



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

December 13, 1999

Peter W. van Wilgen, Director – Real Estate Operations
SNET Wireless, Inc.
500 Enterprise Drive
Rocky Hill, CT 06067-3900

RE: TS-SCLP-013-990317 - Springwich Cellular Limited Partnership request for an order to approve tower sharing at an existing telecommunications facility located off 3 Polly Lane in Bozrah, Connecticut.

Dear Mr. van Wilgen:

At a public meeting held December 8, 1999, the Connecticut Siting Council (Council) ruled that the shared use of this existing tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility as reconfigured to avoid the unnecessary proliferation of tower structures.

This facility has been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequency now used on this tower. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

The proposed shared use is to be implemented as specified in your letter dated November 15, 1999 concerning relocation of antennas from the 160-foot level to the 195-foot level of this existing tower, in additional information dated November 24, 1999, and in a letter dated December 7, 1999 concerning tower sharing for Sprint PCS antennas.

Thank you for your attention and cooperation.

Very truly yours,

Mortimer A. Gelston
Chairman

MAG/SLL/sll

cc: Honorable Raymond C. Barber, First Selectman, Town of Bozrah
Steve Kotfila, Site Development Manager, Sprint PCS
Ronald C. Clark, Manager – Real Estate, Nextel Communications
J. Brendan Sharkey, Esq., Omnipoint Communications

HURWITZ & SAGARIN LLC

December 7, 1999

Via Facsimile and Overnight Delivery

Mr. Mortimer A. Gelston, Chairman
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

RECEIVED

DEC 08 1999

CONNECTICUT
SITING COUNCIL

RE: Sprint co-location on CDT telecommunications tower located at
2 Polly Lane, Bozrah, Connecticut.

Dear Chairman Gelston:

Sprint Spectrum L.P. ("Sprint PCS") entered into a lease agreement with Cordless Data Transfer, Inc. ("CDT") to install antennas and related base station equipment on the existing telecommunications tower located at 2 Polly Lane, Bozrah, Connecticut ("Facility"). The Facility is located on property owned by Alice Maynard and is operated and managed by CDT. CDT received zoning approval from the Town of Bozrah ("Town") for the construction of the Facility on October 9, 1997. In accordance with its policy of co-location whenever possible, Sprint PCS sought to co-locate on the Facility, rather than construct a new telecommunications tower in this area.

Sprint PCS supplied the Town with its site plans and information regarding its proposed installation. Sprint PCS received a building permit for its proposed co-location on May 6, 1999 and subsequently installed its antennas and base station equipment in accordance with this permit. A copy of the building permit is attached hereto.

It has been brought to my attention that Springwiche Cellular Limited Partnership received approval from the Connecticut Siting Council ("Council") on April 6, 1999 to co-locate on the Facility. At the time Sprint PCS received the Town's approval to co-locate on the Facility, Springwiche was not yet located on the Facility and Sprint PCS was unaware that Springwiche had received approval from the Council a month earlier. As a result, Sprint PCS hereby submits its power density calculations for this installation and requests that the Council approve its co-location on this Facility. Sprint PCS respectfully submits that its co-location on this Facility is technically, legally, environmentally, and economically feasible and is in compliance with the provisions of C.G.S. §16-50aa. Further, Sprint PCS represents that, in compliance with the provisions of R.C.S.A. § 16-50j-72(b)(2), the Sprint PCS co-location on this Facility has not increased the existing height of the tower, extended the boundaries of the site, increased the noise level at the site by six decibels, or increased the radio frequency electromagnetic radiation to or above the applicable standard.

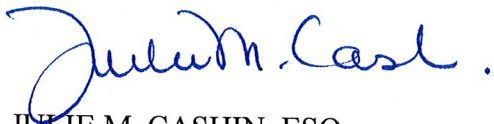
LAW OFFICES

147 North Broad Street, P.O. Box 112, Milford, Connecticut 06460-0112

Tel. 203-877-8000 • Fax 203-878-9800

Please contact me if I can provide you with any further information or documentation.

Very truly yours,



JULIE M. CASHIN, ESQ.

JMC/dsw

Enclosure

cc: Joel Rinebold, Executive Director, Connecticut Siting Council
Steve Levine, Staff Analyst, Connecticut Siting Council
Michelle Briggs, SNET
William McElwaine

TOWN OF BOZRAH

Zone: L-30

Building Permit Record Date: 5-6-99

ALICE MAYNARD

Owner: Sprint Spectrum LP, 9 Barnes Ind Rd Wallingford, CT 06492
 Address: 2 Polly Lane, Bozrah

DESCRIPTION RESIDENTIAL COMMERCIAL INDUSTRIAL OTHER
 New: Addition: Accessory: Remodel: Alteration: Improvements: Other:

RADIO COMMUNICATIONS EQUIPMENT INSTALLATION ON EXISTING TOWER OWNED BY CORDLESS DATA TRANSFER.

Class: <u>U</u>	Flooring:	Tile Bath:	Lot No.:
Tv <u>/</u>	Int. Walls:	Walls:	Lot Size:
No. of Rms:	Electrical:	Shower:	Set Back:
No. of Stories:		Floors:	Side Yard:
Floor Area:		Heating:	Back Yard:
Foundation:	No. of Bathrooms:	Wa. Htg:	Sub-Div.:
Construction: <u>CONCRETE SLAB</u>	Plumbing Fixtures:	Stm. Htg:	Hot Water Supply
Ext. Walls: <u>PRE FAB EQUIP BUILDING</u>	Sink:	H. W. Htg:	Fireplace:
Roofing:	Toilets:	Space Htg:	City Water:
Basement:	Basins:	Fuel:	Weil Water:
	Bathtubs:	Oil:	Septic
	Shrstoil:	Gas:	Sewer:
		Elec.:	
		Air Cond.:	

Architect: <u>NATCOM LLC</u>	Est. Costs: <u>25,000</u>
Address: <u>63-2 N. Branford Rd. Branford, CT 06405</u>	Sewerage Permit Fee:
Phone: <u>CORDLESS DATA TRANSFER, INC 860-745-0445</u>	Building Permit Fee: <u>\$200.00</u>
Address: <u>17 Ridgewood Drive, MARLBOROUGH, CT 06147</u>	Trade Permit Fee:
Applicant's Signature: <u>[Signature] President CDT</u>	
Issued by Building Inspector: <u>[Signature]</u>	Total: <u>\$200.00</u>

**CT33XC570 - Bozrah
Worst Case Power Density Analysis of Sprint PCS Antennas @ Base of Tower. Assumes Max ERP & No Antenna Pattern Adjustment**

Operating Frequency (MHz)	Number of Trans.	Effective Radiated Power (ERP) Per Transmitter (Watts)	Total ERP (Watts)	Antenna Height (Feet)	Distance from Base of Tower (Feet)	Calculated Power Density (mW/cm ²)	Maximum Permissible Exposure*	%MPE
1962.5	11	397	4367	150	0	0.069872	1	6.9872%
1962.5	11	397	4367	150	50	0.062885	1	6.2885%
1962.5	11	397	4367	150	100	0.048373	1	4.8373%
1962.5	11	397	4367	150	150	0.034936	1	3.4936%
1962.5	11	397	4367	150	200	0.025154	1	2.5154%
1962.5	11	397	4367	150	250	0.018496	1	1.8496%
1962.5	11	397	4367	150	300	0.013974	1	1.3974%
1962.5	11	397	4367	150	350	0.010842	1	1.0842%
1962.5	11	397	4367	150	400	0.008614	1	0.8614%
1962.5	11	397	4367	150	450	0.006987	1	0.6987%
1962.5	11	397	4367	150	500	0.005769	1	0.5769%

*Requirements set forth in OET Bulletin 65. Based on NCRP Report No. 86 and ANSI/IEEE C95.1-1992



SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

Peter W. van Wilgen
Director - Real Estate Operations

November 24, 1999

RECEIVED

NOV 24 1999

**CONNECTICUT
SITING COUNCIL**

Mr. Joel M. Rinebold, Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Re. Springwich Cellular Limited Partnership – Bozrah
Cellular Communications Site – Additional Information

Dear Mr. Rinebold:

At the request of Siting Analyst Steve Levine, the following additional information is provided to supplement SCLP's November 16, 1999 amended Bozrah cell site filing.

SCLP's original filing of March 17, 1999 listed only the power density calculations for Omnipoint, Nextel and SCLP. At the time of the original filing, these were the only carriers proposed for this site. Sometime between March 17, 1999 and November 16, 1999, Sprint PCS also located on the tower. SCLP amended its original filing, but forgot to include the information for Sprint PCS. Please see the attached corrected power density table, which includes SCLP and all other existing carriers.

The height of the actual tower is 180 feet, not including the platform for Omnipoint, which is located on the top of the tower. Thus, the top of the Omnipoint antennas are at approximately 186 feet.

At the time SCLP was ready to begin construction for this site, it was discovered that a tower-guying mount had been located at the height of SCLP's proposed antenna placement. (SCLP's November 16, 1999 Amendment addressed this situation.)

Still desiring to use the existing tower, SCLP researched attaching its antennas outboard of the guying mount, however the additional width and weight of the mounting hardware and antennas placed too much wind loading and structural

strain on the tower. SCLP also investigated placing its antennas above the guying mount, however SCLP's antennas would then be located too close to those of Nextel and could cause interference to both carriers.

SCLP looked at mounting just below the guying mount, but the physical guy wires were in way of the antenna beams and would cause signal interference. Locating SCLP's antennas below the Sprint antennas at the 140 foot level reduced the coverage received from this location and made the site uneconomical and unacceptable to use.

Thus, the only other alternative was to place an antenna cluster mount at the top of the tower, bringing the total height to the top of the SCLP antennas to approximately 196 feet. The width of the mounting pipe will be 4 inches in diameter, and the amount of exposed pipe between the top of the Omnipoint antennas and the bottom of SCLP's antennas would be approximately 5 feet. The overall diameter of the proposed pipe mount, with the SCLP antennas and mounting hardware, would be approximately 34 inches. In contrast, the platform holding Omnipoint's antennas is approximately ten feet across. This addition has been approved by the Town of Bozrah.

Thank you for your cooperation and understanding in this matter.

Very truly yours,

A handwritten signature in black ink, appearing to be "Lewy", with a long, sweeping horizontal stroke extending to the right.

1. The first part of the document is a letter from the author to the editor of the journal. The letter discusses the author's interest in the journal and the author's qualifications for the position.

2. The second part of the document is a letter from the editor to the author. The editor discusses the author's qualifications and the editor's interest in the author's work.

3. The third part of the document is a letter from the author to the editor. The author discusses the author's interest in the journal and the author's qualifications for the position.

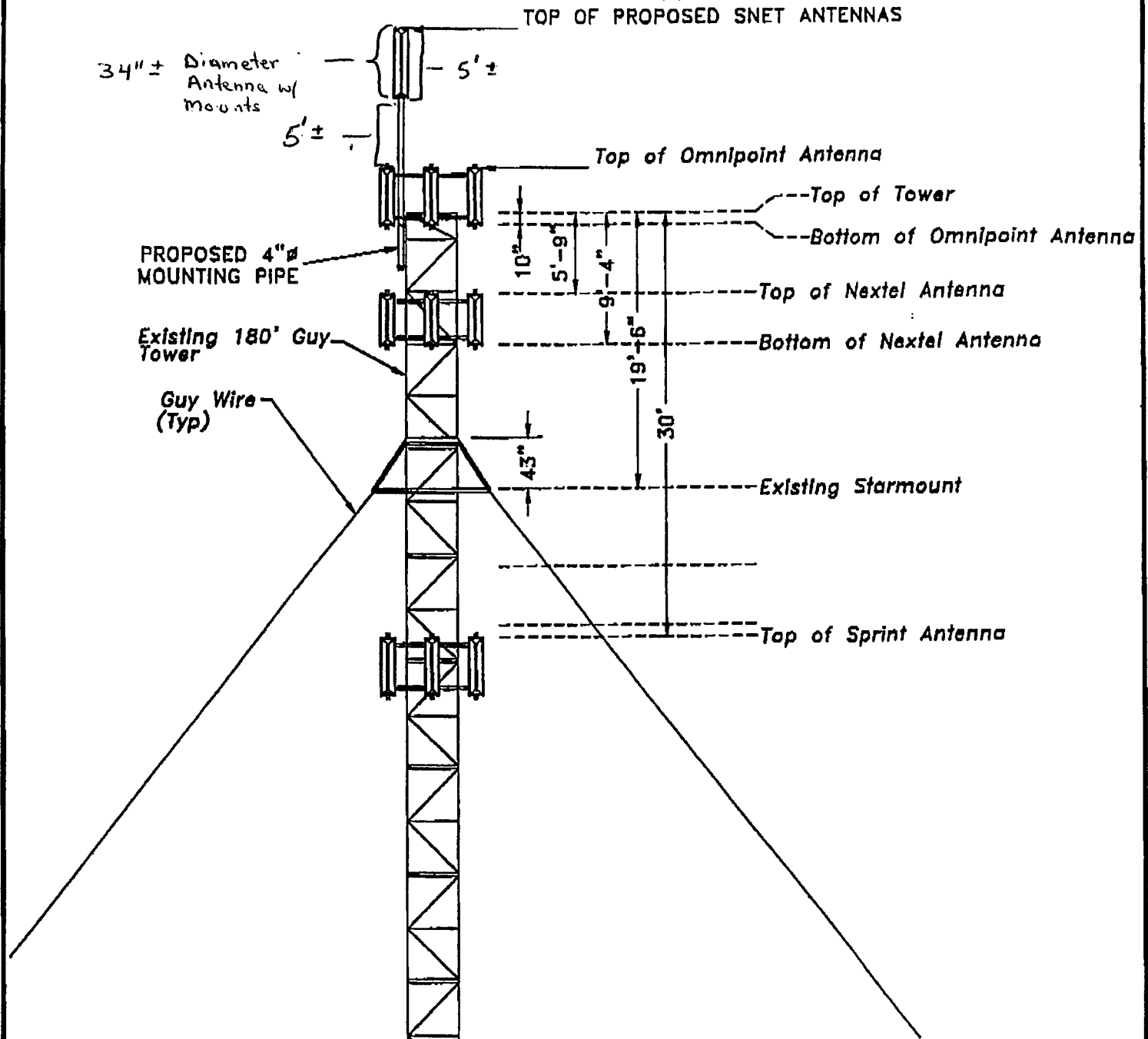
4. The fourth part of the document is a letter from the editor to the author. The editor discusses the author's qualifications and the editor's interest in the author's work.

5. The fifth part of the document is a letter from the author to the editor. The author discusses the author's interest in the journal and the author's qualifications for the position.



FREQUENCY	POWER DENSITY	HEIGHT	ANSI/IEEE STANDARD LIMITS (mW/cm2)	% OF MPE
Omnipoint 1945	.0111	181'	1.0000	1.11
SCLP 880-894	0.0290	195'	0.5867	3.32
Sprint	0.0245	147'	1.0000	2.45
Nextel 851	0.0228	175'	0.5673	4.02
TOTAL	N/A		N/A	10.90

RAD. CENTER: 194.5± FT. (AGL)

BASED ON INFORMATION PROVIDED BY ED BADON (SNET MOBILITY)

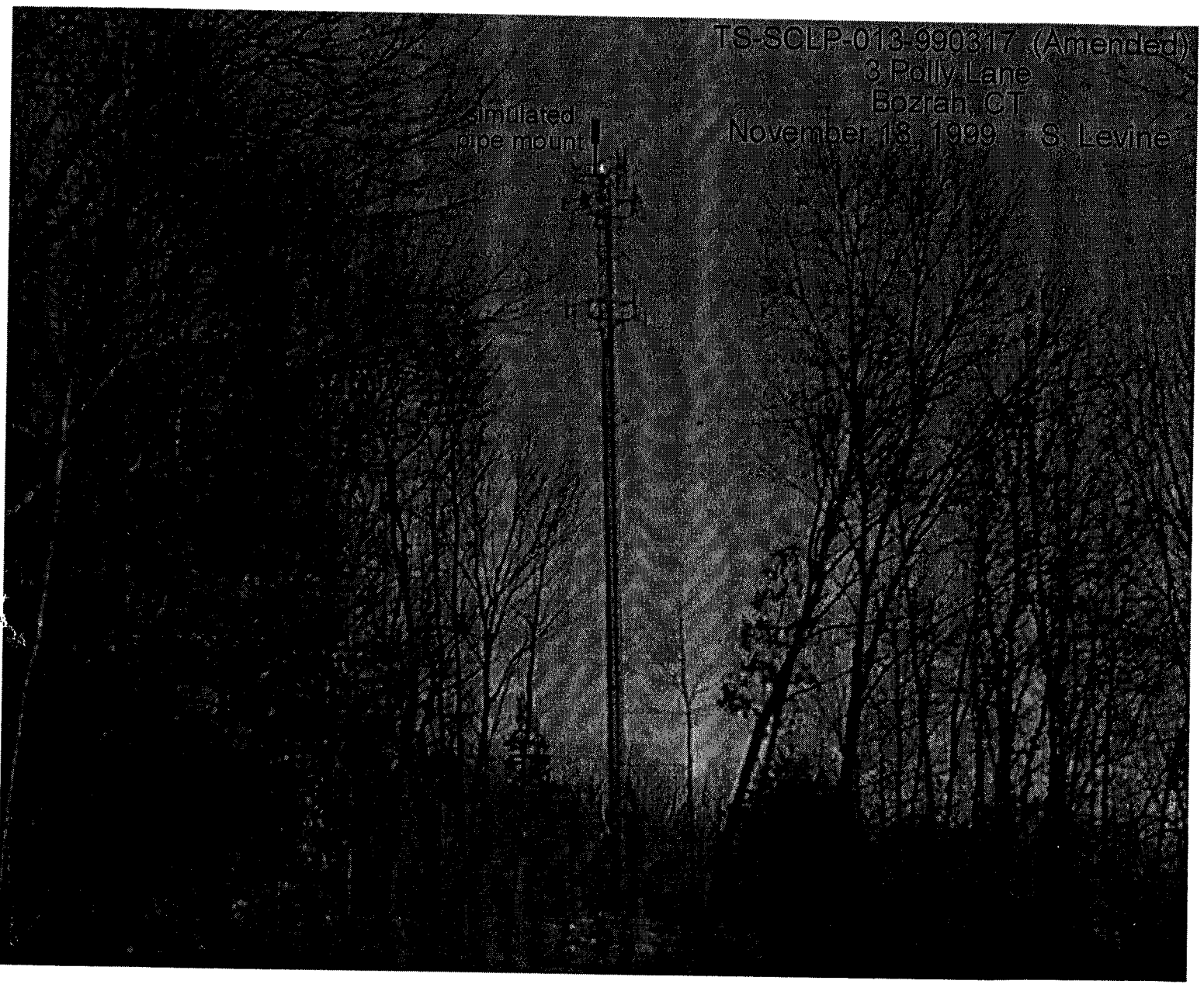


PROPOSED TOWER LAYOUT

SNET MOBILITY PRELIMINARY DESIGN EXHIBIT	NORTH	SITE NAME: CDT-BOZRAH	SNET #:
		ADDRESS: POLLY LANE BOZRAH, CT	MGI #: 14777
		DRAWN:GMP CHECKED:RGT SCALE: 1"=10'	TASK #: 2122
			DATE: 11/5/99
 Maguire Group Inc. Architects·Engineers·Planners One Court Street New Britain, Connecticut 06051	THIS DRAWING AND ALL DATA CONTAINED HEREIN IS FOR INFORMATIONAL PURPOSES ONLY. NOT INTENDED FOR DESIGN OR CONSTRUCTION USE. ALL DATA SHOULD BE VERIFIED		

TS-SCLP-013-990317 (Amended)
3 Polly Lane
Bozrah CT
November 13, 1999 S. Levine

simulated
pipe mooring





SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

November 15, 1999

Peter W. van Wilgen
Director - Real Estate Operations

RECEIVED

NOV 15 1999

CONNECTICUT
SITING COUNCIL

Mr. Mortimer A. Gelston, Chairman
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

**RE: Springwich Cellular Limited Partnership—Bozrah Cellular
Communication Site-Amended Filing**

Dear Chairman Gelston:

On April 6, 1999, Springwich Cellular Limited Partnership (SCLP) received Connecticut Siting Council (Council) approval for tower sharing at the tower facility owned by Mrs. Alice Maynard of Colchester, Connecticut, and constructed, managed, and operated by Cordless Data Transfer, Inc. (CDT) of Marlborough, Connecticut.

SCLP has discovered that, upon construction of the tower, a guyed wire brace was installed at the original level approved for SCLP's antennas, and has prevented SCLP from placing their antennas in that location.

SCLP has negotiated a new agreement with CDT to install its antennas at the top of the tower, as shown on the attached tower profile. The tower manufacturer has conducted a structural analysis and approved the new antenna location (see attached). CDT has contacted the Town of Bozrah regarding the new location of SCLP's antennas and has received a letter stating that the new location is agreeable to the Town (see letter attached).

The operation of the additional antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base, to a level at or above the ANSI standard. The following table summarizes the power densities at the site from the various sources on the tower (including SCLP's revised antenna height) in relation to the standard.

FREQUENCY	POWER DENSITY	HEIGHT	ANSI/IEEE STANDARD LIMITS (mW/cm2)	% OF MPE
Omnipoint 1945	.0111	181'	1.0000	1.11
SCLP 880-894	0.0290	195'	0.5867	3.32
Nextel 851	0.0228	175'	0.5673	4.02
TOTAL	N/A		N/A	8.45

As the table demonstrates, SCLP's proposed antennas would contribute 3.32% of the ANSI standard for the cellular frequency range, bringing the site total to 8.45% of the standard as calculated for a mixed frequency site.

SCLP submits that the proposed additions will not cause a significant change or alteration in the physical and environmental characteristics of the site and comply with R.C.S.A. Section 16-50aa. SCLP therefore requests that the Council acknowledge that the new location of the antennas and equipment on the existing tower do not constitute a substantial environmental effect under R.C.S.A. Section 16-50aa, and that the requested tower sharing be re-approved.

Thank you for your consideration.

Sincerely,



The first part of the document discusses the importance of maintaining accurate records of all transactions. It emphasizes that every entry should be supported by a valid receipt or invoice. This ensures transparency and allows for easy verification of the data.

Additionally, it is noted that regular audits are essential to identify any discrepancies or errors early on. By conducting these checks frequently, the organization can prevent small mistakes from escalating into larger financial issues.

The second section focuses on the role of technology in modern accounting. It highlights how software solutions can streamline the process, reduce manual errors, and provide real-time insights into the company's financial health.

However, it also cautions against over-reliance on technology. While tools are helpful, they cannot replace the critical thinking and attention to detail provided by a skilled accountant.

In conclusion, the document stresses that a combination of diligent record-keeping, regular audits, and the effective use of technology is the key to successful financial management.

The final part of the document provides a summary of the key points discussed. It reiterates the importance of accuracy, transparency, and the integration of technology into the accounting process.

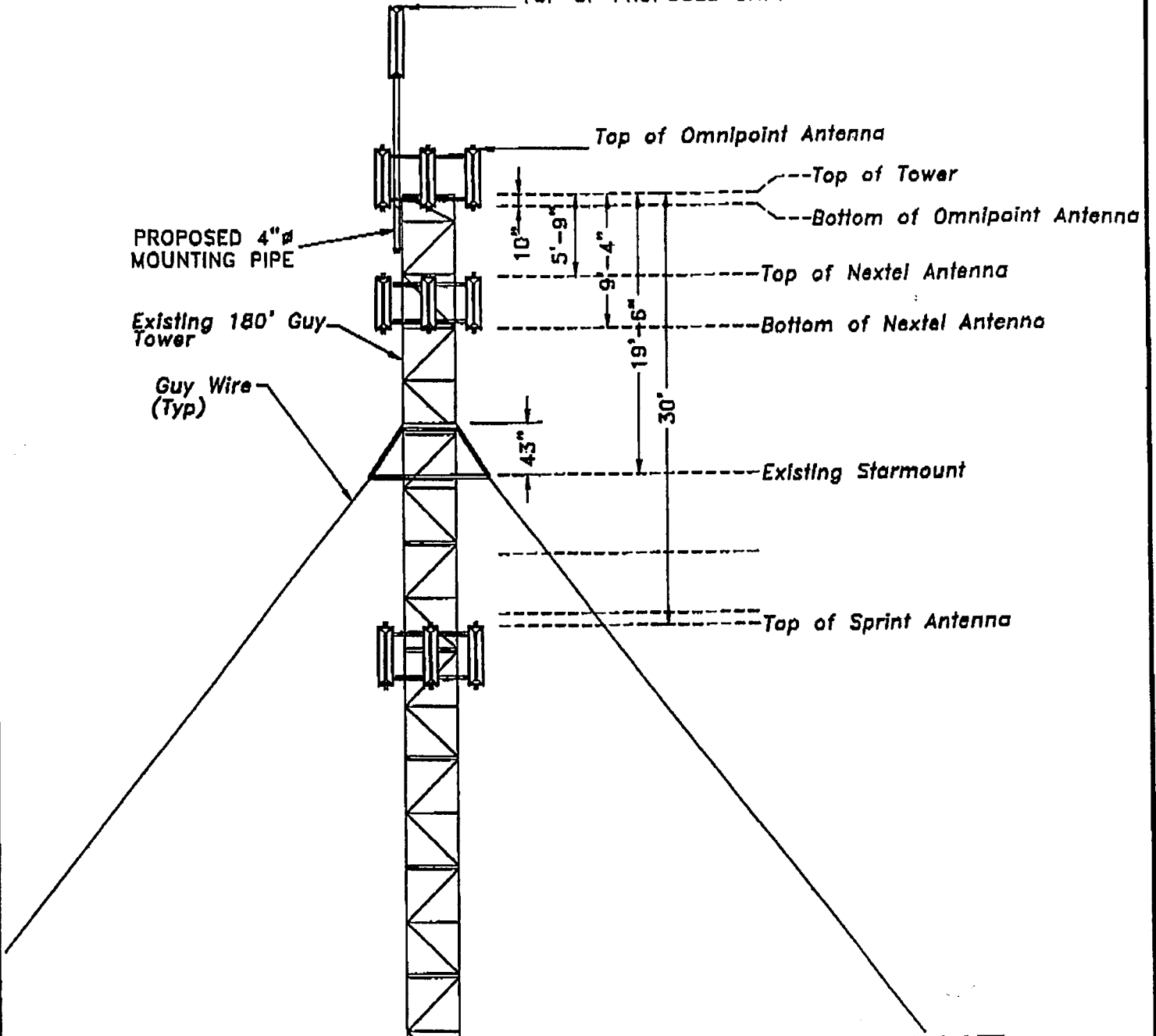
It also offers some practical advice for businesses looking to improve their financial reporting, such as implementing standardized procedures and investing in quality accounting software.

The document is signed by the author, who is a professional accountant with over 10 years of experience in the field.

RAD. CENTER: 194.5± FT. (AGL)

BASED ON INFORMATION PROVIDED
BY ED BADON (SNET MOBILITY)

TOP OF PROPOSED SNET ANTENNAS



PROPOSED TOWER LAYOUT

SNET MOBILITY
PRELIMINARY
DESIGN EXHIBIT

NORTH

SITE NAME: CDT-BOZRAH

ADDRESS: POLLY LANE
BOZRAH, CT

SNET #:

MGI #: 14777

TASK #: 2122

DATE: 11/5/99

DRAWN: GMP

CHECKED: RGT

SCALE: 1"=10'



Maguire Group Inc.
Architects-Engineers-Planners
One Court Street
New Britain, Connecticut 06051

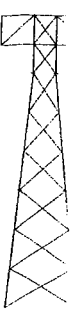
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OR CONSTRUCTION USE. ALL DATA SHOULD BE VERIFIED





FRED A. NUDD CORPORATION

1743 ROUTE 104, BOX 577
ONTARIO, NY 14519
(315) 524 -2531 FAX (315) 524-4249
www.nuddtowers.com



October 12, 1999

Ken Lee
SNET MOBILITY
500 Enterprise Dr., 3rd Floor
Rocky Hill, CT 06067

Ken,

We have completed the analysis of the CDT – Bozrah tower and have found it adequate within the scope of this analysis to support the proposed antenna loading. The analysis was performed using 85 mph wind speed with 1/2" radial ice per EIA/TIA 222-F recommended standard.

The tower we analyzed is a 185' Nudd G42WPAR guyed supporting tower consisting of pipe legs and angle/rod bracing. Tower sections are all-welded with a face dimension of 42". Foundation capacities were predicated on original design criteria.

The antenna loading used in the analysis consisted of the existing antennas as well as the following antenna configuration:

QTY	Antenna	Elev.	T-Line	Status
3	EMS RS90-10	192	(9) 1-1/4" Heliax	SNET Proposed

The results of the analysis showed all tower and foundation elements to be loaded within acceptable limits. Note that the antenna mounting pipe to be used is 4" Sch.40 pipe.

If you have any questions concerning this analysis, please contact me.

Sincerely,

FRED A. NUDD CORPORATION

Patrick Botimer
Engineer

OFFICE OF THE FIRST SELECTMAN
TOWN OF BOZRAH
TOWN HALL
1 RIVER ROAD
BOZRAH, CONN. 06334

OCTOBER 22, 1999

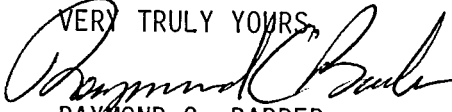
TO WHOM IT MAY CONCERN:

PLEASE BE ADVISED THAT THE TOWN OF BOZRAH HAS BEEN INFORMED THAT
A NEW ANTENNA WILL BE INSTALLED ON THE TOWER ON POLLY LANE.

THIS ANTENNA, WHICH WILL BE INSTALLED BY SNET WIRELESS, WILL
BRING THE TOTAL HEIGHT OF THIS TOWER TO 196 FEET.

THE TOWN OF BOZRAH HAS NO PROBLEM WITH THIS NEW HEIGHT.

RCB:kg

VERY TRULY YOURS,

RAYMOND C. BARBER
FIRST SELECTMAN
TOWN OF BOZRAH



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

April 7, 1999

Peter van Wilgen
SNET Mobility Inc.
500 Enterprise Drive
Rocky Hill, CT 06067-3900

RE: **TS-SCLP-013-990317** - Springwich Cellular Limited Partnership request for an order to approve tower sharing at an existing telecommunications facility located off 3 Polly Lane in Bozrah, Connecticut.

Dear Mr. van Wilgen:

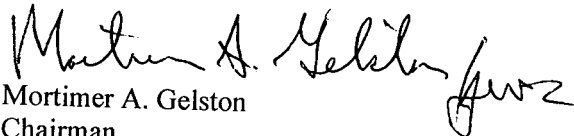
At a public meeting held April 6, 1999, the Connecticut Siting Council (Council) ruled that the shared use of this existing tower site is technically, legally, environmentally, and economically feasible and meets public safety concerns, and therefore, in compliance with General Statutes § 16-50aa, the Council has ordered the shared use of this facility to avoid the unnecessary proliferation of tower structures.

This facility has been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequency now used on this tower. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

This decision applies only to this request for tower sharing and is not applicable to any other request or construction.

The proposed shared use is to be implemented as specified in your letter dated March 17, 1999, and additional information provided on April 6, 1999. Please notify the Council when all work is complete.

Very truly yours,


Mortimer A. Gelston
Chairman

MAG/RKE/kj

c: Honorable Raymond Barber, First Selectman, Town of Bozrah

RECEIVED

APR - 6 1999

CONNECTICUT
SITING COUNCIL

Design of
180' Guyed Tower

MODEL #: G42WPAR

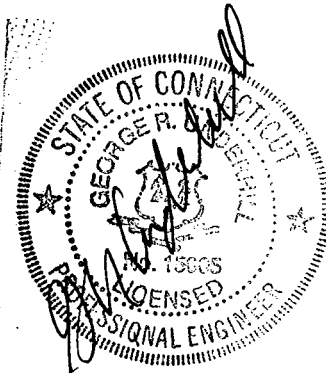
PROJECT #: 5463

LOCATED IN: Bozrah, **CT**

for

CDT
PO BOX 363
Marlborough, CT 06447

November, 1997



TOWER DESIGN CONDITIONS
 Tower was designed to resist 85 mph wind speed with 1/2" radial ice per AWS/SEI/ATL 22E recommended standard. Worst case load condition is wind from East. All allowable steel stresses per AISC ASD 9th Edition. All allowable concrete stresses per ACI 318-88.

MATERIAL SPECIFICATIONS
 Tower Legs: ASTM A36 Modified, Fy > XX ksi. See Section Schedule.
 Guy Anchors: ASTM A36 Modified, Fy > XX ksi
 All other steel: ASTM A36, Fy > 36 ksi
 Guy Cable: Extra High Strength Grade
 Hardware: A325 Nut and Nuts
 Galvanizing: ASTM A123

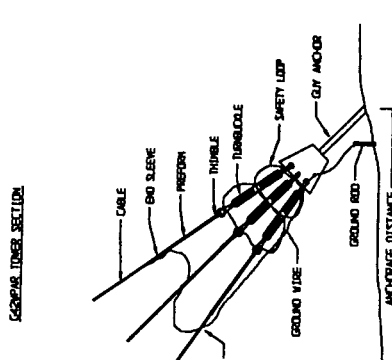
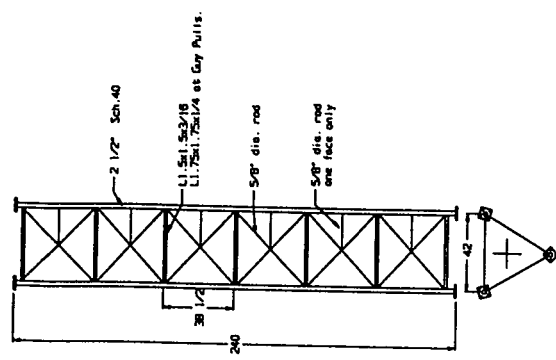
TOWER LOADING CONDITIONS

QTY	Member	Elevation	Windload	Deadload
1	12' Cellular Boom	170	252	170
9	Structural SRL 411CSR130	170	90	90
10	PD 10017	170	243	175
3	12' Cellular Boom	170	243	175
9	ALP 8212	170	124	77
3	12' Cellular Boom	160	283	170
9	Structural SRL 411CSR130	160	300	180
3	12' Cellular Boom	150	278	170
9	ALP 8212	150	119	27
1	8" HP Dish	140	837	814
1	6" HP Dish	130	837	814
1	6" HP Dish	120	837	814
1	G42 Torque Arm	170	537	282
1	G42 Torque Arm	150	486	262

QTY	Type	Start Elevation	Stop Elevation	Windload	Deadload
19	LPF-50A 1-5/8"	0	180	0.00	2.40
9	LPF-50A 1-5/8"	0	170	0.00	2.40
9	LPF-50A 1-5/8"	0	160	0.00	2.40
9	LPF-50A 1-5/8"	0	150	0.00	2.40
1	LPF-50A 1-5/8"	0	140	0.00	2.40
1	LPF-50A 1-5/8"	0	130	0.00	2.40
1	LPF-50A 1-5/8"	0	120	0.00	2.40
1	Tower Span 1	0	60	195.00	51.90
1	Tower Span 2	60	120	207.00	51.90
1	Tower Span 3	120	180	239.00	51.90

NOTE: Any deviation from the proposed design antenna loading will require a tower analysis for verification of structural integrity.

Initial Installation:
 Tower: Full Height-Partial Sections?
 Antenna: 3-48'

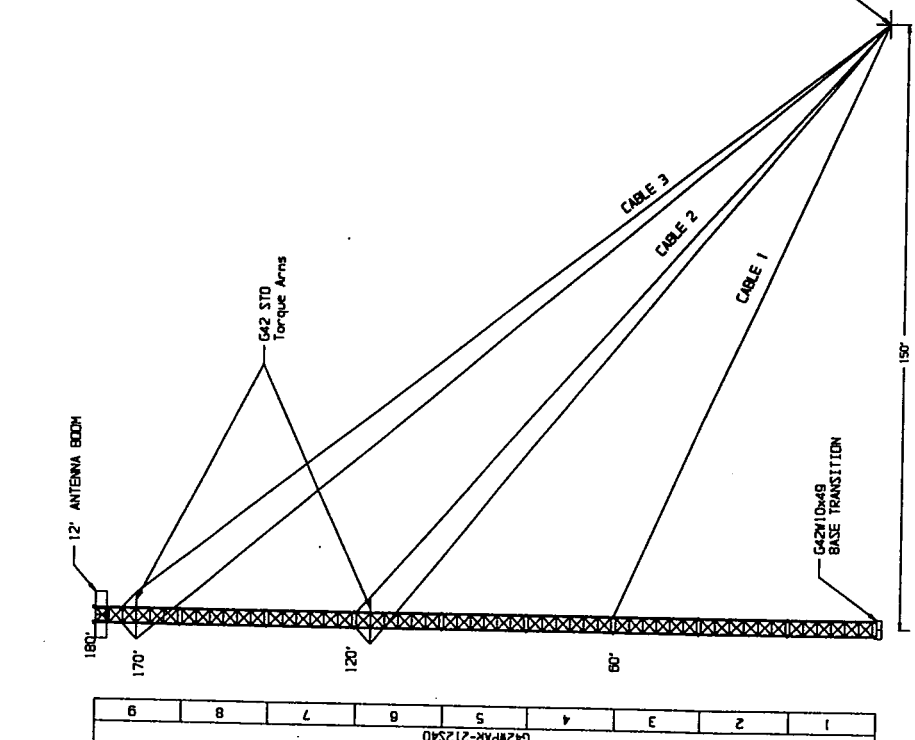


CABLE HARDWARE ASSEMBLY
NOTE: Install cable hardware per manufacturer's specifications.

GUY CABLE SCHEDULE

Cable #	Qty	City/Town	Length	Ti	Turnbuckle	Preform	Endsize Sock
1	2	5/8" J-BUS	270	4200	5/8" J-J	5/8" BG	3/4"
2	2	5/8" J-BUS	180	3500	5/8" J-J	5/8" BG	3/4"
3	2	5/8" J-BUS	157	3500	5/8" J-J	5/8" BG	3/4"

NOTE: Cable lengths assume anchors at elevation of 0'. Cable lengths and anchor layout must compensate for site topography.

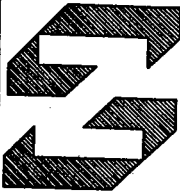


INSTALLATION NOTES

1. Installation of tower must be performed by a qualified tower erector.
2. Install sections with section number on the bottom, and climbing device is aligned.
3. Install safety climb, lights, cable attachments per manufacturer's recommendations.
4. Do not lift more than 100' of assembled tower sections.
5. Install "sharp" edge of adapter plates against face of tower.
6. Tension and tension tower and cables as erected.
7. "1" initial tension of cable.

G42 Section Weights: 785/865 1/2"
 Top Frame: 1000 1/2"

SECTION DESIGNATION:
 G42PAR-2125S = 2-1/2" x (212), (S)Sch. 40 (EH)Sch. 80, (55 Msi strength)
 96-47-xx = Year-(47) ksi strength-xx



FRED A. NUDD CORPORATION
 Route 104-Ontario, New York 14518-315-2531

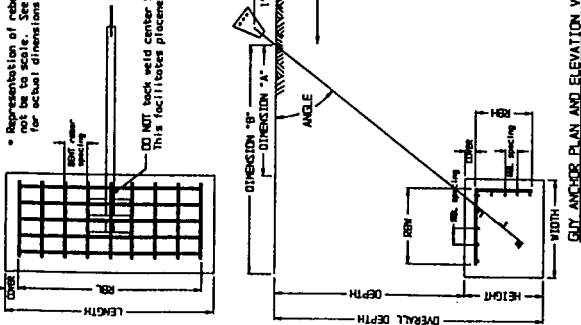
SCALE: N/S
 DATE: 11/03/97
ELP

180' G42PAR TOWER

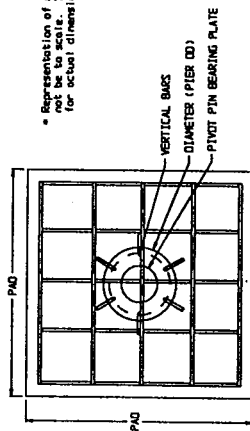
DESIGNED BY: [Signature]
 CHECKED BY: [Signature]
 DRAWN BY: [Signature]

COT BOZRAH, CT 97-5463-1

* Representation of rebar placement may not be to scale. See General Schedule for actual dimensions and sizes.



GUY ANCHOR PLAN AND ELEVATION VIEWS



* Representation of rebar placement may not be to scale. See Footing Specifications for actual dimensions and sizes.

PIER SPECIFICATIONS

- Diameter: 2'-0"
- Depth: 3'-0"
- Height: 4'-0"
- Thickness: 1'-0"
- Pier Tie Bars: 4 # 10, 5'-0", 18" DIA., 5/16" cut length
- Vertical Bars: 8 # 5 @ 22" DIA., 9" bent leg.
- Mat Bars: 4 # 6 bars, 54" DIA., 13.50" spacing
- 5 bars crossed each way.

DESIGN LOADS

- Deadload: 22.0 cu. yd.
- Live Load: 118 kip
- Shear: 3,002 kip

PAO & PIER PLAN & ELEVATION VIEW

This guy anchor foundation conforms to AWS/EIA 22-E recommended Standard.

INNER GUY ANCHOR

- Guy Anchor ID: GAG-115-15
- Bar Dimensions: 1 @ 1.75" HR F_y=8000
- Vertical: 54.9 kip
- Horizontal: 61.1 kip
- Shear: 61.1 kip
- Surface Area: 2.13
- Anchor Dimensions: 145 ft
- Length: 1'-0"
- Width: 1'-0"
- Depth: 6'-0"
- Vertical Dimension: 6'-0"
- Horizontal Dimension: 12'-3"
- Angle: 41.9°

- Long Rebar BBL: 121°
- BBL Vert. Spacing: 4"
- BBL Hor. Spacing: 7"
- Bent Rebar BBL: 12°
- Bent Rebar BBL: 59°
- Bent Rebar Spacing: 11"
- Rebar Size: #4 Bar

Concrete Volume: 3 @ 4.7 cu yds

Total Concrete: 14.1 cu yds

NOTE: *Install the extra one long rebar inside the bottom chord of the guy anchor.

*Field size the anchor bent rebar.

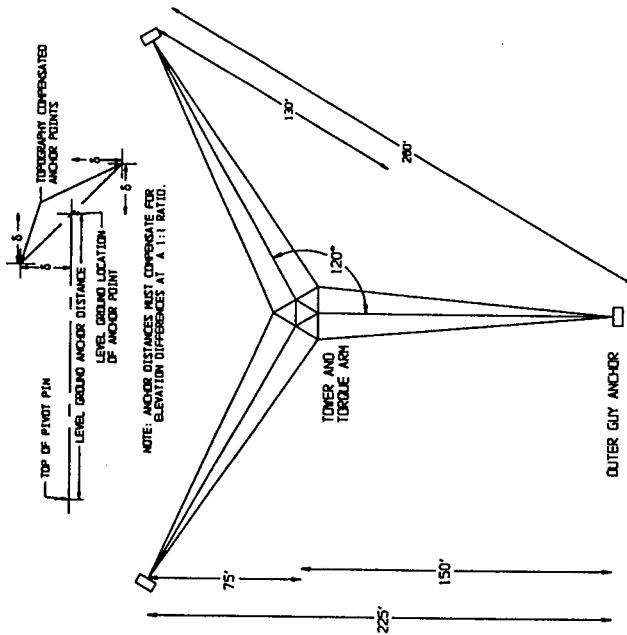
*Rebar QTY's for one anchor only.

CONCRETE SPECIFICATIONS

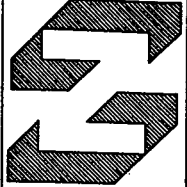
- Concrete shall have a minimum compressive strength of at least 3000 psi at 28 days. It is our recommendation that 4000 psi concrete be used for this application. The concrete mix design shall be submitted for approval. Concrete placement variables that could degrade the concrete. Concrete installation shall meet ACI 318-89 installation requirements for reinforced concrete.
- All concrete shall be placed against undisturbed soil free of water and oil.
- Reinforcing bars shall be 3" over all main objects and materials.
- Reinforcing bars shall be ASTM A-615 Grade 60.
- Reinforcing bars shall be ASTM A-615 Grade 60.
- Assemble bars with tie wires or weld. Welding of bars must conform to AWS/AWS D1.4-DQ specifications. Structural weld splices on bars must be inspected by a qualified welder.
- Chamfer all sharp corners of exposed concrete.

SOIL SPECIFICATIONS

- Soil to be per boring logs by XXXX dated XXXXX.
- Per customer specification soil is assumed to be XXXX.
- All foundation soil shall be free of free standing water as far as possible prior to pouring concrete and shall be kept thus until bearing capacity is established.
- Backfill shall be compacted to 100% in 6" lifts using excavated material.
- Backfill shall be placed so as to prevent accumulation of water around foundations or anchors.



TOWER PLOT PLAN AND ANCHOR LAYOUT



FRED A. NUDD CORPORATION
Route 104-Danbar, New York 14518-3154-2531

Scale: N/S
Date: 11/03/97
EJR

FOUNDATION DETAILS

Project No: 97-5463-2
City: Danbar, CT

11-18-1997
 16:55:27
 CDT
 Bozrah, NY
 5463

Guy Cable Data		ft, lb			Wind	Total	Cable
	Elev	Horiz	Length	Angle	Length	Length	Type
Cable 3 :	170	145	224	49.70	1189	1345	EHS
Cable 2 :	120	145	189	39.84	938	1133	EHS
Cable 1 :	60	145	157	22.81	339	472	EHS

Cable Loads		-lb		Cable Size	%Loaded
	Shear	Download	Cable Load		
Cable 3 :	23979	32654	42813	2 - 5/8x7	100.97
Cable 2 :	17133	16509	25766	2 - 9/16x7	73.62
Cable 1 :	11798	5731	14779	1 - 9/16x7	84.45

Cable Safety Factor: 2
 Shear at 0': 3602 lb
 Shear on Guy Anchors: 351 lb

Accumulated Down Loads	
Elevation	Down load (lb)
170.0	49138
145.0	55546
120.0	87542
90.0	93703
60.0	107550
30.0	112635
0.0	117720

Guy Anchor Reactions

Vertical Reaction: 54894 lbs
 Horizontal Reaction: 61095 lbs
 Resultant: 82134 lbs
 Angle: 41.93 Degrees

Tower Plot Dimensions

A= 217.5 ft
 B= 145 ft
 C= 72.5 ft
 D= 251.2 ft
 E= 125.58 ft

MOMENT DISTRIBUTION OUTPUT - boz

Beam Configuration:

4 Spans		3 Beams			dfB	dfT
SPAN	FEMB	FEMT	VB	VT		
1	-46500	46500	4650	4650	1.0000	0.5000
2	-62100	62100	6210	7533	0.5000	0.4545
3	-77160	96212	8763	13551	0.5455	1.0000
4	-71396	0	9217	0	0.0000	0.0000

10 Iterations

SPAN #	DISTRIBUTED MOMENTS (ft-lb)			SHEARS (lb)	REACTIONS (lb)
	MOM B	MOM T	VB	VT	
1	0	62855	3602	5697	3602
2	-62856	74379	6017	7725	11715
3	-74380	71395	8823	13492	16548
4	-71396	0	9217	0	22709
					0

Eleva- tion	Moment	Accum. Download	Resolved Legload	Leg Capacity	% Loaded
0	0	102558	34186	74828	45.7
1	3525	102388	35137	74828	47.0
2	6895	102219	36043	74828	48.2
3	10110	102049	36905	74828	49.3
4	13170	101880	37723	74828	50.4
5	16075	101710	38496	74828	51.4
6	18824	101541	39225	74828	52.4
7	21419	101371	39910	74828	53.3
8	23859	101202	40551	74828	54.2
9	26144	101032	41147	74828	55.0
10	28274	100863	41699	74828	55.7
11	30249	100693	42207	74828	56.4
12	32069	100524	42670	74828	57.0
13	33734	100354	43090	74828	57.6
14	35244	100185	43465	74828	58.1
15	36599	100015	43795	74828	58.5
16	37799	99846	44082	74828	58.9
17	38844	99676	44324	74828	59.2
18	39733	99507	44521	74828	59.5
19	40468	99337	44675	74828	59.7
20	41048	99168	44784	74828	59.8
21	41473	98998	44849	74828	59.9
22	41743	98829	44870	74828	60.0
23	41858	98659	44846	74828	59.9
24	41818	98490	44778	74828	59.8
25	41623	98320	44666	74828	59.7
26	41273	98151	44509	74828	59.5
27	40768	97981	44308	74828	59.2
28	40108	97812	44063	74828	58.9
29	39293	97642	43774	74828	58.5
30	38322	97473	43440	74828	58.1
31	37197	97303	43062	74828	57.5
32	35917	97134	42640	74828	57.0
33	34482	96964	42173	74828	56.4
34	32892	96795	41663	74828	55.7
35	31147	96625	41108	74828	54.9
36	29247	96456	40508	74828	54.1
37	27192	96286	39865	74828	53.3
38	24982	96117	39177	74828	52.4
39	22617	95947	38444	74828	51.4
40	20097	95778	37668	74828	50.3
41	17421	95608	36847	74828	49.2
42	14591	95439	35982	74828	48.1
43	11606	95269	35073	74828	46.9
44	8466	95100	34119	74828	45.6
45	5171	94930	33121	74828	44.3
46	1721	94761	32079	74828	42.9
47	-1884	94591	32069	74828	42.9
48	-5644	94422	33087	74828	44.2
49	-9559	94252	34149	74828	45.6

Elevation	Moment	Accum. Download	Resolved Legload	Leg Capacity	% Loaded
50	-13629	94083	35255	74828	47.1
51	-17854	93913	36406	74828	48.7
52	-22234	93744	37601	74828	50.2
53	-26770	93574	38840	74828	51.9
54	-31460	93405	40123	74828	53.6
55	-36305	93235	41451	74828	55.4
56	-41305	93066	42823	74828	57.2
57	-46460	92896	44240	74828	59.1
58	-51770	92727	45700	74828	61.1
59	-57235	92557	47205	74828	63.1
60	-62855	92388	48755	74828	65.2
61	-56941	92098	46968	74828	62.8
62	-51233	91929	45281	74828	60.5
63	-45733	91759	43653	74828	58.3
64	-40439	91590	42084	74828	56.2
65	-35353	91420	40574	74828	54.2
66	-30474	91251	39124	74828	52.3
67	-25801	91081	37732	74828	50.4
68	-21336	90912	36400	74828	48.6
69	-17077	90742	35127	74828	46.9
70	-13026	90573	33913	74828	45.3
71	-9181	90403	32758	74828	43.8
72	-5544	90234	31662	74828	42.3
73	-2114	90064	30625	74828	40.9
74	1110	89895	30282	74828	40.5
75	4126	89725	31087	74828	41.5
76	6936	89556	31834	74828	42.5
77	9538	89386	32521	74828	43.5
78	11934	89217	33149	74828	44.3
79	14122	89047	33717	74828	45.1
80	16103	88878	34227	74828	45.7
81	17878	88708	34677	74828	46.3
82	19445	88539	35069	74828	46.9
83	20806	88369	35401	74828	47.3
84	21959	88200	35674	74828	47.7
85	22906	88030	35888	74828	48.0
86	23645	87861	36043	74828	48.2
87	24177	87691	36138	74828	48.3
88	24503	87522	36175	74828	48.3
89	24621	87352	36152	74828	48.3
90	24533	87183	36070	74828	48.2
91	24237	87013	35929	74828	48.0
92	23734	86844	35729	74828	47.7
93	23025	86674	35470	74828	47.4
94	22108	86505	35152	74828	47.0
95	20985	86335	34774	74828	46.5
96	19654	86166	34337	74828	45.9
97	18117	85996	33842	74828	45.2
98	16372	85827	33287	74828	44.5
99	14420	85657	32673	74828	43.7

Eleva- tion	Moment	Accum. Download	Resolved Legload	Leg Capacity	% Loaded
100	12262	85488	31999	74828	42.8
101	9896	85318	31267	74828	41.8
102	7324	85149	30475	74828	40.7
103	4544	84979	29625	74828	39.6
104	1558	84810	28715	74828	38.4
105	-1636	84640	28681	74828	38.3
106	-5037	84471	29596	74828	39.6
107	-8644	84301	30570	74828	40.9
108	-12459	84132	31604	74828	42.2
109	-16480	83962	32696	74828	43.7
110	-20709	83793	33848	74828	45.2
111	-25144	83623	35059	74828	46.9
112	-29787	83454	36329	74828	48.5
113	-34637	83284	37658	74828	50.3
114	-39693	83115	39046	74828	52.2
115	-44957	82945	40493	74828	54.1
116	-50427	82776	42000	74828	56.1
117	-56105	82606	43565	74828	58.2
118	-61989	82437	45190	74828	60.4
119	-68081	82267	46874	74828	62.6
120	-74380	82098	48617	74828	65.0
121	-80676	8201	34831	74828	46.5
122	-57211	48034	32357	74828	43.2
123	-48986	47866	29951	74828	40.0
124	-40999	47699	27614	74828	36.9
125	-33251	47532	25344	74828	33.9
126	-25742	47365	23143	74828	30.9
127	-18473	47198	21011	74828	28.1
128	-11442	47031	18946	74828	25.3
129	-4650	46864	16950	74828	22.7
130	1902	46697	16109	74828	21.5
131	7379	45718	17348	74828	23.2
132	12617	45553	18789	74828	25.1
133	17616	45389	20163	74828	26.9
134	22376	45224	21468	74828	28.7
135	26897	45059	22705	74828	30.3
136	31179	44895	23873	74828	31.9
137	35222	44730	24973	74828	33.4
138	39026	44565	26005	74828	34.8
139	42591	44400	26969	74828	36.0
140	45917	44236	27864	74828	37.2
141	48167	43259	28182	74828	37.7
142	50178	43097	28702	74828	38.4
143	51950	42935	29155	74828	39.0
144	53484	42773	29539	74828	39.5
145	54778	42610	29854	74828	39.9
146	55833	42448	30102	74828	40.2
147	56649	42286	30281	74828	40.5
148	57226	42123	30392	74828	40.6
149	57565	41961	30434	74828	40.7

Eleva- tion	Moment	Accum. Download	Resolved Legload	Leg Capacity	% Loaded
150	57664	41799	30408	74828	40.6
151	55617	40905	29525	74828	39.5
152	53331	40764	28825	74828	38.5
153	50806	40624	28057	74828	37.5
154	48042	40483	27220	74828	36.4
155	45039	40342	26316	74828	35.2
156	41797	40201	25342	74828	33.9
157	38315	40061	24301	74828	32.5
158	34595	39920	23191	74828	31.0
159	30636	39779	22013	74828	29.4
160	26438	39639	20767	74828	27.8
161	17730	38290	17829	74828	23.8
162	8784	38170	15233	74828	20.4
163	-402	38051	12799	74828	17.1
164	-9827	37932	15452	74828	20.6
165	-19491	37813	18173	74828	24.3
166	-29394	37694	20963	74828	28.0
167	-39536	37575	23821	74828	31.8
168	-49917	37456	26747	74828	35.7
169	-60536	37337	29742	74828	39.7
170	-71395	37218	32805	74828	43.8
171	-62297	2357	18585	74828	24.8
172	-53439	2260	16022	74828	21.4
173	-44819	2162	13526	74828	18.1
174	-36438	2065	11099	74828	14.8
175	-28296	1967	8740	74828	11.7
176	-20393	1870	6450	74828	8.6
177	-12729	1772	4228	74828	5.6
178	-5304	1675	2074	74828	2.8
179	-2533	347	839	74828	1.1
180	0	250	83	74828	0.1

$i := 0, \text{step}.. M_{\text{last}}(M < 0 >), 0$

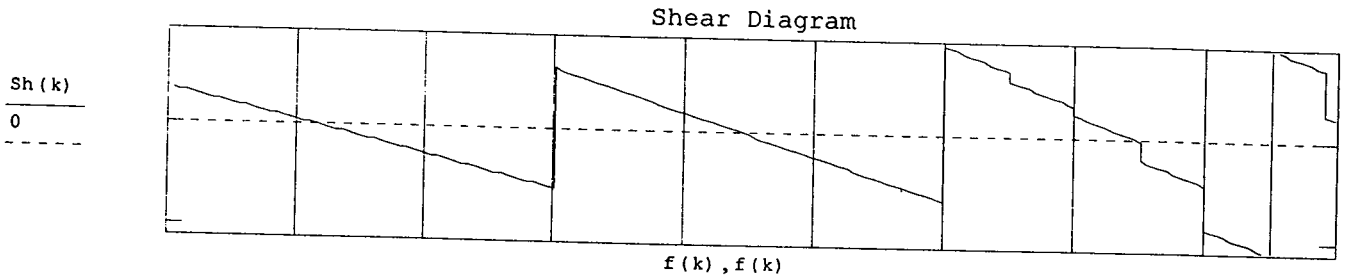
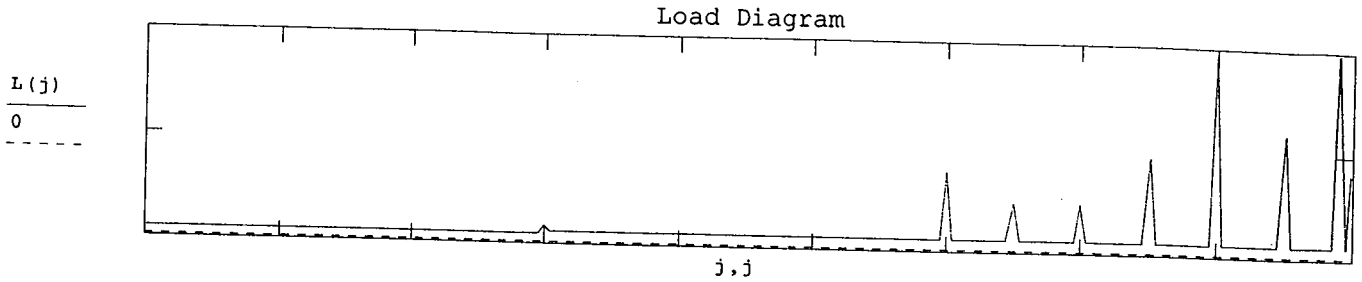
$j := 0, 1.. L_{\text{last}}(L < 0 >), 0$

Maximum_Download := 117720

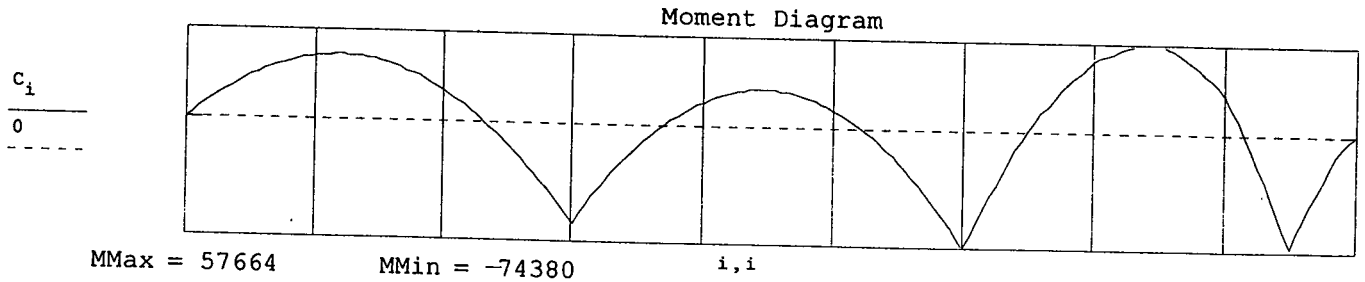
Maximum_Load = 4653.2

Lmax := Maximum_Load

Top := 180 ft High

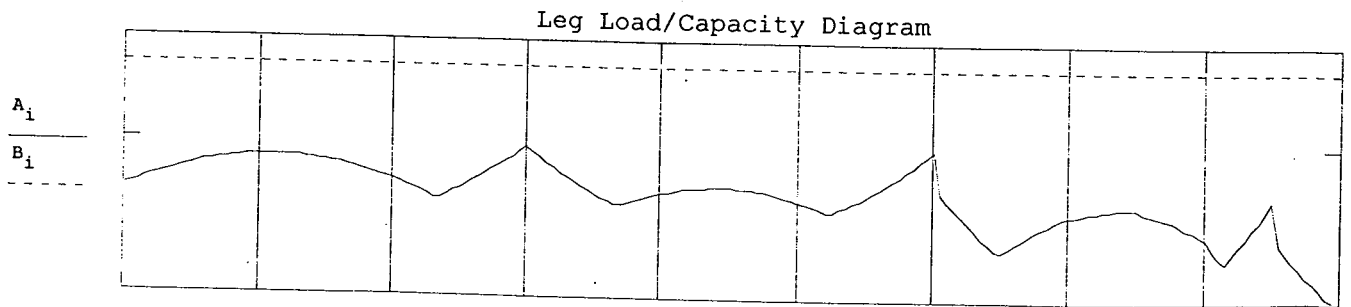


SMax = 9217.4 SMin = -10978.4



MMax = 57664

MMin = -74380



A_i =Leg Load
 B_i =Leg Capacity
 C_i =Moment

Elevation=60
 Moment = -62855

Leg_Load = 48755
 Leg_Capacity = 74828

Percent_Loaded = 65.2 %

Check Girts at Guy Pulls:

Tensile capacity of (1) L1.75x1.75x1/4:

$$\text{Area} := [1.75^2 - (1.75 - .25)^2 - .375 \cdot .25] \cdot \text{in}^2$$

$$\text{Capacity} := .6 \cdot F_{y_{\text{girt}}} \cdot \frac{4}{3} \cdot \text{Area} \cdot 1 \cdot \text{bars}$$

Maximum Single cable shear is 11798 lb,
resolved into each brace.

$$\text{Percent_Loaded}_2 := \frac{11798 \cdot \text{lb}f}{2 \cdot \text{girt} \cdot \cos(30 \cdot \text{deg}) \cdot \text{Capacity}}$$

Steel Properties:

$$E := 29 \cdot 10^6 \cdot \text{psi}$$

$$F_{y_{\text{girt}}} := 45000 \cdot \text{psi}$$

$$F_{y_{\text{diag}}} := 45000 \cdot \text{psi}$$

$$\text{Capacity} = 25875 \cdot \text{lb}f$$

$$\text{Percent_Loaded}_2 = 26.3\%$$

Check compression capacity of girts against maximum shear:

$$l := (42 - 2.875) \cdot \text{in} \quad \text{Area} := [1.5^2 - (1.5 - .1875)^2] \cdot \text{in}^2$$

$$r := .293 \cdot \text{in} \quad \text{L1.5x1.5x.1875"} \quad \text{Area} = 0.527 \cdot \text{in}^2$$

$$K := .70 \quad \text{All welded}$$

$$klr := \frac{K \cdot l}{r}$$

$$C_c := \sqrt{\frac{2 \cdot \pi^2 \cdot E}{F_{y_{\text{girt}}}}}$$

$$klr = 93.5$$

$$C_c = 112.8$$

$$F_a := \frac{\left[1 - \frac{\left(\frac{klr}{C_c}\right)^2}{2}\right] \cdot F_{y_{\text{girt}}}}{\frac{5}{3} + \frac{3}{8} \cdot \frac{klr}{C_c} - \left(\frac{klr}{2 \cdot C_c}\right)^3} \cdot (klr < C_c) + \frac{12 \cdot \pi^2 \cdot E}{23 \cdot klr^2} \cdot (klr \geq C_c)$$

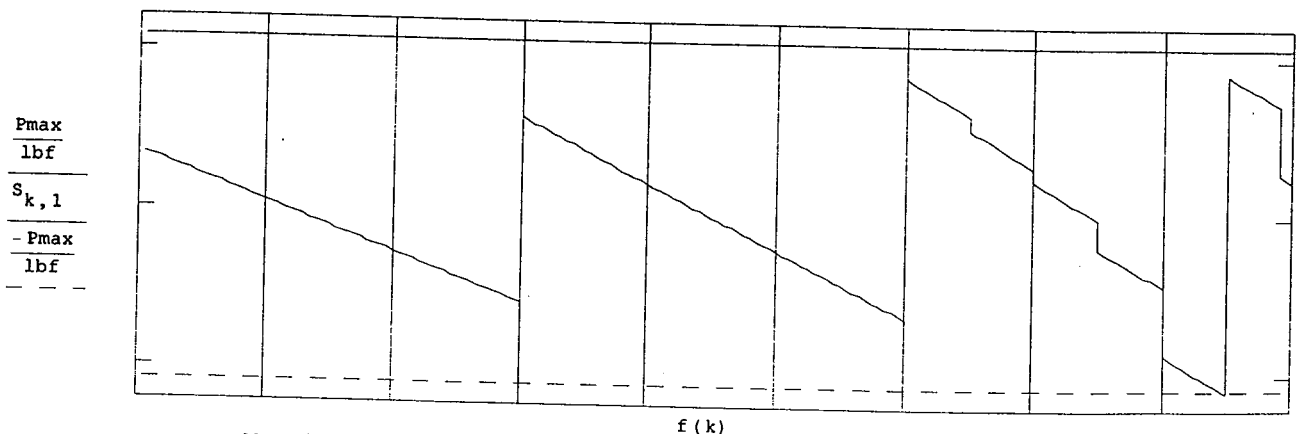
$$F_a = 15499.2 \cdot \text{psi}$$

Maximum allowable compression load:

$$P_{\text{max}} := F_a \cdot \frac{4}{3} \cdot \text{Area}$$

$$P_{\text{max}} = 10897.9 \cdot \text{lb}f$$

$$\text{MaxShear} = 10978.4$$



$$\text{Percent_Loaded}_3 := \frac{\text{MaxShear}}{P_{\text{max}}} \cdot \text{lb}f$$

$$\text{Percent_Loaded}_3 = 100.7\%$$

Check tension capacity of diagonals:

$$P_{max} := \frac{\pi}{4} \cdot \left(\frac{5}{8} \cdot \text{in}\right)^2 \cdot .6 \cdot F_{Y_{diag}} \cdot \frac{4}{3}$$

$$S(k) := \frac{Sh(k)}{2 \cdot \text{braces} \cdot \cos(45 \cdot \text{deg})}$$

$$P_{max} = 11044.7 \cdot \text{lbf}$$

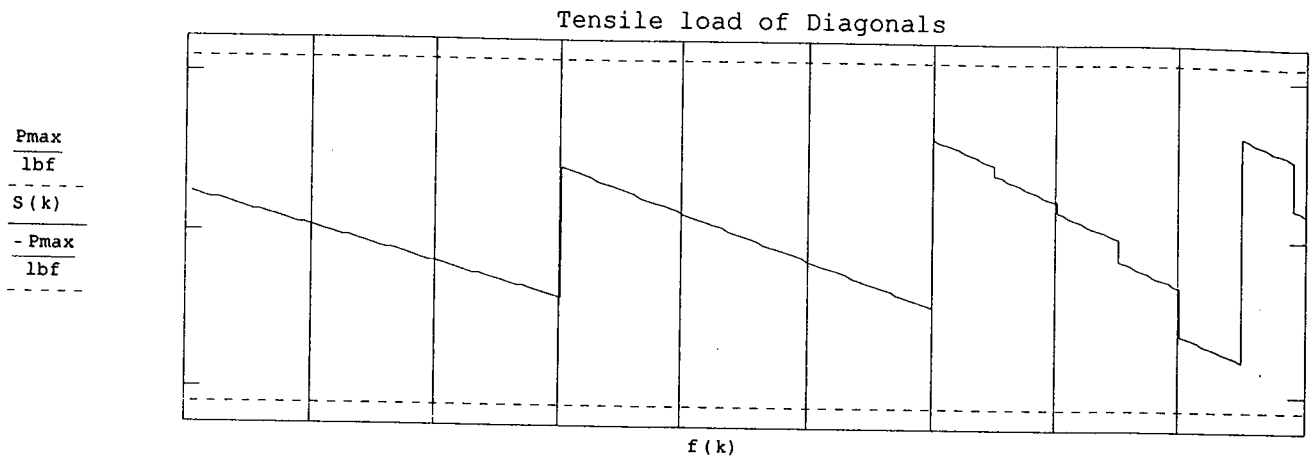


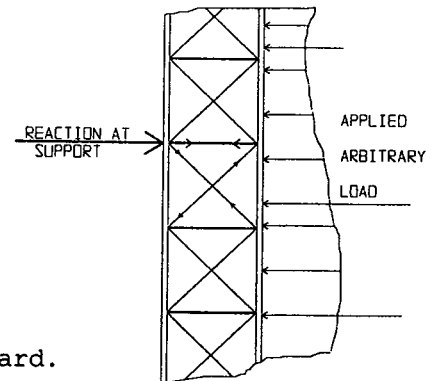
Diagram of force resolution:

Bracing:

Use 5/8" diagonals throughout tower,
3/4" at gypull panels.

Use L1.75x1.75x1/4 at gypulls,
L1.5x1.5x.1875" everywhere else.

Legs: 2-1/2"/3" pipe



All allowable stresses per
American Institute of Steel Construction 9th edition and
Electronics Industry Association 222-E recommended standard.

Calculate the required weld for connection of the double rod on the guy anchor head:

$$\text{Resultant} := 100 \cdot \text{kip}$$

$$\text{BarLoad} := \frac{\text{Resultant}}{2 \cdot \text{bars}}$$

$$\text{WeldLength} := 4 \cdot \text{in}$$

Minimum partial penetration groove weld: Assume only 80% penetration

$$\text{Weld} := \frac{\text{BarLoad}}{2 \cdot \text{WeldLength} \cdot 80\% \cdot .75 \cdot \text{in}}$$

$$\frac{\text{Weld}}{.30 \cdot 70000 \cdot \text{psi}} = 49.6\%$$

Check Block Shear failure of guy head.

$$F_u := 58000 \cdot \text{psi}$$

$$\text{Plate} := .75 \cdot \text{in}$$

$$\text{TensionArea} := 1.5 \cdot \text{in} \cdot \text{Plate}$$

$$\text{ShearArea} := 4 \cdot \text{in} \cdot 2 \cdot \text{sides} \cdot \text{Plate}$$

$$\text{Capacity}_1 := \text{ShearArea} \cdot .30 \cdot F_u + \text{TensionArea} \cdot .50 \cdot F_u$$

$$\text{Capacity}_1 = 137 \cdot \text{kip}$$

$$\text{ShearArea} \cdot .30 \cdot F_u = 104.4 \cdot \text{kip}$$

$$\text{TensionArea} \cdot .50 \cdot F_u = 32.6 \cdot \text{kip}$$

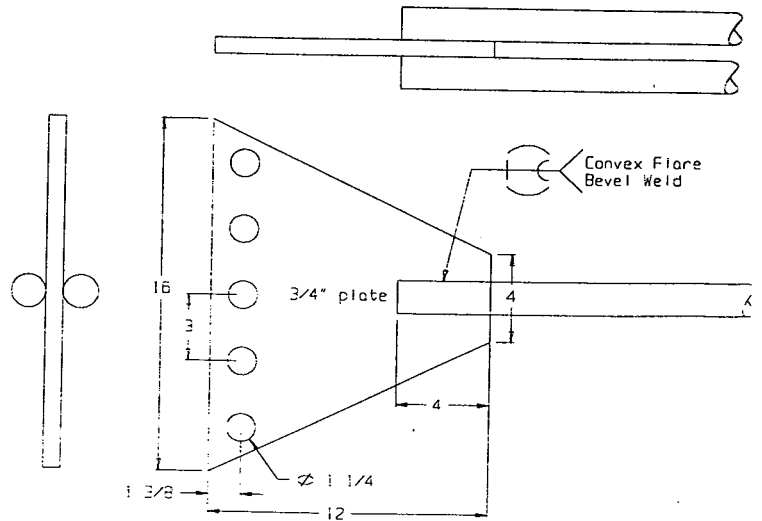
$$\frac{\text{Resultant}}{\text{Capacity}_1} = 73\%$$

Check block shear of bolt hole using splitter for top two guy levels:

$$\text{Load} := 35 \cdot \text{kip} \quad (\text{Full allowable load for } 9/16" \text{ EHS})$$

$$\text{Capacity}_2 := .30 \cdot F_u \cdot \text{Plate} \cdot 1.375 \cdot \text{in} \cdot 2 \cdot \text{sides}$$

$$\frac{\text{Load}}{\text{Capacity}_2} = 97.5\%$$



INNER GUY ANCHOR DESIGN CALCULATIONS

Customer: CDT
 Project: Bozrah, NY
 11/19/97 7:23 AM

REACTIONS:

Vertical 54.9 kips
 Horizontal 61.1 kips
 Resultant 82.1 kips
 Hor. Angle 41.9 °
 Submerged? 0 No
 Water Depth: 0 ft

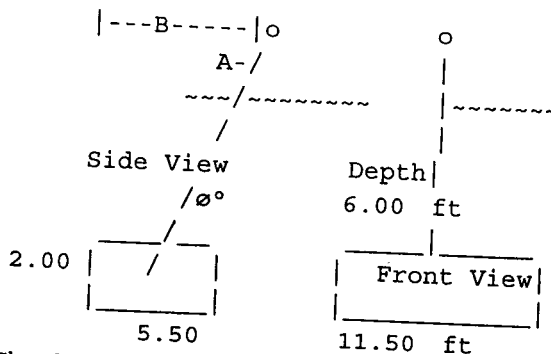
Soil Wt: 100.0 lb/ft³
 Soil Gs: 2.65
 Subm Soil Wt 62.3 lb/ft³
 H.Bearing 400.0 psf/ft
 Rebar Fy: 60.0 ksi
 Conc. Wt: 150.0 lb/ft³
 Conc f`c: 4.0 ksi

CONCRETE WEIGHT:

Block Volume 4.7 cu yds
 Block Wt 19.0 kips

SOIL FRUSTUM WEIGHT:

Frustum: 30 °
 Block: 38.0 kips
 Edges: 35.3 kips
 Corners: 9.6 kips
 Total Wt: 82.9 kips
 Excavatn: 506 cuft



Check anchor shaft embedment? OK

HORIZONTAL CAPACITY: EIA 7.1.2

Load @ 7 ft
 Load: 64400 lb

Uplift 54.89
 Horizontal 61.10 kips
 Capacity:* 56.62
 % Loaded: 97%
 * EIA 7.2.4
 64.40 kips
 95% OK

GUY ANCHOR ROD:

Resultant 82.13 kips
 Hole QTY 6 holes
 # of rods 1
 Fy 48000 psi
 Min. Area 2.139 in²/bar
 Min. Dia. 1.650 in
 Act. Area 2.405 in²/bar
 Act. Dia. 1.75 in, 88.9% Loaded
 Anchor ID: GA6-115-15

Concrete Volume: 14.1 cu yds

ANCHOR ROD LENGTH:

Minimum: 13.22 ft
 Maximum: 14.96 ft
 Recommend: 14.00 ft
 Actual: 15 ft

BLOCK REINFORCEMENT:

Cover: 6 in

	Vertical	Horizontal	
Factored Loads:	71.4	79.4	kips EIA 3.1.13
Factored Moment:	1367.8	1522.3	kip-inch
Minimum As:	1.710	0.566	in ² ACI 10.5.1
Minimum Qty:	9	3	Bar #:
Actual Qty:	9	3	4
Actual As:	1.767	0.589	in ² OK

ANCHOR DIMENSIONS

Length - 11'- 6"
 Width - 5'- 6"
 Height - 2'- 0"
 Depth - 6'- 0"
 OADepth- 8'- 0"
 Dim. A: 6'- 11"
 Dim. B: 12'- 5"
 ∅: 41°

REBAR DIMENSIONS:

RBL: 121"
 RBH: 12"
 RBW: 56"
 Bent OAL: 68"
 QTY Long: 13 Bars ea
 QTY Bent: 14 Bars ea
 Rebar Wt. 157 lb ea

MASTER CHECK: OK

SQUARE FOOTING AND PIER DESIGN

Customer: CDT
 Project: Bozrah, NY
 11/19/97 7:23 AM

Dead Load 0.0 kips
 Live Load 120 kips

G42W10x49 Base Transition ID

ASSUMED DIMENSIONS:

Width	5.50 ft	OK	f'c:	3000	psi
Thickness	1.50 ft		Fy:	60000	psi
Pier OD	2.00 ft		Soil:	4000	psf bearing capacity
Sqr Pier	0				
Rnd Pier	1		Pier Area:	452	inch ²
Depth	3.00 ft		Ht. above Grade	12	inches
Cover	6	inches			
Bar #	4	0.5			
Eff. Depth	11.750	inches			

CALCULATIONS: Minimum Width: 5.477 ft
 Ultimate Load: 168.3 kips ACI 9.2.2
 Net Load: 5562 psf (factored)

CHECK SHEAR

Two Way Action: Assumes $\beta_c=1$	One Way Action Load Area:	4.240	ft ²
Vu: 129481 lbs	Vu:	23581	lbs
Vc: 245756 lbs	Vc:	72209	lbs
52.69%	<= OK =>	32.66%	

LOAD TRANSFER

Pier Capacity/Pu ACI 15.8

@ Pad/Pier interfac 480% OK - Dowels not required.

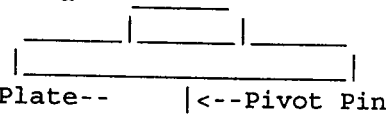
Pivot Pin Bearing Stress: ACI 10.15.1

Minimum Area 47 inch²

Minimum plate OD 7.75 inch \emptyset , 6.87" ea. side square

Distance "d" to edge 0.5 inch -> d

Minimum Plate Thickness: 0.2945 inch



MINIMUM PIER REINFORCING ACI 15.8.2.1, 7.10.5

.5% Req. 2.262 inch² Steel Area:
 8 Bars of # 5 2.454 inch² OK

Bar Length: 55.5 inch

Pier Tie bar #: 4 10 " tie bar spacing

PAD BENDING MOMENT REINFORCEMENT

Mu: 46843 ft-lbs

Ratio: 0.001552 ACI 10.5.1

Steel: 1.203 inch²

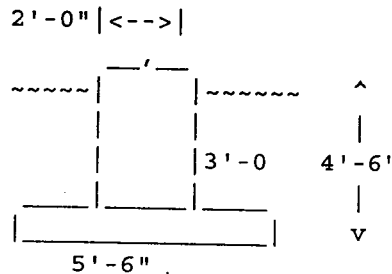
Bar #: 5

Req'd QTY: 4

Act'l QTY: 5 OK

Act. Stl: 1.534 inch²

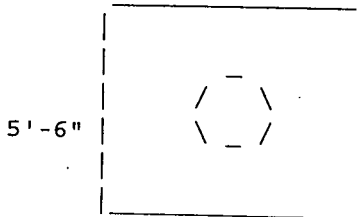
Act. d: 11.500 inches



Moment? OK

Ldb: 11.25 inches OK

Mat Bars: Concrete:
 10 @ 13.50" spacing 2.0 cuyd
 85 lb 8220.0 lb



MASTER CHECK: OK

Tower Loads

Point Loads

No.	QTY	Antenna	Elevation	Windload	Deadload
1	3	12' Cellular Boom	178	292	170
2	9	Sinclair SRL 411C9R130	178	393	80
3	10	PD 10017	180	241	25
4	3	12' Cellular Boom	170	288	170
5	9	ALP 9212	170	124	27
6	3	12' Cellular Boom	160	283	170
7	9	Sinclair SRL 411C9R130	160	380	80
8	3	12' Cellular Boom	150	278	170
9	9	ALP 9212	150	119	27
10	1	6' MHP Dish	140	837	814
11	1	6' MHP Dish	130	837	814
12	1	6' MHP Dish	120	837	814
13	1	G42 Torque Arm	170	537	262
14	1	G42 Torque Arm	120	486	262

Uniform Loads

No.	QTY	Type	Start	Stop	Windload	Deadload
1	19	LDF7-50A 1-5/8"	0	180	0.00	2.40
2	9	LDF7-50A 1-5/8"	0	170	0.00	2.40
3	9	LDF7-50A 1-5/8"	0	160	0.00	2.40
4	9	LDF7-50A 1-5/8"	0	150	0.00	2.40
5	1	LDF7-50A 1-5/8"	0	140	0.00	2.40
6	1	LDF7-50A 1-5/8"	0	130	0.00	2.40
7	1	LDF7-50A 1-5/8"	0	120	0.00	2.40
8	1	Tower Span 1	0	60	155.00	51.90
9	1	Tower Span 2	60	120	207.00	51.90
10	1	Tower Span 3	120	180	239.00	51.90

TRIANGULAR TOWER SECTION DATA

Client: CDT

=====

Project: Bozrah, CT

Guyed Tower Section

11/18/97 4:09 PM

Tria

Wind Angle 0,60,90 90 °

Span: 3

Elevation of Foundation: 1 ft

Elev@Top 160 feet

Wind Speed 85 mph

Elev@Base 140 feet

Gh 1.12 EIA 2.3.4

Tower Ht. 180 feet

Wind Pres. 32.0 psf EIA 2.3.3

Top Face 42 inches 3.50

Radial Ice 0.5 inch

Bot Face 42 inches 3.50

EIA 2.3.15 Wind/Ice Reductn? Yes

Taper 0 in./sect.

ANSI/EIA Overstress Factor: Yes

Ave Face 42 inches

Length 240 inches

LEGS OD,L1 ID,L2 wall

FL.to BR 6 inches

2.5" Sch40 2.875 2.469 0.203

Panel 6 panels

DIAGONALS

Panel 38.00 inches

5/8" Rod 0.625 0.000 0.313

Br/Panel 2 |x|

HORIZONTALS

Br Lngth 54.54 inches

L1.5x1.5x3 1.500 1.500 0.188

Horiz 7 7

Density 0.283 lb/in^3

Dbl Angle Gap: 0 in

Bracing Type: 1 |x|

Galvanizing? Yes

WaveGuide hole reduction? Yes

SECTION GEOMETRY » 1508 in^4

Section Ixx,Iyy » 1508 in^4

ITEM DL WL

Face Vert. Angle 0.000 °

Ladder: 10 10

Leg Angle in face 0.000 °

Misc. 10 10

Leg/Axis Angle 0.000 °

Total lbf: 20 20

Brace Angle 42.138 °

SECTION WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Total Weig 702 336 lbs

Ag:	11010	
Af:	411	Df: 0.850
Ar:	3197	Rr: 0.625
SR(e):	0.328	Dr: 1.000
Cf:	2.496	

K 1.00

Legs: KL/r 40.1 OK

Fy 67000 psi

EIA 3.1.1, Cc 92.4

AISC E2 Fa 44483 psi

Max.Compresn.Force 75802 lbs

Area: 16.30 ft^2

Shear: 996 49.8 lbf,lbf/ft

CnMoment: 9964 ft-lbf

Deadload: 1038 51.9 lbf,lbf/ft

K 0.70

Solid Area Windloads:

Diagonals: KL/r 119.1 OK

Shear: 4787 239.4 lbf,lbf/ft

Fy 36000 psi

Cc 126.1

inches^2 feet^2

EIA 3.1.1 Fa 13882 psi

Ae 0° 2408.5 16.73

Max.Compresn.Force 4259 lbs

Ae 45° 2890.2 20.07

Max.Tension.Force* 8836 lbs

Ae 60° 2326.3 16.16

*Verify Net Section on member.

Ae 90° 2346.9 16.30

K 0.7

Horizontals: KL/r 93.4 OK

Span Length 60 ft

Cc 126.1

Span Capacity 74828 lbf/leg

EIA 3.1.1 Fa 18401 psi

Max.Compresn.Force 8194 lbs

TRIANGULAR TOWER SECTION DATA
 =====

Client: CDT
 Project: Bozrah, CT
 11/18/97 4:09 PM Tria

Guyed Tower Section
 Wind Angle 0,60,90 90 °
 Elevation of Foundation: 1 ft
 Wind Speed 85 mph
 Gh 1.12 EIA 2.3.4
 Wind Pres. 20.7 psf EIA 2.3.3
 Radial Ice 0.5 inch
 EIA 2.3.15 Wind/Ice Reductn? Yes
 ANSI/EIA Overstress Factor: Yes

Span: 1
 Elev@Top 40 feet
 Elev@Base 20 feet
 Tower Ht. 180 feet
 Top Face 42 inches 3.50
 Bot Face 42 inches 3.50
 Taper 0 in./sect.
 Ave Face 42 inches
 Length 240 inches
 FL.to BR 6 inches
 # Panel 6 panels
 Panel 38.00 inches
 Br/Panel 2 |x|
 Br Lngth 54.54 inches
 # Horiz 7 7
 Density 0.283 lb/in^3
 Bracing Type: 1 |x|

LEGS OD,L1 ID,L2 wall
 2.5" Sch40 2.875 2.469 0.203
 DIAGONALS
 5/8" Rod 0.625 0.000 0.313
 HORIZONTALS
 L1.5x1.5x3 1.500 1.500 0.188

SECTION GEOMETRY » 1508 in^4
 Section Ixx,Iyy » 1508 in^4
 Face Vert. Angle 0.000 °
 Leg Angle in face 0.000 °
 Leg/Axis Angle 0.000 °
 Brace Angle 42.138 °

Dbl Angle Gap: 0 in
 Galvanizing? Yes
 WaveGuide hole reduction? Yes

ITEM DL WL
 Ladder: 10 10
 Misc. 10 10
 Total lbf: 20 20

SECTION WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

-----			Total Weig	702	336 lbs
Ag:	11010				
Af:	411	Df: 0.850			
Ar:	3197	Rr: 0.625			
SR(e):	0.328	Dr: 1.000	Legs:	K	1.00
Cf:	2.496			KL/r	40.1 OK
				Fy	67000 psi
			EIA 3.1.1,	Cc	92.4
Area:	16.30	ft^2	AISC E2	Fa	44483 psi
Shear:	652	32.6 lbf,lbf/	Max.Compresn.Force		75802 lbs
CnMoment:	6523	ft-lbf			
Deadload:	1038	51.9 lbf,lbf/ft		K	0.70
Solid Area Windloads:			Diagonals :	KL/r	119.1 OK
Shear:	3100	155.0 lbf,lbf/ft		Fy	36000 psi
				Cc	126.1
	inches^2	feet^2	EIA 3.1.1	Fa	13882 psi
Ae 0°	2408.5	16.73	Max.Compresn.Force		4259 lbs
Ae 45°	2890.2	20.07	Max.Tension.Force*		8836 lbs
Ae 60°	2326.3	16.16	*Verify Net Section on member.		
Ae 90°	2346.9	16.30		K	0.7
Span Length	60	ft	Horizontals:	KL/r	93.4 OK
pan Capacity	74828	lbf/leg		Cc	126.1
			EIA 3.1.1	Fa	18401 psi
			Max.Compresn.Force		8194 lbs

TRIANGULAR TOWER SECTION DATA

=====

Guyed Tower Section

Wind Angle 0,60,90 90 °

Elevation of Foundation: 1 ft

Wind Speed 85 mph

Gh 1.12 EIA 2.3.4

Wind Pres. 27.7 psf EIA 2.3.3

Radial Ice 0.5 inch

EIA 2.3.15 Wind/Ice Reductn? Yes

ANSI/EIA Overstress Factor: Yes

LEGS OD,L1 ID,L2 wall

2.5" Sch40 2.875 2.469 0.203

DIAGONALS

5/8" Rod 0.625 0.000 0.313

HORIZONTALS

L1.5x1.5x3 1.500 1.500 0.188

Dbl Angle Gap: 0 in

Galvanizing? Yes

WaveGuide hole reduction? Yes

ITEM DL WL

Ladder: 10 10

Misc. 10 10

Total lbf: 20 20

Client: CDT

Project: Bozrah, CT

11/18/97 4:09 PM

Tria

Span: 2

Elev@Top 100 feet

Elev@Base 80 feet

Tower Ht. 180 feet

Top Face 42 inches 3.50

Bot Face 42 inches 3.50

Taper 0 in./sect.

Ave Face 42 inches

Length 240 inches

FL.to BR 6 inches

Panel 6 panels

Panel 38.00 inches

Br/Panel 2 |x|

Br Lngth 54.54 inches

Horiz 7 7

Density 0.283 lb/in^3

Bracing Type: 1 |x|

SECTION GEOMETRY » 1508 in^4

Section Ixx,Iyy » 1508 in^4

Face Vert. Angle 0.000 °

Leg Angle in face 0.000 °

Leg/Axis Angle 0.000 °

Brace Angle 42.138 °

SECTION WIND LOAD / WEIGHT CALCULATIONS:

	Pro OD	X-Area	Weight	Ice Wt
Legs	3.875	1.704	347.2	123.7 lbs
Diagonals	1.625	0.307	170.5	112.4 lbs
Horizontals	2.500	0.527	131.6	100.0 lbs

Total Weig 702 336 lbs

Ag: 11010

Af: 411 Df: 0.850

Ar: 3197 Rr: 0.625

SR(e): 0.328 Dr: 1.000

Cf: 2.496

Legs: K 1.00

KL/r 40.1 OK

Fy 67000 psi

EIA 3.1.1, Cc 92.4

AISC E2 Fa 44483 psi

Max.Compresn.Force 75802 lbs

Area: 16.30 ft^2

Shear: 865 43.2 lbf,lbf/ft

CnMoment: 8649 ft-lbf

Deadload: 1038 51.9 lbf,lbf/ft

Solid Area Windloads:

Shear: 4142 207.1 lbf,lbf/ft

Diagonals: K 0.70

KL/r 119.1 OK

Fy 36000 psi

Cc 126.1

EIA 3.1.1 Fa 13882 psi

Max.Compresn.Force 4259 lbs

Max.Tension.Force* 8836 lbs

*Verify Net Section on member.

K 0.7

Horizontals: KL/r 93.4 OK

Cc 126.1

EIA 3.1.1 Fa 18401 psi

Max.Compresn.Force 8194 lbs

Span Length 60 ft

Span Capacity 74828 lbf/leg

Input File:boz

Tower Data File

Associated Data Files

boz.out

boz.mom

boz.mcn

ID

CDT

Bozrah, NY

5463

th face wind ice vo int az

180 42 85 .5 1 1 0

Beam Configuration

HBHBHBHC

Guy Data

3

2 170 145 EHS

2 120 145 EHS

1 60 145 EHS

Section Inertia

3

0 60 7.270259E-02

60 120 7.270259E-02

120 180 7.270259E-02

Leg Capacity

3

0 80 74827.66

80 140 74827.66

140 180 74827.66

Point Loads

14

3 12' Cellular Boom , 178 292.0766 170

9 Sinclair SRL 411C9R130 , 178 393.1072 80

10 PD 10017 , 180 241.3179 25

3 12' Cellular Boom , 170 288.2642 170

9 ALP 9212 , 170 123.5418 27

3 12' Cellular Boom , 160 283.3141 170

9 Sinclair SRL 411C9R130 , 160 380.0984 80

3 12' Cellular Boom , 150 278.1378 170

9 ALP 9212 , 150 119.2019 27

1 6' MHP Dish , 140 836.7584 814

1 6' MHP Dish , 130 836.7584 814

1 6' MHP Dish , 120 836.7584 814

1 G42 Torque Arm , 170 537.1382 262

1 G42 Torque Arm , 120 486.258 262

Uniform Loads

10

19 LDF7-50A 1-5/8" , 0 180 0 2.4

9 LDF7-50A 1-5/8" , 0 170 0 2.4

9 LDF7-50A 1-5/8" , 0 160 0 2.4

9 LDF7-50A 1-5/8" , 0 150 0 2.4

1 LDF7-50A 1-5/8" , 0 140 0 2.4

1 LDF7-50A 1-5/8" , 0 130 0 2.4
1 LDF7-50A 1-5/8" , 0 120 0 2.4
1 Tower Span 1 , 0 60 155 51.9
1 Tower Span 2 , 60 120 207 51.9
1 Tower Span 3 , 120 180 239 51.9
End



STATE OF CONNECTICUT
CONNECTICUT SITING COUNCIL

Ten Franklin Square
New Britain, Connecticut 06051
Phone: (860) 827-2935
Fax: (860) 827-2950

March 19, 1999

Honorable Raymond C. Barber
First Selectman
Town of Bozrah
Town Hall
1 River Road
Bozrah, CT 06334

RE: TS-SCLP-013-990317 - Springwich Cellular Limited Partnership request for an order to approve tower sharing at an existing telecommunications facility located off 3 Polly Lane in Bozrah, Connecticut.

Dear Mr. Barber:

On March 17, 1999, the Connecticut Siting Council (Council) received a request from Springwich Cellular Limited Partnership for an order to approve tower sharing at an existing telecommunications facility located off 3 Polly Lane in Bozrah, Connecticut, pursuant to Connecticut General Statutes § 16-50aa.

The Council will consider this item at the next meeting tentatively scheduled for Tuesday, April 6, 1999 at 1:30 p.m., in Hearing Room Two, Ten Franklin Square, New Britain, Connecticut.

Please call me or inform the Council if you have any questions or comments regarding this modification of an existing facility.

Thank you for your cooperation and consideration.

Very truly yours,

Joel M. Rinebold
Executive Director

JMR/jlh

Enclosure: Notice of Intent



RECEIVED

MAR 17 1999

**CONNECTICUT
SITING COUNCIL**

SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

March 17, 1999

Peter W. van Wilgen
Director - Real Estate Operations

Mr. Mortimer A. Gelston, Chairman
Connecticut Siting Council
10 Franklin Square
New Britain, Connecticut 06051

**RE: Springwich Cellular Limited Partnership—Bozrah Cellular
Communication Site**

Dear Chairman Gelston:

Springwich Cellular Limited Partnership (SCLP) plans to install cellular antennas and a related equipment building at the tower facility owned by Mrs. Alice Maynard of Colchester, Connecticut, and managed by Cordless Data Transfer, Inc. of Marlborough, Connecticut. Please accept this letter as notice of intent, pursuant to R.C.S.A. Section 16-50aa, of the placement of associated equipment on an existing non-facility tower pursuant to R.C.S.A. Section 16-50aa. In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter is being sent to the First Selectman of Bozrah.

The existing non-facility tower is a 185' guyed tower located at 3 Polly Lane, Bozrah, Connecticut. Omnipoint and NEXTEL Communications are presently located on the tower, and SCLP plans to install up to twelve panel-type cellular antennas on the tower. SCLP will also install a single story, approximately 12'x26' equipment building, which will contain radio transmission equipment.

The addition of SCLP's antennas and equipment to the tower site does not constitute a substantial environmental affect since such additions do not cause a significant change or alteration in the physical and environmental characteristics of the site (see attached site plan). Rather, the planned changes to the existing non-facility tower falls squarely within those activities explicitly provided for in R.C.S.A. Section 16-50aa.

First, the height of the existing tower will be unaffected. Twelve antennas, ALP Model 11011N, will be mounted four per sector on a triangular platform to be attached to the tower. The center of radiation will be 160' AGL and the top of the antennas will be 162' high. The tower will not require any structural modification to support the proposed attachments.

Second, the proposed addition will not extend the site boundaries. The proposed equipment building will be located next to the tower on a parcel of land of approximately 312 square feet in size, which will be leased to SCLP (see attached site plan).

Third, the proposed addition will not increase the noise levels at the existing facility by six decibels or more.

Fourth, operation of the additional antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base, to a level at or above the ANSI standard. The following table summarizes the power densities at the site from the various sources on the tower (including proposed herein) in relation to the standard.

FREQUENCY	POWER DENSITY	HEIGHT	ANSI/IEEE STANDARD LIMITS (mW/cm ²)	% OF MPE
Omnipoint 1945	.0111	181'	1.0000	1.11
SCLP 880-894	0.0290	160'	0.5867	4.95
Nextel 851	0.0228	175'	0.5673	4.02
TOTAL	N/A		N/A	10.08

As the table demonstrates, SCLP's proposed antennas would contribute 4.95% of the ANSI standard for the cellular frequency range, bringing the site total to 10.08% of the standard as calculated for a mixed frequency site.

Finally, SCLP will obtain the necessary municipal approvals and permits for the project once Connecticut Siting Council approval has been received, as the Town of Bozrah requires proof of CSC approval before any permits will be issued.

SCLP submits that the proposed additions would not cause a significant change or alteration in the physical and environmental characteristics of the site and comply with R.C.S.A. Section 16-50aa. For the foregoing reasons, SCLP therefore requests a determination that the placement of the antennas and equipment on the existing non-facility tower site does not constitute a substantial environmental effect under R.C.S.A. Section 16-50aa, and that the requested tower sharing be approved.

Thank you for your consideration.

Sincerely,

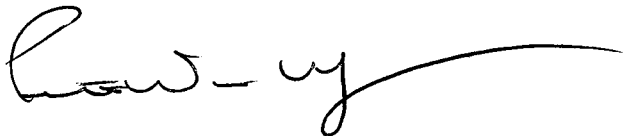


EXHIBIT A
The Site

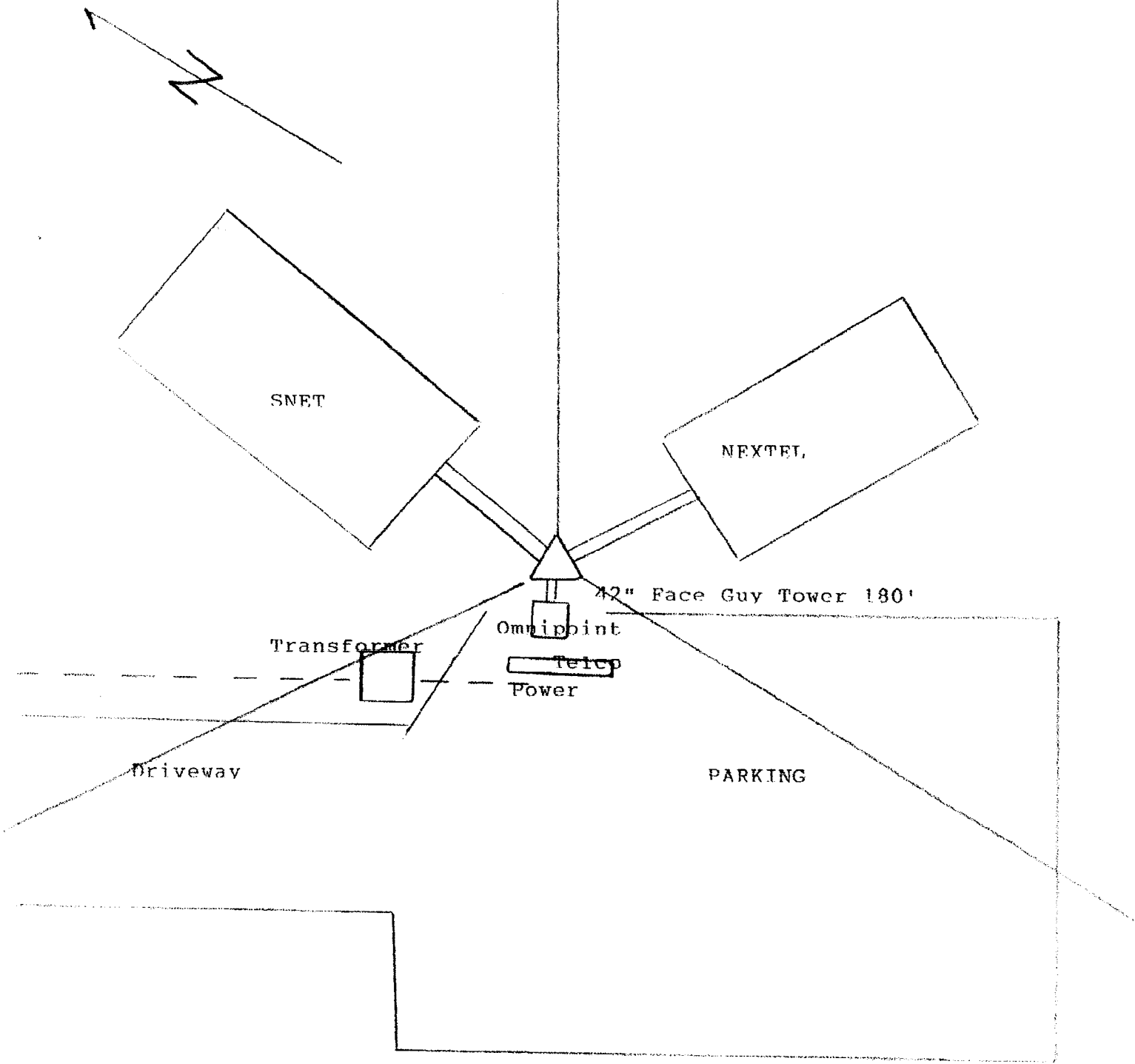
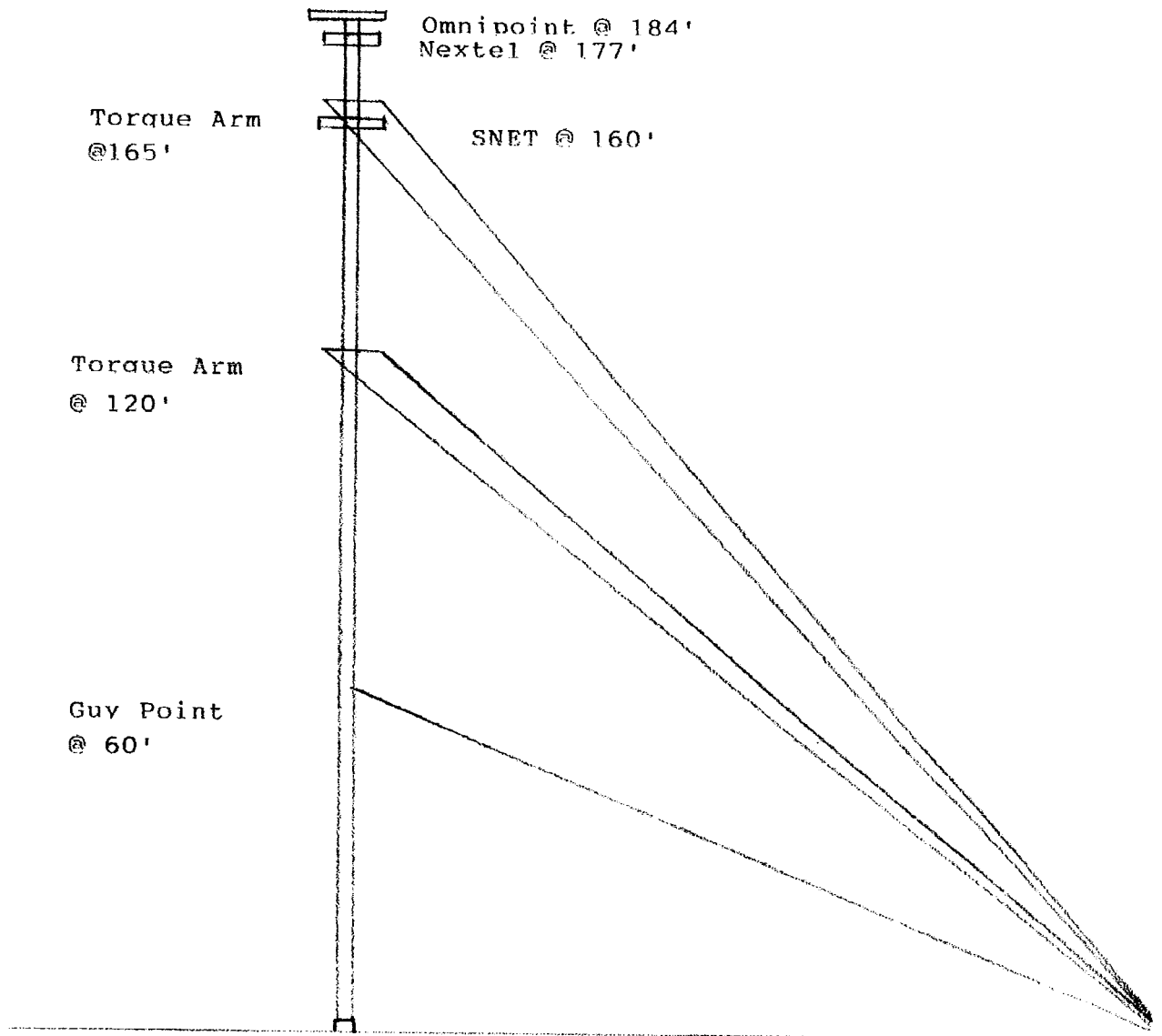


EXHIBIT B
Antennae Placement





SNET Mobility, Inc.
500 Enterprise Drive
Rocky Hill, Connecticut 06067-3900
Phone: (860) 513-7730
Fax: (860) 513-7614

March 17, 1999

Peter W. van Wilgen
Director - Real Estate Operations

Mr. Raymond Barber, First Selectman
Town of Bozrah
1 River Road
Bozrah, Connecticut 06334

Dear First Selectman Barber:

Springwich Cellular Limited Partnership (SCLP) plans to install antennas and associated equipment at the existing tower facility owned by Mrs. Alice Maynard of Colchester, Connecticut and managed by Cordless Data Transfer of Marlborough, Connecticut. As required by Section 16-50j-73 of the Regulations of Connecticut State Agencies (R.C.S.A.), please accept this letter and the attached letter to the Connecticut Siting Council dated March 16, 1999, describing SCLP's planned use of this tower facility.

The attached letter fully describes SCLP's proposal. However, if you have any questions or require any further information on our plans or the Siting Council's procedures, please call me at (860) 513-7730 or Mr. Joel Rinebold, Executive Director, Connecticut Siting Council at (860) 827-2935.

Sincerely,

A handwritten signature in dark ink, appearing to read "Peter W. van Wilgen". The signature is fluid and cursive, with a long horizontal stroke extending to the right.

Enclosure