# JULIE D. KOHLER 

PLEASE REPLY TO: Bridgeport
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March 25, 2015

Attorney Melanie Bachman<br>Acting Executive Director Connecticut Siting Council<br>Ten Franklin Square<br>New Britain, CT 06051

## Re: Notice of Exempt Modification <br> Blue Sky Towers/T-Mobile equipment upgrade T-Mobile Site ID CT11115F 38 Spring Hill Lane, Bethel Connecticut

Dear Attorney Bachman:
This office represents T-Mobile Northeast LLC ("T-Mobile") and has been retained to file exempt modification filings with the Connecticut Siting Council on its behalf.

In this case, Blue Sky Towers owns the existing telecommunications tower and related facility at 38 Spring Hill Lane, Bethel Connecticut (latitude 41.421013 /longitude -72.749453). T-Mobile intends to add three (3) antennas, and related equipment at this existing facility in Bethel ("Bethel Facility"). Please accept this letter as notification, pursuant to R.C.S.A. § 16 $50 \mathrm{j}-73$, of construction which constitutes an exempt modification pursuant to R.C.S.A. § $16-$ $50 \mathrm{j}-72(\mathrm{~b})(2)$. In accordance with R.C.S.A. § $16-50 \mathrm{j}-73$, a copy of this letter is being sent to the First Selectman, Matt Knickerbocker and the property owner, Spring Hill Lane Properties, LLC.

The existing Bethel Facility consists of a 124 foot monopole tower. ${ }^{1}$ T-Mobile plans to add three (3) antennas and three (3) RRUs (remote radio units) on proposed pipe mounts on the tower at a centerline of 101 feet. T-Mobile will also add hybrid cable that will run inside the monopole and within the compound area. (See the plans revised to March 23, 2015 attached hereto as Exhibit A). The existing tower is structurally capable of supporting T-Mobile's proposed use. See the Structural Analysis Report dated February 25, 2015 attached hereto as Exhibit B.

The planned modifications to the Bethel Facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

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Site ID CT11115F
Page 2

1. The proposed modification will not increase the height of the tower. T-Mobile's new antennas and equipment will be installed at the 101 foot level. The enclosed tower drawing confirms that the proposed modification will not increase the height of the tower.
2. The installation of the hybrid cable in the existing compound, as reflected on the attached site plan, will not require an extension of the site boundaries. (See Sheet A-1).
3. The proposed modification to the Facility will not increase the noise levels at the existing facility by six decibels or more.
4. The operation of the additional antennas will not increase the total radio frequency (RF) power density, measured at the base of the tower, to a level at or above the applicable standard. According to a Radio Frequency Emissions Analysis Report prepared by EBI dated March 13, 2015 T-Mobile's operations would add 13.37\% of the FCC Standard. Therefore, the calculated "worst case" power density for the planned combined operation at the site including all of the proposed antennas would be $90.77 \%$ of the FCC Standard as calculated for a mixed frequency site as evidenced by the engineering exhibit attached hereto as Exhibit C.

For the foregoing reasons, T-Mobile respectfully submits that the proposed additional antennas and equipment at the Bethel Facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Upon acknowledgement by the Council of this proposed exempt modification, T-Mobile shall commence construction approximately sixty days from the date of the Council's notice of acknowledgement.

Sincerely,

cc: First Selectman, Matt Knickerbocker
Blue Sky Towers
Spring Hill Lane Properties, LLC
Elizabeth Jamieson, Transcend Wireless (via e-mail)

## EXHIBIT A







## STRUCTURAL ANALYSIS REPORT

For

## CT11115F

CT115/SNET VALLEY $\qquad$
38 SPRING HILL LANE BETHEL, CT 06801

Antennas Mounted to the Monopole


Prepared for:

## Transcend Wireless

Dated: February 25, 2015

Prepared by:

1600 Osgood Street BIdg. 20 N Suite 3090
North Andover, MA 01845
(P) 978.557.5553 (F) 978.336 .5586
www.hudsondesigngroupllc.com

## SCOPE OF WORK:

Hudson Design Group LLC (HDG) has been authorized by T-Mobile to conduct a structural evaluation of the 124 ' monopole supporting the existing and proposed TMobile's antennas located at elevation 101 ' above the ground level.

This report represents this office's findings, conclusions and recommendations pertaining to the support of T-Mobile's existing and proposed antennas listed below.

Record drawings of the existing monopole were not available for our use. The previous structural analysis report prepared by RAMAKER \& Associates, Inc., dated December 29, 2014, was available and obtained for our use.

## CONCLUSION SUMMARY:

Based on our evaluation, we have determined that the existing monopole is in conformance with the ANSI/TIA-222-F Standard for the loading considered under the criteria listed in this report. The monopole structure is rated at $94.9 \%$ - (Pole section L2 from EL.47.7' to EL.96.0' Controllingl.

APPURTANENCES CONFIGURATION:

| Tenant | Appurtenances | Elev. | Mount |
| :---: | :--- | :--- | :--- |
|  | $15^{\prime}$ Omni | $130^{\prime}$ | Low Profile Platform |
| AT\&T | (3) RRUS-11 | $124^{\prime}$ | Low Profile Plafform |
| AT\&T | (6) 7770 Antennas | $1235^{\prime}$ | Low Profile Platform |
| AT\&T | (9) LGP13519 | $123.5^{\prime}$ | Low Profile Platform |
| AT\&T | (3) P65-16-XLH-RR Antennas | $122^{\prime}$ | Low Profile Platform |
| AT\&T | Surge Arrestor DC6-48-60-18-8F | $120^{\prime}$ | Low Profile Platform |
| Sprint | (3) APXVSPP18 Antennas | $116^{\prime}$ | Low Profile Platform |
| Sprint | (3) APXV9TM14 Antennas | $116^{\prime}$ | Low Profile Plafform |
| Sprint | (3) RRH8x20-25 | $116^{\prime}$ | Low Profile Platform |
| Sprint | (3) RRH-800 | $108^{\prime}$ | Low Profile Platform |
| Sprint | (6) RRH-1900 | $105^{\prime}$ | Low Profile Platform |
|  | 10' Dipole | $106^{\prime}$ | Low Profile Platform |
| T-Mobile | (6) APX16PV-16PVL Antennas | $101^{\prime}$ | Low Profile Platform |
| T-Mobile | (3) LNX-6515DS-VTM Antennas | $101^{\prime}$ | Low Profile Platform |
| T-Mobile | (3) RRUS-11 | $101^{\prime}$ | Low Profile Platform |
|  | (2) 10' Omni | $96^{\prime}$ | Low Profile Platform |
| Verizon | (6) RRUS-11 | $93^{\prime}$ | Low Profile Platform |
| Verizon | (6) 5' Panel Antennas | $92^{\prime}$ | Low Profile Platform |
| Verizon | (3) 2' Antennas | $92^{\prime}$ | Low Profile Platform |
| Verizon | (3) 6.5' Panel Antennas | $91^{\prime}$ | Low Profile Platform |
|  | Low Profile Platform | $81^{\prime}$ |  |
|  | Low Profile Plafform | $71^{\prime}$ |  |
|  | $15^{\prime}$ Dipole | $63^{\prime}$ | Low Profile Platform |

*Proposed T-Mobile Appurtenances shown in Bold.

## T-MOBILE EXISTING/PROPOSED COAX CABLES:

| Tenant | Coax Cables | Elev. | Mount |
| :---: | :--- | :--- | :--- |
| T-Mobile | (12) $15 / 8^{\prime \prime}$ Cables | $101^{\prime}$ | Inside Monopole |
| T-Mobile | (1) Hybrid Cable | $101^{\prime}$ | Inside Monopole |

*Proposed T-Mobile Coax Cables shown in Bold.

ANALYSIS RESULTS SUMMARY:

| Component | Max. Stress <br> Ratio | Elev. of Component <br> (ft) | Pass/Fail | Comments |
| :---: | :---: | :---: | :---: | :---: |
| Pole Section-L1 | $48.7 \%$ | $96.0-124$ | PASS |  |
| Pole Section-L2 | $94.9 \%$ | $47.7-96.0$ | PASS | Controlling |
| Pole Section-L3 | $88.8 \%$ | $1.0-47.7$ | PASS |  |
| Anchor Rod \& Base <br> Plate | $92.7 \%$ | 1.0 | PASS |  |

## DESIGN CRITERIA:

1. EIA/TIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures

County: Fairfield
Wind Load: 85 mph (fastest mile)
105 mph ( 3 second gust)
Nominal Ice Thickness: 1/2 inch
2. Approximate height above grade to proposed antennas: $101^{\prime}$

## *Calculations and referenced documents are aftached.

## ASSUMPTIONS:

1. The monopole dimensions, member sizes and strength of material are as indicated in the previous structural analysis report prepared by RAMAKER \& Associates, Inc., dated December 29, 2014.
2. The appurtenances configuration is as stated in the previous structural analysis report prepared by RAMAKER \& Associates, Inc., dated December 29, 2014. All antennas, coax cables and waveguide cables are assumed to be properly installed and supported as per the manufacturer requirements.
3. The monopole and foundation are properly constructed and maintained. All structural members and their connections are assumed to be in good condition and are free from defects with no deterioration to its member capacities.
4. The support mounts and platforms are not analyzed and are considered adequate to support the loading. The analysis is limited to the primary support structure itself.
5. All prior structural modification, if any, are assumed to be as per the data supplied (if available), and installed properly.
6. The foundation of the monopole was not checked due to lack of information. Asbuilt foundation drawings and geotechnical report would be required to determine whether the foundation is capable of supporting the proposed loadings.

## SUPPORT RECOMMENDATIONS:

HDG recommends that the proposed antennas and RRHs be mounted on the existing steel platform supported by the monopole.

Reference HDG's Latest Construction Drawings for all component and connection requirements (attached).

## ONGOING AND PERIODIC INSPTECTION AND MAINTENANCE:

After the Contractor has successfully completed the installation and the work has been accepted, the Owner will be responsible for the ongoing and periodic inspection and maintenance of the tower.

The owner shall refer to TIA/EIA-222-F for recommendations for maintenance and inspection. The frequency of the inspection and maintenance intervals is to be determined by the owner based upon actual site and environmental conditions. It is recommended that a complete and thorough inspection of the entire tower structural system be performed at lease yearly and more frequently as conditions warrant. According to TIA/EIA-222-F section 14.1, Note 1: It is recommended that the structure be inspected after severe wind and/or ice storms or other extreme loading conditions.


Photo 1: Photo illustrating the Monopole with Appurtenances shown.



DESIGNED APPURTENANCE LOADING

| TYPE | ELEVATION | TYPE | ELEVATION |
| :---: | :---: | :---: | :---: |
| Collar Mount | 124 | RRH-800 | 106 |
| PiROD 13' Low Profile Platform (ATI) | 122 | RRH-800 | 106 |
| 2"x8' pipe | 122 | RRH-800 | 106 |
| $2^{14} \times 8^{\prime}$ pipe | 122 | Collar Mount | 105 |
| 2"x8' pipe | 122 | PiROD 13' Low Profile Platform (T-MOBILE - existing) | 101 |
| Powerwave 7770 w/mount pipe | 122 |  |  |
| Powerwave 7770 w/mount pipe | 122 | (4) 2" ' $^{\text {P }}$ ' pipe | 104 |
| Powerwave 7770 w/mount pipe | 122 | (4) 2"x8' pipe | 101 |
| Powerwave 7770 w/mount pipe | 122 | (4) 2"x8' pipe | 101 |
| Powerwave 7770 w/mount pipe | 122 | (2) RFS APX16PV-16PVL | 104 |
| Powerwave 7770 w/mount pipe | 122 | (2) RFS APX16PV-16PVL | 101 |
| Powerwave P65-16-XLH-RR w/mount pipe | 122 | (2) RFS APX16PV-16PVL | 109 |
|  |  | 10' Dipole | 101 |
| Powerwave P65-16-XLH-RR w/mount pipe | 122 | LNX-6515DS-VTM (T-MOB:LE - proposed) | 101 |
| Powerwave P65-16-XLH-RR w/mount pipe | 122 | LNX-6515DS-VTM | 101 |
|  |  | LNX-6515DS-VTM | 101 |
| Powerwave LGP13519 diplexer | 122 | Ericsson RRUS-11 | 101 |
| Powerwave LGP13519 diplexer | 122 | Ericssan RRUS-11 | 101 |
| Powerwave LGP13519 diplexer | 122 | Ericsson RRUS-11 | 101 |
| Powerwave LGP13519 diplexer | 122 | PiROD 13' Low Profile Piatform (Verizon) | 91 |
| Powerwave LGP13519 diplexer | 122 |  |  |
| Powerwave LGP13519 diplexer | 122 | Panel Antenna $5^{\prime} \times 8^{\prime \prime} \times 6^{\prime \prime}$ w/mount pipe | 91 |
| Powerwave LGP13519 diplexer | 122 | Panel Antenna $5^{\prime} \times 8^{\prime \prime} \times 6^{\prime \prime}$ w/mount pipe | 91 |
| Powerwave LGP13519 diplexer | 122 | Panel Antenna $5^{\prime} \times 8^{\prime \prime} \times 66^{\prime \prime}$ w/mount pipe | 91 |
| Powerwave LGP13519 diplexer | 122 | Panel Antenna 60"x8" $\times 3$ " w/mount pipe | 91 |
| Omni 3"x15' | 122 |  |  |
| Ericsson RRUS-11 | 120 | Panei Antenna 60" $\times 0^{\prime \prime} \times 3^{" 1}$ w/mount pipe | 91 |
| Ericsson RRUS-11 | 120 |  |  |
| Ericsson RRUS-11 | 120 | Panel Antenna 60 " $\times 5^{\prime \prime} \times 3^{\prime \prime}$ w/mount pipe | 91 |
| DC6-48-60-18-8F | 120 | Panel Antenna 6.5'x11"x5" w/mount pipe | 91 |
| (4) 2"x8' pipe | 116 |  |  |
| (4) $2^{\prime \prime} \times 8^{\prime}$ pipe | 116 | Panel Antenna 6.5'x11" $\times 5^{\prime \prime}$ w/mount pipe | 91 |
| (4) 2"x8' pipe | 116 |  |  |
| APXV9TM14 w/mount pipe | 116 | Panel Antenna 6.5'x11" $\times 5$ "' w/mount pipe | 91 |
| APXV9TM14 w/mount pipe | 116 |  |  |
| APXV9TM14 w/mount pipe | 176 | 2'x5" Antenna | 91 |
| APXVSPP18-C w/mount pipe | 116 | 2'x5" Antenna | 91 |
| APXVSPP18-C w/mount pipe | 116 | 2'x5" Antenna | 91 |
| APXVSPP18-C w/mount pipe | 116 | RRUS 11 | 91 |
| RRH 8 $\times 20-25$ | 116 | RRUS 11 | 91 |
| RRH 8x20-25 | 116 | RRUS 11 | 91 |
| RRH 8x20-25 | 116 | RRUS 11 | 91 |
| PiROD 13' Low Profile Platform (SPRINT) | 113 | RRUS 11 | 91 |
|  |  | RRUS 11 | 91 |
| RRH-1900 | 106 | Omni $21 / 2^{\prime \prime} \times 10^{\prime}$ | 91 |
| RRH-1900 | 106 | Omni $21 / 2^{\prime \prime} \times 10^{\prime}$ | 91 |
| RRH-1900 | 106 | PiROD 13' Low Profile Platform | 81 |
| RRH-1900 | 106 | PiROD 13' Low Profile Platform | 71 |
| RRH-1900 | 106 | 15' Dipole | 71 |
| RRH-1900 | 106 |  |  |

MATERIAL STRENGTH

| GRADE | Fy | Fu | GRADE | Fy | Fu |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $4572-65$ | 65 ksi | 80 ksi |  |  |  |

## TOWER DESIGN NOTES

1. Tower is located in Fairfield County, Connecticut.
2. Tower designed for a 85.0 mph basic wind in accordance with the TIANEIA-222-F Standard.
3. Tower is also designed for a 73.6 mph basic wind with 0.50 in ice.
4. Deflections are based upon a 50.0 mph wind.

|  | ${ }^{\text {Pob }}$ CT11115F |  |  |
| :---: | :---: | :---: | :---: |
|  | Project: 124 ft monopo/e |  |  |
|  | Client: T-MOBILE | Drawn by: kw | App'd: |
|  | Code: TIA/EIA-222-F | Daale: 02/24/15 | Scale: NTS |
|  | Path: |  | Dwg No. E-1 |


| tnxTower <br> Hudson Design Group, LLC <br> 1600 Osgood Street, Building 20 North, <br> Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\text { Page } \quad \text { of } 10$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{array}{\|l\|} \hline \text { Date } \\ 16: 43: 3702 / 24 / 15 \end{array}$ |
|  | Client | T-MOBILE | Designed by kw |

## Tower Input Data

There is a pole section.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in Fairfield County, Connecticut.
Basic wind speed of 85.0 mph .
Nominal ice thickness of 0.5000 in.
Ice density of 56.0 pcf .
A wind speed of 73.6 mph is used in combination with ice.
Temperature drop of $50.0^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50.0 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

| Tapered Pole Section Geometry |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation $f t$ | Section <br> Length <br> $f t$ | Splice <br> Length <br> $f t$ | Number of Sides | Top <br> Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| L1 | 125.00-96.04 | 28.96 | 3.92 | 18 | 18.0000 | 26.9000 | 0.1875 | 0.7500 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L2 | $96.04-47.67$ | 52.29 | 5.67 | 18 | 25.3203 | 41.2800 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | 47.67-1.00 | 52.34 |  | 18 | 39.0494 | 55.0000 | 0.3125 | 1.2500 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |

## Monopole Base Plate Data

| Base Plate Data |  |
| :---: | :---: |
| Base plate is square |  |
| Base plate is grouted |  |
| Anchor bolt grade | A615-75 |
| Anchor bolt size | 2,2500 in |
| Number of bolts | 12 |
| Embedment length | 60.0000 in |
| $\mathrm{f}_{\mathrm{c}}$ | 3.0 ksi |
| Grout space | 3.2500 in |
| Base plate grade | A572-60 |
| Base plate thickness | 1.7500 in |
| Bolt circle diameter | 63.0000 in |
| Outer diameter | 69.0000 in |
| Inner diameter | 45.0000 in |
| Base plate type | Stiffened Plate |
| Bolts per stiffener | 1 |
| Stiffener thickness | 0.5000 in |
| Stiffener height | 12.0000 in |


| tnx Tower | Job | CT11115F | $\begin{aligned} & \text { Page } \\ & \\ & 2 \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Project | 124 ft monopole | Date $16: 43: 37 \text { 02/24/15 }$ |
|  | Client | T-MOBILE | Designed by kw |

Feed Line/Linear Appurtenances - Entered As Area

| Description | Face <br> or <br> Leg | Allow <br> Shield | Component <br> Type |  | Placement |  | Total <br> Number | $C_{A} A_{A}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Avimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \begin{tabular}{l}
\(C_{A} A_{A}\) Side \\
\(f t^{2}\)
\end{tabular} \& Weight

$l b$ <br>

\hline Omni $3^{\prime \prime} \times 15^{\prime}$ \& C \& From Leg \& \[
$$
\begin{aligned}
& 3.50 \\
& 0.00 \\
& 8.00
\end{aligned}
$$

\] \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.50 \\
& 6.03
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.50 \\
& 6.03
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
70.00 \\
102.48
\end{gathered}
$$
\] <br>

\hline | ********** |
| :--- |
| PiROD 13' Low Profile |
| Platform |
| (AT\&T) | \& A \& None \& \& 0.0000 \& 122.00 \& No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$ \& \[

$$
\begin{aligned}
& 15.70 \\
& 20.10
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 15.70 \\
& 20.10
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1300.00 \\
& 1765.00
\end{aligned}
$$
\] <br>

\hline 2"x8' pipe \& A \& From Face \& $$
\begin{gathered}
3.50 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 1.90 \\
& 2.73
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.90 \\
& 2.73
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 30.00 \\
& 44.37
\end{aligned}
$$
\] <br>

\hline $2^{\prime \prime} \times 8^{1}$ pipe \& B \& From Face \& \[
$$
\begin{array}{r}
3.50 \\
-2.00 \\
0.00
\end{array}
$$

\] \& 0.0000 \& 122.00 \& | No Ice |
| :--- |
| $1 / 2^{\prime \prime}$ Ice | \& \[

$$
\begin{aligned}
& 1.90 \\
& 2.73
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.90 \\
& 2.73
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 30.00 \\
& 44.37
\end{aligned}
$$
\] <br>

\hline 2"x8' pipe \& C \& From Face \& $$
\begin{gathered}
3.50 \\
-2.00 \\
0.00
\end{gathered}
$$ \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.90 \\
& 2.73
\end{aligned}
$$

\] \& \[

$$
\begin{array}{r}
1.90 \\
2.73
\end{array}
$$

\] \& \[

$$
\begin{aligned}
& 30.00 \\
& 44.37
\end{aligned}
$$
\] <br>

\hline Powerwave $7770 \mathrm{w} / \mathrm{mount}$ pipe \& A \& From Face \& \[
$$
\begin{gathered}
3.50 \\
-6.00 \\
1.50
\end{gathered}
$$

\] \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline Powerwave $7770 \mathrm{w} / \mathrm{mount}$ pipe \& B \& From Face \& \[
$$
\begin{gathered}
3.50 \\
-6.00 \\
1.50
\end{gathered}
$$

\] \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline Powerwave $7770 \mathrm{w} /$ mount pipe \& C \& From Face \& \[
$$
\begin{gathered}
3.50 \\
-6.00 \\
1.50
\end{gathered}
$$

\] \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline Powerwave $7770 \mathrm{w} /$ mount pipe \& A \& From Face \& \[
$$
\begin{aligned}
& 3.50 \\
& 2.00 \\
& 1.50
\end{aligned}
$$

\] \& 0.0000 \& 122.00 \& | No Ice |
| :--- |
| $1 / 2^{11}$ Ice | \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline
\end{tabular}

| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, <br> Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\begin{aligned} & \text { Page } \\ & \\ & \\ & \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 16:43:37 02/24/15 } \end{array}$ |
|  | Client | T-MOBILE | Designed by kw |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
ft \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f^{2}$ | \& $C_{A} A_{A}$ Side $\pi^{2}$ \& Weight <br>

\hline Powerwave $7770 \mathrm{w} / \mathrm{mount}$ pipe \& B \& From Face \& \[
$$
\begin{aligned}
& 3.50 \\
& 2.00 \\
& 1.50
\end{aligned}
$$

\] \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline Powerwave $7770 \mathrm{w} /$ mount pipe \& C \& From Face \& \[
$$
\begin{aligned}
& 3.50 \\
& 2.00 \\
& 1.50
\end{aligned}
$$

\] \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 6.02 \\
& 6.47
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 4.10 \\
& 4.75
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
57.25 \\
103.17
\end{gathered}
$$
\] <br>

\hline Powerwave P65-16-XLH-RR w/mount pipe \& A \& From Face \& $$
\begin{aligned}
& 3.50 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 8.64 \\
& 9.29
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.36 \\
& 7.54
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
48.55 \\
114.33
\end{gathered}
$$
\] <br>

\hline Powerwave P65-16-XLH-RR w/mount pipe \& B \& From Face \& $$
\begin{aligned}
& 3.50 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 8.64 \\
& 9.29
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.36 \\
& 7.54
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
48.55 \\
114.33
\end{gathered}
$$
\] <br>

\hline Powerwave P65-16-XLH-RR w/mount pipe \& C \& From Face \& $$
\begin{aligned}
& 3.50 \\
& 6.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\text {" }}$ Ice \& \[

$$
\begin{aligned}
& 8,64 \\
& 9.29
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 6.36 \\
& 7.54
\end{aligned}
$$

\] \& \[

$$
\begin{gathered}
48.55 \\
114.33
\end{gathered}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& A \& From Face \& $$
\begin{gathered}
3.00 \\
-6.50 \\
1.50
\end{gathered}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{11}$ Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& A \& From Face \& $$
\begin{gathered}
3.00 \\
-5.50 \\
1.50
\end{gathered}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& B \& From Face \& $$
\begin{gathered}
3.00 \\
-6.50 \\
1.50
\end{gathered}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& B \& From Face \& $$
\begin{gathered}
3.00 \\
-5.50 \\
1.50
\end{gathered}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{\prime \prime}$ Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& C \& From Face \& \[
$$
\begin{gathered}
3.00 \\
-6.50 \\
1.50
\end{gathered}
$$

\] \& 0.0000 \& 122.00 \& | No Ice |
| :--- |
| $1 / 2^{\text {II }}$ Ice | \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& C \& From Face \& \[
$$
\begin{gathered}
3.00 \\
-5.50 \\
1.50
\end{gathered}
$$

\] \& 0.0000 \& 122.00 \& | No Ice |
| :--- |
| $1 / 2^{\text {n }}$ Ice | \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& A \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 2.00 \\
& 1.50
\end{aligned}
$$ \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& B \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 2.00 \\
& 1.50
\end{aligned}
$$ \& 0.0000 \& 122.00 \& No Ice $1 / 2^{11}$ Ice \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Powerwave LGP13519 diplexer \& C \& From Face \& $$
\begin{aligned}
& 3.00 \\
& 2.00 \\
& 1.50
\end{aligned}
$$ \& 0.0000 \& 122.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.23 \\
& 1.38
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 0.41 \\
& 0.52
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 14.10 \\
& 21.29
\end{aligned}
$$
\] <br>

\hline Collar Mount \& A \& None \& \& 0.0000 \& 124.00 \& $$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$ \& \[

$$
\begin{aligned}
& 1.40 \\
& 2.40
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.40 \\
& 2.40
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 20.00 \\
& 35.00
\end{aligned}
$$
\] <br>

\hline Ericsson RRUS-11 \& A \& From Face \& $$
\begin{aligned}
& 0.50 \\
& 0.00 \\
& 4.00
\end{aligned}
$$ \& 0.0000 \& 120.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 3.26 \\
& 3.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.38 \\
& 1.56
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 50.70 \\
& 71.57
\end{aligned}
$$
\] <br>

\hline Ericsson RRUS-11 \& B \& From Face \& $$
\begin{aligned}
& 0.50 \\
& 0.00 \\
& 4.00
\end{aligned}
$$ \& 0.0000 \& 120.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 3.26 \\
& 3.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.38 \\
& 1.56
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 50.70 \\
& 71.57
\end{aligned}
$$
\] <br>

\hline Ericsson RRUS-11 \& C \& From Face \& $$
\begin{aligned}
& 0.50 \\
& 0.00 \\
& 4.00
\end{aligned}
$$ \& 0.0000 \& 120.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 3.26 \\
& 3.50
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.38 \\
& 1.56
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 50.70 \\
& 71.57
\end{aligned}
$$
\] <br>

\hline DC6-48-60-18-8F

********** \& A \& From Leg \& $$
\begin{aligned}
& 1.00 \\
& 0.00 \\
& 0.00
\end{aligned}
$$ \& 0.0000 \& 120.00 \& \[

$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.27 \\
& 1.46
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 1.27 \\
& 1.46
\end{aligned}
$$

\] \& \[

$$
\begin{aligned}
& 20.00 \\
& 35.12
\end{aligned}
$$
\] <br>

\hline
\end{tabular}

| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | CT11115F | 4 of 10 |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 | Project |  | Date |
|  |  | 124 ft monopole | 16:43:37 02/24/15 |
| North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Client | T-MOBILE | Designed by kw |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
。
\end{tabular} \& Placement \& \& \(C_{A} A_{A}\) Front
\[
f t^{2}
\] \& \(C_{.} A_{A}\)
Side \& Weight

$7 b$ <br>

\hline \multirow[t]{4}{*}{| PiROD $13^{1}$ Low Profile Platform (SPRINT) |
| :--- |
| (4) $2^{\prime \prime} x 8^{\prime}$ pipe |} \& A \& None \& \& 0.0000 \& 113.00 \& \& 15.70 \& 15.70 \& 1300.00 <br>

\hline \& \& \& \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 20.10 \& 20.10 \& 1765.00 <br>

\hline \& A \& From Face \& 3.50 \& 0.0000 \& 116.00 \& No Ice \& 1.90 \& 1.90 \& 30.00 <br>
\hline \& \& \& 0.00
-3.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.73 \& 2.73 \& 44.37 <br>

\hline \multirow[t]{2}{*}{(4) $2^{\prime \prime} \mathrm{x}^{\prime}$ pipe} \& \multirow[t]{2}{*}{B} \& \multirow[t]{2}{*}{From Face} \& 3.50 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{116.00} \& \multirow[t]{2}{*}{| No Ice |
| :--- |
| $1 / 2^{\prime \prime}$ Ice |} \& \multirow[t]{2}{*}{1.90

2.73} \& \multirow[t]{2}{*}{1.90
2.73} \& \multirow[t]{2}{*}{30.00
44.37} <br>
\hline \& \& \& 0.00
-3.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(4) $2^{\prime \prime} x 8^{\prime}$ pipe} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\text {I }}$ Ice} \& 1.90 \& 1.90 \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& \& \multirow[t]{2}{*}{2.73} \& \multirow[t]{2}{*}{2.73} \& \multirow[t]{2}{*}{44.37} <br>
\hline \& \& \& -3.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14 w/mount pipe} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{11}$ Ice} \& 7.21 \& 5.03 \& 91.90 <br>
\hline \& \& \& -2.00 \& \& \& \& \multirow[t]{2}{*}{7.77} \& \multirow[t]{2}{*}{5.89} \& \multirow[t]{2}{*}{147.31} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14 w/mount pipe} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& 7.21 \& 5.03 \& 91.90 <br>
\hline \& \& \& -2.00 \& \& \& \& \multirow[t]{2}{*}{7.77} \& \multirow[t]{2}{*}{5.89} \& \multirow[t]{2}{*}{147.31} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXV9TM14 w/mount pipe} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& 7.21 \& 5.03 \& 91.90 <br>
\hline \& \& \& -2.00 \& \& \& \& \multirow[t]{2}{*}{7.77} \& \multirow[t]{2}{*}{5.89} \& \multirow[t]{2}{*}{147.31} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXVSPP18-C w/mount pipe} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\prime \prime}$ Ice} \& 8.55 \& 7.30 \& 97.53 <br>
\hline \& \& \& 2.00 \& \& \& \& \multirow[t]{2}{*}{9.18} \& \multirow[t]{2}{*}{8.32} \& \multirow[t]{2}{*}{168.85} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXVSPP18-C w/mount pipe} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice

$$
1 / 2^{\prime \prime} \text { Ice }
$$} \& 8.55 \& 7.30 \& 97.53 <br>

\hline \& \& \& 2.00 \& \& \& \& \multirow[t]{2}{*}{9.18} \& \multirow[t]{2}{*}{8.32} \& \multirow[t]{2}{*}{168.85} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{APXVSPP18-C w/mount pipe} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\text {" }}$ Ice} \& 8.55 \& 7.30 \& 97.53 <br>
\hline \& \& \& 2.00 \& \& \& \& \multirow[t]{2}{*}{9.18} \& \multirow[t]{2}{*}{8.32} \& \multirow[t]{2}{*}{168.85} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RRH 8×20-25} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{11}$ Ice} \& 4.72 \& 1.70 \& 70.00 <br>
\hline \& \& \& -2.00 \& \& \& \& \multirow[t]{2}{*}{5.01} \& \multirow[t]{2}{*}{1.92} \& \multirow[t]{2}{*}{97.14} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RRH 8x20-25} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{116.00} \& \multirow[t]{3}{*}{No Ice

$$
1 / 2^{11} \text { Ice }
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 4.72 \\
& 5.01
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 1.70 \\
& 1.92
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 70.00 \\
& 97.14
\end{aligned}
$$
\]} <br>

\hline \& \& \& -2.00 \& \& \& \& \& \& <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RRH 8×20-25} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 3.50 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{116.00} \& \multirow[t]{4}{*}{No Ice $1 / 2^{\text {" }}$ Ice} \& 4.72 \& 1.70 \& 70.00 <br>
\hline \& \& \& -2.00 \& \& \& \& \multirow[t]{3}{*}{5.01} \& \multirow[t]{3}{*}{1.92} \& \multirow[t]{3}{*}{97.14} <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline ********** \& \& \& \& \& \& \& \& \& <br>
\hline \multirow[t]{2}{*}{Collar Mount} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{None} \& \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{105.00} \& \multirow[t]{2}{*}{No Ice $1 / 2^{\text {" Ice }}$} \& 1.40 \& 1.40 \& 20.00 <br>
\hline \& \& \& \& \& \& \& 2.40 \& 2.40 \& 35.00 <br>

\hline \multirow[t]{3}{*}{RRH-1900} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{106.00} \& \multirow[t]{2}{*}{| No Ice |
| :--- |
| $1 / 2^{\text {" }}$ Ice |} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 2.71 \\
& 2.95
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 3.66 \\
& 3.92
\end{aligned}
$$

\]} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 60.00 \\
& 88.32
\end{aligned}
$$
\]} <br>

\hline \& \& \& -1.00 \& \& \& \& \& \& <br>
\hline \& \& \& -1.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{RRH-1900} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{106.00} \& \multirow[t]{2}{*}{| No Ice |
| :--- |
| $1 / 2^{\text {" }}$ Ice |} \& \multirow[t]{2}{*}{\[

$$
\begin{aligned}
& 2.71 \\
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& 3.66 \\
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\begin{aligned}
& 60.00 \\
& 88.32
\end{aligned}
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\hline \& \& \& 1.00 \& \& \& \& \& \& <br>
\hline \& \& \& -1.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{RRH-1900} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& \multirow[t]{2}{*}{0.0000} \& \multirow[t]{2}{*}{106.00} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{\prime \prime} \text { Ice }
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

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\begin{aligned}
& 2.71 \\
& 2.95
\end{aligned}
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\]} \& \multirow[t]{3}{*}{\[

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\begin{aligned}
& 3.66 \\
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$$
\begin{aligned}
& 60.00 \\
& 88.32
\end{aligned}
$$
\]} <br>

\hline \& \& \& -1.00 \& \& \& \& \& \& <br>
\hline \& \& \& -1.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{RRH-1900} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{106.00} \& \multirow[t]{3}{*}{No Ice $1 / 2^{\text {" }}$ Ice} \& \multirow[t]{3}{*}{\[
$$
\begin{aligned}
& 2.71 \\
& 2.95
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 3.66 \\
& 3.92
\end{aligned}
$$
\]} \& 60.00 <br>

\hline \& \& \& 1.00 \& \& \& \& \& \& \multirow[t]{2}{*}{88.32} <br>
\hline \& \& \& -1.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{RRH-1900} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& \multirow[t]{3}{*}{0.0000} \& \multirow[t]{3}{*}{106.00} \& \multirow[t]{3}{*}{$$
\begin{aligned}
& \text { No Ice } \\
& 1 / 2^{11} \text { Ice }
\end{aligned}
$$} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 2.71 \\
& 2.95
\end{aligned}
$$

\]} \& \multirow[t]{3}{*}{\[

$$
\begin{aligned}
& 3.66 \\
& 3.92
\end{aligned}
$$
\]} \& 60.00 <br>

\hline \& \& \& -1.00 \& \& \& \& \& \& \multirow[t]{2}{*}{88.32} <br>
\hline \& \& \& -1.00 \& \& \& \& \& \& <br>
\hline
\end{tabular}

| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\begin{aligned} & \text { Page } \\ & \\ & 5 \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{array}{\|l\|} \text { Date } \\ \text { 16:43:37 02/24/15 } \end{array}$ |
|  | Client | T-MOBILE | Designed by <br> kw |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement \& \& \begin{tabular}{l}
\(C_{A} A_{A}\) \\
Front \\
\(f t^{2}\)
\end{tabular} \& \(C_{A} A_{A}\)
Side \& Weight

$l b$ <br>
\hline \multirow[t]{2}{*}{RRH-1900} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{From Face} \& 1.00 \& 0.0000 \& 106.00 \& No Ice \& 2.71 \& 3.66 \& 60.00 <br>
\hline \& \& \& 1.00
-1.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.95 \& 3.92 \& 88.32 <br>
\hline \multirow[t]{3}{*}{RRH-800} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 106.00 \& No Ice \& 2.49 \& 3.22 \& 64.00 <br>
\hline \& \& \& 1.00 \& \& \& 1/2" Ice \& 2.71 \& 3.46 \& 91.74 <br>
\hline \& \& \& 2.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RRH-800} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 106.00 \& No Ice \& 2.49 \& 3.22 \& 64.00 <br>
\hline \& \& \& 1.00 \& \& \& $1 / 2^{1 \prime}$ Ice \& 2.71 \& 3.46 \& 91.74 <br>
\hline \& \& \& 2.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{RRH-800} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 1.00 \& 0.0000 \& 106.00 \& No Ice \& 2.49 \& 3.22 \& 64.00 <br>
\hline \& \& \& 1.00 \& \& \& $1 / 2^{1 \prime}$ Ice \& 2.71 \& 3.46 \& 91.74 <br>
\hline \& \& \& 2.00 \& \& \& \& \& \& <br>
\hline \multicolumn{10}{|l|}{**********} <br>
\hline \multirow[t]{5}{*}{PiROD 13' Low Profile Platform (T-MOBILE - existing) (4) $2^{\prime \prime} x 8^{\prime}$ pipe} \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{None} \& \& 0.0000 \& 101.00 \& No Ice \& 15.70 \& 15.70 \& 1300.00 <br>
\hline \& \& \& \& \& \& $1 / 2^{11}$ Ice \& 20.10 \& 20.10 \& 1765.00 <br>
\hline \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 1.90 \& 1.90 \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.73 \& 2.73 \& 44.37 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(4) 2"x8' pipe} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 1.90 \& 1.90 \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.73 \& 2.73 \& 44.37 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(4) $2^{\prime \prime}$ x8' pipe} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 1.90 \& 1.90 \& 30.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 2.73 \& 2.73 \& 44.37 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>

\hline \multirow[t]{3}{*}{(2) RFS APX16PV-16PVL} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& $$
6.70
$$ \& \[

2.84

\] \& \[

40.00
\] <br>

\hline \& \& \& 0.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& \[

7.13

\] \& \[

3.17

\] \& \[

75.57
\] <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(2) RFS APX16PV-16PVL} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 6.70 \& 2.84 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.13 \& 3.17 \& 75.57 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{(2) RFS APX16PV-16PVL} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 6.70 \& 2.84 \& 40.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\text {I }}$ Ice \& 7.13 \& 3.17 \& 75.57 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{$10^{\prime}$ Dipole} \& \multirow[t]{4}{*}{A} \& \multirow[t]{3}{*}{From Face} \& \& 0.0000 \& 101.00 \& \& 4.00 \& 4.00 \& 25.00 <br>

\hline \& \& \& -3.00 \& \& \& $$
1 / 2^{11} \text { Ice }
$$ \& 4.97 \& 4.97 \& 53.13 <br>

\hline \& \& \& 5.00 \& \& \& \& \& \& <br>
\hline \multicolumn{9}{|l|}{**********} \& <br>

\hline \multirow[t]{3}{*}{| LNX-6515DS-VTM |
| :--- |
| (T-MOBILE - proposed) |} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 11.45 \& 7.70 \& 50.30 <br>

\hline \& \& \& -3.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 12.06 \& 8.29 \& 116.17 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{LNX-6515DS-VTM} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& No Ice \& 11.45 \& 7.70 \& 50.30 <br>
\hline \& \& \& -3.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 12.06 \& 8.29 \& 116.17 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{LNX-6515DS-VTM} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Face} \& 3.50 \& 0.0000 \& 101.00 \& \& 11.45 \& 7.70 \& 50.30 <br>

\hline \& \& \& -3.00 \& \& \& $$
1 / 2^{\prime \prime} \text { Ice }
$$ \& 12.06 \& 8.29 \& 116.17 <br>

\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Ericsson RRUS-11} \& \multirow[t]{3}{*}{A} \& \multirow[t]{3}{*}{From Face} \& 2.50 \& 0.0000 \& 101.00 \& No Ice \& 3.26 \& 1.38 \& 50.70 <br>
\hline \& \& \& -3.00 \& \& \& $1 / 2^{\text {" }}$ Ice \& 3.50 \& 1.56 \& 71.57 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Ericsson RRUS-11} \& \multirow[t]{3}{*}{B} \& \multirow[t]{3}{*}{From Face} \& 2.50 \& 0.0000 \& 101.00 \& No Ice \& 3.26 \& 1.38 \& 50.70 <br>
\hline \& \& \& -3.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.50 \& 1.56 \& 71.57 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline \multirow[t]{3}{*}{Ericsson RRUS-11} \& \multirow[t]{4}{*}{C} \& \multirow[t]{4}{*}{From Face} \& 2.50 \& 0.0000 \& 101.00 \& No Ice \& 3.26 \& 1.38 \& 50.70 <br>
\hline \& \& \& -3.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.50 \& 1.56 \& 71.57 <br>
\hline \& \& \& 0.00 \& \& \& \& \& \& <br>
\hline ********** \& \& \& \& \& \& \& \& \& <br>
\hline
\end{tabular}



| Description | $\begin{aligned} & \text { Face } \\ & \text { or } \\ & \text { Leg } \end{aligned}$ | $\begin{aligned} & \text { Offset } \\ & \text { Type } \end{aligned}$ | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> ft | Azimuth Adjustment <br> - | Placement |  | $C_{A} A_{A}$ Front $f t^{2}$ | $C_{A} A_{A}$ Side <br> $f^{2}$ | Weight |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| PiROD 13' Low Profile Platform (Verizon) | A | None |  | 0.0000 | 91.00 | No Ice $1 / 2^{\prime \prime} \text { Ice }$ | $\begin{aligned} & 15.70 \\ & 20.10 \end{aligned}$ | $\begin{aligned} & 15.70 \\ & 20.10 \end{aligned}$ | $\begin{aligned} & 1300.00 \\ & 1765.00 \end{aligned}$ |
| Panel Antenna 5'x8"x6" w/mount pipe | A | From Face | $\begin{aligned} & 3.50 \\ & 6.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice $1 / 2^{\prime \prime}$ Ice | $\begin{aligned} & 4.96 \\ & 5.43 \end{aligned}$ | $\begin{aligned} & 5.17 \\ & 6.05 \end{aligned}$ | $\begin{aligned} & 51.90 \\ & 99.00 \end{aligned}$ |
| Panel Antenna 5'x8"x6" w/mount pipe | B | From Face | $\begin{aligned} & 3.50 \\ & 6.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice $1 / 2^{\text {I }}$ Ice | $\begin{aligned} & 4.96 \\ & 5.43 \end{aligned}$ | $\begin{aligned} & 5.17 \\ & 6.05 \end{aligned}$ | $\begin{aligned} & 51.90 \\ & 99.00 \end{aligned}$ |
| Panel Antenna 5'x8"x6" w/mount pipe | C | From Face | $\begin{aligned} & 3.50 \\ & 6.00 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice $1 / 2^{11}$ Ice | $\begin{aligned} & 4.96 \\ & 5.43 \end{aligned}$ | $\begin{aligned} & 5.17 \\ & 6.05 \end{aligned}$ | $\begin{aligned} & 51.90 \\ & 99.00 \end{aligned}$ |
| Panel Antenna $60^{\prime \prime} \times 6^{\prime \prime} \times 3^{\prime \prime}$ w/mount pipe | A | From Face | $\begin{aligned} & 3.50 \\ & 4.50 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice $1 / 2^{\text {1 }}$ Ice | $\begin{aligned} & 4.22 \\ & 4.81 \end{aligned}$ | $\begin{aligned} & 3.95 \\ & 5.04 \end{aligned}$ | $\begin{aligned} & 55.55 \\ & 94.39 \end{aligned}$ |
| Panel Antenna 60" $\times 6^{\prime \prime} \times 3^{\prime \prime}$ w/mount pipe | B | From Face | $\begin{aligned} & 3.50 \\ & 4.50 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice <br> $1 / 2^{11}$ Ice | $\begin{aligned} & 4.22 \\ & 4.81 \end{aligned}$ | $\begin{aligned} & 3.95 \\ & 5.04 \end{aligned}$ | $\begin{aligned} & 55.55 \\ & 94.39 \end{aligned}$ |
| Panel Antenna 60"x6"x3" w/mount pipe | C | From Face | $\begin{aligned} & 3.50 \\ & 4.50 \\ & 1.00 \end{aligned}$ | 0.0000 | 91.00 | No Ice $1 / 2^{\prime \prime}$ Ice | $\begin{aligned} & 4.22 \\ & 4.81 \end{aligned}$ | $\begin{aligned} & 3.95 \\ & 5.04 \end{aligned}$ | $\begin{aligned} & 55.55 \\ & 94.39 \end{aligned}$ |
| Panel Antenna $6.5^{\prime} \times 11^{\prime \prime} \times 5^{\prime \prime}$ w/mount pipe | A | From Face | $\begin{gathered} 3.50 \\ -1.00 \\ 0.00 \end{gathered}$ | 0.0000 | 91.00 | No Ice $1 / 2^{\prime \prime}$ Ice | $\begin{aligned} & 8.48 \\ & 9.09 \end{aligned}$ | $\begin{aligned} & 6.23 \\ & 7.43 \end{aligned}$ | $\begin{gathered} 55.55 \\ 119.35 \end{gathered}$ |
| Panel Antenna $6.5^{\prime} \times 11^{\prime \prime} \times 5^{\prime \prime}$ w/mount pipe | B | From Face | $\begin{gathered} 3.50 \\ -1.00 \\ 0.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 8.48 \\ & 9.09 \end{aligned}$ | $\begin{aligned} & 6.23 \\ & 7.43 \end{aligned}$ | $\begin{gathered} 55.55 \\ 119.35 \end{gathered}$ |
| Panel Antenna 6.5'x11"x5" w/mount pipe | C | From Face | $\begin{gathered} 3.50 \\ -1.00 \\ 0.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{11} \text { Ice } \end{aligned}$ | $\begin{aligned} & 8.48 \\ & 9.09 \end{aligned}$ | $\begin{aligned} & 6.23 \\ & 7.43 \end{aligned}$ | $\begin{gathered} 55.55 \\ 119.35 \end{gathered}$ |
| 2'x.5' Antenna | A | From Face | $\begin{gathered} 3.50 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 91.00 | No Ice $1 / 2^{11}$ Ice | $\begin{aligned} & 1.17 \\ & 1.36 \end{aligned}$ | $\begin{aligned} & 0.72 \\ & 0.88 \end{aligned}$ | $\begin{aligned} & 20.00 \\ & 27.78 \end{aligned}$ |
| 2'x5' Antenna | B | From Face | $\begin{gathered} 3.50 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 1.17 \\ & 1.36 \end{aligned}$ | $\begin{aligned} & 0.72 \\ & 0.88 \end{aligned}$ | $\begin{aligned} & 20.00 \\ & 27.78 \end{aligned}$ |
| 2'x5' Antenna | C | From Face | $\begin{gathered} 3.50 \\ -6.00 \\ 1.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 1.17 \\ & 1.36 \end{aligned}$ | $\begin{aligned} & 0.72 \\ & 0.88 \end{aligned}$ | $\begin{aligned} & 20.00 \\ & 27.78 \end{aligned}$ |
| RRUS 11 | A | From Face | $\begin{array}{r} 3.00 \\ -1.00 \\ 2.00 \end{array}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |
| RRUS 11 | B | From Face | $\begin{gathered} 3.00 \\ -1.00 \\ 2.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{11} \text { Ice } \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |
| RRUS 11 | C | From Face | $\begin{gathered} 3.00 \\ -1.00 \\ 2.00 \end{gathered}$ | 0.0000 | 91.00 | No Ice <br> $1 / 2^{\text {" Ice }}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |
| RRUS 11 | A | From Face | $\begin{gathered} 3.00 \\ -6.00 \\ 2.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |
| RRUS 11 | B | From Face | $\begin{gathered} 3.00 \\ -6.00 \\ 2.00 \end{gathered}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |
| RRUS 11 | C | From Face | $\begin{array}{r} 3.00 \\ -6.00 \\ 2.00 \end{array}$ | 0.0000 | 91.00 | $\begin{aligned} & \text { No Ice } \\ & 1 / 2^{\prime \prime} \text { Ice } \end{aligned}$ | $\begin{aligned} & 3.25 \\ & 3.49 \end{aligned}$ | $\begin{aligned} & 1.37 \\ & 1.55 \end{aligned}$ | $\begin{aligned} & 50.70 \\ & 71.50 \end{aligned}$ |


| tnxTower | Job |  | Page |
| :---: | :---: | :---: | :---: |
|  |  | CT11115F | 7 of 10 |
| Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 | Project |  | Date |
|  |  | 124 ft monopole | 16:43:37 02/24/15 |
| North Andover, MA 01845 Phone: (978) 557-5553 FAX: (978) 226-5586 | Client | T-MOBILE | Designed by kW |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \[
\begin{aligned}
\& \text { Offset } \\
\& \text { Type }
\end{aligned}
\] \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\)
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& $C_{A} A_{A}$ Front

\[
f^{2}

\] \& | $C_{A} A_{A}$ Side |
| :--- |
| $f t^{2}$ | \& Weight

lb <br>
\hline \multirow[t]{2}{*}{Omni $21 / 2^{\prime \prime} \times 10^{\prime}$} \& \multirow[t]{2}{*}{B} \& \multirow[t]{2}{*}{From Leg} \& 6.50 \& 0.0000 \& 91.00 \& No Ice \& 2.50 \& 2.50 \& 25.00 <br>
\hline \& \& \& 0.00
5.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.53 \& 3.53 \& 43.64 <br>
\hline \multirow[t]{3}{*}{Omni $21 / 2^{\prime \prime} \times 10^{\prime}$} \& \multirow[t]{3}{*}{C} \& \multirow[t]{3}{*}{From Leg} \& 6.50 \& 0.0000 \& 91.00 \& No Ice \& 2.50 \& 2.50 \& 25.00 <br>
\hline \& \& \& 0.00 \& \& \& $1 / 2^{\prime \prime}$ Ice \& 3.53 \& 3.53 \& 43.64 <br>
\hline \& \& \& 5.00 \& \& \& \& \& \& <br>
\hline \multicolumn{10}{|l|}{**********} <br>
\hline \multirow[t]{2}{*}{PiROD 13' Low Profile Platform} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{None} \& \& 0.0000 \& 81.00 \& No Ice \& 15.70 \& 15.70 \& 1300.00 <br>
\hline \& \& \& \& \& \& $1 / 2^{\prime \prime}$ Ice \& 20.10 \& 20.10 \& 1765.00 <br>
\hline \multirow[t]{4}{*}{PiROD 13' Low Profile Platform 15' Dipole} \& \multirow[t]{2}{*}{C} \& \multirow[t]{2}{*}{None} \& \& 0.0000 \& 71.00 \& No Ice \& 15.70 \& 15.70 \& 1300.00 <br>
\hline \& \& \& \& \& \& $1 / 2^{\text {" }}$ Ice \& 20.10 \& 20.10 \& 1765.00 <br>
\hline \& \multirow[t]{2}{*}{A} \& \multirow[t]{2}{*}{From Face} \& 3.50 \& 0.0000 \& 71.00 \& No Ice \& 6.00 \& 6.00 \& 40.00 <br>

\hline \& \& \& $$
\begin{aligned}
& -5.00 \\
& -8.00
\end{aligned}
$$ \& \& \& $1 / 2^{\prime \prime}$ Ice \& 7.54 \& 7.54 \& 81.87 <br>

\hline
\end{tabular}

## Load Combinations

| Comb. No. |  | Description |
| :---: | :---: | :---: |
| 1 | Dead Only |  |
| 2 | Dead+Wind 0 deg - No Ice |  |
| 3 | Dead+Wind 30 deg - No Ice |  |
| 4 | Dead+Wind 60 deg - No Ice |  |
| 5 | Dead+Wind 90 deg - No Ice |  |
| 6 | Dead+Wind 120 deg - No Ice |  |
| 7 | Dead+Wind 150 deg - No Ice |  |
| 8 | Dead+Wind 180 deg - No Ice |  |
| 9 | Dead+Wind 210 deg - No Ice |  |
| 10 | Dead+Wind 240 deg - No Ice |  |
| 11 | Dead+Wind 270 deg - No Ice |  |
| 12 | Dead+Wind 300 deg - No Ice |  |
| 13 | Dead+Wind 330 deg - No Ice |  |
| 14 | Dead + Ice + Temp |  |
| 15 | Dead+Wind 0 deg+Ice + Temp |  |
| 16 | Dead+Wind 30 deg + Ice + Temp |  |
| 17 | Dead+Wind 60 deg + Ice + Temp |  |
| 18 | Dead + Wind $90 \mathrm{deg}+$ Ice + Temp |  |
| 19 | Dead + Wind 120 deg + Ice + Temp |  |
| 20 | Dead + Wind 150 deg + Ice + Temp |  |
| 21 | Dead + Wind $180 \mathrm{deg}+$ Ice + Temp |  |
| 22 | Dead+Wind 210 deg+Ice+Temp |  |
| 23 | Dead+Wind 240 deg+Ice+Temp |  |
| 24 | Dead+Wind 270 deg+Ice+Temp |  |
| 25 | Dead+Wind 300 deg + Ice + Temp |  |
| 26 | Dead+Wind 330 deg+Ice + Temp |  |
| 27 | Dead + Wind 0 deg - Service |  |
| 28 | Dead + Wind 30 deg - Service |  |
| 29 | Dead +Wind 60 deg - Service |  |
| 30 | Dead+Wind 90 deg - Service |  |
| 31 | Dead+Wind 120 deg - Service |  |
| 32 | Dead+Wind 150 deg - Service |  |
| 33 | Dead+Wind 180 deg - Service |  |
| 34 | Dead + Wind 210 deg - Service |  |


| tnxTower <br> Hudson Design Group, LLC <br> 1600 Osgood Street, Building 20 North <br> Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\begin{aligned} & \text { Page } \\ & 8 \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{array}{\|l\|} \hline \text { Date } \\ 16: 43: 3702 / 24 / 15 \end{array}$ |
|  | Client | T-MOBILE | Designed by kw |


| Comb. | Description |  |
| :---: | :---: | :---: |
| No. |  |  |
| 35 | Dead+Wind 240 deg - Service |  |
| 36 | Dead+Wind 270 deg - Service |  |
| 37 | Dead+Wind 300 deg - Service |  |
| 38 | Dead+Wind 330 deg - Service |  |


|  |  | Maximum Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Location | Condition | Gov. <br> Load <br> Comb. | $\begin{gathered} \text { Vertical } \\ \text { Ib } \end{gathered}$ | $\begin{gathered} \text { Horizontal, } X \\ \quad l b \end{gathered}$ | $\begin{gathered} \text { Horizontal, } Z \\ l b \end{gathered}$ |
| Pole | Max. Vert | 24 | 39715.47 | 24121.08 | 0.00 |
|  | Max. $\mathrm{H}_{x}$ | 11 | 31136.01 | 28174.68 | -0.00 |
|  | Max. $\mathrm{H}_{z}$ | 2 | 31136.01 | 0.00 | 28174.68 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 2583298.98 | 0.00 | 28174.68 |
|  | Max. $\mathrm{M}_{\mathrm{z}}$ | 5 | 2583009.22 | -28174.68 | -0.00 |
|  | Max. Torsion | 13 | 3594.47 | 14087.34 | 24399.99 |
|  | Min. Vert | 1 | 31136.01 | 0.00 | 0.00 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 5 | 31136.01 | -28174.68 | -0.00 |
|  | Min. $\mathrm{H}_{2}$ | 8 | 31136.01 | 0.00 | -28174.68 |
|  | Min. $\mathrm{M}_{x}$ | 8 | -2584109.79 | 0.00 | -28174.68 |
|  | Min. $\mathrm{M}_{\mathbf{z}}$ | 11 | -2584399.54 | 28174.68 | $-0.00$ |
|  | Min. Torsion | 7 | -3594.45 | -14087.34 | -24399.99 |

## Tower Mast Reaction Summary

| Load Combination | Vertical <br> $l b$ | Sheary <br> $l b$ | Shear <br> $l b$ | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 31136.01 | 0.00 | 0.00 | 388.26 | 666.69 | 0.00 |
| Dead+Wind 0 deg - No Ice | 31136.01 | -0.00 | -28174.68 | -2583298.98 | 682.73 | -3214.73 |
| Dead+Wind 30 deg - No rce | 31136.01 | 14087.34 | -24399.99 | -2237146.51 | -1291164.90 | -1973.50 |
| Dead+Wind 60 deg - No Ice | 31136.01 | 24399.99 | -14087.34 | -1291447.30 | -2236861.00 | -203.54 |
| Dead+Wind 90 deg - No Ice | 31136.01 | 28174.68 | 0.00 | 399.18 | -2583009.22 | 1621.02 |
| Dead+Wind 120 deg - No Ice | 31136.01 | 24399.99 | 14087.34 | 1292248.76 | -2236866.42 | 3011.16 |
| Dead+Wind 150 deg - No Ice | 31136.01 | 14087.34 | 24399.99 | 2237954.21 | -1291170.32 | 3594.45 |
| Dead+Wind 180 deg - No Ice | 31136.01 | -0.00 | 28174.68 | 2584109.79 | 682.72 | 3214.68 |
| Dead+Wind 210 deg - No Ice | 31136.01 | -14087.34 | 24399.99 | 2237965.00 | 1292541.93 | 1973.47 |
| Dead+Wind 240 deg - No Ice | 31136.01 | -24399.99 | 14087.34 | 1292259.54 | 2238250.50 | 203.51 |
| Dead + Wind 270 deg - No Ice | 31136.01 | -28174.68 | 0.00 | 399.17 | 2584399.54 | -1620.99 |
| Dead + Wind 300 deg - No Ice | 31136.01 | -24399.99 | -14087.34 | -1291458.11 | 2238245.09 | -3011.10 |
| Dead+Wind 330 deg - No Ice | 31136.01 | -14087.34 | -24399.99 | -2237157.31 | 1292536.53 | -3594.47 |
| Dead+Ice+Temp | 39715.47 | -0.00 | 0.00 | 668.41 | 1238.55 | -0.00 |
| Dead+Wind 0 deg+Ice+Temp | 39715.47 | 0.00 | -24121.08 | -2272843.75 | 1287.19 | -3064.77 |
| Dead+Wind 30 deg+Ice+Temp | 39715.47 | 12060.54 | -20889.47 | -1968241.88 | -1135479.58 | -1824.16 |
| Dead+Wind 60 deg+Ice + Temp | 39715.47 | 20889.47 | -12060.54 | -1136069.71 | -1967648.57 | -94.80 |
| Dead+Wind 90 deg+Ice + Temp | 39715.47 | 24121.08 | -0.00 | 695.92 | -2272246.10 | 1660.01 |
| Dead + Wind 120 deg + Ice + Temp | 39715.47 | 20889.47 | 12060.54 | 1137465.60 | -1967655.62 | 2970.00 |
| Dead+Wind $150 \mathrm{deg}+$ Ice + Temp | 39715.47 | 12060.54 | 20889.47 | 1969645.89 | -1135486.65 | 3484.11 |
| Dead+Wind 180 deg + Ice + Temp | 39715.47 | 0.00 | 24121.08 | 2274251.81 | 1287.16 | 3064.69 |
| Dead + Wind 210 deg + Ice + Temp | 39715.47 | -12060.54 | 20889.47 | 1969658.42 | 1138068.22 | 1824.11 |
| Dead+Wind 240 deg+Ice+Temp | 39715.47 | -20889.47 | 12060.54 | 1137478.12 | 1970251.69 | 94.74 |
| Dead+Wind 270 deg + Ice + Temp | 39715.47 | -24121.08 | -0.00 | 695.88 | 2274849.42 | -1659.97 |
| Dead+Wind $300 \mathrm{deg}+$ Ice + Temp | 39715.47 | -20889.47 | -12060.54 | -1136082.28 | 1970244.66 | -2969.92 |
| Dead + Wind 330 deg+Ice+Temp | 39715.47 | -12060.54 | -20889.47 | -1968254.43 | 1138061.20 | -3484.15 |


| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\begin{aligned} & \text { Page } \\ & \qquad 9 \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{aligned} & \text { Date } \\ & \text { 16:43:37 02/24/15 } \end{aligned}$ |
|  | Client | T-MOBILE | Designed by <br> kw |


| Load Combination | Vertical <br> $l b$ | Shear $x_{x}$ <br> $l b$ | Shear $z_{z}$ <br> $l b$ | Overturning Moment, $M_{x}$ $l b-f t$ | Overturning Moment, $M_{z}$ $l b-f t$ | Torque <br> $l b-f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead+Wind 0 deg - Service | 31136.01 | -0.00 | -9749.03 | -894440.83 | 698.37 | -1119.44 |
| Dead+Wind 30 deg - Service | 31136.01 | 4874.51 | -8442.90 | -774553.37 | -446725.35 | -687.17 |
| Dead+Wind 60 deg - Service | 31136.01 | 8442.90 | -4874.51 | -447016,35 | -774262.00 | -70.78 |
| Dead+Wind 90 deg - Service | 31136.01 | 9749.03 | 0.00 | 407.23 | -894148.95 | 564.58 |
| Dead+Wind 120 deg - Service | 31136.01 | 8442.90 | 4874.51 | 447831.19 | -774262.65 | 1048.66 |
| Dead+Wind 150 deg - Service | 31136.01 | 4874.51 | 8442.90 | 775368.96 | -446726.01 | 1251.74 |
| Dead+Wind 180 deg - Service | 31136.01 | -0.00 | 9749.03 | 895256.79 | 698.36 | 1119.43 |
| Dead+Wind 210 deg - Service | 31136.01 | -4874.51 | 8442.90 | 775370.25 | 448123.48 | 687.16 |
| Dead+Wind 240 deg - Service | 31136.01 | -8442.90 | 4874.51 | 447832.48 | 775661.62 | 70.77 |
| Dead+Wind 270 deg - Service | 31136.01 | -9749.03 | 0.00 | 407.23 | 895548.67 | -564.58 |
| Dead+Wind 300 deg - Service | 31136.01 | -8442.90 | -4874.51 | -447017.65 | 775660.97 | -1048.66 |
| Dead+Wind 330 deg - Service | 31136.01 | -4874.51 | -8442.90 | -774554.67 | 448122.83 | -1251.76 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ | PY | PZ |  |
| Comb. | $l b$ | $l b$ | $l b$ | $l b$ | $1 b$ | $l b$ |  |
| 1 | 0.00 | -31136.01 | 0.00 | 0.00 | 31136.01 | 0.00 | 0.000\% |
| 2 | 0.00 | -31136.01 | -28174.68 | 0.00 | 31136.01 | 28174.68 | 0.000\% |
| 3 | 14087,34 | -31136.01 | -24399.99 | -14087,34 | 31136.01 | 24399.99 | 0.000\% |
| 4 | 24399.99 | -31136.01 | -14087.34 | -24399.99 | 31136.01 | 14087.34 | 0.000\% |
| 5 | 28174.68 | -31136.01 | 0.00 | -28174.68 | 31136.01 | -0.00 | 0.000\% |
| 6 | 24399.99 | -31136.01 | 14087.34 | -24399.99 | 31136.01 | -14087.34 | 0.000\% |
| 7 | 14087.34 | -31136.01 | 24399.99 | -14087.34 | 31136.01 | -24399.99 | 0.000\% |
| 8 | 0.00 | -31136.01 | 28174.68 | 0.00 | 31136.01 | -28174.68 | 0.000\% |
| 9 | -14087.34 | -31136.01 | 24399.99 | 14087.34 | 31136.01 | -24399.99 | 0.000\% |
| 10 | -24399.99 | -31136.01 | 14087.34 | 24399.99 | 31136.01 | -14087.34 | 0.000\% |
| 11 | -28174.68 | -31136.01 | 0.00 | 28174.68 | 31136.01 | -0.00 | 0.000\% |
| 12 | -24399.99 | -31136.01 | -14087.34 | 24399.99 | 31136.01 | 14087.34 | 0.000\% |
| 13 | -14087.34 | -31136.01 | -24399.99 | 14087.34 | 31136.01 | 24399.99 | 0.000\% |
| 14 | 0.00 | -39715.47 | 0.00 | 0.00 | 39715.47 | -0.00 | 0.000\% |
| 15 | 0.00 | -39715.47 | -24121.07 | -0.00 | 39715.47 | 24121.08 | 0.000\% |
| 16 | 12060.54 | -39715.47 | -20889.46 | -12060.54 | 39715.47 | 20889.47 | 0.000\% |
| 17 | 20889.46 | -39715.47 | -12060.54 | -20889.47 | 39715.47 | 12060.54 | 0.000\% |
| 18 | 24121.07 | -39715.47 | 0.00 | -24121.08 | 39715.47 | 0.00 | 0.000\% |
| 19 | 20889.46 | -39715.47 | 12060.54 | -20889.47 | 39715.47 | -12060.54 | 0.000\% |
| 20 | 12060.54 | -39715.47 | 20889.46 | -12060.54 | 39715.47 | -20889.47 | 0.000\% |
| 21 | 0.00 | -39715.47 | 24121.07 | -0.00 | 39715.47 | -24121.08 | 0.000\% |
| 22 | -12060.54 | -39715.47 | 20889.46 | 12060.54 | 39715.47 | -20889.47 | 0.000\% |
| 23 | -20889.46 | -39715.47 | 12060.54 | 20889.47 | 39715.47 | -12060.54 | 0.000\% |
| 24 | -24121.07 | -39715.47 | 0.00 | 24121.08 | 39715.47 | 0.00 | 0.000\% |
| 25 | -20889.46 | -39715.47 | -12060.54 | 20889.47 | 39715.47 | 12060.54 | 0.000\% |
| 26 | -12060.54 | -39715.47 | -20889.46 | 12060.54 | 39715.47 | 20889.47 | 0.000\% |
| 27 | 0.00 | -31136.01 | -9749.02 | 0.00 | 31136.01 | 9749.03 | 0.000\% |
| 28 | 4874.51 | -31136.01 | -8442.90 | -4874.51 | 31136.01 | 8442.90 | 0.000\% |
| 29 | 8442.90 | -31136.01 | -4874.51 | -8442.90 | 31136.01 | 4874.51 | 0.000\% |
| 30 | 9749.02 | -31136.01 | 0.00 | -9749.03 | 31136.01 | -0.00 | 0.000\% |
| 31 | 8442.90 | -31136.01 | 4874.51 | -8442.90 | 31136.01 | -4874.51 | 0.000\% |
| 32 | 4874.51 | -31136.01 | 8442.90 | -4874.51 | 31136.01 | -8442.90 | 0.000\% |
| 33 | 0.00 | -31136.01 | 9749.02 | 0.00 | 31136.01 | -9749.03 | 0.000\% |
| 34 | -4874.51 | -31136.01 | 8442.90 | 4874.51 | 31136.01 | -8442.90 | 0.000\% |
| 35 | -8442.90 | -31136.01 | 4874.51 | 8442.90 | 31136.01 | -4874.51 | 0.000\% |
| 36 | -9749.02 | -31136.01 | 0.00 | 9749.03 | 31136.01 | -0.00 | 0.000\% |
| 37 | -8442.90 | -31136.01 | -4874.51 | 8442.90 | 31136.01 | 4874.51 | 0.000\% |
| 38 | -4874.51 | -31136.01 | -8442.90 | 4874.51 | 31136.01 | 8442.90 | 0.000\% |


| tnxTower <br> Hudson Design Group, LLC 1600 Osgood Street, Building 20 North, <br> Suite 3090 <br> North Andover, MA 01845 <br> Phone: (978) 557-5553 <br> FAX: (978) 226-5586 | Job | CT11115F | $\begin{aligned} & \text { Page } 10 \text { of } 10 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
|  | Project | 124 ft monopole | $\begin{array}{\|l\|} \text { Date } \\ \text { 16:43:37 02/24/15 } \end{array}$ |
|  | Client | T-MOBILE | Designed by kw |


|  | Maximum Tower Deflections - Service W |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Horz. | Gov. | Tilt | Twist |
| No. |  | Deflection | Load |  |  |
|  | $f$ | in | Comb. | 0 | - |
| L1 | 125-96.04 | 24.0311 | 35 | 1.7332 | 0.0093 |
| L2 | 99.96-47.67 | 15.2683 | 35 | 1.5384 | 0.0062 |
| L3 | 53.34-1 | 3.9261 | 35 | 0.7137 | 0.0018 |

Critical Deflections and Radius of Curvature - Service Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f$ |  | Comb. | in | $\circ$ | 0 | ft |

## Section Capacity Table

| Section No. | Elevation $f t$ | Component Type | Size | Critical <br> Element | $\begin{aligned} & P \\ & l b \end{aligned}$ | $\begin{gathered} S F^{*} P_{\text {allow }} \\ l b \end{gathered}$ | $\begin{gathered} \% \\ \text { Capacity } \end{gathered}$ | Pass <br> Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 125-96.04 | Pole | TP26.9x18x0.1875 | 1 | -7808.54 | 789179.96 | 48.7 | Pass |
| L2 | 96.04-47.67 | Pole | TP41.28x25.3203x0.25 | 2 | -19094.50 | 1588016.16 | 94.9 | Pass |
| L3 | 47.67-1 | Pole | TP55x39.0494x0.3125 | 3 | -31114.10 | 2618145.19 | 88.8 | Pass |
|  |  |  |  |  |  |  | Summary |  |
|  |  |  |  |  |  | Pole (L2) | 94.9 | Pass |
|  |  |  |  |  |  | Base Plate | 92.7 | Pass |
|  |  |  |  |  |  | RATING = | 94.9 | Pass |



# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility

Site ID: CT11115F
SNET Valley_FT
38 Spring Hill Lane Bethel, CT 06801

March 13, 2015
EBI Project Number: 6215001452

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general public <br> allowable limit: | $90.77 \%$ |

March 13, 2015

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

## Emissions Analysis for Site: CT11115F - SNET Valley_FT

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 38 Spring Hill Lane,
Bethel, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307 (b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter $\left(\mu \mathrm{W} / \mathrm{cm}^{2}\right)$. The general population exposure limit for the 700 MHz Band is $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the PCS and AWS bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at $\mathbf{3 8}$ Spring Hill Lane, Bethel, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65 . Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels (PCS Band -1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
2) 2 UMTS channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (AWS Band -2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 1 LTE channel ( 700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antennas used in this modeling are the Ericsson AIR21 (B4A/B2P\& B2A/B4P) for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the Commscope LNX-6515DS-VTM for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The Ericsson AIR21 (B4A/B2P\& B2A/B4P) has a maximum gain of 15.9 dBd at its main lobe. The Commscope LNX-6515DS-VTM has a maximum gain of $\mathbf{1 4 . 6}$ dBd at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antenna mounting height centerline of the proposed antennas is $\mathbf{1 0 1}$ feet above ground level (AGL).
9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

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T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | 1 | Antenna \#: | 1 | Antenna \#: | 1 |
| Make / Model: | Ericsson AIR21 <br> B4A/B2P | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B4A/B2P } \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 101 | Height (AGL): | 101 | Height (AGL): | 101 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 2 | Channel Count | 2 | \# PCS Channels: | 2 |
| Total TX Power: | 120 | Total TX Power: | 120 | \# AWS Channels: | 120 |
| ERP (W): | 4,668.54 | ERP (W): | 4,668.54 | ERP (W): | 4,668.54 |
| Antenna A1 MPE\% | 1.86 | Antenna B1 MPE\% | 1.86 | Antenna C1 MPE\% | 1.86 |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B2A/B4P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson ATR21 } \\ \text { B2A/B4P } \\ \hline \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Ericsson AIR21 } \\ \text { B2A/B4P } \\ \hline \end{gathered}$ |
| Gain: | 15.9 dBd | Gain: | 15.9 dBd | Gain: | 15.9 dBd |
| Height (AGL): | 101 | Height (AGL): | 101 | Height (AGL): | 101 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz} \text { (PCS) / } \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 4 | Channel Count | 4 | Channel Count | 4 |
| Total TX Power: | 120 | Total TX Power: | 120 | Total TX Power: | 120 |
| ERP (W): | 4,668.54 | ERP (W): | 4,668.54 | ERP (W): | 4,668.54 |
| Antenna A2 MPE\% | 1.86 | Antenna B2 MPE\% | 1.86 | Antenna C2 MPE\% | 1.86 |
| Antenna \#: | 3 | Antenna \#: | 3 | Antenna\#: | 3 |
| Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM | Make / Model: | Commscope LNX-6515DS-VTM |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 101 | Height (AGL): | 101 | Height (AGL): | 101 |
| Frequency Bands | 700 MHz | Frequency Bands | 700 MHz | Frequency Bands | 700 MHz |
| Channel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power: | 30 | Total TX Power: | 30 |
| ERP (W): | 865.21 | ERP (W): | 865.21 | ERP (W): | 865.21 |
| Antenna A3 MPE\% | 0.74 | Antenna B3 MPE\% | 0.74 | Antenna C3 MPE\% | 0.74 |
|  | Site Composite MPE\% |  |  | T-Mobile Sector 1 Total: | 1: $4.46 \%$ |
|  | Carrier | MPE\% |  | T-Mobile Sector 2 Total: | 1: $4.46 \%$ |
|  | T-Mobile | 13.37 |  | T-Mobile Sector 3 Total: | l: $4.46 \%$ |
|  | Bethel PD | No Data Available |  | Site Total: | 1: $90.77 \%$ |

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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector 1: | $4.46 \%$ |
| Sector 2: | $4.46 \%$ |
| Sector 3: | $4.46 \%$ |
| T-Mobile Total: | $13.37 \%$ |
|  |  |
| Site Total: | $90.77 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{9 0 . 7 7 \%}$ of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


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[^0]:    ${ }^{1}$ This Facility was approved in Docket No. 288. The Docket No. 288 Decision and Order contains no limitations or restrictions relevant to T-Mobile's proposed modifications.

