branford, CT

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T-Mobile Loading:

| Development of Wind & Ice Load on Antennas | |
|--|--|
|--|--|

| Antenna Data: | | | |
|--------------------------------|--|---------------|--------------|
| Antenna Model = | RFSAPXVAA24_43 | -U-A20 | |
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 95.9 | in | (User Input) |
| Antenna Width = | W _{ant} := 24 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 8.7 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 128 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |
| Wind Load (Front) | | | |
| Surface Area for One Antenna = | SA _{ant} := $\frac{L_{ant} \cdot W_a}{144}$ | ant — = 16 | |

| Antenna Projected Surface Area = | $A_{ant} := SA_{ant} \cdot N_{ant} = 48$ | sf |
|----------------------------------|--|----|
| | | |

| $F_{ant} := F \cdot A_{ant} = 1614$ | lbs |
|-------------------------------------|-----|
|-------------------------------------|-----|

Wind Load (Side)

Surface Area for One Antenna =

Total Antenna Wind Force =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

 $SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 5.8$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 17.4$ sf

F_{ant} := F·A_{ant} = 585 lbs

WT_{ant}·N_{ant} = 384



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

Development of Wind & Ice Load on Antennas

| Antenna Model = | EricssonAIR21 (KR | C118023-1) | 1 |
|----------------------|---------------------------|------------|--------------|
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 56.3 | in | (User Input) |
| Antenna Width = | W _{ant} := 12.1 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 7.9 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 91.5 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |

Wind Load (Front)

| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} W_{ant}}{144} = 4.7$ | sf |
|--------------------------------|---|----|
|--------------------------------|---|----|

141

Antenna Projected Surface Area =

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

| $A_{ant} := SA_{ant} \cdot N_{ant} =$ | 14.2 | sf |
|---------------------------------------|------|-----|
| $F_{ant} := F \cdot A_{ant} = 478$ | | lbs |

 $SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 3.1$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 9.3$ sf

 $F_{ant} := F \cdot A_{ant} = 312$ lbs

lbs

 $WT_{ant} \cdot N_{ant} = 275$



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

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| Ericsson 4449 B12/B71 | |
|---|---|
| Flat (User Input) | |
| L _{RRH} ≔ 15.0 in <mark>(User Input)</mark> | |
| W _{RRH} := 13.2 in (User Input) | |
| T _{RRH} := 10.4 in (User Input) | |
| WT _{RRH} := 75 lbs (User Input) | |
| N _{RRH} := 3 (User Input) | |
| | |
| $SA_{RRH} := \frac{L_{RRH} W_{RRH}}{144} = 1.4$ | sf |
| $A_{RRH} := SA_{RRH} \cdot N_{RRH} = 4.1$ | sf |
| F _{RRH} := F·A _{RRH} = 139 | lbs |
| | |
| $SA_{RRH} := \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.1$ | sf |
| A _{RRH} := SA _{RRH} ·N _{RRH} = 3.3 | sf |
| F _{RRH} := F·A _{RRH} = 109 | lbs |
| | |
| WT _{RRH} ·N _{RRH} = 225 | lbs |
| | Flat(User Input) $L_{RRH} \coloneqq 15.0$ in(User Input) $W_{RRH} \simeq 13.2$ in(User Input) $T_{RRH} \simeq 10.4$ in(User Input) $W_{RRH} \simeq 75$ lbs(User Input) $W_{RRH} \simeq 75$ lbs(User Input) $W_{RRH} \simeq 3$ (User Input) $SA_{RRH} \simeq \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.4$ $A_{RRH} \simeq SA_{RRH} \cdot N_{RRH} = 4.1$ $F_{RRH} \simeq F \cdot A_{RRH} = 139$ $SA_{RRH} \coloneqq \frac{L_{RRH} \cdot T_{RRH}}{144} = 1.1$ $A_{RRH} \coloneqq SA_{RRH} \cdot N_{RRH} = 3.3$ $F_{RRH} \coloneqq F \cdot A_{RRH} = 109$ |



Location:

Rev. 0: 6/10/2019

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Wind Load on Equipment per ASCE 7-10

sf

lbs

lbs

lbs

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

Sprint Loading:

Development of Wind & Ice Load on Antennas

| <u>Antenna Data:</u> | | | | |
|----------------------|-------------------------|-----|--------------|--|
| Antenna Model = | Generic 6'Antenna | | | |
| Antenna Shape = | Flat | | (User Input) | |
| Antenna Height = | L _{ant} := 72 | in | (User Input) | |
| Antenna Width = | W _{ant} := 12 | in | (User Input) | |
| Antenna Thickness = | T _{ant} := 9.0 | in | (User Input) | |
| Antenna Weight = | WT _{ant} := 80 | lbs | (User Input) | |
| Number of Antennas = | N _{ant} := 3 | | (User Input) | |
| | | | | |

Wind Load (Front)

| Surface Area for One Antenna = SA _{ant} := - | $\frac{L_{ant} W_{ant}}{144} = 6$ | sf |
|---|-----------------------------------|----|
|---|-----------------------------------|----|

 $A_{ant} := SA_{ant} \cdot N_{ant} = 18$

 $F_{ant} := F \cdot A_{ant} = 606$

Antenna Projected Surface Area =

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

$SA_{ant} := \frac{L_{ant} T_{ant}}{144} = 4.5$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 13.5$ sf

 $F_{ant} := F \cdot A_{ant} = 454$

WT_{ant}·N_{ant} = 240



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

lbs

lbs

Branford, CT

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Development of Wind & Ice Load on Antennas

Surface Area for

Antenna Projected

| Antenna Model = | Generic 4'Antenna | | |
|----------------------|---------------------------|-----|--------------|
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 56 | in | (User Input) |
| Antenna Width = | W _{ant} := 12 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 8.0 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 60.0 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 3 | | (User Input) |

Wind Load (Front)

| r One Antenna = | $SA_{ant} := \frac{L_{ant} W_{ant}}{144} = 4.7$ | sf |
|-----------------|---|----|
| SurfaceArea = | $A_{ant} := SA_{ant} \cdot N_{ant} = 14$ | sf |

 $F_{ant} := F \cdot A_{ant} = 471$

Total Antenna Wind Force =

Wind Load (Side)

Surface Area for One Antenna =

Antenna Projected Surface Area =

Total Antenna Wind Force =

Gravity Load (without ice)

Weight of All Antennas =

 $SA_{ant} := \frac{L_{ant} \cdot T_{ant}}{144} = 3.1$ sf

 $A_{ant} := SA_{ant} \cdot N_{ant} = 9.3$ sf

F_{ant} := F·A_{ant} = 314 lbs

WT_{ant}·N_{ant} = 180



Subject:

Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

sf

sf

lbs

sf

sf

lbs

lbs

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

| Development of Wind & Ice Load on Antennas | | | |
|--|---|--------------------|--------------|
| Antenna Model = | Generic 3'MW Ante | enna | |
| Antenna Shape = | Flat | | (User Input) |
| Antenna Height = | L _{ant} := 36 | in | (User Input) |
| Antenna Width = | W _{ant} := 32 | in | (User Input) |
| Antenna Thickness = | T _{ant} := 12.0 | in | (User Input) |
| Antenna Weight = | WT _{ant} := 60.0 | lbs | (User Input) |
| Number of Antennas = | N _{ant} := 1 | | (User Input) |
| | | | |
| Wind Load (Front) | | | |
| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} \cdot W}{144}$ | $\frac{1}{2}$ = 8 | |
| Antenna Projected Surface Area = | A _{ant} := SA _{ant} ·N | ant ⁼ 8 | |
| Total Antenna Wind Force = | F _{ant} := F·A _{ant} = | 269 | |
| Wind Load (Side) | | | |
| Surface Area for One Antenna = | $SA_{ant} := \frac{L_{ant} T_{ant}}{144}$ | ant = 3 | |
| Antenna Projected Surface Area = | A _{ant} := SA _{ant} ·N _a | ant ^{= 3} | |
| Total Antenna Wind Force = | F _{ant} := F·A _{ant} = | 101 | |
| Gravity Load (without ice) | | | |
| Weight of All Antennas = | $WT_{ant} \cdot N_{ant} = 60$ | 0 | |
| | | | |



Location:

Rev. 0: 6/10/2019

Wind Load on Equipment per ASCE 7-10

Branford, CT

Prepared by: CAG Checked by: TJL Job No. 19027.41

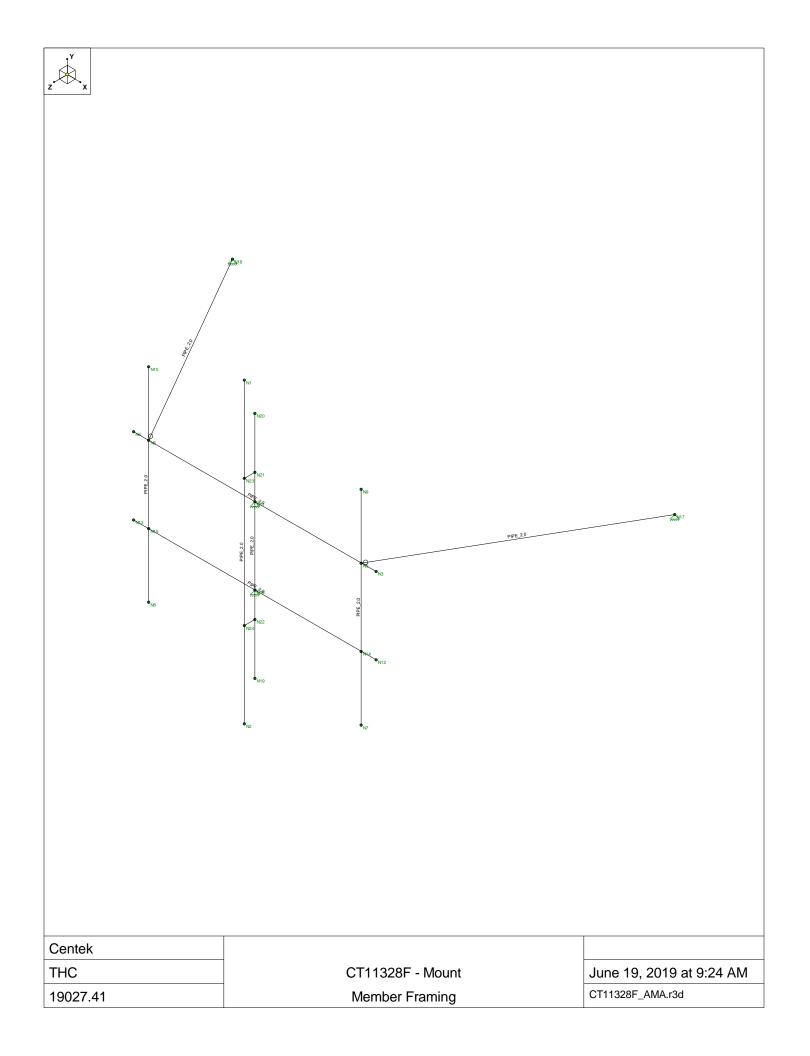
| Development of Wind & Ice Load on RRHs |
|--|
| |

| RRH Data: | | | |
|------------------|---------------------------|-----|--------------|
| RRH Model = | Generic RRH 1 | | |
| RRH Shape = | Flat | | (User Input) |
| RRH Height = | L _{RRH} := 20.9 | in | (User Input) |
| RRH Width = | W _{RRH} := 12.2 | in | (User Input) |
| RRH Thickness = | T _{RRH} := 10.8 | in | (User Input) |
| RRH Weight = | WT _{RRH} := 50.7 | lbs | (User Input) |
| Number of RRHs = | N _{RRH} := 9 | | (User Input) |

Wind Load (Front)

| Surface Area for One RRH = | $SA_{RRH} := \frac{L_{RRH} \cdot W_{RRH}}{144} = 1.8$ | sf |
|------------------------------|--|-----|
| RRH Projected Surface Area = | A _{RRH} := SA _{RRH} ·N _{RRH} = 15.9 | sf |
| Total RRH Wind Force = | F _{RRH} := F·A _{RRH} = 537 | lbs |
| Wind Load (Side) | | |
| Surface Area for One RRH = | $SA_{RRH} := \frac{L_{RRH} T_{RRH}}{144} = 1.6$ | sf |
| RRH Projected Surface Area = | A _{RRH} := SA _{RRH} ·N _{RRH} = 14.1 | sf |
| Total RRH Wind Force = | F _{RRH} := F·A _{RRH} = 475 | lbs |
| Gravity Load (without ice) | | |
| Weight of All RRHs = | WT _{RRH} ·N _{RRH} = 456 | lbs |

Wind on Other Stuctures (IBC 2012 ASCE 7-



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| Úæl{^ÁÔ^œeÁØæ&q[¦ÁQÚÔŒD | ÊÍ |
| Ô[}&\^&ÂĴd^••ÂÔ [&\ | Ü^&ca)* * a= |
| ₩•^ÁÔ¦æ&\^åÂÙ^&cąį}•Ñ | Ÿ^∙ |
| W∙^ÁÔ¦æ&∖^åÂÙ^&aąį}•ÂÛ æàÑ | Þ[|
| ÓæåÁØlæ{ā]*ÁYæ}}ãj*•Ñ | Þ[|
| W} ັ ∙ ^ å ÁØ[¦&^ÁY æ}}āj * •Ñ | Ϋ́^∙ |
| Tậ, ÁF Á Óæi Á Öãæ; ĐÂU] æ 8a; * Ñ | Þ[|
| Ô[}&\^&ÂÜ^àæłÂÜ^c | ÜÒӌܴÙÒV´ŒÙVT ŒÊFÍ |
| T ∄, ÁÃ ÁÙ c^^ Á[¦ ÁÔ[ĭ { } | F |
| Tæ¢ÆÃÂÛ&^^ Á[¦ÂÔ[˘{} | Ì |

fţ`cVUŁAcXY`GYHŋb[gź7cbl]bi YX

| Ù^ã{ ã&ÁÔ[å^ | ŒÙÔÒÄËF€ |
|------------------------------|--------------|
| Ù^ã { ã&/Óæ•^ÁÒ ^çæaã[}ÁĢdD | Þ[🕉 e^¦^å |
| ŒååÁÓæ•^ÁY^ãt@Ñ | Ÿ^∙ |
| ÔđÝ | È€G |
| Ô¢Ź | È€G |
| VÄYÁÇ∮^&D | Þ[🕉 🖓 🖒 ¦^å |
| VÁZÁĢ^&D | Þ[🕉 🖒 Å |
| ÜÄ | Н |
| ÜÆ | Н |
| ÔcĐ¢] ÈÝ | ËÍ |
| ÔơÔ¢] ĦŹ | ĔÍ |
| ÙÖF | F |
| ÙÖÙ | F |
| ÙF | F |
| VŠÁĢ^&D | ĺ |
| Üã∖ÁÔæ | CÁN HÁOQ |
| Ö¦ãð Öæc | Uc@\ |
| U{ÁZ | F |
| U{Ä | F |
| ÔåÁZ | I |
| ÔåÁÝ | |
| ÜQÁZ | F |
| ÜQÂY | F |
| | |

<chiFc``YX`GhYY`DfcdYfh]Yg

| | Šæà^ | ÒÃ. •ãa | ÕÃŽ•ãã | Þĭ | V@∾¦{ Áça∓ÒÍ Á⊘D | Ö^}∙ãĉŽĐcâHá | Ÿã∿∣åŽ∙ãá | Ü^ | ØŽ∙ãa | Üc |
|---|--------------|---------|--------|----|------------------|--------------|-----------|-----|-------|-----|
| F | O⊞Ĥ ÁÕ¦ÈHÎ | GJ€€€ | FFFÍ I | ÈH | ÊÍ | ÈJ | HÎ | FĚ | ÎÌ | FÈG |
| G | OÉÍGÁÕ¦Ě€ | GJ€€€ | FFFÍ I | ÈH | ÊÍ | ÈJ | Í€ | FÈF | ÍÌ | FÈG |
| Н | ŒJG | GJ€€€ | FFFÍ I | ÈH | ĒÍ | ÈJ | Í€ | FÈF | ÍÌ | FÈG |
| | OÉL€€ÃÕ¦ÈLG | GJ€€€ | FFFÍ I | ÈH | ĒÍ | ÈJ | ١G | FÈH | ÍÌ | FÈ |
| Í | OÉL€€ÃÕ¦ÈLÎ | GJ€€€ | FFFÍ I | ÈH | ĒÍ | ÈJ | ΙÎ | FÈG | ÍÌ | FÈ |
| Î | OÉLHÃÕ¦æå^ÁÓ | GJ€€€ | FFFÍ I | È | ÊÍ | ÈJ | HÍ | FĚ | ÍÌ | FÈG |

< chiFc``YX'GhYY'8 Yg][b'DUfUa YhYfg

| | Šæè^∣ | Ù@a∳^ | Š^}*c@Žcá | Šà^^Žeá | Šà∷Žcá | Š&[{]Á{[]Žcá | iŠ&[{]Áa[cŽcáŠĒq[¦˘˘⊞ | È S^^ | S:: | Ôà | Ø { & ca[i } |
|---|-------|--------------|-----------|---------|--------|--------------|-----------------------|-------|-----|----|--------------|
| F | ΤF | 05,0^}}æ∕Tæ | ¢FFËÎÎÏ | | | Šà^^ | Ù^*{ ∧È | È | | | Šæe^¦æ⊧ |
| G | ΤG | P[¦ã[}œ | JĚ | | | Šà^^ | Î | | | | Šæc^¦æ⊧ |
| Н | ΤН | 05, c^}}æÁTæ | ¢Ì | | | Šà^^ | | | | | Šææ^¦æ⊧ |
| | TI | 05, c^}}æ∕Tæ | ¢Ì | | | Šà^^ | | | | | Šææ^¦æ⊧ |
| Í | ТÍ | P[¦ã[}œ | JĚ | | | Šà^^ | Î | | | | Šææ^¦æ⊧ |
| Î | ΤÎ | Úą ∧ÁŒ€ | ÌÈJÌ | | | Šà^^ | | | | | Šææ^¦æ⊧ |
| Ï | ΤÏ | Úa¦^ÁGÈ€ | ÌÈJÌ | | | Šà^^ | | | | | Šææ^¦æ⊧ |
| Ì | ΤÌ | 05, ₫}}æ∕{Tæ | ¢ J | | | Šà^^ | | | | | Šæe^¦æ⊧ |

<chiFc``YX'GhYY''GYWFjcb'GYhg

| | Šæè^ | Ù@#}^ | V^]^ | Ö^∙ā*}ÁŠã≉c | Tæe∿¦ãæ¢ | Ö^• ã} ÁÜ⊞ | È07£ÄğiGá | Q^ÂŽajlá | Q:ÁŽájlá | RÁŽájlá |
|---|---------------|------------|--------|-------------|--------------|------------|-----------|----------|----------|---------|
| F | Úą]^ÁGÈ€ | ÚQÚÒ´GÈ€ (| Ó^æ{ | Úą ^ | OÉ HÃÕ¦æå^ÁÓ | V^] ã&æ¢ | FÈ€G | ÊĠ | ÊĞ | FÈGÍ |
| G | OEjc^}}æÁTæec | ÚQÚÒ′GÈ€ Ĉ | Ď[゙{} | Úą ^ | OÉ HÃÕ¦æå∧ÁÓ | V^] ã&æ | FÈ€G | ÊĠ | ÊĞ | FÉG |

<chiFc``YX'GhYY'GYWjcb'GYhg'f7cbhjbiYXŁ

| | Šæà^ | Ù@a} | V^]^ | Ö^∙ā*}ÁŠãa:c | Tæe∿¦ãæ¢ | Ö^• ã} ÁÜÈÈ | | Q,^ÁŽajlá | Q∷ÁŽajlá | RÁŽájlá |
|---|-----------|----------|------|--------------|--------------|-------------|------|-----------|----------|---------|
| H | P[¦ã[}œa∳ | ÚQÚÒ′GÈ€ | Ó^æ | Úą ^ | OÉ HÁÕ¦æå^ÁÓ | V^] 38æ | FÈ€G | ÊĠ | ÊĠ | FÈGÍ |

A Ya VYf Df]a Ufm8 UhU

| | Šæè^ | ØÂR[ậic | RÁR[ã}c | SÁR[ậ]c | Ü[œæ^Ģ∰ | | V^]^ | Ö^∙ã*}ÁŠãa:c | <u>Tæc</u> °¦ãæ; Ö^∙ð} ÁÜĭ ⊞ |
|----|------|---------|---------|---------|---------|---------------|--------|--------------|-------------------------------|
| F | TF | ÞF | ÞG | | | O5;c^}}æÁTærc | Ô[˘{} | Úą ^ | OEIHAO¦æEEE V^]ã&æe≱ |
| G | ΤG | ÞI | ÞH | | | P[¦ã[}œe) | Ó^æ | Úą ^ | OÉHÁÕ¦æ∰EV^]ã&æe |
| Н | ΤН | ÞÌ | ÞF€ | | | O5;c^}}æÁTærc | Ô[˘{} | Úą ^ | OÉHÁŐ¦æ∰EV^]ã&æ¢ |
| | TI | ÞÏ | ÞJ | | | O5;c^}}æÁTærc | Ô[˘{} | Úą ^ | OÉHÁÕ¦æ∰EV^]ã&æe |
| Í | ТÍ | ÞFH | ÞFG | | | P[¦ã[}œe) | Ó^æ | Úą ^ | OÉHÁŐ¦æ∰EV^]ã&æ¢ |
| Î | ΤÎ | ÞÎ | ÞFÌ | | | Úą ∧ÁGÈ€ | Ó^æ | Úą ^ | OÉHÁÕ¦æ∰EV^]ã&æe |
| Ï | ΤÏ | ÞÍ | ÞFÏ | | | Úą ∧ÁGÈ€ | Ó^æ | Úą ^ | OÉHÁŐ¦æ∰EV^]ã&æ¢ |
| Ì | ТÌ | ÞFJ | ÞŒ | | | O5;c^}}æÁTærc | Ô[゙{} | Úą ^ | OÉHÁÕ¦æ∰EV^]ã&æe |
| J | ТJ | ÞŒ | ÞGH | | | ÜÕÖ | Þ[}^ | Þ[}^ | ÜÕÕÖÖ V^]ä&aa |
| F€ | TF€ | ÞŒ | ÞG | | | ÜÕÖ | Þ[}^ | Þ[}^ | ÜÕÕÖÖ V^]ã&æ‡ |

>c]bh7ccfX]bUhYg'UbX'HYa dYfUh fYg

| | Šæà^ | ÝÆcá | ΫÆά | ZÁŽcá | V^{] <i>Ä</i> 226á | Ö^cæ&@%21[{ ÄÖãæ]@æ*{ |
|----|------|---------------|---------|----------|--------------------|---------------------------|
| F | ÞF | € | ÍÈH+⊪+⊪ | HÈEFÎÎÎÏ | € | |
| G | ÞG | € | ĔĖHH | HÈEFÎÎÎÏ | € | |
| Н | ÞH | ΙËÍ | FĚ | Н | € | |
| | ÞI | ËËÍ | FĚ | Н | € | |
| Í | ÞÍ | I È Î Î Î Î Ï | FĚ | Н | € | |
| Î | ÞÎ | ËÈÎÎÎÎÏ | FĚ | Н | € | |
| Ï | ÞÏ | I È Î Î Î Î Ï | Ë | Н | € | |
| Ì | ÞÌ | ËÈÎÎÎÎÏ | Ë | Н | € | |
| J | ÞJ | I ÈFÎÎÎÎÎ | | Н | € | |
| F€ | ÞF€ | ËÈÎÎÎÎÏ | | Н | € | |
| FF | ÞFF | €IËí | FĚ | Н | € | |
| FG | ÞFG | ΙËΊ | ËĚ | Н | € | |
| FH | ÞFH | ËËÍ | ËĚ | Н | € | |
| FI | ÞFI | I È Î Î Î Î Ï | ËĚ | Н | € | |
| FÍ | ÞFÍ | ËÈÎÎÎÎ | ËĒĚ | Н | € | |
| FÎ | ÞFÎ | € | ËĚ | Н | € | |
| FΪ | ÞFÏ | ÌÈÎÎÎÎÏ | FĚ | ËËJFÎÎÏ | € | |
| FÌ | ÞFÌ | ËÈÎÎÎÎ | FĚ | ËËJFÎÎÏ | € | |
| FJ | ÞFJ | €È | ËĚ | Н | € | |
| G€ | ÞŒ | €È | ΙĚ | Н | € | |
| GF | ÞŒ | € | GĚ | Н | € | |
| GG | ÞGG | € | ËGĚ | Н | € | |
| GH | ÞGH | € | GĚ | HÈEFÎÎÎÏ | € | |
| G | ÞĠ | € | ËGĚ | HÈFÎÎÎÏ | € | |

>c]bhi6 ci bXUf m7 cbX]h]cbg

| | R[ð] 0ÁŠæà∧ | ÝÄŽHBjá | ΫÁΣΈλ)já | ZÃŽHBjá | Ý ÁÜ[dĚŽ ËdĐæåá | ŸÁÜ[dĚŽËeĐæåá | ZÁÜ[dĚŽËe®Dæåá |
|---|-------------|------------|-------------|-----------|------------------|---------------|----------------|
| F | ÞFF | Ü^æ\$kaį[} | Ü^æ\$kaįį } | Ü^æ\$cāį} | | | |
| G | ÞĤ | Ü^æ\$cā[} | Ü^æ\$kaįį } | Ü^æ\$cā[} | | | |
| Η | ÞFÌ | Ü^æ\$ka‡i} | Ü^æ\$kaãį} | Ü^æ\$cā[} | | | |

>c]bh6cibXUfm7cbX]h]cbgf7cbh]biYXŁ

| _ | R[ð] o∕Šæà^∣ | ÝÃŽĐãjá | ΫÄΣីĐϡjá | ZÁŽIBAjá | Ý ÁÜ[dĚŽ ËdĐæåá | ŸÁÜ[dĚŽËeĐæåá | ZÁÜ[dĚŽË+®Dæåá |
|---|--------------|-------------|-------------|-------------|------------------|---------------|----------------|
| | ÞFÏ | Ü^æ\$kaji } | Ü^æ\$kaji } | Ü^æ\$ka¶{ } | | | |
| Í | ÞŒ | | | | | | |
| Î | ÞGG | | | | | | |
| Ï | ÞGH | | | | | | |
| Ì | ÞG | | | | | | |

A Ya VYf Dc]bh@cUXg f6 @ &. K Y][\ hcZ9ei]da YbhL

| | T^{à^¦ÁŠæèà^∣ | Öãi^&cãa;} | Tæ*}ãčå^ŽÈËœá ∰∃Î | Š[&æa‡]}ŽeĐÃá à F€€ |
|---|---------------|------------|----------------------|------------------------|
| F | TI | Ϋ́ | | à F€€ |
| G | TI | Ϋ́ | Ë Î | HÈHÀ |
| Н | TH | Ϋ́ | Ë Î | à F€€ |
| | TH | Ϋ́ | Ë Î | HÈHÀ |
| Í | TH | Ϋ́ | i i i | FÈEI G |
| Î | TF | Ϋ́ | Ë I | € |
| Ï | TF | Ϋ́ | Ë I | Ì |
| Ì | TF | Ϋ́ | i i i | FÈG |

A Ya VYf Dc]bh'@cUXg f6 @7 '' . K]bX @ UX LŁ

| | T^{à^¦AŠæèà^∣ | Öãi^&cãį} | Tæ*}ãčå^ŽÊËcá | ŠĮ&aæaį}ŽebÃá HĒHĒÌ |
|---|---------------|-----------|---------------------------------------|------------------------|
| F | TI | Ý | ÌÈÉÍ G | HÈHÌ |
| G | TI | Ý | Ì È€Í G | à F€€ |
| Н | TH | Ý | Ì È€Í G | HÈHÈ |
| 1 | TH | Ý | Ì È€Í G | à F€€ |
| Í | TH | Ý | È€FF | FÈEI G |
| Î | TF | Ý | Ì È.JÌ | € |
| Ï | TF | Ý | L L L L L L L L L L L L L L L L L L L | Ì |
| Ì | TF | Ý | ÌÈ€HÎ | FÉG |

A Ya VYf Dc jbh@cUXg f6 @r (. K jbX @ UX NL

| | T^{ à^¦ÁŠæè^ | Öã^&cãį} | Tæ*}ããå^ŽÈËœá | Š[&ææð[}Žeb∄á à F€€ |
|---|--------------|----------|---------------|------------------------|
| F | TI | Z | Ē | à F€€ |
| G | TI | Z | È | HÈHÊ |
| Н | ТН | Z | È | à F€€ |
| 1 | ТН | Z | È | HÈHÊ |
| Í | ТН | Z | È€FÏ | FÈEI G |
| Î | TF | Z | ÈĴJ | € |
| Ï | TF | Z | ÈĴJ | Ì |
| Ì | TF | Z | È Î | FÈG |

>c]bhi@UXg'UbX'9 bZcf WXX'8]gd`UWYa Ybhg'

| F[ậ c/Šæà^ | ŠÊÊÊ | Öã^&cãį} | Tæ*}ãc å^Ž0;Ê:Ë:edDÉ4QãÈÈ |
|-------------|----------------------|----------|---------------------------|
| | Þ[ÁÖæsæák[ÁÚ¦ð] dÁ 🗄 | | |
| | | | |

A Ya VYf 8]ghf]Vi hYX @ UXg f6 @ '' . K]bX @ UX L Ł

| | T^{à^¦ÁŠæaà^∣ | Öãi^&cãįį} | ÙcæloÁTæ*}ãĩå^ŽĐeB2Ê∙-á | Ò}åÁTæ≛}ãčå^ŽĐdÊ2Ê∙-á | ÙcæloÁŠ[&ææā]}ŽeÉÃá | Ò}åÆŠ[&ææã[}ŽdÉÄá |
|---|---------------|------------|-------------------------|-----------------------|---------------------|-------------------|
| F | ΤÎ | Ý | Ì€€Ï | Ì€€Ï | € | € |
| | | | | | | |

A Ya VYf 8 jghf jVi hYX @ UXg f6 @ " ' . K jbX @ UX L Ł ff c bljbi YXŁ

| | T^{à^¦∕Šæèà^∣ | Öãi^&cãį}} | Ùcæ¦c∕∓ æ*}ãĩå^ŽÐe£DÊ•-á | Ò}åÁTætੋ}ãčå^ŽīĐœÊØÊ∙-á | Ùcælo∕ÄŠ[&æaā]}ŽeÉÃá | Ò}åÆŠ[&æa∰[}ŽdÉÃá |
|---|---------------|------------|--------------------------|-------------------------|----------------------|-------------------|
| G | ΤÏ | Ý | Ì€€Ï | Ì€€Ï | € | € |
| Н | TF | Ý | Ì€€Ï | Ì€€Ï | € | € |
| | TH | Ý | Ì€€Ï | Ì€€Ï | € | € |
| Í | TI | Ý | Ì€€Ï | Ì€€Ï | € | € |
| Î | ΤÌ | Ý | Ì€€Ï | Ì€€Ï | € | € |

A Ya VYf 8]ghf]Vi hYX @ UXg f6 @ (`. K]bX @ UX NL

| | T^{à^¦∕iŠæaà^∣ | Öãi^&cã∦} | ÙcælcÁTæ*}ãčå^ŽĐe£DÊ∙~á | Ò}åÁTætੋ}ãčå^ŽĐœÊ2Ê∙-á | Ùcæ¦oÆŠ[&æe‡ā]}ŽeÉÃá | Ò}åÆŠ[&ææã[}ŽdÉÃá |
|---|----------------|-----------|-------------------------|------------------------|----------------------|-------------------|
| F | TG | Z | Ì€€Ï | Ì€€Ï | € | € |
| G | ΤÍ | Z | Ì€€Ï | Ì€€Ï | € | € |
| Н | TH | Z | Ì€€Ï | Ì€€Ï | € | HÈHÈ |
| | TI | Z | Ì€€Ï | Ì€€Ï | € | HÈHÈ |
| Í | TF | Z | Ì€€Ï | Ì€€Ï | Ì | FFËÎÏ |

6 Ug]W@ UX 7 UgYg

| | ÓŠÔÁÖ^•&¦ājcāj} | Ôæe^*[¦^ | ÝÁÕ¦æçãcî | ŸÁÕ¦æçãĉ | ZÁÕ¦æçÈ | ÈR[ậ]c | Ú[ậ]c | ÖãidiãaĭÈÈ | ÈE^æÇT ÈË | È Ùĭ¦æ&∿QÚ∥æc∿ÐYæ∦D |
|---|--------------------|----------|-----------|----------|---------|--------|-------|------------|-----------|---------------------|
| F | Ù^ ÁY ^ã@c | ÖŠ | | Ë | | | | | | |
| G | Y^ãt@da(ÁÔ°°ã]{^}c | ÖŠ | | | | | Ì | | | |
| Н | YājåÁŠ[æáðÁÝ | Y ŠÝ | | | | | Ì | Î | | |
| | Yā}åÁŠ[æåÁZ | ΥŠΖ | | | | | Ì | Í | | |

@UX'7 ca V]bUhjcbg

| | Ö^∙&¦ājcāj} | Ù[ç^ | ÚÖÈ | €ÜÜÈÉÓŠÔ | Øæ | ÈÓŠÔ | Øæ | ÈÓÈÈ | Øæ | Ó∰C | (addit) | ÎÊØæ | ŤÓĤ | Øæ | ΰ | Øæ | ĔÓÈ | Øæ | Ť | Øæ | Ŭ₩ | Øæ |
|----|---------------------|--------|-----|----------|----|------|----|------|----|-----|---------|------|-----|----|---|----|-----|----|---|----|----|----|
| F | cá ô á fí ê | Ÿ^∙ | Ÿ | ÖŠ | F | | | | | | | | | | | | | | | | | |
| G | QÓÔÁFÎ ËJ | Ϋ́^∙ | Ÿ | ÖŠ | F | ŠŠ | F | Š⊞ | F | | | | | | | | | | | | | |
| Н | QÓÔÁFĨ ËFGÁQÐÁQÐ | Ϋ́^∙ | Ÿ | ÖŠ | F | Y ŠÝ | Ê | | | | | | | | | | | | | | | |
| 1 | QÓÔÁFĨ ËFGÁQÐÁQAD | Ϋ́^∙ | Ÿ | ÖŠ | F | ΥŠΖ | Ê | | | | | | | | | | | | | | | |
| Í | ÓÓÁFÎ ËFGÁÇæÐÁÇ&D | Ϋ́^∙ | Ÿ | ÖŠ | F | Y ŠÝ | Ĩ | | | | | | | | | | | | | | | |
| Î | ÓÓÔÁFÎËFGÁGÆÐÁGàD | Ϋ́∧∙ | Ÿ | ÖŠ | F | ΥŠΖ | Ë | | | | | | | | | | | | | | | |
| Ï | QÓÔÁFÎ ËFHÁÇæÐÁÇæÐ | Ϋ́^∙ | Ÿ | ÖŠ | F | Y ŠÝ | | ŠŠ | | ŠĦ | | | | | | | | | | | | |
| Ì | QÓÔÁFÎ ËFHÁÇaĐÁÇa D | Ϋ́∧∙ | Ÿ | ÖŠ | F | Y ŠZ | ÈÍ | ŠŠ | | ŠĦ | | | | | | | | | | | | |
| J | QÓÔÁFÎ ËFHÁÇæÐÁQ&D | Ÿ^∙ | Ÿ | ÖŠ | F | Y ŠÝ | | ŠŠ | | ŠĦ | | | | | | | | | | | | |
| F€ | QÓÔÁFÎ ËFHÁÇaĐÁÇã D | Ÿ^∙ | Ÿ | ÖŠ | F | ΥŠΖ | ₿É | ŠŠ | ËÍ | ŠĦ | Í | | | | | | | | | | | |
| FF | có ôáfî 🛱 Á Gar | Ÿ^∙ | Ÿ | ÖŠ | Ê | Y ŠÝ | Ê | | | | | | | | | | | | | | | |
| FG | QÓÔÁFÎ ËFÍ ÁGAD | Ÿ^∙ | Ÿ | ÖŠ | Ê | ΥŠΖ | Ê | | | | | | | | | | | | | | | |
| FH | góôáfî Éfí Á Sed | Ÿ^∙ | Ÿ | ÖŠ | Ê | Y ŠÝ | | | | | | | | | | | | | | | | |
| FI | QÓÔÁFÎ ËFÍ ÁQªD | Ϋ́^∙ | Ÿ | ÖŠ | Ê | ΥŠΖ | Ϊ | | | | | | | | | | | | | | | |

9bjYcdY>c]bhFYUMJcbg

| | RĮą̃ic | | ÝÄŽá | ŠÔ | ŸÁŽÍá | ŠÔ | ZÄŽá | ŠÔ | ΤÝÄŽËcá | ŠÔ | ΤΫÁŽËcá | ŠÔ | TZÁŽËcá | ŠÔ |
|---|--------|------------|----------------------|----|-------|----|------|----|---------|----|---------|----|---------|----|
| F | ÞFF | { 28¢ | Ě FF | Í | FÈHG | Î | ÈĤI | FI | € | FI | € | FI | € | FI |
| G | | { ā | ⊞H I | FF | ËËÎÍ | FG | ËÈFÏ | I | € | F | € | F | € | F |
| Н | ÞFÎ | { 28¢ | i i ter ì | FH | FÈHFI | Ι | ÈËÏÎ | Î | € | FI | € | FI | € | FI |
| | | { ā | ⊞n J | Η | ËÏG | FI | Ë€GH | FG | € | F | € | F | € | F |
| Í | ÞFÌ | { 28¢ | È | FI | Ì€FÎ | Ι | ÈGJ | FI | € | FI | € | FI | € | FI |
| Î | | { ā | ÉÉÉÍ | | È€€J | F | ËÈH | - | € | F | € | F | € | F |
| Ï | ÞFÏ | { æ¢ | ÈÎJ | | Ì€ | | ÈÈFJ | FI | € | FI | € | FI | € | FI |

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| | RĮą̃c | | ÝÃÃjá | ŠÔ | ΫÄãjá | ŠÔ | ZÄŽājá | ŠÔ | Ý ÁÜ[cæqā]} Á À ÉÉÉŠÔ | ŸÁÜ[cæaā]}Á2Ê | ÈŠÔZÁÜ[œaaā]}ÁŽÈÈÈŠÔ |
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| Н | ÞG | { æ¢ | È€ÍÏ | H | È€€J | FI | È | FI | GÈEÎÍ∧ËEH I | ÎÈ€JH^Ë€I | H FÈÈÌG∿Ë€H H |
| | | { a | ËEHÏ | FH | Ë€FG | | Ë€JJ | 1 | ËFÈLÌF^ËEH FI | ËËËJI∧Ë€I | FH ÉÈÈGF∧Ë€I FH |
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| GG | | { a | € | F | € | F | € | F | ËFÈLÍ^Ë€H FI | ËHÈUJ^ËE | Í ÈÈÌHNËEI FF |
| GH | ÞFG | { 286¢ | € | FF | Ë€G | FH | È€FH | FG | ÏËEG∿Ë€IÎ | HÈLIF^Ë€ | Î ËGËGËÎ^ËE FH |
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| HH | ÞFÏ | { 28¢ | € | FI | € | FI | € | FI | GÈEH^Ë€H H | FÈ€JÏ ^Ë€H | |
| H | | { a | € | F | € | F | € | F | <u>ÏÈHÎH^ÊG FH</u> | ËFÈEJI^ËEH | FH ËFÈGÂ^ËEI FG |
| HÍ | ÞFÌ | { æ¢ | € | FI | € | FI | € | FI | | FÈ€JH^Ë€H | |
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| ΙÎ | | { ā | Ë | Í | ËEFÍ | - | Ë€GÎ | FI | ËGËLFJ^ËEH FI | ËÈÌÎ^ËE | Í | ËGËËÏÎ∧ËEH | FF |
| ΠÏ | ÞG | { æ¢ | È€FH | H | È€€J | F | Ì€€J | FI | GÈHG+∧Ë€HI | ÎÈ€JH^Ë€I | Н | JÆJ €A ÆI | Н |
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| F | TF | ÚŒÚÒ GÈE | ÈJF | HÈGÈÈÈ | I | È€H€ | FÈHÏ | | 1 | IÈ€Ì | ŒĤÏ | FÈGIÍ | FÈGIÍ | IÈFJ | PFËFà |
| G | TG | ÚQÚÒ′ GÈ€ | ÈË | IËÍ | Н | È€IÏ | ΙËÍ | | 1 | ÏÈÉÍG | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | FÈÏÎ | PFËFà |
| Н | TH | ÚQÚÒ′ GÈ€ | ÈGF | ÍĚ | Í | È€IH | HÈHH | | Î | JÐG | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | HÈ€F | PFËFà |
| 1 | TI | ÚQÚÒ′ GÈ€ | ÈÎÎ | ÍĚ | H | Ì€GÍ | HÈHH | | Î | JÐG | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | HÈHGÍ | PFËFà |
| Í | ΤÍ | ÚQÚÒ′ GÈ€ | ÈĜÎ | IËÍ | Í | È€ÍF | ΙËΊ | | 1 | ÏÈGÍG | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | FÈÏG | PFËFà |
| Î | ΤÎ | ÚQÚÒ′ GÈ€ | ÈEIF | IÈÈ | Í | È€€I | ÌÈJÌ | | Í | | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | FÈFHÎ | PFËFà |
| Ï | ΤÏ | ÚQÚÒ′ GÈ€ | È€IF | IÈÈ | Η | È€€I | ÌÈJÌ | | Í | | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | FÈEĤ | PFËFà |
| Ì | TÌ | ÚŒÚÒ′ GÈE | ÈGÍH | Î | FI | ÈÏI | Î | | Í | ÌÈÈÌ | ŒÈÏÏ | FÈGIÍ | FÈGIÍ | HÈHÌI | PFËrà |

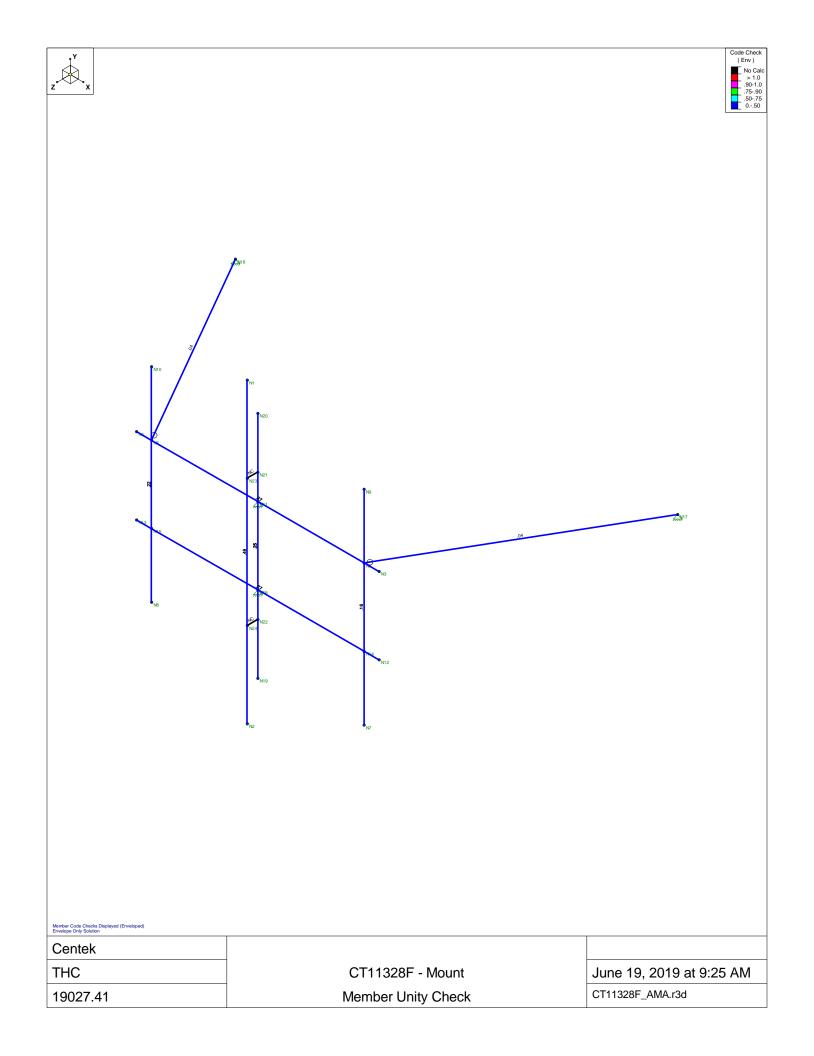


Exhibit F Power Density/RF Emissions Report



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11328F

Marine Sys. Smoke Stack 50 Maple Street Branford, Connecticut 06405

May 29, 2019

EBI Project Number: 6219001861

| Site Complian | ce Summary |
|---|------------|
| Compliance Status: | COMPLIANT |
| Site total MPE% of FCC general population allowable limit: | 12.81% |



May 29, 2019

T-Mobile Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, Connecticut 06002

Emissions Analysis for Site: CT11328F - Marine Sys. Smoke Stack

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **50 Maple Street** in **Branford, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm²). The number of μ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

<u>General population/uncontrolled exposure</u> limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400 μ W/cm² and 467 μ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



<u>Occupational/controlled exposure</u> limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over their exposure and can exercise control over the potential for exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 50 Maple Street in Branford, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 GSM/UMTS channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 2 UMTS channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 2 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.



- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the Ericsson AIR21 B2A_B4P for the 1900 MHz / 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 700 MHz channel(s), the Ericsson AIR21 B2P_B4A for the 2100 MHz channel(s) in Sector A, the Ericsson AIR21 B2A_B4P for the 1900 MHz / 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 700 MHz channel(s), the Ericsson AIR21 B2P_B4A for the 2100 MHz channel(s) in Sector B, the Ericsson AIR21 B2A_B4P for the 1900 MHz / 2100 MHz channel(s) in Sector B, the Ericsson AIR21 B2A_B4P for the 1900 MHz / 2100 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 700 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 700 MHz channel(s), the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 700 MHz channel(s), the Ericsson AIR21 B2P_B4A for the 2100 MHz channel(s) in Sector C. This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerline of the proposed antennas is 96 feet above ground level (AGL).
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 11) All calculations were done with respect to uncontrolled / general population threshold limits.



T-Mobile Site Inventory and Power Data

| | | | | | - |
|---------------------|------------------------------|---------------------|------------------------------|---------------------|------------------------------|
| Sector: | A | Sector: | В | Sector: | С |
| Antenna #: | I | Antenna #: | I | Antenna #: | I |
| Make / Model: | Ericsson AIR21 B2A_B4P | Make / Model: | Ericsson AIR21 B2A_B4P | Make / Model: | Ericsson AIR21 B2A_B4P |
| Frequency Bands: | 1900 MHz / 2100 MHz | Frequency Bands: | 1900 MHz / 2100 MHz | Frequency Bands: | 1900 MHz / 2100 MHz |
| Gain: | 15.35 dBd / 15.35 dBd | Gain: | 15.35 dBd / 15.35 dBd | Gain: | 15.35 dBd / 15.35 dBd |
| Height (AGL): | 96 feet | Height (AGL): | 96 feet | Height (AGL): | 96 feet |
| Channel Count: | 4 | Channel Count: | 4 | Channel Count: | 4 |
| Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts |
| ERP (VV): | 4,113.21 | ERP (VV): | 4,113.21 | ERP (VV): | 4,113.21 |
| Antenna AI MPE %: | 1.60% | Antenna BI MPE %: | 1.60% | Antenna CI MPE %: | 1.60% |
| Antenna #: | 2 | Antenna #: | 2 | Antenna #: | 2 |
| Make / Model: | RFS APXVAARR24_43-U- NA20 | Make / Model: | RFS APXVAARR24_43-U- NA20 | Make / Model: | RFS APXVAARR24_43-U- NA20 |
| Frequency Bands: | 600 MHz / 700 MHz | Frequency Bands: | 600 MHz / 700 MHz | Frequency Bands: | 600 MHz / 700 MHz |
| Gain: | 12.95 dBd / 13.35 dBd | Gain: | 12.95 dBd / 13.35 dBd | Gain: | 12.95 dBd / 13.35 dBd |
| Height (AGL): | 96 feet | Height (AGL): | 96 feet | Height (AGL): | 96 feet |
| Channel Count: | 4 | Channel Count: | 4 | Channel Count: | 4 |
| Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts |
| ERP (VV): | 2,481.08 | ERP (VV): | 2,481.08 | ERP (VV): | 2,481.08 |
| Antenna A2 MPE %: | 2.24% | Antenna B2 MPE %: | 2.24% | Antenna C2 MPE %: | 2.24% |
| Antenna #: | 3 | Antenna #: | 3 | Antenna #: | 3 |
| Make / Model: | Ericsson AIR21 B2P_B4A | Make / Model: | Ericsson AIR21 B2P_B4A | Make / Model: | Ericsson AIR21 B2P_B4A |
| Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz | Frequency Bands: | 2100 MHz |
| Gain: | 15.35 dBd | Gain: | 15.35 dBd | Gain: | 15.35 dBd |
| Height (AGL): | 96 feet | Height (AGL): | 96 feet | Height (AGL): | 96 feet |
| Channel Count: | 2 | Channel Count: | 2 | Channel Count: | 2 |
| Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts | Total TX Power (W): | 120 Watts |
| ERP (VV): | 4,113.21 | ERP (VV): | 4,113.21 | ERP (VV): | 4,113.21 |
| Antenna A3 MPE %: | 1.60% | Antenna B3 MPE %: | 1.60% | Antenna C3 MPE %: | 1.60% |



environmental | engineering | due diligence

| Site Composite MPE % | | | | | | | |
|-----------------------------|--------|--|--|--|--|--|--|
| Carrier | MPE % | | | | | | |
| T-Mobile (Max at Sector A): | 5.45% | | | | | | |
| Sprint | 7.36% | | | | | | |
| Site Total MPE % : | 12.81% | | | | | | |

| T-Mobile Sector A Total: | 5.45% |
|--------------------------|--------|
| T-Mobile Sector B Total: | 5.45% |
| T-Mobile Sector C Total: | 5.45% |
| | |
| | |
| Site Total: | 12.81% |

| T-Mobile Maximum MPE Power Values (Sector A) | | | | | | | | |
|---|---------------|-------------------------------|------------------|------------------------------------|--------------------|---------------------------|------------------|--|
| T-Mobile Frequency Band / Technology (Sector A) | # Channels | Watts ERP (Per Channel) | Height (feet) | Total Power Density (µW/cm²) | Frequency (MHz) | Allowable MPE (µW/cm²) | Calculated % MPE | |
| T-Mobile 1900 MHz GSM/UMTS | 2 | 1028.30 | 96.0 | 8.02 | 1900 MHz GSM/UMTS | 1000 | 0.80% | |
| T-Mobile 2100 MHz UMTS | 2 | 1028.30 | 96.0 | 8.02 | 2100 MHz UMTS | 1000 | 0.80% | |
| T-Mobile 600 MHz LTE | 2 | 591.73 | 96.0 | 4.62 | 600 MHz LTE | 400 | 1.15% | |
| T-Mobile 700 MHz LTE | 2 | 648.82 | 96.0 | 5.06 | 700 MHz LTE | 467 | 1.08% | |
| T-Mobile 2100 MHz LTE AWS | 2 | 2056.61 | 96.0 | 16.05 | 2100 MHz LTE AWS | 1000 | 1.60% | |
| | | | | | | Total: | 5.45% | |

• NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (%) | | | |
|-------------------------|-------------------------|--|--|--|
| Sector A: | 5.45% | | | |
| Sector B: | 5.45% | | | |
| Sector C: | 5.45% | | | |
| T-Mobile Maximum | 5.45% | | | |
| MPE % (Sector A): | | | | |
| | | | | |
| Site Total: | 12.81% | | | |
| | | | | |
| Site Compliance Status: | COMPLIANT | | | |

The anticipated composite MPE value for this site assuming all carriers present is **12.81%** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

Exhibit G Mailing Receipts/Proof of Notice

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