Alex Murshteyn, Site Acquisition
c/o Cellco Partnership d/b/a Verizon Wireless
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767
Mobile: (508) 821-0159
AMurshteyn@centerlinecommunications.com

December 6, 2017
Melanie A. Bachman
Acting Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051


RE: Notice of Exempt Modification // Site: North Bloomfield CT (ATC: 283562) (2627) Day Hill Road (aka 2619 Day Hill Rd), Bloomfield, CT 06002 N 41.87650 // W -73.74183

Dear Ms. Bachman:

Cellco Partnership d/b/a Verizon Wireless currently maintains 15 antennas at the 110 -foot mount on the existing 110 -foot monopole tower, located at (2619) Day Hill Road, Bloomfield, CT. The tower is owned by American Tower. The property is owned by the River Bend Development CT LLC. Verizon Wireless now intends to replace all 6 of its existing antennas and install side-byside mounts for 6 LTE ( $700 / 850 / 1900 / 2100 \mathrm{MHz}$ ) replacements for its PCS/AWS/LTE upgrade. Additionally, Verizon Wireless will remove 3 new remote radio heads (RRHs) and install 12 new RRHs, with its new antennas, 1 new over voltage protector (OVP) surge arrestor box, as well as 1 new hybrid fiber cable; while removing certain unused coax cabling and updating leased equipment rights, as more fully reflected by the final configuration proposed hereby.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16$50 \mathrm{j}-72(\mathrm{~b})(2)$. In accordance with R.C.S.A. § $16-50 \mathrm{j}-73$, a copy of this letter is being sent to Suzette DeBeatham-Brown, Mayor for the Town of Bloomfield, Jose Giner, the Town's Director of the Planning and Zoning Department, American Tower, the tower owner, and the ground owner, River Bend Development CT LLC.

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2). Enclosed to accommodate this filing are construction drawings dated October 19, 2017 by ATC Tower Services, LLC, a structural analysis dated September 11, 2017 by Tower Engineering Professionals, Inc. and radio frequency (RF) analysis table showing worst-case RF emission calculation by Verizon Wireless RF Design Engineering.

CENTERLINE
COMMUNICATIONS

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the new antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading, as shown in the attached structural analysis by Tower Engineering Professionals, Inc., dated September 11, 2017.

For the foregoing reasons, Verizon Wireless respectfully submits that the proposed modifications to the above referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,


Alex Murshteyn, Site Acquisition c/o Cellco Partnership d/b/a Verizon Wireless
Centerline Communications, LLC
95 Ryan Drive, Suite 1
Raynham, MA 02767
Mobile: (508) 821-0159
AMurshteyn@centerlinecommunications.com
Attachments
cc: Suzette DeBeatham-Brown, Mayor, Town of Bloomfield - as elected official - 1Z9Y45030306985716
Jose Giner, Director, Planning and Zoning Department - as P\&Z official - 1Z9Y45030304130722
American Tower Corporation - as tower owner-1Z9Y45030310277732
River Bend Development CT LLC - as property owner - 1Z9Y45030305826747


Eng. Number OAA710465_C3_01
September 11, 2017

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## Introduction

The purpose of this report is to summarize results of a structural analysis performed on the 109 ft monopole to reflect the change in loading by Verizon.

## Supporting Documents

| Tower Drawings | Sabre Job \#67167, dated October 15, 2012 |
| :--- | :--- |
| Foundation Drawing | Sabre Job \#67167, dated September 19, 2012 |
| Geotechnical Report | DET Job \#2011-20, dated January 28, 2012. |

## Analysis

The tower was analyzed using American Tower Corporation's tower analysis software. This program considers an elastic three-dimensional model and second-order effects per ANSI/TIA-222.

| Basic Wind Speed: | 97 mph (3-Second Gust, $\mathrm{V}_{\text {add }} / 125 \mathrm{mph}$ (3-Second Gust, $\mathrm{V}_{\text {ull }}$ ) |
| :--- | :--- |
| Basic Wind Speed w/ Ice: | $50 \mathrm{mph}(3-$ Second Gust) w/ 1" radial ice concurrent |
| Code: | ANSI/TIA-222-G /2012 IBC / 2016 Connecticut State Building Code |
| Structure Class: | II |
| Exposure Category: | B |
| Topographic Category: | 1 |
| Crest Height: | 0 ft |
| Spectral Response: | $\mathrm{St}=0.18, \mathrm{~S}_{1}=0.06$ |
| Site Class: | D-Stiff Soil |

## Conclusion

Based on the analysis results, the structure meets the requirements per the applicable codes listed above. The tower and foundation can support the equipment as described in this report.

If you have any questions or require additional information, please contact American Tower via email at Engineering@americantower.com. Please include the American Tower site name, site number, and engineering number in the subject line for any questions.

## Existing and Reserved Equipment

| Elevation ${ }^{1}(\mathrm{ft})$ |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 109.0 | 110.0 | 3 | Antel BXA-70063/6CF | T-Arms | (22) 15/8" Coax | Verizon |
|  |  | 6 | Antel LPA-80063/6CF |  |  |  |
| 102.0 | 102.0 | 3 | Ericsson RRUS 1182 | T-Arms | (3) $15 / 8^{\prime \prime}$ (1.63") Fiber | T-Mobile |
|  |  | 3 | Ericsson AlR 21 B4A B2P |  |  |  |
|  |  | 3 | Ericsson AIR 21, 1.3M, B2A B4P (91.5 lbs) |  |  |  |
|  |  | 3 | Commscope LNX-6515D5-VTM |  |  |  |

## Equipment to be Removed

| Elevation ${ }^{1}(\mathrm{ft})$ |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 109.0 | 110.0 | 3 | Antel LPA-171063-12CF-EDIN-X | - | (1) $15 / 8^{\prime \prime}$ Coax <br> (1) $15 / 8$ " Hybriflex | Verizon |
|  |  | 6 | Commscope HBX-6517DS-VTM |  |  |  |
|  |  | 3 | Alcatel-Lucent RRH2×40-AWS. |  |  |  |
|  |  | 1 | RFS DB-T1-6Z-8AB-02 |  |  |  |

## Proposed Equipment

| Elevation' $(\mathrm{ft})$ |  | Qty | Antenna | Mount Type | Lines | Carrier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Mount | RAD |  |  |  |  |  |
| 109.0 | 110.0 | 3 | Nokia AirScale RRH 4T4R B5 160W AHCA | T-Arms | (1) $11 / 4^{\prime \prime}$ Hybriflex (1) $15 / 8$ " Fiber | Verizon |
|  |  | 3 | Alcatel-Lucent B25 RRH4x30 |  |  |  |
|  |  | 3 | Alcatel-Lucent B13 RRH4×30-4R |  |  |  |
|  |  | 3 | Alcatel-Lucent B66A RRH 4×45 |  |  |  |
|  |  | 1 | Raycap RC3DC-3315-PF-48 |  |  |  |
|  |  | 6 | Commscope JAHH-65B-R3B |  |  |  |

[^0]Install proposed coax inside the pole shaft.

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## Structure Usages

| Structural Component | Controlling Usage | Pass/Fail |
| :---: | :---: | :---: |
| Anchor Bolts | $54 \%$ | Pass |
| Shaft | $61 \%$ | Pass |
| Base Plate | $60 \%$ | Pass |

## Foundations

| Reaction Component | Original Design <br> Reactions | Factored Design <br> Reactions* | Analysis Reactions | \% of Design |
| :---: | :---: | :---: | :---: | :---: |
| Moment (Kips-Ft) | $1,612.5$ | $2,176.9$ | $1,081.2$ | $50 \%$ |
| Shear (Kips) | 19.6 | 26.4 | 12.9 | $49 \%$ |

* The design reactions are factored by 1.35 per ANSI/TIA-222-G, Sec. 15.5.1

The structure base reactions resulting from this analysis are acceptable when compared to those shown on the original structure drawings, therefore no modification or reinforcement of the foundation will be required.

Deflection and Sway*

| Antenna Elevation ( ft ) | Antenna | Carrier | Deflection <br> (ft) | Sway (Rotation) ( ${ }^{\circ}$ ) |
| :---: | :---: | :---: | :---: | :---: |
| 109.0 | Nokia AirScale RRH 4T4R B5 160W AHCA | Verizon | 0.909 | 0.823 |
|  | Alcatel-Lucent B25 RRH4×30 |  |  |  |
|  | Alcatel-Lucent B13 RRH4×30-4R |  |  |  |
|  | Alcatel-Lucent B66A RRH 4×45 |  |  |  |
|  | Raycap RC3DC-3315-PF-48 |  |  |  |
|  | Commscope JAHH-65B-R3B |  |  |  |

[^1]
## Standard Conditions

All engineering services are performed on the basis that the information used is current and correct. This information may consist of, but is not necessary limited, to:
-- Information supplied by the client regarding the structure itself, antenna, mounts and feed line loading on the structure and its components, or other relevant information.
-- Information from drawings in the possession of American Tower Corporation, or generated by field inspections or measurements of the structure.

It is the responsibility of the client to ensure that the information provided to A.T. Engineering Service, PLLC and used in the performance of our engineering services is correct and complete. In the absence of information to the contrary, we assume that all structures were constructed in accordance with the drawings and specifications and that their capacity has not significantly changed from the "as new" condition.

Unless explicitly agreed by both the client and American Tower Corporation, all services will be performed in accordance with the current revision of ANSI/TIA -222. The design basic wind speed will be determined based on the minimum basic wind speed as prescribed in ANSI/TIA-222. Although every effort is taken to ensure that the loading considered is adequate to meet the requirements of all applicable regulatory entities, we can provide no assurance to meet any other local and state codes or requirements. If wind and ice loads or other relevant parameters are to be different from the minimum values recommended by the codes, the client shall specify the exact requirement.

All services are performed, results obtained, and recommendations made in accordance with generally accepted engineering principles and practices. A.T. Engineering Service, PLLC is not responsible for the conclusions, opinions and recommendations made by others based on the information we supply.

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| Job Information |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |
| Sections Properties |  |  |  |  |  |  |  |  |
| Shaft Section | Length <br> (ft) | Diameter (in) Accross Fiats Top Bottom |  | Thick <br> (in) | Joint <br> Type | Overlap Length (in) |  Steel <br> Taper <br> Grade <br> (infti) (ksi) |  |
| 1 | 53.250 | 32.27 | 42.92 | 0.250 |  | 0.000 | 0.200000 | 65 |
| 2 | 53.500 | 23.02 | 33.72 | 0.250 | sup Joint | 57.000 | 0.200000 | 65 |
| 3 | 10.500 | 22.00 | 24.09 | 0.188 | Sllp Joint | 42.000 | 0.200000 | 65 |


|  |  |  |  |
| :--- | :--- | :--- | :--- |
| Discrete Appurtenance |  |  |  |
| Attach | Force <br> Elev (ft) | Qty | Description |


|  | Load Cases |
| :--- | :--- |
| $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No Ice |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No Ice (Reduced DL) |
| $1.2 \mathrm{D}+1.0 \mathrm{DI}+1.0 \mathrm{Wi}$ | 50 mph with 1.00 in Radial Ice |
| $(1.2+0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E}$ | Seismic Equivalent Lateral Forces Method |
| $(1.2+0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E}$ | Seismic Equivalent Modal Analysis Method |
| $(0.9-0.2 \mathrm{Sds}) * \mathrm{DL}+\mathrm{E}$ | Seismic (Reduced DL$)$ Equivalent Lateral |
| $(0.9-0.2 S d s) * \mathrm{DL}+\mathrm{E}$ | Seismic (Reduced DL$)$ Equivalent Modal |
| $1.0 \mathrm{D}+1.0 \mathrm{~W}$ | Serviceabllity 60 mph |


| Reactions |  |  |  |
| :--- | :---: | :---: | :---: |
| Load Case | Moment <br> (kip-ft) | Shear <br> (kip) | Axial <br> (kip) |
| $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 1081.21 | 12.87 | 19.49 |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 1072.41 | 12.86 | 14.61 |
| $1.2 \mathrm{D}+1.0 \mathrm{DI}+1.0 \mathrm{WI}$ | 311.30 | 3.76 | 37.86 |


|  |  |  |  |
| :--- | ---: | ---: | :--- |
| $(1.2+0.2 S d s) *$ DL + E ELFM | 75.95 | 0.84 | 19.27 |
| $(1.2+0.2 S d s) *$ DL + E EMAM | 142.82 | 1.48 | 19.27 |
| $(0.9-0.2 S d s) *$ DL + E ELFM | 75.23 | 0.84 | 13.41 |
| $(0.9-0.2 S d s) *$ DL + E EMAM | 141.38 | 1.48 | 13.41 |
| $1.0 D+1.0 W$ | 257.28 | 3.08 | 16.26 |


| Dish Deflections |  |  |  |
| :---: | :---: | :---: | :---: |
| Load Case | Attach <br> Elev (ft) | Deflection <br> (in) | Rotation <br> (deg) |
|  | 0.00 | 0.000 | $\mathbf{0 . 0 0 0}$ |


$\qquad$

53'-3"
$\qquad$
$48^{\prime}-6^{\prime \prime}$

Load Case : $1.2 \mathrm{D}+1.6 \mathrm{~W}$
Max Ratio $60.76 \%$ at 0.0 ft


| Site Number: | 283562 | Code: ANSI/TIA-222-G | $\oplus$ 2007-2017 by ATC IP LLC. All rights reserved. |
| :--- | :--- | :---: | :---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:45 AM |
| Customer: | VERIZON WIRELESS |  |  |


|  |  | Analysis Parameters |  |
| :---: | :---: | :---: | :---: |
| Location: | HARTFORD County, CT | Height ( ft ): | 109 |
| Code: | ANSI/TIA-222-G | Base Diameter (in): | 42.92 |
| Shape: | 18 Sides | Top Diameter (in): | 22.00 |
| Pole Type: | Taper | Taper (in/ft) : | 0.200 |
| Pole Manfacturer: |  | Rotation (deg) : | 0.00 |


|  |  | Ice \& Wind Parameters |  |
| :--- | :--- | :--- | :--- |
| Structure Class: | 11 | Design Wind Speed Without Ice: | 97 mph |
| Exposure Category: | B | Design Wind Speed With Ice: | 50 mph |
| Topographic Category: | 1 | Operational Wind Speed: | 60 mph |
| Crest Height: | 0.0 ft | Design Ice Thickness: | 1.00 in |

## Seismic Parameters

Analysis Method:
Equivalent Modal Analysis \& Equivalent Lateral Force Methods

| Site Class: D-Stiff Soil |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Period Based on Rayleigh Method (sec): |  | 1.72 |  |  |  |
| $\mathrm{T}_{\mathrm{L}}(\mathrm{sec})$ : | 6 | p: | 1.3 | $\mathrm{C}_{5}$ : | 0.040 |
| $S_{\text {s }}$ : | 0.179 | $S_{1}$ | 0.064 | $\mathrm{C}_{5}$ Max: | 0.040 |
| $\mathrm{F}_{\mathrm{a}}$ : | 1.600 | $\mathrm{F}_{\mathrm{v}}$ : | 2.400 | $C_{5} \mathrm{Min}$ : | 0.030 |
| $\mathrm{S}_{\mathrm{ds}}$ : | 0.191 | $\mathrm{S}_{\mathrm{d} 1}$ : | 0.102 |  |  |

## Load Cases

| $1.2 \mathrm{D}+1.6 \mathrm{~W}$ |
| :---: |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ |
| $(1.2+0.2 S d s) \cdot D L+E E L F M$ |
| $(1.2+0.2 \mathrm{Sds})^{\prime} \mathrm{DL}+$ E EMAM |
| (0.9-0.2Sds) ${ }^{\circ} \mathrm{DL}+\mathrm{E}$ ELFM |
| (0.9-0.2Sds) ${ }^{\text {c }}$ DL + E EMAM |
| 1.00 + 1.0 W |

97 mph with No Ice
97 mph with No Ice (Reduced DL)
50 mph with 1.00 in Radial Ice
Seismic Equivalent Lateral Forces Method
Seismic Equivalent Modal Analysis Method
Selsmic (Reduced DL) Equivalent Lateral Forces Method
Seismic (Reduced DL) Equivalent Modal Analysis Method
Serviceability 60 mph

| Shaft Section Properties |  |  |  |  |  |  | Bottom |  |  |  |  |  | Top |  |  |  |  |  | Taper (infif) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{aligned} & \text { Sect } \\ & \text { Info } \end{aligned}$ | Length (ft) | Thick (in) | $\begin{gathered} \text { Fy } \\ \text { (kSi) } \end{gathered}$ | Joint <br> Type | Sitp <br> Joint <br> Len (in) | Weight (Ib) | $\begin{aligned} & \text { Dia } \\ & \text { (in) } \end{aligned}$ | $\begin{gathered} \text { Elev } \\ \text { (ft) } \end{gathered}$ | Area <br> (in ${ }^{2}$ ) | $\begin{aligned} & 1 \mathrm{x} \\ & \left(\mathrm{in} \mathrm{n}^{4}\right) \end{aligned}$ | $\begin{gathered} \text { Wht } \\ \text { Ratio } \end{gathered}$ | D/t Ratio | $\begin{aligned} & \text { Dia } \\ & \text { (in) } \end{aligned}$ | $\begin{gathered} \text { Elev } \\ (\mathrm{ft}) \end{gathered}$ | Area (in ${ }^{2}$ ) | $\operatorname{lix}_{\left(i^{4}\right)}$ | W/t Ratio | D/t Ratio |  |
| 1-18 | 53.250 | 0.2500 | 65 |  | 0.00 | 5,369 | 42.92 | 0.00 | 33.86 | 7788.5 | 28.86 | 171.68 | 32.27 | 53.25 | 25.41 | 3291.9 | 21.35 | 129.09 | 0.199954 |
| $2 \cdot 18$ | 53.500 | 02500 | 65 | Slip | 57.00 | 4,062 | 33.72 | 48.50 | 26.56 | 3759.6 | 22.37 | 134.89 | 23.02 | 102.00 | 18.07 | 1184.2 | 14.83 | 92.10 | 0.199954 |
| 3-18 | 10.500 | 0.1875 | 65 | Slip | 42.00 | 486 | 24.10 | 98.50 | 14.23 | 1028.0 | 21.25 | 128.53 | 22.00 | 109.00 | 12.98 | 780.3 | 19.28 | 117.33 | 0.199954 |
|  |  |  |  | aft We | ight | 9,918 |  |  |  |  |  |  |  |  |  |  |  |  |  |

## Discrete Appurtenance Properties

| Attach <br> Elev <br> (ft) | Description | Qty | Weight (Ib) | $\begin{aligned} & \text { No Io } \\ & \text { EPAa } \\ & \text { (sf) } \end{aligned}$ | $\begin{aligned} & \text { Orientation } \\ & \text { Factor } \end{aligned}$ | Weight (Ib) | $\begin{aligned} & \text { Ice } \\ & \text { EPAa } \\ & \text { (Sf) } \\ & \hline \end{aligned}$ | $\begin{gathered} \text { Orientation } \\ \text { Factor } \\ \hline \end{gathered}$ | Distance From Face <br> (ft) | Vert Ecc (ft) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 109.00 | Alcatel-Lucent B13 RRH4×30- | 3 | 57.80 | 2.140 | 0.67 | 169.14 | 2.964 | 0.67 | 0.000 | 1.000 |
| 109.00 | Alcatel-Lucent B25 RRH4x30 | 3 | 53.00 | 2.120 | 0.67 | 154.54 | 2.949 | 0.67 | 0.000 | 1.000 |
| 109.00 | Alcatel-Lucent B66A RRH | 3 | 67.00 | 2.580 | 0.67 | 184.92 | 3.505 | 0.67 | 0.000 | 1.000 |
| 109.00 | Antel BXA-70063/6CF_ | 3 | 17.00 | 7.570 | 0.65 | 199.67 | 11.133 | 0.65 | 0.000 | 1.000 |
| 109.00 | Antel LPA-80063/6CF | 6 | 27.00 | 9.590 | 0.76 | 414.05 | 11.374 | 0.76 | 0.000 | 1.000 |
| 109.00 | Commscope JAHH-65B-R3B | 6 | 60.60 | 9.110 | 0.69 | 372.69 | 10.876 | 0.69 | 0.000 | 1.000 |
| 109.00 | Nokia AirScale RRH 4T4R B5 | 3 | 35.30 | 1.290 | 0.50 | 105.01 | 1.931 | 0.50 | 0.000 | 1.000 |
| 109.00 | Raycap RC3DC-3315-PF-48 | 1 | 32.00 | 3.780 | 0.67 | 204.20 | 4.858 | 0.67 | 0.000 | 1.000 |
| 109.00 | Round T-Arm | 3 | 250.00 | 9.700 | 0.67 | 519.96 | 20.349 | 0.67 | 0.000 | 0.000 |
| 102.00 | Commscope LNX-6515DS- | 3 | 50.30 | 11.450 | 0.70 | 344.93 | 15.609 | 0.70 | 0.000 | 0.000 |
| 102.00 | Ericsson AIR 21 B4A B2P | 3 | 90.00 | 5.800 | 0.71 | 271.33 | 8.483 | 0.71 | 0.000 | 0.000 |
| 102.00 | Ericsson AlR 21, 1.3M, B2A | 3 | 91.50 | 6.040 | 0.70 | 278.48 | 8.796 | 0.70 | 0.000 | 0.000 |
| 102.00 | Ericsson RRUS 11 B2 | 3 | 50.70 | 2.790 | 0.65 | 143.69 | 4.198 | 0.65 | 0.000 | 0.000 |
| 102.00 | Round T-Arm | 3 | 250.00 | 9.700 | 0.67 | 518.41 | 20.287 | 0.67 | 0.000 | 0.000 |
|  | Totals | 46 | 3595.40 |  | 13,594.87 |  |  | Number of Loadings : |  |  |

Linear Appurtenance Properties

Site Number: $283562 \quad$ Code: ANSI/TIA-222-G 2007-2017 by ATC IP LLC. All rights reserved.

Site Name: NORTH BLOOMFIELD CT. CT Engineering Number:OAA710465_C3_01 9/11/2017 10:50:45 AM
Customer: VERIZON WIRELESS

| Segment Properties | (Max Len : 5.ft) |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg Top Elev <br> (ft) Description | Thick <br> (in) | Flat Dia <br> (in) | Area (in²) | $\begin{gathered} 1 \mathrm{x} \\ \left(\mathrm{in}{ }^{4}\right) \end{gathered}$ | W/t Ratio | D/t Ratio |  | $\underset{\left(\mathrm{in}^{3}\right)}{\mathrm{S}}$ | $\underset{\left(\mathrm{in}^{3}\right)}{\mathrm{Z}}$ | Weight (Ib) |
| 0.00 | 0.2500 | 42.920 | 33.857 | 7.788.5 | 28.86 | 171.68 | 67.5 | 357.4 | 0.0 | 0.0 |
| 5.00 | 0.2500 | 41.920 | 33.064 | 7.253.7 | 28.16 | 167.68 | 68.3 | 340.8 | 0.0 | 569.3 |
| 10.00 | 0.2500 | 40.920 | 32.271 | 6,744.1 | 27.45 | 163.68 | 69.1 | 324.6 | 0.0 | 555.8 |
| 15.00 | 0.2500 | 39.921 | 31.478 | 6,258.8 | 26.75 | 159.68 | 69.9 | 308.8 | 0.0 | 542.3 |
| 20.00 | 0.2500 | 38.921 | 30.684 | 5,797.5 | 26.04 | 155.68 | 70.8 | 293.4 | 0.0 | 528.8 |
| 25.00 | 0.2500 | 37.921 | 29.891 | 5,359.3 | 25.34 | 151.68 | 71.6 | 278.4 | 0.0 | 515.3 |
| 30.00 | 0.2500 | 36.921 | 29.098 | 4,943.9 | 24.63 | 147.69 | 72.4 | 263.7 | 0.0 | 501.8 |
| 35.00 | 0.2500 | 35.922 | 28.304 | 4,550.4 | 23.93 | 143.69 | 73.3 | 249.5 | 0.0 | 488.3 |
| 40.00 | 0.2500 | 34.922 | 27.511 | 4,178.4 | 23.22 | 139.69 | 74.1 | 235.7 | 0.0 | 474.8 |
| 45.00 | 0.2500 | 33.922 | 26.718 | 3,827.3 | 22.51 | 135.69 | 74.9 | 222.2 | 0.0 | 461.3 |
| 48.50 Bot - Section 2 | 0.2500 | 33.222 | 26.163 | 3,593.6 | 22.02 | 132.89 | 75.5 | 213.1 | 0.0 | 314.9 |
| 50.00 ( | 0.2500 | 32.922 | 25.925 | 3,496.4 | 21.81 | 131.69 | 75.7 | 209.2 | 0.0 | 267.9 |
| 53.25 Top - Section 1 | 0.2500 | 32.772 | 25.806 | 3,448.5 | 21.70 | 131.09 | 75.9 | 207.3 | 0.0 | 572.1 |
| 55.00 | 0.2500 | 32.423 | 25.528 | 3,338.4 | 21.46 | 129.69 | 76.2 | 202.8 | 0.0 | 152.8 |
| 60.00 | 0.2500 | 31.423 | 24.735 | 3,036.8 | 20.75 | 125.69 | 77.0 | 190.3 | 0.0 | 427.6 |
| 65.00 | 0.2500 | 30.423 | 23.941 | 2,753.8 | 20.05 | 121.69 | 77.8 | 178.3 | 0.0 | 414.1 |
| 70.00 | 0.2500 | 29.423 | 23.148 | 2,489.1 | 19.34 | 117.69 | 78.7 | 166.6 | 0.0 | 400.6 |
| 75.00 | 0.2500 | 28.423 | 22.355 | 2,241.8 | 18.64 | 113.69 | 79.5 | 155.3 | 0.0 | 387.1 |
| 80.00 | 0.2500 | 27.424 | 21.562 | 2,011.5 | 17.93 | 109.69 | 80.3 | 144.5 | 0.0 | 373.6 |
| 85.00 | 0.2500 | 26.424 | 20.768 | 1,797.6 | 17.23 | 105.70 | 81.1 | 134.0 | 0.0 | 360.1 |
| 90.00 | 0.2500 | 25.424 | 19.975 | 1,599.4 | 16.52 | 101.70 | 82.0 | 123.9 | 0.0 | 346.6 |
| 95.00 | 0.2500 | 24.424 | 19.182 | 1,416.3 | 15.82 | 97.70 | 82.6 | 114.2 | 0.0 | 333.1 |
| 98.50 Bot - Section 3 | 0.2500 | 23.725 | 18.626 | 1,296.8 | 15.32 | 94.90 | 82.6 | 107.7 | 0.0 | 225.1 |
| 100.0 | 0.2500 | 23.425 | 18.388 | 1,247.7 | 15.11 | 93.70 | 82.6 | 104.9 | 0.0 | 166.6 |
| 102.0 Top - Section 2 | 0.1875 | 23.400 | 13.814 | 940.4 | 20.59 | 124.80 | 77.2 | 79.2 | 0.0 | 218.9 |
| 105.0 | 0.1875 | 22.800 | 13.457 | 869.3 | 20.03 | 121.60 | 77.8 | 75.1 | 0.0 | 139.2 |
| 109.0 | 0.1875 | 22.000 | 12.981 | 780.3 | 19.28 | 117.33 | 78.7 | 69.9 | 0.0 | 179.9 |
|  |  |  |  |  |  |  |  |  |  | 9,918.0 |

Site Number: 283562

| Load Case: $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No Ice | 22 Iterations |
| :---: | :---: | :---: |
| Gust Response Factor :1.10 |  | Wind Importance Factor 1.00 |
| Dead Load Factor: 1.20 |  |  |
| Wind Load Factor :1.60 |  |  |

Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg Elev <br> (ft) | Description | Wind FX <br> (b) | Dead L.oad <br> (Ib) | Wind FX <br> (b) | Torsion MY <br> (lb-ft) | Moment MZ <br> ( $\mathrm{lb}-\mathrm{ft}$ ) | Dead Load <br> (b) | Wind FX <br> (Ib) |  | Wind FX <br> (Ib) | $\begin{gathered} \hline \text { Dead } \\ \text { Load } \\ \text { (Ib) } \\ \hline \end{gathered}$ | Torsion MY (lb-ft) | Moment MZ (Ib) |
| 0.00 |  | 164.4 | 0.0 |  |  |  |  | 0.0 | 0.0 | 164.4 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 325.0 | 683.2 |  |  |  |  | 0.0 | 152.9 | 325.0 | 836.0 | 0.0 | 0.0 |
| 10.00 |  | 317.3 | 667.0 |  |  |  |  | 0.0 | 152.9 | 317.3 | 819.8 | 0.0 | 0.0 |
| 15.00 |  | 309.5 | 650.8 |  |  |  |  | 0.0 | 152.9 | 309.5 | 803.6 | 0.0 | 0.0 |
| 20.00 |  | 301.8 | 634.6 |  |  |  |  | 0.0 | 152.9 | 301.8 | 787.4 | 0.0 | 0.0 |
| 25.00 |  | 294.0 | 618.4 |  |  |  |  | 0.0 | 152.9 | 294.0 | 771.3 | 0.0 | 0.0 |
| 30.00 |  | 289.6 | 602.2 |  |  |  |  | 0.0 | 152.9 | 289.6 | 755.1 | 0.0 | 0.0 |
| 35.00 |  | 291.1 | 586.0 |  |  |  |  | 0.0 | 152.9 | 291.1 | 738.9 | 0.0 | 0.0 |
| 40.00 |  | 294.0 | 569.8 |  |  |  |  | 0.0 | 152.9 | 294.0 | 722.7 | 0.0 | 0.0 |
| 45.00 |  | 251.0 | 553.6 |  |  |  |  | 0.0 | 152.9 | 251.0 | 706.5 | 0.0 | 0.0 |
| 48.50 | Bot - Section 2 | 148.5 | 377.9 |  |  |  |  | 0.0 | 107.0 | 148.5 | 484.9 | 0.0 | 0.0 |
| 50.00 |  | 142.5 | 321.5 |  |  |  |  | 0.0 | 45.9 | 142.5 | 367.3 | 0.0 | 0.0 |
| 53.25 | Top - Section 1 | 149.9 | 686.5 |  |  |  |  | 0.0 | 99.4 | 149.9 | 785.9 | 0.0 | 0.0 |
| 55.00 |  | 201.5 | 183.4 |  |  |  |  | 0.0 | 53.5 | 201.5 | 236.9 | 0.0 | 0.0 |
| 60.00 |  | 297.1 | 513.1 |  |  |  |  | 0.0 | 152.9 | 297.1 | 666.0 | 0.0 | 0.0 |
| 65.00 |  | 294.3 | 496.9 |  |  |  |  | 0.0 | 152.9 | 294.3 | 649.8 | 0.0 | 0.0 |
| 70.00 |  | 290.8 | 480.7 |  |  |  |  | 0.0 | 152.9 | 290.8 | 633.6 | 00 | 0.0 |
| 75.00 |  | 286.5 | 464.5 |  |  |  |  | 0.0 | 152.9 | 286.5 | 617.4 | 00 | 0.0 |
| 80.00 |  | 281.5 | 448.3 |  |  |  |  | 0.0 | 152.9 | 281.5 | 601.2 | 00 | 0.0 |
| 85.00 |  | 276.0 | 432.1 |  |  |  |  | 0.0 | 152.9 | 276.0 | 585.0 | 0.0 | 0.0 |
| 90.00 |  | 270.0 | 415.9 |  |  |  |  | 0.0 | 152.9 | 270.0 | 568.8 | 0.0 | 0.0 |
| 95.00 |  | 224.8 | 399.7 |  |  |  |  | 0.0 | 152.9 | 224.8 | 552.6 | 0.0 | 0.0 |
| 98.50 | Bot - Section 3 | 130.6 | 270.2 |  |  |  |  | 0.0 | 107.0 | 130.6 | 377.2 | 0.0 | 00 |
| 100.00 |  | 91.0 | 200.0 |  |  |  |  | 0.0 | 45.9 | 91.0 | 245.8 | 0.0 | 0.0 |
| 102.00 | Top - Section 2 | 128.4 | 262.7 | 2,331.1 | 0.0 | 0.0 | 1,917.0 | 0.0 | 61.2 | 2,459.5 | 2,240.8 | 0.0 | 0.0 |
| 105.00 |  | 176.6 | 167.0 |  |  |  |  | 0.0 | 74.3 | 176.6 | 241.4 | 0.0 | 0.0 |
| 109.00 | Appertunance(s) | 100.0 | 215.9 | 4,340.3 | 0.0 | 3.743.8 | 2,397.5 | 0.0 | 99.1 | 4,440.2 | 2.712 .5 | 0.0 | 00 |
|  |  |  |  |  |  |  |  |  | als: | 12,999.0 | 19,508.3 | 0.00 | 0.00 |

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| Load Case: $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No lce |
| :---: | :---: |
| Gust Response Factor :1.10 |  |
| Dead Load Factor: 1.20 | Wind Importance Factor 1.00 |
| Wind Load Factor: 1.60 |  |

Calculated Forces

| Seg <br> Elev <br> (ft) | $\begin{aligned} & \mathrm{Pu} \\ & \mathrm{FY}(-) \\ & \text { (kips) } \end{aligned}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi <br> (kips) | $\begin{aligned} & \text { phi } \\ & \text { Vn } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \mathrm{phi} \\ \mathrm{Tn} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{aligned} & \text { phi } \\ & \text { Mn } \\ & \text { (ft-kips) } \end{aligned}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -19.49 | -12.87 | 0.00 | -1,081.21 | 0.00 | 1,081.21 | 2,055 | 1,027.73 | 3,611 | 1,808.21 | 0.00 | 0.00 | 0.608 |
| 5.00 | -18.61 | -12.60 | 0.00 | -1,016.88 | 0.00 | 1,016.88 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.10 | -0.19 | 0.592 |
| 10.00 | -17.75 | -12.34 | 0.00 | -953.86 | 0.00 | 953.86 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.41 | -0.38 | 0.576 |
| 15.00 | -16.91 | -12.08 | 0.00 | -892.15 | 0.00 | 892.15 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.92 | -0.58 | 0.559 |
| 20.00 | -16.08 | -11.83 | 0.00 | -831.73 | 0.00 | 831.73 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 1.63 | -0.78 | 0.542 |
| 25.00 | -15.28 | -11.57 | 0.00 | -772.59 | 0.00 | 772.59 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 2.55 | -0.97 | 0.525 |
| 30.00 | -14.49 | -11.32 | 0.00 | -714.72 | 0.00 | 714.72 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 3.67 | -1.17 | 0.507 |
| 35.00 | -13.72 | -11.06 | 0.00 | -658.11 | 0.00 | 658.11 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 5.00 | -1.37 | 0.488 |
| 40.00 | -12.97 | -10.79 | 0.00 | -602.81 | 0.00 | 602.81 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 6.54 | -1.56 | 0.468 |
| 45.00 | -12.24 | -10.56 | 0.00 | -548.84 | 0.00 | 548.84 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 8.28 | -1.76 | 0.446 |
| 48.50 | -11.74 | -10.41 | 0.00 | -511.89 | 0.00 | 511.89 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 9.62 | -1.90 | 0.431 |
| 50.00 | -11.36 | -10.28 | 0.00 | -496.27 | 0.00 | 496.27 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 10.23 | -1.96 | 0.424 |
| 53.25 | -10.56 | -10.12 | 0.00 | -462.87 | 0.00 | 462.87 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 11.61 | -2.08 | 0.399 |
| 55.00 | -10.31 | -9.93 | 0.00 | -445.16 | 0.00 | 445.16 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 12.39 | -2.15 | 0.390 |
| 60.00 | -9.63 | -9.64 | 0.00 | -395.51 | 0.00 | 395.51 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 14.74 | -2.33 | 0.366 |
| 65.00 | -8.96 | -9.34 | 0.00 | -347.33 | 0.00 | 347.33 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 17.27 | -2.51 | 0.339 |
| 70.00 | -8.32 | -9.05 | 0.00 | -300.62 | 0.00 | 300.62 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 19.99 | -2.67 | 0.311 |
| 75.00 | -7.69 | -8.75 | 0.00 | -255.38 | 0.00 | 255.38 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 22.88 | -2.83 | 0.281 |
| 80.00 | -7.08 | -8.46 | 0.00 | -211.62 | 0.00 | 211.62 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 25.92 | -2.98 | 0.248 |
| 85.00 | -6.50 | -8.17 | 0.00 | -169.34 | 0.00 | 169.34 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 29.12 | -3.12 | 0.212 |
| 90.00 | -5.93 | -7.88 | 0.00 | -128.51 | 0.00 | 128.51 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 32.44 | -3.23 | 0.173 |
| 95.00 | -5.38 | -7.63 | 0.00 | -89.13 | 0.00 | 89.13 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 35.88 | -3.33 | 0.130 |
| 98.50 | -5.01 | -7.48 | 0.00 | -62.44 | 0.00 | 62.44 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 38.35 | -3.38 | 0.097 |
| 100.00 | -4.76 | -7.37 | 0.00 | -51.23 | 0.00 | 51.23 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 39.41 | -3.40 | 0.082 |
| 102.00 | -2.67 | -4.79 | 0.00 | -36.48 | 0.00 | 36.48 | 959.49 | 479.75 | 914.96 | 458.16 | 40.84 | -3.42 | 0.083 |
| 105.00 | -2.44 | -4.60 | 0.00 | -22.13 | 0.00 | 22.13 | 942.73 | 471.37 | 875.56 | 438.43 | 43.00 | -3.44 | 0.053 |
| 109.00 | 0.00 | -4.44 | 0.00 | -3.74 | 0.00 | 3.74 | 919.72 | 459.86 | 823.73 | 412.48 | 45.89 | -3.46 | 0.009 |


| Load Case: $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No Ice (Reduced DL ) |
| :--- | :--- |
| Gust Response Factor: 1.10 |  |
| Dead Load Factor :0.90 | Wind Importance Factor 1.00 |
| Wind Load Factor: 1.60 |  |

Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg Elev <br> (ft) | Description | Wind FX <br> (Ib) | Dead Load (Ib) | Wind $F X$ <br> (Ib) | Torsion MY <br> ( $\mathrm{lb}-\mathrm{ft}$ ) | Moment MZ <br> ( $\mathrm{lb}-\mathrm{ft}$ ) | Dead Load <br> (lb) | Wind FX <br> (Ib) | Dead Load <br> (Ib) | Wind FX <br> (Ib) | Dead <br> Load <br> (Ib) | Torsion MY ( $\mathrm{lb}-\mathrm{ft}$ ) | Moment MZ <br> (Ib) |
| 0.00 |  | 164.4 | 0.0 |  |  |  |  | 0.0 | 0.0 | 164.4 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 325.0 | 512.4 |  |  |  |  | 0.0 | 114.7 | 325.0 | 627.0 | 0.0 | 00 |
| 10.00 |  | 317.3 | 500.2 |  |  |  |  | 0.0 | 114.7 | 317.3 | 614.9 | 0.0 | 0.0 |
| 15.00 |  | 309.5 | 488.1 |  |  |  |  | 0.0 | 114.7 | 309.5 | 602.7 | 0.0 | 00 |
| 20.00 |  | 301.8 | 475.9 |  |  |  |  | 0.0 | 114.7 | 301.8 | 590.6 | 0.0 | 00 |
| 25.00 |  | 294.0 | 463.8 |  |  |  |  | 0.0 | 114.7 | 294.0 | 578.4 | 0.0 | 00 |
| 30.00 |  | 289.6 | 451.6 |  |  |  |  | 0.0 | 114.7 | 289.6 | 566.3 | 0.0 | 00 |
| 35.00 |  | 291.1 | 439.5 |  |  |  |  | 0.0 | 114.7 | 291.1 | 554.1 | 0.0 | 00 |
| 40.00 |  | 294.0 | 427.3 |  |  |  |  | 0.0 | 114.7 | 294.0 | 542.0 | 00 | 0.0 |
| 45.00 |  | 251.0 | 415.2 |  |  |  |  | 0.0 | 114.7 | 251.0 | 529.9 | 0.0 | 0.0 |
| 48.50 | Bot - Section 2 | 148.5 | 283.4 |  |  |  |  | 0.0 | 80.3 | 148.5 | 363.7 | 0.0 | 0.0 |
| 50.00 |  | 142.5 | 241.1 |  |  |  |  | 0.0 | 34.4 | 142.5 | 275.5 | 0.0 | 0.0 |
| 53.25 | Top - Section 1 | 149.9 | 514.9 |  |  |  |  | 00 | 74.5 | 149.9 | 589.4 | 0.0 | 0.0 |
| 55.00 |  | 201.5 | 137.6 |  |  |  |  | 00 | 40.1 | 201.5 | 177.7 | 0.0 | 00 |
| 60.00 |  | 297.1 | 384.8 |  |  |  |  | 0.0 | 114.7 | 297.1 | 499.5 | 0.0 | 0.0 |
| 65.00 |  | 294.3 | 372.7 |  |  |  |  | 0.0 | 114.7 | 294.3 | 487.3 | 0.0 | 0.0 |
| 70.00 |  | 290.8 | 360.5 |  |  |  |  | 0.0 | 114.7 | 290.8 | 475.2 | 0.0 | 0.0 |
| 75.00 |  | 286.5 | 348.4 |  |  |  |  | 0.0 | 114.7 | 286.5 | 463.0 | 0.0 | 0.0 |
| 80.00 |  | 281.5 | 336.2 |  |  |  |  | 0.0 | 114.7 | 281.5 | 450.9 | 0.0 | 0.0 |
| 85.00 |  | 276.0 | 324.1 |  |  |  |  | 0.0 | 114.7 | 276.0 | 438.7 | 0.0 | 0.0 |
| 90.00 |  | 270.0 | 311.9 |  |  |  |  | 0.0 | 114.7 | 270.0 | 426.6 | 0.0 | 0.0 |
| 95.00 |  | 224.8 | 299.8 |  |  |  |  | 0.0 | 114.7 | 224.8 | 414.5 | 0.0 | 0.0 |
| 98.50 | Bot - Section 3 | 130.6 | 202.6 |  |  |  |  | 0.0 | 80.3 | 130.6 | 282.9 | 0.0 | 0.0 |
| 100.00 |  | 91.0 | 150.0 |  |  |  |  | 0.0 | 34.4 | 91.0 | 184.4 | 0.0 | 0.0 |
| 102.00 | Top - Section 2 | 128.4 | 197.0 | 2,331.1 | 0.0 | 0.0 | 1.437 .7 | 0.0 | 45.9 | 2,459.5 | 1,680.6 | 0.0 | 0.0 |
| 105.00 |  | 176.6 | 125.3 |  |  |  |  | 0.0 | 55.8 | 176.6 | 181.0 | 0.0 | 0.0 |
| 109.00 | Appertunance(s) | 100.0 | 161.9 | 4,340.3 | 0.0 | 3,743.8 | 1,798.1 | 0.0 | 74.3 | 4,440.2 | 2,034.4 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  | Totals: |  | 12,999.0 | 14,631.2 | 0.00 | 0.00 |

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| Load Case: $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 97 mph with No Ice (Reduced DL) | 22 Iterations |
| :---: | :---: | :---: |
| Gust Response Factor : 1.10 |  | Wind Importance Factor 1.00 |
| Dead Load Factor :0.90 |  |  |
| Wind Load Factor : 1.60 |  |  |

Calculated Forces

| Seg <br> Elev <br> (ft) | Pu FY (-) (kips) | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \mathrm{Tu} \\ \mathrm{MY} \\ \text { (ft-kips) } \end{gathered}$ | Mu MZ (ft-kips) | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi <br> (kips) | $\begin{aligned} & \text { phi } \\ & \text { Vn } \\ & \text { (kips) } \end{aligned}$ |  | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -14.61 | -12.86 | 0.00 | -1,072.41 | 0.00 | 1,072.41 | 2,055.47 | ,027.73 | 3,611.06 | 1,808,21 | 0.00 | 0.00 | 0.600 |
| 5.00 | -13.94 | -12.58 | 0.00 | -1,008.12 | 0.00 | 1,008.12 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.10 | -0.19 | 0.585 |
| 10.00 | . 13.29 | -12.30 | 0.00 | -945.22 | 0.00 | 945.22 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.40 | -0.38 | 0.569 |
| 15.00 | - 12.65 | -12.03 | 0.00 | -883.70 | 0.00 | 883.70 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.91 | -0.57 | 0.552 |
| 20.00 | - 12.02 | -11.76 | 0.00 | -823.54 | 0.00 | 823.54 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 1.61 | -0.77 | 0.535 |
| 25.00 | -11.41 | -11.50 | 0.00 | -764.72 | 0.00 | 764.72 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 2.52 | -0.96 | 0.518 |
| 30.00 | -10.81 | -11.24 | 0.00 | -707.22 | 0.00 | 707.22 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 3.64 | -1.16 | 0.499 |
| 35.00 | -10.22 | -10.97 | 0.00 | -651.04 | 0.00 | 651.04 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 4.95 | -1.35 | 0.481 |
| 40.00 | -9.65 | -10.69 | 0.00 | -596.19 | 0.00 | 596.19 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 6.48 | -1.55 | 0.461 |
| 45.00 | -9.10 | -10.45 | 0.00 | -542.72 | 0.00 | 542.72 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 8.20 | -1.74 | 0.440 |
| 48.50 | . 8.72 | -10.31 | 0.00 | -506.13 | 0.00 | 506.13 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 9.53 | -1.88 | 0.425 |
| 50.00 | -8.44 | -10.17 | 0.00 | -490.67 | 0.00 | 490.67 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 10.13 | -1.94 | 0.418 |
| 53.25 | -7.84 | -10.01 | 0.00 | -457.61 | 0.00 | 457.61 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 11.50 | -2.06 | 0.393 |
| 55.00 | -7.64 | -9.82 | 0.00 | -440.09 | 0.00 | 440.09 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 12.27 | -2.13 | 0.384 |
| 60.00 | -7.13 | -9.53 | 0.00 | -390.98 | 0.00 | 390.98 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 14.59 | -2.31 | 0.360 |
| 65.00 | -6.63 | -9.23 | 0.00 | -343.34 | 0.00 | 343.34 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 17.10 | -2.48 | 0.334 |
| 70.00 | -6.14 | -8.94 | 0.00 | -297.17 | 0.00 | 297.17 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 19.79 | -2.65 | 0.306 |
| 75.00 | -5.67 | -8.65 | 0.00 | -252.48 | 0.00 | 252.48 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 22.65 | -2.80 | 0.276 |
| 80.00 | -5.21 | -8.35 | 0.00 | -209.25 | 0.00 | 209.25 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 25.66 | -2.95 | 0.244 |
| 85.00 | -4.77 | -8.07 | 0.00 | -167.48 | 0.00 | 167.48 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 28.82 | -3.08 | 0.209 |
| 90.00 | -4.34 | -7.78 | 0.00 | -127.15 | 0.00 | 127.15 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 32.12 | -3.20 | 0.170 |
| 95.00 | -3.93 | -7.54 | 0.00 | -88.24 | 0.00 | 88.24 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 35.52 | -3.30 | 0.128 |
| 98.50 | -3.65 | -7.39 | 0.00 | -61.86 | 0.00 | 61.86 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 37.96 | -3.35 | 0.096 |
| 100.00 | -3.47 | -7.29 | 0.00 | -50.76 | 0.00 | 50.76 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 39.01 | -3.37 | 0.081 |
| 102.00 | -1.94 | -4.74 | 0.00 | -36.18 | 0.00 | 36.18 | 959.49 | 479.75 | 914.96 | 458.16 | 40.43 | -3.39 | 0.081 |
| 105.00 | -1.77 | -4.55 | 0.00 | -21.96 | 0.00 | 21.96 | 942.73 | 471.37 | 875.56 | 438.43 | 42.56 | -3.41 | 0.052 |
| 109.00 | 0.00 | -4.44 | 0.00 | -3.74 | 0.00 | 3.74 | 919.72 | 459.86 | 823.73 | 412.48 | 45.42 | -3.42 | 0.009 |

Site Number: 283562
Site Name: NORTH BLOOMFIELD CT, CT Engineering Number:OAA710465_C3_01 9/11/2017 10:50:46 AM
Customer: VERIZON WIRELESS

| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ | 50 mph with 1.00 in Radial Ice | 21 Iterations |
| :--- | ---: | ---: |
| Gust Response Factor :1.10 | Ice Dead Load Factor 1.00 | Wind Importance Factor 1.00 |
| Dead Load Factor: 1.20 | Ice Importance Factor :1.00 |  |
| Wind Load Factor: 1.00 |  |  |

Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (Ib) | Dead Load <br> (Ib) | Wind FX <br> (lb) | Torsion MY <br> (lb-ft) | Moment MZ <br> (lb-ft) | Dead Load (Ib) | Wind $F X$ <br> (Ib) | $\begin{aligned} & \text { Dead } \\ & \text { Load } \\ & \text { (Ib) } \\ & \hline \end{aligned}$ | Wind FX <br> (Ib) | $\begin{aligned} & \hline \text { Dead } \\ & \text { Load } \\ & \text { (Ib) } \end{aligned}$ | Torsion MY ( $1 \mathrm{~b}-\mathrm{ft}$ ) | Moment MZ (Ib) |
| 0.00 |  | 54.0 | 0.0 |  |  |  |  | 0.0 | 0.0 | 54.0 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 107.3 | 1,103.8 |  |  |  |  | 0.0 | 152.9 | 107.3 | 1,256.7 | 0.0 | 0.0 |
| 10.00 |  | 105.5 | 1,127.6 |  |  |  |  | 0.0 | 152.9 | 105.5 | 1,280.4 | 0.0 | 0.0 |
| 15.00 |  | 103.5 | 1,125.1 |  |  |  |  | 0.0 | 152.9 | 103.5 | 1,278.0 | 0.0 | 0.0 |
| 20.00 |  | 101.4 | 1,114.1 |  |  |  |  | 0.0 | 152.9 | 101.4 | 1,267.0 | 0.0 | 0.0 |
| 25.00 |  | 99.2 | 1,098.7 |  |  |  |  | 0.0 | 152.9 | 99.2 | 1,251.5 | 0.0 | 0.0 |
| 30.00 |  | 98.2 | 1,080.4 |  |  |  |  | 0.0 | 152.9 | 98.2 | 1,233.2 | 0.0 | 0.0 |
| 35.00 |  | 99.1 | 1,060.1 |  |  |  |  | 0.0 | 152.9 | 99.1 | 1.213 .0 | 0.0 | 0.0 |
| 40.00 |  | 100.5 | 1,038.4 |  |  |  |  | 0.0 | 152.9 | 100.5 | 1,191.3 | 0.0 | 0.0 |
| 45.00 |  | 86.1 | 1,015.6 |  |  |  |  | 0.0 | 152.9 | 86.1 | 1,168.5 | 0.0 | 0.0 |
| 48.50 | Bot - Section 2 | 51.1 | 698.2 |  |  |  |  | 0.0 | 107.0 | 51.1 | 805.2 | 0.0 | 0.0 |
| 50.00 |  | 49.1 | 460.3 |  |  |  |  | 0.0 | 45.9 | 49.1 | 506.2 | 0.0 | 0.0 |
| 53.25 | Top. Section 1 | 51.7 | 983.3 |  |  |  |  | 0.0 | 99.4 | 51.7 | 1,082.6 | 0.0 | 0.0 |
| 55.00 |  | 69.8 | 342.4 |  |  |  |  | 0.0 | 53.5 | 69.8 | 395.9 | 0.0 | 0.0 |
| 60.00 |  | 103.2 | 957.0 |  |  |  |  | 0.0 | 152.9 | 103.2 | 1,109.9 | 0.0 | 0.0 |
| 65.00 |  | 102.7 | 931.4 |  |  |  |  | 0.0 | 152.9 | 102.7 | 1,084.3 | 0.0 | 0.0 |
| 70.00 |  | 102.0 | 905.3 |  |  |  |  | 0.0 | 152.9 | 102.0 | 1,058.2 | 0.0 | 0.0 |
| 75.00 |  | 101.0 | 878.8 |  |  |  |  | 0.0 | 152.9 | 101.0 | 1,031.7 | 0.0 | 0.0 |
| 80.00 |  | 99.9 | 851.9 |  |  |  |  | 0.0 | 152.9 | 99.9 | 1,004.8 | 0.0 | 0.0 |
| 85.00 |  | 98.5 | 824.7 |  |  |  |  | 0.0 | 152.9 | 98.5 | 977.6 | 0.0 | 0.0 |
| 90.00 |  | 96.9 | 797.2 |  |  |  |  | 0.0 | 152.9 | 96.9 | 950.1 | 0.0 | 0.0 |
| 95.00 |  | 81.2 | 769.4 |  |  |  |  | 0.0 | 152.9 | 81.2 | 922.3 | 0.0 | 0.0 |
| 98.50 | Bot - Section 3 | 47.4 | 523.4 |  |  |  |  | 0.0 | 107.0 | 47.4 | 630.4 | 0.0 | 0.0 |
| 100.00 |  | 33.1 | 309.1 |  |  |  |  | 0.0 | 45.9 | 33.1 | 355.0 | 0.0 | 0.0 |
| 102.00 | Top - Section 2 | 46.8 | 406.2 | 615.4 | 0.0 | 0.0 | 4,291.6 | 0.0 | 61.2 | 662.2 | 4,759.0 | 0.0 | 0.0 |
| 105.00 |  | 64.7 | 377.9 |  |  |  |  | 0.0 | 74.3 | 64.7 | 452.2 | 0.0 | 0.0 |
| 109.00 | Appertunance(s) | 36.7 | 489.0 | 988.5 | 0.0 | 780.7 | 9,010.1 | 0.0 | 99.1 | 1,025.2 | 9,598 3 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 3,794.64 | 37,863.2 | 0.00 | 0.00 |

Page: 8

| Load Case: $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ <br> Gust Response Factor :1.10 <br> Dead Load Factor :1.20 <br> Wind Load Factor :1.00 |  |  |  | 50 mph with 1.00 in Radial Ice Ice Dead Load Factor :1.00 |  |  |  |  | 21 Iterations <br> Wind Importance Factor 1.00 Ice Importance Factor :1.00 |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Calculated Forces |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Seg <br> Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(\cdot) \\ \text { (kips) } \end{gathered}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MX} \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | $\begin{aligned} & \text { phi } \\ & \text { Pn } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ |  | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflec (in) | Rotation (deg) | Ratio |
| 0.00 | . 37.86 | -3.76 | 0.00 | -311.30 | 00.00 | 311.30 | 2,055.47 | 1,027.73 | 3,611.06 | 1,808.21 | 0.00 | 0.00 | 0.191 |
| 5.00 | -36.60 | -3.69 | 0.00 | -292.51 | 10.00 | 292.51 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.03 | -0.06 | 0.186 |
| 10.00 | -35.32 | -3.61 | 0.00 | -274.08 | - 0.00 | 274.08 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.12 | -0.11 | 0.180 |
| 15.00 | -34.04 | -3.54 | 0.00 | -256.02 | 20.00 | 256.02 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.26 | -0.17 | 0.175 |
| 20.00 | -32.77 | -3.47 | 0.00 | -238.32 | 20.00 | 238.32 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.47 | -0.22 | 0.170 |
| 25.00 | -31.51 | -3.39 | 0.00 | -220.99 | - 0.00 | 220.99 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.73 | -0.28 | 0.164 |
| 30.00 | -30.28 | -3.32 | 0.00 | -204.03 | 30.00 | 204.03 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 1.05 | -0.34 | 0.158 |
| 35.00 | -29.06 | -3.24 | 0.00 | -187.45 | 50.00 | 187.45 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 1.44 | -0.39 | 0.152 |
| 40.00 | -27.87 | -3.16 | 0.00 | -171.25 | - 0.00 | 171.25 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 1.88 | -0.45 | 0.146 |
| 45.00 | -26.70 | -3.08 | 0.00 | -155.47 | $7 \quad 0.00$ | 155.47 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 2.38 | -0.50 | 0.139 |
| 48.50 | -25.89 | -3.04 | 0.00 | -144.68 | 80.00 | 144.68 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 2.76 | -0.54 | 0.134 |
| 50.00 | -25.38 | -3.00 | 0.00 | -140.12 | 20.00 | 140.12 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 2.93 | -0.56 | 0.132 |
| 53.25 | -24.30 | -2.94 | 0.00 | -130.39 | 90.00 | 130.39 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 3.33 | -0.60 | 0.124 |
| 55.00 | -23.90 | -2.88 | 0.00 | -125.23 | 30.00 | 125.23 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 3.55 | -0.61 | 0.122 |
| 60.00 | -22.79 | -2.79 | 0.00 | -110.81 | 10.00 | 110.81 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 4.22 | -0.66 | 0.114 |
| 65.00 | -21.71 | -2.69 | 0.00 | -96.87 | $7 \quad 0.00$ | 96.87 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 4.94 | -0.71 | 0.106 |
| 70.00 | -20.65 | -2.59 | 0.00 | -83.41 | $1 \quad 0.00$ | 83.41 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 5.71 | -0.76 | 0.097 |
| 75.00 | -19.62 | -2.49 | 0.00 | -70.45 | $5 \quad 0.00$ | 70.45 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 6.53 | -0.80 | 0.088 |
| 80.00 | -18.61 | -2.39 | 0.00 | -57.99 | 90.00 | 57.99 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 7.40 | -0.84 | 0.079 |
| 85.00 | -17.63 | -2.29 | 0.00 | -46.05 | 50.00 | 46.05 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 8.30 | -0.88 | 0.068 |
| 90.00 | -16.68 | -2.18 | 0.00 | -34.61 | 10.00 | 34.61 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 9.25 | -0.91 | 0.057 |
| 95.00 | -15.76 | -2.09 | 0.00 | -23.69 | - 0.00 | 23.69 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 10.22 | -0.94 | 0.045 |
| 98.50 | -15.13 | -2.04 | 0.00 | -16.37 | $7 \quad 0.00$ | 16.37 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 10.91 | -0.95 | 0.035 |
| 100.00 | -14.78 | -2.00 | 0.00 | -13.31 | 10.00 | 13.31 | 1,366.16 | 683.08 | 1.297.16 | 649.54 | 11.21 | -0.96 | 0.031 |
| 102.00 | -10.03 | -1.26 | 0.00 | -9.31 | 10.00 | 9.31 | 959.49 | 479.75 | 914.96 | 458.16 | 11.61 | -0.96 | 0.031 |
| 105.00 | . 9.58 | -1.19 | 0.00 | -5.53 | 30.00 | 5.53 | 942.73 | 471.37 | 875.56 | 438.43 | 12.22 | . 0.97 | 0.023 |
| 109.00 | 0.00 | -1.03 | 0.00 | -0.78 | 80.00 | 0.78 | 919.72 | 459.86 | 823.73 | 412.48 | 13.04 | -0.97 | 0.002 |

Site Number: 283562

| Load Case: $1.0 \mathrm{O}+1.0 \mathrm{~W}$ | Serviceability 60 mph | 21 Iterations |
| :---: | :---: | :---: |
| Gust Response Factor :1.10 |  | Wind Importance Factor 1.00 |
| Dead Load Factor :1.00 |  |  |
| Wind Load Factor :1.00 |  |  |

Applied Segment Forces Summary

|  |  | Shaft Forces |  | Discrete Forces |  |  |  | Linear Forces |  | Sum of Forces |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Seg <br> Elev <br> (ft) | Description | Wind FX <br> (Ib) | Dead Load <br> ( B ) | Wind FX <br> (Ib) | Torsion MY <br> ( $\mathrm{lb} \cdot \mathrm{ft}$ ) | Moment MZ <br> ( lb -ft) | Dead Load <br> (Ib) | Wind FX <br> (b) | $\begin{aligned} & \hline \text { Dead } \\ & \text { Load } \\ & \text { (Ib) } \\ & \hline \end{aligned}$ | Wind FX <br> (Ib) | $\begin{gathered} \hline \text { Dead } \\ \text { Load } \\ \text { (Ib) } \\ \hline \end{gathered}$ | Torsion MY ( $\mathrm{lb}-\mathrm{ft}$ ) | Moment MZ (Ib) |
| 0.00 |  | 39.3 | 0.0 |  |  |  |  | 0.0 | 0.0 | 39.3 | 0.0 | 0.0 | 0.0 |
| 5.00 |  | 77.7 | 569.3 |  |  |  |  | 0.0 | 127.4 | 77.7 | 696.7 | 0.0 | 0.0 |
| 10.00 |  | 75.9 | 555.8 |  |  |  |  | 0.0 | 127.4 | 75.9 | 683.2 | 0.0 | 0.0 |
| 15.00 |  | 74.0 | 542.3 |  |  |  |  | 0.0 | 127.4 | 74.0 | 669.7 | 0.0 | 0.0 |
| 20.00 |  | 72.2 | 528.8 |  |  |  |  | 0.0 | 127.4 | 72.2 | 656.2 | 0.0 | 0.0 |
| 25.00 |  | 70.3 | 515.3 |  |  |  |  | 0.0 | 127.4 | 70.3 | 642.7 | 0.0 | 0.0 |
| 30.00 |  | 69.3 | 501.8 |  |  |  |  | 0.0 | 127.4 | 69.3 | 629.2 | 0.0 | 0.0 |
| 35.00 |  | 69.6 | 488.3 |  |  |  |  | 0.0 | 127.4 | 69.6 | 615.7 | 0.0 | 0.0 |
| 40.00 |  | 70.3 | 474.8 |  |  |  |  | 0.0 | 127.4 | 70.3 | 602.2 | 0.0 | 0.0 |
| 45.00 |  | 60.0 | 461.3 |  |  |  |  | 0.0 | 127.4 | 60.0 | 588.7 | 0.0 | 0.0 |
| 48.50 | Bot - Section 2 | 35.5 | 314.9 |  |  |  |  | 0.0 | 89.2 | 35.5 | 404.1 | 0.0 | 0.0 |
| 50.00 |  | 34.1 | 267.9 |  |  |  |  | 0.0 | 38.2 | 34.1 | 306.1 | 0.0 | 0.0 |
| 53.25 | Top - Section 1 | 35.8 | 572.1 |  |  |  |  | 0.0 | 82.8 | 35.8 | 654.9 | 0.0 | 0.0 |
| 55.00 |  | 48.2 | 152.8 |  |  |  |  | 0.0 | 44.6 | 48.2 | 197.4 | 0.0 | 0.0 |
| 60.00 |  | 71.1 | 427.6 |  |  |  |  | 0.0 | 127.4 | 71.1 | 555.0 | 0.0 | 0.0 |
| 65.00 |  | 70.4 | 414.1 |  |  |  |  | 0.0 | 127.4 | 70.4 | 541.5 | 0.0 | 0.0 |
| 70.00 |  | 69.5 | 400.6 |  |  |  |  | 0.0 | 127.4 | 69.5 | 528.0 | 0.0 | 0.0 |
| 75.00 |  | 68.5 | 387.1 |  |  |  |  | 0.0 | 127.4 | 68.5 | 514.5 | 0.0 | 0.0 |
| 80.00 |  | 67.3 | 373.6 |  |  |  |  | 0.0 | 127.4 | 67.3 | 501.0 | 0.0 | 0.0 |
| 85.00 |  | 66.0 | 360.1 |  |  |  |  | 0.0 | 127.4 | 66.0 | 487.5 | 0.0 | 0.0 |
| 90.00 |  | 64.6 | 346.6 |  |  |  |  | 0.0 | 127.4 | 64.6 | 474.0 | 0.0 | 0.0 |
| 95.00 |  | 53.7 | 333.1 |  |  |  |  | 0.0 | 127.4 | 53.7 | 460.5 | 0.0 | 0.0 |
| 98.50 | Bot - Section 3 | 31.2 | 225.1 |  |  |  |  | 0.0 | 89.2 | 31.2 | 314.3 | 0.0 | 0.0 |
| 100.00 |  | 21.8 | 166.6 |  |  |  |  | 0.0 | 38.2 | 21.8 | 204.9 | 0.0 | 0.0 |
| 102.00 | Top - Section 2 | 30.7 | 218.9 | 557.5 | 0.0 | 0.0 | 1,597.5 | 00 | 51.0 | 588.2 | 1,867.3 | 0.0 | 0.0 |
| 105.00 |  | 42.2 | 139.2 |  |  |  |  | 0.0 | 61.9 | 42.2 | 201.1 | 0.0 | 0.0 |
| 109.00 | Appertunance(s) | 23.9 | 179.9 | 1,037.9 | 0.0 | 895.3 | 1,997.9 | 0.0 | 82.6 | 1,061.8 | 2,260.4 | 0.0 | 0.0 |
|  |  |  |  |  |  |  |  |  | als: | 3,108.50 | 16,256.9 | 0.00 | 0.00 |

Site Number: $283562 \quad$ Code: ANSIITIA-222-G $\quad 2007 \cdot 2017$ by ATC IP LLC. All rights reserved.

Site Name: NORTH BLOOMFIELD CT, CT
Engineering Number:OAA710465_C3_01
9/11/2017 10:50:47 AM
Customer: VERIZON WIRELESS

| Load Case: $1.0 \mathrm{D}+1.0 \mathrm{~W}$ | Serviceability 60 mph | 21 Iterations |
| :--- | :--- | ---: |
| Gust Response Factor :1.10 |  | Wind Importance Factor 1.00 |
| Dead Load Factor:1.00 |  |  |
| Wind Load Factor: $: 1.00$ |  |  |

## Calculated Forces

| Seg <br> Elev <br> (ft) | Pu FY (-) (kips) | Vu <br> FX (.) <br> (kips) | $\begin{gathered} \mathrm{Tu} \\ \mathrm{MY} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MX} \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | phi <br> (kips) | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \mathrm{phi} \\ \mathrm{Tn} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{aligned} & \mathrm{phi} \\ & \mathrm{Mn} \\ & \text { (ft-kips) } \end{aligned}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -16.26 | -3.08 | 0.00 | -257.28 | 0.00 | 257.28 | 2,055.47 | 1,027.73 | 3,611 | 1,808.21 | 0.00 | 0.00 | 0.150 |
| 5.00 | -15.56 | -3.01 | 0.00 | -241.90 | 0.00 | 241.90 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.02 | -0.05 | 0.146 |
| 10.00 | -14.87 | -2.95 | 0.00 | -226.85 | 0.00 | 226.85 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.10 | -0.09 | 0.142 |
| 15.00 | -14.20 | -2.88 | 0.00 | -212.13 | 0.00 | 212.13 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.22 | -0.14 | 0.138 |
| 20.00 | -13.54 | -2.82 | 0.00 | -197.72 | 0.00 | 197.72 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.39 | -0.18 | 0.134 |
| 25.00 | . 12.90 | -2.76 | 0.00 | -183.63 | 0.00 | 183.63 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.61 | -0.23 | 0.130 |
| 30.00 | -12.27 | -2.69 | 0.00 | -169.85 | 0.00 | 169.85 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 0.87 | -0.28 | 0.125 |
| 35.00 | -11.65 | -2.63 | 0.00 | -156.38 | 0.00 | 156.38 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 1.19 | -0.33 | 0.120 |
| 40.00 | -11.04 | -2.57 | 0.00 | -143.23 | 0.00 | 143.23 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 1.55 | -0.37 | 0.115 |
| 45.00 | -10.45 | -2.51 | 0.00 | -130.40 | 0.00 | 130.40 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 1.97 | -0.42 | 0.110 |
| 48.50 | -10.05 | -2.47 | 0.00 | -121.61 | 0.00 | 121.61 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 2.29 | -0.45 | 0.106 |
| 50.00 | -9.74 | -2.44 | 0.00 | -117.90 | 0.00 | 117.90 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 2.43 | -0.47 | 0.105 |
| 53.25 | -9.09 | -2.40 | 0.00 | -109.97 | 0.00 | 109.97 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 2.76 | -0.50 | 0.098 |
| 55.00 | -8.89 | -2.36 | 0.00 | -105.76 | 0.00 | 105.76 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 2.95 | -0.51 | 0.096 |
| 60.00 | -8.33 | -2.29 | 0.00 | -93.97 | 0.00 | 93.97 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 3.50 | -0.55 | 0.090 |
| 65.00 | -7.79 | -2.22 | 0.00 | -82.52 | 0.00 | 82.52 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 4.11 | -0.60 | 0.084 |
| 70.00 | -7.26 | -2.15 | 0.00 | -71.43 | 0.00 | 71.43 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 4.75 | -0.64 | 0.077 |
| 75.00 | -6.75 | -2.08 | 0.00 | -60.69 | 0.00 | 60.69 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 5.44 | -0.67 | 0.070 |
| 80.00 | -6.25 | -2.01 | 0.00 | -50.30 | 0.00 | 50.30 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 6.16 | -0.71 | 0.062 |
| 85.00 | -5.76 | -1.94 | 0.00 | -40.26 | 0.00 | 40.26 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 6.92 | -0.74 | 0.053 |
| 90.00 | -5.28 | -1.87 | 0.00 | -30.56 | 0.00 | 30.56 | 1,473.59 | 736.79 | 1,521,17 | 761.71 | 7.71 | -0.77 | 0.044 |
| 95.00 | -4.82 | -1.81 | 0.00 | -21.20 | 0.00 | 21.20 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 8.53 | -0.79 | 0.033 |
| 98.50 | -4.51 | -1.78 | 0.00 | -14.86 | 0.00 | 14.86 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 9.12 | -0.80 | 0.026 |
| 100.00 | -4.30 | -1.75 | 0.00 | -12.19 | 0.00 | 12.19 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 9.37 | -0.81 | 0.022 |
| 102.00 | -2.45 | -1.14 | 0.00 | -8.69 | 0.00 | 8.69 | 959.49 | 479.75 | 914.96 | 458.16 | 9.71 | -0.81 | 0.022 |
| 105.00 | -2.24 | -1.09 | 0.00 | -5.27 | 0.00 | 5.27 | 942.73 | 471.37 | 875.56 | 438.43 | 10.22 | -0.82 | 0.014 |
| 109.00 | 0.00 | -1.06 | 0.00 | -0.90 | 0.00 | 0.90 | 919.72 | 459.86 | 823.73 | 412.48 | 10.91 | . 0.82 | 0.002 |


| Site Number: | 283562 | Code: ANSI/TIA-222-G | o 2007.2017 by ATC IP LLC. All rights reserved. |
| :--- | :--- | :---: | :---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |
| Customer: | VERIZON WIRELESS |  |  |

## Equivalent Lateral Forces Method Analysis

(Based on ASCE7-10 Chapters 11, 12، 15)

| Spectral Response Acceleration for Short Period (S ${ }_{\mathrm{S}}$ ): | 0.18 |
| :---: | :---: |
| Spectral Response Acceleration at 1.0 Second Period ( $\mathrm{S}_{1}$ ): | 006 |
| Long-Period Transition Period ( $\mathrm{T}_{\mathrm{L}}$ ) : | 6 |
| Importance Factor ( $\mathrm{I}_{\mathrm{E}}$ ): | 1.00 |
| Site Coefficient $\mathrm{F}_{\mathrm{a}}$ : | 1.60 |
| Site Coeffiecient $\mathrm{F}_{\mathrm{v}}$ : | 2.40 |
| Response Modification Coefficient (R): | 1.50 |
| Design Spectral Response Acceleration at Short Period ( $\mathrm{S}_{\mathrm{ds}}$ ): | 0.19 |
| Design Spectral Response Acceleration at 1.0 Second Period (S $\mathrm{Sa}_{1}$ ): | 0.10 |
| Seismic Response Coefficient ( C s ${ }_{\text {s }}$ ): | 0.04 |
| Upper Limit $\mathrm{C}_{\text {s }}$ | 0.04 |
| Lower Limit $\mathrm{C}_{5}$ | 0.03 |
| Period based on Rayleigh Method (sec): | 1.72 |
| Redundancy Factor (p): | 1.30 |
| Seismic Force Distribution Exponent (k): | 1.61 |
| Total Unfactored Dead Load: | 16.26 |
| Seismic Base Shear ( E ): | 0.84 |



| Segment | (ft) | (lb) | ( $\mathrm{lb}-\mathrm{ft}$ ) | $\mathrm{c}_{\mathrm{vx}}$ | (Ib) | (Ib) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 107.00 | 263 | 485 | 0.033 | 28 | 325 |
| 25 | 103.50 | 201 | 352 | 0.024 | 20 | 249 |
| 24 | 101.00 | 270 | 454 | 0.031 | 26 | 334 |
| 23 | 99.25 | 205 | 335 | 0.023 | 19 | 254 |
| 22 | 96.75 | 314 | 494 | 0.034 | 28 | 389 |
| 21 | 92.50 | 461 | 673 | 0.046 | 38 | 570 |
| 20 | 87.50 | 474 | 634 | 0.043 | 36 | 587 |
| 19 | 82.50 | 487 | 593 | 0.040 | 34 | 604 |
| 18 | 77.50 | 501 | 551 | 0.037 | 31 | 620 |
| 17 | 72.50 | 514 | 508 | 0.035 | 29 | 637 |
| 16 | 67.50 | 528 | 465 | 0.032 | 27 | 654 |
| 15 | 62.50 | 541 | 421 | 0.029 | 24 | 670 |
| 14 | 57.50 | 555 | 377 | 0.026 | 22 | 687 |
| 13 | 54.13 | 197 | 122 | 0.008 | 7 | 244 |
| 12 | 51.63 | 655 | 374 | 0.025 | 21 | 811 |
| 11 | 49.25 | 306 | 162 | 0.011 | 9 | 379 |
| 10 | 46.75 | 404 | 197 | 0.013 | 11 | 500 |
| 9 | 42.50 | 589 | 246 | 0.017 | 14 | 729 |
| 8 | 37.50 | 602 | 206 | 0.014 | 12 | 746 |
| 7 | 32.50 | 616 | 167 | 0.011 | 10 | 762 |
| 6 | 27.50 | 629 | 131 | 0.009 | 7 | 779 |
| 5 | 22.50 | 643 | 97 | 0.007 | 6 | 796 |
| 4 | 17.50 | 656 | 66 | 0.004 | 4 | 813 |

Page: 12

| Site Number: 283562 |  | Code: ANSI/TIA-222-G |  |  | - 2007 - 2017 by ATC IP LLC. All rights reserved. |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Site Name: NORTH BLO | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 |  |  | 9/11/2017 10:50:47 AM |  |
| Customer: VERIZON WIRELESS |  |  |  |  |  |  |
| 3 | 12.50 | 670 | 39 | 0.003 | 2 | 829 |
| 2 | 7.50 | 683 | 18 | 0.001 | 1 | 846 |
| 1 | 2.50 | 697 | 3 | 0.000 | 0 | 863 |
| Nokia AirScale RRH 4 | 109.00 | 106 | 202 | 0.014 | 12 | 131 |
| Alcatel-Lucent B25 R | 109.00 | 159 | 303 | 0.021 | 17 | 197 |
| Alcatel-Lucent B13 R | 109.00 | 173 | 330 | 0.022 | 19 | 215 |
| Alcatel-Lucent B66A | 109.00 | 201 | 383 | 0026 | 22 | 249 |
| Raycap RC3DC-3315-PF | 109.00 | 32 | 61 | 0.004 | 3 | 40 |
| Antel BXA-70063/6CF | 109.00 | 51 | 97 | 0.007 | 6 | 63 |
| Commscope JAHH-65B-R | 109.00 | 364 | 692 | 0.047 | 39 | 450 |
| Antel LPA-80063/6CF | 109.00 | 162 | 308 | 0.021 | 18 | 201 |
| Round T-Arm | 109.00 | 750 | 1,428 | 0.097 | 81 | 929 |
| Ericsson RRUS 11 B2 | 102.00 | 152 | 260 | 0.018 | 15 | 188 |
| Ericsson AIR 21 B4A | 102.00 | 270 | 462 | 0.031 | 26 | 334 |
| Ericsson AIR 21, 1.3 | 102.00 | 275 | 470 | 0.032 | 27 | 340 |
| Round T-Arm | 102.00 | 750 | 1,283 | 0.087 | 73 | 929 |
| Commscope LNX-6515DS | 102.00 | 151 | 258 | 0.018 | 15 | 187 |
|  |  | 16,257 | 14,708 | 1,000 | 839 | 20,129 |

Load Case (0.9-0.2Sds) " DL + E ELFM
Seismic (Reduced DL) Equivalent Lateral Forces Method
Height

| Above Weight |  |  |
| :---: | :---: | :---: | :---: |
| Base | $W_{2}$ | Horizontal Fertical |

Segment (ft)

| 26 | 107.00 | 263 | 485 | 0.033 | 28 | 226 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 25 | 103.50 | 201 | 352 | 0.024 | 20 | 173 |
| 24 | 101.00 | 270 | 454 | 0.031 | 26 | 233 |
| 23 | 99.25 | 205 | 335 | 0.023 | 19 | 177 |
| 22 | 96.75 | 314 | 494 | 0.034 | 28 | 271 |
| 21 | 92.50 | 461 | 673 | 0.046 | 38 | 397 |
| 20 | 87.50 | 474 | 634 | 0.043 | 36 | 408 |
| 19 | 82.50 | 487 | 593 | 0.040 | 34 | 420 |
| 18 | 77.50 | 501 | 551 | 0.037 | 31 | 432 |
| 17 | 72.50 | 514 | 508 | 0.035 | 29 | 443 |
| 16 | 67.50 | 528 | 465 | 0.032 | 27 | 455 |
| 15 | 62.50 | 541 | 421 | 0.029 | 24 | 467 |
| 14 | 57.50 | 555 | 377 | 0.026 | 22 | 478 |
| 13 | 54.13 | 197 | 122 | 0.008 | 7 | 170 |
| 12 | 51.63 | 655 | 374 | 0.025 | 21 | 564 |
| 11 | 49.25 | 306 | 162 | 0.011 | 9 | 264 |
| 10 | 46.75 | 404 | 197 | 0.013 | 11 | 348 |
| 9 | 42.50 | 589 | 246 | 0.017 | 14 | 507 |
| 8 | 37.50 | 602 | 206 | 0.014 | 12 | 519 |
| 7 | 32.50 | 616 | 167 | 0.011 | 10 | 531 |
| 6 | 27.50 | 629 | 131 | 0.009 | 7 | 542 |
| 5 | 22.50 | 643 | 97 | 0.007 | 6 | 554 |
| 4 | 17.50 | 656 | 66 | 0.004 | 4 | 566 |
| 3 | 12.50 | 670 | 39 | 0.003 | 2 | 577 |
| 2 | 7.50 | 683 | 18 | 0.001 | 1 | 589 |
| 1 | 2.50 | 697 | 3 | 0.000 | 0 | 600 |
| Nokia AirScale RRH 4 | 109.00 | 106 | 202 | 0.014 | 12 | 91 |
| Alcatel-Lucent B25 R | 109.00 | 159 | 303 | 0.021 | 17 | 137 |
| Alcatel-Lucent B13 R | 109.00 | 173 | 330 | 0.022 | 19 | 149 |
| Alcatel-Lucent B66A | 109.00 | 201 | 383 | 0.026 | 22 | 173 |
| Raycap RC3DC-3315-PF | 109.00 | 32 | 61 | 0.004 | 3 | 28 |
| Antel BXA-70063/6CF_ | 109.00 | 51 | 97 | 0.007 | 6 | 44 |
| Commscope JAHH-65B-R | 109.00 | 364 | 692 | 0.047 | 39 | 313 |
| Antel LPA-80063/6CF | 109.00 | 162 | 308 | 0.021 | 18 | 140 |
| Round T-Arm | 109.00 | 750 | 1,428 | 0.097 | 81 | 646 |
| Ericsson RRUS 11 B2 | 102.00 | 152 | 260 | 0.018 | 15 | 131 |
| Ericsson AIR 21 B4A | 102.00 | 270 | 462 | 0.031 | 26 | 233 |


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| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NORTH BLOOMFIELD CT, CT |  | Engineering Number:OAA710465_C3_01 |  |  | 9/11/2017 10:50:47 AM |  |
| Customer: VERIZON W | VERIZON WIRELESS |  |  |  |  |  |
| Ericsson AIR 21, 1.3 | 102.00 | 275 | 470 | 0.032 | 27 | 237 |
| Round T-Arm | 102.00 | 750 | 1.283 | 0.087 | 73 | 646 |
| Commscope LNX-6515DS | 102.00 | 151 | 258 | 0.018 | 15 | 130 |
|  |  | 16,257 | 14,708 | 1.000 | 839 | 14,010 |


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| :--- | :--- | ---: | ---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |
| Customer: | VERIZON WIRELESS |  |  |

Load Case (1.2+0.2Sds) *DL + E ELFM Seismic Equivalent Lateral Forces Method
Calculated Forces

| Seg Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \\ \text { (kips) } \end{gathered}$ | Vu FX(-) (kips) | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MX} \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | phi Pn (kips) | phi Vn (kips) | phi Tn (ft-kips) | $\begin{gathered} \mathrm{phi} \\ \mathrm{Mn} \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -19.27 | -0.84 | 0.00 | -75.95 | 0.00 | 75.95 | 2,055.47 | 1,027.73 | 3,611.06 | 1,808.21 | 0.00 | 0.00 | 0.051 |
| 5.00 | -18.42 | -0.84 | 0.00 | -71.75 | 0.00 | 71.75 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.01 | -0.01 | 0.050 |
| 10.00 | -17.59 | -0.85 | 0.00 | -67.53 | 0.00 | 67.53 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.03 | -0.03 | 0.049 |
| 15.00 | -16.78 | -0.85 | 0.00 | -63.30 | 0.00 | 63.30 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.06 | -0.04 | 0.048 |
| 20.00 | -15.98 | -0.84 | 0.00 | -59.07 | 0.00 | 59.07 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.11 | -0.05 | 0.046 |
| 25.00 | -15.20 | -0.84 | 0.00 | -54.85 | 0.00 | 54.85 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.18 | -0.07 | 0.045 |
| 30.00 | -14.44 | -0.83 | 0.00 | -50.66 | 0.00 | 50.66 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 0.26 | -0.08 | 0.043 |
| 35.00 | -13.69 | -0.82 | 0.00 | -46.50 | 0.00 | 46.50 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 0.35 | -0.10 | 0.041 |
| 40.00 | -12.97 | -0.81 | 0.00 | -42.39 | 0.00 | 42.39 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 0.46 | -0.11 | 0.039 |
| 45.00 | -12.46 | -0.80 | 0.00 | -38.34 | 0.00 | 38.34 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 0.59 | -0.12 | 0.038 |
| 48.50 | - 12.09 | -0.79 | 0.00 | -35.54 | 0.00 | 35.54 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 0.68 | -0.13 | 0.036 |
| 50.00 | -11.27 | -0.77 | 0.00 | -34.36 | 0.00 | 34.36 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 0.72 | -0.14 | 0.035 |
| 53.25 | -11.03 | -0.76 | 0.00 | -31.85 | 0.00 | 31.85 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 0.82 | -0.15 | 0.033 |
| 55.00 | -10.34 | -0.74 | 0.00 | -30.52 | 0.00 | 30.52 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 0.88 | -0.15 | 0.032 |
| 60.00 | -9.67 | -0.72 | 0.00 | -26.81 | 0.00 | 26.81 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 1.04 | -0.16 | 0.030 |
| 65.00 | -9.02 | -0.69 | 0.00 | -23.22 | 0.00 | 23.22 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 1.22 | -0.18 | 0.028 |
| 70.00 | -8.38 | -0.66 | 0.00 | -19.77 | 0.00 | 19.77 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 1.41 | -0.19 | 0.025 |
| 75.00 | -7.76 | -0.63 | 0.00 | -16.46 | 0.00 | 16.46 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 1.61 | -0.20 | 0.023 |
| 80.00 | -7.16 | -0.59 | 0.00 | -13.31 | 0.00 | 13.31 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 1.82 | -0.21 | 0.020 |
| 85.00 | -6.57 | -0.56 | 0.00 | -10.34 | 0.00 | 10.34 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 2.04 | -0.21 | 0.017 |
| 90.00 | -6.00 | -0.52 | 0.00 | -7.56 | 0.00 | 7.56 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 2.27 | -0.22 | 0.014 |
| 95.00 | -5.61 | -0.49 | 0.00 | -4.97 | 0.00 | 4.97 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 2.51 | -0.23 | 0.011 |
| 98.50 | -5.36 | -0.47 | 0.00 | -3.26 | 0.00 | 3.26 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 2.68 | -0.23 | 0.009 |
| 100.00 | -5.02 | -0.44 | 0.00 | -2.56 | 0.00 | 2.56 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 2.75 | -0.23 | 0.008 |
| 102.00 | -2.80 | -0.26 | 0.00 | -1.68 | 0.00 | 1.68 | 959.49 | 479.75 | 914.96 | 458.16 | 2.85 | -0.23 | 0.007 |
| 105.00 | -2.47 | -0.23 | 0.00 | -0.91 | 0.00 | 0.91 | 942.73 | 471.37 | 875.56 | 438.43 | 2.99 | -0.23 | 0.005 |
| 109.00 | 0.00 | -0.22 | 0.00 | 0.00 | 0.00 | 0.00 | 919.72 | 459.86 | 823.73 | 412.48 | 3.19 | -0.23 | 0.000 |


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| :--- | :--- | ---: | ---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |

Customer: VERIZON WIRELESS

| Load Case (0.9-0.2Sds) * DL + E ELFM |  |  |  |  | Seismic (Reduced DL) Equivalent Lateral Forces Method |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Calculated Forces |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Seg <br> Elev <br> (ft) | $\begin{gathered} \mathrm{Pu} \\ \mathrm{FY}(-) \\ \text { (kips) } \end{gathered}$ | $\begin{aligned} & \text { Vu } \\ & \text { FX (-) } \\ & \text { (kips) } \end{aligned}$ | $\begin{gathered} \mathrm{Tu} \\ \mathrm{MY} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MX} \\ \text { (ft-kips) } \end{gathered}$ | Resultant Moment (ft-kips) | $\begin{gathered} \text { phi } \\ \text { Pn } \\ \text { (kips) } \end{gathered}$ | $\begin{aligned} & \text { phi } \\ & \text { Vn } \\ & \text { (kips) } \end{aligned}$ |  |  | Total Deflect (in) | Rotation (deg) | Ratio |
| 0.00 | -13.41 | -0.84 | 0.00 | -75.23 | 0.00 | 75.23 | 2,055.47 | 1,027.73 | 3,611.06 | 808.21 | 0.00 | 0.00 | 0.048 |
| 5.00 | -12.82 | -0.84 | 0.00 | -71.03 | 0.00 | 71.03 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.01 | -0.01 | 0.047 |
| 10.00 | -12.24 | -0.84 | 0.00 | -66.82 | 0.00 | 66.82 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.03 | -0.03 | 0.046 |
| 15.00 | -11.68 | -0.84 | 0.00 | -62.61 | 0.00 | 62.61 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.06 | -0.04 | 0.045 |
| 20.00 | -11.12 | -0.84 | 0.00 | -58.40 | 0.00 | 58.40 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.11 | -0.05 | 0.043 |
| 25.00 | - 10.58 | -0.83 | 0.00 | -54.21 | 0.00 | 54.21 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.18 | -0.07 | 0.042 |
| 30.00 | - 10.05 | -0.82 | 0.00 | -50.05 | 0.00 | 50.05 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 0.26 | -0.08 | 0.040 |
| 35.00 | -9.53 | -0.81 | 0.00 | -45.93 | 0.00 | 45.93 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 0.35 | -0.10 | 0.039 |
| 40.00 | -9.02 | -0.80 | 0.00 | -41.86 | 0.00 | 41.86 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 0.46 | -0.11 | 0.037 |
| 45.00 | -8.68 | -0.79 | 0.00 | -37.85 | 0.00 | 37.85 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 0.58 | -0.12 | 0.035 |
| 48.50 | - 8.41 | -0.78 | 0.00 | -35.08 | 0.00 | 35.08 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 0.67 | -0.13 | 0.034 |
| 50.00 | -7.85 | -0.76 | 0.00 | - 33.90 | 0.00 | 33.90 | 1,767.37 | 883.69 | 2,373.20 | 1.188 .37 | 0.72 | -0.14 | 0.033 |
| 53.25 | -7.68 | -0.75 | 0.00 | -31.43 | 0.00 | 31.43 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 0.81 | -0.15 | 0.031 |
| 55.00 | -7.20 | -0.73 | 0.00 | -30.11 | 0.00 | 30.11 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 0.87 | -0.15 | 0.030 |
| 60.00 | -6.73 | -0.71 | 0.00 | -26.45 | 0.00 | 26.45 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 1.03 | -0.16 | 0.028 |
| 65.00 | -6.28 | -0.68 | 0.00 | -22.91 | 0.00 | 22.91 | 1,676.85 | 838.42 | 2,078.10 | 1.040.59 | 1.21 | -0.17 | 0.026 |
| 70.00 | -5.83 | -0.65 | 0.00 | -19.49 | 0.00 | 19.49 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 1.39 | -0.18 | 0.023 |
| 75.00 | -5.40 | -0.62 | 0.00 | -16.23 | 0.00 | 16.23 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 1.59 | -0.19 | 0.021 |
| 80.00 | -4.98 | -0.59 | 0.00 | -13.13 | 0.00 | 13.13 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 1.80 | -0.20 | 0.018 |
| 85.00 | -4.57 | -0.55 | 0.00 | -10.19 | 0.00 | 10.19 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 2.02 | -0.21 | 0.016 |
| 90.00 | -4.18 | -0.51 | 0.00 | -7.45 | - 0.00 | 7.45 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 2.25 | -0.22 | 0.013 |
| 95.00 | -3.91 | -0.48 | 0.00 | -4.90 | - 0.00 | 4.90 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 2.48 | -0.22 | 0.010 |
| 98.50 | -3.73 | -0.46 | 0.00 | -3.21 | - 0.00 | 3.21 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 2.64 | -0.23 | 0.008 |
| 100.00 | -3.50 | -0.43 | 0.00 | -2.52 | - 0.00 | 2.52 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 2.72 | -0.23 | 0.006 |
| 102.00 | -1.95 | -0.25 | 0.00 | -1.65 | - 0.00 | 1.65 | 959.49 | 479.75 | 914.96 | 458.16 | 2.81 | -0.23 | 0.006 |
| 105.00 | -1.72 | -0.22 | 0.00 | -0.90 | - 0.00 | 0.90 | 942.73 | 471.37 | 875.56 | 438.43 | 2.96 | -0.23 | 0.004 |
| 109.00 | 0.00 | -0.22 | 0.00 | 0.00 | - 0.00 | 0.00 | 919.72 | 459.86 | 823.73 | 412.48 | 3.15 | -0.23 | 0.000 |


| Site Number: 283562 | Code: ANSIITIA-222-G | © 2007-2017 by ATC IP LLLC. All rights reserved. |  |
| :--- | :--- | ---: | ---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |
| Customer: | VERIZON WIRELESS |  |  |

## Equivalent Modal Forces Analysis

(Based on ASCE7-10 Chapters 11, 12 \& 15 and ANSI/TIA-G, section 2.7)

| Spectral Response Acceleration for Short Period (S ${ }_{\mathrm{s}}$ ): | 0.18 |
| :---: | :---: |
| Spectral Response Acceleration at 1.0 Second Period ( $\mathrm{S}_{1}$ ): | 0.06 |
| Importance Factor ( $\mathrm{I}_{\mathrm{E}}$ ): | 1.00 |
| Site Coefficient $\mathrm{F}_{\mathrm{a}}$ : | 1.60 |
| Site Coefficient F v | 2.40 |
| Response Modification Coefficient (R): | 1.50 |
| Design Spectral Response Acceleration at Short Period (S ds): | 0.19 |
| Desing Spectral Response Acceleration at 1.0 Second Period ( $\mathrm{S}_{\mathrm{d} 1}$ ): | 0.10 |
| Period Based on Rayleigh Method (sec): | 1.72 |
| Redundancy Factor (p): | 1.30 |

$\underline{\text { Load Case }} \underline{(1.2+0.2 S d s)}$ * DL + E EMAM Seismic Equivalent Modal Analysis Method

| Segment | Height Above Base <br> (ft) | Weight <br> (Ib) | a | b | c | Saz | Horizontal Force (b) | Vertical Force <br> (Ib) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 107.00 | 263 | 1.821 | 1.637 | 1.014 | 0.329 | 75 | 325 |
| 25 | 103.50 | 201 | 1.704 | 1.138 | 0.821 | 0.260 | 45 | 249 |
| 24 | 101.00 | 270 | 1.623 | 0.851 | 0.701 | 0.215 | 50 | 334 |
| 23 | 99.25 | 205 | 1.567 | 0.680 | 0.626 | 0.187 | 33 | 254 |
| 22 | 96.75 | 314 | 1.489 | 0.474 | 0.530 | 0.149 | 41 | 389 |
| 21 | 92.50 | 461 | 1.361 | 0.214 | 0.393 | 0.095 | 38 | 570 |
| 20 | 87.50 | 474 | 1.218 | 0022 | 0.268 | 0.044 | 18 | 587 |
| 19 | 82.50 | 487 | 1.083 | -0.079 | 0.176 | 0.010 | 4 | 604 |
| 18 | 77.50 | 501 | 0.955 | -0.118 | 0.110 | -0.011 | -5 | 620 |
| 17 | 72.50 | 514 | 0.836 | -0.118 | 0.065 | -0.017 | -8 | 637 |
| 16 | 67.50 | 528 | 0.725 | -0.094 | 0.035 | -0.012 | -6 | 654 |
| 15 | 62.50 | 541 | 0.621 | -0.061 | 0.017 | 0.000 | 0 | 670 |
| 14 | 57.50 | 555 | 0.526 | -0.026 | 0.008 | 0.015 | 7 | 687 |
| 13 | 54.13 | 197 | 0.466 | -0.004 | 0.006 | 0.025 | 4 | 244 |
| 12 | 51.63 | 655 | 0.424 | 0.010 | 0.006 | 0.031 | 17 | 811 |
| 11 | 49.25 | 306 | 0.386 | 0.022 | 0.007 | 0.035 | 9 | 379 |
| 10 | 46.75 | 404 | 0.348 | 0.033 | 0.009 | 0.039 | 14 | 500 |
| 9 | 42.50 | 589 | 0.287 | 0.048 | 0.013 | 0.044 | 22 | 729 |
| 8 | 37.50 | 602 | 0.224 | 0.060 | 0.020 | 0.045 | 24 | 746 |
| 7 | 32.50 | 616 | 0.168 | 0.066 | 0.028 | 0.045 | 24 | 762 |
| 6 | 27.50 | 629 | 0.120 | 0.070 | 0.034 | 0.043 | 23 | 779 |
| 5 | 22.50 | 643 | 0.081 | 0.072 | 0.040 | 0.041 | 23 | 796 |
| 4 | 17.50 | 656 | 0.049 | 0.071 | 0.042 | 0.039 | 22 | 813 |
| 3 | 12.50 | 670 | 0.025 | 0.066 | 0.039 | 0.036 | 21 | 829 |
| 2 | 7.50 | 683 | 0.009 | 0.053 | 0.031 | 0.029 | 17 | 846 |
| 1 | 2.50 | 697 | 0.001 | 0.024 | 0.013 | 0.014 | 8 | 863 |
| Nokia AirScale RRH 4 | 109.00 | 106 | 1.890 | 1.980 | 1.140 | 0.371 | 34 | 131 |
| Alcatel-Lucent B25 R | 109.00 | 159 | 1.890 | 1.980 | 1.140 | 0.371 | 51 | 197 |
| Alcatel-Lucent B13 R | 109.00 | 173 | 1.890 | 1.980 | 1.140 | 0.371 | 56 | 215 |
| Alcatel-Lucent B66A | 109.00 | 201 | 1.890 | 1.980 | 1.140 | 0.371 | 65 | 249 |
| Raycap RC3DC.3315.PF | 109.00 | 32 | 1.890 | 1.980 | 1.140 | 0.371 | 10 | 40 |
| Antel BXA-70063/6CF_ | 109.00 | 51 | 1.890 | 1.980 | 1.140 | 0.371 | 16 | 63 |
| Commscope JAHH-65B- | 109.00 | 364 | 1.890 | 1.980 | 1.140 | 0.371 | 117 | 450 |
| Antel LPA.80063/6CF | 109.00 | 162 | 1.890 | 1.980 | 1.140 | 0.371 | 52 | 201 |

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Site Number: 283562
Code: ANSI/TIA-222-G © 2007 - 2017 by ATC IP LLC. All rights reserved.
Site Name: NORTH BLOOMFIELD CT, CT
Engineering Number:OAA710465_C3_01
9/11/2017 10:50:47 AM
Customer: VERIZON WIRELESS

| Round T-Arm | 109.00 | 750 | 1.890 | 1.980 | 1.140 | 0.371 | 241 | 929 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Ericsson RRUS 11 B2 | 102.00 | 152 | 1.655 | 0.959 | 0.747 | 0.233 | 31 | 188 |
| Ericsson AIR 21 B4A | 102.00 | 270 | 1.655 | 0.959 | 0.747 | 0.233 | 54 | 334 |
| Ericsson AIR 21, 1.3 | 102.00 | 275 | 1.655 | 0.959 | 0.747 | 0.233 | 55 | 340 |
| Round T-Arm | 102.00 | 750 | 1.655 | 0.959 | 0.747 | 0.233 | 151 | 929 |
| Commscope LNX- | 102.00 | 151 | 1.655 | 0.959 | 0.747 | 0.233 | 30 | 187 |
|  |  | 16,257 | 43.402 | 27.729 | 19.050 | 6.234 | 1,488 | 20,129 |

Load Case (0.9-0.2Sds) * DL + E EMAM Seismic (Reduced DL) Equivalent Modal Analysis Method

| Segment | Height Above Base <br> (ft) | Weight <br> (Ib) | a | b | c | Saz | Horizontal Force (b) | Vertical Force (Ib) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 26 | 107.00 | 263 | 1.821 | 1.637 | 1.014 | 0.329 | 75 | 226 |
| 25 | 103.50 | 201 | 1.704 | 1.138 | 0.821 | 0.260 | 45 | 173 |
| 24 | 101.00 | 270 | 1.623 | 0.851 | 0.701 | 0.215 | 50 | 233 |
| 23 | 99.25 | 205 | 1.567 | 0.680 | 0.626 | 0.187 | 33 | 177 |
| 22 | 96.75 | 314 | 1.489 | 0.474 | 0.530 | 0.149 | 41 | 271 |
| 21 | 92.50 | 461 | 1.361 | 0.214 | 0.393 | 0.095 | 38 | 397 |
| 20 | 87.50 | 474 | 1.218 | 0.022 | 0.268 | 0.044 | 18 | 408 |
| 19 | 82.50 | 487 | 1.083 | -0.079 | 0.176 | 0.010 | 4 | 420 |
| 18 | 77.50 | 501 | 0.955 | -0.118 | 0.110 | -0.011 | -5 | 432 |
| 17 | 72.50 | 514 | 0.836 | -0.118 | 0.065 | -0.017 | -8 | 443 |
| 16 | 67.50 | 528 | 0.725 | -0.094 | 0.035 | -0.012 | . 6 | 455 |
| 15 | 62.50 | 541 | 0.621 | -0.061 | 0.017 | 0.000 | 0 | 467 |
| 14 | 57.50 | 555 | 0.526 | -0.026 | 0.008 | 0.015 | 7 | 478 |
| 13 | 54.13 | 197 | 0.466 | -0.004 | 0.006 | 0.025 | 4 | 170 |
| 12 | 51.63 | 655 | 0.424 | 0.010 | 0.006 | 0.031 | 17 | 564 |
| 11 | 49.25 | 306 | 0.386 | 0.022 | 0.007 | 0.035 | 9 | 264 |
| 10 | 46.75 | 404 | 0.348 | 0.033 | 0.009 | 0.039 | 14 | 348 |
| 9 | 42.50 | 589 | 0.287 | 0.048 | 0.013 | 0.044 | 22 | 507 |
| 8 | 37.50 | 602 | 0.224 | 0.060 | 0020 | 0.045 | 24 | 519 |
| 7 | 32.50 | 616 | 0.168 | 0.066 | 0.028 | 0.045 | 24 | 531 |
| 6 | 27.50 | 629 | 0.120 | 0.070 | 0.034 | 0.043 | 23 | 542 |
| 5 | 22.50 | 643 | 0.081 | 0.072 | 0.040 | 0.041 | 23 | 554 |
| 4 | 17.50 | 656 | 0.049 | 0.071 | 0.042 | 0.039 | 22 | 566 |
| 3 | 12.50 | 670 | 0.025 | 0.066 | 0.039 | 0.036 | 21 | 577 |
| 2 | 7.50 | 683 | 0.009 | 0.053 | 0.031 | 0.029 | 17 | 589 |
| 1 | 2.50 | 697 | 0.001 | 0.024 | 0.013 | 0.014 | 8 | 600 |
| Nokia AirScale RRH 4 | 109.00 | 106 | 1.890 | 1.980 | 1.140 | 0.371 | 34 | 91 |
| Alcatel-Lucent B25 R | 109.00 | 159 | 1.890 | 1.980 | 1.140 | 0.371 | 51 | 137 |
| Alcatel-Lucent B13 R | 109.00 | 173 | 1.890 | 1.980 | 1.140 | 0.371 | 56 | 149 |
| Alcatel-Lucent B66A | 109.00 | 201 | 1.890 | 1.980 | 1.140 | 0.371 | 65 | 173 |
| Raycap RC3DC-3315-PF | 109.00 | 32 | 1,890 | 1.980 | 1.140 | 0.371 | 10 | 28 |
| Antel BXA-70063/6CF. | 109.00 | 51 | 1.890 | 1.980 | 1.140 | 0.371 | 16 | 44 |
| Commscope JAHH-65B- | 109.00 | 364 | 1.890 | 1.980 | 1.140 | 0.371 | 117 | 313 |
| Antel LPA-80063/6CF | 109.00 | 162 | 1.890 | 1.980 | 1.140 | 0.371 | 52 | 140 |
| Round T-Arm | 109.00 | 750 | 1.890 | 1.980 | 1.140 | 0.371 | 241 | 646 |
| Ericsson RRUS 11 B2 | 102.00 | 152 | 1.655 | 0.959 | 0.747 | 0.233 | 31 | 131 |
| Ericsson AIR 21 B4A | 102.00 | 270 | 1.655 | 0.959 | 0.747 | 0.233 | 54 | 233 |
| Ericsson AIR 21, 1.3 | 102.00 | 275 | 1.655 | 0.959 | 0.747 | 0.233 | 55 | 237 |
| Round T-Arm | 102.00 | 750 | 1.655 | 0.959 | 0.747 | 0.233 | 151 | 646 |
| Commscope LNX- | 102.00 | 151 | 1.655 | 0.959 | 0.747 | 0.233 | 30 | 130 |
|  |  | 16,257 | 43.402 | 27.729 | 19.050 | 6.234 | 1.488 | 14.010 |


| Site Number: 283562 | Code: ANSI/TIA-222-G | o 2007 - 2017 by ATC IP LLC. All rights reserved. |  |
| :--- | :--- | ---: | ---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |
| Customer: | VERIZON WIRELESS |  |  |

Load Case (1.2+0.2Sds) * DL + E EMAM Seismic Equivalent Modal Analysis Method Calculated Forces

| Seg <br> Elev <br> (ft) | $\begin{aligned} & \text { Pu } \\ & \text { FY (-) } \\ & \text { (kips) } \end{aligned}$ | Vu FX (-) (kips) |  | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | Mu MX (ft-kips) | Resultant Moment (ft-kips) | phi <br> Pn <br> (kips) | phi Vn (kips) | $\begin{gathered} \text { phi } \\ \text { Tn } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \text { phi } \\ \text { Mn } \\ \text { (ft-kips) } \end{gathered}$ | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -19.27 | -1.48 | 0.00 | -142.82 | 0.00 | 142.82 | 2,055 | , 027.73 | 3,611 | 1,808.21 | 0.00 | 0.00 | 0.088 |
| 5.00 | -18.42 | -1.47 | 0.00 | -135.40 | 0.00 | 135.40 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.01 | -0.03 | 0.087 |
| 10.00 | - 17.59 | -1.46 | 0.00 | -128.04 | 0.00 | 128.04 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.05 | -0.05 | 0.085 |
| 15.00 | -16.78 | -1.45 | 0.00 | -120.73 | 0.00 | 120.73 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.12 | -0.08 | 0.083 |
| 20.00 | -15.98 | -1.43 | 0.00 | -113.51 | 0.00 | 113.51 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.22 | -0.10 | 0.081 |
| 25.00 | -15.20 | -1.41 | 0.00 | -106.36 | 0.00 | 106.36 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.34 | -0.13 | 0.079 |
| 30.00 | -14.44 | -1.39 | 0.00 | -99.31 | 0.00 | 99.31 | 1,896.82 | 948.41 | 2,861.15 | 1.432 .70 | 0.49 | -0.16 | 0.077 |
| 35.00 | -13.69 | -1.37 | 0.00 | -92.35 | 0.00 | 92.35 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 0.67 | -0.19 | 0.075 |
| 40.00 | -12.96 | -1.35 | 0.00 | -85.48 | 0.00 | 85.48 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 0.88 | -0.21 | 0.072 |
| 45.00 | - 12.46 | -1.34 | 0.00 | -78.71 | 0.00 | 78.71 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 1.12 | -0.24 | 0.070 |
| 48.50 | - 12.08 | -1.34 | 0.00 | . 74.01 | 0.00 | 74.01 | 1.777.74 | 888.87 | 2,409.20 | 1,206.39 | 1.31 | -0.26 | 0.068 |
| 50.00 | -11.27 | -1.32 | 0.00 | . 72.00 | 0.00 | 72.00 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 1.39 | -0.27 | 0.067 |
| 53.25 | -11.03 | -1.31 | 0.00 | -67.72 | 0.00 | 67.72 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 1.58 | -0.29 | 0.064 |
| 55.00 | -10.34 | -1.31 | 0.00 | -65.42 | 0.00 | 65.42 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 1.69 | -0.30 | 0.062 |
| 60.00 | -9.67 | -1.31 | 0.00 | -58.89 | 0.00 | 58.89 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 2.02 | -0.33 | 0.059 |
| 65.00 | -9.01 | -1.31 | 0.00 | -52.35 | 0.00 | 52.35 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 2.37 | -0.35 | 0.056 |
| 70.00 | -8.38 | -1.32 | 0.00 | -45.78 | 0.00 | 45.78 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 2.75 | -0.38 | 0.052 |
| 75.00 | -7.75 | -1.32 | 0.00 | -39.17 | 0.00 | 39.17 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 3.16 | -0.40 | 0.047 |
| 80.00 | -7.15 | -1.32 | 0.00 | -32.55 | 0.00 | 32.55 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 3.59 | -0.42 | 0.042 |
| 85.00 | -6.56 | -1.30 | 0.00 | -25.95 | 0.00 | 25.95 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 4.05 | -0.44 | 0.036 |
| 90.00 | -5.99 | -1.26 | 0.00 | -19.46 | 0.00 | 19.46 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 4.52 | -0.46 | 0.030 |
| 95.00 | -5.60 | -1.22 | 0.00 | -13.16 | 0.00 | 13.16 | 1.425.10 | 712.55 | 1,412.12 | 707.11 | 5.01 | -0.48 | 0.023 |
| 98.50 | -5.35 | -1.18 | 0.00 | -8.91 | 0.00 | 8.91 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 5.37 | -0.48 | 0.017 |
| 100.00 | -5.02 | -1.13 | 0.00 | -7.14 | 0.00 | 7.14 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 5.52 | -0.49 | 0.015 |
| 102.00 | -2.79 | -0.74 | 0.00 | -4.88 | 0.00 | 4.88 | 959.49 | 479.75 | 914.96 | 458.16 | 5.73 | -0.49 | 0.014 |
| 105.00 | -2.47 | -0.66 | 0.00 | -2.66 | 0.00 | 2.66 | 942.73 | 471.37 | 875.56 | 438.43 | 6.03 | -0.49 | 0.009 |
| 109.00 | 0.00 | -0.64 | 0.00 | 0.00 | 0.00 | 0.00 | 919.72 | 459.86 | 823.73 | 412.48 | 6.45 | -0.49 | 0.000 |


| Site Number: 283562 | Code: ANSI/TIA-222-G | $\circ 2007 \cdot 2017$ by ATC IP LLC. All rights reserved. |  |
| :--- | :--- | ---: | :--- |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |

Customer: VERIZON WIRELESS

Load Case (0.9-0.2Sds) * DL + E EMAM Seismic (Reduced DL) Equivalent Modal Analysis Method
Calculated Forces

| Seg <br> Elev <br> (ft) | $\begin{aligned} & \text { Pu } \\ & \text { FY (-) } \\ & \text { (kips) } \end{aligned}$ | Vu FX (-) (kips) | $\begin{gathered} \text { Tu } \\ \text { MY } \\ \text { (ft-kips) } \end{gathered}$ | $\begin{gathered} \mathrm{Mu} \\ \mathrm{MZ} \\ \text { (ft-kips) } \end{gathered}$ | $M \mathrm{Mu}$ MX (ft-kips) | Resultant Moment (ft-kips) | phi <br> Pn <br> (kips) | $\begin{gathered} \text { phi } \\ \text { Vn } \\ \text { (kips) } \end{gathered}$ | $\begin{gathered} \mathrm{phi} \\ \mathrm{Tn} \\ \text { (ft-kips) } \end{gathered}$ | phi Mn (ft-kips) | Total Deflect (in) | Rotation (deg) | Ratio |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.00 | -13.41 | -1.48 | 0.00 | -141.38 | 0.00 | 141.38 | 2,055.47 | 1,027.73 | 3.611 .06 | 1,808.21 | 0.00 | 0.00 | 0.085 |
| 5.00 | -12.82 | -1.47 | 0.00 | -133.98 | 0.00 | 133.98 | 2,031.99 | 1,015.99 | 3,485.68 | 1,745.43 | 0.01 | -0.03 | 0.083 |
| 10.00 | -12.24 | -1.45 | 0.00 | -126.63 | 0.00 | 126.63 | 2,007.32 | 1,003.66 | 3,360.26 | 1,682.63 | 0.05 | -0.05 | 0.081 |
| 15.00 | -11.68 | -1.44 | 0.00 | -119.35 | 0.00 | 119.35 | 1,981.47 | 990.74 | 3,234.95 | 1,619.88 | 0.12 | -0.08 | 0.080 |
| 20.00 | -11.12 | -1.42 | 0.00 | -112.17 | 0.00 | 112.17 | 1,954.44 | 977.22 | 3,109.90 | 1,557.26 | 0.21 | -0.10 | 0.078 |
| 25.00 | -10.58 | -1.40 | 0.00 | -105.07 | 0.00 | 105.07 | 1,926.22 | 963.11 | 2,985.25 | 1,494.84 | 0.34 | -0.13 | 0.076 |
| 30.00 | -10.05 | -1.38 | 0.00 | -98.08 | 0.00 | 98.08 | 1,896.82 | 948.41 | 2,861.15 | 1,432.70 | 0.49 | -0.16 | 0.074 |
| 35.00 | -9.53 | -1.36 | 0.00 | -91.19 | 0.00 | 91.19 | 1,866.23 | 933.12 | 2,737.75 | 1,370.91 | 0.67 | -0.18 | 0.072 |
| 40.00 | -9.02 | -1.34 | 0.00 | -84.40 | 0.00 | 84.40 | 1,834.46 | 917.23 | 2,615.19 | 1,309.54 | 0.87 | -0.21 | 0.069 |
| 45.00 | -8.67 | -1.33 | 0.00 | -77.71 | 0.00 | 77.71 | 1,801.51 | 900.75 | 2,493.63 | 1,248.67 | 1.11 | -0.24 | 0.067 |
| 48.50 | -8.41 | -1.32 | 0.00 | . 73.06 | 0.00 | 73.06 | 1,777.74 | 888.87 | 2,409.20 | 1,206.39 | 1.29 | -0.26 | 0.065 |
| 50.00 | -7.84 | -1.30 | 0.00 | -71.08 | 0.00 | 71.08 | 1,767.37 | 883.69 | 2,373.20 | 1,188.37 | 1.37 | -0.27 | 0.064 |
| 53.25 | -7.67 | -1.30 | 0.00 | -66.86 | 0.00 | 66.86 | 1,762.15 | 881.08 | 2,355.26 | 1,179.38 | 1.56 | -0.29 | 0.061 |
| 55.00 | -7.19 | -1.29 | 0.00 | -64.59 | 0.00 | 64.59 | 1,749.86 | 874.93 | 2,313.48 | 1,158.46 | 1.67 | -0.30 | 0.060 |
| 60.00 | -6.73 | -1.29 | 0.00 | -58.14 | 0.00 | 58.14 | 1,713.95 | 856.97 | 2,195.04 | 1,099.15 | 1.99 | -0.32 | 0.057 |
| 65.00 | -6.27 | -1.30 | 0.00 | -51.69 | 0.00 | 51.69 | 1,676.85 | 838.42 | 2,078.10 | 1,040.59 | 2.34 | -0.35 | 0.053 |
| 70.00 | -5.83 | -1.30 | 0.00 | -45.21 | 0.00 | 45.21 | 1,638.56 | 819.28 | 1,962.82 | 982.87 | 2.72 | -0.37 | 0.050 |
| 75.00 | -5.39 | -1.31 | 0.00 | -38.69 | 0.00 | 38.69 | 1,599.10 | 799.55 | 1,849.34 | 926.04 | 3.12 | -0.40 | 0.045 |
| 80.00 | -4.97 | -1.30 | 0.00 | -32.15 | 0.00 | 32.15 | 1,558.44 | 779.22 | 1,737.80 | 870.19 | 3.55 | -0.42 | 0.040 |
| 85.00 | -4.57 | -1.28 | 0.00 | -25.64 | 0.00 | 25.64 | 1,516.61 | 758.30 | 1,628.36 | 815.39 | 4.00 | -0.44 | 0.034 |
| 90.00 | . 4.17 | -1.24 | 0.00 | -19.23 | 0.00 | 19.23 | 1,473.59 | 736.79 | 1,521.17 | 761.71 | 4.47 | -0.46 | 0.028 |
| 95.00 | -3.90 | -1.20 | 0.00 | -13.02 | 0.00 | 13.02 | 1,425.10 | 712.55 | 1,412.12 | 707.11 | 4.96 | -0.47 | 0.021 |
| 98.50 | -3.72 | -1.17 | 0.00 | -8.81 | 0.00 | 8.81 | 1,383.85 | 691.92 | 1,331.13 | 666.56 | 5.30 | -0.48 | 0.016 |
| 100.00 | -3.49 | -1.11 | 0.00 | -7.06 | 0.00 | 7.06 | 1,366.16 | 683.08 | 1,297.16 | 649.54 | 5.45 | -0.48 | 0.013 |
| 102.00 | -1.94 | -0.73 | 0.00 | -4.83 | 0.00 | 4.83 | 959.49 | 479.75 | 914.96 | 458.16 | 5.66 | -0.48 | 0.013 |
| 105.00 | -1.72 | -0.66 | 0.00 | -2.63 | 0.00 | 2.63 | 942.73 | 471.37 | 875.56 | 438.43 | 5.96 | -0.49 | 0.008 |
| 109.00 | 0.00 | -0.64 | 0.00 | 0.00 | 0.00 | 0.00 | 919.72 | 459.86 | 823.73 | 412.48 | 6.37 | -0.49 | 0.000 |


| Site Number: 283562 | Code: ANSI/TIA-222-G | 0 2007-2017 by ATC IP LLC. All rights reserved. |  |
| :--- | :--- | ---: | ---: |
| Site Name: | NORTH BLOOMFIELD CT, CT | Engineering Number:OAA710465_C3_01 | $9 / 11 / 2017$ 10:50:47 AM |
| Customer: | VERIZON WIRELESS |  |  |

## Analysis Summary

| Load Case | Reactions |  |  |  |  |  | Max Usage |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Shear FX (kips) | $\begin{aligned} & \text { Shear } \\ & \text { FZ } \\ & \text { (kips) } \end{aligned}$ | Axial FY (kips) | Moment MX <br> (ft-kips) | Mornent MY (ft-kips) | Moment MZ <br> (ft-kips) |  | nteraction Ratio |
| $1.2 \mathrm{D}+1.6 \mathrm{~W}$ | 12.87 | 0.00 | 19.49 | 0.00 | 0.00 | 1081.21 | 0.00 | 0.61 |
| $0.9 \mathrm{D}+1.6 \mathrm{~W}$ | 12.86 | 0.00 | 14.61 | 0.00 | 0.00 | 1072.41 | 0.00 | 0.60 |
| $1.2 \mathrm{D}+1.0 \mathrm{Di}+1.0 \mathrm{Wi}$ | 3.76 | 0.00 | 37.86 | 0.00 | 0.00 | 311.30 | 0.00 | 0.19 |
| (1.2 + 0.2Sds) * DL + E ELFM | 0.84 | 0.00 | 19.27 | 0.00 | 0.00 | 75.95 | 0.00 | 0.05 |
| $(1.2+0.2 S d s) *$ DL + E EMAM | 1.48 | 0.00 | 19.27 | 0.00 | 0.00 | 142.82 | 0.00 | 0.09 |
| (0.9-0.2Sds) * DL + E ELFM | 0.84 | 0.00 | 13.41 | 0.00 | 0.00 | 75.23 | 0.00 | 0.05 |
| (0.9-0.2Sds) * DL + E EMAM | 1.48 | 0.00 | 13.41 | 0.00 | 0.00 | 141.38 | 0.00 | 0.08 |
| $1.0 \mathrm{D}+1.0 \mathrm{~W}$ | 3.08 | 0.00 | 16.26 | 0.00 | 0.00 | 257.28 | 0.00 | 0.15 |

Site Name:
Job Number:
Engineer:
Date:

North Bloomfield CT, CT
OAA710465
Warren.Atkinson
9/11/2017

## Base Plate and Bolt Analysis

Moment:
Shear/Leg:
Compression/Leg:
1081.2 k-ft
12.9 k
19.5 k

TIA-222 Code Revision (F/G):
Anchor Bolt Arrangement:
Monopole Shaft Diameter (Across Flats):
Lower Monopole Thickness:
\# of Sides of Pole:
Monopole Shaft Yield Strength:
Baseplate Diameter / Length:
Base Plate Thickness:
Base Plate Yield Strength:
Baseplate Detail Type:
Include Plate Thickness Beyond Bolt Circle:
Stress Increase:
Fillet Weld Size:
Weld Type (CJP or F/F):
Weld Strength:

|  |
| :---: |
|  |  |
|  |
| 0.250 |
| 18 |
| 65 |
| 46.75 |
| 2.00 |
| 50 |
| D |
| Y |
| 1.00 |
| 0.313 |
| CJP |
| 70 |

## Anchor Bolts

Anchor Bolt Yield Strength: 75 ksi
Anchor Bolt Ultimate Strength: 100 ksi
Anchor Bolt Diameter: 2.25 in
Anchor Bolt Circle: $\quad 48.75$ in
\# of Anchor Bolts:
Minimum Anchor Bolt Separation:
Additional Anchor Bolts Installed:
N

|  | Baseplate Flexural Capacity |  |  |  |  | Baseplate Shear Capacity |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Failure Mode: | Effective Width (in) | Moment <br> (k-in) | $\begin{gathered} S / Z \\ \left(\text { in }^{\circ}\right) \end{gathered}$ | Capacity (k-in) | Usage | Shear <br> (k) | Area <br> (in ${ }^{\text {c }}$ ) | Capacity (k) | Usage |
| AA | 25.84 | 644.9 | 25.8 | 1163.0 | 0.55 | 268.8 | 51.7 | 1395.6 | 0.19 |
| BA | 27.12 | 733.9 | 27.1 | 1220.3 | 0.60 | 268.8 | 54.2 | 1464.4 | 0.18 |

Anchor Bolt Capacity

| Area of Bolt: | $3.25 \mathrm{in}^{2}$ |
| :--- | ---: |
| Inertia of Bolt: | $0.84 \mathrm{in}^{4}$ |
| Total Bolt Inertia: | $7725.0 \mathrm{in}^{4}$ |
| Maximum Bolt Tension: | 130.5 k |
| Maximum Bolt Compression: | 135.4 k |
| Bolt Shear: | 1.6 k |
| Tensile Bolt Capacity: | 259.8 k |
| Compressive Bolt Capacity: | 259.8 k |
| Shear Bolt Capacity: | 140.3 k |
| Interaction Equation: | 0.54 Result: |
|  | OK |

Base Weld Capacity

Force / Weld:
Weld Capacity:
Interaction Equation:
$7.1 \mathrm{k} / \mathrm{in}$
$19.8 \mathrm{k} / \mathrm{in}$
0.36 Result:

OK

Site Name: $\quad$ North Bloomfield, CT
Cumulative Power Density

| Operator | Operating Frequency | Number of Trans. | ERP Per Trans. | Total ERP | Distance to Target | Calculated Power Density | Maximum Permissable Exposure* | Fraction of MPE |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (MHz) |  | (watts) | (watts) | (feet) | (mW/cm $\left.{ }^{\wedge} 2\right)$ | (mW/cm $\left.{ }^{\wedge} 2\right)$ | (\%) |
| VZWPCS | 1970 | 1 | 5000 | 5000 | 110 | 0.1486 | 1.0 | 14.86\% |
| VZW Cellular LTE | 869 | 1 | 3050 | 3050 | 110 | 0.0906 | 0.579333333 | 15.65\% |
| VZW Cellular | 869 | 3 | 389 | 1167 | 110 | 0.0347 | 0.579333333 | 5.99\% |
| VZW AWS | 2145 | 1 | 7400 | 7400 | 110 | 0.2199 | 1.0 | 21.99\% |
| VZW700 | 746 | 1 | 2200 | 2200 | 110 | 0.0654 | 0.497333333 | 13.15\% |

*Guidelines adopted by the FCC on August 1, 1996, 47 CFR Section 1.13101 based on NCRP Report 86,1986 and generally on ANSI/IEEE C95.1-1992
$\mathrm{MHz}=$ Megahertz
$\mathrm{mW} / \mathrm{cm}^{\wedge} 2=$ milliwatts per square centimeter
ERP = Effective Radiated Power
Absolute worst case maximum values used, including the following assumptions:

1. closest accessible point is distance from antenna to base of pole;
2. continuous transmission from all available channels at full power for indefinite time period; and,
3. all RF energy is assumed to be directed solely to the base of the pole.

## Town of Bloomfield

Geographic Information System (GIS)


Date Printed: 12/5/2017


## MAP DISCLAIMER - NOTICE OF LIABILITY

This map is for assessment purposes only. It is not for legal description or conveyances. All information is subject to verification by any user. The Town of Bloomfield and its mapping contractors assume no legal responsibility for the information contained herein.

Approximate Scale: 1 inch $=150$ feet



Town of Bloomfield, CT

## Property Information

| Property Location | 2627 DAY HILL RD |
| :--- | :--- |
| Owner | RIVER BEND DEVELOPMENT CT LLC |
| Co-Owner | \% GRIFFIN INDUSTRIAL REALTY INC |
| Mailing Address | 204 WEST NEWBERRY ROAD <br> BLOOMFIELD $\quad$ CT $\quad 06002$ |
| Land Use | 717 |
| Land Class | Soodland |
| Zoning Code | R-40 |
| Census Tract |  |
| Sub Lot |  |
| Neighborhood | 11.8 |
| Acreage |  |
| Utilities |  |
| Lot Setting/Desc |  |
| Survey Map |  |
| Foundation |  |

## Photo

## No Photo Available

## Sketch

## Primary Construction Details

| Year Built |  |
| :--- | :--- |
| Stories |  |
| Building Style |  |
| Building Use |  |
| Building Condition |  |
| Floors |  |
| Total Rooms |  |


| Bedrooms |  |
| :--- | :--- |
| Full Bathrooms |  |
| Half Bathrooms |  |
| Bath Style |  |
| Kitchen Style |  |
| Roof Style |  |
| Roof Cover |  |


| Exterior Walls |  |
| :--- | :--- |
| Interior Walls |  |
| Heating Type |  |
| Heating Fuel |  |
| AC Type |  |
| Gross Bldg Area |  |
| Total Living Area |  |

Town of Bloomfield, CT

| Valuation Summary $\quad$ (Assessed value $=70 \%$ of Appraised Value) |
| :--- |
| Item |
| Appraised |
| Buildings |
| Extras |
| Outbuildings |
| Land |
| Total |

Sub Areas

| Subarea Type | Gross Area (sq ft) | Living Area (sq ft) |
| :--- | :--- | :--- |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  |  |
|  |  | 0 |
| Total Area |  |  |

Outbuilding and Extra Items

| Type | Description |
| :--- | :--- |
| Barn | 4392 S.F. |
| Shed | 2900 S.F. |
| Shed | 1600 S.F. |
|  |  |
|  |  |
|  |  |

## Sales History

| Owner of Record | Book/ Page | Sale Date | Sale Price |
| :--- | :---: | :---: | :---: |
| RIVER BEND DEVELOPMENT CT LLC | $1737 / 22$ | $7 / 12 / 2013$ |  |
| RIVER BEND ASSOCIATES INC | $737 / 25$ |  | 0 |



VICINITY MAP


AMERICAN TOWER ${ }^{\text {® }}$
ATC SITE NAME: NORTH BLOOMFIELD CT ATC SITE NUMBER: 283562
VERIZON SITE NAME: NORTH BLOOMFIELD CT
SITE ADDRESS: DAY HILL ROAD
BLOOMFIELD, CT 06002

## VERIZON WIRELESS

ANTENNA AMENDMENT DRAWINGS

| COMPLIANCE CODE | PROJECT SUMMARY | PROJECT DESCRIPTION | SHEET INDEX |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | SITE ADDRESS: | THE PROPOSED PROJECT INCLUDES MODIFYING GROUND BASED AND TOWER MOUNTED EQUIPMENT AS INDICATED PER BELOW: <br> REMOVE (6) PANELS, AND (3) RRUs <br> INSTALL (6) NEW PANELS, (12) RRUs, (1) 1-1/4" HYBRID CABLES AND (1) OVPs <br> EXISTING (6) PANELS, (22) 1-5/8" COAX CABLES, (1) 1-1/4" HYBRID CABLES TO REMAIN | $\begin{aligned} & \text { SHEET } \\ & \text { NO: } \end{aligned}$ | DESCRIPTION: | REV: | DATE: | ${ }^{\text {BY: }}$ |
| FOLLOMNG CODES AS ADOPTED BY THE LOCAL GOVERNMENT AUTHORITIES. NOTHING $\operatorname{liN}$ THESE PLANS IS | DAY HILL ROAD |  | G-001 | cover sheet | 0 | 10/1917 | кL |
| TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE COESS. | COUNTY: HARTFORD |  | G-002 | general notes | 0 | 10191917 | kL |
|  | EOGRAPHIC COORDINATES: |  | C-101 | detalled site plan and tower elevation | 0 | 10/1917 | kL |
| 1. INTERNATIONAL BUILIING CODE (IBC) | LATTUDE: 41.87650 LONGITUDE:-72.74183 GROUND ELEVATION: 207' AMsL |  | C.501 | rf Schedule and antenna installation | 0 | 10/1917 | кL |
| 2. NATIONAL ELECTRIC CODE (NEC) |  |  | C. 502 | COnstruction detalls | 0 | 101/9177 | kL |
| 3. Local bulling code |  | PROJECT NOTES |  |  |  |  |  |
| 4. CITY'COUNTY ORDINANCES |  | 1. THE FACILITY IS UNMANNED <br> 2. A TECHNICIAN WILL VIIIT THE SITE APPROXIMATELY ONCE A MONTH FOR ROUTINE INSPECTION AND MAINTENANCE. <br> 3. THE PROJECT WILL NOT RESULT IN ANY SIGNFICANT LAND DISTURBANCE OR EFFECT OF STORM WATER DRAINAGE. |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| UTILITY COMPANIES | PROJECT TEAM | 4. NO SANITARY SEWER, POTABLE WATER OR TRASH DISPOSAL IS REQUIRED. |  |  |  |  |  |
| POWER COMPANY: CONNECTICUT LIGHT \& POWER PHONE: (888) 783-6617 | TOWER OUNER: AMERICAN TOWER 10 PRESIDENTIAL WAY Woburn, MA 01801 | 5. HANIICAP ACCESS IS Not required. |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
| TELEPHONE COMPANY: FRONTIER COMMUNICATIONS PHONE: (800) 921-8102 | ENGINEER: <br> ATC TOWER SERVICES, LLC 3500 REGENCY PKWY STE 100 CARY, NC 27518 |  |  |  |  |  |  |
|  |  | PROJECT LOCATION DIRECTIONS |  |  |  |  |  |
|  |  | FROM HARTFORD, CT: <br> TAKE I-91 NORTH TOWARD SPRINGFIELD MA TAKE EXIT 36 CT-178 TOWARD BLOOMFIELD. TURN LEFT ONTO CT-178. TURN RIGHT ONTO BLUE HILLS AVE CT-187. TURN LEFT ONT DAY HILL ROAD. SITE IS ON LEFT JUST PAST RR TRACKS |  |  |  |  |  |
| Know what's below. <br> Call before you dig. | PROPERTY OUNER: |  |  |  |  |  |  |
|  | RIVER BEND ASSOCIATED, INC 204 WEST NEWBERRY ROAD BLOOMFIELD, CT 06002 <br> APPLICANT: <br> VERIZON WIRELESS <br> 99 EAST RIVER DRIVE, 9TH FLOOR EAST HARTFORD, CT 06108 |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |



NORTH BLOOMFIELD CT


Oct 202017 9:29 AM cesien

| DRAWN BY: |  |  |
| :---: | :---: | :---: |
| APPROVED BY: | KRF |  |
| DATE DRAWN: | 10/1917 |  |
| ATC Job no: | 12157423 |  |
| CUSTOMERID: | NORTH BLOOMFIELD CT |  |
| COVER SHEET |  |  |
|  | $-001$ | $\begin{array}{\|c} \hline \text { ReVIIION: } \\ 0 \end{array}$ |

GENERAL CONSTRUCTION NOTES
ALL WORK SHALL CONFORM TO ALL OURERN APPLICABLE EEDERAL. STATE, AND LOCAL CODES
NCLUDING ANSIEATIA-222, AND COMPLY WTH ATC MASTER SPECIFICATINS
CONTRACTOR SHALL CONTACT LOCAL 811 FOR IDENTIFICATION OF UNDER GROUND UTILTIES
3. Contractor shall be responsible for coordinating all reaured inspections
 REPORTED TO THE ENGINEER
DO Not Change size or spacing of structural elements.
6. DETALIL SHOWN ARE TYPICAL; SIMLAR DETALLS APPLY TO SIMLAR CONDITIONS UNLESS
OTHRWIIE NOTEE.

THESE DRAMNGS DO NOT INCLUDE NECESSARY COMPPNENTS SOR CONSTRUCTION SAFETY
WHICH SHALL BE THE SOLE RESPONSIBLITY OF THE CONTRACTOR
 BOLTS. ETC
9. CONTRACTOR SHALL DETERMINE EXACT LOCATION OF EIISTING UTILTIES, GROUNDS DRAINS,
DRAIN PIPES. VENTS. ETC. BEFORE COMMENNING WORK.
0. INCORRECTLL FABRICATED. DAMAGED. OR OTHERMISE MISEITTNG OR NONCONFORMING


1. EACH CONTRACTOR SHALL COOPERATE WTH THE VERIZON WIRELESS REP. AND COORDINATE
HIS WORK WTH THE WORK OF OTHERS.
2. CONTRACTOR SHALL REPAR ANY DAMAGE CAUSED BY CONSTRUCTION OF THIS PROUECT TO
MATCH EXISTNG PRE-CONSTRUCTON CONITIONS TO THE SATISACCTION OF THE VERIZON MATCH EXISTING PRE-CONSTRUCTIO
WIRELESS CONSTRUCTION MANAGE
3. ALL CABEEICONDUIT ENTRYEXIT PORTS SHALL BE WEATHERPROOFED DURING INSTALLATION
USING A SILCONE SEALANT.
4. WHERE EXISTING CONDITIONSD NOT MATCH THOSE SH
5. CONTRACTOR SHALL ENSURE ALL SUBCONTPACTORS ARE PROYDEDOT

位
6. Contractor shall remove all rubbish and debris from the siteat the end ofena
7. CONTRACTOR SHALL COORDINATE WORK SCHEDULE MTH LANDLORD AND TAKE PRECAUTIONS
TO MINIIZE MPACT AND DISRUPTION OF OTHER OCCUPANTS OF THE FACLITY.
18. CONTRACTOR SHALL FURNISH VERIZON MIRELESS WTH A PDF MARKED UP AS-BULTT SET OF
DRAMNGS UPON COMPLETION OF WORK.
19. PRIIR TO SUBMISSION OF BID, CONTRACTOR SHALL COORDINATE WTH VERRZON WIRELESSRER
 PROVIDED.
20. PRIOR TO SUBMISSION OF BID. CONTRACTOR SHALL COORDINATE MTH VERIZON WIRELESSREP
TO DETERMINEIF ANY PERMITS WILEE OBAINED BY CONTRACTOR. ALL REQUIRED PERMITS Not obtained by verizon mrelless must be obtaning. AND Paid for. By The

CONTRACTOR SHALL INSTAL ALL SITE SIGNAGE IN ACCORDANCE WITH VERIZON MRELESS
SPECIFICATIONS AND REQUREMENTS.
22. CONTRACTOR SHALL SUEMIT ALL SHOP DRAMINGS TO VERIZON MRELESS FOR REVEW AND
APPROVAL PRIOR TO FABRICATION.
23. ALL EQUIPMENT SHAL BE ISTALLED ACCORDING TO MANUFACTURER'S SPECIFICATIONS AND
LOCATED ACCORDING TO VERIZON WRELESS SPELFICATIONS, AND AS SHOW IN THESE PLANS.
24. THE CONTRACTOR SHALL SUPERVISE AND DRECT THE PROUECT DESCRIBED HEREIN. THE TECHNIOUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE TECHNIGUES, SEQUENCESAND
WORK UNDER THE CONTRACT.
25. CONTRACTOR SHALL NOTIFY YERIZON WIRELESS REP AMNMUM OF 48 HOURS IN ADVANCE OF POERING CONCRETL OR EACKILILING ANY UDEERGROUND UTLITES, FOUNDATINS OR SEALING AN
APPROVAL.
26. CONTRACTOR SHALL BE RESPONSIBLE FOR STIE SAFETY INCLUDING COMPLIANCE WTH ALL
 ANFIRE PREVENTION, TEMPORARY SHORING, SCAFFOLDING, TRENCH BOXESILLOPING
BARRIERS. ETC.

The contractor shall protect at his own Expense, All Existing facilites and such


 SUBJECT TO THE APPROVAL OF THE VERIZON WIRELESS REP. ANY WORK FOUND BY THE VERIZON MRELLESS REP TO BE OF INFERIOR QUALITY ANDIOR WORKMANSHIP SHALL EE
REPLACED ANDOR REWORKED AT CONTRACTOR EXPENSE UNTILAPPROVAL IS OBTAINED
29. IN ORDER TO ESTABLISH STANDARDS OF QUALITY AND PERFORMANCE. ALL TYPES OF
MATERIALS LISTED HEREINAFTTR BY MANUFACTUEER'S NAMES ANDIOR MANUFACTURER CATALOG NIITEDER HEREINAFTER BY MANUFACTURER' S NAMES ANDIOR MANUFACT

## STRUCTURAL STEEL NOTES

STRUCTURAL STEEL SHALL CONFORM TO THE LATEST EDITION OF THE AISC SPECIFICATION
FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BULIINGS:
STRUCTURAL STEEL ROLLED SHAPES, PLATES AND BARS SHALL CONFORM TO THE FOLLOWING
ASTM DESIGNATIONS:
A. ASTM A-572, GRADE 50 - ALL WSHAPES. UNLESS NOTED OR A992 OTHERWISE
B. ASTM A-36 - ALL OTHER ROLLED SHAPES, PLATES AND BARS UNLESS NOTED OTHERWISE
C. ASTM A-500, GRADE B-HSS SECTION (SQUARE, RECTANGULAR, AND ROUND)
D. ASTM A-325. TYPE SC OR N - AlL BoLt For connecting structural members
E. ASTM F-1554 07-ALL ANCHOR BOLTS, UNLESS NOTED OTHERWISE

ALL EXPOSED STRUCTURAL STEEL MEMBERS SHALL BE HOT-DIPPED GALVANIZED AFTER
FABRICATION PER ASTM AI23. EXPOSED STEEL HARDWARE AND ANCHOR BOLTS SHALL BE FABRICATION PER ASTM A123. EXPOSOSE
GALVANIZD PER ASTM A1530R R695

ALL IIELD CUT SURFACES, FIELD DRILLED HOLES AND GROUND SURFACES WHERE EXISTING
PAINT OR GALVANIZATION REMOVAL WAS REQURED SHALL BE REPARED WTH (2) BRUSHED COATS OF ZRC GALVLITE COLD GALVANIING COMPOUND PER ASTM A ABO AND

Do not drill holes Through structural steel members except As shown and
DETAlLED on structural drawiges.
6. CONNECTIONS
A. ALL WELDING TO BE PERFORMED BY AWS CERTIFIIED WELDERS AND CONDUCTED IN
ACCORDANCE WTH THE LATEST EDTIION OFTHE AWS WELDNG CODE D1.1.
B. ALL WELDS SHALL BE INSPECTED VIIUALLY. $25 \%$ OF WELDS SHALL BE INSPECTED WITH
DYE PENETRANT OR MAGNETII PATTCLLE TO MEET THE ACCEPTANCE CRTERIA OF AWS D1.1. REPAIR ALL WELDS AS NECESSAAY
c. INSPECTION SHALL BE PERFORMED BY AN AWS CERTIFIED WELD INSPECTOR.
 REOURED BY LOCAL GOVERNING AUTHORITY AND
DEPARTMENT DETAL FOR ANY WELDING ACTIVITY
E. ALL ELECTRODES TO BE LOWHYDROGEN, MATCHING FLLLER METAL. PER AWS D1.1
F. MINIMUM WELD SIZE TO BE 0.1875 INCH FILLET WELDS, UNLESS NOTED OTHERWISE
 NASFCCTIN IS COMPLETE. RERARR ALL GR OUND AND WELDED SURFACES WTH Z ZRC
GALVITTE CO GALVITITE COLD GAL
RECOMMENDATIONS.


Oct 202017 9:29 AM cosi8f

| DRAWN BY: | KL |
| :--- | :--- |
| APPROVED BY: | KRF |

DATE DRAMN: 10/19/1

| ATC JOB NO: | 12157423 |
| :--- | :--- |
| CUSTOMER ID: | NORTH |

GENERAL NOTES





[^0]:    ${ }^{1}$ Mount elevation is defined as height above bottom of steel structure to the bottom of mount, RAD elevation is defined as center of antenna above ground level (AGL).

[^1]:    *Deflection and Sway was evaluated considering a design wind speed of 60 mph (3-Second Gust) per ANSI/TIA-222-G

