



Filed by:
Kri Pelletier, Property Specialist - SBA Communications
134 Flanders Rd., Suite 125, Westborough, MA 01581
508.251.0720 x 3804 - kpelletier@sbsite.com

July 27, 2018

Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
Ten Franklin Square
New Britain, CT 06051

Notice of Exempt Modification

131 Gifford Lane, Bozrah, CT

41 33 9.06 N

-72 9 2.55 W

Sprint #: CT33XC574

Dear Ms. Bachman:

Sprint currently maintains antennas at the 175-foot level of the existing 195-foot Self Support Tower at 131 Gifford Lane in Bozrah, CT. The tower is owned by SBA Towers, LLC. The property is owned by Richard Orr and Patti Duerrler. Sprint now intends to replace (6) existing cell antennas with (6) newer technology cell antennas at the 99-foot level of the tower. The proposed full scope of work is as follows:

Remove:

- (6) 1-5/8" lines

Remove and Replace:

- Remove:
 - (6) Decibel DB908h90e-m Panel Antennas
- Replace with:
 - (3) RFS APXVTM14-C-I20 Panel Antennas
 - (3) Commscope NNVV-65B-R4 Panel Antennas

Install:

- (3) ALU 1900 MHz RRHs
- (6) ALU 800 MHz RRHs
- (3) ALU TD-RRH 8x20-25
- (3) Sitepro SFS H-L
- (4) 1-1/4" fiber

Existing Equipment to Remain (Including entitlements):

- (3) T -Frames

This facility was originally approved by the Town of Bozrah's on February 11, 1999. The Planning & Zoning Commission approved Special Permit for a 196' telecom tower with the condition that the drive/access road be construction per the Town's guidelines. No further conditions were set. As such, this modification complies with all conditions.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16.50j-72(b)(2). In accordance with R.C.S.A. § 16.50j-73, a copy of this letter is being sent to the Town of Bozrah's First Selectman, Glenn Pianka, and Chair of the Planning & Zoning Commission, Seymour Adelman, as well as to the property owner. (Separate notice is not being sent to tower owner, as it belongs to SBA.)

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. §16.50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modification will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modification will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Sprint respectfully submits that the proposed modifications to the above-referenced telecommunication facility constitute an exempt modifications under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,



Kri Pelletier
Property Specialist
SBA COMMUNICATIONS CORPORATION
134 Flanders Rd., Suite 125
Westborough, MA 01581
508.251.0720 x3804 + T
508.366.2610 + F
203.446.7700 + C
kpelletier@sbsite.com

Attachments

cc: Glenn Painka, First Selectman / with attachments
Town of Bozrah, Town Hall, 1 River Road, Bozrah, CT 06334
Seymour Adelman, Chair-Planning & Zoning Commission / with attachments
Town of Bozrah, Town Hall, 1 River Road, Bozrah, CT 06334
Patti Duerrler and Richard Orr / with attachments
131 Gifford Lane, Bozrah, CT 06334



POWER DENSITY

SPRINT Site Inventory and Power Data by Antenna

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4
Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd
Height (AGL):	175 feet	Height (AGL):	175 feet	Height (AGL):	175 feet
Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)
Channel Count	10	Channel Count	10	Channel Count	10
Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts
ERP (W):	7,378.61	ERP (W):	7,378.61	ERP (W):	7,378.61
Antenna A1 MPE%	1.15 %	Antenna B1 MPE%	1.15 %	Antenna C1 MPE%	1.15 %
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	RFS APXVTM14- ALU- I20	Make / Model:	RFS APXVTM14- ALU- I20	Make / Model:	RFS APXVTM14- ALU- I20
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	175 feet	Height (AGL):	175 feet	Height (AGL):	175 feet
Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)
Channel Count	8	Channel Count	8	Channel Count	8
Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts
ERP (W):	6,224.72	ERP (W):	6,224.72	ERP (W):	6,224.72
Antenna A2 MPE%	0.78 %	Antenna B2 MPE%	0.78 %	Antenna C2 MPE%	0.78 %

Site Composite MPE%	
Carrier	MPE%
SPRINT – Max per sector	1.93 %
Omnipoint (T-Mobile)	0.08 %
Verizon Wireless	1.91 %
AT&T	1.81 %
Site Total MPE %:	5.73 %

SPRINT Sector A Total:	1.93 %
SPRINT Sector B Total:	1.93 %
SPRINT Sector C Total:	1.93 %
Site Total:	5.73 %

SPRINT Frequency Band / Technology Max Power Values (All Sectors)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (μ W/cm ²)	Frequency (MHz)	Allowable MPE (μ W/cm ²)	Calculated % MPE
Sprint 850 MHz CDMA	1	376.73	175	0.47	850 MHz	567	0.09%
Sprint 850 MHz LTE	2	941.82	175	2.37	850 MHz	567	0.42%
Sprint 1900 MHz (PCS) CDMA	5	511.82	175	3.22	1900 MHz (PCS)	1000	0.32%
Sprint 1900 MHz (PCS) LTE	2	1,279.56	175	3.22	1900 MHz (PCS)	1000	0.32%
Sprint 2500 MHz (BRS) LTE	8	778.09	175	7.84	2500 MHz (BRS)	1000	0.78%
Total:							1.93%

ORIGIN ID:BFEA (508) 251-0720
KRI PELLETIER
SBA COMMUNICATIONS CORPORATION
134 FLANDERS RD
SUITE 125
WESTBOROUGH, MA 01581
UNITED STATES US

SHIP DATE: 27 JUL 18
ACT/WGT: 1.00 LB
CAD: 105843304/NET4040

BILL SENDER

TO SEYMOUR ADELMAN, PLANNING & ZONING
TOWN OF BORZAH
1 RIVER ROAD

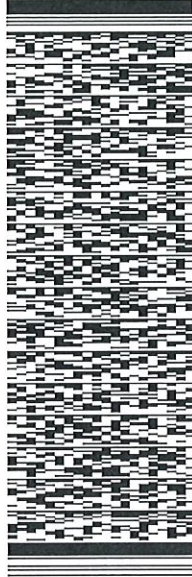
BOZRAH CT 06334

(508) 251-0720 X 3804

REF: 10-56-92009-8089

INV:

DEPT:



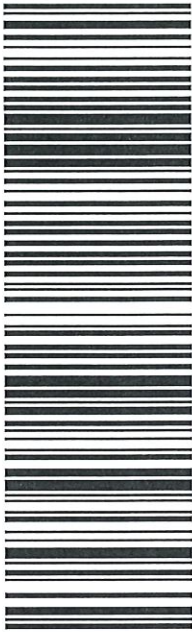
J182018072201uv

TRK# 0201 7728 3460 3482

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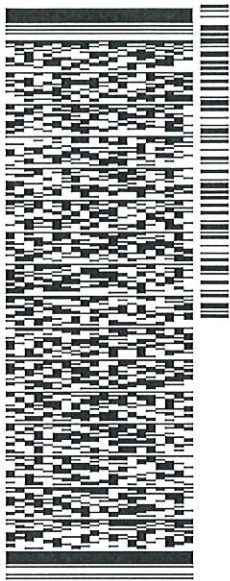
SHIP DATE: 27 JUL 18
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TO
GLENN PAINKA, FIRST SELECTMAN
TOWN OF BOZRAH
1 RIVER RD.

BOZRAH CT 06334
(508) 251-0720 X 3804 REF: 10-56-92009-6089
INV. DEPT:
PO:

552J28532JDCA5



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KRIPEL LETTER
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WESTBOROUGH MA 01581
UNITED STATES US

SHIP DATE: 27 JUL 18
ACTWGT: 1.00 LB
CAD: 105843304IN/ET4040

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TO PATTI DUERLER AND RICHARD ORR

131 GIFFORD LANE

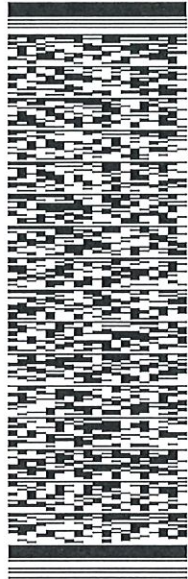
BOZRAH CT 06334

(508) 251-0720 X 3804

REF: 10-56-92009-6089

PO:

DEPT:



J182018072201uv

TRK# 7728 3464 8731
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All information is for assessment purposes only. Assessments are calculated at 70% of the estimated October 1, 2017 market value which was the date of the last revaluation as completed by eQuality Valuation Services, LLC.



Information on the Property Records for the Municipality of Bozrah was last updated on 5/4/2018.

Property Summary Information

Parcel Data And Values

Building ▾

Outbuildings

Sales

Permits

Google Map

Parcel Information

Location:	131 GIFFORD LA	Property Use:	Residential	Primary Use:	Residential
Unique ID:	00083400	Map Block Lot:	07/119-B	Acres:	1.97
490 Acres:	0.00	Zone:	R-1	Volume / Page:	0092/0318
Developers Map / Lot:		Census:	7131		

Value Information

	Appraised Value	Assessed Value
Land	67,710	47,390
Buildings	152,597	106,820
Detached Outbuildings	1,094	770
Total	221,401	154,980

Owner's Information

Owner's Data

ORR RICHARD & DUERRLER PATTI
131 GIFFORD LANE
BOZRAH, CT 06334

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RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

SPRINT Existing Facility

Site ID: CT33XC574

N. Bozrah
131 Gifford Lane
Bozrah, CT 06334

July 6, 2018

EBI Project Number: 6218004931

Site Compliance Summary	
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	5.73 %



July 6, 2018

SPRINT

Attn: RF Engineering Manager
1 International Boulevard, Suite 800
Mahwah, NJ 07495

Emissions Analysis for Site: **CT33XC574 – N. Bozrah**

EBI Consulting was directed to analyze the proposed SPRINT facility located at **131 Gifford Lane, Bozrah, CT**, for the purpose of determining whether the emissions from the Proposed SPRINT Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The number of $\mu\text{W}/\text{cm}^2$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

General population exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ($\mu\text{W}/\text{cm}^2$). The general population exposure limits for the 850 MHz Band is approximately $567 \mu\text{W}/\text{cm}^2$. The general population exposure limit for the 1900 MHz (PCS) and 2500 MHz (BRS) bands is $1000 \mu\text{W}/\text{cm}^2$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed SPRINT Wireless antenna facility located at **131 Gifford Lane, Bozrah, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since SPRINT is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 1 CDMA channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.
- 2) 2 LTE channels (850 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 50 Watts per Channel.
- 3) 5 CDMA channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 16 Watts per Channel.
- 4) 2 LTE channels (1900 MHz (PCS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 5) 8 LTE channels (2500 MHz (BRS)) were considered for each sector of the proposed installation. These Channels have a transmit power of 20 Watts per Channel.



- 6) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 7) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 8) The antennas used in this modeling are the **Commscope NNVV-65B-R4 and the RFS APXVTM14-ALU-I20** for transmission in the 850 MHz, 1900 MHz (PCS) and 2500 MHz (BRS) frequency bands. This is based on feedback from the carrier with regards to anticipated antenna selection. Maximum gain values for all antennas are listed in the Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antenna mounting height centerlines of the proposed antennas are **175 feet** above ground level (AGL) for **Sector A**, **175 feet** above ground level (AGL) for **Sector B** and **175 feet** above ground level (AGL) for Sector C.
- 10) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general population threshold limits.



SPRINT Site Inventory and Power Data by Antenna

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4	Make / Model:	Commscope NNVV-65B-R4
Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd	Gain:	12.75 / 15.05 dBd
Height (AGL):	175 feet	Height (AGL):	175 feet	Height (AGL):	175 feet
Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)	Frequency Bands	850 MHz / 1900 MHz (PCS)
Channel Count	10	Channel Count	10	Channel Count	10
Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts	Total TX Power(W):	280 Watts
ERP (W):	7,378.61	ERP (W):	7,378.61	ERP (W):	7,378.61
Antenna A1 MPE%	1.15 %	Antenna B1 MPE%	1.15 %	Antenna C1 MPE%	1.15 %
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	RFS APXVTM14-ALU-I20	Make / Model:	RFS APXVTM14-ALU-I20	Make / Model:	RFS APXVTM14-ALU-I20
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	175 feet	Height (AGL):	175 feet	Height (AGL):	175 feet
Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)	Frequency Bands	2500 MHz (BRS)
Channel Count	8	Channel Count	8	Channel Count	8
Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts	Total TX Power(W):	160 Watts
ERP (W):	6,224.72	ERP (W):	6,224.72	ERP (W):	6,224.72
Antenna A2 MPE%	0.78 %	Antenna B2 MPE%	0.78 %	Antenna C2 MPE%	0.78 %

Site Composite MPE%	
Carrier	MPE%
SPRINT – Max per sector	1.93 %
Omnipoint (T-Mobile)	0.08 %
Verizon Wireless	1.91 %
AT&T	1.81 %
Site Total MPE %:	5.73 %

SPRINT Sector A Total:	1.93 %
SPRINT Sector B Total:	1.93 %
SPRINT Sector C Total:	1.93 %
Site Total:	5.73 %

SPRINT _ Frequency Band / Technology Max Power Values (All Sectors)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ($\mu\text{W}/\text{cm}^2$)	Frequency (MHz)	Allowable MPE ($\mu\text{W}/\text{cm}^2$)	Calculated % MPE
Sprint 850 MHz CDMA	1	376.73	175	0.47	850 MHz	567	0.09%
Sprint 850 MHz LTE	2	941.82	175	2.37	850 MHz	567	0.42%
Sprint 1900 MHz (PCS) CDMA	5	511.82	175	3.22	1900 MHz (PCS)	1000	0.32%
Sprint 1900 MHz (PCS) LTE	2	1,279.56	175	3.22	1900 MHz (PCS)	1000	0.32%
Sprint 2500 MHz (BRS) LTE	8	778.09	175	7.84	2500 MHz (BRS)	1000	0.78%
						Total:	1.93%



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the SPRINT facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

SPRINT Sector	Power Density Value (%)
Sector A:	1.93 %
Sector B:	1.93 %
Sector C:	1.93 %
SPRINT Maximum Total (per sector):	1.93 %
Site Total:	5.73 %
Site Compliance Status:	COMPLIANT

The anticipated composite MPE value for this site assuming all carriers present is **5.73 %** of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.



CONSULTING GROUP, INC.

9221 Lyndon B. Johnson Freeway, #204, Dallas, TX 75243 * PHONE 972-231-8893 * FAX 1-866-364-8375
www.allprocgi.com * e-mail: info@allprocgi.com

**Tower Structural Analysis Report for
SBA Communications Corporation**



Existing 195' Self Support Tower

SBA Site Name: Bozrah
SBA Site Number: CT01105-S-02
Carrier Name: Sprint Nextel
Carrier Site ID/Name: CT33XC574 / N. Bozrah
App #: 73320, v3

Site Location:
131 Gifford Lane,
Bozrah, CT 06334
New London County

Latitude: 41.552517
Longitude: -72.150708

ACGI Job # 18-3611

ANALYSIS RESULTS		
Tower Components	87.3 %	Pass
Tower Foundation Capacity	72.1 %	Pass
Net Change in Tower Stress	-1.4 %	Change from previous Structural Analysis by SBA, Project # CT01105-VZW-011816, dated 01/26/2016 (F Code)
Net change in stress due to Mount Modification	+2.2 %	Addition of (6) Site Pro 1 SCXx-K to (3) V-Brace Kit SFS-H-L Mounts.

Prepared By:
Bob Akech.



05/25/2018
Approved By:
Joji Geroge, P.E.
CT PE #24444



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 TNX TOWER CALCULATION PRINTOUT..... XIV

1. ANALYSIS SUMMARY

The existing 195' Self Support Tower located in Bozrah, CT was analyzed by Allpro Consulting Group, Inc (ACGI) for the existing loads and the proposed **Sprint Nextel** antennas and coaxes as per application 73320, v3 as authorized by **SBA Communication Corp.** Based on the results of the analysis, the existing tower with mentioned proposed and existing loading is found **to be in code compliance** with *TIA-222-G, Structural Standards for Steel Antenna Towers and Antenna Supporting Structures* and *IBC 2012*.

2. SCOPE & SOURCE OF INFORMATION

The purpose of this structural analysis is to determine whether the existing structure is capable of supporting additional proposed loads.

SOURCE OF INFORMATION		
Tower Data:	Pirod Inc.	Original Tower Drawings by Pirod, Inc. (Job No. A-115466 dated 04/01/1999)
	SBA	Previous Structural Analysis by SBA, Project # CT01105-VZW-011816 dated 01/26/2016.
Foundation Data:	Pirod Inc.	Original Tower Drawings by Pirod, Inc. (Job No. A-115466 dated 04/01/1999)
Geotechnical Report:	Jaworski Geotech, Inc.	Geotechnical report by Jaworski Geotech, Inc., Project # C98492G, dated 12/14/1998.
Loading Data:	SBA	Existing loading as per redlined previous Structural Analysis by SBA, Project # CT01105-VZW-011816 dated 01/26/2016.
	SBA Communication Corp.	Site information based on SBA Site Summary, dated 02/10/2017. Proposed final loading for Sprint Nextel as per SBA Portal, App #73320, v3.
Authorization:	SBA Communication Corp.	

3. ANALYSIS METHODS & DATA

The analysis was performed in accordance with Telecommunication Industry Association specification TIA-222-G. The tower was modeled using TNX Tower, a 3-D finite element program. TNX Tower is a general-purpose modeling, analysis, and design program created specifically for communication towers using the EIA-222-C, EIA-222-D, TIA/EIA-222-F or TIA-222-G standards. The 3-D model included the tower, with existing appurtenances and all proposed loads.

SITE DATA	
SBA Site Name:	Bozrah
SBA Site Number:	CT01105-S-02
Carrier Site ID:	CT33XC574 / N. Bozrah
City, State:	Bozrah, CT
County:	New London County
Code Wind Load Requirement:	TIA-222-G & IBC 2012 (132 mph ultimate wind speed equivalent to 102 mph basic wind speed)
Wind Load Used:	TIA-222-G Code: <ul style="list-style-type: none"> • Basic wind speed of 102 mph (3 second gust wind speed) • Structure Class II*. • Exposure Category B. • Topographic Category 1. • Crest Height 0.00 ft. • A wind speed of 50 mph is used in combination with ice • Nominal ice thickness of 0.75 in.
Seismic Check:	$S_s=0.170 < 1.0$, thus seismic loading can be ignored as per 2.7.3 of the TIA-222-G Code

*This structural analysis is based upon the tower being classified as a class II; however, if a different classification is required subsequent to the date hereof, the tower classification will be changed to meet such requirement and a new structural analysis will be run.

TOWER DATA	
Tower Type:	Self Support Tower
Height:	195s'
Cross Section:	Triangular
Steel Strength:	Legs – 50 ksi , Braces – 36 ksi & 50 ksi
Type of Foundation:	Mat Foundation

TOWER HISTORY	
Tower Manufacturer / Model:	Pirod Inc./ U-22.0 x 193'
Date of Original Design:	04/01/1999
Previous Modifications:	N/A
Original Design Code Requirements:	TIA/EIA-222-F-1996 85 mph basic wind speed and 0.5" ice with 25% reduced wind speed

4. CONCLUSIONS

RESULT SUMMARY		
MEMBER	% Capacity	Pass/Acceptable
Legs	71.0 %	Pass
Diagonals	87.3 %	Pass
Girts	6.1 %	Pass
Bolt checks	87.3 %	Pass
Anchor Bolts	26.7 %	Pass
Foundation (see attached MathCAD for details)	Bearing (3.3 %)	Pass
	Horizontal shear (8.6 %)	Pass
	Safety against overturning (72.1 %)	Pass
OVERALL TOWER RATING = 87.3 %		

As per the results of the analysis, the existing tower is in code compliance for the new and existing antenna loads.

Maximum tower stress is less than 100%, the acceptable stress ratio making it in code compliance under the TIA-222-G code and 2012 International Building Code adopted by 2016 CSBC (Connecticut State Building Code).

5.

DISCLAIMER

Installation procedures and related loading are not within the scope of this analysis. A contractor experienced in similar work should perform all installation work. The engineering services provided by Allpro Consulting Group, Inc. (ACGI) are limited to the computer analysis and calculations of the structure with the proposed and existing loads. This analysis is considered void if the loading mentioned in this report is changed or is different as installed. It is assumed that the existing structure is properly maintained and is in good condition free of any defects. Scope of this analysis does not include existing connections, except as noted in this report.

ACGI does not make any warranties, expressed or implied in connection with this engineering analysis report and disclaims any liability arising from deficiencies or any existing conditions of the original structure. ACGI will not be responsible for consequential or incidental damages sustained by any parties as a result of any data or conclusions included in this Report. The maximum liability of ACGI pursuant to this report shall be limited to the consulting fee received for the preparation of the report.

6.

ASSUMPTIONS

This analysis was completed based on the following assumptions:

- Tower has been properly maintained.
- Tower erection was in accordance to manufacturer drawings and modification reports.
- Leg flanges have been properly designed by manufacturer to not be a limiting reaction.
- Welds have been properly designed and installed by manufacturer to not be a limiting reaction.
- Foundation data was not provided. It is assumed that the foundation is designed to resist the original tower reactions.
- Foundation does not have structural damage.
- Bolts have been properly tightened according to manufacturer specifications.
- Appurtenance, mount and transmission line sizes and weights are best estimates using the tnxTower database and manufacturer information.

7.

APPURTENANCE LISTING

EXISTING LOAD DESCRIPTION					
<u>ELEV</u> <u>(ft.)</u>	<u>Qty.</u>	<u>Antenna Description</u>	<u>Mount Type &</u> <u>Qty.</u>	<u>TX. LINE (in)</u>	<u>TENANT</u>
195±	9	EMS RR90-17-02DP	(1) Low Profile Platform	(12) 1-5/8"	T-Mobile
182±	6	CCI HPA-65R-BUU-H8 Antennas	(3) 12.5' TFrames (Commscope P/N: MTC 3615)	(12) 1-5/8" (2) 5/8" Fiber (4) 3/4" DC Power	AT&T
	3	Powerwave 7770 Antennas			
	6	Powerwave LGP21401 TMAs			
	6	Ericsson RRUS 11			
	3	Ericsson RRUS 12			
	3	Ericsson RRUS A2			
	3	Ericsson RRUS 32			
	3	Polyphases 1000860			
	6	Powerwave LGP21903			
2	Raycap DC6-48-60-18-8F				
175±	6	Decibel DB908h90e-m Antennas	(3) T -Frames	(6) 1-5/8"	Sprint Nextel
162±	6	Commscope HBXX-6517DS-A2M	(3) T -Frames	(12) 1-5/8" Coax (2) 1-5/8" Fiber	Verizon
	3	Commscope LNX-6514DS-A1M			
	3	Amphenol QUAD656C0000x			
	3	Alcatel Lucent RRH2x60-AWS			
	3	Alcatel Lucent RRH2x60-1900			
	3	Alcatel Lucent RRH2x60-700			
	6	RFS FD9R6004/2CL-3CL			
2	RFS DB-T1-6Z-8AB-0Z				
100±	1	Lucent KS24019-L112A GPS	Direct Mount	(1) GPS Line	
30±	2	Andrew PC1N0F-0190B-002ME911 Omnis	Direct Mount	(2) 1/2"	T-Mobile

FINAL SPRINT NEXTEL LOAD DESCRIPTION					
<u>ELEV</u> <u>(ft.)</u>	<u>Qty.</u>	<u>Antenna Description</u>	<u>Mount Type &</u> <u>Qty.</u>	<u>TX. LINE (in)</u>	<u>TENANT</u>
175±	3	RFS APXVTM14-C-I20 Antennas	(3) T –Frames (3) Sitepro SFS-H-L	(4) 1-1/4" Fiber	Sprint Nextel
	3	Commscope NNVV-65B-R4 Antenna			
	3	ALU 1900 MHz RRH			
	6	ALU 800 MHz RRH			
	3	ALU TD-RRH 8X20-25			

1. ACGI should be notified of any discrepancies found in the data listed in this report.
2. Notify ACGI if any potential physical and other interference with existing antennas for a redesign.

8. SUMMARY OF WORKING PERCENTAGE OF STRUCTURAL COMPONENTS

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
T1	193 - 185	Leg	2	1	-6.21	111.48	5.6	Pass	
		Diagonal	1	11	-1.28	13.28	9.6	Pass	
		Horizontal	7/8	23	-0.15	3.94	3.9	Pass	
		Top Girt	1 1/4	5	-0.62	16.42	3.8	Pass	
T2	185 - 170	Bottom Girt	1 1/4	8	-0.69	16.42	4.2	Pass	
		Leg	2	32	-43.07	111.48	38.6	Pass	
		Diagonal	1	44	-5.90	13.28	44.4	Pass	
		Horizontal	7/8	48	-0.34	3.94	8.7	Pass	
		Top Girt	1 1/4	33	-0.23	16.42	1.4	Pass	
		Bottom Girt	1 1/4	36	-1.00	16.42	6.1	Pass	
		Mid Girt	1 1/4	39	-0.36	16.42	2.2	Pass	
T3	170 - 160	Leg	Pirod 105244	84	-52.85	142.49	51.2	Pass	
		Diagonal	L2 1/2x2 1/2x3/16	87	-9.87	13.56	72.8	Pass	
T4	160 - 140	Leg	Pirod 105217	93	-107.86	214.86	83.8 (b)	Pass	
		Diagonal	L3x3x3/16	102	-10.20	18.18	50.2	Pass	
T5	140 - 120	Leg	Pirod 105217	108	-152.48	214.86	56.1	Pass	
		Diagonal	L3x3x3/16	111	-8.30	14.96	71.0	Pass	
T6	120 - 100	Leg	Pirod 105218	123	-192.63	300.68	55.5	Pass	
		Diagonal	L3x3x5/16	126	-8.18	19.32	71.1 (b)	Pass	
T7	100 - 80	Leg	Pirod 105219	138	-230.18	399.87	42.3	Pass	
		Diagonal	L3x3x5/16	141	-8.26	15.76	57.6	Pass	
T8	80 - 60	Leg	Pirod 105219	153	-265.76	399.87	52.4	Pass	
		Diagonal	L3 1/2x3 1/2x5/16	158	-8.81	20.74	66.5	Pass	
T9	60 - 40	Leg	Pirod 105220	168	-300.52	512.38	42.5	Pass	
		Diagonal	L3 1/2x3 1/2x5/16	173	-8.92	17.15	58.7	Pass	
T10	40 - 20	Leg	Pirod 105220	183	-336.18	512.38	60.3 (b)	Pass	
		Diagonal	L3 1/2x3 1/2x5/16	194	-10.63	15.65	52.0	Pass	
T11	20 - 0	Leg	Pirod 112738	198	-349.82	613.14	65.6	Pass	
		Diagonal	2L3 1/2x3 1/2x5/16x1	203	-19.22	44.46	67.0 (b)	Pass	
							Summary		
							Leg (T5)	71.0	Pass
							Diagonal (T4)	87.3	Pass
							Horizontal (T2)	8.7	Pass
							Top Girt (T1)	3.8	Pass
							Bottom Girt (T2)	6.1	Pass
							Mid Girt (T2)	2.2	Pass
							Bolt Checks	87.3	Pass
							RATING =	87.3	Pass

APPENDIX



Tower Data

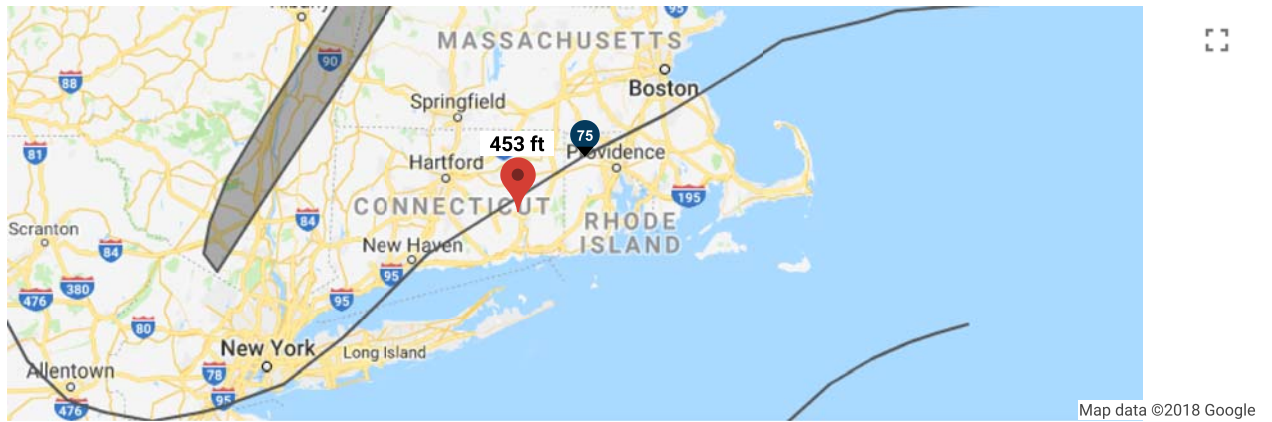
⚠ This is a beta release of the new ATC Hazards by Location website. Please contact us with feedback.

ATC Hazards by Location

Search Information

Coordinates: 41.552517, -72.150708
Timestamp: 2018-05-25T21:18:21.618Z
Hazard Type: Wind

Map Results



Text Results

ASCE 7-16

MRI 10-Year	76 mph
MRI 25-Year	86 mph
MRI 50-Year	96 mph
MRI 100-Year	101 mph
Risk Category I	114 mph
Risk Category II	124 mph
Risk Category III	⚠ 133 mph
<p>If the structure under consideration is a healthcare facility, you are in a wind-borne debris region. If other occupancy, use the Risk Category II basic wind speed contours to determine if you are in a wind-borne debris region.</p>	
Risk Category IV	⚠ 137 mph
<p>You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.</p>	

ASCE 7-10

MRI 10-Year	79 mph
MRI 25-Year	89 mph
MRI 50-Year	98 mph
MRI 100-Year	106 mph
Risk Category I	121 mph

Risk Category II ⚠ 132 mph

You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.

Risk Category III-IV ⚠ 142 mph

If the structure under consideration is a healthcare facility, you are in a wind-borne debris region. If other occupancy, use the Risk Category II basic wind speed contours to determine if you are in a wind-borne debris region.

ASCE 7-05

ASCE 7-05 Wind Speed ⚠ 112 mph

You are in a wind-borne debris region if you are also within 1 mile of the coastal mean high water line.

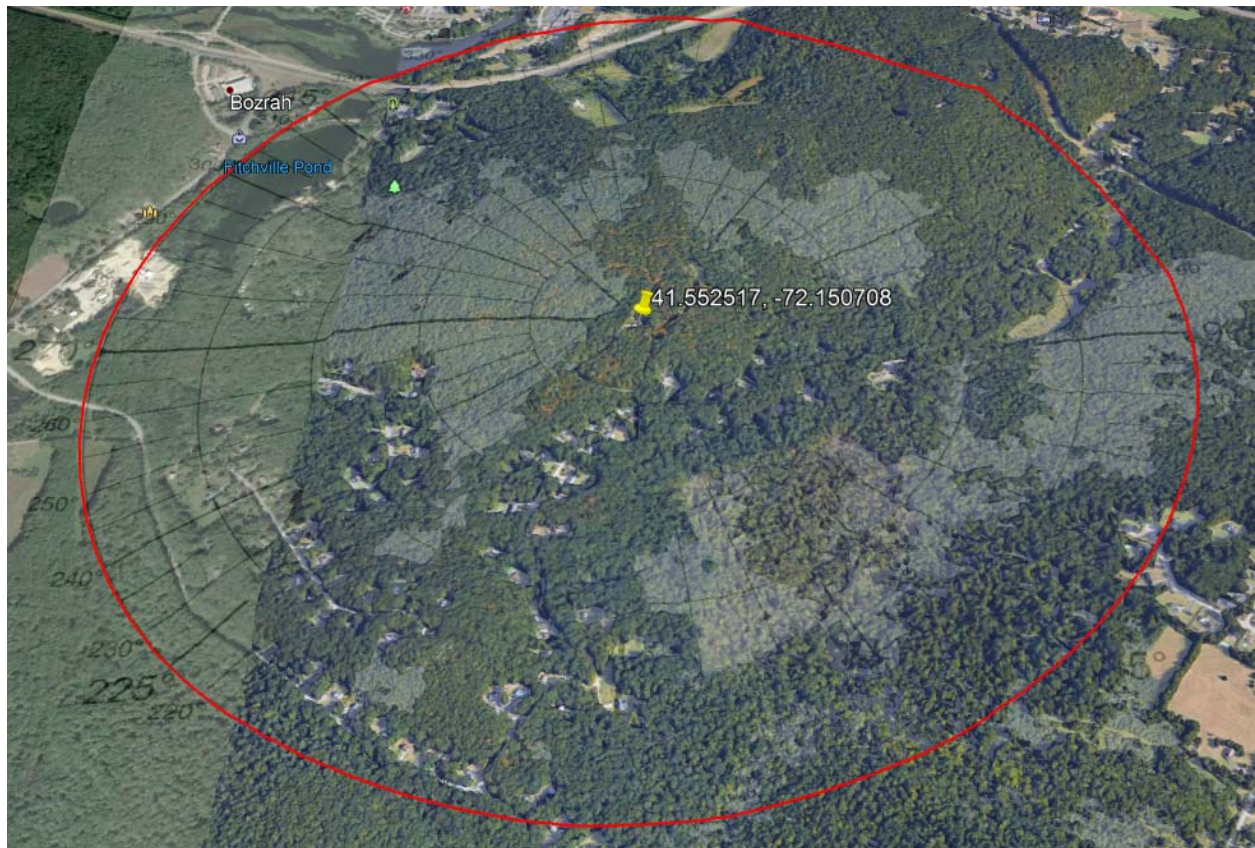
The results indicated here DO NOT reflect any state or local amendments to the values or any delineation lines made during the building code adoption process. Users should confirm any output obtained from this tool with the local Authority Having Jurisdiction before proceeding with design.

Disclaimer

Hazard loads are interpolated from data provided in ASCE 7 and rounded up to the nearest whole integer. Per ASCE 7, islands and coastal areas outside the last contour should use the last wind speed contour of the coastal area – in some cases, this website will extrapolate past the last wind speed contour and therefore, provide a wind speed that is slightly higher. NOTE: For queries near wind-borne debris region boundaries, the resulting determination is sensitive to rounding which may affect whether or not it is considered to be within a wind-borne debris region.

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CT01105-S-02 Bozrah



Exposure Category B.
Topographic Category 1.

USGS Design Maps Summary Report

User-Specified Input

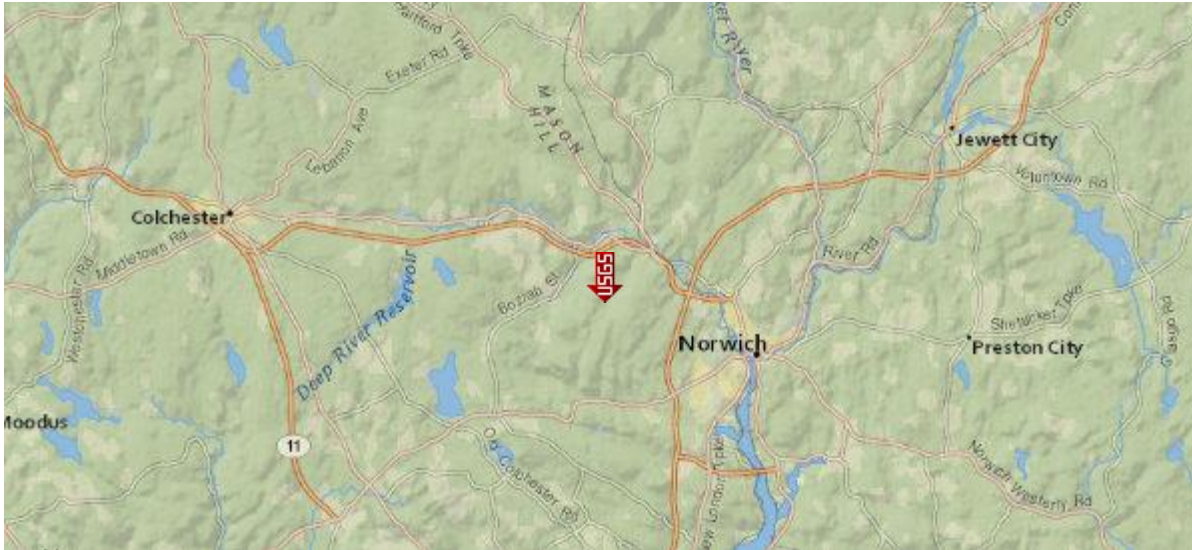
Report Title CT01105-S-02 BOZRA
Fri May 25, 2018 21:35:46 UTC

Building Code Reference Document 2012/2015 International Building Code
(which utilizes USGS hazard data available in 2008)

Site Coordinates 41.55252°N, 72.15071°W

Site Soil Classification Site Class D – “Stiff Soil”

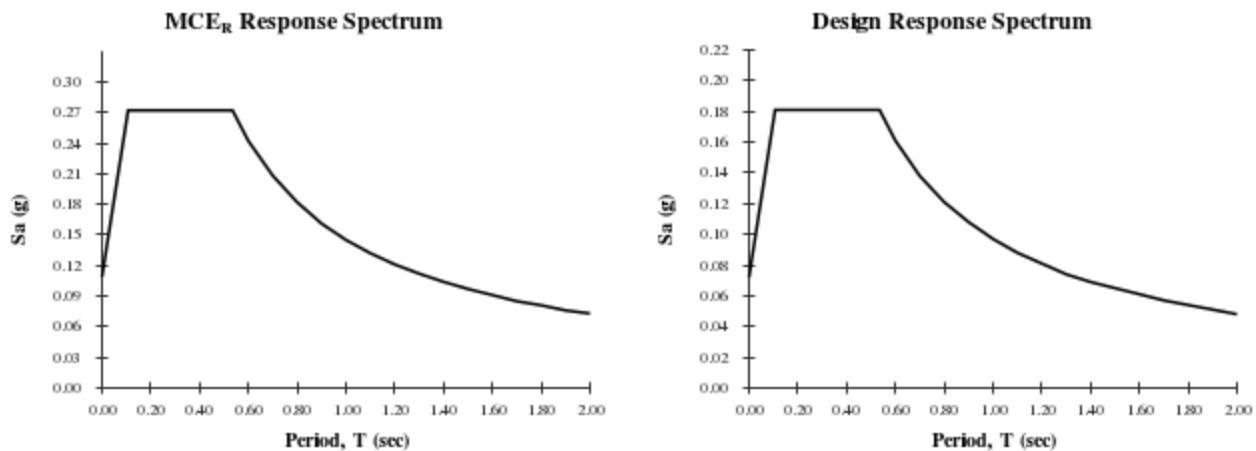
Risk Category I/II/III



USGS-Provided Output

$$\begin{array}{lll} S_S = 0.170 \text{ g} & S_{MS} = 0.272 \text{ g} & S_{DS} = 0.181 \text{ g} \\ S_1 = 0.061 \text{ g} & S_{M1} = 0.145 \text{ g} & S_{D1} = 0.097 \text{ g} \end{array}$$

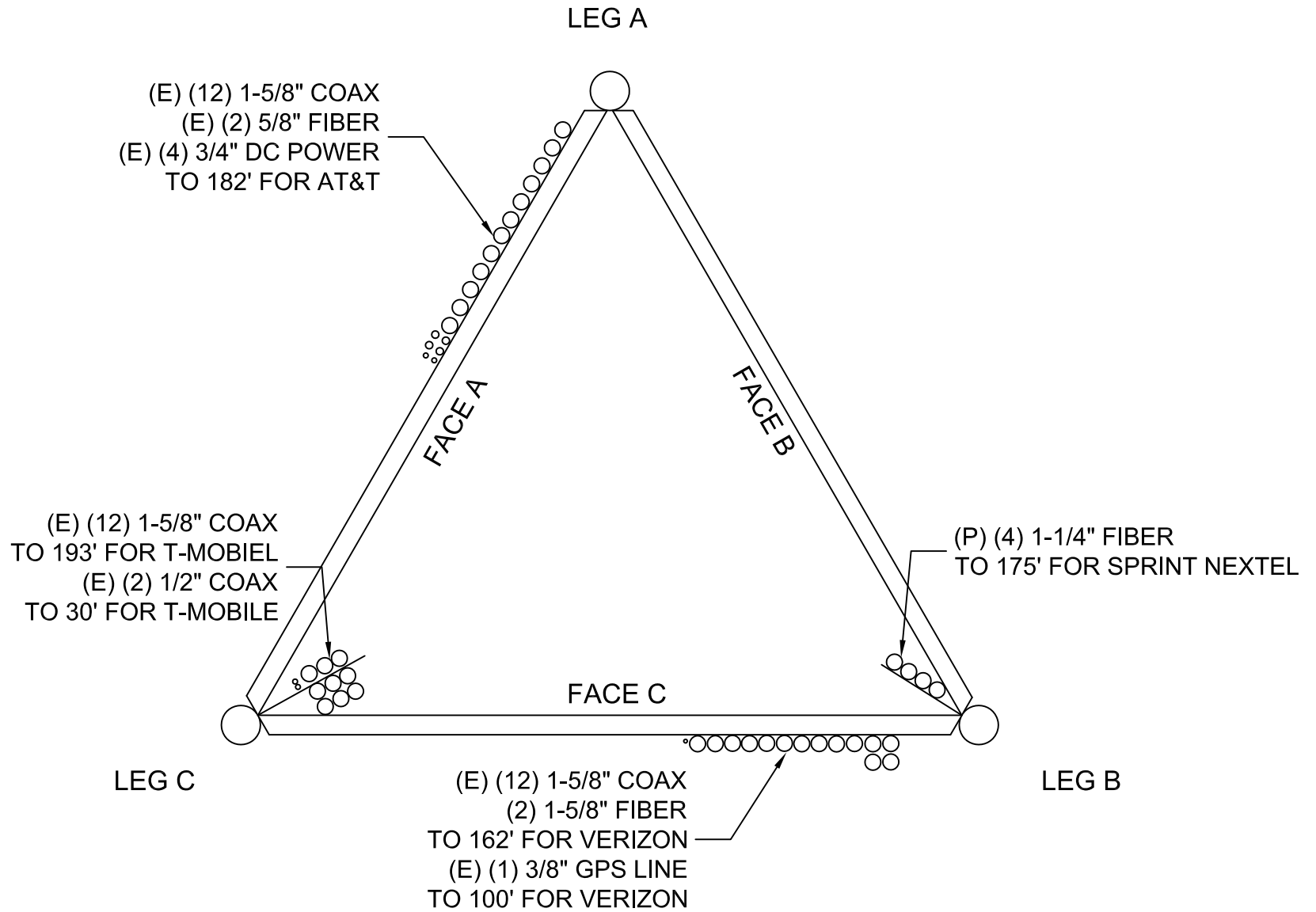
For information on how the S_S and S_1 values above have been calculated from probabilistic (risk-targeted) and deterministic ground motions in the direction of maximum horizontal response, please return to the application and select the “2009 NEHRP” building code reference document.



Although this information is a product of the U.S. Geological Survey, we provide no warranty, expressed or implied, as to the accuracy of the data contained therein. This tool is not a substitute for technical subject-matter knowledge.



COAX LAYOUT

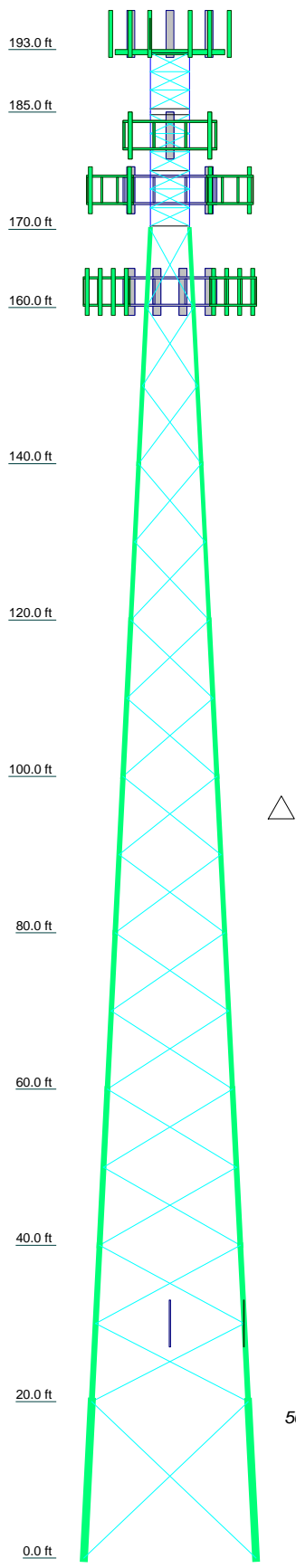


COAX LAYOUT

N.T.S.

TOWER ELEVATION DRAWING

Section	T1	T2	T3	T4	T5	T6	T7	T8	T9	T10	T11	5
Legs		SR 2	A		Pirod 105217	Pirod 105218	Pirod 105219	Pirod 105220			Pirod 112738	
Leg Grade		SR 1	B		L3x3x5/16	A572-50 L3x3x5/16	A36	L3 1/2x3 1/2x5/16			2L3 1/2x3 1/2x5/16x1	
Diagonals		A572-50 SR 1 1/4					N.A.					
Top Girts		SR 1 1/4					N.A.					
Mid Girts		SR 1 1/4					N.A.					
Bottom Girts		SR 1 1/4					N.A.					
Horizontals		SR 7/8					N.A.					
Face Width (ft)	22		6		8	10	12	14	16	18	20	22
# Panels @ (ft)			1.1		2.4	3.4	4.1	4.5	5.1	5.3	7.7	
Weight (K)	38.0		0.7		1.3	2.5	4.1	4.5	5.1	5.3	7.7	



SYMBOL LIST

MARK	SIZE	MARK	SIZE
A	Pirod 105244	B	L2 1/2x2 1/2x3/16

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

TOWER DESIGN NOTES

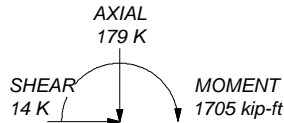
1. Tower is located in New London County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 102 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 87.3%

ALL REACTIONS
ARE FACTORED

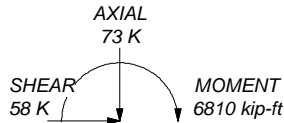
MAX. CORNER REACTIONS AT BASE:

DOWN: 375 K
SHEAR: 43 K

UPLIFT: -321 K
SHEAR: 37 K



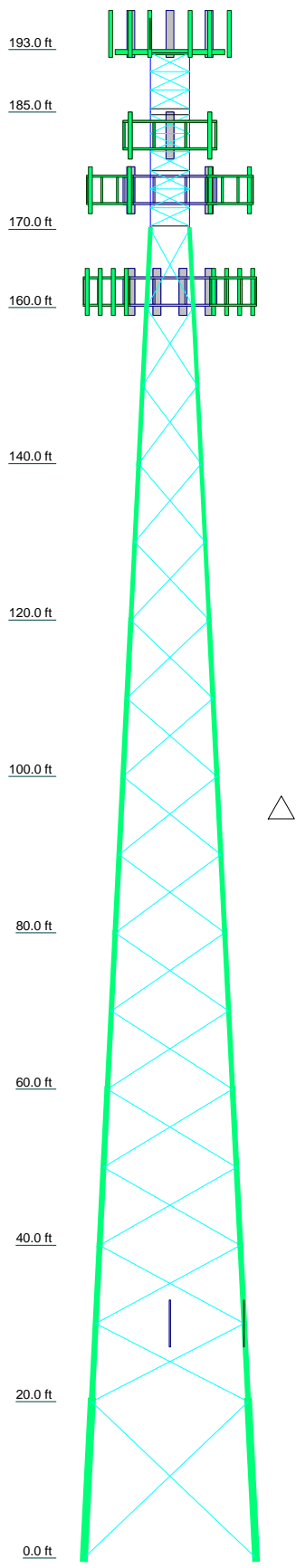
TORQUE 7 kip-ft
50 mph WIND - 0.7500 in ICE



TORQUE 33 kip-ft
REACTIONS - 102 mph WIND

Allpro Consultants group inc		Job: 18-3611	
9221 lyndon B johson Freeway. Suite 204		Project: CT01105-S-02 BOZRAH	
Dalls Tx. 75243		Client: SBA	Drawn by: bakech
Phone: 972 231 8893		Code: TIA-222-G	Date: 05/29/18
FAX: 866 364 8375		Path:	Scale: NTS
			Dwg No. E-1

Section	T11	T10	T9	T8	T7	T6	T5	T4	T3	T2	T1
Legs	Pirod 112738	Pirod 105220	Pirod 105219	Pirod 105218	Pirod 105217				A	SR 2	
Leg Grade	2L3 1/2x3 1/2x5/16x1	L3 1/2x3 1/2x5/16	A36	A572-50	L3x3x5/16				B	SR 1	
Diagonals										A572-50	
Top Girts										SR 1 1/4	
Mid Girts										SR 1 1/4	N.A.
Bottom Girts										SR 1 1/4	
Horizontals										SR 7/8	
Face Width (ft)	20	18	16	14	12	10	8	6			5
# Panels @ (ft)	1 @ 20				15 @ 10					9 @ 2.375	
Weight (K)	38.0	5.3	5.1	4.5	4.1	3.4	2.5	2.4	1.1	1.3	0.7



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
(3) RR90-17-02DP w/ Mount Pipe	193	NNVV-65B-R4 Antenna	175
(3) RR90-17-02DP w/ Mount Pipe	193	NNVV-65B-R4 Antenna	175
(3) RR90-17-02DP w/ Mount Pipe	193	(2) 800 MHz RRRH	175
(1) Low Profile Platform	193	(2) 800 MHz RRRH	175
Lightning Rod	193	(2) 800 MHz RRRH	175
Powerwave 7770 w/ Mount Pipe	182	1900 MHz RRRH	175
Powerwave 7770 w/ Mount Pipe	182	1900 MHz RRRH	175
(2) HPA-65R-BUU-H8 w/ Mount Pipe	182	1900 MHz RRRH	175
(2) HPA-65R-BUU-H8 w/ Mount Pipe	182	TD-RRH8x20-25	175
(2) HPA-65R-BUU-H8 w/ Mount Pipe	182	TD-RRH8x20-25	175
(2) LGP21401	182	TD-RRH8x20-25	175
(2) LGP21401	182	(2) FD9R6004/2C-3L	162
(2) LGP21401	182	Empty Mount Pipe	162
(2) LGP21903 Diplexer	182	Empty Mount Pipe	162
(2) LGP21903 Diplexer	182	Empty Mount Pipe	162
(2) LGP21903 Diplexer	182	RRH2x60-AWS	162
(2) RRUS 11	182	RRH2x60-AWS	162
(2) RRUS 11	182	RRH2x60-AWS	162
(2) RRUS 11	182	RRH2x60-1900	162
RRUS 12	182	RRH2x60-1900	162
RRUS 12	182	RRH2x60-1900	162
RRUS 12	182	RRH2x60-700	162
(2) RRUS A2	182	RRH2x60-700	162
RRUS A2	182	RRH2x60-700	162
RRUS A2	182	(3) T-Frames	162
RRUS-32	182	(2) HBXX-6517DS-A2M w/ Mount Pipe	162
RRUS-32	182	(2) HBXX-6517DS-A2M w/ Mount Pipe	162
RRUS-32	182	(2) HBXX-6517DS-A2M w/ Mount Pipe	162
1000860	182	LNx-6514DS-A1M	162
1000860	182	LNx-6514DS-A1M	162
1000860	182	LNx-6514DS-A1M	162
DC6-48-60-18-8F	182	QUAD656C0000x	162
DC6-48-60-18-8F	182	QUAD656C0000x	162
(3) 12.5' T-Frames (Commscope P/N: MTC3615)	182	QUAD656C0000x	162
Powerwave 7770 w/ Mount Pipe	182	DB-T1-6Z-8AB-OZ	162
Modified T-Frames (3)	175	DB-T1-6Z-8AB-OZ	162
RFS APXVSPP18-C-A20	175	(2) FD9R6004/2C-3L	162
RFS APXVSPP18-C-A20	175	(2) FD9R6004/2C-3L	162
RFS APXVSPP18-C-A20	175	KS24019-L112A	100
RFS APXVSPP18-C-A20	175	PC1N0F-0190B-002M	30
NNVV-65B-R4 Antenna	175	PC1N0F-0190B-002M	30

SYMBOL LIST

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A	Pirod 105244	B	L2 1/2x2 1/2x3/16

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6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft

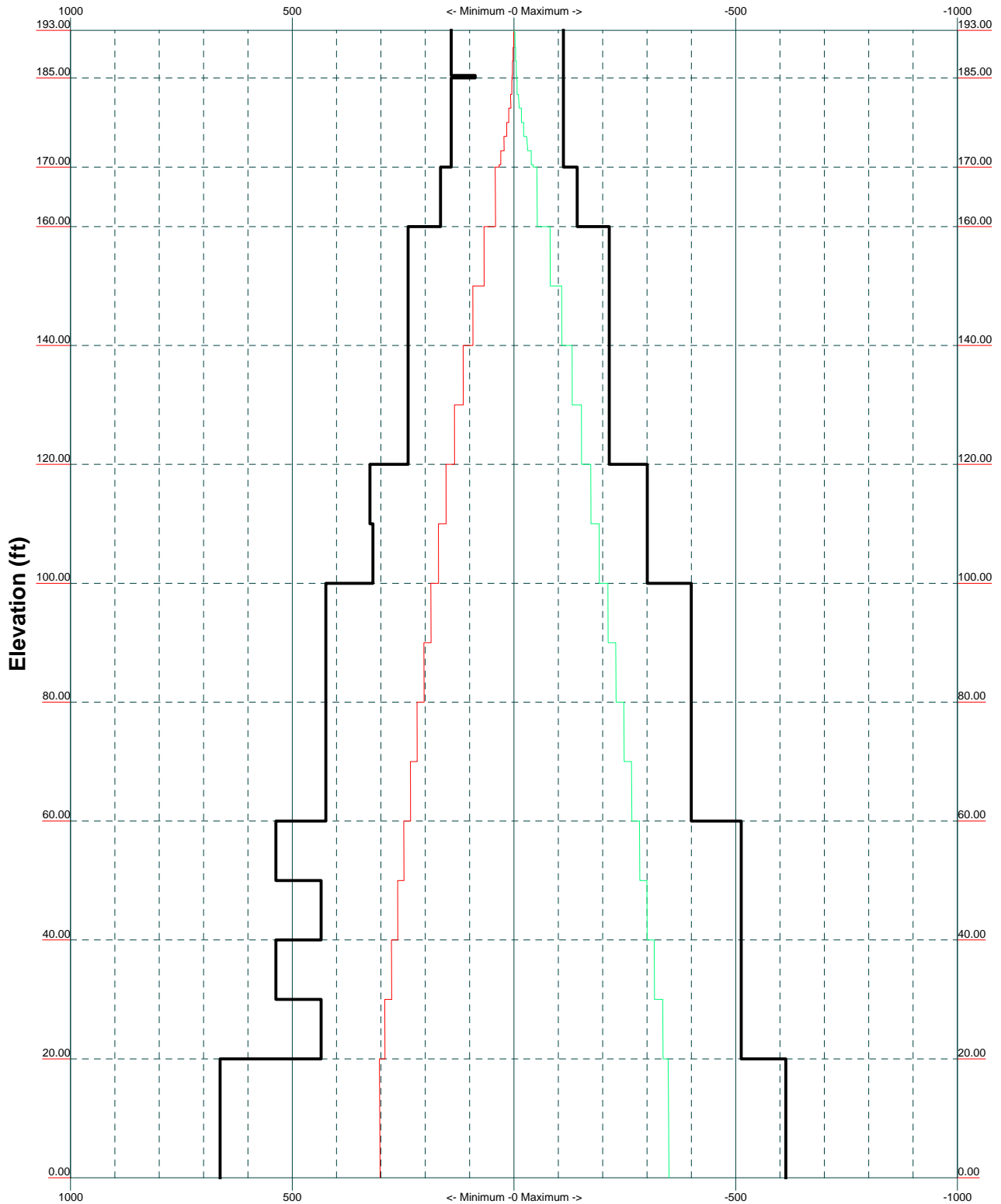
Allpro Consultants group inc		Job: 18-3611	
9221 lyndon B johson Freeway. Suite 204		Project: CT01105-S-02 BOZRAH	
Dalls Tx. 75243		Client: SBA	Drawn by: bakech
Phone: 972 231 8893		Code: TIA-222-G	Date: 05/29/18
FAX: 866 364 8375		Path:	Scale: NTS
			Dwg No. E-1



MISCELLANEOUS PLOTS

TIA-222-G - 102 mph/50 mph 0.7500 in Ice Exposure B

Leg Capacity ——— Leg Compression (K)



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			Project: CT01105-S-02 BOZRAH		
Client: SBA		Drawn by: bakech		App'd:	
Code: TIA-222-G		Date: 05/25/18		Scale: NTS	
Path:			Dwg No. E-3		

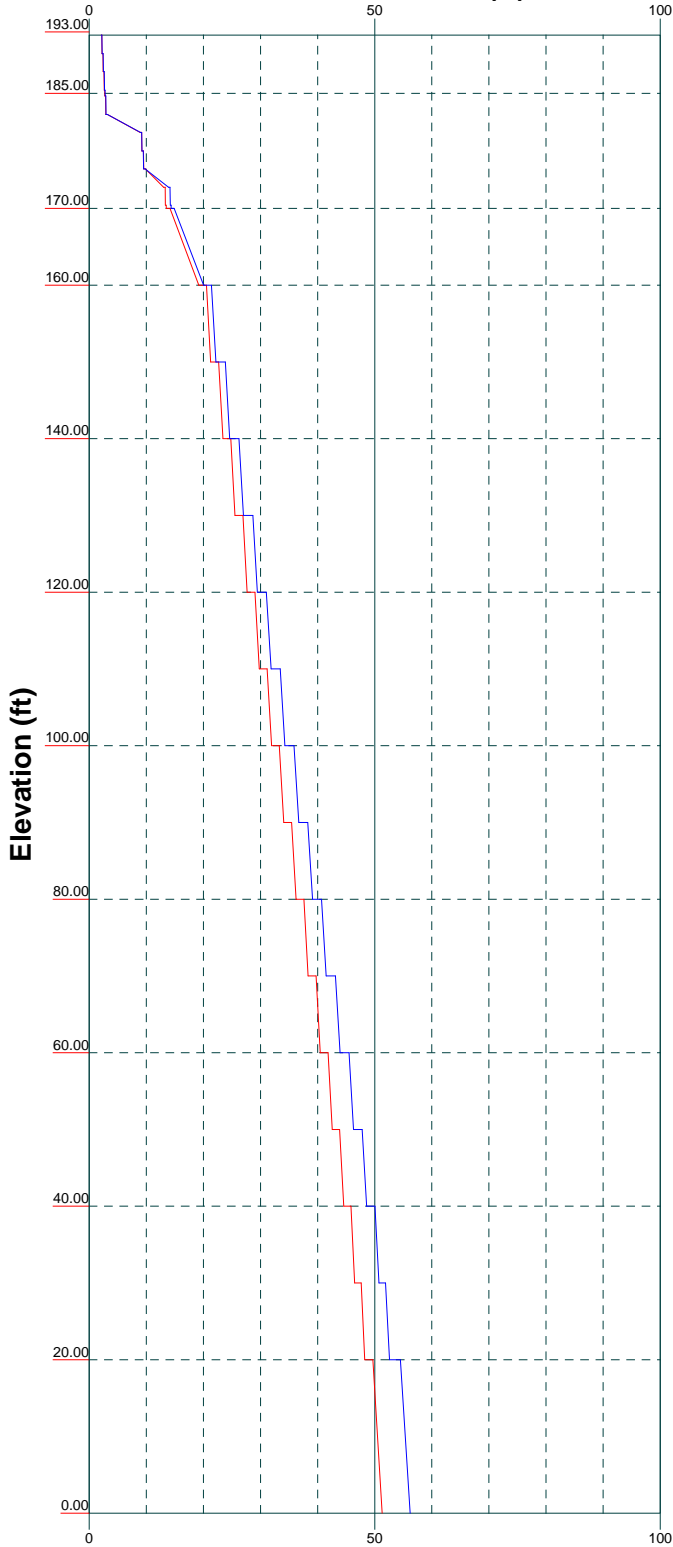
Vx

Vz

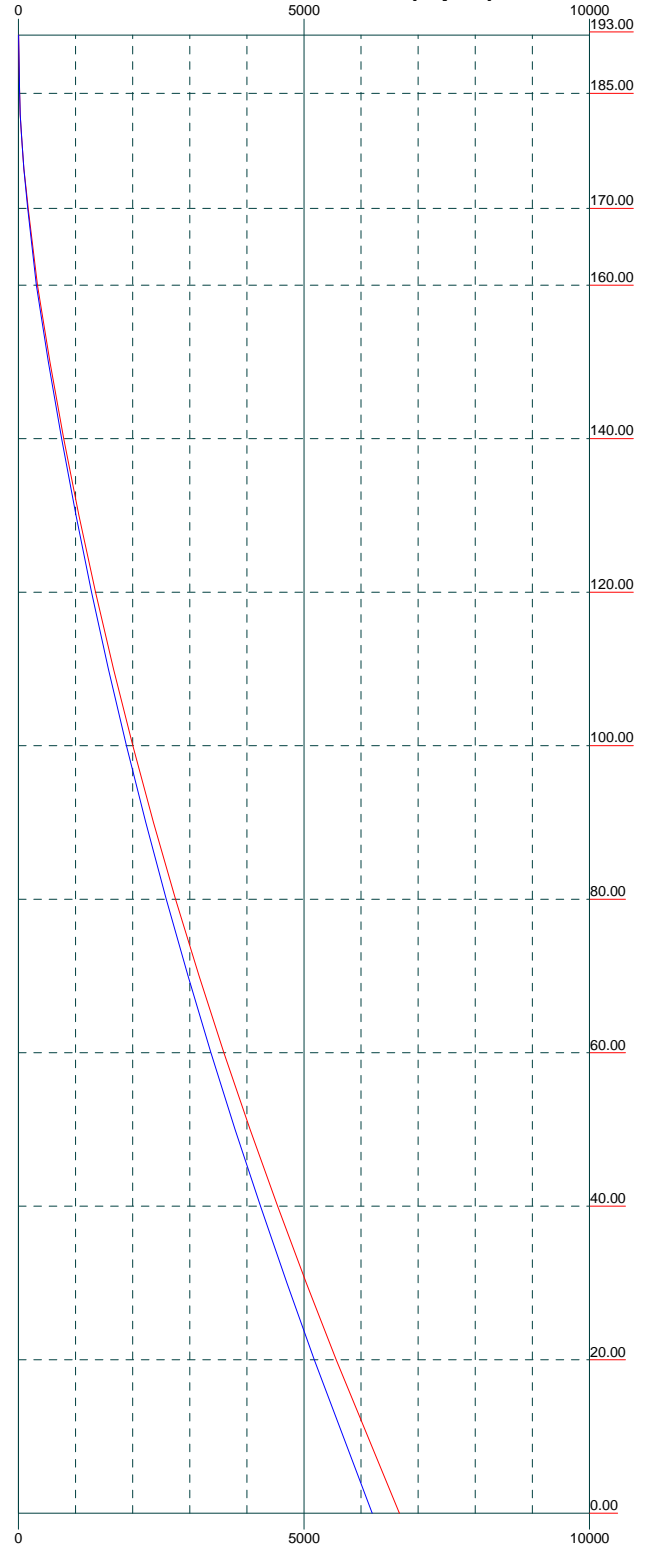
Mx

Mz

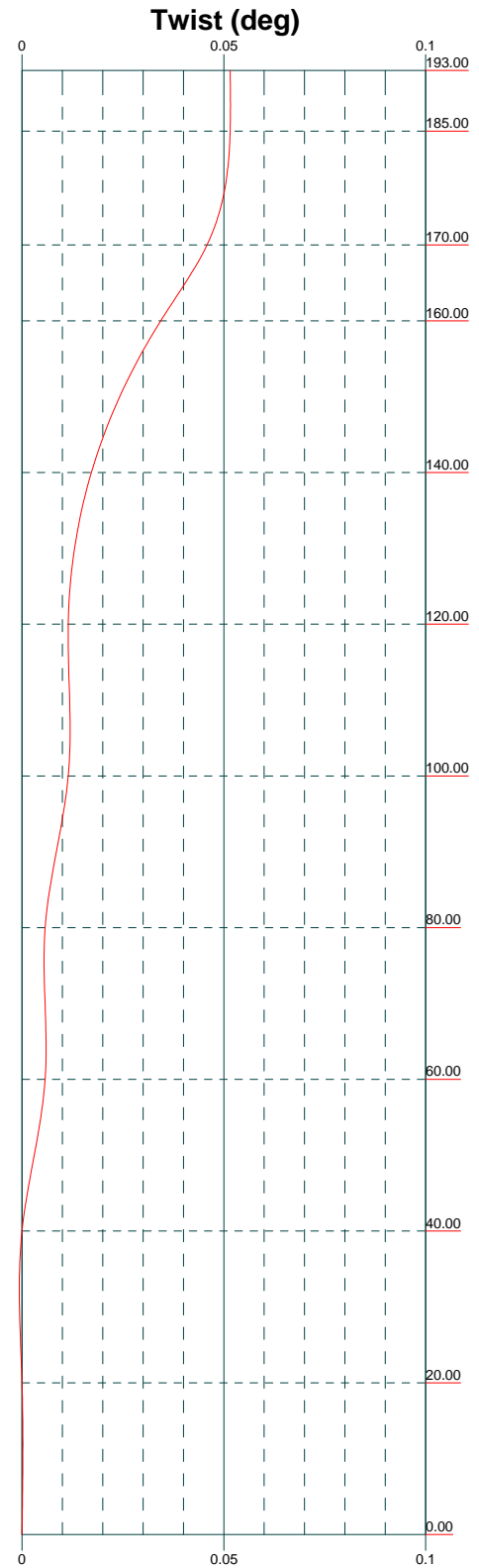
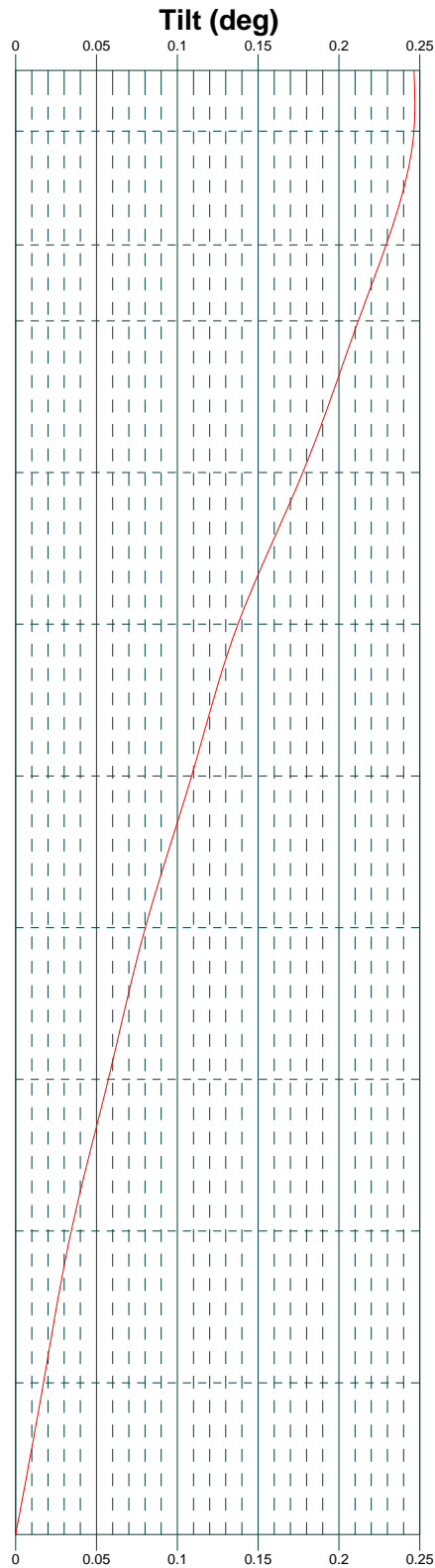
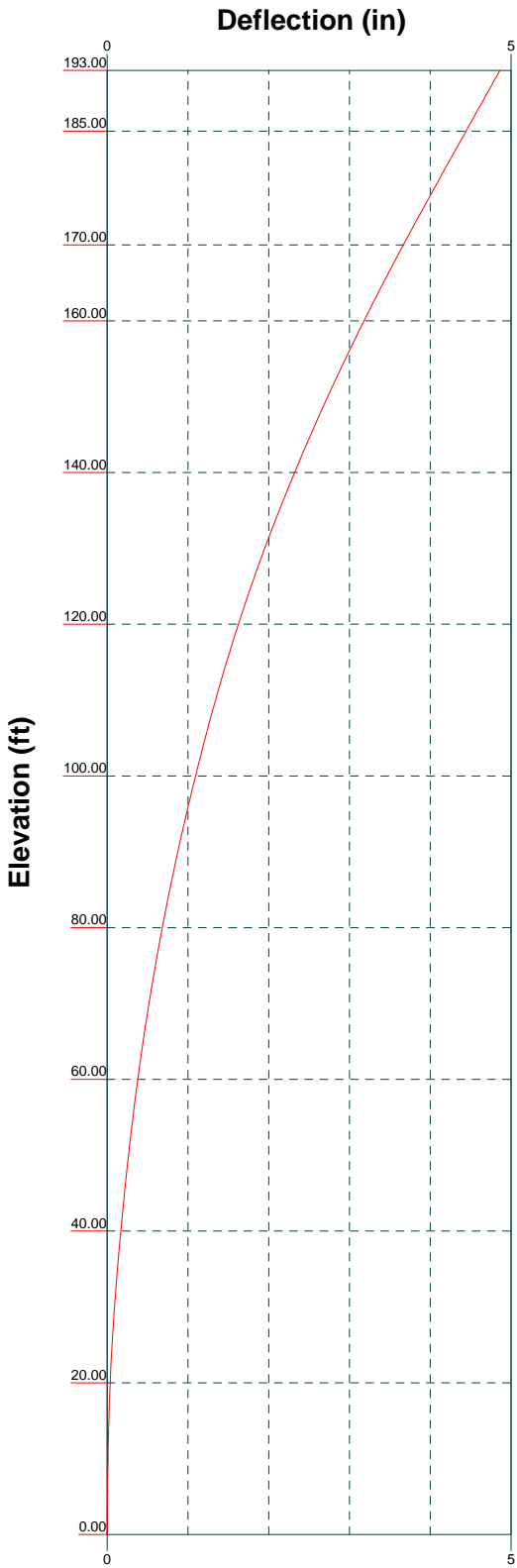
Global Mast Shear (K)



Global Mast Moment (kip-ft)



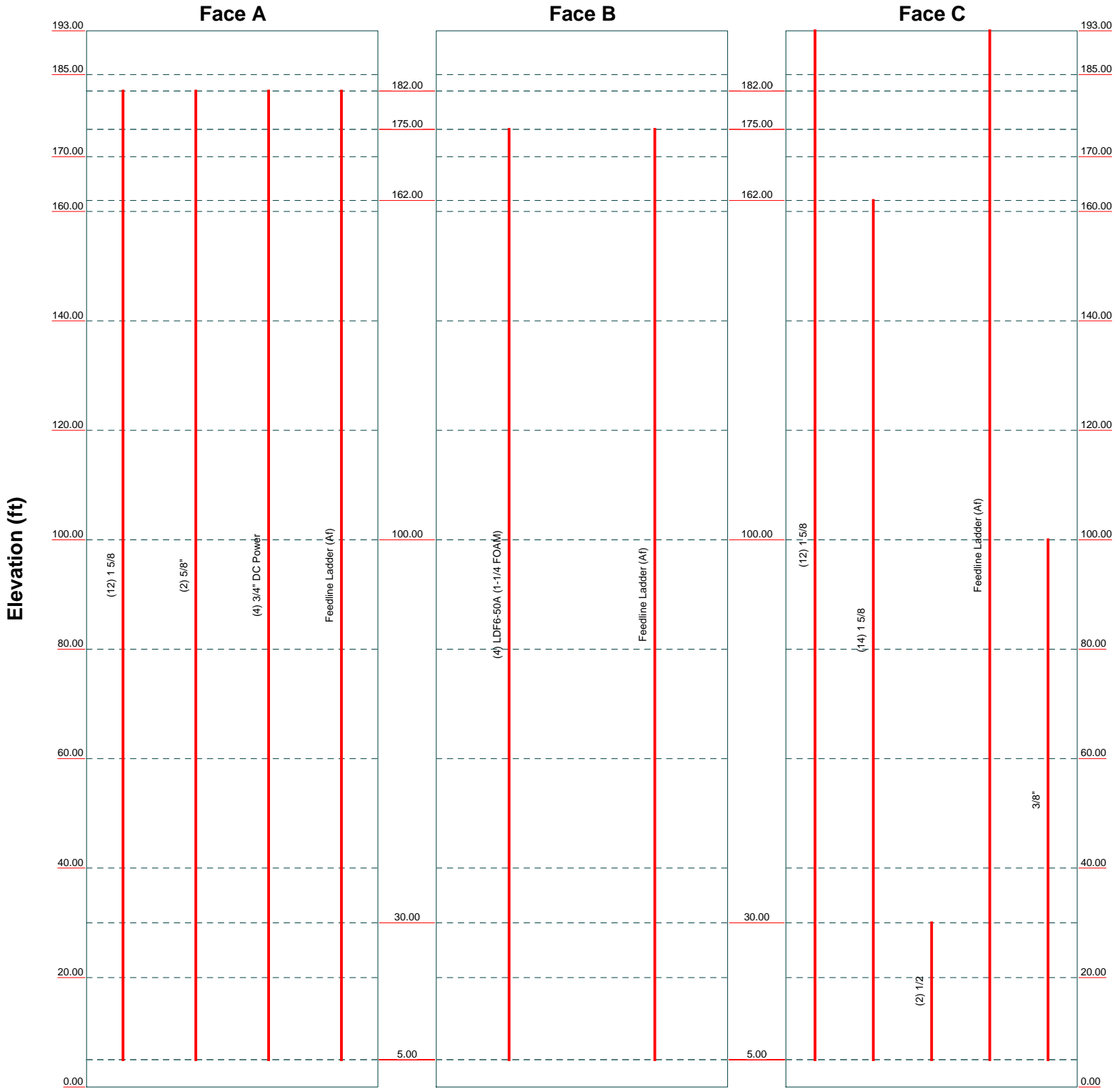
<p>Allpro Consultants group inc 9221 lyndon B Johnson Freeway, Suite 204 Dalls Tx. 75243 Phone: 972 231 8893 FAX: 866 364 8375</p>		<p>Job: 18-3611</p>	
		<p>Project: CT01105-S-02 BOZRAH</p>	
<p>Client: SBA</p>	<p>Drawn by: bakech</p>	<p>App'd:</p>	
<p>Code: TIA-222-G</p>	<p>Date: 05/25/18</p>	<p>Scale: NTS</p>	
<p>Path:</p>	<p>Dwg No. E-4</p>		



<p>Allpro Consultants group inc 9221 lyndon B johson Freeway. Suite 204 Dalls Tx. 75243 Phone: 972 231 8893 FAX: 866 364 8375</p>			Job: 18-3611		
			Project: CT01105-S-02 BOZRAH		
Client: SBA		Drawn by: bakech		App'd:	
Code: TIA-222-G		Date: 05/25/18		Scale: NTS	
Path:				Dwg No. E-5	

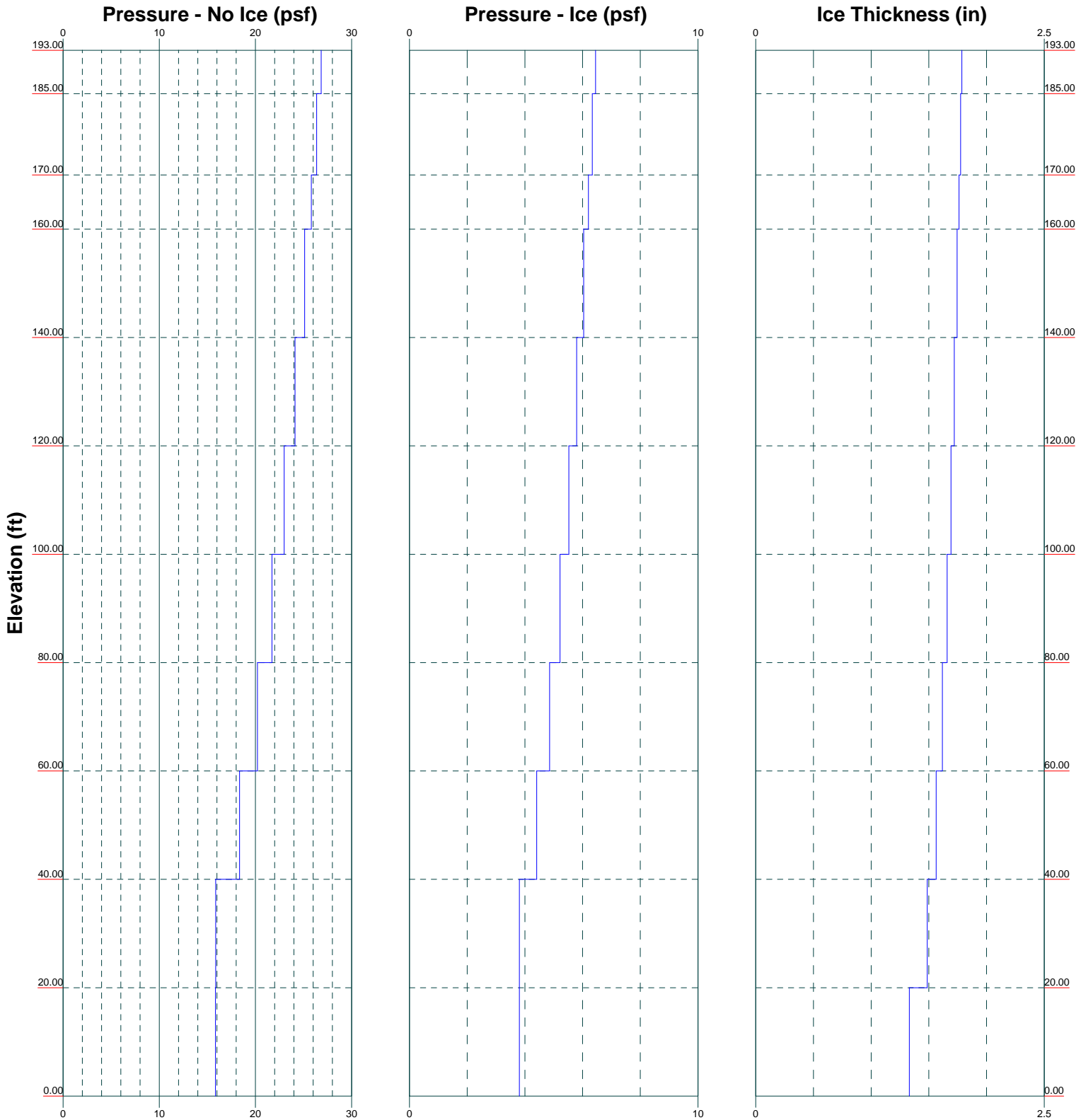
Feed Line Distribution Chart 0' - 193'

— Round
 — Flat
 — App In Face
 — App Out Face
 — Truss Leg



Allpro Consultants group inc		Job: 18-3611	
9221 lyndon B Johnson Freeway, Suite 204		Project: CT01105-S-02 BOZRAH	
Dalls Tx. 75243		Client: SBA	Drawn by: bakech
Phone: 972 231 8893		Code: TIA-222-G	Date: 05/25/18
FAX: 866 364 8375		Path:	Scale: NTS
			Dwg No. E-7

Wind Pressures and Ice Thickness
TIA-222-G - 102 mph/50 mph 0.7500 in Ice Exposure B



Allpro Consultants group inc		
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Dalls Tx. 75243		
Phone: 972 231 8893		
FAX: 866 364 8375		
Job: 18-3611	Project: CT01105-S-02 BOZRAH	
Client: SBA	Drawn by: bakech	App'd:
Code: TIA-222-G	Date: 05/25/18	Scale: NTS
Path:		Dwg No. E-9

TNX TOWER CALCULATION PRINTOUT

<p style="text-align: center;">tnxTower</p> <p><i>Allpro Consultants group inc</i> 9221 lyndon B johson Freeway. Suite 204 Dalls Tx. 75243 Phone: 972 231 8893 FAX: 866 364 8375</p>	Job	18-3611	Page	1 of 26	
	Project	CT01105-S-02 BOZRAH		Date	16:18:49 05/29/18
	Client	SBA		Designed by	bakech

Tower Input Data

The main tower is a 3x free standing tower with an overall height of 193.00 ft above the ground line.

The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 5.00 ft at the top and 22.00 ft at the base.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in New London County, Connecticut.

ASCE 7-10 Wind Data is used (wind speeds converted to nominal values).

Basic wind speed of 102 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.00 ft.

Nominal ice thickness of 0.7500 in.

Ice thickness is considered to increase with height.

Ice density of 56 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50 °F.

Deflections calculated using a wind speed of 60 mph.

A non-linear (P-delta) analysis was used.

Pressures are calculated at each section.

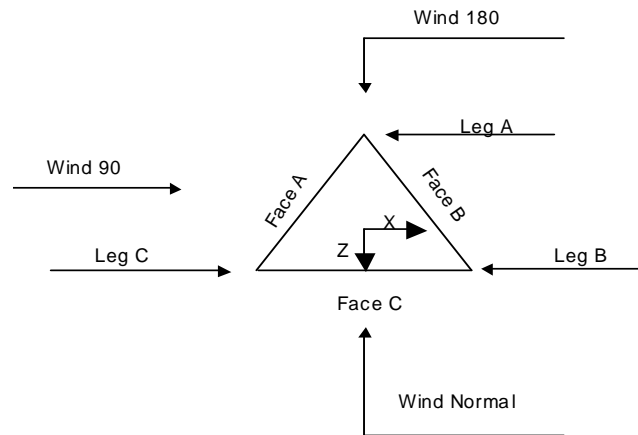
Stress ratio used in tower member design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

<ul style="list-style-type: none"> Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification √ Use Code Stress Ratios √ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile √ Include Bolts In Member Capacity Leg Bolts Are At Top Of Section √ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric 	<ul style="list-style-type: none"> Distribute Leg Loads As Uniform Assume Legs Pinned √ Assume Rigid Index Plate √ Use Clear Spans For Wind Area √ Use Clear Spans For KL/r Retension Guys To Initial Tension √ Bypass Mast Stability Checks √ Use Azimuth Dish Coefficients √ Project Wind Area of Appurt. Autocalc Torque Arm Areas Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder 	<ul style="list-style-type: none"> Use ASCE 10 X-Brace Ly Rules √ Calculate Redundant Bracing Forces Ignore Redundant Members in FEA √ SR Leg Bolts Resist Compression √ All Leg Panels Have Same Allowable Offset Girt At Foundation √ Consider Feed Line Torque √ Include Angle Block Shear Check Use TIA-222-G Bracing Resist. Exemption Use TIA-222-G Tension Splice Exemption <li style="text-align: center;">Poles Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are Known
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Triangular Tower

Tower Section Geometry

Tower Section	Tower Elevation	Assembly Database	Description	Section Width	Number of Sections	Section Length
	<i>ft</i>			<i>ft</i>		<i>ft</i>
T1	193.00-185.00			5.00	1	8.00
T2	185.00-170.00			5.00	1	15.00
T3	170.00-160.00			5.00	1	10.00
T4	160.00-140.00			6.00	1	20.00
T5	140.00-120.00			8.00	1	20.00
T6	120.00-100.00			10.00	1	20.00
T7	100.00-80.00			12.00	1	20.00
T8	80.00-60.00			14.00	1	20.00
T9	60.00-40.00			16.00	1	20.00
T10	40.00-20.00			18.00	1	20.00
T11	20.00-0.00			20.00	1	20.00

Tower Section Geometry (cont'd)

Tower Section	Tower Elevation	Diagonal Spacing	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset	Bottom Girt Offset
	<i>ft</i>	<i>ft</i>				<i>in</i>	<i>in</i>
T1	193.00-185.00	2.38	X Brace	No	Steps	5.2500	5.2500
T2	185.00-170.00	2.38	X Brace	No	Steps	4.5000	4.5000
T3	170.00-160.00	10.00	X Brace	No	No	0.0000	0.0000
T4	160.00-140.00	10.00	X Brace	No	No	0.0000	0.0000

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Tower Section	Tower Elevation ft	Diagonal Spacing ft	Bracing Type	Has K Brace End Panels	Has Horizontals	Top Girt Offset in	Bottom Girt Offset in
T5	140.00-120.00	10.00	X Brace	No	No	0.0000	0.0000
T6	120.00-100.00	10.00	X Brace	No	No	0.0000	0.0000
T7	100.00-80.00	10.00	X Brace	No	No	0.0000	0.0000
T8	80.00-60.00	10.00	X Brace	No	No	0.0000	0.0000
T9	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T10	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T11	20.00-0.00	20.00	X Brace	No	No	0.0000	0.0000

Tower Section Geometry (cont'd)

Tower Elevation ft	Leg Type	Leg Size	Leg Grade	Diagonal Type	Diagonal Size	Diagonal Grade
T1 193.00-185.00	Solid Round	2	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T2 185.00-170.00	Solid Round	2	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T3 170.00-160.00	Truss Leg	Pirod 105244	A572-50 (50 ksi)	Equal Angle	L2 1/2x2 1/2x3/16	A36 (36 ksi)
T4 160.00-140.00	Truss Leg	Pirod 105217	A572-50 (50 ksi)	Equal Angle	L3x3x3/16	A36 (36 ksi)
T5 140.00-120.00	Truss Leg	Pirod 105217	A572-50 (50 ksi)	Equal Angle	L3x3x3/16	A36 (36 ksi)
T6 120.00-100.00	Truss Leg	Pirod 105218	A572-50 (50 ksi)	Equal Angle	L3x3x5/16	A36 (36 ksi)
T7 100.00-80.00	Truss Leg	Pirod 105219	A572-50 (50 ksi)	Equal Angle	L3x3x5/16	A36 (36 ksi)
T8 80.00-60.00	Truss Leg	Pirod 105219	A572-50 (50 ksi)	Equal Angle	L3 1/2x3 1/2x5/16	A36 (36 ksi)
T9 60.00-40.00	Truss Leg	Pirod 105220	A572-50 (50 ksi)	Equal Angle	L3 1/2x3 1/2x5/16	A36 (36 ksi)
T10 40.00-20.00	Truss Leg	Pirod 105220	A572-50 (50 ksi)	Equal Angle	L3 1/2x3 1/2x5/16	A36 (36 ksi)
T11 20.00-0.00	Truss Leg	Pirod 112738	A572-50 (50 ksi)	Double Equal Angle	2L3 1/2x3 1/2x5/16x1	A36 (36 ksi)

Tower Section Geometry (cont'd)

Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 193.00-185.00	Solid Round	1 1/4	A572-50 (50 ksi)	Solid Round	1 1/4	A572-50 (50 ksi)
T2 185.00-170.00	Solid Round	1 1/4	A572-50 (50 ksi)	Solid Round	1 1/4	A572-50 (50 ksi)

Tower Section Geometry (cont'd)

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Tower Elevation ft	Calc K Single Angles	Calc K Solid Rounds	K Factors ¹								
			Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace	
				X Y	X Y	X Y	X Y	X Y	X Y	X Y	
T5	Yes	Yes	1	1	1	1	1	1	1	1	1
140.00-120.00				1	1	1	1	1	1	1	1
T6	Yes	Yes	1	1	1	1	1	1	1	1	1
120.00-100.00				1	1	1	1	1	1	1	1
T7	Yes	Yes	1	1	1	1	1	1	1	1	1
100.00-80.00				1	1	1	1	1	1	1	1
T8	Yes	Yes	1	1	1	1	1	1	1	1	1
80.00-60.00				1	1	1	1	1	1	1	1
T9	Yes	Yes	1	1	1	1	1	1	1	1	1
60.00-40.00				1	1	1	1	1	1	1	1
T10	Yes	Yes	1	1	1	1	1	1	1	1	1
40.00-20.00				1	1	1	1	1	1	1	1
T11	Yes	Yes	1	1	1	1	1	1	1	1	1
20.00-0.00				1	1	1	1	1	1	1	1

¹Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

Tower Section Geometry (cont'd)

Tower Elevation ft	Truss-Leg K Factors					
	Truss-Legs Used As Leg Members			Truss-Legs Used As Inner Members		
	Leg Panels	X Brace Diagonals	Z Brace Diagonals	Leg Panels	X Brace Diagonals	Z Brace Diagonals
T3	1	0.5	0.85	1	0.5	0.85
170.00-160.00						
T4	1	0.5	0.85	1	0.5	0.85
160.00-140.00						
T5	1	0.5	0.85	1	0.5	0.85
140.00-120.00						
T6	1	0.5	0.85	1	0.5	0.85
120.00-100.00						
T7	1	0.5	0.85	1	0.5	0.85
100.00-80.00						
T8	1	0.5	0.85	1	0.5	0.85
80.00-60.00						
T9	1	0.5	0.85	1	0.5	0.85
60.00-40.00						
T10	1	0.5	0.85	1	0.5	0.85
40.00-20.00						
T11	1	0.5	0.85	1	0.5	0.85
20.00-0.00						

Tower Section Geometry (cont'd)

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Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Face Offset in	Lateral Offset (Frac FW)	#	# Per Row	Clear Spacing in	Width or Diameter in	Perimeter in	Weight plf
1 5/8 ***	C	No	Ar (CaAa)	193.00 - 5.00	0.0000	0.15	12	4	0.5000	1.9800		1.04
1 5/8	A	No	Ar (CaAa)	182.00 - 5.00	0.0000	0.3	12	12	0.5000	1.9800		1.04
5/8"	A	No	Ar (CaAa)	182.00 - 5.00	0.0000	0.25	2	1	0.5000	0.8800		0.40
3/4" DC Power ***	A	No	Ar (CaAa)	182.00 - 5.00	0.0000	0.2	4	2	0.5000	0.9950		0.47
LDF6-50A (1-1/4 FOAM) ***	B	No	Ar (CaAa)	175.00 - 5.00	0.0000	0.15	4	4	0.5000	1.5500		0.66
1 5/8 ***	C	No	Ar (CaAa)	162.00 - 5.00	0.0000	0.2	14	12	0.5000	1.9800		1.04
1/2 ***	C	No	Ar (CaAa)	30.00 - 5.00	0.0000	0.4	2	1	0.5000	0.5800		0.25
Feedline Ladder (Af) ***	A	No	Af (CaAa)	182.00 - 5.00	0.0000	0.25	1	1	3.0000	1.5000		8.40
Feedline Ladder (Af) ***	C	No	Af (CaAa)	193.00 - 5.00	0.0000	0.2	1	1	3.0000	1.5000		8.40
3/8" ***	C	No	Ar (CaAa)	100.00 - 5.00	0.0000	0.28	1	1	0.3750	0.3750		0.18
Feedline Ladder (Af)	B	No	Af (CaAa)	175.00 - 5.00	0.0000	0.15	1	1	3.0000	1.5000		8.40

Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number	C _{AA} ft ² /ft	Weight plf

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T1	193.00-185.00	A	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	21.008	0.000	0.17
T2	185.00-170.00	A	0.000	0.000	38.400	0.000	0.28
		B	0.000	0.000	4.350	0.000	0.06
		C	0.000	0.000	39.390	0.000	0.31
T3	170.00-160.00	A	0.000	0.000	32.000	0.000	0.24
		B	0.000	0.000	8.700	0.000	0.11
		C	0.000	0.000	31.804	0.000	0.24
T4	160.00-140.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	107.960	0.000	0.71

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Tower Section	Tower Elevation ft	Face	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T5	140.00-120.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	107.960	0.000	0.71
T6	120.00-100.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	107.960	0.000	0.71
T7	100.00-80.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	108.710	0.000	0.71
T8	80.00-60.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	108.710	0.000	0.71
T9	60.00-40.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	108.710	0.000	0.71
T10	40.00-20.00	A	0.000	0.000	64.000	0.000	0.47
		B	0.000	0.000	17.400	0.000	0.22
		C	0.000	0.000	109.870	0.000	0.72
T11	20.00-0.00	A	0.000	0.000	48.000	0.000	0.35
		B	0.000	0.000	13.050	0.000	0.17
		C	0.000	0.000	83.272	0.000	0.54

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
T1	193.00-185.00	A	1.786	0.000	0.000	0.000	0.000	0.00
		B		0.000	0.000	0.000	0.000	0.00
		C		0.000	0.000	21.570	0.000	0.53
T2	185.00-170.00	A	1.775	0.000	0.000	80.939	0.000	1.30
		B		0.000	0.000	10.745	0.000	0.19
		C		0.000	0.000	40.351	0.000	0.98
T3	170.00-160.00	A	1.762	0.000	0.000	67.295	0.000	1.08
		B		0.000	0.000	21.421	0.000	0.37
		C		0.000	0.000	35.265	0.000	0.80
T4	160.00-140.00	A	1.745	0.000	0.000	134.192	0.000	2.14
		B		0.000	0.000	42.664	0.000	0.73
		C		0.000	0.000	137.728	0.000	2.74
T5	140.00-120.00	A	1.720	0.000	0.000	133.601	0.000	2.12
		B		0.000	0.000	42.401	0.000	0.72
		C		0.000	0.000	137.305	0.000	2.71
T6	120.00-100.00	A	1.692	0.000	0.000	132.922	0.000	2.09
		B		0.000	0.000	42.099	0.000	0.71
		C		0.000	0.000	136.819	0.000	2.68
T7	100.00-80.00	A	1.658	0.000	0.000	132.122	0.000	2.05
		B		0.000	0.000	41.742	0.000	0.70
		C		0.000	0.000	143.629	0.000	2.73
T8	80.00-60.00	A	1.617	0.000	0.000	131.142	0.000	2.01
		B		0.000	0.000	41.307	0.000	0.68
		C		0.000	0.000	142.762	0.000	2.69
T9	60.00-40.00	A	1.564	0.000	0.000	129.869	0.000	1.95
		B		0.000	0.000	40.740	0.000	0.66
		C		0.000	0.000	141.636	0.000	2.63
T10	40.00-20.00	A	1.486	0.000	0.000	128.018	0.000	1.87
		B		0.000	0.000	39.918	0.000	0.64
		C		0.000	0.000	147.374	0.000	2.62
T11	20.00-0.00	A	1.331	0.000	0.000	93.261	0.000	1.29

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Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A _R ft ²	A _F ft ²	C _{AA} In Face ft ²	C _{AA} Out Face ft ²	Weight K
		B		0.000	0.000	28.717	0.000	0.44
		C		0.000	0.000	112.815	0.000	1.88

Feed Line Center of Pressure

Section	Elevation ft	CP _x in	CP _z in	CP _x Ice in	CP _z Ice in
T1	193.00-185.00	-9.4121	20.3071	-9.8164	19.9308
T2	185.00-170.00	-6.7049	-9.8412	-6.3408	-8.9762
T3	170.00-160.00	-5.6740	-10.9638	-4.3959	-9.8672
T4	160.00-140.00	-10.3423	-10.7581	-8.7107	-9.5225
T5	140.00-120.00	-13.2447	-13.9660	-11.1696	-12.3828
T6	120.00-100.00	-16.1471	-17.1738	-13.6456	-15.2608
T7	100.00-80.00	-19.1912	-19.9332	-17.0302	-15.8375
T8	80.00-60.00	-22.1155	-23.0717	-19.6805	-18.4445
T9	60.00-40.00	-25.0399	-26.2103	-22.3689	-21.1226
T10	40.00-20.00	-28.3271	-28.3259	-26.4734	-21.2047
T11	20.00-0.00	-31.2825	-29.9238	-30.3834	-21.2641

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _a No Ice	K _a Ice
T1	1	1 5/8	185.00 - 193.00	0.6000	0.4614
T1	15	Feedline Ladder (Af)	185.00 - 193.00	0.6000	0.4614
T2	1	1 5/8	170.00 - 185.00	0.6000	0.4628
T2	3	1 5/8	170.00 - 182.00	0.6000	0.4628
T2	5	5/8"	170.00 - 182.00	0.6000	0.4628
T2	6	3/4" DC Power	170.00 - 182.00	0.6000	0.4628
T2	8	LDF6-50A (1-1/4 FOAM)	170.00 - 175.00	0.6000	0.4628
T2	14	Feedline Ladder (Af)	170.00 - 182.00	0.6000	0.4628
T2	15	Feedline Ladder (Af)	170.00 - 185.00	0.6000	0.4628
T2	19	Feedline Ladder (Af)	170.00 - 175.00	0.6000	0.4628
T3	1	1 5/8	160.00 - 170.00	0.6000	0.3192
T3	3	1 5/8	160.00 - 170.00	0.6000	0.3192
T3	5	5/8"	160.00 - 170.00	0.6000	0.3192
T3	6	3/4" DC Power	160.00 -	0.6000	0.3192

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Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
			170.00		
T3	8	LDF6-50A (1-1/4 FOAM)	160.00 -	0.6000	0.3192
			170.00		
T3	10	1 5/8	160.00 -	0.6000	0.3192
			162.00		
T3	14	Feedline Ladder (Af)	160.00 -	0.6000	0.3192
			170.00		
T3	15	Feedline Ladder (Af)	160.00 -	0.6000	0.3192
			170.00		
T3	19	Feedline Ladder (Af)	160.00 -	0.6000	0.3192
			170.00		
T4	1	1 5/8	140.00 -	0.6000	0.4127
			160.00		
T4	3	1 5/8	140.00 -	0.6000	0.4127
			160.00		
T4	5	5/8"	140.00 -	0.6000	0.4127
			160.00		
T4	6	3/4" DC Power	140.00 -	0.6000	0.4127
			160.00		
T4	8	LDF6-50A (1-1/4 FOAM)	140.00 -	0.6000	0.4127
			160.00		
T4	10	1 5/8	140.00 -	0.6000	0.4127
			160.00		
T4	14	Feedline Ladder (Af)	140.00 -	0.6000	0.4127
			160.00		
T4	15	Feedline Ladder (Af)	140.00 -	0.6000	0.4127
			160.00		
T4	19	Feedline Ladder (Af)	140.00 -	0.6000	0.4127
			160.00		
T5	1	1 5/8	120.00 -	0.6000	0.5118
			140.00		
T5	3	1 5/8	120.00 -	0.6000	0.5118
			140.00		
T5	5	5/8"	120.00 -	0.6000	0.5118
			140.00		
T5	6	3/4" DC Power	120.00 -	0.6000	0.5118
			140.00		
T5	8	LDF6-50A (1-1/4 FOAM)	120.00 -	0.6000	0.5118
			140.00		
T5	10	1 5/8	120.00 -	0.6000	0.5118
			140.00		
T5	14	Feedline Ladder (Af)	120.00 -	0.6000	0.5118
			140.00		
T5	15	Feedline Ladder (Af)	120.00 -	0.6000	0.5118
			140.00		
T5	19	Feedline Ladder (Af)	120.00 -	0.6000	0.5118
			140.00		
T6	1	1 5/8	100.00 -	0.6000	0.5764
			120.00		
T6	3	1 5/8	100.00 -	0.6000	0.5764
			120.00		
T6	5	5/8"	100.00 -	0.6000	0.5764
			120.00		
T6	6	3/4" DC Power	100.00 -	0.6000	0.5764
			120.00		
T6	8	LDF6-50A (1-1/4 FOAM)	100.00 -	0.6000	0.5764
			120.00		
T6	10	1 5/8	100.00 -	0.6000	0.5764
			120.00		
T6	14	Feedline Ladder (Af)	100.00 -	0.6000	0.5764
			120.00		
T6	15	Feedline Ladder (Af)	100.00 -	0.6000	0.5764

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Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K_a No Ice	K_a Ice
			120.00		
T6	19	Feedline Ladder (Af)	100.00 - 120.00	0.6000	0.5764
T7	1	1 5/8	80.00 - 100.00	0.6000	0.6000
T7	3	1 5/8	80.00 - 100.00	0.6000	0.6000
T7	5	5/8"	80.00 - 100.00	0.6000	0.6000
T7	6	3/4" DC Power	80.00 - 100.00	0.6000	0.6000
T7	8	LDF6-50A (1-1/4 FOAM)	80.00 - 100.00	0.6000	0.6000
T7	10	1 5/8	80.00 - 100.00	0.6000	0.6000
T7	14	Feedline Ladder (Af)	80.00 - 100.00	0.6000	0.6000
T7	15	Feedline Ladder (Af)	80.00 - 100.00	0.6000	0.6000
T7	18	3/8"	80.00 - 100.00	0.6000	0.6000
T7	19	Feedline Ladder (Af)	80.00 - 100.00	0.6000	0.6000
T8	1	1 5/8	60.00 - 80.00	0.6000	0.6000
T8	3	1 5/8	60.00 - 80.00	0.6000	0.6000
T8	5	5/8"	60.00 - 80.00	0.6000	0.6000
T8	6	3/4" DC Power	60.00 - 80.00	0.6000	0.6000
T8	8	LDF6-50A (1-1/4 FOAM)	60.00 - 80.00	0.6000	0.6000
T8	10	1 5/8	60.00 - 80.00	0.6000	0.6000
T8	14	Feedline Ladder (Af)	60.00 - 80.00	0.6000	0.6000
T8	15	Feedline Ladder (Af)	60.00 - 80.00	0.6000	0.6000
T8	18	3/8"	60.00 - 80.00	0.6000	0.6000
T8	19	Feedline Ladder (Af)	60.00 - 80.00	0.6000	0.6000
T9	1	1 5/8	40.00 - 60.00	0.6000	0.6000
T9	3	1 5/8	40.00 - 60.00	0.6000	0.6000
T9	5	5/8"	40.00 - 60.00	0.6000	0.6000
T9	6	3/4" DC Power	40.00 - 60.00	0.6000	0.6000
T9	8	LDF6-50A (1-1/4 FOAM)	40.00 - 60.00	0.6000	0.6000
T9	10	1 5/8	40.00 - 60.00	0.6000	0.6000
T9	14	Feedline Ladder (Af)	40.00 - 60.00	0.6000	0.6000
T9	15	Feedline Ladder (Af)	40.00 - 60.00	0.6000	0.6000
T9	18	3/8"	40.00 - 60.00	0.6000	0.6000
T9	19	Feedline Ladder (Af)	40.00 - 60.00	0.6000	0.6000
T10	1	1 5/8	20.00 - 40.00	0.6000	0.6000
T10	3	1 5/8	20.00 - 40.00	0.6000	0.6000
T10	5	5/8"	20.00 - 40.00	0.6000	0.6000
T10	6	3/4" DC Power	20.00 - 40.00	0.6000	0.6000
T10	8	LDF6-50A (1-1/4 FOAM)	20.00 - 40.00	0.6000	0.6000
T10	10	1 5/8	20.00 - 40.00	0.6000	0.6000
T10	12	1/2	20.00 - 30.00	0.6000	0.6000
T10	14	Feedline Ladder (Af)	20.00 - 40.00	0.6000	0.6000
T10	15	Feedline Ladder (Af)	20.00 - 40.00	0.6000	0.6000
T10	18	3/8"	20.00 - 40.00	0.6000	0.6000
T10	19	Feedline Ladder (Af)	20.00 - 40.00	0.6000	0.6000
T11	1	1 5/8	5.00 - 20.00	0.6000	0.6000
T11	3	1 5/8	5.00 - 20.00	0.6000	0.6000
T11	5	5/8"	5.00 - 20.00	0.6000	0.6000
T11	6	3/4" DC Power	5.00 - 20.00	0.6000	0.6000
T11	8	LDF6-50A (1-1/4 FOAM)	5.00 - 20.00	0.6000	0.6000
T11	10	1 5/8	5.00 - 20.00	0.6000	0.6000
T11	12	1/2	5.00 - 20.00	0.6000	0.6000
T11	14	Feedline Ladder (Af)	5.00 - 20.00	0.6000	0.6000
T11	15	Feedline Ladder (Af)	5.00 - 20.00	0.6000	0.6000
T11	18	3/8"	5.00 - 20.00	0.6000	0.6000
T11	19	Feedline Ladder (Af)	5.00 - 20.00	0.6000	0.6000

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Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _A A _A Front	C _A A _A Side	Weight
			Horz	Lateral					
			ft	ft	°	ft	ft ²	ft ²	K
(3) RR90-17-02DP w/ Mount Pipe	A	From Leg	3.00	0.0000	193.00	No Ice	4.59	3.32	0.03
			0.00			1/2" Ice	5.09	4.09	0.07
			2.00			1" Ice	5.58	4.78	0.12
(3) RR90-17-02DP w/ Mount Pipe	B	From Leg	3.00	0.0000	193.00	No Ice	4.59	3.32	0.03
			0.00			1/2" Ice	5.09	4.09	0.07
			2.00			1" Ice	5.58	4.78	0.12
(3) RR90-17-02DP w/ Mount Pipe	C	From Leg	3.00	0.0000	193.00	No Ice	4.59	3.32	0.03
			0.00			1/2" Ice	5.09	4.09	0.07
			2.00			1" Ice	5.58	4.78	0.12
(1) Low Profile Platform	A	None		0.0000	193.00	No Ice	24.33	24.33	1.65
						1/2" Ice	30.22	30.22	2.03
						1" Ice	36.11	36.11	2.41

Powerwave 7770 w/ Mount Pipe	A	From Leg	3.00	0.0000	182.00	No Ice	6.46	4.59	0.06
			0.00			1/2" Ice	7.14	5.66	0.11
			0.00			1" Ice	7.73	6.45	0.17
Powerwave 7770 w/ Mount Pipe	B	From Leg	3.00	0.0000	182.00	No Ice	6.46	4.59	0.06
			0.00			1/2" Ice	7.14	5.66	0.11
			0.00			1" Ice	7.73	6.45	0.17
Powerwave 7770 w/ Mount Pipe	C	From Leg	3.00	0.0000	182.00	No Ice	6.46	4.59	0.06
			0.00			1/2" Ice	7.14	5.66	0.11
			0.00			1" Ice	7.73	6.45	0.17
(2) HPA-65R-BUU-H8 w/ Mount Pipe	A	From Leg	3.00	0.0000	182.00	No Ice	13.30	9.18	0.09
			0.00			1/2" Ice	13.99	10.48	0.19
			0.00			1" Ice	14.70	11.49	0.29
(2) HPA-65R-BUU-H8 w/ Mount Pipe	B	From Leg	3.00	0.0000	182.00	No Ice	13.30	9.18	0.09
			0.00			1/2" Ice	13.99	10.48	0.19
			0.00			1" Ice	14.70	11.49	0.29
(2) HPA-65R-BUU-H8 w/ Mount Pipe	C	From Leg	3.00	0.0000	182.00	No Ice	13.30	9.18	0.09
			0.00			1/2" Ice	13.99	10.48	0.19
			0.00			1" Ice	14.70	11.49	0.29
(2) LGP21401	A	From Leg	3.00	0.0000	182.00	No Ice	0.00	0.23	0.01
			0.00			1/2" Ice	0.00	0.31	0.02
			0.00			1" Ice	0.00	0.40	0.03
(2) LGP21401	B	From Leg	3.00	0.0000	182.00	No Ice	0.00	0.23	0.01
			0.00			1/2" Ice	0.00	0.31	0.02
			0.00			1" Ice	0.00	0.40	0.03
(2) LGP21401	C	From Leg	3.00	0.0000	182.00	No Ice	0.00	0.23	0.01
			0.00			1/2" Ice	0.00	0.31	0.02
			0.00			1" Ice	0.00	0.40	0.03
(2) LGP21903 Diplexer	A	From Leg	3.00	0.0000	182.00	No Ice	0.27	0.18	0.01
			0.00			1/2" Ice	0.34	0.25	0.01
			0.00			1" Ice	0.43	0.32	0.01
(2) LGP21903 Diplexer	B	From Leg	3.00	0.0000	182.00	No Ice	0.27	0.18	0.01
			0.00			1/2" Ice	0.34	0.25	0.01
			0.00			1" Ice	0.43	0.32	0.01
(2) LGP21903 Diplexer	C	From Leg	3.00	0.0000	182.00	No Ice	0.27	0.18	0.01
			0.00			1/2" Ice	0.34	0.25	0.01
			0.00			1" Ice	0.43	0.32	0.01
(2) RRUS 11	A	From Leg	3.00	0.0000	182.00	No Ice	3.25	1.37	0.05
			0.00			1/2" Ice	3.49	1.55	0.07
			0.00			1" Ice	3.74	1.74	0.10
(2) RRUS 11	B	From Leg	3.00	0.0000	182.00	No Ice	3.25	1.37	0.05
			0.00			1/2" Ice	3.49	1.55	0.07
			0.00			1" Ice	3.74	1.74	0.10

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight	
			Horz	Lateral						°
(2) RRUS 11	C	From Leg	0.00		0.0000	182.00	1" Ice	3.74	1.74	0.10
			3.00				No Ice	3.25	1.37	0.05
			0.00				1/2" Ice	3.49	1.55	0.07
RRUS 12	A	From Leg	0.00		0.0000	182.00	1" Ice	3.74	1.74	0.10
			3.00				No Ice	3.67	1.49	0.06
			0.00				1/2" Ice	3.93	1.67	0.08
RRUS 12	B	From Leg	0.00		0.0000	182.00	1" Ice	4.19	1.87	0.11
			3.00				No Ice	3.67	1.49	0.06
			0.00				1/2" Ice	3.93	1.67	0.08
RRUS 12	C	From Leg	0.00		0.0000	182.00	1" Ice	4.19	1.87	0.11
			3.00				No Ice	3.67	1.49	0.06
			0.00				1/2" Ice	3.93	1.67	0.08
(2) RRUS A2	A	From Leg	0.00		0.0000	182.00	1" Ice	4.19	1.87	0.11
			3.00				No Ice	2.41	0.53	0.02
			0.00				1/2" Ice	2.62	0.67	0.03
RRUS A2	B	From Leg	0.00		0.0000	182.00	1" Ice	2.84	0.81	0.05
			3.00				No Ice	2.41	0.53	0.02
			0.00				1/2" Ice	2.62	0.67	0.03
RRUS A2	C	From Leg	0.00		0.0000	182.00	1" Ice	2.84	0.81	0.05
			3.00				No Ice	2.41	0.53	0.02
			0.00				1/2" Ice	2.62	0.67	0.03
RRUS-32	A	From Leg	0.00		0.0000	182.00	1" Ice	2.84	0.81	0.05
			3.00				No Ice	3.87	2.76	0.08
			0.00				1/2" Ice	4.15	3.02	0.10
RRUS-32	B	From Leg	0.00		0.0000	182.00	1" Ice	4.44	3.29	0.14
			3.00				No Ice	3.87	2.76	0.08
			0.00				1/2" Ice	4.15	3.02	0.10
RRUS-32	C	From Leg	0.00		0.0000	182.00	1" Ice	4.44	3.29	0.14
			3.00				No Ice	3.87	2.76	0.08
			0.00				1/2" Ice	4.15	3.02	0.10
1000860	A	From Leg	0.00		0.0000	182.00	1" Ice	4.44	3.29	0.14
			3.00				No Ice	1.95	0.50	0.03
			0.00				1/2" Ice	2.13	0.62	0.04
1000860	B	From Leg	0.00		0.0000	182.00	1" Ice	2.33	0.75	0.06
			3.00				No Ice	1.95	0.50	0.03
			0.00				1/2" Ice	2.13	0.62	0.04
1000860	C	From Leg	0.00		0.0000	182.00	1" Ice	2.33	0.75	0.06
			3.00				No Ice	1.95	0.50	0.03
			0.00				1/2" Ice	2.13	0.62	0.04
DC6-48-60-18-8F	B	From Leg	0.00		0.0000	182.00	1" Ice	2.33	0.75	0.06
			3.00				No Ice	2.57	2.57	0.02
			0.00				1/2" Ice	2.80	2.80	0.04
DC6-48-60-18-8F	C	From Leg	0.00		0.0000	182.00	1" Ice	3.04	3.04	0.07
			3.00				No Ice	2.57	2.57	0.02
			0.00				1/2" Ice	2.80	2.80	0.04
(3) 12.5' T-Frames (Commscope P/N: MTC3615) ***	C	None	0.00		0.0000	182.00	1" Ice	3.04	3.04	0.07
			0.00				No Ice	49.30	49.30	2.29
			0.00				1/2" Ice	52.20	52.20	2.68
PC1N0F-0190B-002M	A	From Leg	0.00		0.0000	30.00	1" Ice	55.10	55.10	3.07
			0.00				No Ice	0.03	0.03	0.00
			0.00				1/2" Ice	0.06	0.06	0.00
PC1N0F-0190B-002M	B	From Leg	0.00		0.0000	30.00	1" Ice	0.10	0.10	0.00
			0.00				No Ice	0.03	0.03	0.00
			0.00				1/2" Ice	0.06	0.06	0.00
***			0.00				1" Ice	0.10	0.10	0.00

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
Lightning Rod	C	From Leg	0.00	0.0000	193.00	No Ice	0.25	0.25	0.03
			0.00			1/2" Ice	0.66	0.66	0.03
			2.00			1" Ice	0.97	0.97	0.04

(3) T-Frames	C	None	0.00	0.0000	162.00	No Ice	19.83	19.83	0.92
						1/2" Ice	29.41	29.41	1.33
						1" Ice	38.99	38.99	1.73
(2) HBXX-6517DS-A2M w/ Mount Pipe	A	From Leg	4.00	0.0000	162.00	No Ice	8.98	6.96	0.07
			0.00			1/2" Ice	9.65	8.18	0.14
			0.00			1" Ice	10.29	9.14	0.21
(2) HBXX-6517DS-A2M w/ Mount Pipe	B	From Leg	4.00	0.0000	162.00	No Ice	8.98	6.96	0.07
			0.00			1/2" Ice	9.65	8.18	0.14
			0.00			1" Ice	10.29	9.14	0.21
(2) HBXX-6517DS-A2M w/ Mount Pipe	C	From Leg	4.00	0.0000	162.00	No Ice	8.98	6.96	0.07
			0.00			1/2" Ice	9.65	8.18	0.14
			0.00			1" Ice	10.29	9.14	0.21
LNX-6514DS-A1M	A	From Leg	4.00	0.0000	162.00	No Ice	8.41	5.41	0.04
			0.00			1/2" Ice	8.96	5.86	0.09
			0.00			1" Ice	9.52	6.33	0.15
LNX-6514DS-A1M	B	From Leg	4.00	0.0000	162.00	No Ice	8.41	5.41	0.04
			0.00			1/2" Ice	8.96	5.86	0.09
			0.00			1" Ice	9.52	6.33	0.15
LNX-6514DS-A1M	C	From Leg	4.00	0.0000	162.00	No Ice	8.41	5.41	0.04
			0.00			1/2" Ice	8.96	5.86	0.09
			0.00			1" Ice	9.52	6.33	0.15
QUAD656C0000x	A	From Leg	4.00	0.0000	162.00	No Ice	13.24	5.62	0.05
			0.00			1/2" Ice	14.01	6.32	0.13
			0.00			1" Ice	14.78	7.02	0.21
QUAD656C0000x	B	From Leg	4.00	0.0000	162.00	No Ice	13.24	5.62	0.05
			0.00			1/2" Ice	14.01	6.32	0.13
			0.00			1" Ice	14.78	7.02	0.21
QUAD656C0000x	C	From Leg	4.00	0.0000	162.00	No Ice	13.24	5.62	0.05
			0.00			1/2" Ice	14.01	6.32	0.13
			0.00			1" Ice	14.78	7.02	0.21
DB-T1-6Z-8AB-0Z	A	From Leg	4.00	0.0000	162.00	No Ice	4.80	2.00	0.04
			0.00			1/2" Ice	5.21	2.29	0.08
			0.00			1" Ice	5.62	2.58	0.12
DB-T1-6Z-8AB-0Z	B	From Leg	4.00	0.0000	162.00	No Ice	4.80	2.00	0.04
			0.00			1/2" Ice	5.21	2.29	0.08
			0.00			1" Ice	5.62	2.58	0.12
(2) FD9R6004/2C-3L	A	From Leg	4.00	0.0000	162.00	No Ice	0.37	0.08	0.00
			0.00			1/2" Ice	0.45	0.14	0.01
			0.00			1" Ice	0.54	0.20	0.01
(2) FD9R6004/2C-3L	B	From Leg	4.00	0.0000	162.00	No Ice	0.37	0.08	0.00
			0.00			1/2" Ice	0.45	0.14	0.01
			0.00			1" Ice	0.54	0.20	0.01
(2) FD9R6004/2C-3L	C	From Leg	4.00	0.0000	162.00	No Ice	0.37	0.08	0.00
			0.00			1/2" Ice	0.45	0.14	0.01
			0.00			1" Ice	0.54	0.20	0.01
KS24019-L112A	A	From Leg	4.00	0.0000	100.00	No Ice	0.16	0.16	0.01
			0.00			1/2" Ice	0.22	0.22	0.01
			0.00			1" Ice	0.30	0.30	0.01

Empty Mount Pipe	A	From Leg	4.00	0.0000	162.00	No Ice	1.43	1.43	0.02
			0.00			1/2" Ice	1.92	1.92	0.03
			0.00			1" Ice	2.29	2.29	0.05

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight
			Horz	Lateral					
Empty Mount Pipe	B	From Leg	4.00	0.0000	162.00	No Ice	1.43	1.43	0.02
			0.00			1/2" Ice	1.92	1.92	0.03
			0.00			1" Ice	2.29	2.29	0.05
Empty Mount Pipe	C	From Leg	4.00	0.0000	162.00	No Ice	1.43	1.43	0.02
			0.00			1/2" Ice	1.92	1.92	0.03
			0.00			1" Ice	2.29	2.29	0.05
RRH2x60-AWS	A	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10
RRH2x60-AWS	B	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10
RRH2x60-AWS	C	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10
RRH2x60-1900	A	From Leg	4.00	0.0000	162.00	No Ice	1.87	1.22	0.04
			0.00			1/2" Ice	2.14	1.44	0.06
			0.00			1" Ice	2.41	1.66	0.08
RRH2x60-1900	B	From Leg	4.00	0.0000	162.00	No Ice	1.87	1.22	0.04
			0.00			1/2" Ice	2.14	1.44	0.06
			0.00			1" Ice	2.41	1.66	0.08
RRH2x60-1900	C	From Leg	4.00	0.0000	162.00	No Ice	1.87	1.22	0.04
			0.00			1/2" Ice	2.14	1.44	0.06
			0.00			1" Ice	2.41	1.66	0.08
RRH2x60-700	A	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10
RRH2x60-700	B	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10
RRH2x60-700	C	From Leg	4.00	0.0000	162.00	No Ice	3.50	1.82	0.06
			0.00			1/2" Ice	3.89	2.17	0.08
			0.00			1" Ice	4.28	2.52	0.10

Modified T-Frames (3)	C	None		0.0000	175.00	No Ice	26.91	26.91	1.50
						1/2" Ice	34.78	34.78	2.00
						1" Ice	42.65	42.65	2.50
RFS APXVSPP18-C-A20	A	From Leg	3.00	0.0000	175.00	No Ice	8.02	5.28	0.06
			0.00			1/2" Ice	8.48	5.74	0.11
			0.00			1" Ice	8.94	6.20	0.16
RFS APXVSPP18-C-A20	B	From Leg	3.00	0.0000	175.00	No Ice	8.02	5.28	0.06
			0.00			1/2" Ice	8.48	5.74	0.11
			0.00			1" Ice	8.94	6.20	0.16
RFS APXVSPP18-C-A20	C	From Leg	3.00	0.0000	175.00	No Ice	8.02	5.28	0.06
			0.00			1/2" Ice	8.48	5.74	0.11
			0.00			1" Ice	8.94	6.20	0.16
NNVV-65B-R4 Antenna	A	From Leg	3.00	0.0000	175.00	No Ice	12.27	5.75	0.08
			0.00			1/2" Ice	12.77	6.21	0.16
			0.00			1" Ice	13.27	6.67	0.24
NNVV-65B-R4 Antenna	A	From Leg	3.00	0.0000	175.00	No Ice	12.27	5.75	0.08
			0.00			1/2" Ice	12.77	6.21	0.16
			0.00			1" Ice	13.27	6.67	0.24
NNVV-65B-R4 Antenna	A	From Leg	3.00	0.0000	175.00	No Ice	12.27	5.75	0.08
			0.00			1/2" Ice	12.77	6.21	0.16
			0.00			1" Ice	13.27	6.67	0.24
(2) 800 MHz RRH	A	From Leg	30.00	0.0000	175.00	No Ice	2.06	1.71	0.05
			0.00			1/2" Ice	2.24	1.88	0.07

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Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C _{AA} Front	C _{AA} Side	Weight					
			Horz	Lateral						Vert	°	ft	ft ²	ft ²
(2) 800 MHz RRH	B	From Leg	0.00		0.0000	175.00	1" Ice	2.43	2.06	0.09				
			3.00								No Ice	2.06	1.71	0.05
			0.00								1/2" Ice	2.24	1.88	0.07
(2) 800 MHz RRH	C	From Leg	0.00		0.0000	175.00	1" Ice	2.43	2.06	0.09				
			3.00								No Ice	2.06	1.71	0.05
			0.00								1/2" Ice	2.24	1.88	0.07
1900 MHz RRH	A	From Leg	0.00		0.0000	175.00	1" Ice	2.43	2.06	0.09				
			3.00								No Ice	2.31	2.38	0.05
			0.00								1/2" Ice	2.52	2.58	0.07
1900 MHz RRH	B	From Leg	0.00		0.0000	175.00	1" Ice	2.73	2.79	0.10				
			3.00								No Ice	2.31	2.38	0.05
			0.00								1/2" Ice	2.52	2.58	0.07
1900 MHz RRH	C	From Leg	0.00		0.0000	175.00	1" Ice	2.73	2.79	0.10				
			3.00								No Ice	2.31	2.38	0.05
			0.00								1/2" Ice	2.52	2.58	0.07
TD-RRH8x20-25	A	From Leg	0.00		0.0000	175.00	1" Ice	2.73	2.79	0.10				
			3.00								No Ice	3.70	1.29	0.07
			0.00								1/2" Ice	3.95	1.46	0.09
TD-RRH8x20-25	A	From Leg	0.00		0.0000	175.00	1" Ice	4.20	1.64	0.12				
			3.00								No Ice	3.70	1.29	0.07
			0.00								1/2" Ice	3.95	1.46	0.09
TD-RRH8x20-25	A	From Leg	0.00		0.0000	175.00	1" Ice	4.20	1.64	0.12				
			3.00								No Ice	3.70	1.29	0.07
			0.00								1/2" Ice	3.95	1.46	0.09
			0.00				1" Ice	4.20	1.64	0.12				

Truss-Leg Properties

Section Designation	Area	Area Ice	Self Weight	Ice Weight	Equiv. Diameter	Equiv. Diameter Ice	Leg Area
	in ²	in ²	K	K	in	in	in ²
Pirod 105244	1026.8606	3167.5615	0.56	0.62	7.1310	21.9970	3.6816
Pirod 105217	2130.7479	6575.8153	0.62	1.19	7.3984	22.8327	5.3014
Pirod 105217	2130.7479	6553.8954	0.62	1.16	7.3984	22.7566	5.3014
Pirod 105218	2263.4687	6600.7000	0.75	1.16	7.8593	22.9191	7.2158
Pirod 105219	2441.8688	6642.9857	0.94	1.16	8.4787	23.0659	9.4248
Pirod 105219	2441.8688	6606.6036	0.94	1.12	8.4787	22.9396	9.4248
Pirod 105220	2578.8005	6631.3031	1.12	1.08	8.9542	23.0254	11.9282
Pirod 105220	2578.8005	6562.4670	1.12	1.00	8.9542	22.7863	11.9282
Pirod 112738	3466.5160	8653.0272	1.69	1.18	12.0365	30.0452	14.7262

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice

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Comb. No.	Description
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 30 deg - No Ice
5	0.9 Dead+1.6 Wind 30 deg - No Ice
6	1.2 Dead+1.6 Wind 60 deg - No Ice
7	0.9 Dead+1.6 Wind 60 deg - No Ice
8	1.2 Dead+1.6 Wind 90 deg - No Ice
9	0.9 Dead+1.6 Wind 90 deg - No Ice
10	1.2 Dead+1.6 Wind 120 deg - No Ice
11	0.9 Dead+1.6 Wind 120 deg - No Ice
12	1.2 Dead+1.6 Wind 150 deg - No Ice
13	0.9 Dead+1.6 Wind 150 deg - No Ice
14	1.2 Dead+1.6 Wind 180 deg - No Ice
15	0.9 Dead+1.6 Wind 180 deg - No Ice
16	1.2 Dead+1.6 Wind 210 deg - No Ice
17	0.9 Dead+1.6 Wind 210 deg - No Ice
18	1.2 Dead+1.6 Wind 240 deg - No Ice
19	0.9 Dead+1.6 Wind 240 deg - No Ice
20	1.2 Dead+1.6 Wind 270 deg - No Ice
21	0.9 Dead+1.6 Wind 270 deg - No Ice
22	1.2 Dead+1.6 Wind 300 deg - No Ice
23	0.9 Dead+1.6 Wind 300 deg - No Ice
24	1.2 Dead+1.6 Wind 330 deg - No Ice
25	0.9 Dead+1.6 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	193 - 185	4.861	50	0.2465	0.0506
T2	185 - 170	4.442	50	0.2455	0.0509
T3	170 - 160	3.666	50	0.2318	0.0461
T4	160 - 140	3.180	50	0.2145	0.0326
T5	140 - 120	2.320	50	0.1804	0.0199

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Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T6	120 - 100	1.624	50	0.1393	0.0126
T7	100 - 80	1.094	50	0.1069	0.0093
T8	80 - 60	0.682	50	0.0816	0.0065
T9	60 - 40	0.379	50	0.0561	0.0045
T10	40 - 20	0.169	50	0.0360	0.0026
T11	20 - 0	0.037	50	0.0158	0.0008

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
193.00	(3) RR90-17-02DP w/ Mount Pipe	50	4.861	0.2465	0.0506	Inf
182.00	Powerwave 7770 w/ Mount Pipe	50	4.285	0.2442	0.0510	211425
175.00	Modified T-Frames (3)	50	3.920	0.2384	0.0497	58322
162.00	(3) T-Frames	50	3.275	0.2181	0.0353	33792
100.00	KS24019-L112A	50	1.094	0.1069	0.0093	43549
30.00	PC1N0F-0190B-002M	50	0.091	0.0257	0.0016	51237

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
T1	193 - 185	22.274	24	1.1194	0.2345
T2	185 - 170	20.370	24	1.1148	0.2362
T3	170 - 160	16.845	24	1.0552	0.2137
T4	160 - 140	14.627	24	0.9805	0.1511
T5	140 - 120	10.680	24	0.8278	0.0922
T6	120 - 100	7.484	24	0.6404	0.0584
T7	100 - 80	5.041	24	0.4920	0.0429
T8	80 - 60	3.146	24	0.3759	0.0303
T9	60 - 40	1.746	24	0.2583	0.0208
T10	40 - 20	0.778	24	0.1657	0.0120
T11	20 - 0	0.173	24	0.0726	0.0039

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
193.00	(3) RR90-17-02DP w/ Mount Pipe	24	22.274	1.1194	0.2345	257382
182.00	Powerwave 7770 w/ Mount Pipe	24	19.656	1.1089	0.2365	47787
175.00	Modified T-Frames (3)	24	18.003	1.0835	0.2305	14208
162.00	(3) T-Frames	24	15.059	0.9961	0.1635	7768
100.00	KS24019-L112A	24	5.041	0.4920	0.0429	9493
30.00	PC1N0F-0190B-002M	24	0.422	0.1183	0.0076	11113

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Bolt Design Data

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size in	Number Of Bolts	Maximum Load per Bolt K	Allowable Load per Bolt K	Ratio Load Allowable	Allowable Ratio	Criteria
T1	193	Leg	A325N	0.6250	5	1.24	24.85	0.050 ✓	1	Bolt DS
T2	185	Leg	A325N	1.0000	6	5.57	53.01	0.105 ✓	1	Bolt Tension
T3	170	Leg	A325N	1.0000	6	7.04	53.01	0.133 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	8.94	10.66	0.838 ✓	1	Member Block Shear
T4	160	Leg	A325N	1.0000	6	15.47	53.01	0.292 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	10.19	11.68	0.873 ✓	1	Member Block Shear
T5	140	Leg	A325N	1.0000	6	22.37	53.01	0.422 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	8.30	11.68	0.711 ✓	1	Member Block Shear
T6	120	Leg	A325N	1.0000	6	28.38	53.01	0.535 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	1	7.96	19.47	0.409 ✓	1	Member Block Shear
T7	100	Leg	A325N>1'	1.2500	6	33.85	72.48	0.467 ✓	1	Bolt Tension
		Diagonal	A325N>1'	1.2500	1	7.95	20.30	0.391 ✓	1	Member Block Shear
T8	80	Leg	A325N>1'	1.2500	6	38.92	72.48	0.537 ✓	1	Bolt Tension
		Diagonal	A325N>1'	1.2500	1	8.34	23.70	0.352 ✓	1	Member Block Shear
T9	60	Leg	A325N>1'	1.2500	6	43.72	72.48	0.603 ✓	1	Bolt Tension
		Diagonal	A325N>1'	1.2500	1	8.69	23.70	0.366 ✓	1	Member Block Shear
T10	40	Leg	A325N>1'	1.2500	6	48.56	72.48	0.670 ✓	1	Bolt Tension
		Diagonal	A325N>1'	1.2500	1	10.58	23.70	0.446 ✓	1	Member Block Shear
T11	20	Leg	A687	2.0000	6	50.56	220.89	0.229 ✓	1	Bolt Tension
		Diagonal	A325N	1.0000	2	8.16	35.53	0.230 ✓	1	Member Block Shear

Compression Checks

Leg Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in^2	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	2	8.00	2.38	57.0 K=1.00	3.1416	-6.21	111.48	0.056 ¹

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	185 - 170	2	15.00	2.38	57.0 K=1.00	3.1416	-43.07	111.48	0.386 ¹ ✓
T3	170 - 160	Pirod 105244	10.02	10.02	45.4 K=1.00	3.6816	-52.85	142.49	0.371 ¹ ✓
T4	160 - 140	Pirod 105217	20.03	10.02	37.8 K=1.00	5.3014	-107.86	214.86	0.502 ¹ ✓
T5	140 - 120	Pirod 105217	20.03	10.02	37.8 K=1.00	5.3014	-152.48	214.86	0.710 ¹ ✓
T6	120 - 100	Pirod 105218	20.03	10.02	32.4 K=1.00	7.2158	-192.63	300.68	0.641 ¹ ✓
T7	100 - 80	Pirod 105219	20.03	10.02	28.4 K=1.00	9.4248	-230.18	399.87	0.576 ¹ ✓
T8	80 - 60	Pirod 105219	20.03	10.02	28.4 K=1.00	9.4248	-265.76	399.87	0.665 ¹ ✓
T9	60 - 40	Pirod 105220	20.03	10.02	25.2 K=1.00	11.9282	-300.52	512.38	0.587 ¹ ✓
T10	40 - 20	Pirod 105220	20.03	10.02	25.2 K=1.00	11.9282	-336.18	512.38	0.656 ¹ ✓
T11	20 - 0	Pirod 112738	20.03	20.03	32.6 K=1.00	14.7262	-349.82	613.14	0.571 ¹ ✓

¹ P_u / φP_n controls

Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L _d ft	Kl/r	φP _n K	A in ²	V _u K	φV _n K	Stress Ratio
T3	170 - 160	0.5	1.48	121.0	165.67	0.1963	1.73	3.39	0.512 ✓
T4	160 - 140	0.5	1.47	120.0	238.57	0.1963	0.30	3.34	0.090 ✓
T5	140 - 120	0.5	1.47	120.0	238.57	0.1963	0.31	3.34	0.093 ✓
T6	120 - 100	0.5	1.46	119.0	324.71	0.1963	0.26	3.38	0.077 ✓
T7	100 - 80	0.625	1.45	94.4	424.12	0.3068	0.26	6.96	0.038 ✓
T8	80 - 60	0.625	1.45	94.4	424.12	0.3068	0.27	6.96	0.039 ✓
T9	60 - 40	0.625	1.43	93.6	536.77	0.3068	0.45	7.01	0.065 ✓
T10	40 - 20	0.625	1.43	93.6	536.77	0.3068	2.95	7.01	0.422 ✓
T11	20 - 0	0.75	1.73	93.9	662.68	0.4418	1.48	14.36	0.104 ✓

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Diagonal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1	5.54	2.68	115.6 K=0.90	0.7854	-1.28	13.28	0.096 ¹ ✓
T2	185 - 170	1	5.54	2.68	115.6 K=0.90	0.7854	-5.90	13.28	0.444 ¹ ✓
T3	170 - 160	L2 1/2x2 1/2x3/16	11.42	4.98	120.8 K=1.00	0.9023	-9.87	13.56	0.728 ¹ ✓
T4	160 - 140	L3x3x3/16	11.93	5.38	111.2 K=1.03	1.0898	-10.20	18.18	0.561 ¹ ✓
T5	140 - 120	L3x3x3/16	13.80	6.33	127.3 K=1.00	1.0898	-8.30	14.96	0.555 ¹ ✓
T6	120 - 100	L3x3x5/16	15.24	7.08	144.3 K=1.00	1.7800	-8.18	19.32	0.423 ¹ ✓
T7	100 - 80	L3x3x5/16	16.80	7.84	159.7 K=1.00	1.7800	-8.26	15.76	0.524 ¹ ✓
T8	80 - 60	L3 1/2x3 1/2x5/16	18.45	8.68	150.9 K=1.00	2.0900	-8.81	20.74	0.425 ¹ ✓
T9	60 - 40	L3 1/2x3 1/2x5/16	20.16	9.54	165.9 K=1.00	2.0900	-8.92	17.15	0.520 ¹ ✓
T10	40 - 20	L3 1/2x3 1/2x5/16	21.03	9.99	173.7 K=1.00	2.0900	-10.63	15.65	0.679 ¹ ✓
T11	20 - 0	2L3 1/2x3 1/2x5/16x1	29.01	13.87	145.7 K=0.95	4.1797	-19.22	44.46	0.432 ¹ ✓

¹ P_u / φP_n controls

Horizontal Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	7/8	5.00	4.83	185.6 K=0.70	0.6013	-0.15	3.94	0.039 ¹ ✓
T2	185 - 170	7/8	5.00	4.83	185.6 K=0.70	0.6013	-0.34	3.94	0.087 ¹ ✓

¹ P_u / φP_n controls

Top Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1 1/4	5.00	4.83	129.9 K=0.70	1.2272	-0.62	16.42	0.038 ¹ ✓

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	185 - 170	1 1/4	5.00	4.83	129.9 K=0.70	1.2272	-0.23	16.42	0.014 ¹ ✓

¹ P_u / φP_n controls

Bottom Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1 1/4	5.00	4.83	129.9 K=0.70	1.2272	-0.69	16.42	0.042 ¹ ✓
T2	185 - 170	1 1/4	5.00	4.83	129.9 K=0.70	1.2272	-1.00	16.42	0.061 ¹ ✓

¹ P_u / φP_n controls

Mid Girt Design Data (Compression)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	185 - 170	1 1/4	5.00	4.83	129.9 K=0.70	1.2272	-0.36	16.42	0.022 ¹ ✓

¹ P_u / φP_n controls

Tension Checks

Leg Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	2	8.00	2.38	57.0	1.7942	4.26	87.47	0.049 ¹ # ✓
T2	185 - 170	2	15.00	2.38	57.0	3.1416	33.39	141.37	0.236 ¹ ✓
T3	170 - 160	Pirod 105244	10.02	10.02	45.4	3.6816	42.27	165.67	0.255 ¹ ✓
T4	160 - 140	Pirod 105217	20.03	10.02	37.8	5.3014	92.82	238.57	0.389 ¹ ✓

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T5	140 - 120	Pirod 105217	20.03	10.02	37.8	5.3014	134.23	238.57	0.563 ¹
T6	120 - 100	Pirod 105218	20.03	10.02	32.4	7.2158	170.29	324.71	0.524 ¹
T7	100 - 80	Pirod 105219	20.03	10.02	28.4	9.4248	203.07	424.12	0.479 ¹
T8	80 - 60	Pirod 105219	20.03	10.02	28.4	9.4248	233.50	424.12	0.551 ¹
T9	60 - 40	Pirod 105220	20.03	10.02	25.2	11.9282	262.34	536.77	0.489 ¹
T10	40 - 20	Pirod 105220	20.03	10.02	25.2	11.9282	291.36	536.77	0.543 ¹
T11	20 - 0	Pirod 112738	20.03	20.03	32.6	14.7262	303.35	662.68	0.458 ¹

¹ P_u / φP_n controls

Based on net area of leg in section below

Truss-Leg Diagonal Data

Section No.	Elevation ft	Diagonal Size	L _d ft	Kl/r	φP _n K	A in ²	V _u K	φV _n K	Stress Ratio
T3	170 - 160	0.5	1.48	121.0	165.67	0.1963	1.73	3.39	0.512
T4	160 - 140	0.5	1.47	120.0	238.57	0.1963	0.30	3.34	0.090
T5	140 - 120	0.5	1.47	120.0	238.57	0.1963	0.31	3.34	0.093
T6	120 - 100	0.5	1.46	119.0	324.71	0.1963	0.26	3.38	0.077
T7	100 - 80	0.625	1.45	94.4	424.12	0.3068	0.26	6.96	0.038
T8	80 - 60	0.625	1.45	94.4	424.12	0.3068	0.27	6.96	0.039
T9	60 - 40	0.625	1.43	93.6	536.77	0.3068	0.45	7.01	0.065
T10	40 - 20	0.625	1.43	93.6	536.77	0.3068	2.95	7.01	0.422
T11	20 - 0	0.75	1.73	93.9	662.68	0.4418	1.48	14.36	0.104

Diagonal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1	5.54	2.68	128.4	0.7854	1.24	35.34	0.035 ¹

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Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T2	185 - 170	1	5.54	2.68	128.4	0.7854	5.80	35.34	0.164 ¹ ✓
T3	170 - 160	L2 1/2x2 1/2x3/16	11.42	4.98	80.0	0.5186	8.94	22.56	0.396 ¹ ✓
T4	160 - 140	L3x3x3/16	11.93	5.38	71.4	0.6592	10.19	28.67	0.356 ¹ ✓
T5	140 - 120	L3x3x3/16	13.13	6.02	79.5	0.6592	8.30	28.67	0.290 ¹ ✓
T6	120 - 100	L3x3x5/16	14.50	6.73	90.3	1.0713	7.96	46.60	0.171 ¹ ✓
T7	100 - 80	L3x3x5/16	16.01	7.45	100.3	1.0127	7.95	44.05	0.180 ¹ ✓
T8	80 - 60	L3 1/2x3 1/2x5/16	18.45	8.68	99.2	1.2452	8.34	54.17	0.154 ¹ ✓
T9	60 - 40	L3 1/2x3 1/2x5/16	20.16	9.54	108.8	1.2452	8.69	54.17	0.160 ¹ ✓
T10	40 - 20	L3 1/2x3 1/2x5/16	21.92	10.43	118.6	1.2452	10.58	54.17	0.195 ¹ ✓
T11	20 - 0	2L3 1/2x3 1/2x5/16x1	29.01	13.87	156.9	2.6074	16.31	113.42	0.144 ¹ ✓

¹ P_u / φP_n controls

Horizontal Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	7/8	5.00	4.83	265.1	0.6013	0.21	19.48	0.011 ¹ ✓
T2	185 - 170	7/8	5.00	4.83	265.1	0.6013	0.55	19.48	0.028 ¹ ✓

¹ P_u / φP_n controls

Top Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L _u ft	Kl/r	A in ²	P _u K	φP _n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1 1/4	5.00	4.83	185.6	1.2272	0.61	55.22	0.011 ¹ ✓
T2	185 - 170	1 1/4	5.00	4.83	185.6	1.2272	0.25	55.22	0.005 ¹ ✓

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¹ $P_u / \phi P_n$ controls

Bottom Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in^2	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T1	193 - 185	1 1/4	5.00	4.83	185.6	1.2272	0.74	55.22	0.013 ¹
T2	185 - 170	1 1/4	5.00	4.83	185.6	1.2272	1.17	55.22	0.021 ¹

¹ $P_u / \phi P_n$ controls

Mid Girt Design Data (Tension)

Section No.	Elevation ft	Size	L ft	L_u ft	Kl/r	A in^2	P_u K	ϕP_n K	Ratio $\frac{P_u}{\phi P_n}$
T2	185 - 170	1 1/4	5.00	4.83	185.6	1.2272	0.55	55.22	0.010 ¹

¹ $P_u / \phi P_n$ controls

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail
T1	193 - 185	Leg	2	1	-6.21	111.48	5.6	Pass
		Diagonal	1	11	-1.28	13.28	9.6	Pass
		Horizontal	7/8	23	-0.15	3.94	3.9	Pass
		Top Girt	1 1/4	5	-0.62	16.42	3.8	Pass
T2	185 - 170	Bottom Girt	1 1/4	8	-0.69	16.42	4.2	Pass
		Leg	2	32	-43.07	111.48	38.6	Pass
		Diagonal	1	44	-5.90	13.28	44.4	Pass
		Horizontal	7/8	48	-0.34	3.94	8.7	Pass
		Top Girt	1 1/4	33	-0.23	16.42	1.4	Pass
T3	170 - 160	Bottom Girt	1 1/4	36	-1.00	16.42	6.1	Pass
		Mid Girt	1 1/4	39	-0.36	16.42	2.2	Pass
		Leg	Pirod 105244	84	-52.85	142.49	51.2	Pass
		Diagonal	L2 1/2x2 1/2x3/16	87	-9.87	13.56	72.8	Pass
T4	160 - 140	Leg	Pirod 105217	93	-107.86	214.86	50.2	Pass
		Diagonal	L3x3x3/16	102	-10.20	18.18	56.1	Pass
T5	140 - 120	Leg	Pirod 105217	108	-152.48	214.86	71.0	Pass
		Diagonal	L3x3x3/16	111	-8.30	14.96	55.5	Pass
T6	120 - 100	Leg	Pirod 105218	123	-192.63	300.68	64.1	Pass

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Section No.	Elevation ft	Component Type	Size	Critical Element	P K	ϕP_{allow} K	% Capacity	Pass Fail	
T7	100 - 80	Diagonal	L3x3x5/16	126	-8.18	19.32	42.3	Pass	
		Leg	Pirod 105219	138	-230.18	399.87	57.6	Pass	
T8	80 - 60	Diagonal	L3x3x5/16	141	-8.26	15.76	52.4	Pass	
		Leg	Pirod 105219	153	-265.76	399.87	66.5	Pass	
T9	60 - 40	Diagonal	L3 1/2x3 1/2x5/16	158	-8.81	20.74	42.5	Pass	
		Leg	Pirod 105220	168	-300.52	512.38	58.7	Pass	
T10	40 - 20	Diagonal	L3 1/2x3 1/2x5/16	173	-8.92	17.15	60.3 (b)	Pass	
		Leg	Pirod 105220	183	-336.18	512.38	65.6	Pass	
T11	20 - 0	Diagonal	L3 1/2x3 1/2x5/16	194	-10.63	15.65	67.9	Pass	
		Leg	Pirod 112738	198	-349.82	613.14	57.1	Pass	
		Diagonal	2L3 1/2x3 1/2x5/16x1	203	-19.22	44.46	43.2	Pass	
							Summary		
							Leg (T5)	71.0	Pass
							Diagonal (T4)	87.3	Pass
							Horizontal (T2)	8.7	Pass
							Top Girt (T1)	3.8	Pass
							Bottom Girt (T2)	6.1	Pass
							Mid Girt (T2)	2.2	Pass
							Bolt Checks	87.3	Pass
							RATING =	87.3	Pass

MATHCAD CALCULATION PRINTOUT

EXISTING 195' SELF SUPPORT TOWER ANCHOR BOLT CHECK

REACTIONS ON THE FOUNDATION

As per Tnx output (see attached)

Down load; $P_v := 375 \cdot \text{kips}$ Shear; $V_u := 37 \cdot \text{kips}$

Uplift load; $P_{up} := 321 \cdot \text{kips}$ Moment; $M := 0 \cdot \text{kips} \cdot \text{ft}$

Anchor Rod Data is as per tower design by Pirod Inc., ENG. File No. A-115466 dated 04/01/1999

Number of Anchor Rods: $N_{\text{anchors}} := 6$

Diameter of Anchors: $D_{\text{anchors}} := 2.0 \text{in}$ $n := 4.5 \text{in}^{-1}$

Area of anchor bolts $A_b := \frac{\pi \cdot (D_{\text{anchors}})^2}{4} = 3.142 \cdot \text{in}^2$

Net Tensile Area of Anchors: $A_{\text{net}} := \frac{\pi}{4} \cdot \left(D_{\text{anchors}} - \frac{0.9743}{n} \right)^2 = 2.498 \cdot \text{in}^2$

Minimum Yield Stress $F_{Y\text{anchors}} := 105 \text{ksi}$
(Grade A354)

Ultimate Tensile Stress: $F_{U\text{anchors}} := 125 \text{ksi}$

Safety Factor for Anchor: $\phi_t := 0.8$ (Section 4.9.9, TIA-222-G Addendum 2)

Allowable Axial Load per Anchor: $T_{\text{cap}} := \phi_t \cdot F_{U\text{anchors}} \cdot A_{\text{net}}$
 $T_{\text{cap}} = 249.822 \cdot \text{kips}$

Interaction Equation for Anchor Rods as per Section 4.9.9, TIA-222-G Addendum 1 and Figure 4.4

For detail type (C) as per Figure 4.4 $\eta := 0.55$

$P_u := \text{if}(\eta > 0.5, P_{up}, P_v) = 321 \cdot \text{kips}$

Maximum Load on Anchor: $T_{\text{max}} := \frac{P_u + \frac{V_u}{\eta}}{N_{\text{anchors}}}$

$T_{\text{max}} = 64.712 \cdot \text{kips}$

Anchor Rod Capacity: $\frac{T_{\text{max}}}{T_{\text{cap}}} = 25.903\%$ OK!

Anchor_Rod_Check := if($T_{\text{max}} < T_{\text{cap}}$, "OK", "Not OK")

Anchor_Rod_Check = "OK"



Summary

-Foundation Reactions from Tower Base-

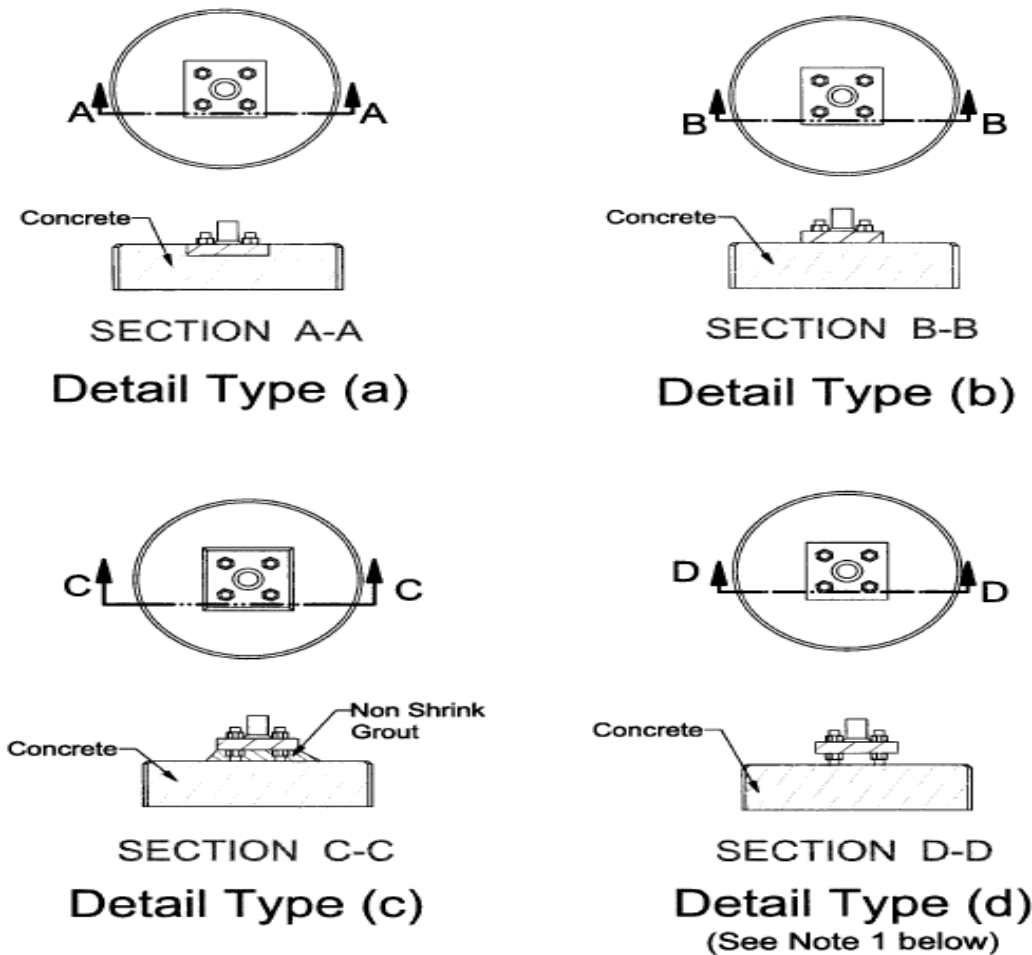
Shear	$V_u = 37 \cdot \text{kips}$
Down load	$P_v = 375 \cdot \text{kips}$
Uplift load	$P_{up} = 321 \cdot \text{kips}$
Moment	$M = 0 \cdot \text{ft} \cdot \text{kip}$

Anchor Rod Check $T_{max} = 64.712 \cdot \text{kips} < T_{cap} = 249.822 \cdot \text{kips}$

Anchor_Rod_Check := if($T_{max} < T_{cap}$, "OK" , "Not OK")

Anchor_Rod_Check = "OK"

ANSI/TIA-222-G



Note:

1. When clear distance from top of concrete to the bottom face of the leveling nut exceeds 1.5 times the diameter of the anchor rod, bending of the anchor rod shall be considered (refer to 4.9.9).

Figure 4-4: Anchor Rod Detail Types

4.9.9 Anchor Rods

For anchor rods, the following interaction equation shall be satisfied:

$$\left(\frac{P_u + \frac{V_u}{\eta}}{\phi R_{nt}} \right) \leq 1$$

where:

$$\phi = 0.80$$

P_u = tension force for detail types (a), (b) & (c) and larger of compression or tension force for type (d) as depicted in Figure 4-4.

V_u = shear force (direct shear and torsion components) corresponding to P_u

R_{nt} = nominal tensile strength of anchor rod as per 4.9.6.1

η = 0.90 for detail type (a)
 = 0.70 for detail type (b)
 = 0.55 for detail type (c)
 = 0.50 for detail type (d)

For detail type (d), when the clear distance from the top of concrete to the bottom leveling nut exceeds 1.0 times the diameter of the anchor rod, the following interaction equation shall also be satisfied:

$$\left(\frac{V_u}{\phi R_{nv}} \right)^2 + \left(\left| \frac{P_u}{\phi R_{nt}} \right| + \left| \frac{M_u}{\phi R_{nm}} \right| \right)^2 \leq 1$$

where:

M_u = bending moment corresponding to V_u
 = $0.65 l_{ar} V_u$

l_{ar} = length from top of concrete to bottom of anchor rod leveling nut

Addendum 1

ϕR_{nv} = design shear strength of anchor rod as per 4.9.6.3

ϕR_{nm} = design flexural strength of anchor rod in accordance with 4.7.1 using the tensile root diameter for the determination of z

d_r = tensile root diameter of rod, in [mm]
 = $d - 0.9743/n$ inches
 = $d - 0.9382(p)$ mm

d = nominal rod diameter, in [mm]

n = number of threads per inch

p = pitch of threads, mm

4.9.6.3 Design Shear Strength

The design shear strength of a bolt, ϕR_{nv} , shall be taken as:

$$\phi = 0.75$$

(a) When threads are excluded from the shear plane:

$$R_{nv} = 0.55 F_{ub} A_b$$

(b) When threads are included in the shear plane:

$$R_{nv} = 0.45 F_{ub} A_b$$

where:

F_{ub} = Specified minimum tensile strength of bolt

A_b = nominal unthreaded area of bolt

4.7.1 Solid Round Members

For solid round members, M_n shall be determined as follows:

$$M_n = F_y' Z$$

where:

F_y' = effective yield stress as determined from 4.5.4.1

Z = plastic section modulus

4.5.4.1 Effective Yield Stress

For 60° and 90° angle members, the effective yield stress for axial compression, F_y' , shall be determined as follows:

$$w/t \leq 0.47 \sqrt{\frac{E}{F_y}}$$

$$F_y' = F_y$$

$$0.47 \sqrt{\frac{E}{F_y}} < w/t \leq 0.85 \sqrt{\frac{E}{F_y}}$$

$$F_y' = \left[1.677 - 0.677 \left(\frac{w/t}{0.47 \sqrt{E/F_y}} \right) \right] F_y$$

$$0.85 \sqrt{\frac{E}{F_y}} < w/t \leq 25$$

$$F_y' = [0.0332 \pi^2 E / (w/t)^2]$$

The width to thickness ratio (w/t) shall not exceed 25 for angle members (refer to Figure 4-3).

For solid round members, the effective yield stress, F_y' , shall be equal to F_y .

For tubular round members, the diameter to thickness ratio (D/t) shall not exceed 400. The effective yield stress, F_y' , shall be determined as follows:

$$D/t \leq 0.114 E/F_y$$

$$F_y' = F_y$$

$$0.114 E/F_y < D/t \leq 0.448 E/F_y$$

$$F_y' = \left(\frac{0.0379E}{(D/t)F_y} + \frac{2}{3} \right) F_y$$

$$0.448 E/F_y < D/t \leq 400$$

$$F_y' = \frac{0.337E}{(D/t)}$$

Existing 195 ft. Self Support Tower Foundation Check

Customer Name: SBA Communications Corporation

Customer Site Name: Bozrah

Customer Site ID: CT01105-S-02

Carrier Name: Sprint Nextel

Foundation check

-Foundation Reactions-

(As per TNX output results from the Tower Structural Analysis by Allpro Consulting Group Inc.)

Total Shear	$S := 58 \cdot \text{kips}$	Compression on Pedestal:	$P_c := 375 \cdot \text{kips}$
Moment	$M := 6810 \cdot \text{ft}_K$	Uplift on Pedestal:	$P_{up} := 321 \cdot \text{kips}$
Down load, Tower weight	$P_v := 73 \cdot \text{kips}$	Shear on Pedestal:	$Sh := 43 \cdot \text{kips}$

-Soil Properties- Soil data is as per Geotechnical Report by Jaworski Geotech, Inc.. Projetc # C98492G, dated 12/14/1998

Factor of Saftey	$FS_b := 3$
Allowable Bearing Capacity	$Brg_{all} := 20 \text{ksf}$
Ultimate Bearing Capacity	$Brg_{ult} := FS_b \cdot Brg_{all} = 60 \cdot \text{ksf}$
Internal angle of friction for soil,	$\phi := 30 \cdot \text{deg}$ (Reduced Internal Friction due to backfill Actual 34 deg)
Unit wt. of soil,	$\gamma_s := 0.170 \cdot \text{kcf}$
Alowable Passive Pressure	see next page
Cohesion of soil,	$c_u := 0 \cdot \text{kcf}$
Friction Factor	$FF := 0.7$
Depth to be neglected	$L_{neg} := 1.5 \text{ft}$ (frost depth)

-Material Parameters-

Conforming to the design requirements as in ACI 318-10

Unit wt. of concrete,	$\gamma_c := 0.150 \cdot \text{kcf}$
Concrete compressive strength,	$f_c := 3000 \cdot \text{psi}$
Rebar yield strength,	$f_y := 60000 \cdot \text{psi}$

-Factor of Safety for soil strength-

$\phi_{s_bear} := 0.75$	as per TIA-222-G code for bearing, 9.4.1
$\phi_{s_friction} := 0.75$	as per TIA-222-G code for skin friction resistance, 9.4.1
$\phi_{s_lateral} := 0.75$	as per TIA-222-G code for lateral resistance, 9.4.1
$\phi_{s_uplift} := 0.75$	as per TIA-222-G code for lateral resistance, 9.4.1

DIMENSIONS

Dimensions of foundation as per Foundation design by Pirod Inc., Job No. A-115466 dated 04/01/1999

Tower face width	$TW_{FW} := 22 \cdot \text{ft}$	Tower ht.	$TW_{ht} := 195 \cdot \text{ft}$
------------------	---------------------------------	-----------	----------------------------------

The tower location is eccentric by $L_{pe} := 3.177 \cdot \text{ft}$

Type of column, col.t=0 for circular,=1 for rectangular/square $col_t := 0$

Depth of mat, $D_f := 4.5 \cdot \text{ft}$

Thickness of mat, $T_f := 5 \cdot \text{ft}$

Pedestal size,	$Ped_s := 0 \cdot \text{ft}$	No. of pedestals	$N_{ped} := 3$
----------------	------------------------------	------------------	----------------

Extension above the grade, $E_g := 0.5 \cdot \text{ft}$

Mat Dimensions, LxB $L := 32.5 \cdot \text{ft}$ x $B := 32.5 \cdot \text{ft}$

-Reinforcement Data-

Typical concrete cover $cc := 3 \text{in}$

MAT CALCULATIONS

$K_p := 5$ (As per Geotechnical Report)

$$P_{\text{pave}} := \frac{(D_f - T_f - L_{\text{neg}}) \cdot K_p \cdot \gamma_s + (D_f - L_{\text{neg}}) \cdot K_p \cdot \gamma_s}{2} \quad P_{\text{pave}} = 0.425 \cdot \text{ksf}$$

Safety against overturning and location of resultant on the base

Resisting Moments about mid axis parallel to base $\text{Area}_{\text{ped}} := \text{if} \left(\text{col}_t = 1, \text{Ped}_s^2, \frac{\pi}{4} \cdot \text{Ped}_s^2 \right) \quad \text{Area}_{\text{ped}} = 0$

component	value, kips	lever arm, ft	resisting moment, ft-kips
1) Concrete wt.	$C_w := L \cdot B \cdot T_f \cdot (\gamma_c) + \text{Area}_{\text{ped}} \cdot \gamma_c \cdot (D_f + E_g - T_f) \cdot N_{\text{ped}}$ $C_w = 792.187 \cdot \text{kips}$	$L_c := \frac{L}{2}$ $L_c = 16.25 \text{ ft}$	$R_c := C_w \cdot L_c$ $R_c = 12873.047 \cdot \text{ft}_K$
2) Soil wt.	$S_w := 0$ $S_w = 0 \cdot \text{kips}$	$L_s := \frac{L}{2}$ $L_s = 16.25 \text{ ft}$	$R_s := S_w \cdot L_s$ $R_s = 0 \cdot \text{ft}_K$
3) Wt. of soil wedge	$W_w := (D_f) \cdot \frac{1}{2} \cdot (D_f \cdot \tan(\phi)) \cdot B \cdot (\gamma_s)$ $W_w = 32.297 \cdot \text{kips}$	$L_w := \left(L + D_f \cdot \frac{\tan(\phi)}{3} \right)$ $L_w = 33.366 \text{ ft}$	$R_w := W_w \cdot L_w$ $R_w = 1077.634 \cdot \text{ft}_K$
4) Passive pressure	$Pe_p := T_f \cdot B \cdot P_{\text{pave}}$ $Pe_p = 69.063 \cdot \text{kips}$	$L_p := \frac{T_f}{3}$ $L_p = 1.667 \text{ ft}$	$R_p := Pe_p \cdot L_p$ $R_p = 115.104 \cdot \text{ft}_K$
5) Vertical	$P_v = 73 \cdot \text{kips}$ $S_{w1} := L \cdot B \cdot D_f \cdot \gamma_s \quad S_{w1} = 808.031 \cdot \text{kips} \quad \text{---- for net calcs}$	$L_v := \frac{L}{2}$	$R_v := P_v \cdot L_v$
Total weight	$T_w := C_w + S_w + W_w + P_v$ $T_w = 897.485 \cdot \text{kips}$	$L_v = 16.25 \text{ ft}$	$R_v = 1186.25 \cdot \text{ft}_K$
Total resisting Moment=	$M_r := R_c + R_s + R_w + R_p + R_v$	$M_r = 15252.035 \cdot \text{ft}_K$	

<u>Overturing Moments component</u>	value, kips	lever arm, ft	Overturing Moment ft-kips
1) Moment on foundation due to eccentric location of tower	$P_v = 73 \cdot \text{kips}$	$L_{pe} = 3.177 \text{ ft}$	$M_{pe} := L_{pe} \cdot P_v$ $M_{pe} = 231.921 \cdot \text{ft}_K$
2) Moment on foundation	-	-	$M = 6810 \cdot \text{ft}_K$
3) Moment due to horizontal shear	$S_t := S$	$L_{hs} := D_f + E_g$ $L_{hs} = 5 \text{ ft}$	$O_{hs} := L_{hs} \cdot S_t$ $O_{hs} = 290 \cdot \text{ft}_K$
Total Overturing Moment=		$M_o := M + O_{hs} + M_{pe}$	$M_o = 7331.921 \cdot \text{ft}_K$

Check Safety Factor against Overturing about mid axis parallel to base

$$SF := \frac{M_r}{M_o} \quad SF = 2.08 > 1.5 \quad \text{O.K.}!$$

Calculate eccentricity, e

$$e := \frac{M_o}{T_w} \quad e = 8.169 \text{ ft}$$

Check location of eccentricity and determine pressure distribution under the mat

$$L_{loc} := \frac{L}{6} \quad L_{loc} = 5.417 \text{ ft} \quad \text{For net bearing calcs } T_{w1} := S_{w1} + W_w \quad T_{w1} = 840.329 \cdot \text{kips}$$

$$P_{max1} := \text{if} \left[e \leq L_{loc}, \frac{T_w}{L \cdot B} \cdot \left[1 + \left(6 \cdot \frac{e}{L} \right) \right], 4 \cdot \frac{T_w}{3 \cdot B \cdot (L - 2 \cdot e)} \right] \quad P_{max1} = 2.278 \cdot \text{ksf}$$

$$P_{max2} := \left(\frac{T_{w1}}{L \cdot B} \right) \quad P_{max2} = 0.796 \cdot \text{ksf} \quad P_{net} := P_{max1} - P_{max2} \quad P_{max} := P_{net}$$

Net soil pressure, $P_{net} = 1.483 \cdot \text{ksf} < Brg_{ult} \cdot \phi_s_{Bear} = 45 \cdot \text{ksf} \quad \text{O.K.}!$

$$P_{min} := \text{if} \left[e \leq L_{loc}, \frac{T_w}{L \cdot B} \cdot \left[1 - \left(6 \cdot \frac{e}{L} \right) \right], 0 \cdot \text{ksf} \right] \quad P_{min} = 0 \cdot \text{ksf}$$

Check for horizontal shear $P_{hor} := P_e + (P_v + C_w + S_w) \cdot FF$

$$P_{hor} = 674.694 \cdot \text{kips} > S = 58 \cdot \text{kips} \quad \text{Since } P_{hor} < S \quad \text{It is safe!}$$

REINFORCED CONCRETE DESIGN CALCULATIONS

General Input parameters

Concrete Cover $\overset{www}{cc} := 3.0 \cdot \text{in}$

Reduction factors as per respective ACI sections

$\phi_{\text{shear}} := 0.75$	as per ACI 9.3.2.3	Reinforced concrete load	$RC_{\text{fac}} := 1.0$
$\phi_{\text{compr}} := 0.75$	as per ACI 9.3.2.2	factor as per EIA 3.1.16	
$\phi_{\text{axten}} := 0.9$	as per ACI 9.3.2.2 a		(Loads already factored under TIA/EIA-222-G Code)

Check for wide beam or single shear in mat

Allowable shear stress in concrete for wide beam shear criteria=

$$\nu_{\text{wide}} := 2 \cdot \phi_{\text{shear}} \cdot \sqrt{f_c \cdot \text{psi}} \quad \nu_{\text{wide}} = 82.158 \cdot \text{psi}$$

Effective depth of steel $d := T_f - cc \quad d = 57 \cdot \text{in}$ $L_{\text{eff}} := \text{if}(e \leq L_{\text{loc}}, L, L - 2 \cdot e) \quad L_{\text{eff}} = 16.161 \text{ ft}$

$$\text{dist} := \text{if} \left[N_{\text{ped}} = 3, \left(\frac{L}{2} - \frac{1}{3} \cdot \sin(60 \cdot \text{deg}) \cdot \text{TWW} - \frac{1}{2} \cdot \text{Ped}_s - d \right), \left(\frac{L}{2} - \frac{\text{TWW}}{2} - \frac{1}{2} \cdot \text{Ped}_s - d \right) \right]$$

Factor load by RC $P_{\text{maxf}} := P_{\text{max}} \cdot RC_{\text{fac}} \quad P_{\text{minf}} := P_{\text{min}} \cdot RC_{\text{fac}}$

shear on the face of concrete=

$$\text{Shear}_{\text{wide}} := (\text{dist}) \cdot B \cdot \left[\frac{P_{\text{maxf}} + \left[P_{\text{maxf}} - \frac{P_{\text{maxf}} - P_{\text{minf}}}{L_{\text{eff}}} \cdot (\text{dist}) \right]}{2} \right] \quad \text{Shear}_{\text{wide}} = 208.6 \cdot \text{kips}$$

Area of concrete in shear $A_{\text{shear}} := B \cdot d \quad A_{\text{shear}} = 22230 \cdot \text{in}^2$

$$\text{Shear stress acting on concrete fa} \nu_{\text{act}} := \frac{\text{Shear}_{\text{wide}}}{A_{\text{shear}}} \quad \nu_{\text{act}} = 9.384 \cdot \text{psi}$$

$\nu_{\text{act}} = 9.384 \cdot \text{psi} < \nu_{\text{wide}} = 82.158 \cdot \text{psi} \quad \mathbf{O.K!}$

Check for punching or two-way shear in mat

Calculate allowable shear stress in concrete for punching/two-way shear

$$\beta := \frac{L}{B} \quad \beta = 1$$

$$\nu_{\text{punch}} := \text{if} \left[\left(2 + \frac{4}{\beta} \right) \cdot \phi_{\text{shear}} \cdot \sqrt{f_c \cdot \text{psi}} \leq 4 \cdot \phi_{\text{shear}} \cdot \sqrt{f_c \cdot \text{psi}}, \left(2 + \frac{4}{\beta} \right) \cdot \phi_{\text{shear}} \cdot \sqrt{f_c \cdot \text{psi}}, 4 \cdot \phi_{\text{shear}} \cdot \sqrt{f_c \cdot \text{psi}} \right]$$

$$\nu_{\text{punch}} = 164.317 \cdot \text{psi} \quad \text{Area}_{\text{col}} := \text{if} \left[\text{col}_t = 0, \frac{\pi}{4} \cdot (\text{Ped}_s + d)^2, (\text{Ped}_s + d)^2 \right]$$

$$P_{\text{avg}} := \frac{P_{\text{maxf}} + P_{\text{minf}}}{2} \quad \text{Peri}_{\text{col}} := \text{if} \left[\text{col}_t = 0, 2 \cdot \pi \cdot \frac{\text{Ped}_s + d}{2}, 4 \cdot (\text{Ped}_s + d) \right]$$

Factor vertical load $P_vf := RC_{fac} \cdot P_v$

Shear stress acting on the concrete face= $\nu_{act} := \frac{P_c - Area_{col} \cdot P_{avg}}{Peri_{col} \cdot d \cdot 4}$

$\nu_{act} = 8.863 \cdot \text{psi} < \nu_{punch} = 164.317 \cdot \text{psi} \quad \text{O.K!}$

Design of mat footing $C_{wped} := Area_{ped} \cdot \gamma_c \cdot (D_f + E_g - T_f) \cdot N_{ped}$ Wt. of concrete pedestals

$P_{upnet} := P_{up} - \frac{C_{wped} + S_w \cdot 0.95}{N_{ped}} \quad P_{upnet} = 321 \cdot \text{kips}$ Net uplift acting at mat level creating bending

Calculate bending moment for mat design:

$\phi_{bend} := 0.9 \quad L_{angle} := \text{if}(N_{ped} = 3, \sin(60 \cdot \text{deg}), 1)$ moment in the slab. Soil wt. reduced by 5 % to account for variation in compaction . ACI 9.3.2.2

$\beta_1 := \text{if} \left[f_c \leq 4000 \cdot \text{psi}, 0.85, \text{if} \left[f_c \geq 8000 \cdot \text{psi}, 0.65, 0.85 - \left(\frac{f_c}{\text{psi}} - 4000 \right) \cdot 0.05 \right] \right]$ ACI 10.2.7.3

$B_{mo} := RC_{fac} \cdot \left[(T_{FW} \cdot P_{upnet}) \cdot L_{angle} + S_t \cdot (D_f + E_g) \right] \quad B_{mo} = 6405.871 \cdot \text{ft}_K$

$B_{mo1} := \frac{P_{max} - P_{min}}{(L - 2 \cdot e) \cdot 2} \cdot \left(T_{FW} \cdot L_{angle} \cdot \frac{1}{3} + \frac{Ped_s}{2} \right) \cdot \left[\left[(L - 2 \cdot e) - \left(T_{FW} \cdot L_{angle} \cdot \frac{1}{3} + \frac{Ped_s}{2} \right) \right]^2 \cdot 0.5 \right] \cdot B$

$W_e := T_{FW} \cdot L_{angle} + Ped_s \quad W_e = 19.053 \text{ ft}$ Reinforcement middle bandwidth. $B_{mo1} = 455624.425 \text{ ft} \cdot \text{lb}$

required $R_u \quad R_u := \frac{B_{mo}}{\phi_{bend} \cdot B \cdot d} \quad R_u = 67.407 \cdot \text{psi} \quad m := \frac{f_y}{\beta_1 \cdot f_c} \quad m = 23.529$

required

$\rho := \frac{1}{m} \cdot \left[1 - \sqrt{1 - \left(\frac{2 \cdot m \cdot R_u}{f_y} \right)} \right] \quad \rho = 0.001$

required area of steel for mat=

$A_{stf} := \rho \cdot B \cdot d \quad A_{stf} = 25.313 \cdot \text{in}^2$

minimum area of steel required,

$A_{stminf} := .0018 \cdot B \cdot T_f \quad A_{stminf} = 42.12 \cdot \text{in}^2$ per ACI 10.5.3 & 7.12

$A_{stfuse} := \text{if}(A_{stf} > A_{stminf}, A_{stf}, A_{stminf}) \quad A_{stfuse} = 42.12 \cdot \text{in}^2$

bar size used $f_{bar} := 11 \quad f_{dia} := \frac{f_{bar}}{8} \cdot \text{in} \quad f_{dia} = 1.375 \cdot \text{in}$

Bar area= $f_{abar} := \pi \cdot \frac{f_{dia}^2}{4} \quad f_{abar} = 1.485 \cdot \text{in}^2$

Number of bars required= $Nf_{bars} := \text{if} \left(A_{stfuse} = A_{stminf}, \frac{A_{stfuse}}{f_{abar}}, \frac{A_{stfuse}}{f_{abar}} \cdot \frac{L}{W_e} \right) \quad Nf_{bars} = 28.366$

(Total 49 Horizontal bars provided each way, Top and Bottom Total = 196)

Nfbars := 49 OK !

Summary

-Foundation Reactions-

Shear $S = 58 \cdot \text{kips}$
 Down load $P_v = 73 \cdot \text{kips}$ (Weight)
 Uplift load $P_{up} = 321 \cdot \text{kips}$
 Moment; $M = 6810 \cdot \text{ft} \cdot \text{kip}$

Size of Mat

$L = 32.5 \text{ ft}$ $B = 32.5 \text{ ft}$
 Depth of base of mat $D_f = 4.5 \text{ ft}$ Thickness of Mat $T_f = 5 \text{ ft}$
 Pedestal size $Ped_s = 0$

The tower location is eccentric by $L_{pe} = 3.177 \text{ ft}$ with respect to the mat foundation center towards the base

Stability Calculations

Safety Factor against Overturning	$SF = 2.08$	$>$	1.5	$\frac{1.5}{SF} = 72.11\%$	O.K.!
Net soil pressure	$P_{net} = 1.483 \cdot \text{ksf}$	$<$	$Brg_{ult} \cdot \phi_{s_Bear} = 45 \cdot \text{ksf}$	$\frac{P_{net}}{Brg_{ult} \cdot \phi_{s_Bear}} = 3.29\%$	O.K.!
Check for horizontal shear	$P_{hor} = 674.694 \cdot \text{kips}$	$>$	$S = 58 \cdot \text{kips}$	$\frac{S}{P_{hor}} = 8.6\%$	O.K.!

SPECIAL CONSTRUCTION NOTE:
 SPRINT WORK IS CONTINGENT ON THE FOLLOWING:
 * COMPLETION OF A GLOBAL STRUCTURAL STABILITY ANALYSIS.
 * COMPLETION OF AN ANTENNA/RRH MOUNT STRUCTURAL ASSESSMENT.
 * GC SHALL FURNISH, INSTALL AND COMPLETE ALL REQUIRED STRUCTURAL MODIFICATIONS AS INDICATED IN BEFORE-MENTIONED ANALYSIS AND ASSESSMENT.



PROGRAM: DO MACRO UPGRADE
EQUIPMENT DEPLOYMENT

SITE NUMBER: CT33XC574

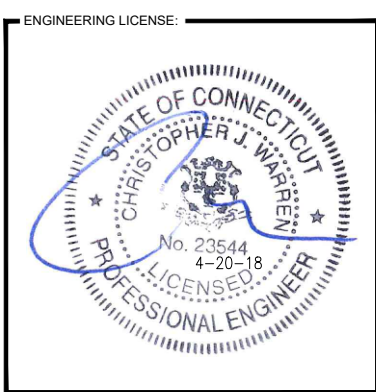
SITE ADDRESS: 131 GIFFORD LANE
BOZRAH, CT 06334

SITE TYPE: EXISTING 195' SELF SUPPORT TOWER

PLANS PREPARED FOR:
Sprint
 INTERNATIONAL BLVD, SUITE 800
 MAHWAH, NJ 07495
 TEL: (800) 357-7641

PROJECT MANAGER:
SBA
 SBA COMMUNICATIONS CORP.
 134 FLANDERS ROAD, SUITE 125
 WESTBOROUGH, MA 01581
 TEL: (508) 251-0720

PLANS PREPARED BY:
INFINIGY
 FROM ZERO TO INFINIGY
 the solutions are endless
 1033 Watervliet Shaker Rd | Albany, NY 12205
 Phone: 518-690-0790 | Fax: 518-690-0793
 www.infinigy.com
 JOB NUMBER 526-104



CHECKED BY:

APPROVED BY:

REVISIONS:	DESCRIPTION	DATE	BY	REV.
	ISSUED FOR CONSTRUCTION	03/22/18	SL	0
	ISSUED FOR REVIEW	01/18/18	RCD	A

SITE NUMBER:
CT33XC574

SITE ADDRESS:
 131 GIFFORD LANE,
 BOZRAH, CT 06334

SHEET DESCRIPTION:
TITLE SHEET & PROJECT DATA

SHEET NUMBER:
T-1

PROJECT INFORMATION

SITE INFORMATION:
 LATITUDE: 41° 33' .0893" N
 (PER SBA RECORDS) 41.55251667"
 LONGITUDE: -72° 09' 02.73" W
 (PER SBA RECORDS) -72.15070833"
 STRUCTURE HEIGHT: 195'±
 STRUCTURE TYPE: SELF SUPPORT TOWER

APPLICANT:
 SPRINT
 1 INTERNATIONAL BLVD, SUITE 800
 MAHWAH, NJ 07495

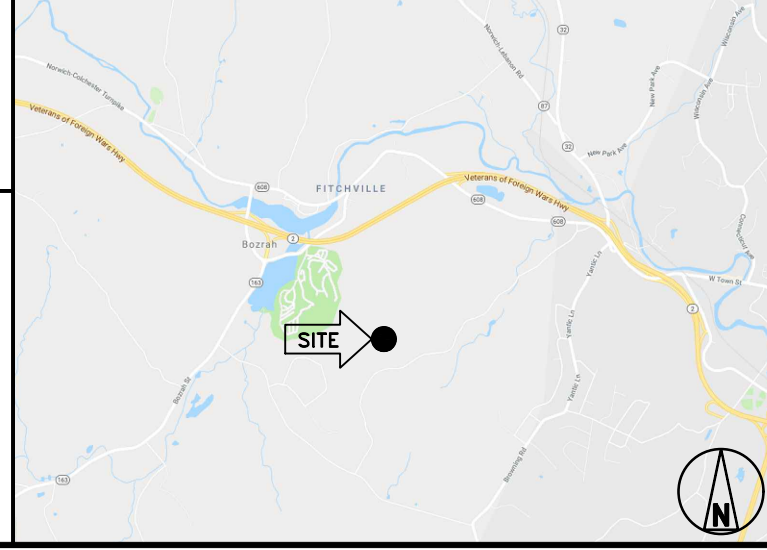
TOWER OWNER:
 SBA TOWERS LLC.
 8051 CONGRESS AVENUE
 BOCA RATON, FL 33487

SBA SITE ID: CT01105-S
 SBA SITE NAME: BOZRAH
 SBA CONTACT: STEPHEN ROTH
 (860) 539-4920
 sroth@sbsite.com

AREA MAP



LOCATION MAP



PROJECT DESCRIPTION

SPRINT PROPOSES TO MODIFY AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY.

- REMOVE (6) PANEL ANTENNAS
- INSTALL (6) PANEL ANTENNAS
- INSTALL (3) 2.5 GHz RRH'S ON PROPOSED DUAL RRH MOUNT
- RELOCATE (3) 1900 MHz RRH'S ON PROPOSED DUAL RRH MOUNT
- INSTALL (6) 800 MHz RRH'S ON PROPOSED DUAL RRH MOUNT
- INSTALL (4) HYBRID CABLES
- INSTALL STRUCTURAL AUGMENTS
- INSTALL RAN EQUIPMENT INSIDE EXISTING MMBTS CABINET
- REMOVE (4) RUNS OF EXISTING 1-5/8" COAX

THESE PLANS HAVE BEEN DEVELOPED FOR THE MODIFICATION OF AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY OWNED OR LEASED BY SPRINT IN ACCORDANCE WITH THE SCOPE OF WORK PROVIDED BY SPRINT. INFINIGY HAS INCORPORATED THIS SCOPE OF WORK IN THE PLANS. THESE PLANS ARE NOT FOR CONSTRUCTION UNLESS ACCOMPANIED BY A PASSING STRUCTURAL STABILITY ANALYSIS PREPARED BY A LICENSED STRUCTURAL ENGINEER. STRUCTURAL ANALYSIS MUST INCLUDE BOTH TOWER AND MOUNT.

APPLICABLE CODES

ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALL IN ACCORDANCE WITH THE CURRENT EDITIONS OF THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES.

- INTERNATIONAL BUILDING CODE (2012 IBC)
- TIA-222-G OR LATEST EDITION
- NFPA 780 - LIGHTNING PROTECTION CODE
- 2014 NATIONAL ELECTRIC CODE OR LATEST EDITION
- ANY OTHER NATIONAL OR LOCAL APPLICABLE CODES, MOST RECENT EDITIONS
- CT BUILDING CODE
- LOCAL BUILDING CODE
- CITY/COUNTY ORDINANCES

GENERAL NOTES

- THIS IS AN UNMANNED TELECOMMUNICATION FACILITY AND NOT FOR HUMAN HABITATION:
 - ADA COMPLIANCE NOT REQUIRED.
 - POTABLE WATER OR SANITARY SERVICE IS NOT REQUIRED.
 - NO OUTDOOR STORAGE OR ANY SOLID WASTE RECEPTACLES REQUIRED.
- CONTRACTOR SHALL VERIFY ALL PLANS, EXISTING DIMENSIONS, AND CONDITIONS ON JOB SITE. CONTRACTOR SHALL IMMEDIATELY NOTIFY THE ARCHITECT/ENGINEER IN WRITING OF ANY DISCREPANCIES BEFORE PROCEEDING WITH THE WORK. FAILURE TO NOTIFY THE ARCHITECT/ENGINEER PLACE THE RESPONSIBILITY ON THE CONTRACTOR TO CORRECT THE DISCREPANCIES AT THE CONTRACTOR'S EXPENSE.

DRAWING INDEX

SHEET NO.	SHEET TITLE	REV.
T-1	TITLE SHEET & PROJECT DATA	0
SP-1	OUTLINE SPECIFICATIONS	0
SP-2	OUTLINE SPECIFICATIONS	0
SP-3	OUTLINE SPECIFICATIONS	0
A-1	SITE PLAN	0
A-2	TOWER ELEVATION	0
A-3	ANTENNA LAYOUT & MOUNTING DETAILS	0
A-4	EQUIPMENT & MOUNTING DETAILS	0
A-5	DETAILS	0
E-1	ELECTRICAL & GROUNDING DETAILS	0
RF-1	RF DATA SHEET	0
RF-2	PLUMBING DIAGRAM	0

APPROVALS

TITLE	SIGNATURE	DATE
PROJECT MANAGER:		
CONSTRUCTION:		
RF ENGINEER:		
ZONING/SITE ACQ:		
OPERATIONS:		
TOWER OWNER:		

THE FOLLOWING PARTIES HEREBY APPROVE AND ACCEPT THESE DOCUMENTS AND AUTHORIZE THE CONTRACTOR TO PROCEED WITH THE CONSTRUCTION DESCRIBED HEREIN. ALL DOCUMENTS ARE SUBJECT TO REVIEW BY THE LOCAL BUILDING DEPARTMENT AND MAY IMPOSE CHANGES OR MODIFICATIONS.

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CONTINUE FROM SP-1

1. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
2. PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS.
3. MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND TELCO BACKHAUL.
4. INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS, AND UNDERGROUND GROUNDING SYSTEM.
5. INSTALL ABOVE GROUND GROUNDING SYSTEMS.
6. PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
7. INSTALL "H-FRAMES", CABINETS AND SHELTERS AS INDICATED.
8. INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
9. ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.
10. PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS.
11. PROVIDE SLABS AND EQUIPMENT PLATFORMS.
12. INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS.
13. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
14. CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER
15. INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
16. INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
17. INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
18. PERFORM, DOCUMENT, AND CLOSE OUT ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
19. PERFORM ANTENNA AND COAX SWEEP TESTING AND MAKE ANY AND ALL NECESSARY CORRECTIONS.
20. REMAIN ON SITE MOBILIZED THROUGHOUT HAND-OFF AND INTEGRATION TO ASSIST AS NEEDED UNTIL SITE IS DEEMED SUBSTANTIALLY COMPLETE AND PLACED "ON AIR."

3.2 GENERAL REQUIREMENTS FOR CIVIL CONSTRUCTION:

- A. CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B. EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS.
- C. CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS CONDITION.
 1. IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.
 2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT, OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD.
- D. CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION
- E. CONDUCT TESTING AS REQUIRED HEREIN.

3.3 DELIVERABLES:

- A. CONTRACTOR SHALL REVIEW, APPROVE, AND SUBMIT TO SPRINT SHOP DRAWINGS, PRODUCT DATA, SAMPLES, AND SIMILAR SUBMITTALS AS REQUIRED HEREINAFTER
- B. PROVIDE DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
 1. ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
 2. PROJECT PROGRESS REPORTS.
 3. CIVIL CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
 4. ELECTRICAL SERVICE COMPLETION DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).

5. LINES AND ANTENNA INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
6. POWER INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
7. TELCO READY DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
8. PPC (OR SHELTER) INSTALL DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
9. TOWER CONSTRUCTION START DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
10. TOWER CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
11. BTS AND RADIO EQUIPMENT DELIVERED AT SITE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
12. NETWORK OPERATIONS HANDOFF CHECKLIST (HOC WALK) COMPLETE (UPLOAD FORM IN SMS)
13. CIVIL CONSTRUCTION COMPLETE DATE (POPULATE FIELD IN SMS AND/OR FORWARD NOTIFICATION).
14. SITE CONSTRUCTION PROGRESS PHOTOS UNLOADED INTO SMS.

SECTION 01 400 - SUBMITTALS & TESTS

PART 1 - GENERAL

- 1.1 THE WORK: THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE OTHER CONTRACT DOCUMENTS AND THE CONSTRUCTION DRAWINGS DESCRIBE THE WORK TO BE PERFORMED BY THE CONTRACTOR.
- 1.2 RELATED DOCUMENTS:
 - A. THE REQUIREMENTS OF THIS SECTION APPLY TO ALL SECTIONS IN THIS SPECIFICATION.
 - B. SPRINT "STANDARD CONSTRUCTION DETAILS FOR WIRELESS SITES" ARE INCLUDED IN AND MADE A PART OF THESE SPECIFICATIONS HERewith.
- 1.3 SUBMITTALS:
 - A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE SPECIFICATIONS.
 - B. SUBMIT THE FOLLOWING TO COMPANY REPRESENTATIVE FOR APPROVAL.
 1. CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING.
 2. CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
 3. SPECIAL FINISHES FOR INTERIOR SPACES, IF ANY.
 4. ALL EQUIPMENT AND MATERIALS SO IDENTIFIED ON THE CONSTRUCTION DRAWINGS.
 5. CHEMICAL GROUNDING DESIGN
 - D. ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

1.4 TESTS AND INSPECTIONS:

- A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT DOCUMENTATION.
- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. COAX SWEEPS AND FIBER TESTS PER TS-0200 REV 4 ANTENNA LINE ACCEPTANCE STANDARDS.
 2. AGL, AZIMUTH AND DOWNTILT USING ELECTRONIC COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL.
 3. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
- C. REQUIRED CLOSEOUT DOCUMENTATION INCLUDES, BUT IS NOT LIMITED TO THE FOLLOWING:
 1. AZIMUTH, DOWNTILT, AGL - UPLOAD REPORT FROM ANTENNA ALIGNMENT TOOL TO SITERRA TASK 465. INSTALLED AZIMUTH, DOWNTILT, AND AGL MUST CONFORM TO THE RF DATA SHEETS. SWEEP AND FIBER TESTS
 2. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT
 3. ALL AVAILABLE JURISDICTIONAL INFORMATION
 4. PDF SCAN OF REDLINES PRODUCED IN FIELD

5. ELECTRONIC AS-BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS. ANY FIELD CHANGE MUST BE REFLECTED BY MODIFYING THE PLANS, ELEVATIONS, AND DETAILS IN THE DRAWING SETS. GENERAL NOTES INDICATING MODIFICATIONS WILL NOT BE ACCEPTED. CHANGES SHALL BE HIGHLIGHTED AS "CLOUDS" IDENTIFIED AS THE "AS-BUILT" CONDITION.
6. LIEN WAIVERS
7. FINAL PAYMENT APPLICATION
8. REQUIRED FINAL CONSTRUCTION PHOTOS
9. CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS
10. ALL POST NTP TASKS INCLUDING DOCUMENT UPLOADS COMPLETED IN SITERRA (SPRINTS DOCUMENT REPOSITORY OF RECORD).

1.5 COMMISSIONING: PERFORM ALL COMMISSIONING AS REQUIRED BY APPLICABLE MOPs

1.6 INTEGRATION: PERFORM ALL INTEGRATION ACTIVITIES AS REQUIRED BY APPLICABLE MOPs

PART 2 - PRODUCTS (NOT USED)

PART 3 - EXECUTION

3.1 REQUIREMENTS FOR TESTING:

A. THIRD PARTY TESTING AGENCY:

1. WHEN THE USE OF A THIRD PARTY INDEPENDENT TESTING AGENCY IS REQUIRED, THE AGENCY THAT IS SELECTED MUST PERFORM SUCH WORK ON A REGULAR BASIS IN THE STATE WHERE THE PROJECT IS LOCATED AND HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.
2. THE THIRD PARTY TESTING AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE, EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.
3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.
4. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM, AASJTO, AND OTHER METHODS IS NEEDED.

3.2 REQUIRED TESTS:

- A. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. CONCRETE CYLINDER BREAK TESTS FOR THE TOWER AND ANCHOR FOUNDATIONS AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
 2. ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED IN SECTION: HOT MIX ASPHALT PAVING.
 3. FIELD QUALITY CONTROL TESTING AS SPECIFIED IN SECTION: PORTLAND CEMENT CONCRETE PAVING.
 4. TESTING REQUIRED UNDER SECTION: AGGREGATE BASE FOR ACCESS ROADS, PADS AND ANCHOR LOCATIONS
 5. STRUCTURAL BACKFILL COMPACTION TESTS FOR THE TOWER FOUNDATION.
 6. SITE RESISTANCE TO EARTH TESTING PER EXHIBIT: CELL SITE GROUNDING SYSTEM DESIGN.
 7. ANTENNA AND COAX SWEEP TESTS PER EXHIBIT: ANTENNA TRANSMISSION LINE ACCEPTANCE STANDARDS.
 8. GROUNDING AT ANTENNA MASTS FOR GPS AND ANTENNAS
 9. ALL OTHER TESTS REQUIRED BY COMPANY OR JURISDICTION.

3.3 REQUIRED INSPECTIONS

- A. SCHEDULE INSPECTIONS WITH COMPANY REPRESENTATIVE.
- B. CONDUCT INSPECTIONS INCLUDING BUT NOT LIMITED TO THE FOLLOWING:
 1. GROUNDING SYSTEM INSTALLATION PRIOR TO EARTH CONCEALMENT DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
 2. FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A&E OR SPRINT REPRESENTATIVE.
 3. COMPACTION OF BACKFILL MATERIALS; AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS; ASPHALT PAVING; AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
 4. PRE- AND POST-CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES.
 5. TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
 6. ANTENNA AZIMUTH , DOWN TILT AND PER SUNLIGHT TOOL SUNSIGHT INSTRUMENTS - ANTENNALIGN ALIGNMENT TOOL (AAT)

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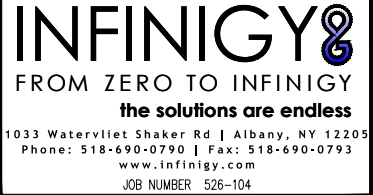


PROJECT MANAGER:

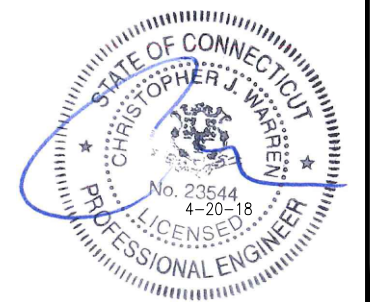


SBA COMMUNICATIONS CORP.
134 FLANDERS ROAD, SUITE 125
WESTBOROUGH, MA 01581
TEL: (508) 251-0720

PLANS PREPARED BY:



ENGINEERING LICENSE:



CHECKED BY:

APPROVED BY:

REVISIONS:

DESCRIPTION	DATE	BY	REV.
ISSUED FOR CONSTRUCTION	03/22/18	SL	0
ISSUED FOR REVIEW	01/18/18	RCD	A

SITE NUMBER:

CT33XC574

SITE ADDRESS:

131 GIFFORD LANE,
BOZRAH, CT 06334

SHEET DESCRIPTION:

OUTLINE SPECIFICATIONS

SHEET NUMBER:

SP-2

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APPROVED BY:

REVISIONS:

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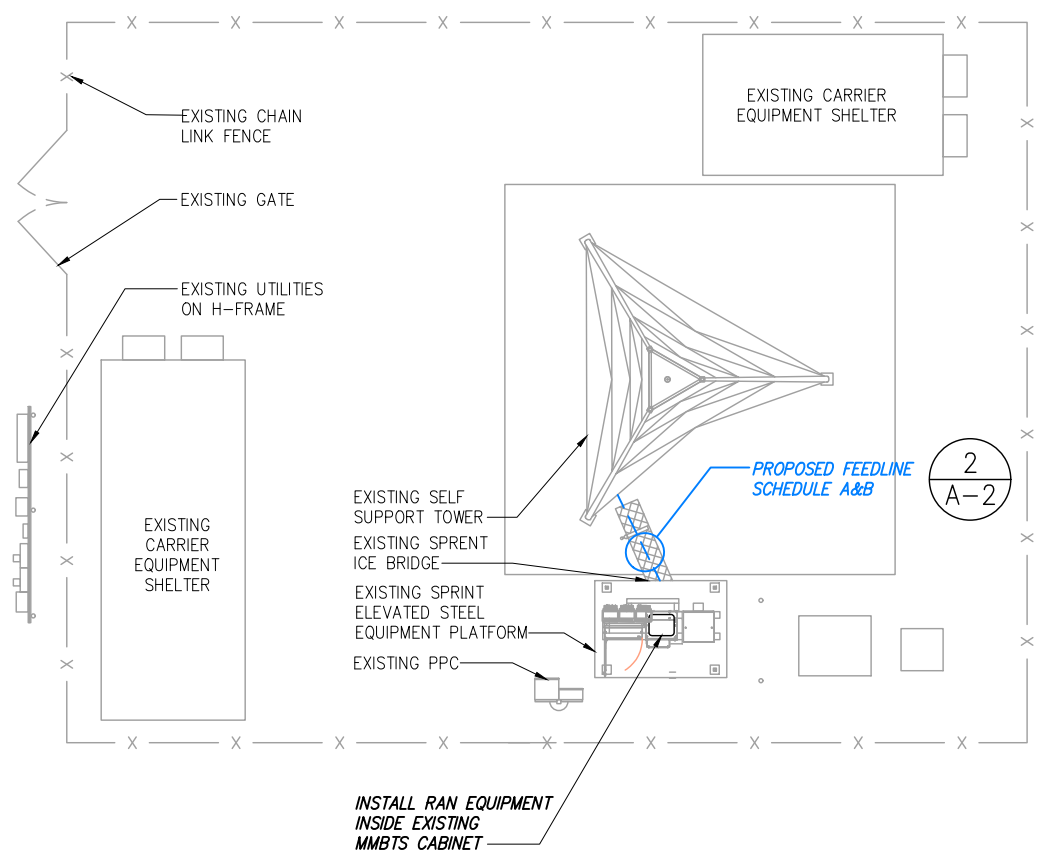
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BOZRAH, CT 06334

SHEET DESCRIPTION:

SITE PLAN

SHEET NUMBER:

A-1



EXISTING SPRINT ICE CANOPY

EXISTING SPRINT MMBTS CABINET

EXISTING SPRINT BBU CABINET

EXISTING METERBOARD

EXISTING SPRINT FIBER JUNCTION BOX

PROPOSED FEEDLINE SCHEDULE A&B

2
A-2

EXISTING SPRINT 1900 MHz RRH'S TO BE RELOCATED TO TOWER TOP

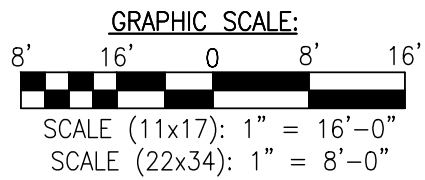
ALL 1,2
A-2 A-3

EXISTING SPRINT EQUIPMENT CONCRETE PAD



SOURCE: WESTCHESTER SERVICES 11/14/17

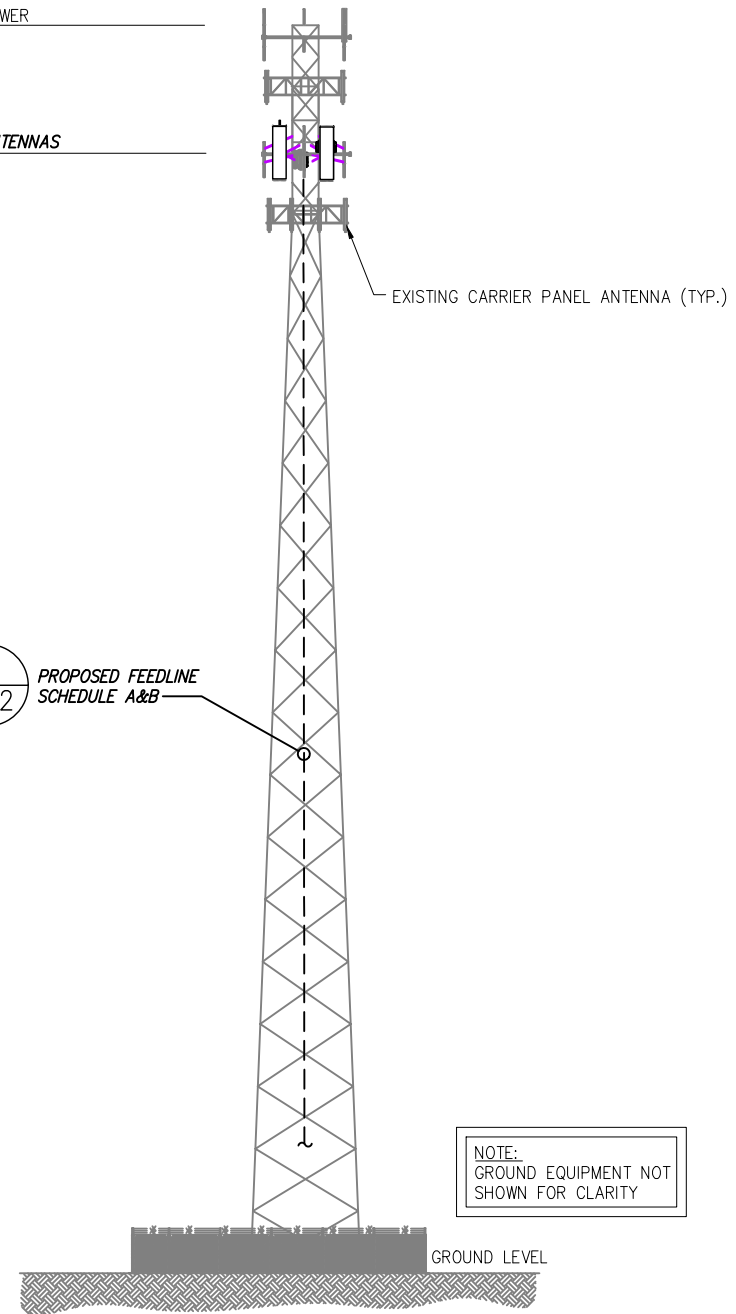
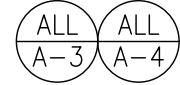
INFORMATION CONTAINED WITHIN DRAWINGS ARE BASED ON PROVIDED INFORMATION AND ARE NOT THE RESULT OF A FIELD SURVEY.



THESE PLANS HAVE BEEN DEVELOPED FOR THE MODIFICATION OF AN EXISTING UNMANNED TELECOMMUNICATIONS FACILITY OWNED OR LEASED BY SPRINT IN ACCORDANCE WITH THE SCOPE OF WORK PROVIDED BY SPRINT. INFINIGY HAS INCORPORATED THIS SCOPE OF WORK IN THE PLANS. THESE PLANS ARE NOT FOR CONSTRUCTION UNLESS ACCOMPANIED BY A PASSING STRUCTURAL STABILITY ANALYSIS PREPARED BY A LICENSED STRUCTURAL ENGINEER. STRUCTURAL ANALYSIS MUST INCLUDE BOTH TOWER AND MOUNT.

TOP OF SELF SUPPORT TOWER
ELEV. = ±195' A.G.L.

Q OF PROPOSED SPRINT ANTENNAS
ELEV. = 175' A.G.L.



NOTE:
GROUND EQUIPMENT NOT SHOWN FOR CLARITY

SPECIAL INSTALLATION NOTE:
JUMPERS FROM RRHs TO ANTENNA SHALL NOT EXCEED 15'. NOTIFY SPRINT CONSTRUCTION MANAGER OF ANY DISCREPANCY

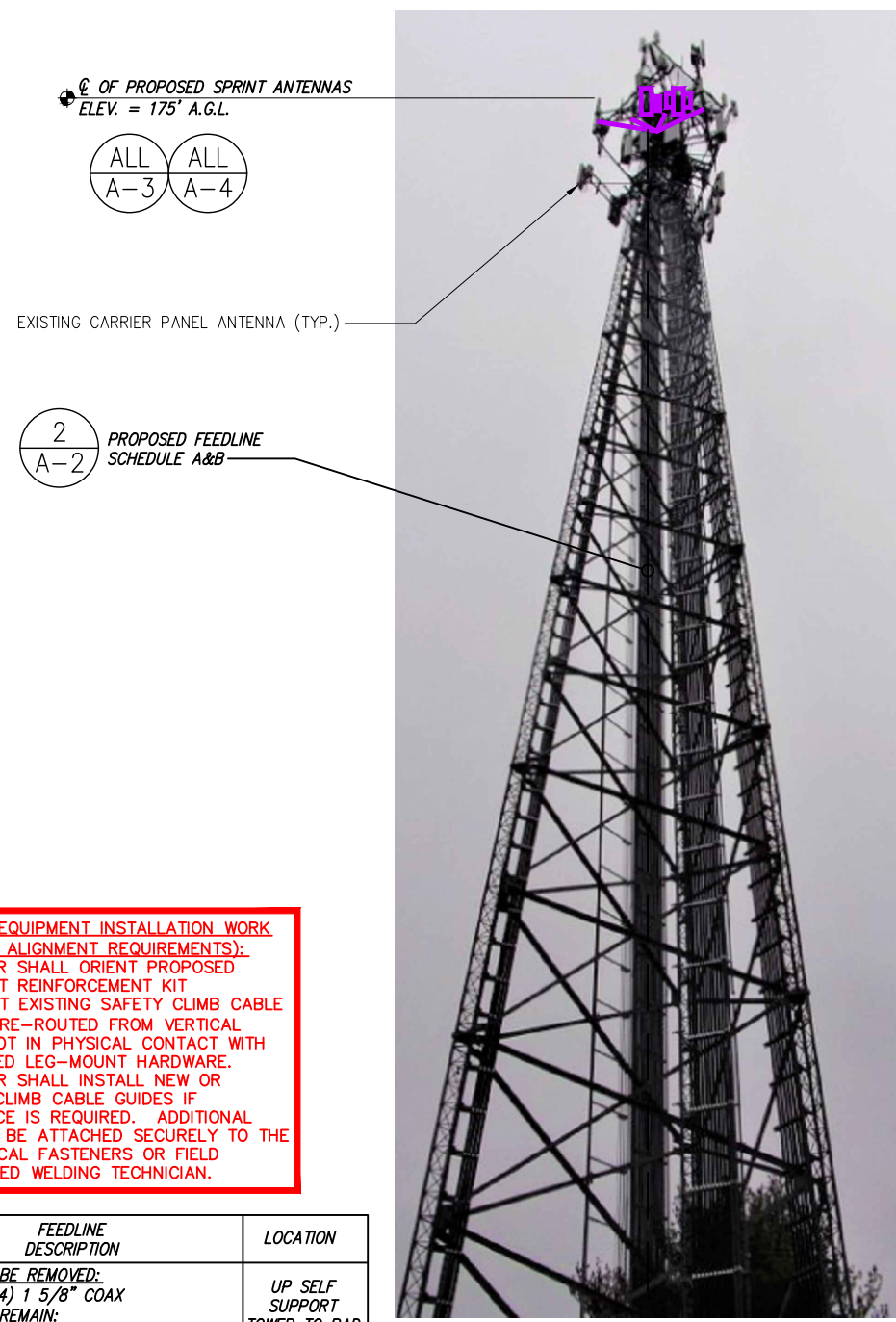
NOTE:
VERIFY PROPOSED AZIMUTHS WITH RF ENGINEER PRIOR TO INSTALLATION

TOWER ELEVATION

NO SCALE

1

Q OF PROPOSED SPRINT ANTENNAS
ELEV. = 175' A.G.L.



EXISTING CARRIER PANEL ANTENNA (TYP.)

SPECIAL TOWER TOP EQUIPMENT INSTALLATION WORK NOTE (SAFETY-CLIMB ALIGNMENT REQUIREMENTS):
GENERAL CONTRACTOR SHALL ORIENT PROPOSED STRUCTURAL AUGMENT REINFORCEMENT KIT LEG-MOUNTS SO THAT EXISTING SAFETY CLIMB CABLE IS NOT OBSTRUCTED/RE-ROUTED FROM VERTICAL ALIGNMENT AND IS NOT IN PHYSICAL CONTACT WITH EXISTING OR PROPOSED LEG-MOUNT HARDWARE. GENERAL CONTRACTOR SHALL INSTALL NEW OR ADDITIONAL SAFETY-CLIMB CABLE GUIDES IF ADDITIONAL CLEARANCE IS REQUIRED. ADDITIONAL CABLE GUIDES SHALL BE ATTACHED SECURELY TO THE POLE USING MECHANICAL FASTENERS OR FIELD WELDED BY A CERTIFIED WELDING TECHNICIAN.

FEEDLINE SCHEDULE	FEEDLINE DESCRIPTION	LOCATION
A	EXISTING TO BE REMOVED: (4) 1 5/8" COAX	UP SELF SUPPORT TOWER TO RAD
	EXISTING TO REMAIN: (2) 1 5/8" COAX	
B	PROPOSED: (4) HYBRID TO 175' RAD	UP SELF SUPPORT TOWER TO RAD

NOTE:
EXISTING SPRINT EQUIPMENT FEEDLINE INVENTORY BASED ON COLOCATION APPLICATION AND SBA RECORD, NOT FIELD OBSERVATIONS. RFDS AND FEEDLINE LEASING ENTITLEMENTS MAY DIFFER.

TOWER ELEVATION PHOTO DETAIL

NO SCALE

2

PLANS PREPARED FOR:

INTERNATIONAL BLVD, SUITE 800
MAHWAH, NJ 07495
TEL: (800) 357-7641

PROJECT MANAGER:

SBA COMMUNICATIONS CORP.
134 FLANDERS ROAD, SUITE 125
WESTBOROUGH, MA 01581
TEL: (508) 251-0720

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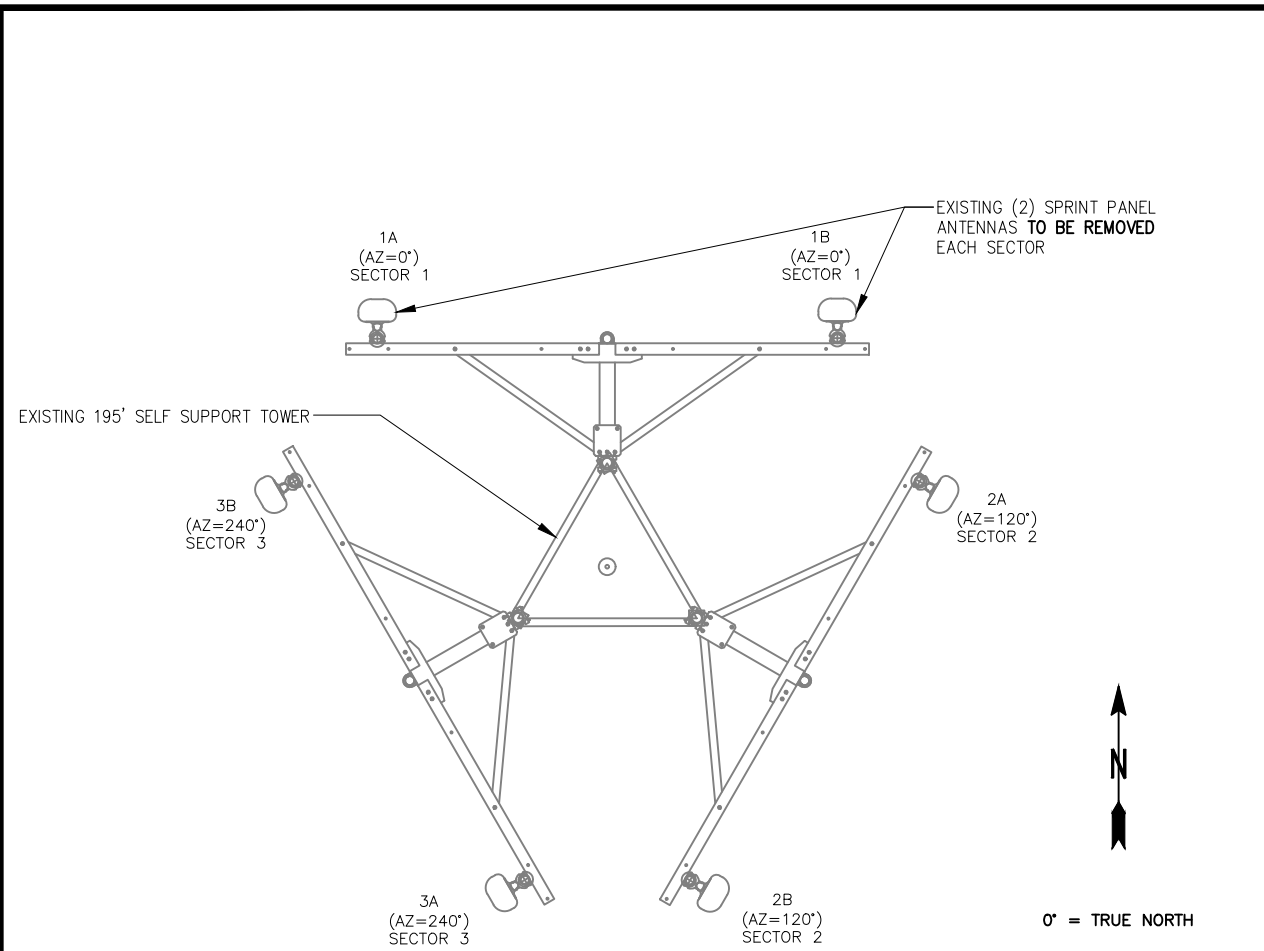
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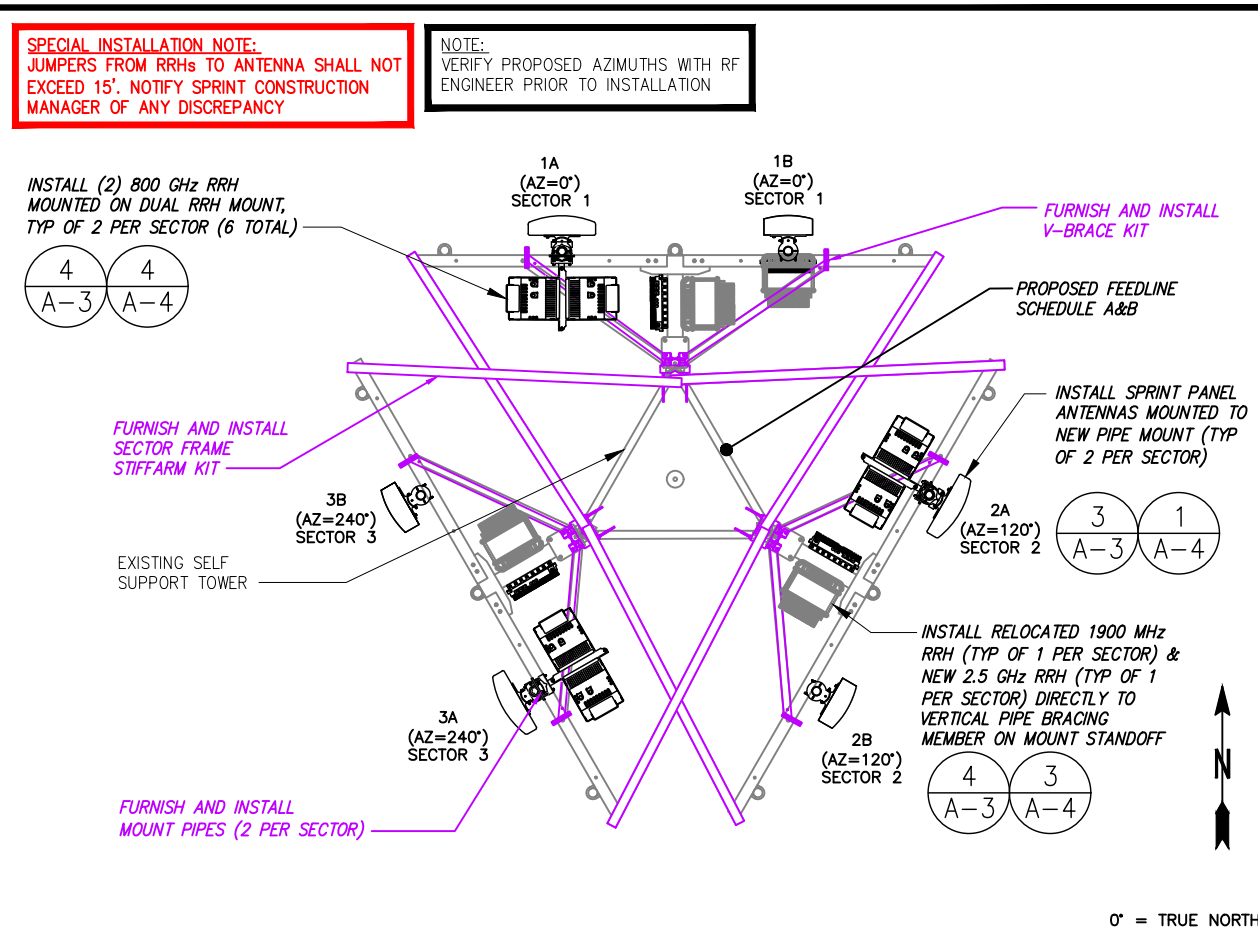
SHEET DESCRIPTION:
TOWER ELEVATION

SHEET NUMBER:
A-2



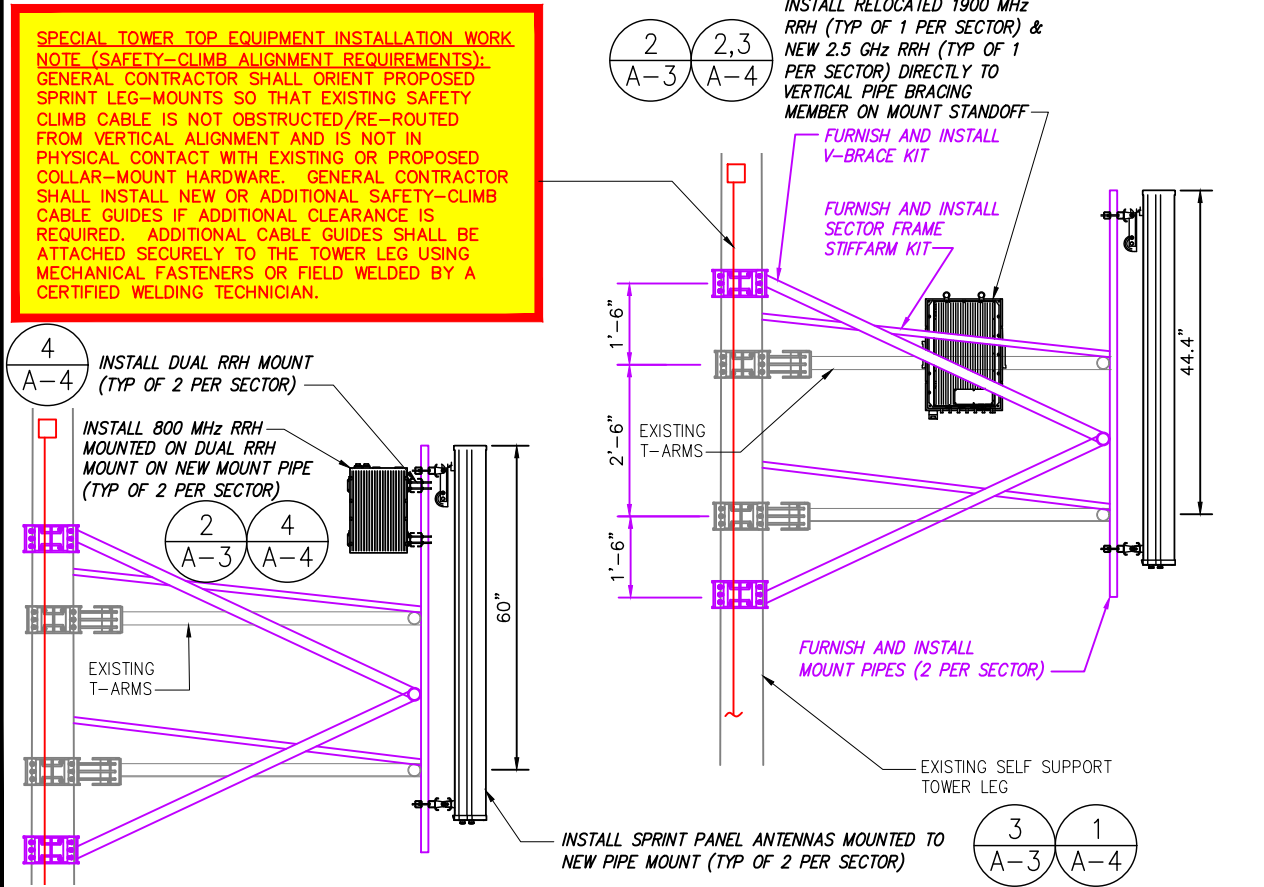
EXISTING ANTENNA & RRH LAYOUT

NO SCALE 1



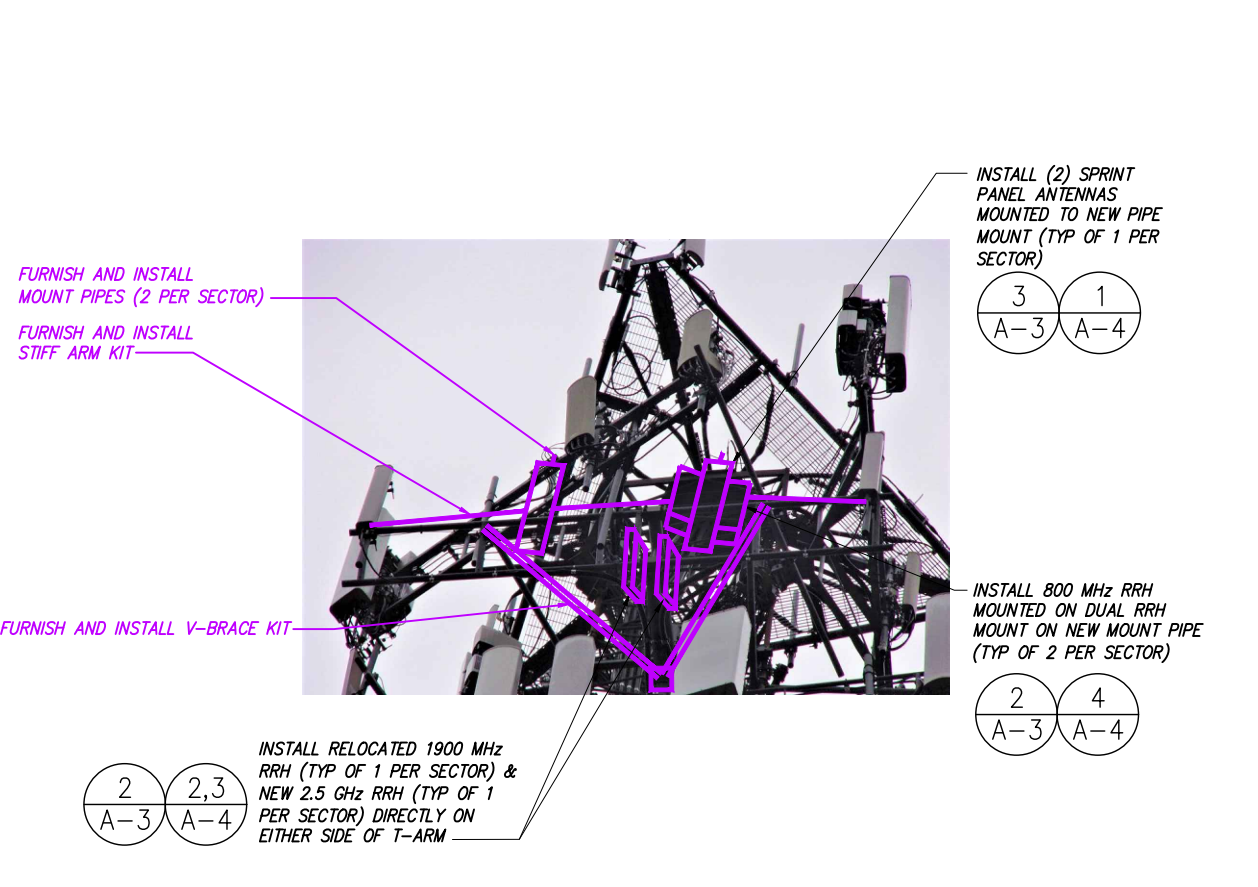
FINAL ANTENNA & RRH LAYOUT

NO SCALE 2



TYPICAL MOUNTING DETAIL

NO SCALE 3



ANTENNA & RRH MOUNTING PHOTO DETAIL

NO SCALE 4

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PROJECT MANAGER:

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134 FLANDERS ROAD, SUITE 125
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www.infinigy.com
JOB NUMBER 526-104

ENGINEERING LICENSE:

STATE OF CONNECTICUT
CHRISTOPHER J. WARREN
No. 23544
4-20-18
PROFESSIONAL ENGINEER

CHECKED BY:

APPROVED BY:

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ISSUED FOR REVIEW		01/18/18	RCD	A

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BOZRAH, CT 06334

SHEET DESCRIPTION:
**ANTENNA LAYOUT
& MOUNTING DETAILS**

SHEET NUMBER:
A-3

CHECKED BY:

APPROVED BY:

REVISIONS:

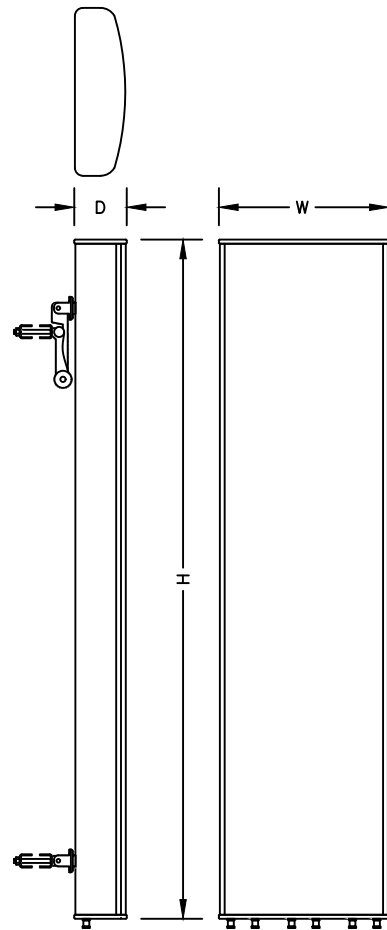
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ISSUED FOR REVIEW	01/18/18	RCD	A

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SHEET DESCRIPTION:
EQUIPMENT & MOUNTING DETAILS

SHEET NUMBER:
A-4



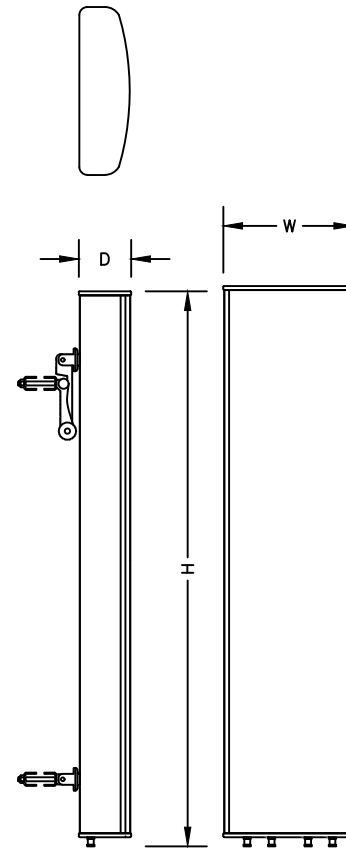
ANTENNA SPECIFICATIONS

MANUF.	COMMSCOPE
MODEL #	NNVV-65B-R4
HEIGHT	72"
WIDTH	19.6"
DEPTH	7.8"
WEIGHT	84.7± LBS.

ANTENNA DETAIL

NO SCALE

1



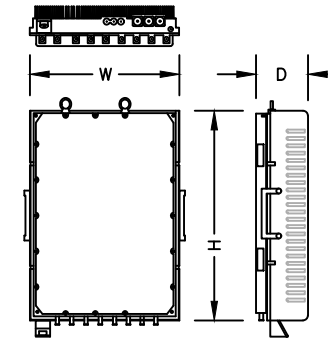
ANTENNA SPECIFICATIONS

MANUF.	RFS
MODEL #	APXVTM14-ALU-I20
HEIGHT	56.3"
WIDTH	12.6"
DEPTH	6.3"
WEIGHT	56.2± LBS.

ANTENNA DETAIL

NO SCALE

2



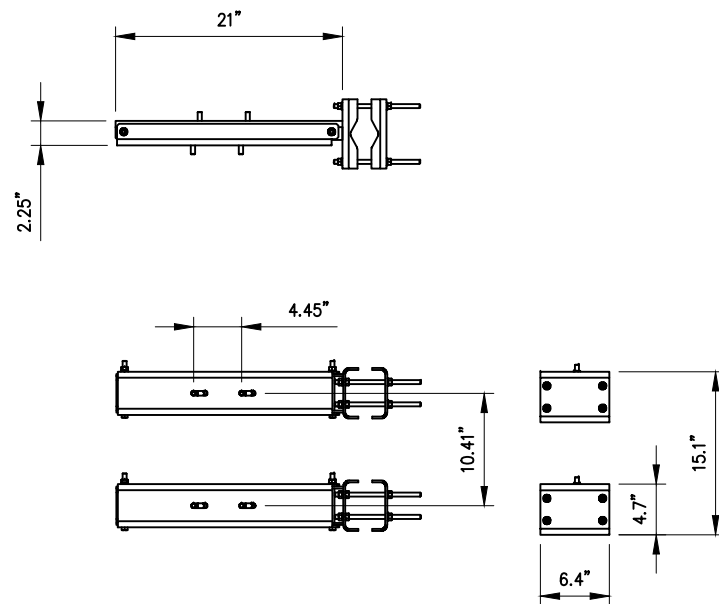
2.5 GHZ RRH SPECIFICATIONS

MANUF.	NOKIA (ALU)
MODEL #	TD-RRH8X20-25
HEIGHT	26.1"
WIDTH	18.6"
DEPTH	6.7"
WEIGHT	70± LBS

2.5 RRH

NO SCALE

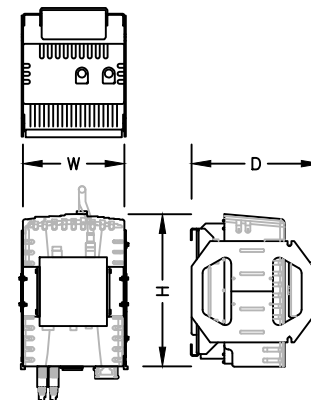
3



DUAL RRH MOUNT DETAIL

NO SCALE

4



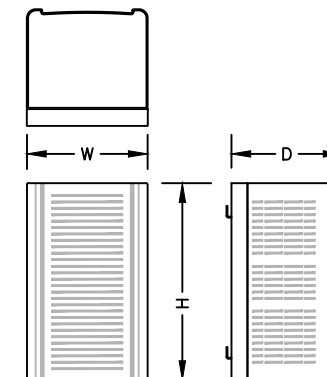
800 MHZ RRH SPECIFICATIONS

MANUF.	NOKIA (ALU)
MODEL #	800MHZ 2X50W
HEIGHT	19.7"
WIDTH	13"
DEPTH	10.8"
WEIGHT	53± LBS

800 MHz RRH

NO SCALE

5



1900 MHZ RRH SPECIFICATIONS

MANUF.	NOKIA (ALU)
MODEL #	1900 4X45 65MHZ
HEIGHT	25"
WIDTH	11.1"
DEPTH	11.4"
WEIGHT	60± LBS

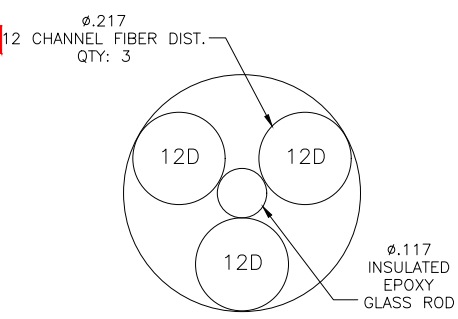
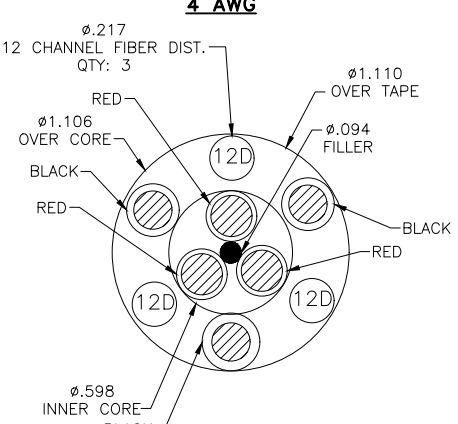
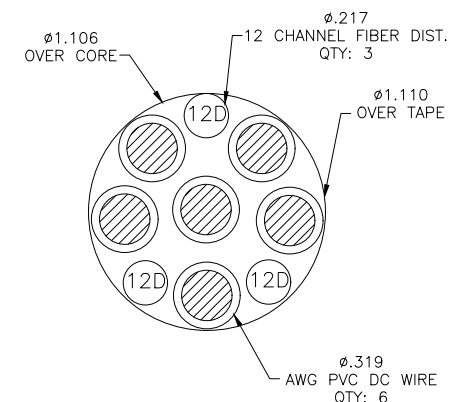
1900 MHz RRH (EXISTING TO BE RELOCATED)

NO SCALE

6

RFS HYBRIFLEX RISER CABLE SCHEDULE

Fiber Only (Existing DC Power)	Hybrid cable MN: HB058-M12-050F 12x multi-mode fiber pairs, Top: Outdoor protected connectors, Bottom: LC Connectors, 5/8 cable, 50 ft	50 ft
	MN: HB058-M12-075F	75 ft
	MN: HB058-M12-100F	100 ft
	MN: HB058-M12-125F	125 ft
	MN: HB058-M12-150F	150 ft
	MN: HB058-M12-175F MN: HB058-M12-200F	175 ft 200 ft
8 AWG Power	Hybrid cable MN: HB114-08U3M12-050F 3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 50 ft	50 ft
	MN: HB114-08U3M12-075F	75 ft
	MN: HB114-08U3M12-100F	100 ft
	MN: HB114-08U3M12-125F	125 ft
	MN: HB114-08U3M12-150F	150 ft
	MN: HB114-08U3M12-175F MN: HB114-08U3M12-200F	175 ft 200 ft
6 AWG Power	Hybrid cable MN: HB114-13U3M12-225F 3x 6 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 225 ft	225 ft
	MN: HB114-13U3M12-250F	250 ft
	MN: HB114-13U3M12-275F	275 ft
	MN: HB114-13U3M12-300F	300 ft
4 AWG Power	Hybrid cable MN: HB114-21U3M12-325F 3x 4 AWG power pair, 12x multi-mode fiber pairs, Outdoor rated connectors & LC Connectors, 1 1/4 cable, 325 ft	325 ft
	MN: HB114-21U3M12-350F	350 ft
	MN: HB114-21U3M12-375F	375 ft



RFS HYBRIFLEX JUMPER CABLE SCHEDULE

Fiber Only	Hybrid Jumper cable MN: HBF012-M3-5F1 5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable	5 ft
	MN: HBF012-M3-10F1	10 ft
	MN: HBF012-M3-15F1	15 ft
	MN: HBF012-M3-20F1	20 ft
	MN: HBF012-M3-25F1	25 ft
	MN: HBF012-M3-30F1	30 ft
8 AWG Power	Hybrid Jumper cable MN: HBF058-08U1M3-5F1 5 ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
	MN: HBF058-08U1M3-10F1	10 ft
	MN: HBF058-08U1M3-15F1	15 ft
	MN: HBF058-08U1M3-20F1	20 ft
	MN: HBF058-08U1M3-25F1	25 ft
	MN: HBF058-08U1M3-30F1	30 ft
6 AWG Power	Hybrid Jumper cable MN: HBF058-13U1M3-5F1 5 ft, 1x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 5/8 cable	5 ft
	MN: HBF058-13U1M3-10F1	10 ft
	MN: HBF058-13U1M3-15F1	15 ft
	MN: HBF058-13U1M3-20F1	20 ft
	MN: HBF058-13U1M3-25F1	25 ft
	MN: HBF058-13U1M3-30F1	30 ft
4 AWG Power	Hybrid Jumper cable MN: HBF078-21U1M3-5F1 5 ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC Connectors, 7/8 cable	5 ft
	MN: HBF078-21U1M3-10F1	10 ft
	MN: HBF078-21U1M3-15F1	15 ft
	MN: HBF078-21U1M3-20F1	20 ft
	MN: HBF078-21U1M3-25F1	25 ft
	MN: HBF078-21U1M3-30F1	30 ft

NOTE:
SPRINT CM TO CONFIRM HYBRID OR FIBER RISER CABLE AND HYBRID OR FIBER JUMPER CABLE MODEL NUMBERS IF HYBRID CABLES ARE REQUIRED BEFORE PREPARING BOM.

* PROPOSED CABLE LENGTH WAS DETERMINED USING THE SUM OF THE RAD CENTER OF ANTENNAS, AND DISTANCE FROM EXISTING EQUIPMENT AREA TO TOWER BASE WITH AN ADDITIONAL 20' BUFFER. LENGTH TO BE VERIFIED IN FIELD PRIOR TO ORDERING MATERIALS.
* SPRINT CM TO CONFIRM HYBRID RISER CABLE AND HYBRID JUMPER CABLE MODEL NUMBERS BEFORE PREPARING BOM.

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ENGINEERING LICENSE:

CHRISTOPHER J. WARREN
No. 23544
4-20-18
PROFESSIONAL ENGINEER

CHECKED BY:

APPROVED BY:

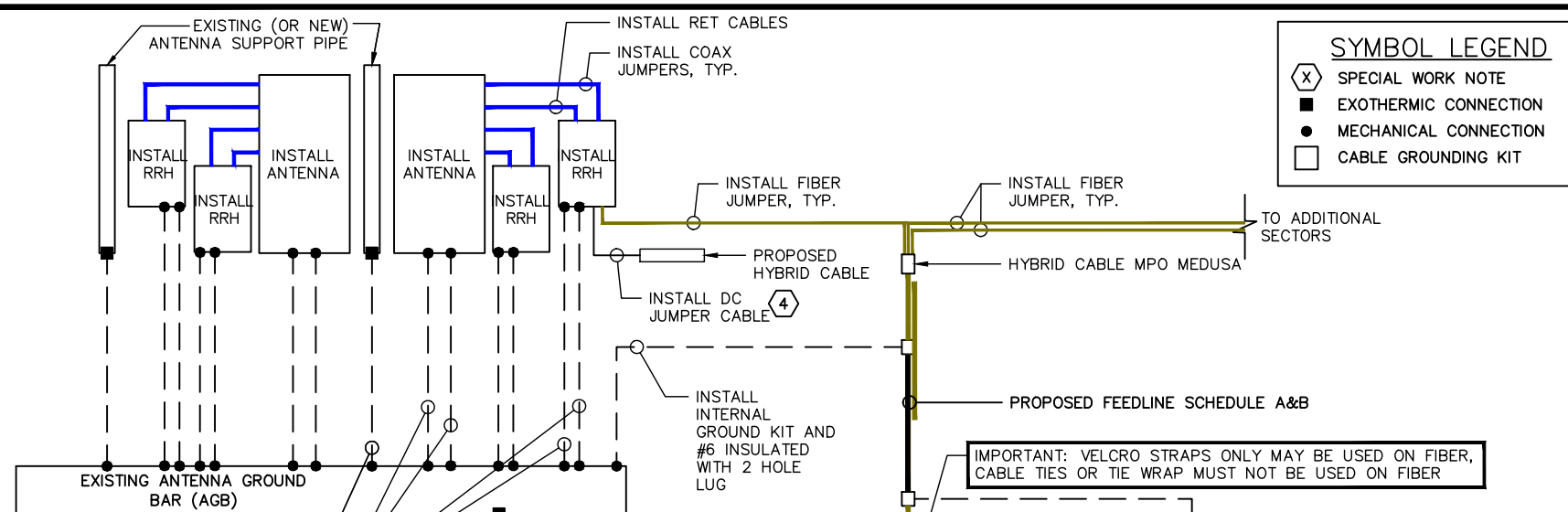
REVISIONS:	DESCRIPTION	DATE	BY	REV.
ISSUED FOR CONSTRUCTION		03/22/18	SL	0
ISSUED FOR REVIEW		01/18/18	RCD	A

SITE NUMBER:
CT33XC574

SITE ADDRESS:
131 GIFFORD LANE,
BOZRAH, CT 06334

SHEET DESCRIPTION:
DETAILS

SHEET NUMBER:
A-5



SYMBOL LEGEND

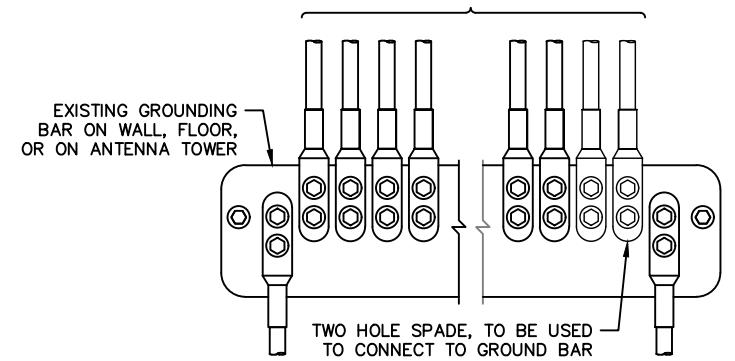
- (X) SPECIAL WORK NOTE
- EXOTHERMIC CONNECTION
- MECHANICAL CONNECTION
- CABLE GROUNDING KIT

- ELECTRICAL NOTES**
- 1) ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) AS WELL AS APPLICABLE STATE AND LOCAL CODES.
 - 2) THE ELECTRICAL CONTRACTOR SHALL COORDINATE ALL CONDUIT ROUTING WITH LOCAL UTILITY COMPANIES AND SPRINT CONSTRUCTION MANAGER.
 - 3) ALL CONDUITS ROUTED BELOW GRADE SHALL TRANSITION TO RIGID GALVANIZED ELBOWS WITH RIGID GALVANIZED STEEL CONDUIT ABOVE GRADE.
 - 4) ALL METAL CONDUITS SHALL BE PROVIDED WITH GROUNDING BUSHINGS.
 - 5) GENERAL CONTRACTOR SHALL PROVIDE ALL DIRECT BURIED CONDUITS WITH PLASTIC WARNING TAPE IDENTIFYING CONTENTS. TAPE COLORS SHALL BE ORANGE FOR TELEPHONE AND RED FOR ELECTRIC.
 - 6) ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED AND PROCURED PER SPECIFICATION REQUIREMENTS.
 - 7) THE ELECTRICAL WORK INCLUDES ALL LABOR AND MATERIALS DESCRIBED BY DRAWINGS AND SPECIFICATIONS INCLUDING INCIDENTAL WORK TO PROVIDE COMPLETE OPERATING AND APPROVED ELECTRICAL SYSTEM.
 - 8) GENERAL CONTRACTOR SHALL PAY FEES FOR PERMITS, AND IS RESPONSIBLE FOR OBTAINING SAID PERMITS AND COORDINATION OF INSPECTIONS.
 - 9) ELECTRICAL AND TELCO WIRING OUTSIDE A BUILDING AND EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUITS OR SCHEDULE 80 PVC (AS PERMITTED BY CODE) AND WHERE REQUIRED IN LIQUID TIGHT FLEXIBLE METAL OR NONMETALLIC CONDUITS.
 - 10) BURIED CONDUIT SHALL BE SCHEDULE 40 PVC.
 - 11) ELECTRICAL WIRING SHALL BE COPPER WITH TYPE XHHW, THWN, OR THIN INSULATION.
 - 12) RUN ELECTRICAL CONDUIT OR CABLE BETWEEN ELECTRICAL UTILITY DEMARCATION POINT AND PROJECT OWNER CELL SITE PPC AS INDICATED ON THIS DRAWING. PROVIDE FULL LENGTH PULL ROPE. COORDINATE INSTALLATION WITH UTILITY COMPANY.
 - 13) RUN TELCO CONDUIT OR CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT AND PROJECT OWNER CELL SITE TELCO CABINET AND BTS CABINET AS INDICATED ON THIS DRAWING. PROVIDE FULL LENGTH PULL ROPE IN INSTALLED TELCO CONDUIT. PROVIDE GREENLEE CONDUIT MEASURING TAPE AT EACH END.
 - 14) FIBER OPTIC CIRCUITS SHALL BE IN ACCORDANCE WITH NEC ARTICLE 770—OPTICAL FIBER CABLES AND RACEWAYS.
 - 15) COMMUNICATIONS CIRCUITS SHALL BE IN ACCORDANCE WITH NEC ARTICLE 800—COMMUNICATIONS SYSTEMS.

- SPECIAL WORK NOTE:**
1. G.C. TO FURNISH AND INSTALL ALL COMPONENTS TO UPGRADE EXISTING ELECTRICAL SERVICE, CONDUIT, CONDUCTOR, PPC AND MCB IN ACCORDANCE WITH SPRINT CONSTRUCTION STANDARDS NV 2.5 ADDENDUM "ENGINEERING NOTICE 2013-002 (POWER UPGRADES) REV." (OR CURRENT VERSION)
 2. G.C. TO FURNISH AND INSTALL UPGRADE THE EXISTING MMBTS BREAKER, CONDUCTOR, AND CONDUIT TO A MINIMUM NEC RATING.
 3. FOR NEW OR REPAIRED GROUNDING EQUIPMENT, REFER TO SPRINT GROUNDING STANDARDS AND FOLLOWING (SUPPLEMENTS):
-ANTI-THEFT UPDATE TO SPRINT GROUNDING DATED 08-24-12 (OR CURRENT VERSION)
-SPRINT ENGINEERING LETTER EL-0504 DATED 04-20-12 (OR CURRENT VERSION)
 4. USE SPARE DC CABLES COILED UP AT TOWER TOP NV ARRAY TO POWER UP 2.5 RRH. INSIDE EXISTING FIBER DISTRIBUTION BOX, TIE SPARE DC CONDUCTORS INTO EXISTING DC BREAKER PANEL PER APPROVED DC WIRING CONNECTIVITY OPTION (BASED ON NV HYBRIFLEX CABLE LENGTH). CONSULT WITH SPRINT CM TO DETERMINE APPROPRIATE DC CONNECTIVITY OPTION, PLUMBING DIAGRAM AND DC BREAKER SIZE.

- PROTECTIVE GROUNDING SYSTEMS GENERAL NOTES:**
1. GROUNDING SHALL BE IN ACCORDANCE WITH NEC ARTICLE 250—GROUNDING AND BONDING.
 2. GROUNDING SHALL BE IN ACCORDANCE WITH SPRINT SSEO DOCUMENTS 3.018.02.004 "BONDING, GROUNDING AND TRANSIENT PROTECTION FOR CELL SITES" AND 3.018.10.002 "SITE RESISTANCE TO EARTH TESTING".
 3. PROVIDE GROUND CONNECTIONS FOR ALL METALLIC STRUCTURES, ENCLOSURES, RACEWAYS AND OTHER CONDUCTIVE ITEMS ASSOCIATED WITH THE INSTALLATION OF CARRIER'S EQUIPMENT.
 4. GROUND CONNECTIONS: CLEAN SURFACES THOROUGHLY BEFORE APPLYING GROUND LUGS OR CLAMPS. IF SURFACE IS COATED, REMOVE THE COATING, APPLY A NON-CORROSIVE APPROVED COMPOUND TO CLEAN SURFACE AND INSTALL LUGS OR CLAMPS. WHERE GALVANIZING IS REMOVED FROM METAL, IT SHALL BE PAINTED OR TOUCHED UP WITH "GALVAMOX" OR EQUAL.
 5. ALL GROUNDING WIRES SHALL PROVIDE A STRAIGHT, DOWNWARD PATH TO GROUND WITH GRADUAL BENDS AS REQUIRED. GROUND WIRES SHALL NOT BE LOOPED OR SHARPLY BENT.
 6. ALL CLAMPS AND SUPPORTS USED TO SUPPORT THE GROUNDING SYSTEM CONDUCTORS AND PVC CONDUITS SHALL BE PVC TYPE (NON CONDUCTIVE). DO NOT USE METAL BRACKETS OR SUPPORTS WHICH WOULD FORM A COMPLETE RING AROUND ANY GROUNDING CONDUCTOR.
 7. ALL GROUND WIRES SHALL BE #2 SOLID TINNED BCW UNLESS NOTED OTHERWISE.
 8. PROVIDE DEDICATED #2 AWG COPPER GROUND WIRE FROM EACH ANTENNA MOUNTING PIPE TO ASSOCIATED CIGBE.
 9. GROUND ANTENNA BASES, FRAMES, CABLE RACKS, AND OTHER METALLIC COMPONENTS WITH #2 INSULATED TINNED STRANDED COPPER GROUNDING CONDUCTORS AND CONNECT TO INSULATED SURFACE MOUNTED GROUND BARS. CONNECTION DETAILS SHALL FOLLOW MANUFACTURER'S SPECIFICATIONS FOR GROUNDING.
 10. EACH EQUIPMENT CABINET SHALL BE CONNECTED TO THE MASTER ISOLATION GROUND BAR (MGB) WITH #2 SOLID TINNED BCW EQUIPMENT CABINETS WALL HAVE (2) CONNECTIONS.
 11. GROUND HYBRIFLEX SHIELD AT TOP, BOTTOM AND AT TRANSITION TO HYBRIFLEX JUMPER CABLES AT EQUIPMENT CABINET ENTRANCE USING MANUFACTURER'S GUIDELINES. WHEN HYBRIFLEX CABLE EXCEEDS 200', GROUND AT INTERVALS NOT EXCEEDING 100'.
 12. THE CONTRACTOR SHALL VERIFY THAT THE EXISTING GROUND BARS HAVE ENOUGH SPACE/HOLES FOR ADDITIONAL TWO HOLE LUGS.
 13. EXOTHERMIC WELDING IS RECOMMENDED FOR GROUNDING CONNECTION WHERE PRACTICAL OTHERWISE. THE CONNECTION SHALL BE MADE USING COMPRESSION TYPE-2 HOLES, LONG BARREL LUGS OR DOUBLE CRIMP "C" CLAMP. THE COPPER CABLES SHALL BE COATED WITH AN ANTI-OXIDANT (THOMAS BETTS KOPR-SHIELD) BEFORE MAKING THE CRIMP CONNECTIONS THE CONTRACTOR SHALL FOLLOW MANUFACTURER'S RECOMMENDED TORQUES ON THE BOLT ASSEMBLY TO SECURE CONNECTIONS.
 14. AT ALL TERMINATIONS AT EQUIPMENT ENCLOSURES, PANEL, AND FRAMES OF EQUIPMENT AND WHERE EXPOSED FOR GROUNDING, CONDUCTOR TERMINATION SHALL BE PERFORMED UTILIZING TWO HOLE BOLTED TONGUE COMPRESSION TYPE LUGS WITH STAINLESS STEEL SELF-TAPPING SCREWS.
 15. THE MASTER GROUND BAR (MGB) SHALL BE MADE OF BARE 1/4"x2" COPPER (FOR OUTDOOR APPLICATIONS IT SHALL BE TINNED COPPER) AND LARGE ENOUGH TO ACCOMMODATE THE REQUIRED NUMBER OF GROUND CONNECTIONS. THE HARDWARE SECURING THE MGB SHALL ELECTRICAL INSULATE THE MGB FROM ANY STRUCTURE TO WHICH IT IS FASTENED.
 16. ALL BOLTS, WASHERS, AND NUTS USED ON GROUNDING CONNECTIONS SHALL BE STAINLESS STEEL.
 17. ALL GROUNDING CONNECTIONS SHALL BE COATED WITH A COPPER SHIELD ANTI-CORROSIVE AGENT SUCH AS T&B KOPR SHIELD. VERIFY PRODUCT WITH SPRINT CONSTRUCTION MANAGER.
 18. FOR NEW OR REPAIRED GROUNDING EQUIPMENT. REFER TO SPRINT GROUNDING STANDARDS AND FOLLOWING (SUPPLEMENTS):
-ANTI-THEFT UPDATE TO SPRINT GROUNDING DATED 08-24-12 (OR CURRENT VERSION)
-SPRINT ENGINEERING LETTER EL-0504 DATED 04-20-12 (OR CURRENT VERSION)

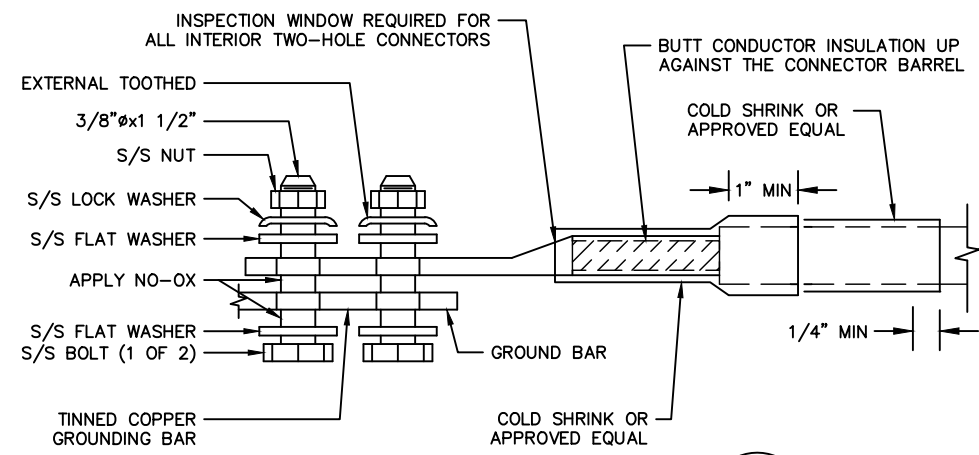
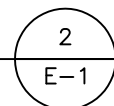
2# AWG STRANDED INSULATED,
#4 OR #6 AWG SOLID CU
CONDUCTOR WITH GREEN, 600V,
THWN-2 INSULATION



1. APPLY NO-OX TO LUG AND BAR CONTACT SURFACE. DO NOT COAT INLINE LUG.
2. IF STOLEN GROUND BARS ARE ENCOUNTERED, CONTACT SPRINT CM FOR REPLACEMENT THREADED ROD KIT.

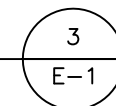
INSTALLATION OF GROUNDING CONDUCTOR TO GROUNDING BAR

SCALE: N.T.S.



TWO HOLE LUG

SCALE: N.T.S.



ELECTRICAL & GROUNDING DETAILS

PLANS PREPARED FOR:

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ENGINEERING LICENSE:

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APPROVED BY:

REVISIONS:

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ISSUED FOR CONSTRUCTION	03/22/18	SL	0
ISSUED FOR REVIEW	01/18/18	RCD	A

SITE NUMBER:

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SITE ADDRESS:

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BOZRAH, CT 06334

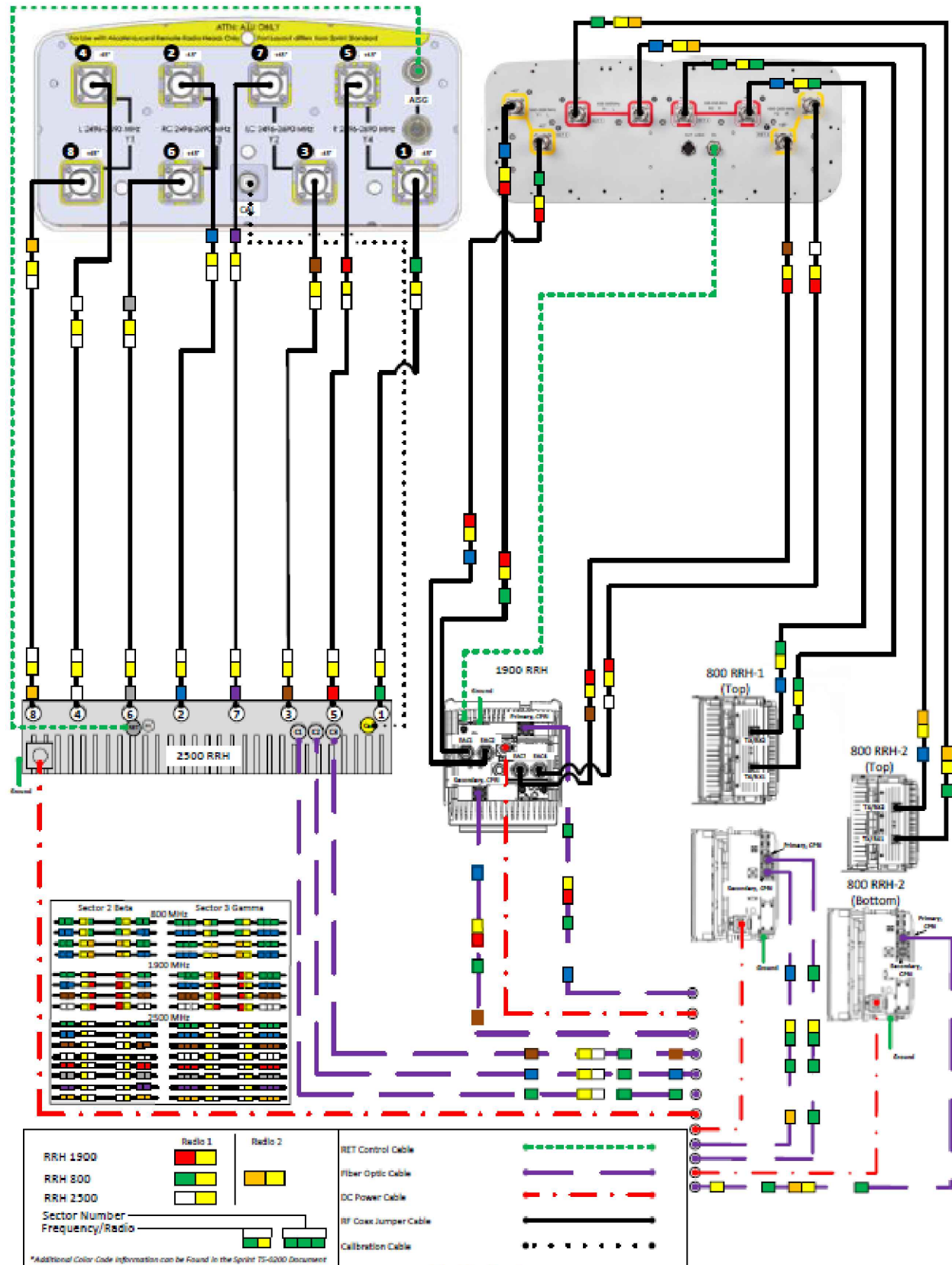
SHEET DESCRIPTION:

ELECTRICAL & GROUNDING DETAILS

SHEET NUMBER:

E-1

ALU 211 APXVTM14-ALU-I20 & NNVV-65B-R4 wo Filters



Prepared By: Mark Elliott | Creation Date: February 13, 2016 | Revision Number: R-1 | Approved By: RAN Hardware & Antenna Teams | Approval Date: February 23, 2017 | Title: Nokia-A Tri-Band Fiber Connections (Nokia-A Two-800, One-1900, & One-2500 RRH) | Sprint

Nokia-A Site Upgrade: Adding 2500 and Second 800 RRH

Existing Cables:
NV Cable 1 - Provides power and fiber for the first 800 and 1900 RRHs of Sector 1
NV Cable 2 - Provides power and fiber for the first 800 and 1900 RRHs of Sector 2
NV Cable 3 - Provides power and fiber for the first 800 and 1900 RRHs of Sector 3

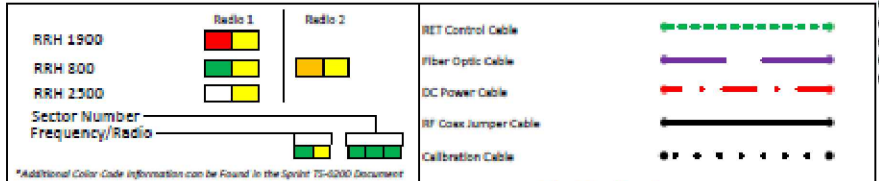
New Cables:
Auxiliary Cable 1 - Provides power and fiber for all 2500 RRHs (All Three Sectors)
Auxiliary Cable 2 - Provides power and fiber for all of the Second 800 RRHs (All Three Sectors)

Legend:
Sector - Frequency/Radio - Fiber Cable Number - Fiber Pair Cable Number

Sector	Frequency/Radio	Fiber Cable Number	Fiber Pair Cable Number
1	800 #1	1	1
1	800 #2	2	2
1	1900 #1	3	3
1	1900 #2	4	4
1	2500 #1	5	5
1	2500 #2	6	6
1	2500 #3	7	7
2	800 #1	8	8
2	800 #2	9	9
2	1900 #1	10	10
2	1900 #2	11	11
2	2500 #1	12	12
2	2500 #2	13	13
2	2500 #3	14	14
3	800 #1	15	15
3	800 #2	16	16
3	1900 #1	17	17
3	1900 #2	18	18
3	2500 #1	19	19
3	2500 #2	20	20
3	2500 #3	21	21

Upper Block: Sector 1/Auxiliary Cable 1/2500 RRH-1/CPRI-1, Sector 1/Auxiliary Cable 1/2500 RRH-1/CPRI-2, Sector 1/Auxiliary Cable 1/2500 RRH-1/CPRI-3, Sector 2/Auxiliary Cable 1/2500 RRH-1/CPRI-1, Sector 2/Auxiliary Cable 1/2500 RRH-1/CPRI-2, Sector 2/Auxiliary Cable 1/2500 RRH-1/CPRI-3, Sector 3/Auxiliary Cable 1/2500 RRH-1/CPRI-1, Sector 3/Auxiliary Cable 1/2500 RRH-1/CPRI-2, Sector 3/Auxiliary Cable 1/2500 RRH-1/CPRI-3.

Lower Block: Sector 1/Auxiliary Cable 2/800 RRH-2/Secondary CPRI, Sector 1/Auxiliary Cable 2/800 RRH-2/Primary CPRI, Sector 2/Auxiliary Cable 2/2500 RRH-1/CPRI-1, Sector 2/Auxiliary Cable 2/2500 RRH-1/CPRI-2, Sector 2/Auxiliary Cable 2/2500 RRH-1/CPRI-3.



Not to Scale

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JOB NUMBER: 526-104

ENGINEERING LICENSE:

No. 23544
4-20-18
PROFESSIONAL ENGINEER

CHECKED BY:

APPROVED BY:

REVISIONS:

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ISSUED FOR REVIEW	01/18/18	RCD	A

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SITE ADDRESS:
131 GIFFORD LANE,
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SHEET DESCRIPTION:
PLUMBING DIAGRAM

SHEET NUMBER:
RF-2