



July 18, 2019

Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification for Verizon Wireless: 841295

Verizon Site ID:104335

719 Amity Rd. Bethany, CT 06524

Latitude: 41° -26' 33.93"/ Longitude: -72° -59' 32.86"

Dear Ms. Bachman:

Verizon currently maintains nine (9) antennas at the 95-foot level of the existing 150-foot monopole tower at 719 Amity Road, Bethany CT 06524. The tower is owned by Crown Castle and the Town of Bethany is the property owner. Verizon now intends to replace six (6) antennas with new antennas. Verizon also intends to add three (3) new remote radios, replace three (3) remote radios with new, add one (1) hybrid cable and one (1) OVP box as well as a handrail kit for the antenna mount.

This facility was approved by the Connecticut Siting Council in Docket No. 168 on June 6, 1995. This approval included the condition that:

1. The self-supporting monopole tower shall be no taller than necessary to provide the proposed communication service and the tower shall not exceed a total height of 150 feet above ground level (AGL).

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to First-Selectwoman - Ms. Paula Cofrancesco, Town of Bethany and Land Use Administrator/Zoning Enforcement – Isabel Kearns, Town of Bethany. The property owner is the Town of Bethany and Crown Castle is the tower owner.

- 1. The proposed modifications will not result in an increase in the height of the existing tower.
- 2. The proposed modifications will not require the extension of the site boundary.
- 3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

The Foundation for a Wireless World.

CrownCastle.com

- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
- 5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Verizon respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Jeffrey Barbadora.

Sincerely

Jeffrey Barbadora Real Estate Specialist

12 Gill Street, Suite 5800, Woburn, MA 01801

781-729-0053

Jeff.Barbadora@crowncastle.com

Attachments:

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

First-Selectwoman - Ms. Paula Cofrancesco Town of Bethany 40 Peck Road 203-393-2100 ext. 1100

Land Use Administrator/Zoning Enforcement – Isabel Kearns Town of Bethany 40 Peck Road 203-393-2100 ext. 1135

Town of Bethany, Land Owner

Crown Castle, Tower Owner

DOCKET NO. 168 - An application of Springwich Cellular Limited Partnership for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telecommunications facility located on the former site of the Bethany Airport, 719 Amity Road (Route 63) in Bethany, Connecticut.

- Connecticut
- } Siting
- } Council
- } July 6, 1995

DECISION AND ORDER

Pursuant to the foregoing Findings of Fact, and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a cellular telecommunications tower and equipment building at the proposed site in Bethany, Connecticut, including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildlife are not disproportionate either alone or cumulatively with other effects when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes § 16-50k, be issued to Springwich Cellular Limited Partnership (Springwich), for the construction, operation, and maintenance of a cellular telecommunications tower, associated equipment, and building at the proposed site located at the Bethany Airport, 719 Amity Road, Bethany, Connecticut.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

- 1. The self-supporting monopole tower shall be no taller than necessary to provide the proposed communications service and the tower shall not exceed a total height of 150 feet above ground level (AGL).
- 2. The Certificate Holder shall prepare a Development and Management (D&M) Plan for this site in compliance with Sections 16-50j-75 through 16-50j-77 of the Regulations of Connecticut State Agencies. The D&M Plan shall be submitted to and approved by the Council prior to the commencement of facility construction and shall include detailed plans for the tower location and tower foundation; the placement of all antennas to be attached to this tower; equipment building, access road, utility line, and security fence; site clearing and tree trimming; and water drainage and erosion and sedimentation controls consistent with the Connecticut Guidelines for Soil Erosion and Sedimentation Control, as amended.
- Upon the establishment of any new State or federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
- 4. The Certificate Holder shall provide the Council a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels originally calculated and provided in the application.

Decision & Order Docket No. 168 July 6, 1995 Pg. 2

- 5. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
- 6. If the facility does not initially provide, or permanently ceases to provide cellular services following completion of construction, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapplication for any continued or new use shall be made to the Council before any such use is made.
- 7. Unless otherwise approved by the Council, this Decision and Order shall be void if all construction authorized herein is not completed within three years of the effective date of this Decision and Order or within three years after all appeals to this Decision and Order have been resolved.
- 8. The Certificate Holder shall notify the Council upon completion of construction and provide the final cost to construct the facility.

Pursuant to General Statutes § 16-50p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in <u>The New Haven Register</u> and <u>Beth-Wood News</u>.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section 16-50j-17 of the Regulations of Connecticut State Agencies.

The parties and intervenors to this proceeding are:

APPLICANT

Springwich Cellular Limited Partnership

INTERVENOR

Metro Mobile CTS of Hartford, Inc.

ITS REPRESENTATIVES

Peter J. Tyrrell, Esq. Springwich Cellular Limited Partnership 227 Church Street New Haven, CT 06510

ITS REPRESENTATIVES

Metro Mobile CTS of Hartford, Inc. 20 Alexander Drive Wallingford, CT 06492 Attn: David S. Malko, P.E., Manager Engineering & Regulatory Services

Robinson & Cole One Commercial Plaza Hartford, CT 06103-3597 Attn: Brian C.S. Freeman, Esq.

CERTIFICATION

The Undersigned members of the Connecticut Siting Council (Council) hereby certify that they have heard this case, or read the record thereof, in Docket No. 168 - An application of Springwich Cellular Limited Partnership for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telecommunications facility located on the former site of the Bethany Airport, 719 Amity Road (Route 63) in Bethany, Connecticut, and voted as follows:

Council Members	Vote Cast
Å	
notime 4. Lobota	YES
Mortimer A. Gelston	
Chairman	
Commissioner Reginaldy. Smith Designee: Gerald J. Heffernan	YES
Frederick L. Quese	YES
Commissioner Sidney J. Holbrook	
Designee: Fred Riese	
Helfon Ducken	YES
William J. Huber	
Gloria Dibble Pond	ABSENT
William H. Smith	YES
Colin C. Tait	ABSTAIN
Edward S. Wilensky	ABSENT
Dana J. Wright	YES
r - U	

Dated at New Britain, Connecticut, July 6, 1995.

STATE OF CONNECTICUT }

ss. New Britain, Connecticut }

COUNTY OF HARTFORD

STATE OF CONNECTICUT }

July 7, 1995

I hereby certify that the foregoing is a true and correct copy of the Findings of Fact, Opinion, and Decision and Order issued by the Connecticut Siting Council, State of Connecticut.

ATTEST:

JoelM. Rinebold Executive Director

Connecticut Siting Council

I certify that a copy of the Findings of Fact, Opinion, and Decision and Order in Docket No. 168 have been forwarded by Certified First Class Return Receipt Requested mail on July 7, 1995, to all parties and intervenors of record as listed on the attached service list, dated April 10, 1995.

ATTEST:

Gloria B. Owens

Administrative Assistant Connecticut Siting Council The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at 70% of the estimated market value of real property at the time of the last revaluation which was 2013.



Information on the Property Records for the Municipality of Bethany was last updated on 9/20/2017.

Property Summary Information

Parcel Data And Values

Building v

Outbuildings

Google Map

Parcel Information

Location:

755 AMITY RD

Property Use:

Public Use

Primary Use:

Fire Station -

Volunteer

Unique ID:

00016500

Map Block

117/1

Acres:

138,50

490 Acres:

0.00

Zone:

Lot:

8&I

Volume /

0044/0306

Page:

Developers

Map / Lot:

Census:

Value Information

Appraised Value

70% Assessed Value

Land

1,476,000

1,033,200

Buildings

1,740,164

1,218,110

	Appraised Value	70% Assessed Value	
Detached Outbuildings	159,624	111,740	
Total	3,375,788	2,363,050	
	Owner's Information		

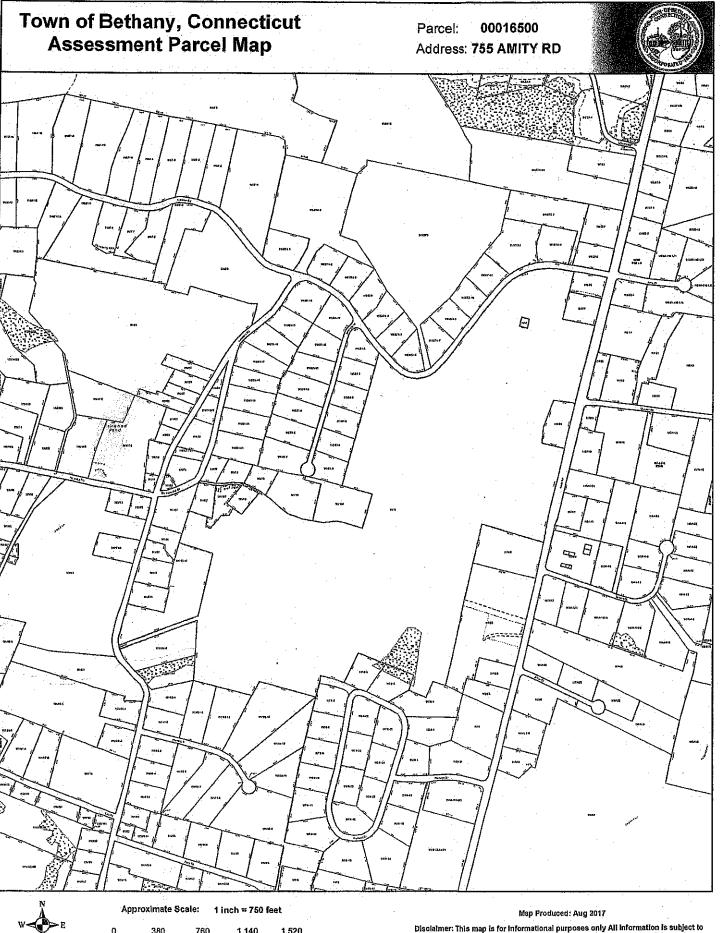
Owner's Data

BETHANY TOWN OF 40 PECK RD BETHANY CT 06524

Back To Search (JavaScript:window.history.back(1);)

Print View (PrintPage.aspx?towncode=008&uniqueid=00016500)

Information Published With Permission From The Assessor





Site Name: Bethany North CT Cumulative Power Density

Operator	Operating Frequency		CONTRACTOR STREET, CONTRACTOR OF STREET, CON	Total ERP	Distance to Target	Calculated Power Density
	(MHz)		(watts)	(watts)	(feet)	(mW/cm^2)
VZW PCS	1970	4	1104	4416.28	110	0.1313
VZW Cellular CDMA	869	2	289	578.16	110	0.0172
VZW Cellular LTE	880	4	463	1853.76	110	0.0551
VZW AWS	2145	4	1225	4898.44	110	0.1456
VZW 700	746	4	492	1968	100	0.0708

Total Percentage of Maximum Permissible Exposure

MHz = Megahertz mW/cm^2 = milliwatts per square centimeter ERP = Effective Radiated Power

Absolute worst case maximum values used, including the following assumptions:

- 1. closest accessible point is distance from antenna to base of pole;
- 2. continuous transmission from all available channels at full power for indefinite time period; and,
- 3. all RF energy is assumed to be directed solely to the base of the pole.

^{*}Guidelines adopted by the FCC on August 1, 1996, 47 CFR Section 1.13101 based on NCRP Report 86, 19

Maximum Permissible Exposure	Fraction of MPE
(mW/cm^2)	(%)
1.0	13.13%
0.579333333	2.97%
0.586666667	9.39%
1.0	14.56%
0.497333333	14.23%

54.27%

86 and generally on ANSI/IEEE C95.1-1992

The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at 70% of the estimated market value of real property at the time of the last revaluation which was 2018.



Information on the Property Records for the Municipality of Bethany was last updated on 7/18/2019.

Property Summary Information

Parcel Data And Values Building W Outbuildings

Parcel Information

Location:	755 AMITY RD	Property Use:	Public Use	Primary Use:	Fire Station - Volunteer
Unique ID:	00016500	Map Block Lot:	117/1	Acres:	138.50
490 Acres:	0.00	Zone:	B&I	Volume / Page:	0044/0306
Developers Map / Lot:		Census:			

Value Information

	Appraised Value	Assessed Value	
	the state of the same of the s	to a contract of the contract	
Land	1,421,200	994,840	

	Appraised Value	Assessed Value
Buildings	1,878,616	1,315,030
Detached Outbuildings	150,924	105,650
Total	3,450,740	2,415,520

Owner's Information

Owner's Data

BETHANY TOWN OF 40 PECK RD BETHANY, CT 06524

Back To Search (JavaScript:window.history.back(1);)

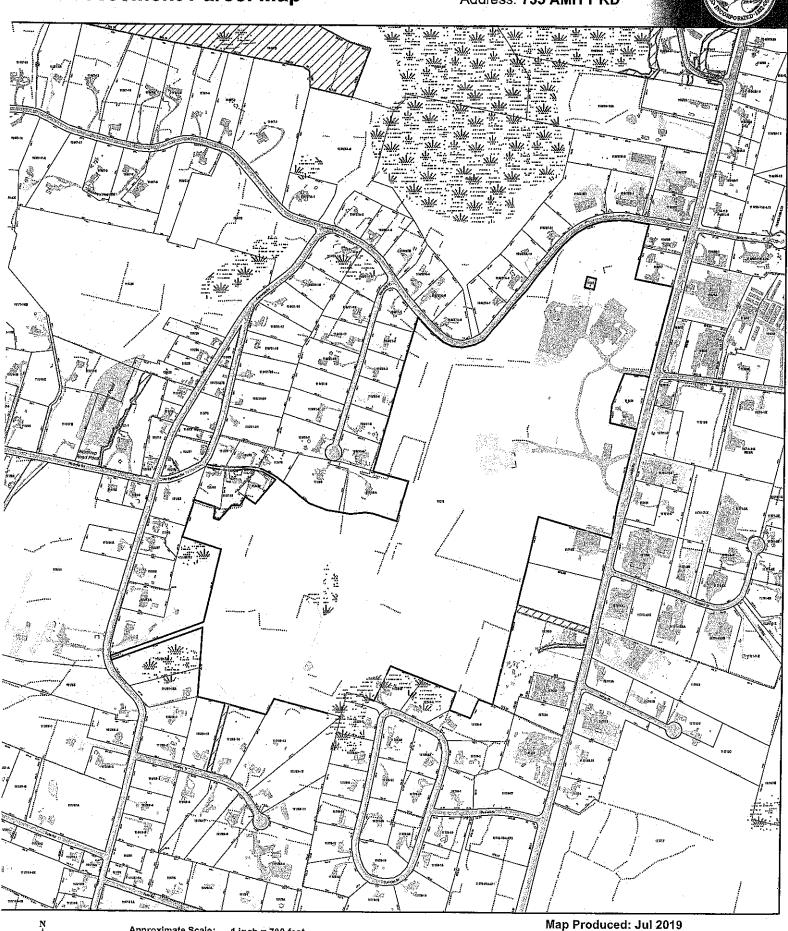
Print View (PrintPage.aspx?towncode=008&uniqueid=00016500)

Information Published With Permission From The Assessor

Town of Bethany, Connecticut Assessment Parcel Map

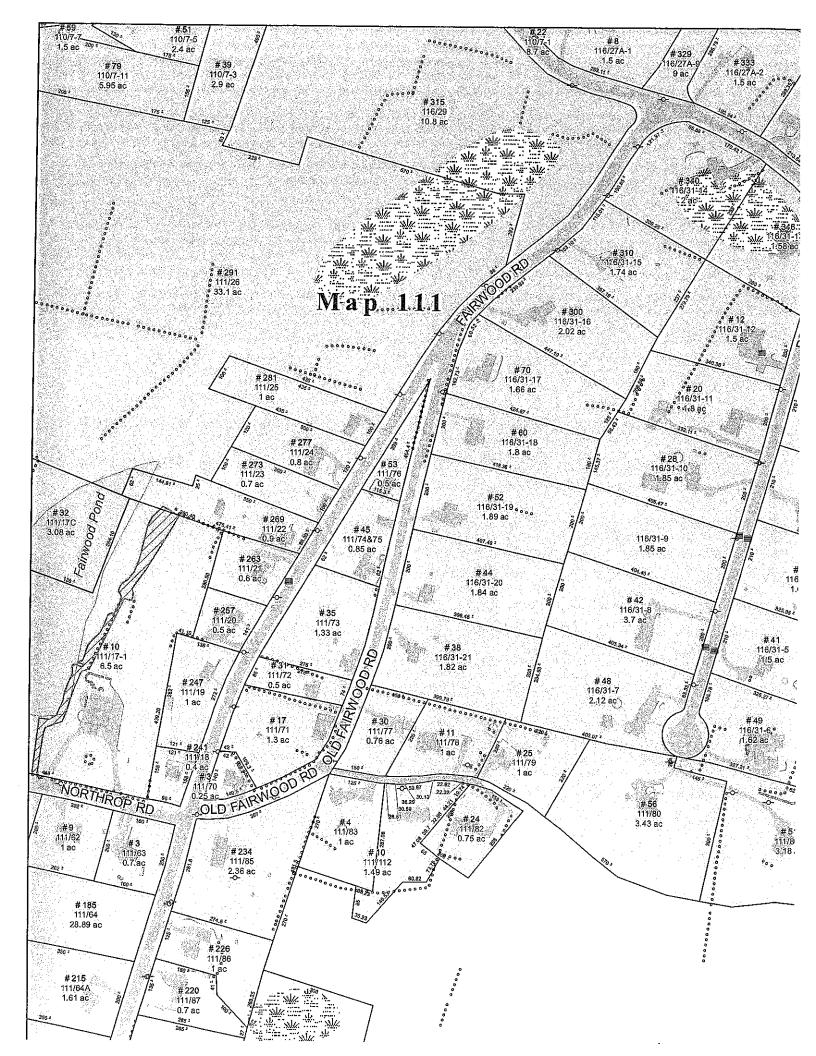
Parcel: 00016500 Address: 755 AMITY RD

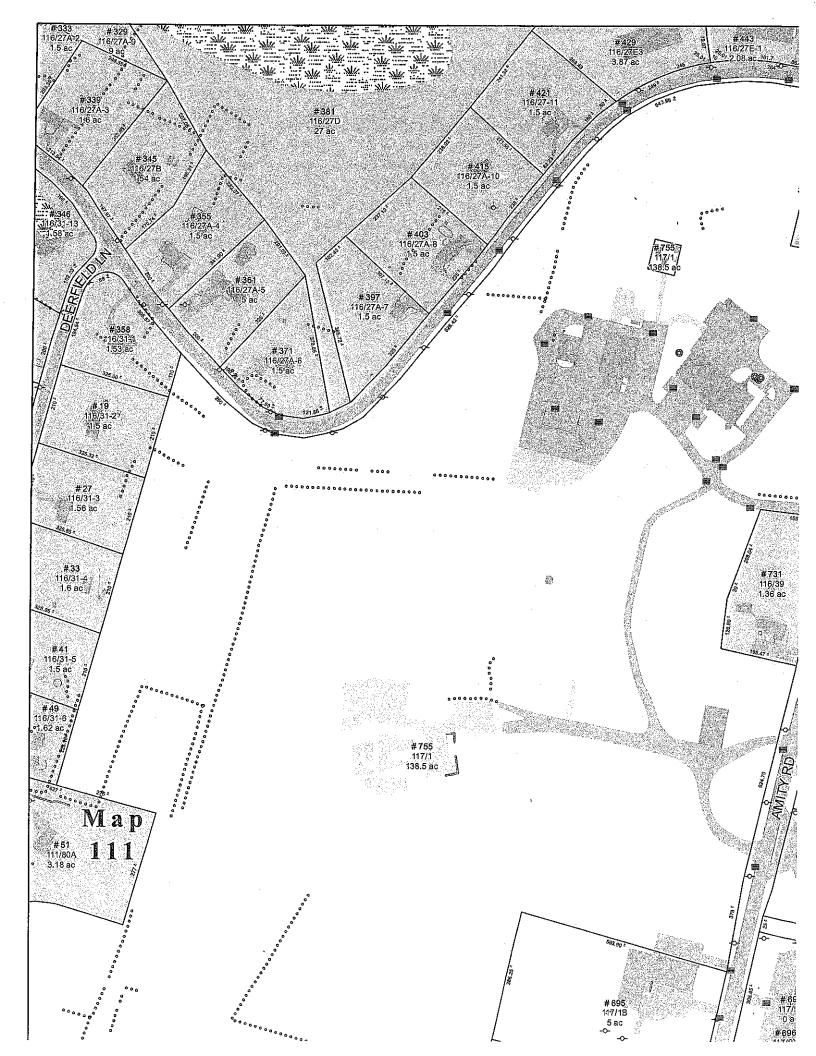




720

1,440





(781) 970-0053

SHIP DATE: 18JUL19 ACTWGT: 0.50 LB CAD: 104924191/INET4160

BILL SENDER

TO LAND USE/ZONE ENF. ISABEL KEARNS **TOWN OF BETHANY 40 PECK ROAD**

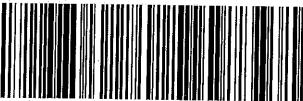
BETHANY CT 06524 (203) 393-2100 X 1135 NV. PO.

REF: 1766.6680

7757 7707 6160

FRI - 19 JUL 10:30A **PRIORITY OVERNIGHT**

06524 BDL



567 J2JA6F9Q5A2

(781) 970-0053

SHIP DATE: 18JUL19 ACTWGT: 0.50 LB CAD: 104924191/INET4160

BILL SENDER

TO FIRST SELECTWOMAN PAULA COFRANCESCO **TOWN OF BETHANY 40 PECK ROAD**

BETHANY CT 06524 (203) 393-2100 X 1100

REF: 1766,6680

TRK# 7757 7705 1682

FRI - 19 JUL 10:30A **PRIORITY OVERNIGHT**

06524 BDL



567 J2JA6F9J05A2

Date: May 28, 2019

Kevin Morrow Crown Castle 3530 Toringdon Way, Suite 300 Charlotte, NC 28277 (704) 405-6619 Kimley»Horn

Kimley-Horn and Associates, Inc. 421 Fayetteville Street, Suite 600 Raleigh, NC 27601 (919) 677-2000 CrownMounts@kimley-horn.com

Subject:

Mount Modification Report

Carrier Designation:

Verizon Wireless Equipment Change-Out Carrier Site Number: 104335

Carrier Site Name:

Bethany North CT

Crown Castle Designation:

Crown Castle BU Number: Crown Castle Site Name:

841295 BETHANY 574490

Crown Castle JDE Job Number: Crown Castle Order Number:

492710, Rev. 0

Engineering Firm Designation:

Kimley-Horn Report Designation: 019558041

Site Data:

719 Amity Road, Bethany, New Haven County, CT 06524

Latitude 41° 26' 33.93" Longitude -72° 59' 32.86"

Structure Information:

Tower Height & Type: 150 ft Monopole

Mount Elevation:

140 ft

Mount Type:

12.5 ft Low Profile Platform

Dear Charles McGuirt.

Kimley-Horn is pleased to submit this "Mount Modification Report" to determine the structural integrity of Verizon Wireless's antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

Low Profile Platform

Sufficient

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2015 International Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: Greg VanMaaren, E.I. under the supervision of Steven C. Ball, P.E., S.E.

Respectfully Submitted by:

Steven C. Ball, P.E., S.E.

が心場



TABLE OF CONTENTS

1) INTRODUCTION

2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration

3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

- 3.1) Analysis Method
- 3.2) Assumptions

4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity

4.1) Recommendations

5) APPENDIX A

Wire Frame and Rendered Models

6) APPENDIX B

Software Input Calculations

7) APPENDIX C

Software Analysis Output

8) APPENDIX D

Additional Calculations

9 APPENDIX E

Mount Modification Design Drawings (MDD)

1) INTRODUCTION

The mounting configuration consists of existing 12.5 ft Low Profile Platform.

2) ANALYSIS CRITERIA

Building Code:

2015 IBC, 2018 Connecticut State Building Code

TIA-222 Revision:

TIA-222-H

Risk Category:

П

Ultimate Wind Speed:

125 mph

Exposure Category:

С

Topographic Factor at Base:

1.0

Topographic Factor at Mount:

- 1.0

Ice Thickness:

0.75 in

Wind Speed with Ice:

Live Loading Wind Speed:

50 mph

Man Live Load at Mount Pipes:

30 mph 500 lb

Table 1 - Proposed Equipment Configuration

Elev	ation (ft)	VALUE OF THE	Antennas
Mount	Centerline	#	Name
		6	CommScope NHH-65C-R2B
		3	decibel (cci) DB854DG65ESX
140	140	1	rfs celwave DB-T1-6Z-8AB-0Z
		3	samsung telecommunications RFV01U-D1A
		3	samsung telecommunications RFV01U-D2A

3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

Document	Remarks	Reference	Source
Photos		_	CCISites
Mount Analysis	Kimley-Horn	8418942	CCISites

3.1) Analysis Method

RISA-3D (version 16.00), a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases.

A proprietary tool internally developed by Kimley-Horn and Associates, Inc. was used to calculate wind loading on all appurtenances, dishes and mount members for various load cases. Selected output from the analysis is included in Appendix B.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 *Tower Mount Analysis* (Revision B).

3.2) Assumptions

- The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
- 2) The configuration of antennas, mounts, and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
- 4) Steel grades have been assumed as follows, unless noted otherwise:

Channel, Solid Round, Angle, Plate	ASTM A36 (Gr. 36)
HSS (Rectangular)	ASTM A36 (Gr. 36)
Pipe	ASTM A53 (Gr. B-35)
Threaded Rods	ASTM A36 (Gr. 36)
Connection Bolts	ASTM A325

This analysis may be affected if any assumptions are not valid or have been made in error. Kimley-Horn should be notified to determine the effect on the structural integrity of the antenna mounting system.

4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity

Component	% Capacity	Pass / Fail
Connections	87%	Pass
Stand Off Horizontals	53%	Pass
Mount Pipes	39%	Pass
Corner Plates	39%	Pass
Face Horizontals	20%	Pass

	ng (max from all com	

Notes:

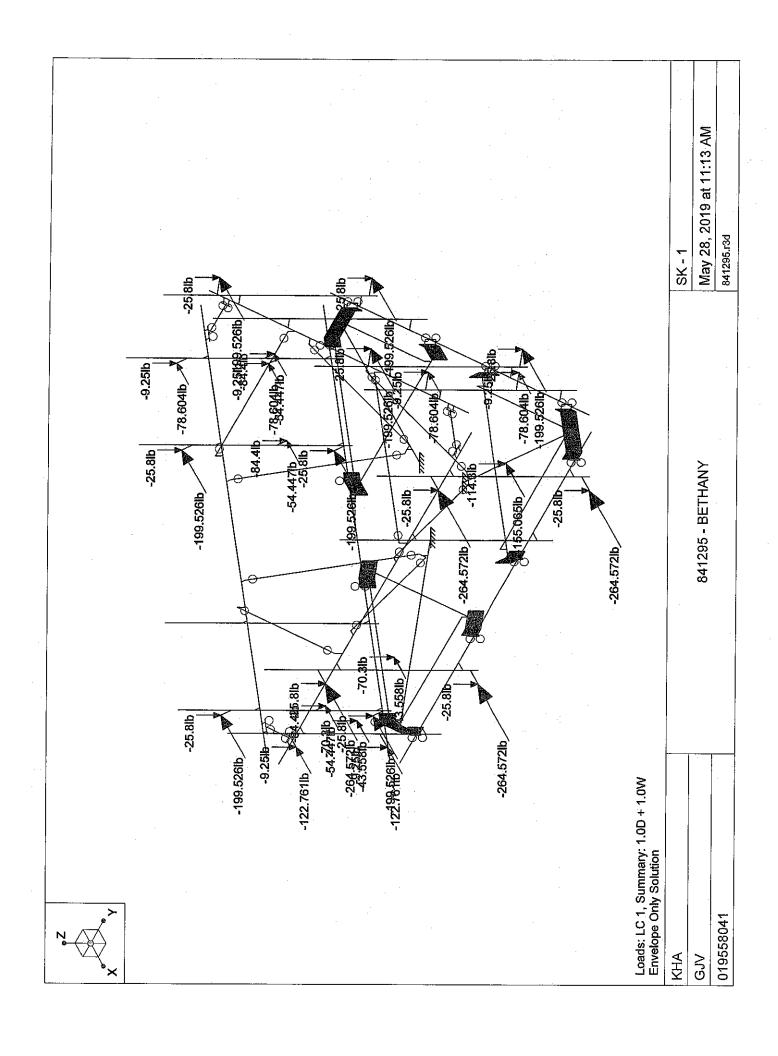
4.1) Recommendations

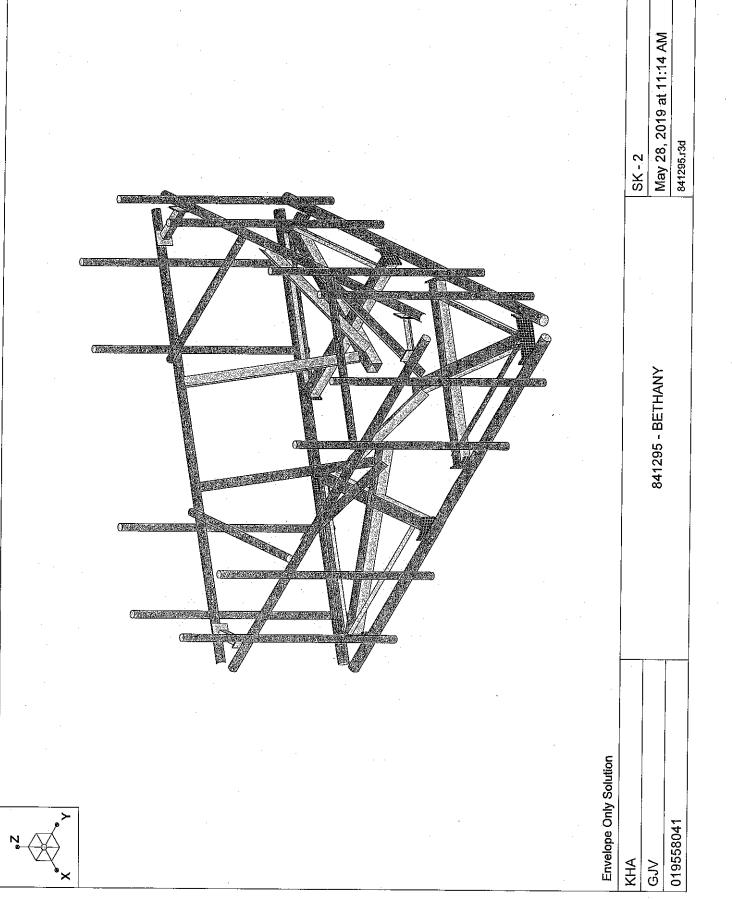
According to our structural analysis, the mounting configuration has been found to **PASS PENDING MODIFICATIONS**. The mounting configuration considered in this analysis will be capable of supporting the referenced loading pursuant to referenced standards once the referenced modifications are installed.

This analysis incorporates modifications per Kimley-Horn, dated 05/28/19.

¹⁾ See additional documentation in "Appendix C - Software Analysis Output" for calculations supporting the % capacity consumed.

APPENDIX A WIRE FRAME AND RENDERED MODELS





APPENDIX B SOFTWARE INPUT CALCULATIONS

General Criteria	
TIA Standard	ТН
IBC Edition	2015
Structure Class	-
Risk Category	11

Site-Specific Criteria	
Exposure Category	С
Topographic Factor, K ₂₁	1.00
Structure Base Elev: (AMSL), z _s (ft)	741.00
Ground Effect Factor, Ka	0.97

Mount & Structure Criter	ia, Si
Mount Elevation (AGL) (ft)	140.00
Structure Height (ft)	150.00
Structure Type M	onapale

Constants	
Wind Direction Probability Factor, Kd	0.95
Gust Effect Factor, Gh	1
Shielding Factor, K _a (antenna)	0.9
Shielding Factor, K _a (mount)	0.9

Wind Summary	
Basic Wind Speed w/o ice, V (mph)	125.00
Velocity Pressure Coeff., K _x	1.36
Velocity Pressure, q _z (w/o ice) (psf)	50.26

Ice Load Summary 2	
Basic Wind Speed w/ ice, V; (mph)	50,00
Design Ice Thick. (ASCE 7-10) , t _i (in)	0.75
Velocity Pressure, q _z (w/ ice) (psf)	8.04
Escalated Ice Thick, @ Mount, t _{iz} (in)	1.73

Seismic Load Summary	
Spectral Response (Short Periods), S.	•
Spectral Response (1-Sec. Period), S ₁	-
Site Class	•
Seismic Design Category	•
Seismic Risk Category	•

THE SAME REPORTED AND PROPERTY OF THE PROPERTY	200 Carrier 1
Snow Load Summary	
Principal parametric and a recipion of the	
Ground Snow Load, pg (psf)	
Snow Load on Flat Roofs, p _f (psf)	
anow Load on riat Roots, pf (pst)	

Kimley»Horn

Date	May 28, 2019	
Client	Crown Castle	
Site#	841295	
Site Name	BETHANY	
Project#	19558041	

Antenna Name	Ofv	Shanë	Dim	ensions	(in)	Weight				Joint	Labels				EPA	(ft²)	V	Vind For	ce, F _A (II	j),
		King to the	in H	W	n.	(lb)	ΔΙ	oha-	Tr. K. D.	eta	Gai		24				No	lce	Will	lce
NHH-65C-R2B	3	Flat	96	11.9	7.1	51.6	-	-	10000	Section 11 Contract 1		N1218B			11.39	7.66	529.14	355.69	400.00	-
NHH-65C-R2B	3	Flat	96	11.9	7.1							N1217B	. 0	<u> </u>	11.39	7.66	529.14	355.69	108.62	80.32
DB854DG85ESX	3	Flat	48	12.6	5.7				-			N1235B		<u> </u>	5.28	2.75	245,52	127.77		80.32
DB-T1-6Z-8AB-0Z	1	Flat	24	24	10		N1245B		n	0	Λ	0		1 0	2.4	2.13	111.51		52.56	32,6
RFV01U-D1A	2	Flat	15	15	10	84.4	0		N1251C	N1250C	n	1 0	0		0.94	1.25	43.56	92.92	23.37	22,91
RFV01U-D2A	2	Flat	15	15	8.1		N1245B			0	0		0		0.94	1.43		58,08	10.56	15.41
RFV01U-D1A	1	Flat	15	15	10	84.4	n	0	N1252A	<u> </u>	0	~		4		-	43.56	47.04	10.56	13.23
RFV01U-D2A	4	Flat	15	15	8.1		N1246B	-	0	-	u	u	<u> </u>	U	0.94	1.25	43.56 43.56	58.08 47.04	10.56	15.41

APPENDIX C SOFTWARE ANALYSIS OUTPUT



KHA GJV

: 019558041 : 841295 - BETHANY

May 28, 2019 11:12 AM Checked By: ZAM

Basic Load Cases

	BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(Me	Surface(P
1	Dead	DL			-1	25				June 30 (1
2	Dead of Ice	RL	C-Market St.	海流流流		25	4-1-4-1 N. 15 PART 1-1	51	10/4/2005	2012
4	Structure Wind (0)	None				7574 STATE		102		
5	Structure Wind (30)	None						102		
6	Structure Wind (45)	None	2 22 45 33 4	10 mm	and the state of the state of	AL NEED AND	25,888	102		100
7	Structure Wind (60)	None						102		
8	Structure Wind (90)	None	3.30 2.75 3		3260	A SWEET	2000年度	102		0.000
9 10	Structure Wind (120)	None	2 - 1/2/2019-44-2019-44-2017-4-2-17-17-17-17-17-17-17-17-17-17-17-17-17-	Carrylain Samorani Janese	Contract of Marie Burner	Superior same William and Superior		102		
	Structure Wind (135)	None						102		
11	Structure Wind (150) Structure Wind w/ Ice //	None	1-0-1-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0-0	The organization of the opening	at 300 solution of the contraction of	TOTAL CONTRACT CONTRACT CONTRACT		102		
	Structure Wind w/ Ice	<u>None</u>		and the second		ale returnist de	10.14	102	100000000000000000000000000000000000000	ade salah in
TATE AND THE TAX AND	Structure Wind w/ Ice	<u>None</u>	- CART POSESSES FOR EST C	Hode Hills and Assets	- A Service Loanes	Control Control		102		
2.00 to \$10.00 person	Structure Wind w/ Ice	None	1.54.74.554.94.	. May be specified	\$100 G5 \$140.	HAMPE FOR	50.55	102	34.57	
	Structure Wind w/ Ice	<u>None</u> None	crowlinaia yang kitan-	. Sagraturas versi vistos.	10000000000000000000000000000000000000	Control control (Section 1986)	. The season which is the reference	102	nami National Policina	
	Structure Wind w/ Ice	None		350000000000000000000000000000000000000				102		
	Structure Wind w/ Ice	None	1995 (Sept. 2015)		2000 Sept 2010 Sept 07	April Delegio Aleita (1985)	r (na resident skrivet skrivet fill	102	Elicitet viananiani	To The selection of the contract of the contra
	Structure Wind w/ Ice	None	1.60%			NEW TOTAL PROPERTY.	13.1 (A. F.) (A. F.)	102	and the second second	5.72
	Antenna Wind (0)	None	Per per general	Transcolution of the second		50		102	Potential constant	1.010.00-0.000.000.000
	Antenna Wind (30)	None	,,3e(1,500),223,5(045,005,0	vage balenter blev		50 50		246044,610.		
	Antenna Wind (45)	None	37.5	760 F6 56544	160 (400)	50	Persenti de Sand	5/15/6/35/6/42/eVc		A SEA WATER
	Antenna Wind (60)	None	355.0 21.00 (1.00	54474751 3350 Jets 1830 ₉ 6		50 50		3107 a2WE 1921	(%C+2054XX)	
	Antenna Wind (90)	None	(17A) (4.09)	V3890 502002	THE PART OF A CO.	50	est of participa	Consumation (ngweid pilasiki	POPER SENSION
25	Antenna Wind (120)	None	P. Albert St. Species	<u> </u>	And the little for the second section of the second	50		Print Markethia	sala aske regist all	and services receive
26	Antenna Wind (135)	None	All and the Board	- Car-, meres 2,000 mm; - Na - Or Car (Albinosia	(4) (4) (7) (7) (4) (4) (6) (7) (7) (7) (7) (7) (7) (7) (7) (7) (7	50	STATE			3802233
27	Antenna Wind (150)	None		a repair of the college of the	5 400 + 3r, 2400 + 1552 ()	50	ACCUMENTATION OF STREET	SAMORETE RESTORATE.	Openio de la Proposició	3205-301 - 602 - 604-45-4
	Antenna Wind w/ Ice (None	ANALOS ESTA		7	50	YS STORWAY		STATISHED STATE	VARANCE II
	Antenna Wind w/ Ice (None				50	A CAS A CONTRACTOR OF SALES	and the second of the second of	ALA TOSTI YALA YA S	Security Annual Control
	Antenna Wind w/ Ice (None	244.770 (14V.34)		12 c. 12	50	or green, cardenises in	1878 (498) 1880	28-17 (EEF 7 175) (FIRE	(attack - (2014-222)
	Antenna Wind w/ Ice (None				50		Turk Angelon Art (great and the Art (great	A LACON BY A CONTRACT OF A STA	- 24/34/14/14/20/20/20/20/20/20/20/20/20/20/20/20/20/
	Antenna Wind w/ Ice (None	E-100 E-100		WAR AND	50	SAN SAN SAN SAN			
	Antenna Wind w/ Ice (None				50		2007	in and a property of	Althornoon Selection
	Antenna Wind w/ Ice (None	SANDYANG QUERTS	LANGE OF STREET		50 🐼	1.0000000	ARI ANTAL	STATISTICS.	1 (A. 18 A.)
	Antenna Wind w/ Ice (None				50			2000 - 1, manager 20	
	Maintenance Live Lm	OL1				777		2-900-20-30-00-0	o an india paragraphi	\$1.500 dogs \$6.60
	Maintenance Live Lm	OL2				1				A - 12 - 18 - 14 - 15 - 15 - 15 - 15 - 15 - 15 - 15
	Vlaintenance Live Lm	OL3		AAAA AAAAA	100 CO 10	1				
39	Maintenance Live Lm	OL4				1				

Load Combinations

	DescriptiSo	PDelta	S	BLC	Fac.	.BLC	Fac.	.BLC	Fac.	.BLC	Fac.	BLC	Fac.	.BLC	Eac	BI C	Eac	BLC	:Fac	BL C	Fac	BLC	Fac.
1	Summar Yes	Υ		DL	1	20	1	1.		Ī			1		1 40.		T		1 00.	<u></u>	<u> </u>		71 ac
2	1.4D Yes	Y		DL	1.4	W.			1000			450	(100 c) (100 c)	198	1833	1838	10000	7800	4.4	345 PE	- 1857 (S)	4600	2000
3	1.2D + 1Yes	Υ	٠.	DL	1.2	4	1	20	1							-			10, 000,00	1 2547 (12	3-2002E-012-2	7048-1	12.15.15.15.
4	1.2D + 1 Yes	Ý		DL	1.2	5	1	21	1		07/2020	475		1985	18/19/2	1994	5700	-3(3)	1980A	1939992	2 2 61 L	HW.	304
5_	1.2D + 1Yes	Υ	Ι	DL	1.2	6	1	22	1								- 340 / 543 / .			3,3%%	- X-2-04-15	41-51, 11	41.1549
6	1.2D + 1Yes	Υ		DL	1.2	7		23	1	72.00	#FE	1482		2 2-116 2 3-35	WAS:		-3593	300	. (Especial) Const.	13.13	1.00	423	578.0X
7	1.2D + 1Yes	Υ		DL	1.2	8	1	24	1					3-22-0	100, 100, 10, 10, 10	1 10000	27.0000	10000	3,00,00	101 17.81	2.500.00000	AGRESTATION OF	2,3,54,50
8	1.2D + 1Yes	Y		DL	1.2	9	2.1	25	1		100	500		8 7 KB	10,372	1237	ana.	4553	17 H 20	300	18574	NG NEW	NOW.
9	1.2D + 1Yes	Υ		DL	1.2	10	1	26	1					.9			20-27-02-	-23.1.25	78,85,95,83	72 N° 5	2 (4/4) 5	F APPORT	100,120.7
10	1.2D + 1Yes	Υ	16.70°	DL	1.2	11	1	27	1	192	2000	\$2.0,5°	N. A.	124/4	1882	197	5000	3000	\$1.000	225128	VIVO	11 10 10 10 10 10 10 10 10 10 10 10 10 1	-7/A/2/A
11	1.2D + 1 Yes	Υ		DL	1.2	4	-1	20	-1					N S AL	2.55.5.2		1000000	200,20	Ağreyre e	24.005.5	, NAS-1	moto.	200
12	1.2D + 1Yes	Υ		DL	1.2	5	X 9 6	21	41	LES!		200		V.	A STATE	49.0	10.00		60.29	: 60K	ineralië Ngavaji		223
13	1.2D + 1Yes	Υ		DL	1.2	6	-1	22	-1		4.040.00	20.00 (0)	r ya Marga			4.5,550	12) 129749	Seat Self.	73.73 J.	955,319	11996	ONORANI	3,5,950,64.78



: KHA : GJV : 019558041 : 841295 - BETHANY May 28, 2019 11:12 AM Checked By: ZAM

Load Combinations (Continued)

LOAG COMDINA	itions (Com	mu	cu/																		
Descripti So.	T	S	BLCF	cBL	CFac	BL(CFac	BLC	Fac.	.BLC	CFac.	.BLC	Fac.	.BLC	Fac.	BLC	Fac	BLC	Fac.	BLC	Fac
14 1.2D + 1 Yes	Y		DL 1									18.00			100	1		W.			
15 1.2D + 1 Yes	Y	1	DL 1	.2 8	-1	24	-1			T						1	1				
16 1.2D + 1 Yes	Y	V (1869)	DL 1			25			1 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1	12.5%	1 2 2	20.30	1957 T.A.S.	955,5	100		37.72	1000	7.76	200	
17 1.2D + 1Yes	Y		DL 1			26		1			T					1,7,7	1		- CHIERO MITTERS	100.00	The works
18 1.2D + 1 Yes	Y	100	DL 1		20 21 22 2	94 27 2 2 7 2	N	100	15.73	. 12	100	3.3	2.6	7576	10.50	337	1000	186	24.42	25.25	10.3%
19 1.2D + 1Yes	Y		DL 1			12		28	1	2-51(2)	SQ 1000/100100		2000,000,00	Spirit Char	17740.75,6790.	, PART 197 (A	61.62.450a.66	F-96447-80	TARRA PERM	30000773	1
20 1.2D + 1Yes		1382	DL 1			13		29		755	V 5550455	12/00/20	1900	25/62	100000	10000		FARSK.	03.63	20.5	0,00000
21 1.2D + 1Yes	.,,,,	200000		2 RI		14		30	1	0,6056	Tacket ent	1.64350	of Franks	C28/4824	APRIL DE	0.500		\$1,50gg	1990	C56(45)	1993/9/201
22 1.2D + 1 Yes		1 1900 1900	DL 1			15		31		285696	588030	35785	Constitution States	96.00	visits i de	- ONE DE	25/19/65/	2000	2.98(64.30)	10E0)E4	A 1820 120
23 1.2D + 1 Yes		1004350	DL 1							10000	19/2/99/3	1400	3808	7505	14600	100	5446	1986	J. 200 (C.	244	1076076
24 1.2D + 1 Yes		(Siz./4)	DL 1			16 17		32	1	146474	1923	ESWEET.	17947 o Novê	100016	533	1850-1939 1850-1939	-67-3300	100037	0.296741	Act (100)	extent/40824
25 1.2D + 1Yes	**************************************	(236)64						33		3440504	S BARRIO	\$14(\$)\$4	300,000	440.00	13660	18/260	ેંદ્રાસર્જિસ્	2000	19,9FE)	a Est	1 NO.55
26 1:2D + 1Yes		G 846	DL 1.	2 RI		18		34	1	1000	201 N	(A)44.5	J85-34857	7 842 N. K.C.	1489 82,561	. Needs	1.000000	100	55A-7455	Alterial Control	
		13000)	DL 1.					35		1000	1200	39.90	38 Q	3623	Vorting.		30000	25	15000	2,500	W 1998
Control of make a factor at the control of the		0.00	DL 1.			12		28	-1	0.000	and the second	W201580	-cc.752 253	COTOLY F	11. Sec 18.4 (42.	5527W6	St. N. Strane	o negration	130507555	. no.235.4	State Company of
28 1.2D + 1 Yes		(0.00)	<u>DL 1.</u>			13		39			2024		32.74(9)					Jack.			
29 1.2D + 1Yes		12.00.00	DL 1.			14		30	-1	arani la ze	F 18,117 1 1 17	2 394 3			r tarurus.						
30 1.2D + 1 Yes		7/8	DL 1.			15		31	-1			3.00	13 7 3 A	NEW Y		7.54		All A	45.00		245
31 1.2D + 1Yes	Y	10001111	DL 1.			16		32	1_					L		L					
32 1.2D + 1 Yes		200	DL 1.	<u> 2 RL</u>	- W	17	-1	33	•1	N.A.	30 m	A.V	4 AND				343.4				
33 1.2D + 1Yes	Υ			2 RL	. 1	18		34		<u></u>									j		
34 1.2D + 1 Yes	Υ		DL 1.	2 RL	*1 \$	19	*1	35	-1	100	300		2 (1) (1) (1) (1) (1) (1) (1) (1) (1) (1)					3		2.15	100
35 1.2D + 1 Yes	Y		DL 1.	2 4	.058	20	.058	OL1	1.5												
36 1.2D + 1Yes	Υ		DL 1.	2 5	.058	21	.058	OL1	1.5	会党						-61480	<u> </u>	35 (52 (32)	035943 155.55	3 Elece	Colorbandos.
37 1.2D + 1Yes	Y		DL 1.												(455.5.			- 2000	.,	2.51.87	34.55.
38 1.2D + 1Yes	Υ	3.2	DL 1.				.058			223	5365		A CONTRACTOR	1866	100 TA	7E.	100	28	1000	100	378374
39 1.2D + 1Yes	Υ		DL 1.				.058			-	0000000	5,0,04.			45. 90	50.000,000	7,900,000,00	227.5	ADMINIST N	26.8.50	2176041,361
40 1.2D + 1Yes	Ý	1.0000 454	DL 1.				.058			(A)(25)	12000	OUS.	Walds.	43.5	9898	(85%)	ENAN.	5.653	152455	3035	5255
41 1.2D + 1Yes	V		DL 1.							Belonda		240,400	Part No.	(9)(9)(9)	2009000	7,11,95,00	357555	1,400,54	14. April 2003	2.529	1907 St. 62
42 1.2D + 1Yes	v v		DL 1		.058					75	380008	S9 84	3077	\$857	9.74799.8	77.75	341554	1256	1,887.57	1,3586	7733638
43 1.2D + 1Yes	V		DL 1.		058					dirigants	of the second	F86.62	094-00	Heigh	Mesega.	addig jar	TEN SEC	24.89	407437	4837	1000 64
44 1.2D + 1Yes	Alegerial Value (Alegeria		DL 1.		058					\$80 x 1	Merchang.	494S	12.00 Miles	1950/26	A NUMBER ONE DOOR	A 994.1	5-1-2-2 5-1-2-2	Gode.	Apply146	NO.56	314547
45 1.2D + 1Yes	<u></u>		DL 1.		058					1445-6	. 3. (12/1/9)	<u> (206)</u>	18.4	10 A	diserce (A)	- 100A	BEATER.	3.753	Greek.	aleste.	Martine,
46 1.2D + 1Yes	J V	$\overline{}$	DL 1.							4852.	AN (1974)	१९७५	Sec. 5.	- €e.u	24673333	wes2784.	aCate 5	20356	10000000		19805.00
47 1.2D + 1Yes	**************************************				058					\$2930v	3500	473475		1000	A \$155.74	25.5		¥46		14754	<u> </u>
48 1.2D + 1Yes	Tanan saran zaran 1974		DL 1.		058					13 w love 19	- 6350 g.m.	1550133	2031/89E	Selface N	6 000,000	13.Gutt.24.	- 40-64-61a-4		Allen Salte	280.00	10 C C C C C C C C C C C C C C C C C C C
	<u> </u>		DL 1.		058					\$4.50	JAMES.	945		992	2243	Allak.		7234	941%		10000
	ASSESSMENT OF THE SEC.	200 000	DL 1.	2 10	058	26	058	ULT	1.5	Cod Service	1.89.15900	25,340 32	rich co	F. 100 TH. 10	22879 270	SUNCE NO.	. Salasser	20.50	757 277-		72 000 000
50 1.2D + 1Yes	**** Y *****		DL 1.		.058					100		34.6		A.J.	2.00	102.5V	100	1000	1000	(3-1)	
51 1.2D + 1Yes	Y.	100	DL 1.:		.058					7410,000	A 11 .00				s Andrews		275 88 1				
52 1.2D + 1 Yes	<u> </u>		DL 1.		.058					28.5	1200	36.	A Sta	-334			A Comment		94. VA	1428 A	18690
53 1.2D + 1Yes	Υ		DL 1.		.058				1.5												
54 1.2D + 1 Yes	Y		DL 1.				.058		1.5		80 Trans.	337	漢語	120		\$3.55 \$4.55	32492	Fig.	4.25		
55 1.2D + 1 Yes	Y		DL 1.																		
56 1.2D + 1Yes			DL 1.								Market Comment		13 m m st			1945 1942 1942			1,129% 2000		1468.29
57 1.2D + 1 Yes	Y		DL 1.2							.]											
58 1.2D + 1 Yes	Υ		DL 1.2							報源	25 A	100 A	A-6-14	EXP	SASS.	1,025 4,166,0	V-20-55	24.7	* 1		(A)
_59 1.2D + 1 Yes	Y		DL 1.2	2 4	058	20	058	OL2	1.5												
60 1.2D + 1 Yes	Y	24.4	DL 1.2	2 5	058	21	058	OL2	1.5	M. C	(4) (4X	TAK.	SEC. 1	44		3/%	7. 7. 1 E	**************************************	TNY.	250	
_61 1.2D + 1 Yes	Υ		DL 1.2	2 6	058																
62 1.2D + 1Yes	Ŷ	1997	DL 1.2	7	058	23	058	OL2	1.5	15	200	<u> </u>	15 V.		1.0000000 1.000000000000000000000000000	y/s/A/	317.63		7 - Age - 1	361	
63 1.2D + 1 Yes	Υ		DL 1.2															× 2 11 1			
64 1.2D + 1Yes	Ý		DL 1.2							4 .7 -3x 71	The state of	20			Sign and	2007 J. J. S.		# Z 13	11.00 p		<u> </u>
65 1.2D + 1Yes	Ÿ		DL 1.2							24502.54	o Car Miggel ()	12.07 TOP	Method Cont	05164	5.5 (2005)51 (SCAN SECTION	m bestilier y	<u> </u>	1794-351,57	10ga/A 11	description
66 1.2D + 1Yes	Ý	3% i	OL 1.2	111	. 058	27	.058	01.2	1.5	187	30M0	96 J	332	,	Çeçey ,	ş (25)	12000	77	- CONT	- Carl	90 (200 mg 200 (200 mg
67 1.2D + 1Yes	Y		DL 1.2							S. Joseph	1,4 (w.80)	1.00 E	38/3/4/3	est of a la	447W	See Syring .	us misel i	200	1,40,435	1000	<u> 1988-9</u>
68 1.2D + 1Yes	Ÿ	[] [] (((()))	DL 1.2	. 4	UKS.	20	050	OI 3	1.0 1 E	3538	5,65,74	9086	135955 F	96 25 2	\$4580X 14	98,950	w n ján .	36/5/5/5/2	1.590	25050 S	Sec. 25.1
69 1.2D + 1Yes	Y										AN TANK	494	335		<u> </u>	Mag.	sa Sa S	3 (F)			36%).
			<u>DL 1.2</u>	(b	0.00	22	.000	OLO	1.5	33800	y 200 a a		100,8115	Constitution in	esergar .	r in gast			J-Q/2 T/F F	V-3-1-1-1-1	(21/24/14)
70 1.2D + 1 Yes	Y	(A)	DL 1.2	47	.058	23	.บ58	UL3	1.5	200	5,44						(基本) (1 (表本) (3				Contraction Survivorse



KHA GJV

019558041 841295 - BETHANY

May 28, 2019 11:12 AM Checked By: ZAM

Load Combinations (Continued)

	Descripti		. PDelta	S	BLC	Fac.	BLC	Fac.	BLO	CFac.	BLC	Fac.	.BLC	Fac	BLC	Fac.	BLC	Fac	BLC	Fac.	BLC	Fac.	BLC	Fac.
	1.2D + 1				DL	1.2	8	.058	24	.058	OL3	1.5												
	1.2D + 1				DL	1.2	9	,058	25	.058	OL3	1.5		4	4900	2.2			438	分的	3/4	24730		1,046,4
	1.2D + 1				DL	1.2	10	.058	26	.058	OL3	1.5											· .	
74	1.2D + 1	Yes	γ		DL	1.2	11	.058	27	.058	OL3	1.5	14.	· 1000000000000000000000000000000000000	3.5		1000	440	300			97.16	100	
75	1.2D + 1	Yes	Υ		DL	1.2	4	058	20	058	OL3	1.5	1					1			1			
76	1.2D + 1	Yes	Υ		DL	1.2	5	058	21	-,058	OL3	1.5	1	Salas.	4.3	10.14				3.0	製造	Shirt.	4	
	1.2D + 1				DL	1.2	6	058	22	058	OL3	1.5							Ī					
78	1.2D + 1	Yes	Υ		DL	1.2	7	058	23	058	OL3	1.5	12.0		2000 E	沙湾	X2007			1000		100000	(B)	N/S
	1.2D + 1		Υ		DL	1.2	8	058	24	058	OL3	1.5			-									
	1.2D + 1			29	DL	1.2	9	058	25	058	OL3	1.5		1.70	3.2	AND AND			18	100 (C. 10)	激烈	303A(0)	100	All Glasses
	1.2D + 1		Υ		DL	1.2	10	058	26	058	OL3	1.5					<u> </u>							
	1.2D + 1		Υ		DL	1.2	11	058	27	058	OL3	1.5	348				A.V	7.4 W.		10 M	10.00	杨婧		30 EU/C
	1.2D + 1				DL	1.2	4	.058	20	.058	OL4	1.5												
	1.2D + 1		Y -	2.8	DL	1.2	5	.058	21	.058	OL4	1.5		100	整裝	海湾	25%		100	V\$3000	N/W	思德		1000
	1.2D + 1		Υ	L	DL	1.2	6	.058	22	058	OL4	1.5											- 1	
	1.2D + 1	Yes	* Y	重整			7	.058	23	.058	OL4	1.5	7 to 1		WAY 25	15975B	WEEK!			A TABURY	思维这 语版		·强制的:	
	1.2D + 1		Y		DL	1.2	8	.058	24	.058	OL4	1.5												
	1.2D + 1		Y	3.5	DL	1.2	9	,058	25	.058	OL4	1.5	源蒙		2.5	1111		-246-54 (Albert	· 多等等	A STANCES	裁算		NG SERVICE SERVICES	COLUMN TO SERVICE
	1.2D + 1		<u> </u>		DL	1.2	10	.058	26	.058	OL4	1,5	-											\Box
90	1.2D + 1	Yes	Y - Ja	5348	DL	1.2	11	.058	27	.058	OL4	1.5	1783	38.Ex	9.49	. S. Z.			3000	243		溢款		
	1.2D + 1		Y		DL	1.2	4	058	20	058	OL4	1.5												
	1.2D + 1		Υ		DL	1.2	5	058	21	058	OL4	1.5					模数				變變	TANK!		350000 (16) 2. 10 (16)
	1.2D + 1		Y		DL	1.2	6	058	22	058	OL4	1.5												
	1.2D + 1		Υ		DL					058					200	V.	200		1000	20/200 52/49/20	92.07 9.06		100 A 100 A	1 1 (10 A)
	1.2D + 1		Υ Υ							058														
	1.2D + 1		Y 48 10 10		DL	1.2	9	-,058	25	058	OL4	1.5	ereg.	2000	13.4		e e	5.64	3.33	基度	(L)	(4)	1000	An Call
	1.2D + 1		Υ		DL	1.2	10	058	26	058	OL4	1.5												
98	1.2D + 1	Yes	Υ	38	DL	1.2	11	058	27	058	OL4	1.5		18 X	1818	19.0		2.70	400	100			78 V	300

Hot Rolled Steel Properties

	Label	E [ksi]	G [ksi]	Nυ	Therm (\1E.,	.Densitv[k/ft	Yield[ksi]	Rv	Fuľksil	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	111
3	A992	29000	11154	<i>.</i> 3	.65	.49	50	1.1	65	1.1
4	A500 Gr.B RND	29000	11154	39.34	.65	.527	42	1.4	58	1.3
5_	A500 Gr.B Rect	29000	11154	.3	.65	.527	46	1.4	58	1.3
-6	A53 Gr.B	29000	11154	.3	.65	.49	35	1.6	60	1.2
7_	A1085	29000	11154	.3	.65	.49	50	1.4	65	1.3

Hot Rolled Steel Section Sets

	the second secon									
	<u>Label</u>	Shape	Туре	Design List	Material	Design Rules	A [in2]	lvv [in4]	Izz [in4]	J fin41
1	Platform Horzont	PIPE 3.0	Beam	Pipe	A53 Gr.B	Typical	2.07	2.85	2.85	5.69
2	Offsett Tube	HSS4x4x4	Beam	SquareTube	A36 Gr.36		3.37	7.8	7.8	12.8
3	Offset Side Plate	0.38 X 6 Pla	Beam	RECT	A36 Gr.36		2.28	.027	6.84	.105
4	Grating Angle	L2x2x3	Beam	Single Angle			.722	.271	271	.009
_ 5	Mount Pipe	PIPE 2.0	Beam	Pipe	A53 Gr.B	Typical	1.02	.627	.627	1.25
6	Offset End Plate	0.5 x 6 Plate	Beam	RECT	A36 Gr.36	Typical	3	.063	9	.237
7	MOD HRK12-3HD	PIPE 2.5	Beam	Pipe	A53 Gr.B	Typical	1.61	1.45	1.45	2.89
8	MOD HRK12-3H	0.38 X 6 Pla	Beam	RECT	A36 Gr.36		2.28	.027	6.84	.105
9	MOD HRK12-3H	L2.5x2.5x4	Beam	Single Angle			1.19	.692	.692	.026
10	MOD HRK12-3H	PIPE 2.0	Beam	Pipe	A53 Gr.B	Typical	1.02	.627	627	1.25
11	MOD HSRK-35	L3x3x4	Beam	Pipe	A36 Gr.36		1.44	1.23	1,23	.031

: KHA : GJV r : 01955804

: 019558041 : 841295 - BETHANY May 28, 2019 11:12 AM Checked By: ZAM

Hot Rolled Steel Design Parameters

	Label	Shape	Lenath[in	Lbyv[in]	I baatin1	Leanen teutin	11 1: (17.1					
1	M51	Offsett Tube	63.007	LOYYINI	Lbzz[in]	Lcomp toplin	lLcomp bot <u>lin</u>	L-torqu.	<u>Куу</u> Т	<u>Kzz</u>	<u>Cb</u>	Function
2	M60	Offsett Tube		(a) 100 (a) (b)	1 5 5 6 7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	Lbyy	TANTHAN STREET	Programme	1983 D.S. 1984 1985 January	40 FV-20	301/86-001/8	Lateral Lateral
3	M63	Offsett Tube	30.437	A CANADA SECURITION OF SECURITION	1 200 / 200 / 200 / 200	Lbyy		144654028344	S. C.	100000000000000000000000000000000000000		Lateral
4	M69	Platform Ho	150	A COMMITTEE OF THE		Lbyy			1000			Lateral
5	M72	Platform Ho	150			Lbyy	CARRIE OF SPECIAL SPEC	PACIFICATION CONTRACTOR OF	L'Araba Disastrati	1 5 5 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	-cuantidas entilenera	Lateral
6	M75	Platform Ho		Section 2	13474848	Lbyy	563 3 2 2	6550	52,400	15 CV 61	支撑 液	Läteral
_ 7	M92	Grating Angle	50.542			Lbyy						Lateral
8	M94	Grating Angle	50.542			Lbyy		01500	Market of	120 (F) (S)		Lateral
9	M98	Grating Angle	50,542			Lbyy						Lateral
10	M100	Grating Angle	50.542			Lbyy					The Control of	Lateral
11	M104	Grating Angle	50.542	Charten of VIII server and	New State Court Accompany	Lbyy	January Constitution	Consultation considers	T v. 92.11 on 21.44			Lateral
13	M106 M160	Grating Angle Mount Pipe		15 (10) (4 mg/s)	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Lbyy.	German 1992	AW 364	A AND		36.0	Lateral
14	M161	Mount Pipe	84 84		78, Kondo S. W. W.	Lbyy	VERTICAL POLICIA (IL DESCRIPTIONES)	- 1914 A. C.	- KANTALOW-ANDA	A SSOROMER ASSOCIA	vest viz By chem to	Lateral
15	M162	Mount Pipe	84			Lbyy		#75 (V2)				Lateral
16	M163	Mount Pipe	84 84	5976945495559659	- 1786 107 F05 FURTHER	Lbyy	1948 E. 2010 S. Avez - Mark	- Wholeski Danski	av veggenetatie	V095630,055,956,9	13.5° (3.10) (2.5° (3.46) (3.46)	Lateral
17	M245A	Offsett Tube	30 438			Lbyy Lbyy	- XV (Ex 0 - 10 / 64, 643)	50 Sa 55 s	A CHIP WAS IN CO.	94-0876 Per 446-14	AND STREET	Lateral
18	M246A	Offsett Tube	30.437	n od School (ed) a Nago, nije abserv		Lbyy		91 Y C S 3 3 5 5 7	10,200,000	10.37625768	i . Statista Malak	Lateral Lateral
19	M279	Offsett Tube	30.438		1998 (1995) E 174 (2000) N 2000) 198	Lbyy	APPENDING TO A STATE OF THE STA		TO SHEET STATES	PARTO ASSESSE	1500 W 1800 S 1800	Lateral
20	M280	Offsett Tube	30.437	70.00		Lbyy		MATO SE	365032.56	VECTOR 689	100000000000000000000000000000000000000	Lateral
21	M242A	Offsett Tube	63.007		- 10 April 244 - 7 C200022 \$40 A-6	HOSENIA Y Y JOURNA		3256 Mart 186, 1364		(1) (2) (2) (2) (2) (2) (2) (2) (2) (2) (2	SECTION STATES	Lateral
22	M243A	Offsett Tube	63.007	317777	SENTENCE CONTROL OF	and the state of the second	refrost velocitations	Cyconec Coleman	46600	988 988 9	19 A 19 C 10 C	Lateral
23	M232A	Mount Pipe	84			Lbyy	**************************************	10.49 (A. C. N. A. A. C. DA. (B.)	green fan 'n fanke oppe	1 7.07 (Mg/Pa	-96g200 (5000 V60g0)	Lateral
24	M233A	Mount Pipe	84	化氯化甲烷 矿石		Lbýý		Name to ser		200		Lateral
25	M234A	Mount Pipe	84			Lbyy						Lateral
26	M235A	Mount Pipe	84	A. 1. 3 1/1/20	reinfaller er s	Lbyy		以形成数 :	2137.10°.17	(s.C.) (3) (s.)	914	Lateral
27	M240A	Mount Pipe	84			Lbyy						Lateral
28	M241A	Mount Pipe	84	3 8 8 3 4		Lbyy	Christian Control					Lateral
29	M242B	Mount Pipe	84	- No. Co. Co. Co. Co. Co. Co. Co. Co. Co. C	Mill Mariana (N.) Strik (M. 1971)	Lbyy	Action of the section of the section					Lateral
30 31	M243B M272A	Mount Pipe MOD HRK1	84			Lbyy		(0.00 pg	9.000 mm.			Lateral
32	M275A	MOD HRK1	150	Section Wilder Section		Lbyy	Samuel Committee 7	San	SALSAV KOOMBO			Lateral
33	M278A	MOD HRK1	5	4) C (SM45/AA)		Lbyy	CANNAGE STATE	NAC M	\$40.5576	12,745		Lateral
34	M283A	MOD HRK1,	5 150	Transactions for the Cold		Lbyy	Attación objeto de desemble	Sirkitus susian n	ere en	amenational v		Lateral
35	M286A	MOD HRK1	5	(#. 868-375-31-35-1-35-1-35-1-35-1-35-1-35-1-35		Lbyy	NGASO KODA KOMA		623 (834)			Lateral
36	M289A	MOD HRK1	5	A VANCOLANCE OF	finestale vestioner s	Lbyy Lbyy	(95,453) (36,554,435)	Military State C	9970999865 C	00000155000		Lateral
37	M294A	MOD HRK1,	150	17 (972) Sept. Charles		Lbyy	<u> </u>			RESERVED, IET		Lateral Lateral
38	M297A	MOD HRK1	5			Lbyy			view Car	150 9000		Lateral
39		MOD HRK1	5		on, E. Live Cape Conserved. U.S.	Lbyy	62 80 2000 pt 1000 1000 25 42 45 1000 pt 123	175,000,000 V.Bha-A. 10	several con L	400000000000000000000000000000000000000		Lateral
40	M301B	MOD HRK1,	13.155	and and a	and discount	Lbyy	6.200.000		* 31/25			Lateral
41	M302B	MOD HRK1	13.155			Lbyy				2, 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1 - 1		Lateral
42	M303B	MOD HRK1	13.155		7 to 10 to 1	Lbyy	480 X 241 340 198 4 241 -				Control or an experience of	Lateral
43	M310B	MOD HRK1	56.619			Lbyy		1,565		2 14 HO MARK TO		Lateral
44	M311B	MOD HRK1	56.619			Lbyy	ARTEN SA ST SE					Lateral
45	M312B	MOD HRK1	<u>56.619</u>			Lbyy			•			Lateral
46	M320	MOD HSRK	56.759	Paragonia da Santes es		Lbyy		ACK S	<u> </u>			Lateral
47	M322	MOD HSRK	56.759	aga desagag desagan seria		Lbyy						Lateral
48	M324	MOD HSRK	56.759			Lbyy				77/70/45 V		Lateral
49	M326	MOD HSRK	56,759	Penduksa Sarah Maraja Sarah	Annies of march theory of a 11	_ Lbyy	Santa	for relief to the				Lateral
50	M328	MOD HSRK.	56.759		Andrew Wester	Lbyy	4120-440 (442-13474)					Lateral
51	M330	MOD HSRK (06./59	•		Lbyy					. 1	ateral

: KHA : GJV : 019558041 : 841295 - BETHANY May 28, 2019 11:12 AM Checked By: ZAM

Envelope Joint Reactions

	Joint		X [lb]	LĊ	[dl] Y	LĊ	Z fibī	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [[b-ft].	LC
1	N88	max	2363.215	3	1743.592		2895.693	19			6207.49	3	1496.137	7
2		min	<u>-3253.827</u>	11	-1745.306	7	-721.106	11	-2327.94	15	-4303.569	11	-1524.983	15
3	N1203B	C. Committee of the Association	2233.289	T-1 - 1 - 1 - 1	2012.2	14			3419.442	6	2606.576	4	1680.908	18
4	Control (Tapper Control)	min	<u>-1769.594</u>	59 S (c)	-2775.58	6	-485.694	6	-5675.354	14	-3951.803	12	-1697,422	10
5	N1205B	MATERIAL CONTRACTOR	1897.733	_3_	2874.979				5291.557		2625.067		1653.475	
<u>6</u>	A MALAS GARAGE		-1470.811	11	-2108.08	8	-761.717	16	-3815.503	16	-3678,112	10	-1657.214	4
7	<u>Totals:</u>		6494.237	3	6464.203	15		20						
8		min	<u>-6494.233</u>	11	-6464.239	7	2355,688	1						2000

Envelope AISC 14th(360-10): LRFD Steel Code Checks

	Member	Shape	Code Check	Loclin	LC	Shear Che	LoclinID	irl C	nhi*Pnc	nhi*Pnt	nhi*Mn	nhi*Mn	Cb Ean
1	M242A	HSS4x4x4	.532	0	14	.271	0 z	10	99760.9.	10918	12663	12663	
2	M243A	HSS4x4x4	, 508	0	8	278	0 2	12	99760.9.	10918	12663		2. H1-1b
3	M51	HSS4x4x4	.508	0	3	.276	0 z	15	99760.9.	.10918	12663	12663	
4	M240A	PIPE 2.0	.391	77,368	12	.075	28.7,		17855.0.			1871.62	52. H1-1b
5	M160	PIPE 2.0	.380	77,368	7	075	28.7	16			1871.625		
6	M161	PIPE 2.0	.365	77.368	15	062	77.3.	17					2 H1-1b
7	M232A	PIPE 2.0	.360	77.368	18	.075	28.7	11	17855.0.		1871.625		
8	M241A		.352	77.368	4	.059	77.3	6	17855.0.				2H1-1b
9	M233A	PIPE 2.0	.346	77.368	9	.058	77.3	11	17855.0.				2 H1-1b
10	M243B	PIPE 2.0	.301	77.368	13	.073	77.3	14	17855.0.				2H1-1b
11	M163	PIPE 2.0	.300	77.368	8	.075	77.3	9	17855,0.				2H1-1b
12	M162	PIPE 2.0	.290	77.368	14	.075	28.7	6	17855,0.				2H1-1b
13	M235A	PIPE 2.0	.289	77.368	3	.075	77.3		17855.0.				2H1-1b
14	M294A	PIPE 2.5	.276	47.368	11	.146	55,2.,.	9	14558.7.				2H1-1b
15	M245A	HSS4x4x4	.276	30.438	13	.100	3.204 Z	-		109188		12663	1H1-1b
<u>1</u> 6	M272A	PIPE 2.5	.272	47.368	6	.151	55.2	4	14558.7.				2H1-1b
_17	M242B	PIPE 2.0	.267	77.368	3	.075	28.7	. 11	17855.0.		1871.625		
18	M283A	PIPE 2.5	.266	47.368	16	.146	55.2	15	14558.7.				2H1-1b
_19	M246A	HSS4x4x4	.264	0	15	.095	27.2 z		106911				1H1-1b
20	M60	HSS4x4x4	.263	30.438	18	.094		8	106911			12663	1H1-1b
21	M279	HSS4x4x4	:258	_30,438	_ 7	.104	3.204 z		106911	109188	12663		1. H1-1b
22	M280	HSS4x4x4	.255	0	9	.092	27.2 z	3	106911	109188	12663	12663	1H1-1b
23	M63	HSS4x4x4	.252	0	4	.095		14	106911	109188	12663	12663	1H1-1b
24	M234A	PIPE_2.0	.248	<u>77.368</u>	8	.075	28.7	16	17855.0	32130	1871.625	1871.625	2H1-1b
25	M75	PIPE 3.0	.204	90,789	13	.086	90.7		28250.5				2H1-1b
26	M72	PIPE_3.0	.191	90.789	3	.085	59.2					5748.75	2H1-1b
27	M69	PIPE 3.0	185	90.789	8	,089	134		28250.5				2H1 -1 b
28	M104	L2x2x3	.158	<u> </u>	16	.007	0 z				557.717		
29	M100	L2x2x3	.156	0	11	.008	0 y		9618.956			1178.909	
30	M92	L2x2x3	152	A 4 0	11	.007	0 z		9618.888			1163,931	2000
31	M98	L2x2x3	.147	0	6	007	0 z		9618.888				
32	M106	L2x2x3	.141	<u>0</u>	6	.007			9618.956			1146,16	
33 34	M94 M301B	L2x2x3 L2.5x2.5x4	.141 .130	0	16	.007	0 v		9618.956		557.717		
35	M289A	0.38 X 6 Pl		13.1 <u>55</u>	<u> 18</u>	.044			37073.2		1113,554		
36	M302B	L2.5x2.5x4	.130 .128	2.5	18	.019	1.053 Z		66218.6		584.82		1H1-1b
37	M286A	0.38 X 6 Pl	.126	0 0	9	.043					1113.554		
38	M303B	L2.5x2.5x4	. 120	2.5	9	.019	1.053 Z		36218.6		584.82		1H1-1b
39	M297A	0.38 X 6 Pl	.116	0 2.5	4	.040			37073.2		1113.554		
40	M278A	0.38 X 6 Pl	.110	2.5 2.5	7	.018 .017			66218.6.		584.82		1H1-1b
41		0.38 X 6 Pl	.103	2.5	14	.017	1.053 Z				584.82		1H1-1b
42	M300B	0.38 X 6 Pl	102	2.5 2.5	13	The Committee of the Contract of the	1.053 Z			73872	584.82	2.42 2.22 2.22	1H1-1b
43	M322	L3x3x4	.066	26.886	3	.016 .000	1.053 z						1H1-1b
	IVIJEE	LOXOX4	.000	20.000	. 3	.009	0 y	10	20423./	40056	1688.138	3420.051	1 H2-1



: KHA : GJV - 01955

019558041 841295 - BETHANY May 28, 2019 11:12 AM Checked By: ZAM

Envelope AISC 14th(360-10): LRFD Steel Code Checks (Continued)

To the disconsister	Member	Shape	Code Check	Loclini	LC	Shear Che	i oclini	iDirl (? nhi*Pnc	nhi*Dnt	nhi*Mn	phi*MnCb	
44	<u> M326</u>	L3x3x4	.064	26,886	14	.009	0	V A	28423 7	AGGEG	1688 13	B3426.6511	Egn
45	<u>M330</u>	L3x3x4	.063	26.886	8	.009	0	VΔ	28423.7	46656	1688 13	83426.6511	U2-1
46	<u> M328</u>	L3x3x4	.062	28.38	11	.010						3426.6511	
47	<u> M324</u>	L3x3x4	.061	28.38	17	.010	56.7	7 18	3 28423.7	46656	1688 13	3426.6511	U231
48	<u>M320</u>	L3x3x4	.059	28.38	6	010	n	亨1:	28423.7	46656	1688 138	3426.6511	<u>1 ⊓∠- </u>
49	M310B	PIPE 2.0	.036	28.31	22	.022	0	18	24603.0	32130	1871 62	1871.6251	U1 1 L
50	M312B	PIPE_2.0	.035	28.31	32	020	56.6					1871.6251	
51	<u>M311B</u>	PIPE_2.0	.035	28.31	27	.022	0	7	24603.0	32130	1871.625	1871.6251	#1_1h

Envelope Plate/Shell Principal Stresses

1 2 3 4 5	Plate P726	max min max	1917	Sigma1 [ksi] 11.178 -1.339	10	Sigma2 [ksi] 1.103	10	Tau Max [ksi] 6.016	LC 18	Angle [rad]	_ <u>LC</u>	Von Mises [ks	
3 4 5	P531	max					1 131						140
4 5	P531		-		82	-13.308	18	.092	25	2.081 367	74 27		18
5	P531	CONTRACTOR AND ADDRESS.	В	7.395	18	1.542	18	2.926	18	2.297	53		25
	P531	min	2000	-1.328	10	-6.355	10	.097	25	2.291 771	52	6.757 .236	18
		max	T	14.286	14	4.41	14	4.938	14	2.13	19	12,671	25
6	A CONTROL COMPANY OF THE CONTROL OF	min	440	-4.016	6	-12.974	6	.024	50	2.13 559	28	.042	14
7		max	В	15.002	6	4.351	6	5.841	14	2.307	55	14.67	50 14
<u>.8</u>	912 5 4 8 5 7	min	1200	-4.782	14	-16.464	14	.038	19	2.751	53	.08	53
9	P436	max	T	14.104	3	4.35	3	4.877	3	1.634	24	12.51	3
10		min_		-4.099	11	-13.223	11	.02	48	195	7	.034	48
11		max	В	15.42	11	4.468	11	5.68	3	1.642	31	14.287	3
12		min		-4.681	3	-16.04	3	.075	65	167	15	.131	65
13	P798	max	T	9.64	4	.748	4	5.886	13	2.142	9	12.322	13
14	(3) SECTION (\$1.74) (\$1.65)	min	48.33	-1.043	12	-12.807	13	.524	18	448	8	.951	18
15		max	В	6.76	13	1.316	12	2.725	13	1.901	3	6.21	13
16		min	TAXDAM.	963	4	-5.105	5	.196	69	102	18	.413	69
17	P627	max	T	13.098	8	4.037	8	4.76	16	2.298	52	12.216	16
18		min	54743 (95) 467-4843	-4.255	16	-13.775	16	.024	87	767	45	.044	87
19		max	В	15.83	16	4.586	16	5.622	16	2.337	35	14.107	16
20	de de la constitución de la cons	min		-4.401	8	-15,258	8	022	91	686	47	.044	91
21	P515	max	T	13.319	14	4.098	14	4.61	14	2.121	19	11.815	14
22		min		-3.732	6	-12.103	6	.029	54	=.23	28	.07	54
23		max	В	12.798	6	3.905	6	4.879	14	2.204	50	12.473	14
24		min		-4.295	14	-14.053	14	A catalog as the continuous and	19	591	42	.078	19
_25	P655	max	T	10.945	15	.946	15	5.557	7	2.201	63	11.77	7
26	25. V 5. V 5. EN EN 25. V	min	三角	-1,218	7	-12.332	7		84	68	82	.066	84
_27		max	В	6.911	7	1.46	7	2.726	7	2.218	83	6.31	7
28		min	EQ.	-1.179	15	-5.864	15		32	75	93	.077	84
29	P526	max	T	13.171	14	4.076	14		14	2.271	18	11.68	14
30		min	10 (S. 110)	-3.675	6	-11.877	6	.059	35	049	17	.116	35
31		max	В	13.972	6	4.014	6		14	2.163	40	13.742	14
32	ACCUSED OF THE STREET	min		-4.463	14		14		35	556	9	139	35
33	P622	max	T	13.072	8	4.041	8		8	2.126	12	11.592	8
34	College (All March 1)	min	145.43	-3.717	16	-11.971	16		81	693	80	.036	81
35		max	В	14.251	16		16	5.335	8	2.176	29	13.409	8
36		min		-4.382	8	-15.052	8		90	484	86	.066	78
37	P420	max	_T	12.974	3	3.994	3		3	1.6	24	11.509	3
38		min			11		11		54	193	7	.007	54
39		max	В	13.096	11		11		3	1.66	31	12.121	3
40	A Company of the State of the S	min	2.5,7	-4.173	3		3		37		15	.054	67
41	P611	max	T_	12.462	8		8		16		46	11.444	16
42		min			16		16		38	753	54		68
43		max	В		16		16		16		46	12.076	16
44		min		-4.021	8	to the printing the transfer for the second of the second	8		33		35		53

APPENDIX D ADDITIONAL CALCUATIONS

CCI Mount Analysis Square Plate Connection 1.0.1



Parky		Locatio	n:		Α	Se
100						
		SITE	DATA			
	BU	Numbe	re.	.82	1295	
	Project	Numbe	r e	019	558041	
25076	A.J.	N / /	100			Nº 1 95 7

BOLT DA	47/4	1
Quantity:	4	
Diameter:	0.625	in
Material:	A325 (1/2 to 1)	Select,
Fy:	92	ksi
Fu;	120	ksi
Bolt Circle:	8.485281374	in

	PLATE D	ATA .		
Andrew St. St. St.	Width:		8.5	in
au	hickness:		0.625	in
	Fy:		36	ks

SUPPORT ARM DATA	
The state of the s	Select
Diameter/Width: 4	'n
Fhickness 0.25 i	n
<i>Fy:</i> 36	csi
Number of Sides: 4	

	TIA Re	vision:	TIA-222-H	Select
		Applying TIA	-222-H Section 1.	5.5
	R	REACTIONS		
	Mo	ment:	6.582	kip-ft
		Axial:	1.229	kips
Orani.	12-18-14-14-15 (N. 180)	Shoore	3.70E	S. S. Latina

Laad Combination	14
BOLT RESI	JLTS
Max Bolt (Cu+ Vu/η):	9.62 kips

POPI MODELS	麴
Max Bolt (Cu+ Vu/η): 9.62	kips
Axial Design Strength: 21.70	kips
Stress Ratio 42,21%	

PLATERE	
Base Plate Stress:	29.51 ksi
Bending Strength:	32.40 ksi
Stress Ratio:	- 86.74%

		14

APPENDIX E

MOUNT MODIFICATION DESIGN DRAWINGS (MDD) / SUPPLEMENTAL DRAWINGS

421 FAYETTEVILLE STREET, SUITE 600 RALEIGH, NC 27601 PHONE: 919-677-2000 WWW.KIMLEY-HORN.COM



CROWN CASTLE

OJECT INFORMATION:

BU: 841295 BETHANY

Kimley≫Hor⊓

1500 CORPORATE DRIVE CANONSBURG, PA 15317 WWW.CROWNCASTLE.COM

MOUNT MODIFICATION **DRAWINGS**

BETHANY

CROWN CASTLE BU#: 841295 VERIZON SITE#: 104335

STRUCTURE INFORMATION

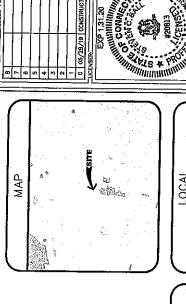
TOWER

150' MONOPOLE TOWER LOW PROFILE PLATFORM

SITE ADDRESS

LATITUDE: N 41° 26' 33.93"± LONGITUDE: W 72° 59' 32.86"± BETHANY, CT 06524 NEW HAVEN COUNTY 719 AMITY ROAD

MOUNT





	57 . Las 8.	A16.00	Zoria .	· · · · · · · · · · · · · · · · · · ·	
	10年7月1日	(3), A	10.00	69 P. C.	200 C 10 B
	展. 14	4.4	A		
	200 4.23	100	1 100	316 10	3000000
	SALE S				
	大 魚田 400			F 100 3	Constant of
	700000		2012014		2.7
	2011	450	-0.00	35 KAR	A September 1
		10			
	400	7	10.23	30 m	100
		45			建二级
⋖					A 20 A 3
٠ì	18 TO 18	100	2.25	3 A 3 2 2	
$_{-}$		1.5	1 a 2		
Ο.	100	27.63			1 A 1 A 1
LOCAL			0.6		\$10 A B B B B B B B B B B B B B B B B B B
_	202	Acres 6	经证据证	3.0	ter Confe
		12 M	1 (4) 4	1848	A 150 A
	100	400.00	对地域		左
	1000	A 17.3			第 美 歌樂
				The Court	2 12 TA
	100	5011		Section 1	
	25 2.00	300			
	005 SCA	38.00	41 300	4-11-11-1	ACOMO P.
		A. A.	2650	2	
	2 - C. C.	A 10	0 L	SALES MANAGEMENT	ALC: NOR
				STATE OF THE STATE	
	以下公共 5	100.00	4.00		SEASON NO.
<u> </u>	THE STATE OF		725 2	张 电压	

					9		
_	0		٥				١
TO LOUIS NO LED	MOUNT WEWS & MODIFICATION	SCHEDULE	PART DETAILS				
ı	 _		~		1	i I	Į

ETS		В	~	<u>~</u>	<u>«</u>						
SHE		ļ 			IFICATION						
유	7		S	OTES	S MOC						
INDEX OF SHEETS	SHEET DESCRIPTION	TITLE SHEET	PROJECT NOTES	INSPECTION NOTES	MOUNT VIEWS & MODIFICATION	SCHEDULE	PART DETAILS				
	SHEET	Ξ.	N I	N-2	S-1		S2	Ì			
_	S								,	_!	

	7	
ı		1

TITLE SHEET

5

ē

1.03

1.05 1.07

2.00 STRUCTURAL STEEL NOTES

2.01 STRUCTURAL STEEL SHALL COMPLY WITH THE FOLLOWING SPECIFICATIONS UNIO:

A. STRUCTURAL STEEL SHAPES, PLATES AND BARS. (CAPECT W-SHAPES). — ASTM AST, Fy=36 KSI B. PPR — ASTM, ASS, GRADE B, Fy=35 KSI, C. HSS-SHAPES — ATSM A500, GRADE B, ಷಭ

2.02

CHENCH ROOS - AND LONGE B. CHENCH ROOS - AND LONGE B. CHENCH ROOS - AND FISH, RECOMBER B. AND LONGE B. CHENCH ROOS - AND FISH, RECOMBER B. CHENCH ROOS - AND FISH, RECOMBER B. CHENCH ROOS - AND FISH, RECOMBER B. CHENCH ROOS - AND LONGE B. CHENCH ROOS - AND FISH, RECOMBER B. CHENCH ROOS - AND LONGE B. CHENCH ROOS - AND 2.03

22/CIDWn/841295/CAD/Mount NOD/841285_NOD_R.dwq ---- 05/28/19 FM by: Jenny-Adom

202 2.05

(CW),
MEMBERS' SHALL BE SHOP-FABRICATED AND WELDED TO THE EXTENT
PRACTICABLE IN ORDER TO REDUCE FIELD INSTALLATION COSTS. 2.06

1.00 GENERAL NOTES

1.01 LIMITERIAS AND WORKHANSHIP SHALL COMPONENCE WITH THE GOVERNMEN COMPONENCE OF THE THE STATE LOAF ON MATCH THE DONE WITH THE GOVERNMEN COMPONENCE OF THE CONTRICTOR SHALL END THE STATE LOAF ON MATCH THE THE STATE LOAF ON MATCH THE LOAF ON MATCH THE CONTRICTOR SHALL END THE CONTRICTOR SHALL END THE CONTRICTOR SHALL END CONTRICTOR SHALL END THE CONT

4.00 CONTRACTOR NOTES

AND FROR TO GEGINNER OCUSTRUCTION ALL CONTRACTORS AND

ENGENATURAL SHETT RECORDING. JUBICESTAND, AND WITH TO STRUCTURE

OWNERS STANDARGS OF PRACTICE. CONSTRUCTION ALIGENING. ALL SITE AND

ENGRENAL CONTRACTOR IN CAUGABLEAN, AND WITH TO STRUCTURE

OWNERS OF CONSTRUCTION ACCURATED. ALL SITE AND

DESCRIPTION OF CAUGABLEAN TO PROPOSE MODIFICATION

ENGRAL CONTRACTOR INCOMES WESD ON SITE, AND PROPOSED MODIFICATION

OWNERS OF COMPACTOR INCOMES WESD ON THE RESPONSEDLENT OF THE CONTRACTOR TO DETAIN THIS DOCUMENTATION FIGH AND SERVICED ON THE CONTRACTOR FOR WESD ON THE CONTRACTOR SHALL SHOW THE OWNER OF THE OWNER.

AND FIGHEN OWNERS OF BROWNERS, OR ANY COMPITIONS THAT ARE NOT REFERENCED ON THE STRUCTURE OWNER.

AND FIGH OWNERS OF BROWNERS, OR ANY COMPITIONS THAT WOULD FEEL OWNER.

AND PROPOSED ON THE STRUCTURE OWNER.

AND PROPOSED ON THE STRUCTURE OF THE CONTRACTOR FOR THE OWNER OWNER.

AND PROPOSED ON THE STRUCTURE OWNER.

AND PROPOSED ON THE STRUCTURE OF THE OWNER OWNER.

AND PROPOSED ON THE STRUCTURE OWNER.

AND PROPOSED ON THE STRUCTURE AND THE STRUCTURE OWNER.

AND PROPOSED ON THE STRUCTURE OWNER.

AND PROPOSED ON THE STRUCTURE OWNER OWNER OF THE CONTRACTOR TO STRUCTOR TO STRUCTURE OWNER OWNER OF THE CONTRACTOR STALL STRUCTURE OWNER OW

Reser of and lespraper relance on this document without written authorized

document, together with the sescueta and deligen presented harvin, as an bathument of service, is interest only for the specific purpose and client for which it was propored.

5.00 BOLT TIGHTENING PROCEDURE 5.01 TIGHTEN BOLTS BU ASC- "TURN OF THE NUT" METHOD, USING THE CHART BELOIR

CROWN

ROJECT INFORMATION: BU: 841295 BETHANY

BEFORE 1/3 JURN

719 AMTY ROAD
BETHANY, CT 06524
NEW HAVEN DOUNTY
LANS PREPARED BY:

Cimley » Horn

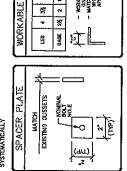
421 FAYETTENNIE STREET, SJATE 800 RALENON, NG 27801 PHONE. STREET, SJATE 1800 WWW.MILLEY-HORN.COM. KHA. COM, P.E. DGGD738

AFTER 1/3 TURN

6.02 SPLICE BOLTS SUBJECT TO DRECT TENSION SHALL BE INSTALLED AND TIGHTENED AS PER SECTION B(4)(1) FTE ASSE MANUAL OF STEEL CONSTRUCTION, THE INSTALLATION PROCEDURE IS PARAPHRASED AS FOLLOWS.

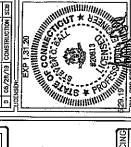
Fasteners shall be installed in propery alighned holes and be tightened by one of methods described in subsection g(d)(t) through g(d)(4).

6(d)(1) TURN-OF-THE-NUT IDATIBNING
BY SHALL BY BY BY BY SHALL DIGHT THE LOSS OF A JOINT ARE IN TRIBLY SHALL BY BY BY SHALL BY BY BY SHALL PROCESS SYSTBANDARY SHALL BY BY SHALL PROCESS SYSTBANDARY WING THAT AND THE CONNECTION IS BY BLILLY COMMENTED. FOLLOW THIS MINLA DEPENDENCE, SHOULD SHALL BY SHALL BY SHALL BY BY SHALL BY SHALL



NOMINAL HOLE DIM SET HOLE SERT SOT No. No.	ľΩI							7
	E DIM'S	SHORT SLOT	% x %	% × %	* *	1/1. x 1/5.	V6 × 96	
NOMINA X: 8: 8: 8: 8: 8: 8: 8: 8: 8: 8: 8: 8: 8:		STANDARD HOLE #	9/6°#	18	1. No. 1	196	ιχε"»	
	NOMINA	B0.7 ¢	7.4	*	*	9.5	ċ	i
		*	-	ļ				
<u>*</u> -, "	S	~	*	Ī	ä	52	1.4	
S 2 3 2 2 2	힣	30	*	1	3	<u>,</u> E	ą,	

__DATE:___ISSUED FOR:



SHORT SLOT

STANDARD HOLE # 2

9 170 Š¢

ALLOWABLE ANGLE COPE

S

EET TREE

PROJECT NOTES

SHEET NUMBER

L, MIN. EDGE

%** 1%** %** 1%** %** 1%**

- COPED PORTION OF ANGLE

ź

SPACING

8

BOLT HOLE -C

OO NOT COPE — BEYOND THIS LINE, TYP.

1.00 GENERAL INSPECTION NOTES.

101 THE POST-HODPICATION INSPECTION 15 A WEBJAL EXAMINATION OF STRUCTURE
MODIFICATIONS AND A RECIPE OF ANY REQUIRED THE MODIFICATION SHOWS AND A RECIPE OF A RECIPE OF A RECORDARY OF ANY REQUIRED THE MODIFICATION AND THE ENGINEER
OF RECORD. THE CONTRACTOR DOCUMENTS AS DESIGN OF THE BUGNEER
OF WHICH SHAPE REQUIRED THE BUGNEER OF THE DESIGN OF THE BUGNEER OF THE BUGNEER OF THE DESIGN OF THE MODIFICATION METERING ASPECTS OF THE DESIGN OF THE MODIFICATION METERING ASPECTS OF THE DESIGN OF THE MODIFICATION METERING ASPECTS OF THE DUTIES. OWNERSHIP OF THE MODIFICATION METAL TOWNERSHIP OF THE MODIFICATION AND THE PRIME CONTRACTOR AND THE PRIME CONTRACTOR AND THE PRIME CONTRACTOR AND THE PRIME CONTRACTOR AND MODIFICATION AND THE

2.00 INSPECTION & REPORT RECOM'S

2.01 THE FOLLOWING ARE PROMISED WITH THE MINITY OF BINHANGING THE
EFFICIAL ARE PROMISED WITH THE MINITY OF BINHANGING THE
EFFICIAL OF THE PROCESS OF TOLLECTIONS AND COMPILIANS THE PROMISED THE
2.01. IT IS RECOMMENDED THE PROMISE THE REPORT
NOTICE FOR WHICH THE SITE WILL BE READY FOR THE MODIFICATION
2.01. THE PROMISED THE CONTRACTOR
2.01. THE PROMISE THE WORLD THE WITHOUT THE PRINTE PROJECT OF THE MODIFICATION
2.01. THE PROMISE THE CONTRACTOR AND MODIFICATION AND MODIFICATION
2.01. THE PRESENT DURING THE WITHAL INSPECTIONS, AND WORLD THE THE MAY BE PRESENTED WITHOUT THE PRINTED THE SHALL BOTH BETTENDED TO THE PROMISE THE PROMISE THE SHALL BOTH BETTENDED TO THE PRESENT DURING THE WITHAL INSPECTIONS, AND YOR HE THE MAY BE PRESENTED THE THE WAY BE PRESENTED THE WAY BE PRESENTED THE THE WAY BE PRESENTED THE WAY BE PRESENTED THE WAY BE PRESENTED THE WAY BE PRESENTED THE WAY BE WAY THE WAY BE WAS AND THE WAY BE WAY THE WAY BE WAY THE WAY THE WAY THE WAY BE WAY THE WAY

3.00 INSPECTION RESCHEDULE & CANCEL
3.01 F THE PRINE CONTRACTOR AND MODIFICATION INSPECTOR HAVE AGREED UPON A
REAL AND DATE FOR A GIVEN INSPECTION AND EITHER PARTY RESCHEDULES OR
CANCELS THE INSPECTION, THE STRUCTURE OWNER SHALL NOT BE RESCHEDULES
FOR COSTS, FESS, LOST DEPOSITS, OR OTHER EXPONSIBLE
FOR COSTS, FESS, LOST DEPOSITS, OR OTHER EXPONSIBLE
OTHERS SCHEDULING CHANGES, RECEPTIONS AND EN MADE IN HE ENVIL OF
UNDONTROLLABLE STANTAIONS SLUCH AS INVITINAL DESSETTES, SEVERE WASHER
OR OTHER CONDITIONS THAT COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

4.00 REMEDIATION OF FAILING INSPECTION
4.01 IN THE EVERT ANY PORTION OF THE MODIFICATION WASHE SCIERLINED TO BE
UNEXTREACTORY BY THE MODIFICATION INSPECTOR, THE PRIME CONTRACTOR
THAT MULL BYTHE.

4.9.1

4.01.2

K./W.M. Wirless/Crow/841295/CAD/Wount MOD/841295_MOD_R.dwg ---- 05/28/19 5:40 PM by: Janny Adoms

5.00 OWNER, INSPECTIONS
5.01 THE STRUCTURE OWNER AXY CONDUCT INSPECTIONS TO VERIFY THE QUALITY AND
COMPLETINESS OF THE PREMOUSEY CONPLETED MODIFICATION INSPECTIONS
5.02 INSPECTIONS MAY BE COMPLETED BY A SIGN-ARMY FIRM OF THE STRUCTURE
OWNERS CAROGNIO AFTER A MODIFICATION PROJECT IS COMPLETED AND A
PASSING MODIFICATION INSPECTION REPORT IS ISSUED.

presented herein, on an indicament of merican, is independ any for the specific purpose and district for which it was proposed. Notes at and improper malitime on the documents without

6_00 MOD INSPECTOR'S RESPONSIBILITIES
6.01 THE MODIFOLIAN INSPECTOR'S RESPONSIBILITIES
6.01 THE MODIFOLIAN INSPECTOR SHALL CONFIDENCE AS SOON
AS THE MEDIFOLIAN INSPECTOR SHALL ENVIOUR THE RECEIVENTS AS THE MEDIFOLIAN INSPECTOR SHALL WORK WITH THE PRINE CONTRACTOR TO DEVELOP A SITE—SECTION GENERALY SHALL WORK WITH THE PRINE CONTRACTOR TO DEVELOP A SITE—SECTION RECEIVENTS OF OTHER CONCERNOR AND INSPECTION RECURSION TO SECTION SECTION SECTION SECTION AND TEST REPORTS (NO.LIDING THOSE OF ASSISTED CONTRACTOR AND TEST REPORTS (NO.LIDING THOSE OF ASSISTED CONTRACTOR AND STATE OF THE REPORTS (NO.LIDING THOSE OF ASSISTED CONTRACTOR OLD AND STATE A

2.00 PRIME CONTRACTOR RESPONSIBILITIES

7.01 THE FAUE CONNEXTOR SHALL DOWNORTHER INSPECTOR AS SOON

7.02 THEY HAVE RECEIVED A PHICKATE THE MODIFICATION INSPECTOR AS SOON

MODIFICATION INSTALLAND. THE PRICE CONTRACTOR SHALL RANKE THE

RECURRIENTS OF THE MODIFICATION INSPECTION OF SHALL WANK WITH

THE MODIFICATION INSPECTION OF DEVELOR SHALL WANK WITH

INSPECTIONS, AND SHALL DECURS SPICIPION AND TESTING

RECURRIENTS WITH THE MODIFICATION INSPECTION AND TESTING

UNDESTALMING OF THE REQUIRED INSPECTION AND TESTING

UNDESTALMING OF THE REQUIRED INSPECTION AND TESTING

THE PRIME CONTRACTOR SHALL PREPORM AND RESIDENCE OF THE MODIFICATION RESPECTIVE AND RESIDENCE OF THE MODIFICATION OF SHALL THE REQUIREMENTS OF THE

MODIFICATION INSPECTION CHECKLIST.

8.00 PHOTOGRAPHY REQUIREMENTS

8.01 HE PRIME CONINACTOR AND MODIFICATION INSPECTOR SHALL, BETWEEN THE EFFORTS OF BOTH PARTIES AND THEE CHRONOSTOR PRISONAL, PRODUCED PHOTOGRAPHS WITH THE INSPECTION REPORT TO INCLUE. THE POLITORANDE OF STATES AND THE REPORT TO INCLUE. THE POLITORANDE OF STATES AND THE PROTOGRAPHS TO INCLUE. THE POLITORANDE OF STATES AND THE RAW MATERIALS WORK REQUIRED ON THE FAMILY AND TOTAL STATES OF THE STATES AND THE PREPARATION AND CONCINCING.

8.3 WELD FREDAKTION WOLLDINGS TECKNIST STEE GAUGE, AS APPLICABLE)

8.4 WELD FREDAKTION WOLLDINGS TECKNIST.

8.5 WELD FREDAKTION WOLDDING THE WELD STEE GAUGE, AS APPLICABLE)

8.5 FIRAL INSTALLED CONDITION (AFTER DEFICIENT CONDITIONS). FANN ARE REMEDENTED THE STEE AND TOTAL STATES OF THE STEE A WORK.

C. POST-MODIFICATION PHOTOGRAPHS OF THE STE AT CONDILISON OF THE WORK OF THE PRIME CONTRACTORS, AND THE WINDSPECTORS. ASSIGNATED ON THE WINDSPECTORS. ASSIGNATED SUBSCIPATION OF THE WINDSPECTORS. ASSIGNATED SUBSCIPATION WORK OF THE PINE STEE AT CONDILISON OF THE WINDSPECTORS. ASSIGNATED SUBSCIPATION RESPECTORS.

6. PHOTOGRAPHS OF THE STEE OF THE STEE AT CONDILISON OF THE WINDSPECTORS. ASSIGNATED SUBSCIPATION OF THE WINDSPECTORS. ASSIGNATED SUBSCIPATION OF THE WINDSPECTORS. ASSIGNATED SUBSCIPATION.

NOTE: PHOTOS OF MODIFICATIONS INSTALLED ON THE STRUCTURE ABOVE AN ELEVATION OF 20° SHALL REQUIRE PHOTOS TAKE FROM THE STRUCTURE AS WELL AS OVERALL PHOTOGRAPHS OF THE MODIFICATIONS TAKEN FROM THE GROUND.

PRE-CONSTRUCTION INSPECTION CHECKLIST

CROWN

								_	
MSPECTION REPORT ITEM	MODIFICATION INSPECTION CHECKLIST	SHOP DRAWINGS APPROVED BY EDR (LATEST REMSION)	FABRICATION INSPECTION	FABRICATOR'S CERTIFIED WELD INSPECTION (CM)	FABRICATOR'S QUALIFIED PERSONNEL FOR WELDING	MATERIAL TEST REPORT(S) / MILL CERTIFICATE(S)	FABRICATOR'S NON-DESTRUCTIVE TESTING (NDT) TECHNICIAN	PACKING SUPS FOR STRUCTURAL MATERIALS	
AND/DR AND/DR INSTALLATION INSPECTIONS REQUIRED FOR REPORT?	YES	ÆS	YES	YES	YES	YES	YES	YES	

Kimley » Horn

719 AMITY ROAD
BETHANY, CT 06524
NEW HAVEN COUNTY
PLANS PREPARED BY:

BU: 841295 BETHANY

OLECT INFORMATION:

421 PAYTHEVALE STREET, SAITE 600 RALEIGH, NG 27001 PHONE. WHENCHLEY-HORACON KHA COMF PELIDOOD738

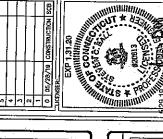
CONSTRUCTION INSPECTION CHECKLIST

	_	_						_	_		
INSPECTION REPORT (TEM	CONSTRUCTION INSPECTION	FOUNDATION INSPECTION	CONCRETE COMPRESSIVE STRENGTH AND SLUMP TESTING RESULTS/CERTIFICATES	ADHESIVE ANCHOR ROD(S) INSTALLATION INSPECTION	BASE PLATE GROUT INSPECTION	THIRD-PARTY CERTIFIED WELD INSPECTION (INCLUDING IBC SPECIAL INSPECTIONS)	SOIL EXCAVATION—DENSITY TESTING, COMPACTION INSPECTION/VERFICATION, USE OF SUITABLE FILL	GALVANIZING REPAIR MATERIAL PREPARATION, INSPECTION & PAINT APPLICATION	GUY WIRE (RE-)TENSION REPORT AND INSPECTION	PRIME CONTRACTOR'S AS"BUILT DOCUMENTS (SIGNED & DATED)	
CONSTRUCTION AND/OR INSTALLATION INSPECTIONS REQUIRED FOR REPORT?	YES							YES		YES	

DATE: ISSUED FOR:

POST-CONS. INSPECTION CHECKLIST

CONSTRUCTION	
INSTALLATION	Hari taodae NOLOSASNI
REQUIRED FOR	
Æ	MODIFICATION INSPECTOR'S ISSUE LIST (INCLUDING
	ACTIONS TAKEN) AND/OR REDLINED RECORD DRAWINGS
	POST-INSTALLED ADHESIVE ANCHOR ROD PULL-QUIT TESTING
	PHOTOGRAPHS OF MODIFICATIONS (INCLUDE PHOTOS OF BOTH
٨٤٥	SIDES OF WELDED OR BOLTED CONNECTIONS, OF OVERALL AND DETAIL MENS OF INSTALL SIDES OF STREET
3	BEFORE/AFTER PHOTOS OF ANY ISSUES IDENTIFIED BY THE
	INSPECTOR)

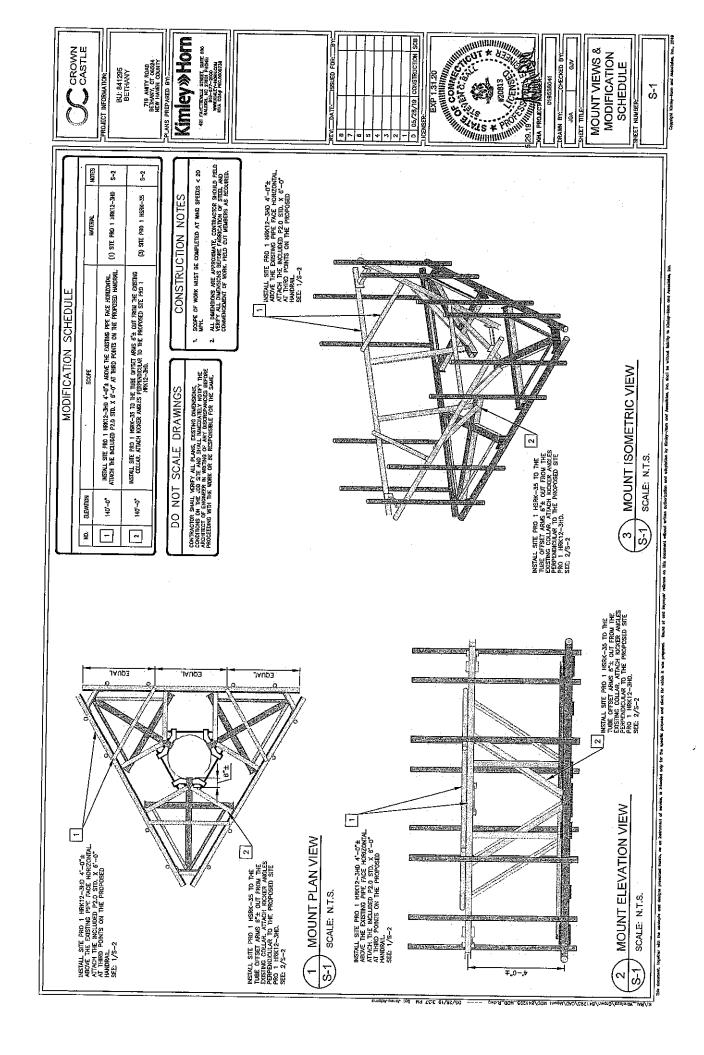


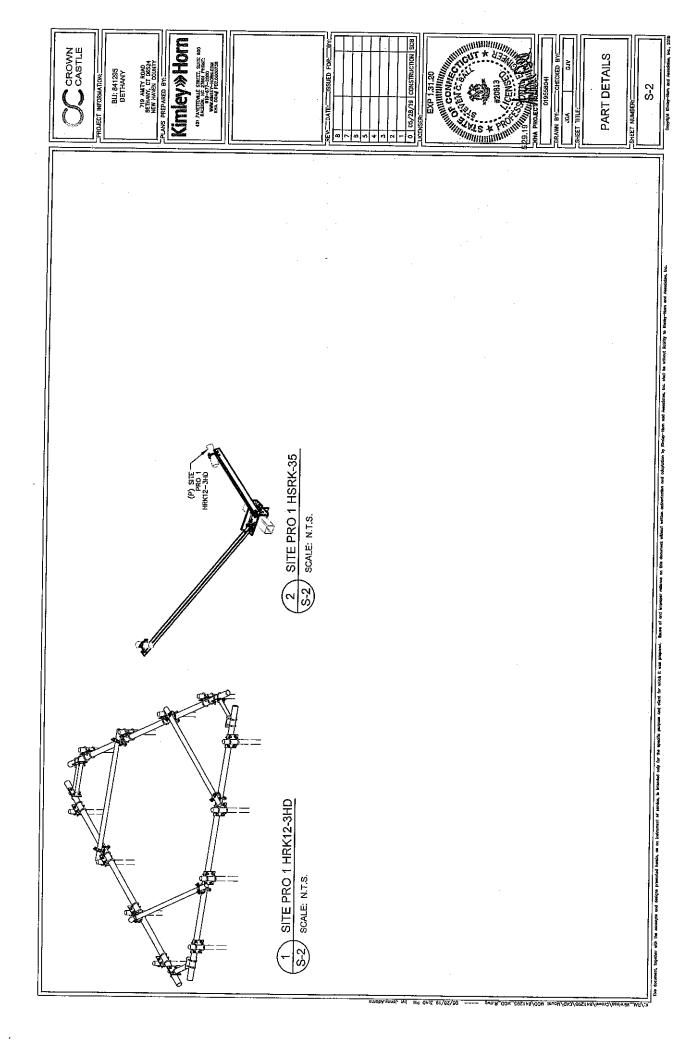
RAWN BY

JOA HEET TITAEN

INSPECTION NOTES

HEET NUMBER







Date: June 06, 2019

Denice Nicholson Crown Castle 3 Corporate Dr, Suite 101 Clifton Park, NY 12065

Paul J. Ford and Company 250 East Broad St., Suite 600 Columbus, OH 43215 (614) 221-6679

Subject:

Structural Analysis Report

Carrier Designation:

Verizon Wireless Co-Locate

Carrier Site Number:

Carrier Site Name:

104335

841295

Bethany North CT

Crown Castle Designation:

Crown Castle BU Number:

Crown Castle Site Name: **Crown Castle JDE Job Number:**

BETHANY 574490 1740548

Crown Castle Work Order Number: Crown Castle Order Number:

492710 Rev. 0

Engineering Firm Designation:

Paul J. Ford and Company Project Number: 37519-2490.001.7805

Site Data:

719 AMITY ROAD, BETHANY, New Haven County, CT Latitude 41° 26′ 33.93″, Longitude -72° 59′ 32.86″

151 Foot - Monopole Tower

Dear Denice Nicholson.

Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Proposed Equipment Configuration

Sufficient Capacity (73.9%)

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 -Analysis Criteria.

Respectfully submitted by:

Aaron E. Pike, E.I. Structural Designer

apike@pauljford.com

06/07/2019

TABLE OF CONTENTS

1) INTRODUCTION

2) ANALYSIS CRITERIA

Table 1 - Proposed Equipment Configuration
Table 2 - Other Considered Equipment

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided 3.1) Analysis Method 3.2) Assumptions

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)
Table 5 - Tower Component Stresses vs. Capacity
4.1) Recommendations

5) APPENDIX A

tnxTower Output

6) APPENDIX B

Base Level Drawing

7) APPENDIX C

Additional Calculations

1) INTRODUCTION

This tower is a 151 ft Monopole tower designed by VALMONT and mapped by FDH in March of 2016.

The tower has been modified per reinforcement drawings prepared by B+T in February of 2012. Reinforcement consist of flat plate reinforcing, post-installed anchor rods, and foundation augmentation.

The tower has been modified per reinforcement drawings prepared by B+T in July of 2012. Reinforcement consist of shaft reinforcing.

2) ANALYSIS CRITERIA

TIA-222 Revision:

TIA-222-H

Risk Category:

II 125 mph

Wind Speed: Exposure Category:

В

Topographic Factor: Ice Thickness:

1

Wind Speed with Ice:

1.5 in 50 mph

Wind Speed with Ice: Service Wind Speed:

60 mph

Table 1 - Proposed Equipment Configuration

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
		6	commscope	NHH-65C-R2B w/ Mount Pipe		
		3	decibel	DB854DG65ESX w/ Mount Pipe]	
		1	rfs celwave	DB-T1-6Z-8AB-0Z		
140.0	140.0	3	samsung telecommunications	RFV01U-D1A	1	4 5/0
140.0	140.0	3	samsung telecommunications	RFV01U-D2A	13	1-5/8
		1	tower mounts	12.5 ft Low Profile Platform]	
		1	site pro 1	Handrail Kit [HRK12-3HD]	1	
		3	site pro 1	Kicker Kit [HSRK-35]		

Table 2 - Other Considered Equipment

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
	160.0	1	dbspectra	DS1F03F36D-N		
]		6	adc	CG-1900DD-FULL-DIN	-	
		6	communication components inc.	DTMABP7819VG12A		
		6	ericsson	RRUS-11	12	1-5/8
:		3	kathrein	800 10121 w/ Mount Pipe	2	7/8
148.0	149.0	3	kathrein	860 10025	2 2	5/8
		6	kmw communications	AM-X-CD-16-65-00T-RET w/ Mount Pipe	1 1	3/8 2" cond.
		12	powerwave technologies	LGP21901		
		1	raycap	DC6-48-60-18-8F		
	148.0	1	tower mounts	Platform Mount [LP 602-1]		

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
	132.0	1	tower mounts	Pipe Mount [PM 601-3]		
132.0	124.0	3	alcatei lucent	800 EXTERNAL NOTCH FILTER		<u></u>
	131.0	3	alcatel lucent	800MHZ RRH		
		3	alcatel lucent	TME-1900MHZ RRH		
	133.0	1	pctel	GPS-TMG-HR-26NCM		
		3	alcatel lucent	TD-RRH8X20-25		
130.0	130.0	3	rfs celwave	APXVSPP18-C-A20 w/ Mount Pipe	1 3	1/2 1-5/8
	130.0	3	rfs celwave	APXVTM14-C-120 w/ Mount Pipe	1	1-1/4
		1	tower mounts	T-Arm Mount [TA 602-3]		
		3	ericsson	ERICSSON AIR 21 B2A B4P w/ Mount Pipe		
122.0	123.0	3	ericsson	RADIO 4449 B12/B71	7	1 E/O
122.0		3	rfs celwave	APXVAARR24_43-U-NA20 w/ Mount Pipe	,	1-5/8
	122.0	1	tower mounts	T-Arm Mount [TA 702-3]		

3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

Document	Remarks	Reference	Source
4-GEOTECHNICAL REPORTS	FDH, 15BBNL1600, 2/18/2016	6133952	CCISITES
4-TOWER FOUNDATION DRAWINGS/DESIGN/SPECS	FDH, 16BBMT1500, 2/17/2016 (mapped)	6133920	CCISITES
4-TOWER MANUFACTURER DRAWINGS	FDH, 16BBMW1500, 3/11/2016 (mapped)	6133951	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	B+T, 83154.003A, 2/21/2012	5135907	CCISITES
4-POST-MODIFICATION INSPECTION	B+T, 83154.004, 8/3/2012	5135928	CCISITES
4-TOWER REINFORCEMENT DESIGN/DRAWINGS/DATA	B+T, 84427.0002, 7/19/2012	4945157	CCISITES

3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

tnxTower was used to determine the loads on the modified structure. Additional calculations were performed to determine the stresses in the pole and in the reinforcing elements. These calculations are presented in Appendix C.

3.2) Assumptions

- Tower and structures were built in accordance with the manufacturer's specifications.
- The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Tower was modified in accordance with the referenced modification documents.
- 5) The rebar in the pad portion of the original foundation is unknown. In this analysis, it is assumed that the rebar at the top and bottom of the pad is consistent with the rebar added per PMI document #5135928 (#7 spaced 12" O.C.).
- The monopole manufacturer drawings are not available at the time of this analysis. Therefore, we have assumed the steel yield strength(s) (Fy) as per the following:
 - a) Anchor rods: ASTM A615 (Fu = 100 ksi, Fy = 75 ksi)
 - b) Pole Shaft: ASTM A572 Gr 65
 - c) Base Plate: ASTM A572 Gr 50
- 7) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically and must be replaced if damaged or cracked. Refer to Crown Castle document ENG-PRC-10012, Base Plate Grout Repair.

This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.

4) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

Elevation (ft)	Component Type	Size	Critical Element	% Capacity	Pass / Fail
151 - 146	Pole	TP18.526x17.59x0.2188	Pole	5.6%	Pass
146 - 141	Pole	TP19.461x18.526x0.2188	Pole	11.9%	Pass
141 - 136	Pole	TP20.397x19.461x0.2188	Pole	23.1%	Pass
136 - 131	Pole	TP21.332x20.397x0.2188	Pole	33.7%	Pass
131 - 126	Pole	TP22.268x21.332x0.2188	Pole	45.6%	Pass
126 - 125,5	Pole	TP22.361x22.268x0.2188	Pole	46.7%	Pass
125.5 - 125.25	Pole + Reinf.	TP22,408x22,361x0,3626	Reinf. 11 Tension Rupture	40.8%	Pass
125.25 - 120.25	Pole + Reinf.	TP23.343x22.408x0,3563	Reinf. 11 Tension Rupture	51,2%	Pass
120.25 - 118.5	Pole + Reinf.	TP23.671x23.343x0.3563	Reinf. 11 Tension Rupture	54.8%	Pass
118.5 - 118.25	Pole + Reinf.	TP23.718x23.671x0.6438	Reinf. 9 Bolt-Shaft Bearing	33.5%	Pass
118.25 - 117.5	Pole + Reinf.	TP23.858x23.718x0.6438	Reinf. 9 Tension Rupture	33.7%	Pass
117.5 - 117.25	Pole + Reinf.	TP23.905x23.858x0.4938	Reinf. 9 Tension Rupture	42.9%	Pass
117.25 - 112.25	Pole + Reinf.	TP24.84x23.905x0,4813	Reinf. 9 Tension Rupture	50.4%	Pass
112.25 - 107.25	Pole + Reinf.	TP25.776x24.84x0.4688	Reinf. 9 Tension Rupture	57.4%	Pass
107.25 - 102.25	Pole + Reinf.	TP26.711x25.776x0.4563	Reinf. 9 Tension Rupture	63.8%	Pass
102.25 - 100.92	Pole + Reinf.	TP27.6x26.711x0,4563	Reinf. 9 Tension Rupture	65.4%	Pass
100.92 - 95.92	Pole + Reinf.	TP27.459x26.523x0.55	Reinf. 9 Tension Rupture	60.5%	Pass
95.92 - 92.5	Pole + Reinf.	TP28.098x27.459x0.55	Reinf. 9 Tension Rupture	63.6%	Pass
92.5 - 92.25	Pole + Reinf.	TP28.145x28.098x0.55	Reinf. 8 Tension Rupture	63.8%	Pass
92.25 - 87.25	Pole + Reinf.	TP29.08x28.145x0,5375	Reinf. 8 Tension Rupture	67.9%	Pass
87.25 - 87	Pole + Reinf.	TP29.127x29.08x0.625	Reinf. 7 Tension Rupture	58.4%	Pass
87 - 82	Pole + Reinf.	TP30.063x29.127x0.6125	Reinf. 7 Tension Rupture	61.9%	Pass
82 - 77	Pole + Reinf.	TP30.998x30.063x0.6	Reinf. 7 Tension Rupture	65.2%	Pass
77 - 72	Pole + Reinf.	TP31.934x30.998x0.5875	Reinf. 7 Tension Rupture	68.2%	Pass
72 - 67	Pole + Reinf.	TP32.869x31,934x0,575	Reinf. 7 Tension Rupture	71.1%	Pass

Elevation (ft)	Component Type	Size	Critical Element	% Capacity	Pass / Fail
67 - 63.25	Pole + Reinf.	TP33.571x32.869x0.575	Reinf. 7 Tension Rupture	73.1%	Pass
63.25 - 63	Pole + Reinf.	TP33.618x33.571x0.575	Reinf. 6 Tension Rupture	73.3%	Pass
63 - 58	Pole + Reinf.	TP34.553x33.618x0.5625	Reinf. 6 Tension Rupture	75.8%	Pass
58 - 56.75	Pole + Reinf.	TP34.787x34.553x0.5625	Reinf. 6 Tension Rupture	76.4%	Pass
56.75 - 56.5	Pole + Reinf.	TP34.834x34.787x0.6375	Reinf. 5 Bolt Shear	66.4%	Pass
56.5 - 52	Pole + Reinf.	TP36.518x34.834x0.6375	Reinf. 5 Compression	66.1%	Pass
52 - 47	Pole + Reinf.	TP35.987x35.051x0.7	Reinf. 5 Compression	63.6%	Pass
47 - 42	Pole + Reinf.	TP36.922x35.987x0.6875	Reinf. 5 Compression	65.4%	Pass
42 - 37	Pole + Reinf.	TP37.858x36.922x0.675	Reinf. 5 Compression	67.0%	Pass
37 - 34.25	Pole + Reinf.	TP38.372x37.858x0.675	Reinf. 5 Bolt Shear	70.3%	Pass
34.25 - 34	Pole + Reinf.	TP38.419x38.372x0.675	Reinf. 4 Bolt Shear	70.4%	Pass
34 - 29	Pole + Reinf.	TP39.354x38.419x0.6625	Reinf. 4 Compression	69.4%	Pass
29 - 26.75	Pole + Reinf.	TP39.775x39.354x0.6625	Reinf. 4 Bolt Shear	72.6%	Pass
26.75 - 26.5	Pole + Reinf.	TP39.822x39.775x0.6625	Reinf. 1 Bolt Shear	72.7%	Pass
26.5 - 21.5	Pole + Reinf.	TP40.757x39.822x0.65	Reinf. 1 Compression	71.5%	Pass
21.5 - 16.75	Pole + Reinf.	TP41.646x40.757x0.65	Reinf. 1 Compression	72.8%	Pass
16.75 - 16.5	Pole + Reinf.	TP41.693x41.646x0.7625	Reinf. 2 Compression	66.9%	Pass
16.5 - 14.25	Pole + Reinf.	TP42.114x41.693x0.7625	Reinf. 2 Compression	67.5%	Pass
14.25 - 14	Pole + Reinf.	TP42.161x42.114x0.725	Reinf. 2 Compression	67.9%	Pass
14 - 9	Pole + Reinf.	TP43.096x42.161x0.7125	Reinf. 2 Compression	69.1%	Pass
9 - 4.25	Pole + Reinf.	TP43.985x43.096x0.7125	Reinf. 2 Bolt Shear	72.7%	Pass
4.25 - 4	Pole + Reinf.	TP44.032x43.985x0.6	Reinf. 10 Connection	74.0%	Pass
4 - 0	Pole + Reinf.	TP44.78x44.032x0.6	Reinf. 10 Connection	74.8%	Pass
				Summary	
			Pole	64.6%	Pass
	;		Reinforcement	76.4%	Pass
			Overall	76.4%	Pass

Table 5 - Tower Component Stresses vs. Capacity - LC7

Notes	Component	Elevation (ft)	% Capacity	Pass / Fail
1	Anchor Rods	0	60.6	Pass
1	Base Plate	0	56.6	Pass
1	Base Foundation Steel	0	47.2	Pass
1	Base Foundation Soil Interaction	0	32.3	Pass
	Structure Rating (max fr	om all components)=	76.4%

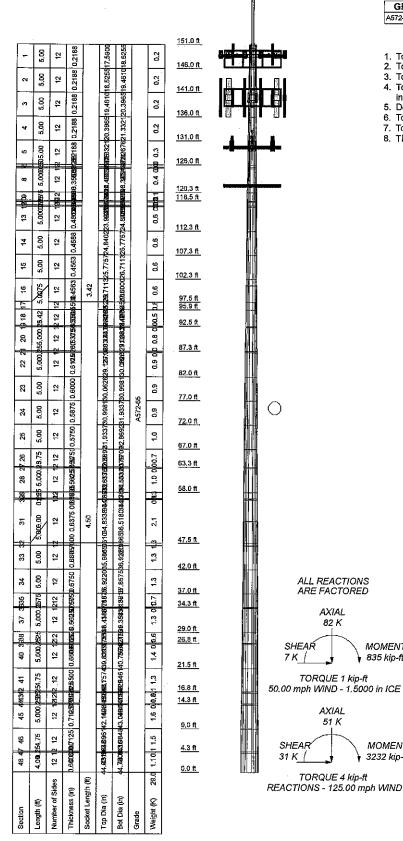
Notes:

4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

All structural ratings are per TIA-222-H Section 15.5 See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

APPENDIX A TNXTOWER OUTPUT



MATERIAL STRENGTH

GRADE	Fy Fy	Fu	GRADE	Fy	Fú
		80 ksi			

TOWER DESIGN NOTES

- Tower is located in New Haven County, Connecticut.
 Tower designed for Exposure B to the TIA-222-H Standard.
- Tower designed for a 125.00 mph basic wind in accordance with the TIA-222-H Standard.
 Tower designed for a 50.00 mph basic wind in accordance with the TIA-222-H Standard.
 Tower is also designed for a 50.00 mph basic wind with 1.50 in ice. Ice is considered to increase in thickness with height.
- 5. Deflections are based upon a 60.00 mph wind.
- 6. Tower Risk Category II.
- 7. Topographic Category 1 with Crest Height of 0.00 ft
- 8. TIA-222-H Annex S

MOMENT

835 kip-ft

MOMENT

3232 kip-ft



Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard.

The following design criteria apply:

- 1) Tower is located in New Haven County, Connecticut.
- 2) Tower base elevation above sea level: 741.00 ft.
- 3) Basic wind speed of 125.00 mph.
- 4) Risk Category II.
- Exposure Category B.
- 6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
- 7) Topographic Category: 1.
- 8) Crest Height: 0.00 ft.
- 9) Nominal ice thickness of 1.5000 in.
- 10) Ice thickness is considered to increase with height.
- 11) Ice density of 56.00 pcf.
- 12) A wind speed of 50.00 mph is used in combination with ice.
- 13) Temperature drop of 50.00 °F.
- 14) Deflections calculated using a wind speed of 60.00 mph.
- 15) TIA-222-H Annex S.
- 16) A non-linear (P-delta) analysis was used.
- 17) Pressures are calculated at each section.
- 18) Stress ratio used in pole design is 1.05.
- 19) Tower analysis based on target reliabilities in accordance with Annex S.
- 20) Load Modification Factors used: $K_{es}(F_w) = 0.95$, $K_{es}(t_i) = 0.85$.
- 21) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification Use Code Stress Ratios

√ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile

Include Bolts In Member Capacity

Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric Distribute Leg Loads As Uniform Assume Legs Pinned

- √ Assume Rigid Index Plate
- ✓ Use Clear Spans For Wind Area
 Use Clear Spans For KL/r
 Retension Guys To Initial Tension
 ✓ Bypass Mast Stability Checks
- √ Use Azimuth Dish Coefficients
- √ Project Wind Area of Appurt.

Autocalc Torque Arm Areas

Add IBC .6D+W Combination Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL/ry For 60 Deg. Angle Legs Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation

√ Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption

Poles
Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No
Appurtenances
Outside and Inside Corner Radii Are
Known

Tapered Pole Section Geometry

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius i n	Pole Grade
L1	151.00-146.00	5.00	0.00	12	17.5900	18.5255	0.2188	0.8752	A572-65 (65 ksi)
L2	146.00-141.00	5.00	0.00	12	18.5255	19.4610	0.2188	0.8752	A572-65 (65 ksi)
L3	141.00-136.00	5.00	0.00	12	19.4610	20.3965	0.2188	0.8752	À572-65 (65 ksi)
L4	136.00-131.00	5.00	0.00	12	20.3965	21.3321	0.2188	0.8752	À572-65 (65 ksi)

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L5	131.00-126.00	5.00	0.00	12	21.3321	22.2676	0.2188	0.8752	A572-65
L6	126.00-125.50	0.50	0.00	12	22.2676	22,3611	0.2188	0.8752	(65 ksi) A572-65
L7	125.50-125.25	0.25	0.00	12	22.3611	22,4079	0.3625	1.4502	(65 ksi) A572-65
L8	125.25-120.25	5.00	0.00	12	22.4079	23.3434	0.3563	1,4252	(65 ksi) A572-65
									(65 ksi)
L9	120.25-118.50	1.75	0.00	12	23,3434	23.6708	0.3563	1.4252	A572-65 (65 ksi)
L10	118.50-118.25	0.25	0.00	12	23.6708	23.7176	0.6438	2.5752	A572-65 (65 ksi)
L11	118.25-117.50	0.75	0.00	12	23.7176	23.8579	0.6438	2.5752	A572-65
L12	117.50-117.25	0.25	0.00	12	23.8579	23,9047	0.4938	1.9752	(65 ksi) A572-65
L13	117.25-112.25	5.00	0.00	12	23.9047	24.8402	0.4813	1.9252	(65 ksi) A572-65
L14	112.25-107.25	5.00	0.00	12	24.8402	25.7757	0.4688	1.8752	(65 ksi) A572-65
									(65 ksi)
L15	107.25-102.25	5.00	0.00	12	25.7757	26.7113	0.4563	1.8252	A572-65 (65 ksi)
L16	102.25-97.50	4.75	3.42	12	26.7113	27.6000	0.4563	1.8252	A572-65 (65 ksi)
L17	97.50-95.92	5.00	0.00	12	26.5233	27.4588	0.5500	2.2000	A572-65 (65 ksi)
L18	95.92-92.50	3.42	0.00	12	27.4588	28.0980	0.5500	2.2000	A572-65
L19	92.50-92.25	0.25	0.00	12	28.0980	28.1447	0.5500	2.2000	(65 ksi) A572-65
L20	92.25-87.25	5.00	0.00	12	28.1447	29.0803	0.5375	2.1500	(65 ksi) A572-65
L21	87.25-87.00	0.25	0.00	12	29.0803	29,1271	0.6250	2.5000	(65 ksi) A572-65
			•						(65 ksi)
L22	87.00-82.00	5.00	0.00	12	29.1271	30.0626	0.6125	2.4500	A572-65 (65 ksi)
L23	82.00-77.00	5.00	0.00	12	30.0626	30.9981	0.6000	2.4000	A572-65 (65 ksi)
L24	77.00-72.00	5.00	0.00	12	30.9981	31.9337	0.5875	2,3500	À572-65 (65 k si)
L25	72.00-67.00	5.00	0.00	12	31.9337	32.8692	0.5750	2.3000	A572-65
L26	67.00-63.25	3.75	0.00	12	32.8692	33.5709	0.5750	2.3000	(65 ksi) A572-65
L27	63.25-63.00	0.25	0.00	12	33.5709	33.6176	0.5750	2.3000	(65 ksi) A572-65
L28	63.00-58.00	5.00	0.00	12	33.6176	34.5532	0.5625	2.2500	(65 ksi) A572 - 65
L29									(65 ksi)
	58.00-56.75	1.25	0.00	12	34.5532	34.7871	0.5625	2.2500	A572 - 65 (65 ksi)
L30	56.75-56.50	0.25	0.00	12	34.7871	34.8338	0.6375	2.5500	A572-65 (65 ksi)
L31	56.50-47.50	9.00	4.50	12	34.8338	36.5180	0.6375	2.5500	A572-65 (65 ksi)
L32	47.50-47.00	5.00	0.00	12	35.0510	35.9865	0.7000	2.8000	A572-65
L33	47.00-42.00	5.00	0.00	12	35,9865	36,9220	0.6875	2.7500	(65 ksi) A572-65
L34	42.00-37.00	5.00	0.00	12	36.9220	37.8575	0.6750	2.7000	(65 ksi) A572-65
L35	37.00-34.25	2.75	0.00	12	37.8575	38.3718	0.6750	2.7000	(65 ksi) A572 - 65
L36	34,25-34.00	0.25	0.00	12	38.3718	38.4186		2.7000	(65 ksi)
							0.6750		A572-65 (65 ksi)
L37	34.00-29.00	5.00	0.00	12	38.4186	39.3541	0.6625	2.6500	A572-65 (65 ksi)
L38	29.00-26.75	2.25	0.00	12	39.3541	39.7751	0.6625	2.6500	À572-65 (65 ksi)
L39	26.75-26.50	0.25	0.00	12	39.775 1	39.8219	0.6625	2.6500	A572-65

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
									(65 ksi)
L40	26.50-21.50	5.00	0.00	12	39,8219	40.7574	0.6500	2.6000	A572-65
									(65 ksi)
L41	21.50-16.75	4.75	0.00	12	40.7574	41.6461	0.6500	2.6000	A572-65
									(65 ksi)
L42	16.75-16.50	0.25	0.00	12	41.6461	41.6929	0.7625	3.0500	A572-65
. 40	40 50 44 05	0.05	0.00	40	44.0000	10.1400	0.7005	0.0500	(65 ksi)
L43	16.50-14.25	2.25	0.00	12	41.6929	42.1138	0.7625	3.0500	A572-65
L44	14.25-14.00	0.25	0.00	12	42.1138	42,1606	0.7250	2.9000	(65 ksi) A572-65
L 44	14.25-14.00	0.25	0.00	12	42.1130	42.1000	0.7250	2.8000	(65 ksi)
L45	14.00-9.00	5.00	0.00	12	42.1606	43.0961	0.7125	2.8500	A572-65
L+0	14.00-3.00	0.00	0.00	12	72.1000	40.0001	0.7 120	2.0000	(65 ksi)
L46	9.00-4.25	4.75	0.00	12	43.0961	43.9848	0.7125	2.8500	A572-65
							****		(65 ksi)
L47	4.25-4.00	0.25	0.00	12	43.9848	44.0316	0.6000	2.4000	À572-65
									(65 ksi)
L48	4.00-0.00	4.00		12	44.0316	44.7800	0.6000	2.4000	À572-65
									(65 ksi)

Tapered Pole Properties

Section	Tip Dia.	Area	1	r	С	I/C	J	lt/Q	W	w/t
	in	in ²	in⁴	in	in	in ³	in⁴	in ²	in	
L1	18.1333	12.2386	471.3881	6.2189	9.1116	51.7348	955.1601	6,0235	4.1277	18.865
	19.1018	12.8977	551.7220	6.5538	9.5962	57.4937	1117.9384	6.3479	4.3785	20.011
L2	19.1018	12.8977	551.7220	6.5538	9.5962	57.4937	1117.9384	6.3479	4.3785	20.011
	20.0704	13.5568	640,7007	6.8887	10.0808	63,5565	1298,2334	6.6723	4.6292	21.157
L3	20.0704	13.5568	640.7007	6.8887	10.0808	63.5565	1298.2334	6.6723	4.6292	21.157
	21.0389	14.2159	738.7659	7.2236	10.5654	69.9231	1496.9400	6.9967	4.8799	22.303
L4	21.0389	14,2159	738,7659	7,2236	10.5654	69.9231	1496.9400	6.9967	4.8799	22,303
	22.0074	14.8750	846.3593	7.5585	11.0500	76.5936	1714.9535	7.3210	5.1306	23.449
L5	22.0074	14.8750	846.3593	7.5585	11.0500	76.5936	1714.9535	7.3210	5.1306	23.449
	22,9759	15,5342	963.9228	7.8935	11.5346	83.5679	1953.1689	7.6454	5.3813	24,595
L6	22.9759	15.5342	963.9228	7.8935	11.5346	83.5679	1953.1689	7.6454	5.3813	24.595
	23.0728	15.6001	976.2445	7.9270	11.5831	84.2821	1978.1360	7.6779	5.4064	24.709
L7	23.0220	25.6814	1586.3287	7.8755	11.5831	136.9525	3214.3320	12.6396	5.0211	13.85
	23.0705	25.7360	1596.4693	7.8922	11.6073	137.5402	3234.8795	12.6665	5.0337	13.884
L8	23.0727	25.2995	1570.2825	7.8945	11.6073	135.2842	3181.8181	12.4516	5.0504	14.175
	24.0412	26.3728	1778.7333	8.2294	12.0919	147,1014	3604,1959	12.9799	5.3012	14.878
L9	24.0412	26.3728	1778.7333	8.2294	12.0919	147.1014	3604.1959	12.9799	5.3012	14.878
	24.3802	26.7484	1855.8303	8.3466	12.2615	151.3543	3760.4153	13.1648	5.3889	15.125
L.10	24.2787	47.7359	3230,7786	8.2437	12.2615	263.4898	6546.4334	23.4942	4.6184	7.174
	24.3272	47.8329	3250.5071	8.2604	12.2857	264.5759	6586.4086	23.5419	4.6309	7.193
L11	24.3272	47.8329	3250.5071	8.2604	12.2857	264.5759	6586,4086	23.5419	4.6309	7.193
	24,4725	48,1238	3310.1739	8.3107	12.3584	267.8478	6707.3098	23.6850	4.6685	7.252
L12	24.5254	37.1498	2588.4664	8.3644	12.3584	209.4497	5244.9346	18.2840	5.0705	10.268
	24.5738	37,2242	2604.0441	8.3811	12.3826	210.2979	5276.4993	18.3206	5.0831	10,294
L13	24.5782	36.3013	2542.1934	8.3856	12.3826	205.3029	5151.1730	17.8664	5,1166	10.631
	25.5467	37.7511	2859.1208	8.7205	12.8672	222.2015	5793.3538	18.5800	5.3673	11.152
L14	25.551 1	36.7896	2789.1550	8.7250	12.8672	216.7640	5651.5843	18.1067	5.4008	11.52
	26.5196	38.2017	3122.8328	9.0599	13,3518	233.8879	6327,7058	18.8017	5.6515	12.055
L15	26.5241	37.2015	3044.0724	9.0644	13.3518	227.9890	6168.1159	18.3095	5.6850	12.459
	27.4926	38.5760	3394.11 4 2	9.3993	13,8364	245,3027	6877,3957	18.9860	5.9357	13.008
L16	27.4926	38.5760	3394,1142	9.3993	13.8364	245.3027	6877.3957	18.9860	5.9357	13.008
	28.4127	39.8819	3750.5886	9.7174	14.2968	262.3376	7599.7094	19.6286	6.1739	13.53
L17	27.9266	45.9986	3960,8075	9.2984	13.7390	288.2884	8025.6699	22.6391	5.6342	10.244
	28,2334	47,6555	4404.4058	9.6333	14.2237	309.6536	8924.5203	23.4546	5.8850	10.7
L18	28.2334	47.6555	4404.4058	9.6333	14.2237	309.6536	8924.5203	23.4546	5.8850	10.7
	28.8951	48.7874	4725.7713	9.8622	14.5547	324.6895	9575.6939	24.0117	6.0563	11.011
L19	28.8951	48.7874	4725.7713	9.8622	14.5547	324.6895	9575.6939	24.0117	6.0563	11.011
	28.9436	48.8703	4749.8856	9.8789	14.5790	325.8039	9624.5559	24.0525	6.0688	11.034
L20	28.9480	47,7812	4648.2446	9.8834	14.5790	318.8321	9418.6039	23.5165	6.1023	11.353
	29.9165	49.4004	5136.9910	10.2183	15.0636	341.0206	10408.936 5	24.3134	6.3530	11.82
L21	29.8856	57.2662	5918.4793	10.1870	15.0636	392.8999	11992.443 6	28.1847	6.1185	9.79

Section	Tip Dia.	Area	1	r	С	I/C	J	It/Q	w	w/t
-	<i>in</i> 29.9341	in² 57.3604	<i>in</i> ⁴ 5947,7151	in 10.2037	<u>in</u> 15.0878	in ³ 394.2066	<i>in⁴</i> 12051.683	in ² 28.2310	<u>in</u> 6.1310	9.81
L22	29.9385	56.2378	5836.4330	10.2082	15.0878	386,8310	2 11826.195	27.6785	6.1645	10.065
	30.9070	58.0829	6429.9530	10.5431	15.5724	412.9064	6 13028.827	28.5867	6.4153	10.474
L23	30.9114	56.9217	6306.7533	10.5476	15.5724	404.9950	9 12779.191	28.0151	6.4488	10.748
	31.8800	58.7292	6926.8161	10.8825	16.0570	431.3883	14035.607	28.9047	6.6995	11.166
L24	31.8844	57.5293	6790.8780	10.8870	16.0570	422.9224	13760.159	28.3142	6.7330	11.46
	32.8529	59.2991	7437.0912	11.2219	16.5416	449.5982	15069.563	29.1852	6.9837	11.887
L.25	32.8573	58.0606	7287.5666	11.2264	16.5416	440.5589	2 14766.585	28.5756	7.0172	12.204
	33.8259	59.7927	7959.4601	11.5613	17.0263	467.4 817	16128.024 0	29.4282	7.2679	12.64
L26	33.8259	59.7927	7959.4601	11.5613	17.0263	4 67.4817	16128.024	29.4282	7.2 679	12.64
	34.5523	61.0918	8489.6181	11.8125	17.3897	488.1979	17202.267 9	30.0675	7.4560	12.967
L27	34.5523	61.0918	8489.6181	11.8125	17.3897	488.1979	17202.267 9	30.0675	7.4560	12.967
	34.6007	61.1784	8525.775 5	11.8293	17.4139	489.5949	1 72 75.532	30.1102	7.4685	12.989
L28	34.6051	59.8711	8349.9017	11.8337	17.4139	479.4953	16919.164 6	29.4667	7.5020	13.337
	35.5737	61.5656	9079,1230	12.1687	17.8985	507.2547	18396.764 7	30.3007	7.7528	13.783
L29	35.5737	61.5656	9079.1230	12.1687	17.8985	507.2547	18396.76 4	30.3007	7.7528	13.783
	35.8158	61.9892	9267.8319	12.2524	18.0197	514.3167	18779.140	30.5092	7.8154	13.894
L30	35.7893	70.1005	10434.641 4	12,2255	18.0197	579.0686	21143.412	34.5013	7.614 4	11.944
	35.8378	70.1965	10477.579 3	12,2423	18.0439	580.6706	21230.416	34.5486	7.6270	11.964
L31	35.8378	70.1965	10477.579	12.2423	18.0439	580.6706	21230.416	34.5486	7.6270	11.964
	37.5813	73.6537	12103.123 6	12.8452	18.9163	639.8243	24524.209 8	36.2501	8.0783	12.672
L32	36.9122	77.4272	11661.611 3	12.2977	18.1564	642.2856	23629.586	38.1073	7.5177	10.74
	37.0090	79.5358	12640.552 2	12.6326	18.6410	678.1044	25613.185 9	39.1451	7.7684	11.098
L33	37.0135	78.1432	12428.026 4	12.6370	18.6410	666.7034	25182.550 8	38.4597	7.8019	11.348
	37.9820	80.2141	13442.550 4	12.9720	19.1256	702.8564	27238.251 5	39.4790	8.0526	11.713
L34	37.9864	78.7829	13211.804	12.9764	19.1256	690.7916	26770.697 1	38.7745	8.0861	11.979
	38.9549	80.8162	14261.381	13.3113	19.6102	727.2434	28897.424 4	39.7753	8.3368	12.351
L35	38.9549	80.8162	14261.381 n	13.3113	19.6102	727.2434	28897.424	39.7753	8.3368	12.351
	39.4873	81.9341	14861.427 8	13.4955	19.8766	747.6841	30113.281	40.3255	8.4747	12.555
L36	39.4873	81.9341	14861.427 8	13.4955	19.8766	747.6841	30113.281	40.3255	8.4747	12.555
	39.5358	82.0358	14916.817 4	13,5122	19.9008	749.5570	30225.516	40.3755	8.4872	12.574
L37	39.5402	80.5432	14655.131 0	13.5167	19.9008	736.4075	29695,268 5	39.6409	8.5207	12.861
	40.5087	82.5389	15771.691 9	13.8516	20.3854	773.6747	31957.723 8	40.6231	8.7714	13.24
L38	40.5087	82.5389	15771.691 9	13.8516	20,3854	773.6747	_	40.6231	8.7714	13,24
	40.9445	83.4369	16292.112 5	14.0023	20.6035	790.7450	33012.236 9	41.0651	8.8842	13.41

Section	Tip Día. in	Area in²	/ in⁴	r in	C in	I/C in³	J in⁴	lt/Q in²	w in	w/t
L39	40.9445	83.4369	16292,112 5	14.0023	20.6035	790,7450	33012.236 9	41.0651	8.8842	13.41
	40.9929	83.5367	16350.633 8	14.0191	20.6277	792.6533	33130.816 9	41.1142	8.8968	13.429
L40	40.9973	81.9867	16057.498 5	14.0235	20.6277	778.4425	32536.845 3	40.3514	8.9303	13.739
	41.9658	83,9447	17235.641 4	14.3584	21.1123	816.3786	34924.082 2	41.3150	9.1810	14.125
L41	41.9658	83,9447	17235,641 4	14.3584	21.1123	816.3786	34924.082 2	41.3150	9.1810	14.125
	42.8859	85.8048	18406.969 6	14.676 6	21.5727	853.2541	37297.510 8	42.2305	9.4192	14.491
L42	42.8462	100.3794	21415.516 1	14.6363	21.5727	992.7151	43393.641 7	49.4037	9.1177	11.958
	42.8946	100.4943	21489.104 6	14.6531	21.5969	995.0087	43542.752 0	49.4602	9.1302	11.974
L43	42.8946	100,4943	21489.104 6	14.6531	21.5969	995.0087	43542.752 0	49.4602	9.1302	11.974
	43.3305	101.5279	22159.001 9	14.8038	21.8150	1015.7707	6	49.9689	9.2430	12.122
L44	43.3437	96.6222	21126.587 6	14.8172	21.8150	968.4447	42808.194 3	47.5545	9.3435	12.888
	43.3921	96.7314	21198.296 2	14.8339	21.8392	970.6538	42953.495 2	47.6083	9.3560	12.905
L45	43.3965	95.0923	20851.668 1	14.8384	21,8392	954.7819	42251.132 7	46.8015	9.3895	13.178
	44.3650	97.2386	22295.661 5	15.1733	22.3238	998.7403	45177.054 9	47.8579	9.6403	13.53
L46	44.3650	97.2386	22295.661 5	15.1733	22.3238	998.7403	45177.054 9	47.8579	9.6403	13.53
	45.2851	99.2775	23727.798 7	15.4915	22.7841		48078.953 0	48.8614	9.8784	13.864
L47	45.3248	83.8195	20137.552 7	15.5318	22.7841	883.8408	40804.141 3	41.2534	10.1799	16.967
	45,3732	83.9099	20202.756 1	15.5485	22.8084	885.7606	40936.261 2	41.2979	10.1925	16.987
L48	45,3732	83.9099	20202.756 1	15.5485	22.8084	885.7606	40936.261 2	41.2979	10.1925	16.987
	46.1480	85.3558	21265.236 0	15.8164	23.1960	916.7615	43089.133 4	42.0095	10.3930	17.322

Tower Elevation ft	Gusset Area (per face) ft²	Gusset Thickness in	Gusset Grade Adjust. Factor A _f	Adjust. Factor Ar	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L1 151.00-			1	1	1			
146.00								
L2 146.00-			1	1	1			
141.00								
L3 141.00-			1	1	1			
136.00					4			
L4 136.00-			1	1	1			
131.00 L5 131.00-			4	4	4			
126.00			1	1	1			
L6 126.00-			1	4	4			
125,50			ı	Ī	į			
L7 125.50-			1	1	0.948306			
125.25			,	•	0.010000			
L8 125,25-			1	1	0.950399			
120.25								
L9 120.25-			1	1	0.945676			
118.50								
L10 118.50-			1	1	0.906367			
118.25								
L11 118.25-			1	1	0.902943			
117.50								

Tower Elevation ft	Gusset Area (per face) ft²	Gusset Thickness in	Gusset Grade Adjust. Factor Aı	Adjust. Factor Ar	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Stitch Bolt Spacing
L12 117.50-			1	1	0.932549			
117.25 L13 117.25-			1	1	0.936991			
112,25 L14 112.25-			1	1	0.943192			
107.25								
L15 107.25- 102.25			1	1	0.951126			
L16 102.25-			1	1	0.946685			•
97.50 L17 97.50-			1	1	0.951449			
95.92 L18 95.92-			1	1	0.942557			
92.50								
L19 92.50- 92.25			. 1	1	0.941922			
L20 92.25-			1	1	0.95087			
87.25 L21 87.25-			1	1	0.931036			
87.00 L22 87.00-			1	1	0.935662			
82.00 L23 82.00-				1				
77.00			1		0.941395			
L24 77.00- 72.00			1	1	0.948222			
L25 72.00-			1	1	0.956139			
67.00 L26 67.00-			1	1	0.947363			
63.25 L27 63,25-			1	1	0.946792			
63.00								
L28 63.00- 58.00			1	1	0.956128			
L29 58.00- 56.75		•	1	1	0.953391			
L30 56.75-			1	1	0.949588			
56.50 L31 56.50-			1	1	0.938546			
47.50 L32 47.50-			1	1	0.941986			
47.00								
L33 47.00- 42.00			1	1	0.948102			
L34 42.00- 37.00			1	1	0.955017			
L35 37.00-			1	1	0.949567			
34.25 L36 34.25-			1	1	0.949078			
34.00 L37 34.00-			1	1	0.956979			
29.00								
L38 29.00- 26.75			1	1	0.952771			
L39 26,75- 26.50			1	1	0.952309			
26.50 L40 26.50-			1	1	0.961137			
21.50 L41 21.50-			1	1	0.952808			
16.75								
L42 16.75- 16.50			1	1	1.02585			
L43 16.50- 14.25			1	1	1.02042			
L44 14.25-			1	1	0.961601			
14.00								

Tower Elevation ft	Gusset Area (per face) ft²	Gusset Thickness in	Gusset Grade Adjust. Factor Ar	Adjust. Factor Ar	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals in	Double Angle Stitch Bolt Spacing Horizontals in	Double Angle Stitch Bolt Spacing Redundants in
L45 14,00-			1	1	0.968203			
9.00								
L46 9.00-4,25			1	1	0.959127			
L47 4.25-4.00			1	1	1.0012			
L48 4.00-0.00			1	1	0.994823			

Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Exclude From Torque	Componen t Type	Placement ft	Total Number	Number Per Row	Start/En d Position	Diamete r	Perimete r in	Weight plf
***		Calculation	 .					in		
AL7-50(1-5/8)	В	No	Surface Ar (CaAa)	122.00 - 0.00	7	4	0.042 0.167	1.9600		0.52
**********	***									
MS-850 (L)	Α	No	Surface Af	30.50 -	1	1	0.250	8.5000	19.5000	0.00
		110	(CaAa)	10.50	•	•	0.250	0.0000	13.0000	0.00
MS-850 (L)	С	No	Surface Af	30.50 -	1	1	0.250	8.5000	19.5000	0.00
MS-850 (L.)	В	No	(CaAa) Surface Af	0.50 30.50 -	1	1	0.250 0.250	8.5000	19.5000	0.00
1110 000 (L)		740	(CaAa)	0.50	'	•	0.250	0.0000	13.3000	0.00
MS-850 (L)	В	No	Surface Af	20.50 -	1	1	-0.500	8.5000	19.5000	0.00
MS-850 (L)	Α	No	(CaAa) Surface Af	0.50 20.50 -	1	1	-0.500 0.000	0 5000	10 5000	0.00
1010-030 (L)	^	NO	(CaAa)	0.50	· ·	'	0.000	8.5000	19,5000	0.00
MS-850 (L)	С	No	Surface Af	40.00 -	1	1	0.000	8.5000	19.5000	0.00
MC OED (II)	В	No	(CaAa)	21.00	4	4	0.000	0.5000	40 5000	0.00
MS-850 (L)	В	No	Surface Af (CaAa)	40.00 - 21.00	1	1	0.000 0.000	8.5000	19.5000	0.00
MS-850 (L)	Α	No	Surface Af	40.00 -	1	1	0.000	8.5000	19.5000	0.00
140 000 (1)			(CaAa)	21.00			0.000			
MS-850 (L)	С	No	Surface Af (CaAa)	60.50 - 30.50	1	1	0.250 0.250	8.5000	19.5000	0.00
MS-850 (L)	В	No	Surface Af	60.50 -	1	1	0.250	8.5000	19.5000	0.00
			(CaAa)	30.50			0.250			
MS-850 (L)	Α	No	Surface Af (CaAa)	60,50 - 30.50	1	1	0.250	8.5000	19.5000	0.00
MS-650 (L)	С	No	Surface Af	69.67 -	1	1	0.250 0.000	6.5000	15.5000	0.00
			(CaAa)	51.33			0.000			
MS-650 (L)	В	No	Surface Af	69.67 -	1	1	0.000	6.5000	15.5000	0.00
MS-650 (L)	Α	No	(CaAa) Surface Af	51.33 69.67 -	1	1	0.000 0.000	6.5000	15.5000	0.00
(-)			(CaAa)	51.33	•	•	0.000	0.0000	10.0000	0.00
MS-650 (L)	С	No	Surface Af	90.50 -	1	1	0.250	6.5000	15.5000	0.00
MS-650 (L)	В	No	(CaAa) Surface Af	60.50 90.50 -	1	1	0.250 0.250	6.5000	15.5000	0.00
		140	(CaAa)	60.50		,	0.250	0.3000	13.3000	0.00
MS-650 (L)	Α	No	Surface Af	90.50 ~	1	1	0.250	6.5000	15.5000	0.00
MS-600 (L)	С	No	(CaAa) Surface Af	60.50 98.58 -	1	1	0.250 0.000	6.0000	14 0000	0.00
WIS-000 (L)	· ·	IVO	(CaAa)	82.42	'	•	0.000	0.0000	14.0000	0.00
MS-600 (L)	В	No	Surface Af	98.58 -	1	1	0.000	6.0000	14.0000	0.00
Me eng (L)	٨	No	(CaAa)	82.42	4	4	0.000	e 0000	44.0000	0.00
MS-600 (L)	Α	No	Surface Af (CaAa)	98.58 - 82.42	1	1	0.000 0.000	6.0000	14.0000	0.00
MS-600 (L)	С	No	Surface Af	120.50 -	1	1	0.250	6.0000	14.0000	0.00
MD 600 (L)	В	NI-	(CaAa)	90.50		4	0.250	0.0000	44.0005	
MS-600 (L)	В	No	Surface Af (CaAa)	120.50 - 90.50	1	1	0.250 0.250	6.0000	14.0000	0.00
MS-600 (L)	Α	No	Surface Af	120.50 -	1	1	0.250	6.0000	14.0000	0.00
*			(CaAa)	90.50			0.250			
MP3-03 (L)	С	No	Surface Af	125,00 -	1	1	-0.250	4.0600	11,2600	0.00
5 55 (2)	•		(CaAa)	115.00	•	'	-0.250	1.0000	11,2000	0.00

Description	Sector	Exclude From Torque Calculation	t Type	Placement ft		Number Per Row	Start/En d Position	Width or Diamete r in	Perimete r in	Weight plf
MP3-03 (L)	В	No	Surface Af	125.00 -	1	1	-0.250	4.0600	11.2600	0.00
			(CaAa)	115.00	_	_	-0.250			
MP3-03 (L)	Α	No	Surface Af	125.00 -	1	1	-0.250	4.0600	11.2600	0.00
			(CaAa)	115.00			-0.250			

							-		
Description	Face	Allow	Exclude	Componen	Placement	Total		C _A A _A	Weight
	or	Shield	From	$_{-}^{t}$	ft	Number		ft²/ft	plf
	Leg		Torque	Туре					
***			Calculation						

LDF2-50(3/8)	С	No	No	Incido Dolo	148.00 - 0.00	2	No Ice	0.00	0.08
EDI 2-30(3/0)	U	INO	140	maide r die	140.00 - 0.00	2	1/2" Ice	0.00	0.08
							1" Ice	0.00	0.08
							2" Ice	0.00	0.08
9776(5/8)	С	No	No	Inside Pole	148.00 - 0.00	2	No Ice	0.00	0.28
3113(3/3)	•	140	140	molde i die	140.00 - 0.00	~	1/2" Ice	0.00	0.28
							1" Ice	0.00	0.28
							2" Ice	0.00	0.28
LDF7-50A(1-5/8)	С	No	No	Inside Pole	148.00 - 0.00	12	No ice	0.00	0.82
22.7.03.4(1.0/0)					1.0.00 0.00		1/2" Ice	0.00	0.82
							1" ice	0.00	0.82
							2" Ice	0.00	0.82
2" (Nominal)	С	No	No	Inside Pole	148.00 - 0.00	1	No Ice	0.00	0.72
Conduit	-						1/2" Ice	0.00	0.72
							1" Ice	0.00	0.72
							2" Ice	0.00	0.72
*									
810921-001(7/8)	С	No	No	Inside Pole	148.00 - 0.00	2	No Ice	0.00	0.40
` '							1/2" Ice	0.00	0.40
							1" lce	0.00	0.40
							2" lce	0.00	0.40

LDF7-50A(1-5/8)	С	No	No	Inside Pole	140.00 - 0.00	12	No Ice	0.00	0.82
							1/2" lce	0.00	0.82
							1" Ice	0.00	0.82
							2" Ice	0.00	0.82
HB158-1-08U8-	С	No	No	Inside Pole	140.00 - 0.00	1	No Ice	0.00	1.30
S8J18(1-5/8)							1/2" Ice	0.00	1.30
							1" Ice	0.00	1,30
							2" Ice	0.00	1.30
***	_								
LDF4-50A(1/2)	С	No	No	Inside Pole	130.00 - 0.00	1	No Ice	0.00	0.15
							1/2" Ice	0.00	0.15
							1" Ice	0.00	0.15
1 DEZ 504 (4 5/5)	_			t day by	400.00 0.00		2" ice	0.00	0.15
LDF7-50A(1-5/8)	С	No	No	inside Pole	130.00 - 0.00	3	No Ice	0.00	0.82
							1/2" Ice	0.00	0.82
							1" Ice	0.00	0.82
LIDAAA GALIOMAG	_	N1~	NIA	Innide Dal-	120.00 0.00	4	2" Ice	0.00	0.82
HB114-21U3M12-	С	No	No	inside Pole	130.00 - 0.00	1	No Ice 1/2" [ce	0.00	1,22
XXXF(1-1/4)								0.00	1.22 1.22
							1" lce	0.00	1.22 1,22
							2" Ice	0,00	1,22

Feed Line/Linear Appurtenances Section Areas

Tower Sectio n	Tower Elevation ft	Face	A _R ft²	A _F ft²	C₄A₄ In Face ft²	C _A A _A Out Face ft²	Weight K
L1	151.00-146.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00

Tower	Tower	Face	AR	A_F	CAAA	C_AA_A	Weight
Sectio n	Elevation ft		ft²	ft²	In Face ft²	Out Face	К
	п	Ç	0.000	0.000	0.000	ft²0.000	0.02
L2	146.00-141.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
	444.00.400.00	Ċ	0.000	0.000	0.000	0.000	0.06
L3	141.00-136.00	A	0.000	0.000	0.000	0.000	0.00
		B C	0.000	0.000	0.000	0.000	0.00
L4	136.00-131.00	Ä	0.000 0.000	0.000 0.000	0.000 0.000	0.000 0.000	0.10 0.00
	100.00-101.00	В	0.000	0.000	0.000	0.000	0.00
		c	0.000	0.000	0.000	0.000	0.12
L5	131.00-126.00	Α	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
	100.00.105.50	Ç	0.000	0.000	0.000	0.000	0.13
L6	126.00-125.50	A	0.000	0.000	0.000	0.000	0.00
		B C	0.000 0.000	0.000 0.000	0.000 0.000	0.000	0.00
L7	125.50-125.25	Ä	0.000	0.000	0.000	0.000 0.000	0.01 0.00
	120.00 120.20	В	0.000	0.000	0.000	0.000	0.00
		Ċ	0.000	0.000	0.000	0.000	0.01
L8	125.25-120.25	Α	0.000	0.000	3.464	0.000	0.00
		₿	0.000	0.000	4.836	0.000	0.01
		Ċ	0.000	0.000	3.464	0.000	0.14
L9	120.25-118.50	A	0.000	0.000	2.934	0.000	0.00
		B C	0.000	0.000	4.306	0.000	0.01
L10	118.50-118.25	Ä	0.000 0.000	0.000 0.000	2.934 0.419	0.000 0.000	0.05
_10	110.00-110.20	B	0.000	0.000	0.615	0.000	0.00 0.00
		č	0.000	0.000	0.419	0.000	0.01
L11	118.25-117.50	Α	0.000	0.000	1.258	0.000	0.00
		В	0.000	0.000	1.846	0.000	0.00
		Ç	0.000	0.000	1.258	0.000	0.02
L12	117.50-117.25	Ā	0.000	0.000	0.419	0.000	0.00
		В	0.000	0.000	0.615	0.000	0.00
L13	117.25-112.25	C	0.000	0.000	0.419	0.000	0.01
1.13	117.20-112.20	A B	0.000 0.000	0.000 0.000	6.523 10.443	0.000 0.000	0.00 0.02
		č	0.000	0.000	6.523	0.000	0.02
L14	112.25-107.25	Ā	0.000	0.000	5.000	0.000	0.00
		В	0.000	0.000	8.920	0.000	0.02
		С	0.000	0.000	5.000	0.000	0.14
L15	107.25-102.25	A	0.000	0.000	5.000	0.000	0.00
		В	0.000	0.000	8.920	0.000	0.02
L16	102.25-97.50	C A	0.000 0.000	0.000 0.000	5.000	0.000	0.14
LIU	102.20-97.50	В	0.000	0.000	5.830 9.554	0.000 0.000	0.00 0.02
		č	0.000	0.000	5.830	0.000	0.02
L17	97.50-95.92	Ã	0.000	0.000	3.168	0.000	0.00
		В	0.000	0.000	4.410	0.000	0.01
		С	0.000	0.000	3.168	0.000	0.04
L18	95.92-92.50	A	0.000	0.000	6.832	0.000	0.00
		В	0.000	0.000	9.510	0.000	0.01
L19	92.50-92.25	C A	0.000	0.000	6.832	0.000	0.09
LIÐ	8 4. 30-82.23	B B	0.000 0.000	0.000 0.000	0.500 0.696	0.000	0.00
		Č	0.000	0.000	0.500	0.000 0.000	0.00 0.01
L20	92.25-87.25	Ă	0.000	0.000	10.271	0.000	0.00
		В	0,000	0.000	14.191	0.000	0.02
		С	0.000	0.000	10.271	0.000	0.14
L21	87.25-87.00	Α	0.000	0.000	0.521	0.000	0.00
		В	0.000	0.000	0.717	0.000	0.00
1 22	07 00 00 00	C	0.000	0.000	0.521	0.000	0.01
L22	87.00-82.00	A	0.000	0.000	9.997	0.000	0.00
		B C	0.000 0.000	0.000 0.000	13.917 9.997	0.000 0.000	0.02
L23	82.00-77.00	Ā	0.000	0.000	9.997 5. 41 7	0.000	0.14 0.00
_		B	0.000	0.000	9.337	0.000	0.00
		Č	0.000	0.000	5.417	0.000	0.02
	77.00.70.00	Ā	0.000	0.000	5.417	0.000	0.00
L24	77.00-72.00	^	0.000	0.000	· · · · ·	0.000	0.00

Tower	Tower	Face	AR	A_F	G _A A _A	CAAA	Weight
Sectio n	Elevation #		ft ²	ft²	In Face	Out Face	ĸ
	ft	С	0.000	 0.000	ft² 5.417	ft² 0.000	0.14
L25	72.00-67.00	Ă	0.000	0.000	8.309	0.000	0.00
		В	0.000	0.000	12.229	0.000	0.02
		C	0.000	0.000	8.309	0.000	0.14
L26	67.00-63.25	A	0.000	0.000	8.125	0.000	0.00
		В	0.000	0.000	11.065	0.000	0.01
L27	63.35.63.00	C	0.000	0.000	8.125	0.000	0.10
LZI	63.25-63.00	A B	0.000 0.000	0.000 0.000	0.542 0.738	0.000	0.00
		Č	0.000	0.000	0.736	0.000 0.000	0.00 0.01
L28	63.00-58.00	Ă	0.000	0.000	11.667	0.000	0.00
		В	0.000	0.000	15.587	0.000	0.02
		С	0.000	0.000	11.667	0.000	0.14
L29	58.00-56.75	A	0.000	0.000	3.125	0.000	0.00
		В	0.000	0.000	4.105	0.000	0.00
L30	E6 75 56 50	Ç	0.000	0.000	3.125	0.000	0.03
LJU	56.75-56.50	A B	0.000 0.000	0.000	0.625	0.000	0.00
		Č	0.000	0.000 0.000	0.821 0.625	0.000 0.000	0.00 0.01
L31	56.50-47.50	Ä	0.000	0.000	18.352	0.000	0.00
== :	33.33	В	0.000	0.000	25.409	0.000	0.03
		С	0.000	0.000	18.352	0.000	0.24
L32	47.50-47.00	Α	0.000	0.000	0.708	0.000	0.00
		В	0.000	0.000	1.100	0,000	0.00
	47.00.40.00	Ç	0.000	0.000	0.708	0.000	0.01
L33	47.00-42.00	A	0.000	0.000	7.083	0.000	0.00
		B C	0.000	0.000	11.003	0.000	0.02
L34	42.00-37.00	Ā	0.000 0.000	0.000 0.000	7.083 11.335	0.000	0.14
LUT	42.00-07.00	B	0.000	0.000	15.255	0.000 0.000	0.00 0.02
		č	0.000	0.000	11.335	0.000	0.14
L35	37.00-34.25	Α	0.000	0.000	7.789	0.000	0.00
		В	0.000	0.000	9.944	0.000	0.01
		С	0.000	0.000	7.789	0.000	0.07
L36	34.25-34.00	A	0.000	0.000	0.708	0.000	0.00
		В	0.000	0.000	0.904	0.000	0.00
L37	34.00-29.00	C	0.000	0.000	0.708	0.000	0.01
LOI	34.00-29.00	A B	0.000 0.000	0.000 0.000	14. 1 67 18.087	0.000	0.00
		Č	0.000	0.000	14.167	0.000 0.000	0.02 0.14
L38	29.00-26.75	Ã	0.000	0.000	6.375	0.000	0.00
		В	0.000	0.000	8,139	0.000	0.01
		С	0.000	0.000	6.375	0.000	0.06
L39	26.75-26.50	Α	0.000	0.000	0.708	0.000	0.00
		В	0.000	0.000	0.904	0.000	0.00
1.40	00 50 04 50	C	0.000	0.000	0.708	0.000	0.01
L40	26.50-21.50	A	0.000	0.000	14.167 18.087	0.000	0.00
		B C	0.000 0.000	0.000 0.000		0.000	0.02
L41	21.50-16.75	Ä	0.000	0.000	14.167 12.750	0.000 0.000	0.14 0.00
		B	0.000	0.000	16.474	0.000	0.00
		Ċ	0.000	0.000	7.438	0.000	0.13
L42	16.75-16.50	Α	0.000	0.000	0.708	0.000	0.00
		В	0.000	0.000	0.904	0.000	0.00
1.40	40 =0 11 ==	C	0.000	0.000	0.354	0.000	0.01
L43	16.50-14.25	A	0.000	0.000	6.375	0.000	0.00
		В	0.000	0.000	8.139	0.000	0.01
L44	14.25-14.00	C A	0.000 0.000	0.000 0.000	3.188 0.708	0.000	0.06
<u>-</u> 77	17.40-14.00	В	0.000	0.000	0.708	0.000 0.000	0.00 0.00
		č	0.000	0.000	0.354	0.000	0.00
L45	14.00-9.00	Ă	0.000	0.000	12.042	0.000	0.00
		В	0.000	0.000	18.087	0.000	0.02
		Ċ	0.000	0.000	7.083	0.000	0.14
L46	9.00-4.25	Α	0.000	0.000	6.729	0.000	0.00
		В	0.000	0.000	17.182	0.000	0.02
		C	0.000	0.000	6.729	0.000	0.13
L47	4.25-4.00	A B	0.000 0.000	0.000 0.000	0.354 0.904	0.000 0.000	0.00 0.00

Tower Sectio n	Tower Elevation ft	Face	A _R ft ²	A _F	C _A A _A In Face ft²	C _A A _A Out Face ft ²	Weight K
		С	0.000	0.000	0.354	0.000	0.01
L48	4.00-0.00	Α	0.000	0.000	4.958	0.000	0.00
		В	0.000	0.000	13.053	0.000	0.01
		С	0.000	0.000	4.958	0.000	0.11

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A _R	A_{\digamma}	C _A A _A	CAAA	Weight
Sectio n	Elevation ft	or Leg	Thickness in	ft²	ft²	In Face ft²	Out Face ft²	Κ
L1	151.00-146.00	A	1.482	0.000	0.000	0.000	0.000	0.00
	101100 110100	В	1.102	0.000	0.000	0.000	0.000	0.00
		č		0.000	0.000	0.000	0.000	0.02
L2	146.00-141.00	Ã	1.477	0.000	0.000	0.000	0.000	0.02
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	0.000	0.06
L3	141.00-136.00	Α	1.472	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	0.000	0.10
Ĺ4	136.00-131.00	Α	1.466	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	0.000	0.12
L5	131.00-126.00	A	1 .4 61	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
1.0	400.00.405.50	Ċ	4 155	0.000	0.000	0.000	0.000	0.13
L6	126.00-125.50	A	1.458	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
L7	125.50-125.25	Ċ	4.457	0.000	0.000	0.000	0.000	0.01
L/	120.50-125.25	A B	1.457	0.000	0.000	0.000	0.000	0.00
		Ĉ		0.000 0.000	0.000	0.000	0.000	0.00
L8	125.25-120.25	Ä	1.454	0.000	0.000	0.000	0.000	0.01
LO	120,20-120,20	B	1.404	0.000	0.000 0.000	4.411	0.000	0.05
		C		0.000	0.000	6.762 4.411	0.000 0.000	0.08 0.18
L9	120,25-118,50	Ä	1.450	0.000	0.000	3.763	0.000	0.18
	120.20 110.00	В	1.400	0.000	0.000	6.112	0.000	0.04
		č		0.000	0.000	3.763	0.000	0.07
L10	118.50-118.25	Ă	1.449	0.000	0.000	0.537	0.000	0.00
	***************************************	В		0.000	0.000	0.873	0.000	0.01
		C		0.000	0.000	0.537	0.000	0.01
L11	118.25-117,50	Α	1.448	0.000	0.000	1,612	0.000	0.02
		В		0.000	0.000	2.619	0.000	0.03
		С		0.000	0.000	1.612	0.000	0.04
L12	117.50-117.25	Α	1.447	0.000	0.000	0.537	0.000	0.01
		В		0.000	0.000	0.873	0.000	0.01
		Ç		0.000	0.000	0.537	0.000	0.01
L13	117.25-112.25	Α	1.444	0.000	0,000	8.378	0.000	0.08
		В		0.000	0.000	15.084	0.000	0.18
	440.05.407.05	Ç	4 155	0.000	0.000	8.378	0.000	0.21
L14	112.25-107.25	A	1.438	0.000	0.000	6.438	0.000	0.05
		B C		0.000	0.000	13.135	0.000	0.15
L15	107.25-102.25		4 404	0.000	0.000	6.438	0.000	0.19
LIS	107.25-102.25	A B	1.431	0.000	0.000	6.431	0.000	0.05
		Č		0.000 0.000	0.000 0.000	13.120	0.000	0.15
L16	102.25-97.50	A	1.424	0.000	0.000	6.431 7.465	0.000 0.000	0.19
210	102.20-07.00	B	1.424	0.000	0.000	13.812	0.000	0.06
		Č		0.000	0.000	7.465	0.000	0.16 0.19
L17	97,50-95,92	Ă	1.420	0.000	0.000	4.034	0.000	0.19
,	000 00.02	В	1.420	0.000	0.000	6.150	0.000	0.03
		č		0.000	0.000	4.034	0.000	0.07
L18	95.92-92.50	Ã	1.416	0.000	0.000	8.690	0.000	0.07
-		В		0.000	0.000	13.247	0.000	0.07
		Ċ		0.000	0.000	8.690	0.000	0.17
L19	92.50-92,25	A	1.413	0.000	0.000	0.636	0.000	0.01
		В		0.000	0.000	0.969	0.000	0.01
		С		0.000	0.000	0.636	0.000	0.01
L20	92.25-87.25	Α	1.409	0.000	0.000	12.980	0.000	0.11
tovTowor	Report - version	2050						

Section	Tower	Tower	Face	lce	AR	A_F	CAAA	CAAA	Weight
L21					ft²	427			K
C	<u>n</u>	π		in	0.000				0.04
L21									
L22	L21	87.25-87.00	Ă	1.405					
C		07.120 07.100	B						
L23			С						
L23	L22	87.00-82.00	Α	1.401	0.000				
L23			В		0.000	0.000	19.235	0.000	0.20
L24			Ç						
C	L23	82.00-77.00	Ā	1.392					
124			R						
L25	1.24	77 00 72 00	, ,	1 202					
C	LZ4	11.00-12.00	R	1.303					
1.25			č						
L26	L25	72,00-67,00		1.374					
C									
L27					0.000				
C	L26	67.00-63.25		1.365		0.000	10.150		0.08
L27									
L28									
L28	L2/	63.25-63,00	A	1.360					
L28			В						
L29	1 28	63 00-58 00	Λ	1 355					
L29	LZU	00.00-00.00		1,500					
L29			Č						
B	L29	58.00-56.75		1.348					
L30			В						
B			С		0.000				
L31	L30	56,75-56,50		1.346				0.000	
L31			В						
B	1.04	50 50 47 50	Ċ						
L32	L31	56.50-47.50	A	1.334					
L32			В						
B	132	47 50-47 00		1 222					
L33 47.00-42.00 A 1.314 0.000 0.000 0.842 0.000 0.02 L34 47.00-42.00 B 0.000 0.000 14.939 0.000 0.15 L34 42.00-37.00 A 1.298 0.000 0.000 13.154 0.000 0.10 L35 37.00-34.25 A 1.285 0.000 0.000 19.677 0.000 0.07 L36 37.00-34.25 A 1.285 0.000 0.000 12.546 0.000 0.07 B 0.000 0.000 12.546 0.000 0.00 0.00 0.00 0.00 B 0.000 0.000 0.000 12.546 0.000 0.01 1.2546 0.000 0.01 1.2546 0.000 0.01 1.2546 0.000 0.01 1.2546 0.000 0.01 1.2546 0.000 0.01 1.254 0.000 0.000 0.01 1.254 0.000 0.000 0.000 0.01	LUZ	JU.30-77-00.17		1.022					
L33 47.00-42.00 A 1.314 0.000 0.000 8.397 0.000 0.066 L34 42.00-37.00 A 1.298 0.000 0.000 13.154 0.000 0.15 L34 42.00-37.00 A 1.298 0.000 0.000 13.154 0.000 0.10 B 0.000 0.000 0.000 13.154 0.000 0.19 L35 37.00-34.25 A 1.285 0.000 0.000 12.546 0.000 0.07 B 0.000 0.000 0.000 12.546 0.000 0.12 L36 34.25-34.00 A 1.279 0.000 0.000 1.140 0.000 0.01 L37 34.00-29.00 A 1.269 0.000 0.000 1.140 0.000 0.01 L37 34.00-29.00 A 1.269 0.000 0.000 16.214 0.000 0.01 L37 34.00-29.00 A 1.269 <td< td=""><td></td><td></td><td>Č</td><td></td><td></td><td></td><td></td><td></td><td></td></td<>			Č						
B	L33	47.00-42.00		1.314					
L34									
L34			С			0.000	8.397		
L35 37.00-34.25 A 1.285 0.000 0.000 13.154 0.000 0.23 B 0.000 0.000 8.969 0.000 0.07 B 0.000 0.000 12.546 0.000 0.12 C 0.000 0.000 8.969 0.000 0.14 L36 34.25-34.00 A 1.279 0.000 0.000 0.815 0.000 0.01 B 0.000 0.000 0.815 0.000 0.01 C 0.000 0.000 0.815 0.000 0.01 L37 34.00-29.00 A 1.269 0.000 0.000 16.214 0.000 0.01 C 0.000 0.000 16.214 0.000 0.12 B 0.000 0.000 16.290 0.000 0.22 C 0.000 0.000 16.290 0.000 0.26 L38 29.00-26.75 A 1.254 0.000 0.000 16.290 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.320 0.000 0.01 L39 26.75-26.50 A 1.248 0.000 0.000 7.320 0.000 0.01 L39 26.75-26.50 A 1.248 0.000 0.000 7.320 0.000 0.01 B 0.000 0.000 1.136 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 1.136 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.238 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.238 0.000 0.01 L41 21.50-16.75 A 1.207 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 14.508 0.000 0.25 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01 B 0.000 0.000 1.136 0.000 0.000 0.18 C 0.000 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.000 1.136 0.000 0.001 C 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 C 0.000 0.0	L34	42.00-37.00		1.298			13.154	0.000	0.10
L35									
B	105	67.00.04.05							
L36 34.25-34.00 A 1.279 0.000 0.000 8.969 0.000 0.14 L37 34.00-29.00 A 1.269 0.000 0.000 16.214 0.000 0.21 L37 34.00-29.00 A 1.269 0.000 0.000 16.214 0.000 0.21 C 0.000 0.000 16.290 0.000 0.25 L38 29.00-26.75 A 1.254 0.000 0.000 16.290 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 C 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.320 0.000 0.01 L39 26.75-26.50 A 1.248 0.000 0.000 7.320 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 1.136 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.01 L40 21.50-16.75 A 1.207 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.25 L42 16.75-16.50 A 1.191 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01 B 0.000 0.000 0.000 14.508 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01	L35	37,00-34,25		1.285					
L36									
B	1.36	34 25-34 00		1 270					
L37 34.00-29.00 A 1.269 0.000 0.000 16.214 0.000 0.12 B 0.000 0.000 16.214 0.000 0.21 C 0.000 0.000 16.290 0.000 0.21 C 0.000 0.000 16.290 0.000 0.26 L38 29.00-26.75 A 1.254 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.210 0.000 0.05 B 0.000 0.000 7.320 0.000 0.01 L39 26.75-26.50 A 1.248 0.000 0.000 7.320 0.000 0.11 C 0.000 0.000 0.801 0.000 0.01 B 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 1.136 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.12 B 0.000 0.000 16.033 0.000 0.12 B 0.000 0.000 16.033 0.000 0.12 C 0.000 0.000 16.238 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 14.508 0.000 0.10 L42 16.75-16.50 A 1.191 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01	200	U7.20-04,00		1.213					
L37									
B	L37	34.00-29.00		1.269					
L38									
B 0.000 0.000 10.230 0.000 0.00 0.00					0.000	0.000		0.000	0.26
L40 26.50-21.50 A 1.248 0.000 0.000 7.320 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.20 C 0.000 0.000 16.003 0.000 0.20 C 0.000 0.000 16.003 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 C 0.000 0.000 20.807 0.000 0.10 L42 16.75-16.50 A 1.191 0.000 0.000 8.667 0.000 0.19 L44 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01 B 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 0.806 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01	L38	29.00-26.75		1.254					
L40 26.50-21.50 A 1.248 0.000 0.000 0.801 0.000 0.01 L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.20 C 0.000 0.000 16.003 0.000 0.12 B 0.000 0.000 16.03 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 20.807 0.000 0.10 C 0.000 0.000 8.667 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 1.136 0.000 0.01 B 0.000 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.000 0.414 0.000 0.01									
L40 26.50-21.50 A 1.235 0.000 0.000 1.136 0.000 0.001 L41 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.12 B 0.000 0.000 0.000 22.682 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 0.000 20.807 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01	1.00	00.75.00.50		4.040					
L40	LJ9	20.75-26.50		1.248					
L40 26.50-21.50 A 1.235 0.000 0.000 16.003 0.000 0.12 B 0.000 0.000 0.000 22.682 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 0.000 20.807 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.000 0.414 0.000 0.01									
B 0.000 0.000 22.682 0.000 0.20 C 0.000 0.000 16.238 0.000 0.25 C 0.000 0.000 16.238 0.000 0.25 C 0.000 0.000 14.508 0.000 0.10 C 0.000 0.000 14.508 0.000 0.10 C 0.000 0.000 14.508 0.000 0.10 C 0.000 0.000 8.667 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 C 0.000 0.000 0.806 0.000 0.01 C 0.000 0.000 0.000 0.136 0.000 0.01 C 0.000 0.000 0.000 0.414 0.000 0.01 C 0.000 0.000 0.000 0.414 0.000 0.01	140	26 50-21 50		1 235					
L41 21.50-16.75 A 1.207 0.000 0.000 14.508 0.000 0.10 B 0.000 0.000 20.807 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01	210	20.00-21,00		1.200					
L41									
B 0.000 0.000 20.807 0.000 0.18 C 0.000 0.000 8.667 0.000 0.19 L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01	L.41	21.50-16.75		1.207					
L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 0.414 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01									
L42 16.75-16.50 A 1.191 0.000 0.000 0.806 0.000 0.01 B 0.000 0.000 1.136 0.000 0.01 C 0.000 0.000 0.414 0.000 0.01									
C 0.000 0.000 0.414 0.000 0.01	L42	16.75-16.50	Α	1.191					0.01
L43 16.50-14.25 A 1.181 0.000 0.000 7.250 0.000 0.05	1.45	40.50 11.05		4.45					
	L43	16.50-14.25	Α	1.181	0.000	0.000	7.250	0.000	0.05

Tower Sectio n	Tower Elevation ft	Face or Leg	lce Thickness in	A _R ft ²	A _F ft ²	C _A A _A In Face ft ²	C _A A _A Out Face ft ²	Weight K
		В		0.000	0.000	10.213	0.000	0.09
		С		0.000	0.000	3.719	0.000	0.09
L44	14.25-14.00	Α	1.171	0.000	0.000	0.805	0.000	0.01
		В		0.000	0.000	1.133	0.000	0.01
		C		0.000	0.000	0.413	0.000	0.01
L45	14.00-9.00	Α	1.147	0.000	0.000	13,665	0.000	0.09
		В		0.000	0.000	22.603	0.000	0.19
		С		0.000	0.000	8.231	0.000	0.19
L46	9.00-4,25	Α	1.086	0.000	0.000	7.606	0.000	0.05
		В		0.000	0.000	21.311	0.000	0.17
		C		0.000	0.000	7.761	0.000	0.18
L47	4.25-4.00	Α	1.036	0.000	0.000	0.399	0.000	0.00
		В		0.000	0.000	1.115	0.000	0.01
		С		0.000	0.000	0.406	0.000	0.01
L48	4.00-0.00	Α	0.963	0.000	0.000	5.561	0.000	0.03
		В		0.000	0.000	16.076	10.000	0.12
		С		0.000	0.000	5.632	0.000	0.14

Feed Line Center of Pressure

Section	Elevation	CP _X	CD	CD	CD
Section	Elevation ft		CP _Z	CPX	<i>CP</i> z
	n	in	in	lc e	lce
L1	454.00.440.00	0.0000	2 2222	in	in
L1 L2	151.00-146.00	0.0000	0.0000	0.0000	0.0000
	146.00-141.00	0.0000	0.0000	0.0000	0.0000
L3	141.00-136.00	0.0000	0.0000	0.0000	0.0000
L4	136.00-131.00	0.0000	0.0000	0.0000	0.0000
L5	131.00-126.00	0.0000	0.0000	0.0000	0.0000
L6	126.00-125.50	0.0000	0.0000	0.0000	0.0000
L7	125.50-125.25	0.0000	0.0000	0.0000	0.0000
L8	125.25-120.25	0.8201	-0.2585	1.0168	-0.3205
L9	120.25-118.50	1.2210	-0.3849	1.5547	-0.4901
L10	118.50-118.25	1.2281	-0.3871	1.5640	-0.4930
L11	118.25-117.50	1.2309	-0.3880	1.5680	-0.4943
L12	117.50-117.25	1.2330	-0.3887	1.5713	-0.4953
L13	117.25-112.25	1.4506	-0.4573	1.8337	-0.5780
L14	112.25-107.25	1.7041	-0.5372	2.1397	-0.6745
L15	107.25-102.25	1.7340	-0.5466	2.1849	-0.6887
L16	102.25-97.50	1.5879	-0.5005	2.0217	-0.6373
L17	97.50-95.92	1.1925	-0.3759	1.5437	-0.4866
L18	95.92-92,50	1.2047	-0.3798	1.5607	-0.4920
. L19	92.50-92.25	1.2137	-0.3826	1.5734	-0.4960
L20	92.25-87.25	1.2053	-0.3799	1.5702	-0.4950
L21	87.25-87.00	1.2070	-0.3805	1.5770	-0,4971
L22	87.00-82.00	1.2519	-0.3946	1.6353	-0.5155
L23	82.00-77.00	1.7937	-0.5654	2.3132	-0.7292
L24	77.00-72.00	1.8193	-0.5735	2,3523	-0.7415
L25	72.00-67.00	1.4749	-0.4649	1.9307	-0.6086
L26	67.00-63.25	1,2744	-0.4017	1,6801	-0.5296
L27	63.25-63.00	1.2830	-0.4044	1.6923	-0.5334
L28	63.00-58.00	1.2344	-0.3891	1.6453	-0.5186
L29	58.00-56.75	1.1924	-0.3759	1.6046	-0.5058
L30	56.75-56.50	1.1957	-0.3769	1.6091	-0.5072
L31	56.50-47.50	1.3803	-0.4351	1,8562	-0.5851
L32	47.50-47.00	1.7003	-0.5360	2.2817	-0.7192
L33	47.00-42.00	1.7124	-0.5398	2,2972	-0,7241
L34	42.00-37.00	1.3295	-0.4191	1.8264	-0.5757
L35	37.00-34.25	1.1648	-0.3672	1.6161	-0.5094
L36	34.25-34.00	1,1702	-0.3689	1.6233	-0.5117
L37	34.00-29.00	1.1796	-0.3718	1.6389	-0.4952
L38	29.00-26.75	1.1925	-0.3759	1.6626	-0.4542
L39	26.75-26.50	1,1969	-0.3773	1.6682	-0.4564
L40	26.50-21.50	1.2061	-0.3802	1.6797	-0.4612
L41	21.50-16.75	-2,2376	-3.4202	-1.5447	-3.3731
L42	16.75-16.50	-3.4048	-4.4732	-2.4634	-4.1150
L43	16.50-14.25	-3.4203	-4.4922	-2.4769	-4.11323
L44	14.25-14.00	-3.4354	-4.5108	-2.4709 -2.4905	-4.1323 -4.1494
L45	14.00-9.00	-3.5337	-3.7808	-2.4905 -2.5467	-4.1494 -3.4886
- +0	14.00-3.00		-0.7000	-2.0407	-0.4000

Section	Elevation ft	CP _X in	CPz in	CPx Ice in	CPz lce in
L46	9.00-4.25	-3.7736	-1.7841	-2.6823	-1.7114
L47	4.25-4.00	-3.8044	-1.7970	-2.7225	-1.7294
L48	4.00-0.00	-3.3723	-1.7824	-2,2882	-1.7233

Note: For pole sections, center of pressure calculations do not consider feed line shielding.

Shielding Factor Ka

=					
Tower Section	Feed Line Record No.	Description	Feed Line Segment	K₃ No Ice	K₃ Ice
	7,000,0,700.		Elev.	110100	100
L8	24	AL7-50(1-5/8)	120.25 - 122.00	1.0000	1.0000
L8	46	MS-600 (L)	120.25 - 120.50	1.0000	1.0000
L8	47	MS-600 (L)	120.25 - 120.50	1.0000	1.0000
L8	48	MS-600 (L)	120.25 - 120.50	1.0000	1.0000
L8	50	MP3-03 (L)	120.25 - 125.00	1.0000	1.0000
L8	51	MP3-03 (L)	120.25 - 125.00	1.0000	1.0000
L8	52	MP3-03 (L)	120.25 - 125.00	1.0000	1.0000
L9	24	AL7-50(1-5/8)	118.50 - 120.25	1.0000	1.0000
L9	46	MS-600 (L)	118.50 - 120.25	1.0000	1.0000
L9.	47	MS-600 (L)	118.50 - 120,25	1.0000	1.0000
L9	48	MS-600 (L)	118.50 - 120.25	1.0000	1.0000
L9	50	MP3-03 (L)	118.50 - 120.25	1.0000	1.0000
L9	51	MP3-03 (L)	118.50 - 120.25	1.0000	1.0000
L9	52	MP3-03 (L)	118.50 - 120.25	1.0000	1.0000
L10	24	AL7-50(1-5/8)	118.25 - 118.50	1.0000	1.0000
L10	46	MS-600 (L)	118.25 - 118.50	1.0000	1.0000
L10	47	MS-600 (L)	118.25 - 118.50	1.0000	1.0000
L10	48	MS-600 (L)	118.25 - 118.50	1.0000	1.0000
L10	50	MP3-03 (L)	118.25 - 118.50	1.0000	1.0000
L10	51	MP3-03 (L)	118,25 - 118.50	1.0000	1.0000
L10	52	MP3-03 (L)	118.25 - 118.50	1.0000	1.0000
L11	24	AL7-50(1-5/8)	117.50 - 118.25	1.0000	1.0000
L11	46	MS-600 (L)	117.50 - 118.25	1.0000	1.0000
L11	47	MS-600 (L)	117.50 - 118.25	1.0000	1.0000
L 1 1	48	MS-600 (L)	117.50 - 118.25	1.0000	1.0000
L11	50	MP3-03 (L)	117.50 - 118.25	1.0000	1.0000
L11	51	MP3-03 (L)	117.50 - 118.25	1.0000	1.0000
L11	52	MP3-03 (L)	117.50 - 118.25	1,0000	1.0000
L12	24	AL7-50(1-5/8)	117.25 - 117.50	1.0000	1.0000

Tower	Feed Line	Description	Feed Line	K _e	Ka	
Section	Record No.		Segment Elev.	No Ice	Ice	
L12	46	MS-600 (L)	117.25 - 117.50	1.0000	1.0000	
L12	47	MS-600 (L)	117.50 117.25 - 117.50	1.0000	1.0000	
L12	48	MS-600 (L)	117.25 - 117.50	1.0000	1.0000	
L12	50	MP3-03 (L)	117.25 - 117.50	1.0000	1.0000	
L12	51	MP3-03 (L)	117.50 117.25 - 117.50	1.0000	1.0000	
L12	52	MP3-03 (L)		1.0000	1.0000	
L13	24	AL7-50(1-5/8)	112.25 - 117.25	1.0000	1.0000	
L13	46	MS-600 (L)	112.25 - 117.25 117.25	1.0000	1.0000	
L13	47	MS-600 (L)	117.25 112.25 - 117.25	1.0000	1.0000	
L13	48	MS-600 (L)	112,25 - 117,25	1.0000	1.0000	
L13	50	MP3-03 (L)	117.25 115.00 - 117.25	1.0000	1.0000	
L13	51	MP3-03 (L)	117.25 115.00 - 117.25	1.0000	1.0000	
L13	52	MP3-03 (L)	117.25 115.00 - 117.25	1.0000	1.0000	
L14	24	AL7-50(1-5/8)	107.25 - 107.25 - 112.25	1.0000	1.0000	
L14	46	MS-600 (L)	107.25 - 112.25	1.0000	1.0000	
L14	47	MS-600 (L)	107.25 - 112.25	1.0000	1.0000	
L14	48	MS-600 (L)	107.25 - 112.25	1.0000	1.0000	
L15	24	AL7-50(1 - 5/8)	102.25 - 107.25	1.0000	1.0000	
L15	46	MS-600 (L)	102.25 - 107.25	1.0000	1.0000	
L15	47	MS-600 (L)	102.25 - 107.25	1.0000	1.0000	
L15	48	MS-600 (L)	102.25 - 107.25	1.0000	1.0000	
L16	24	AL7-50(1-5/8)	97.50 - 102.25	1.0000	1.0000	
L16	43	MS-600 (L)	97.50 - 98.58	1.0000	1.0000	
L16	44	MS-600 (L)	97.50 - 98.58	1.0000	1.0000	
L16	45	MS-600 (L)	97.50 - 98.58	1.0000	1.0000	
L16	46	MS-600 (L)	97.50 - 102.25	1.0000	1.0000	
L16	47	MS-600 (L)	97.50 - 102.25	1.0000	1.0000	
L16	48	MS-600 (L)	97.50 - 102.25	1.0000	1.0000	
L18	24	AL7-50(1-5/8)	92.50 - 95.92	1.0000	1.0000	
L18	43	MS-600 (L)	92.50 - 95.92	1.0000	1.0000	
L18	44	MS-600 (L)	92.50 - 95.92	1.0000	1.0000	
L18	45	MS-600 (L)	92.50 - 95.92	1.0000	1.0000	
L18	46	MS-600 (L)	92.50 - 95.92	1.0000	1.0000	
L18	47	MS-600 (L)	92.50 - 95.92	1.0000	1.0000	

Section Record No. Segment No Ice Ice	Tower	Feed Line	Description	Feed Line	Ka	K _e
L19		Record No.	·	Segment		_
L19	L18	48	MS-600 (L)		1.0000	1.0000
L19	L19	24	AL7-50(1-5/8)	92.25 -	1.0000	1.0000
L19	L19	43	MS-600 (L)	92.25 -	1.0000	1.0000
L19	L19	44	MS-600 (L)	92.25 -	1.0000	1.0000
L19	L19	45	MS-600 (L)	92.25 -	1.0000	1.0000
L19	L19	46	MS-600 (L)	92.25 -	1.0000	1.0000
L19	L19	47	MS-600 (L)	92.25 -	1.0000	1.0000
L20	L19	48	MS-600 (L)	92.25 -	1.0000	1.0000
L20	L20	24	AL7-50(1-5/8)	87.25 -	1.0000	1.0000
L20	L20	40	MS-650 (L)	87.25 -	1.0000	1.0000
L20	L20	41	MS-650 (L)	87.25 -	1,0000	1.0000
L20	L20	42	MS-650 (L)	87.25 -	1.0000	1.0000
L20	L20	43	MS-600 (L)	87.25 -	1.0000	1.0000
L20	L20	44	MS-600 (L)	87.25 -	1.0000	1.0000
L20	L20	45	MS-600 (L)	87.25 -	1.0000	1.0000
L20 47 MS-600 (L) 90.50 - 92.25 1.0000 1.0000 L20 48 MS-600 (L) 90.50 - 92.25 1.0000 1.0000 L21 24 AL7-50(1-5/8) 87.00 - 1.0000 1.0000 1.0000 L21 40 MS-650 (L) 87.00 - 1.0000 1.0000 1.0000 L21 41 MS-650 (L) 87.00 - 1.0000 1.0000 1.0000 L21 42 MS-650 (L) 87.00 - 1.0000 1.0000 1.0000 L21 43 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L21 44 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 1.0000 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 43 MS-650 (L) 87.00 1.0000 1.0000 1.0000	L20	46	MS-600 (L)	90.50 -	1.0000	1.0000
L20 48 MS-600 (L) 90.50 - 92.25 1.0000 1.0000 L21 24 AL7-50(1-5/8) 87.00 - 87.25 1.0000 1.0000 L21 40 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 41 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 42 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 43 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 44 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 87.00 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 87.00 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 42 MS-650 (L) 82.42 - 1.0000 1.0000 L22 43	L20	47	MS-600 (L)	90.50 -	1.0000	1.0000
L21	L20	48	MS-600 (L)	90.50 -	1.0000	1.0000
L21	L21	24	AL7-50(1-5/8)	87.00 -	1.0000	1.0000
L21 41 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 42 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 43 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 44 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 87.00 - 1.0000 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 87.00 - 1.0000 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 7.00 - 1.0000 1.0000 1.0000 L2	L21	40	MS-650 (L)	87.00 -	1.0000	1.0000
L21 42 MS-650 (L) 87.00 - 87.25 1.0000 1.0000 L21 43 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L21 44 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 1.0000 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 43 MS-650 (L) 82.42 - 1.0000 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L21	41	MS-650 (L)	87.00 -	1.0000	1.0000
L21 43 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 44 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 1.0000 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 87.00 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L21	42	MS-650 (L)	87.00 -	1.0000	1.0000
L21 44 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L21 45 MS-600 (L) 87.00 - 87.00 - 1.0000 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 1.0000 - 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 87.00 1.0000 - 1.0000 L22 41 MS-650 (L) 82.00 - 87.00 1.0000 - 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 - 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 - 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 7.00 - 1.0000 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 7.00 - 1.0000 - 1.0000 1.0000	L21	43	MS-600 (L)	87.00 -	1.0000	1.0000
L21 45 MS-600 (L) 87.00 - 87.25 1.0000 1.0000 L22 24 AL7-50(1-5/8) 82.00 - 87.00 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L21	44	MS-600 (L)	87.00 -	1.0000	1.0000
L22 24 AL7-50(1-5/8) 82.00 - 87.00 1.0000 1.0000 L22 40 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L21	45	MS-600 (L)	87.00 -	1.0000	1.0000
L22 40 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 41 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 1.0000 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	24	AL7-50(1-5/8)	82.00 -	1.0000	1.0000
L22 41 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	40	MS-650 (L)	82.00 -	1.0000	1.0000
L22 42 MS-650 (L) 82.00 - 87.00 1.0000 1.0000 L22 43 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 7.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	41	MS-650 (L)	82.00 -	1.0000	1.0000
L22 43 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 44 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 7.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	42	MS-650 (L)	82.00 -	1.0000	1.0000
L22 44 MS-600 (L) 82.42 - 87.00 1.0000 1.0000 L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	43	MS-600 (L)	82.42 -	1.0000	1.0000
L22 45 MS-600 (L) 82.42 - 1.0000 1.0000 L23 24 AL7-50(1-5/8) 77.00 - 82.00 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	44	MS-600 (L)	82.42 -	1.0000	1.0000
L23 24 AL7-50(1-5/8) 77.00 - 1.0000 1.0000 L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L22	45	MS-600 (L)	82.42 -	1.0000	1,0000
L23 40 MS-650 (L) 77.00 - 1.0000 1.0000	L23	24	AL7-50(1-5/8)	77.00 -	1.0000	1.0000
	L23	40	MS-650 (L)		1.0000	1.0000

Tower Feed Line		Description	Feed Line	Ka	Ka
Section	Record No.		Segment Elev.	No Ice	lce
L23	41	MS-650 (L)	77.00 - 82.00	1.0000	1.0000
L23	42	MS-650 (L)	77.00 - 82.00	1.0000	1.0000
L24	24	AL7-50(1-5/8)	72.00 - 77.00	1.0000	1.0000
L24	40	MS-650 (L)	72.00 - 72.00 - 77.00	1.0000	1.0000
L24	41	MS-650 (L)	72.00 - 72.00 - 77.00	1.0000	1.0000
L24	42	MS-650 (L)	72.00 -	1.0000	1.0000
L25	24	AL7-50(1-5/8)	77.00 67.00 -	1.0000	1.0000
L25	37	MS-650 (L)	72.00 67.00 -	1.0000	1.0000
L25	38	MS-650 (L)	69.67 67.00 -	1.0000	1.0000
L25	39	MS-650 (L)	69.67 67.00 -	1.0000	1.0000
L25	40	MS-650 (L)	69.67 67.00 -	1.0000	1.0000
L25	41	MS-650 (L)	72.00 67.00 -	1.0000	1.0000
L25	42	MS-650 (L)	72.00 67.00 -	1.0000	1.0000
L26	24	AL7-50(1-5/8)	72.00 63.25 -	1.0000	1.0000
L26	37	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L26	38	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L26	39	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L26	40	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L26	41	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L26	42	MS-650 (L)	67.00 63.25 -	1.0000	1.0000
L27	24	AL7-50(1-5/8)	67.00 63.00 -	1.0000	1.0000
L27	37	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L27	38	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L27	39	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L27	40	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L27	41	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L27	42	MS-650 (L)	63.25 63.00 -	1.0000	1.0000
L28	24	AL7-50(1-5/8)	63.25 58.00 -	1.0000	1.0000
L28	34	MS-850 (L)	63.00 58.00 -	1.0000	1.0000
L28	35	MS-850 (L)	60.50 58.00 -	1.0000	1.0000
L28	36	MS-850 (L)	60.50 58.00 -	1.0000	1.0000
L28	37	MS-650 (L)	60.50 58.00 -	1.0000	1.0000
L28	38	MS-650 (L)	63.00 58.00 -	1.0000	1.0000
L28	39	MS-650 (L)	63.00 58.00 -	1.0000	1.0000
1	I	İ	63.00	İ	ı

Tower Section	Feed Line Record No.	Description	Feed Line Segment	K₄ No Ice	K _e Ice
L.2	8 40	MS-650 (L)	Elev. 60.50 -	1.0000	1.0000
L2	8 41	MS-650 (L)	63.00 60.50 -	1.0000	1.0000
L2	8 42	MS-650 (L)	63.00 60.50 -	1.0000	1.0000
L2	9 24	AL7-50(1-5/8)	63.00 56.75 -	1.0000	1.0000
L2	9 34	MS-850 (L)	58.00 56.75 - 58.00	1.0000	1.0000
L2	9 35	MS-850 (L)	56.75 - 58.00	1.0000	1.0000
L2	9 36	MS-850 (L)	56.75 - 58.00	1.0000	1.0000
L29	9 37	MS-650 (L)	56.75 - 58.00	1.0000	1.0000
L2:	38	MS-650 (L)	56.75 - 58.00	1.0000	1.0000
L29		MS-650 (L)	56.75 - 58.00	1.0000	1.0000
L36		AL7-50(1 - 5/8)	56.50 - 56.75	1.0000	1.0000
L30		MS-850 (L)	56.50 - 56.75	1.0000	1.0000
L30	1	MS-850 (L)	56.50 - 56.75	1.0000	1.0000
L30		MS-850 (L)	56.50 - 56.75	1.0000	1.0000
L30		MS-650 (L)	56.50 - 56.75	1.0000	1.0000
L30		MS-650 (L)	56.50 - 56.75	1.0000	1.0000
L30		MS-650 (L)	56.50 - 56.75	1.0000	1.0000
L31	ŀ	AL7-50(1-5/8)	47.50 - 56.50	1.0000	1.0000
L31		MS-850 (L)	47.50 - 56.50	1.0000	1.0000
L31		MS-850 (L)	47.50 - 56.50	1.0000	1.0000
L31	1	MS-850 (L)	47.50 - 56.50	1.0000	1.0000
L31	1	MS-650 (L)	51.33 - 56.50	1.0000	1.0000
L31]	MS-650 (L)	51.33 - 56.50	1.0000	1.0000
L31	1	MS-650 (L)	51.33 - 56.50	1.0000	1.0000
L33	i I	AL7-50(1-5/8)	42.00 - 47.00	1.0000	1.0000
L33	1	MS-850 (L)	42.00 - 47.00	1.0000	1.0000
L33	35	MS-850 (L)	42.00 - 47.00	1.0000	1.0000
L33	36	MS-850 (L)	42.00 - 47.00	1.0000	1.0000
L34	24	AL7-50(1-5/8)	37.00 - 42.00	1.0000	1.0000
L34	31	MS-850 (L)	37.00 - 40.00	1.0000	1.0000
L34 L34	32	MS-850 (L)	37.00 - 40.00	1.0000	1.0000
L34 L34	33	MS-850 (L)	37.00 - 40.00	1.0000	1.0000
L34	34	MS-850 (L)	37.00 - 42.00	1.0000	1.0000
L34	35	MS-850 (L)	37.00 - 42.00	1.0000	1.0000

Tower	Feed Line	Description	Feed Line	K₂	K _a	
Section	Record No.	·	Segment Elev.	No Ice	Ice	
L34	36	MS-850 (L)	37.00 -		1.0000	
L35	24	AL7-50(1-5/8)	42.00 34.25 - 37.00	1.0000	1.0000	
L35	31	MS-850 (L)	34.25 -	1.0000	1.0000	
L35	32	MS-850 (L)	37.00 34.25 - 37.00	1.0000	1.0000	
L35	33	MS-850 (L)	34.25 - 37.00	1.0000	1.0000	
L35	34	MS-850 (L)	34.25 - 37.00	1.0000	1.0000	
L35	35	MS-850 (L)	34.25 - 37.00	1.0000	1.0000	
L35	36	MS-850 (L)	34.25 - 37.00	1.0000	1.0000	
L36	24	AL7-50(1-5/8)	34.00 -	1.0000	1.0000	
L36	31	MS-850 (L)	34.25 34.00 - 34.25	1.0000	1.0000	
L36	32	MS-850 (L)	34.00 -	1.0000	1.0000	
L36.	33	MS-850 (L)	34.25 34.00 -	1.0000	1.0000	
L36	34	MS-850 (L)	34.25 34.00 - 34.25	1.0000	1.0000	
L36	35	MS-850 (L)	34.00 - 34.25	1.0000	1.0000	
L36	36	MS-850 (L)	34.00 -	1.0000	1.0000	
L37	24	AL7-50(1-5/8)	34.25 29.00 - 34.00	1.0000	1.0000	
L37	26	MS-850 (L)	29.00 -	1.0000	1.0000	
L37	27	MS-850 (L)	30.50 29.00 -	1.0000	1.0000	
L37	28	MS-850 (L)	30.50 29.00 - 30.50	1.0000	1.0000	
L37	31	MS-850 (L)	29.00 -	1.0000	1.0000	
L37	32	MS-850 (L)	34.00 29.00 -	1.0000	1.0000	
L37	33	MS-850 (L)	34.00 29.00 - 34.00	1.0000	1.0000	
L37	34	MS-850 (L)	30.50 - 34.00	1.0000	1.0000	
L37	35	MS-850 (L)	30.50 -	1.0000	1.0000	
L37	36	MS-850 (L)	34.00 30.50 -	1.0000	1.0000	
L38	24	AL7-50(1-5/8)	34.00 26.75 - 29.00	1.0000	1.0000	
L38	26	MS-850 (L)	26.75 -	1.0000	1.0000	
L38	27	MS-850 (L)	29.00 26.75 - 29.00	1.0000	1.0000	
L38	28	MS-850 (L)	26.75 -	1.0000	1.0000	
L38	31	MS-850 (L)	29.00 26.75 -	1.0000	1.0000	
L38	32	MS-850 (L)	29.00 26.75 - 29.00	1.0000	1.0000	
L38	33	MS-850 (L)	26.75 - 29.00	1.0000	1.0000	
L39	24	AL7-50(1-5/8)	26.50 -	1.0000	1.0000	
L39	26	MS-850 (L)	26.75 26.50 - 26.75	1.0000	1.0000	

ı	Tower	Feed Line	Description	Feed Line	Ka	K _a	
	Section	Record No.	= <i></i>	Segment	No Ice	/ce	
	L39	27	MS-850 (L)	<i>Elev.</i> 26.50 -	1.0000	1.0000	
	L39	28	MS-850 (L)	26.75 26.50 -	1,0000	1.0000	
	L39	31	MS-850 (L)	26.75 26.50 -	1.0000	1.0000	
	L39	32	MS-850 (L)	26.75 26.50 -	1.0000	1.0000	
	L39	33.	MS-850 (L)	26.75 26.50 -	1,0000	1.0000	
İ	L 4 0	24	AL7-50(1-5/8)	26.75 21.50 -	1,0000	1.0000	
l	L40	26	MS-850 (L)	26.50 21.50 - 26.50	1.0000	1.0000	
I	L 4 0	27	MS-850 (L)	21.50 - 26.50	1.0000	1.0000	
	L40	28	MS-850 (L)	21.50 - 21.50 - 26.50	1.0000	1.0000	
	L40	31	MS-850 (L)	26.50 21.50 - 26.50	1.0000	1.0000	
	L40	32	MS-850 (L)	21.50 - 21.50 - 26.50	1.0000	1.0000	
l	L40	33	MS-850 (L)	21.50 - 26.50	1.0000	1.0000	
	L41	24	AL.7-50(1 - 5/8)	16.75 - 21.50	1.0000	1.0000	
	L41	26	MS-850 (L)	16.75 - 21.50	1.0000	1.0000	
١	L41	27	MS-850 (L)	16.75 - 21.50	1.0000	1.0000	
l	L41	28	MS-850 (L)	16.75 - 21.50	1.0000	1.0000	
	L41	29	MS-850 (L)	16.75 - 20.50	1.0000	1.0000	
	L41	30	MS-850 (L)	16.75 - 20.50	1.0000	1.0000	
l	L41	31	MS-850 (L)	21.00 - 21.50	1.0000	1.0000	
	L41	32	MS-850 (L.)	21.00 - 21.50	1.0000	1.0000	
	L41	33	MS-850 (L)	21.00 - 21.50	1.0000	1.0000	
	L42	24	AL7-50(1-5/8)	16.50 - 16.75	1.0000	1.0000	
	L42	26	MS-850 (L)	16.50 - 16.75	1.0000	1.0000	
	L42	27	MS-850 (L)	16.50 - 16.75	1.0000	1.0000	
	L42	28	MS-850 (L)	16.50 - 16.75	1.0000	1.0000	
	L42	29	MS-850 (L)	16.50 - 16.75	1.0000	1.0000	
	L42	30	MS-850 (L)	16.50 - 16.75	1.0000	1.0000	
	L43	24	AL7-50(1-5/8)	14.25 - 16.50	1.0000	1.0000	
	L43	26	MS-850 (L)	14.25 - 16.50	1.0000	1.0000	
	L43	27	MS-850 (L)	14.25 - 16.50	1.0000	1.0000	
	L43	28	MS-850 (L)	14.25 - 16.50	1.0000	1.0000	
	L43	29	MS-850 (L)	14.25 - 16.50	1.0000	1.0000	
	L43	30	MS-850 (L)	14.25 - 16.50	1.0000	1.0000	
	L44	24	AL7-50(1-5/8)	14.00 - 14.25	1.0000	1.0000	
	•	•	•	,31	1	•	

Tower	Feed Line	Description	Feed Line	Ka	K _a
Section	Record No.	•	Seament	No Ice	lce
			Ělev.		,,,,
L44	26	MS-850 (L)	14.00 -	1.0000	1.0000
		` '	14.25		
L44	27	MS-850 (L)	14.00 -	1.0000	1.0000
i i			14.25		
L44	28	MS-850 (L)	14.00 -	1.0000	1.0000
		``'	14.25		
L44	29	MS-850 (L)	14.00 -	1.0000	1.0000
i i			14.25		
L44	30	MS-850 (L)	14.00 -	1.0000	1.0000
l			14.25		
L45	24	AL7-50(1-5/8)	9.00 - 14.00	1.0000	1.0000
L45	26	MS-850 (L)	10.50 -	1.0000	1.0000
			14.00		i
L45	27	MS-850 (L)	9.00 - 14.00	1.0000	1.0000
L45	28	MS-850 (L)	9.00 - 14.00	1.0000	1.0000
L45	29	MS-850 (L)	9.00 - 14.00	1.0000	1.0000
L45	30	MS-850 (L)	9.00 - 14.00	1.0000	1.0000
L46	24	AL7-50(1-5/8)	4.25 - 9.00	1.0000	1.0000
L46	27	MS-850 (L)	4.25 - 9.00	1.0000	1.0000
L46	28	MS-850 (L)	4.25 - 9.00	1.0000	1.0000
L46	29	MS-850 (L)	4.25 - 9.00	1.0000	1.0000
L46	30	MS-850 (L)	4.25 - 9.00	1.0000	1.0000
L47	24	AL7-50(1-5/8)	4.00 - 4.25	1.0000	1.0000
L47	27	MS-850 (L)	4.00 - 4.25	1.0000	1.0000
L47	28	MS-850 (L)	4.00 - 4.25	1.0000	1.0000
L47	29	MS-850 (L)	4.00 - 4.25	1.0000	1.0000
L47	30	MS-850 (L)	4.00 - 4.25	1.0000	1.0000
L48	24	AL7-50(1-5/8)	0.00 - 4.00	1.0000	1.0000
L48	27	MS-850 (L)	0.50 - 4.00	1.0000	1.0000
L48	28	MS-850 (L)	0.50 - 4.00	1.0000	1.0000
L48	29	MS-850 (L)	0.50 - 4.00	1.0000	1.0000
L48	30	MS-850 (L)	0.50 - 4.00	1.0000	1.0000

D		
INCCRATA	LOWAR	1 0000
Discrete	IOWEI	LUdus

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft	Azimuth Adjustmen t	Placement ft		C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K
			ft ft						
(2) AM-X-CD-16-65-00T-	Α	From Leg	4.00	0.0000	148.00	No Ice	4.63	3,27	0.07
RET w/ Mount Pipe		•	0.00		1 10.00	1/2"	5.06	3.69	0.13
			1.00			ice	5.51	4.12	0.20
						1" Ice	6.43	5.00	0.38
						2" Ice		0.00	0.00
(2) AM-X-CD-16-65-00T-	В	From Leg	4.00	0.0000	148.00	No Ice	4.63	3.27	0.07
RET w/ Mount Pipe		-	0.00			1/2"	5.06	3,69	0.13
			1.00			Ice	5.51	4.12	0.20
						1" Ice	6.43	5.00	0.38
4-1						2" Ice			
(2) AM-X-CD-16-65-00T-	С	From Leg	4.00	0.0000	148.00	No Ice	4.63	3.27	0.07
RET w/ Mount Pipe			0.00			1/2"	5.06	3.69	0.13
			1.00			lce	5.51	4.12	0.20
						1" Ice	6.43	5.00	0.38
000 40404 114 174	_	_				2" Ice			
800 10121 w/ Mount Pipe	Α	From Leg	4.00	0.0000	148,00	No Ice	5.74	4.95	0.07
			0.00			1/2"	6.34	6.02	0.12
			1.00			lce	6.86	6.81	0.18
						1" Ice	7.91	8.41	0.32
200 40404 (14) 174	_					2" Ice			
800 10121 w/ Mount Pipe	В	From Leg	4.00	0.0000	148.00	No Ice	5.74	4.95	0.07
			0.00			1/2"	6.34	6.02	0.12
			1.00			lce	6.86	6.81	0.18
						1" Ice	7.91	8.41	0.32
200 40404 (14) 51	_					2" Ice			
800 10121 w/ Mount Pipe	С	From Leg	4.00	0.0000	148.00	No Ice	5.74	4.95	0.07
tnxTower Report - version	8.0.5.6	כ							

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement ft		C _A A _A Front ft ²	C _A A _A Side ft ²	Weight K
	9		Vert ft ft	•			ĸ	ıţ	
			ft 0.00			1/2"	0.04	0.00	
			1.00			lce	6,34 6.86	6.02 6.81	0.12 0.18
			1.00			1" Ice	7.91	8.41	0.16
						2" Ice	7.51	0.41	0.32
(4) LGP21901	Α	From Leg	4.00	0.0000	148.00	No Ice	0.23	0.16	0.01
		J	0.00			1/2"	0.29	0.21	0.01
			1.00			Ice	0.36	0.28	0.01
						1" Ice	0.53	0.42	0.02
						2" Ice			
(4) LGP21901	В	From Leg	4.00	0.0000	148.00	No Ice	0.23	0.16	0.01
			0.00			1/2"	0.29	0.21	0.01
			1.00			ice	0.36	0.28	0.01
						1" Ice	0.53	0.42	0.02
(0) 0=====	_	_				2" Ice			
(4) LGP21901	С	From Leg	4.00	0.0000	148.00	No Ice	0.23	0.16	0.01
			0.00			1/2"	0.29	0.21	0.01
			1.00			lce	0.36	0.28	0.01
						1" Ice	0.53	0.42	0.02
DO0 40 00 40 0E						2" Ice			
DC6-48-60-18-8F	Α	From Leg	4.00	0.0000	148.00	No Ice	1,21	1.21	0.03
			0.00			1/2"	1.89	1.89	0.05
			1.00			Ice	2.11	2.11	80.0
						1" Ice	2.57	2.57	0.14
2) CC 1000DD EUL DIN	۸	F	4.00	0.0000	4.0.00	2" Ice			
2) CG-1900DD-FULL-DIN	Α	From Leg	4.00	0.0000	148.00	No Ice	1.10	0.29	0.01
			0.00			1/2"	1.23	0.37	0.02
			1.00			lce	1.37	0.46	0.03
						1" Ice	1.67	0.66	0.05
2) CG-1900DD-FULL-DIN	В	From Leg	4.00	0.0000	440.00	2" Ice	4.40		
2) CG-1900DD-POLL-DIN	Б	From Leg	4.00	0.0000	148.00	No Ice	1.10	0.29	0.01
			0.00 1.00			1/2"	1.23	0.37	0.02
			1.00			lce	1.37	0.46	0.03
						1" Ice	1.67	0.66	0.05
2) CG-1900DD-FULL-DIN	С	From Leg	4.00	0.0000	148.00	2" ice	4.40	0.00	0.04
E) OS TOUBE TOLE BIT	•	i ioni Leg	0.00	0.0000	140.00	No Ice 1/2"	1.10	0.29	0.01
			1.00			ice	1.23 1.37	0.37	0.02
			1.00			1" Ice	1.67	0.46 0.66	0.03
						2" Ice	1.07	0.00	0.05
(2) DTMABP7819VG12A	Α	From Leg	4.00	0.0000	148.00	No Ice	0.98	0.34	0.02
	• •	7.0 =09	0.00	0.0000	140.00	1/2"	1.10	0.42	0.02
			1.00			Ice	1.23	0.51	0.03
						1" Ice	1.52	0.71	0.04
						2" Ice	1.02	0.11	0.00
(2) DTMABP7819VG12A	В	From Leg	4.00	0.0000	148.00	No Ice	0.98	0.34	0.02
			0.00			1/2"	1.10	0.42	0.03
			1.00			Ice	1.23	0.51	0.04
						1" Ice	1.52	0.71	0.04
						2" Ice	1102	0.7 1	0.00
(2) DTMABP7819VG12A	С	From Leg	4.00	0.0000	148.00	No Ice	0.98	0.34	0.02
		· ·	0.00			1/2"	1.10	0.42	0.03
			1.00			Ice	1.23	0.51	0.04
						1" Ice	1.52	0.71	0.06
						2" Ice			5.55
(2) RRUS-11	Α	From Leg	4.00	0.0000	148.00	No Ice	2.79	1.19	0.05
			0.00			1/2"	3.00	1.34	0.07
			1.00			lce	3.21	1.50	0.09
						1" Ice	3.67	1.84	0.15
						2" Ice			
(2) RRUS-11	В	From Leg	4.00	0.0000	148.00	No Ice	2.79	1.19	0.05
		-	0.00			1/2"	3.00	1.34	0.07
			1.00			Ice	3.21	1.50	0.09
						1" Ice	3.67	1.84	0.15
									7
(2) RRUS-11	С	From Leg	4.00	0.0000		2" Ice			

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustmen t	Placement ft	_	C _A A _A Front ft ²	C _A A _A Side	Weight K
	209		Vert ft ft ft	٥			n-	ft²	
			0.00			1/2"	3.00	1.34	0.07
			1.00			Ice 1" Ice	3.21 3.67	1.50 1.84	0.09 0.15
860 10025	Α	From Leg	4.00	0.0000	148.00	2" Ice No Ice	0.14	0.12	0.00
		g	0.00	0.0000	1-10.00	1/2"	0.19	0.12	0.00
			1.00			Ice	0.25	0.23	0.01
	_					1" Ice 2" Ice	0.40	0.37	0.01
860 10025	В	From Leg	4.00	0.0000	148.00	No Ice	0.14	0.12	0.00
			0.00			1/2"	0.19	0.17	0.00
			1.00			Ice	0.25	0.23	0.01
960 40005	0	F 1	4.00			1" Ice 2" Ice	0.40	0.37	0.01
860 10025	С	From Leg	4.00	0.0000	148.00	No ice	0.14	0.12	0.00
			0.00 1.00			1/2"	0.19	0.17	0.00
			1.00			ice	0.25	0.23	0.01
*						1" Ice 2" Ice	0.40	0.37	0.01
OG-4	Α	From Leg	4.00	0.0000	148.00	No Ice	4 22	4.00	0.00
		r rom Log	0.00	0.0000	140.00	1/2"	4.33 7.14	4.33 7.14	0.02
			7.00			Ice	7.14	7.1 4 7.86	0.06 0.11
			.,			1" ice	9.34	9.34	0.11
						2" Ice	5.07	5.04	0.23
DB286-B	В	From Leg	4.00	0.0000	148.00	No Ice	4.99	4.99	0.08
		_	0.00			1/2"	8.98	8.98	0.11
			6.00			lce	12.97	12.97	0.13
						1" Ice 2" Ice	20.96	20.96	0.18
DS1F03F36D-N	Α	From Leg	4.00	0.0000	148.00	No Ice	6.69	6.69	0.06
			0.00			1/2"	8.95	8.95	0.11
			12.00			Ice	11.23	11.23	0.17
						1" lce 2" lce	15.84	15.84	0.34
Plotform Mount II D 000 41	_								
Platform Mount [LP 602-1]	С	None		0.0000	148.00	No Ice	32.03	32.03	1.34
						1/2"	38.71	38.71	1.80
						Ice	45.39	45.39	2.26
						1" Ice	58.75	5 8.75	3.17
***						2" Ice			
DB854DG65ESX w/ Mount	Α	From Leg	4.00	0.0000	140.00	No Ice	5.55	4.10	0.04
Pipe			0.00			1/2"	5.94	4.73	80.0
			0.00			Ice	6.34	5.36	0.14
						1" Ice 2" Ice	7.17	6.64	0.26
DB854DG65ESX w/ Mount	В	From Leg	4.00	0.0000	140.00	No Ice	5.55	4.10	0.04
Pipe			0.00			1/2"	5.94	4.73	0.08
			0.00			Ice	6.34	5.36	0.14
						1" Ice	7.17	6.64	0.26
DD054D005E0V	_					2" Ice			
DB854DG65ESX w/ Mount	С	From Leg	4.00	0.0000	140.00	No Ice	5,55	4.10	0.04
Pipe			0.00			1/2"	5.94	4.73	0.08
			0.00			Ice	6.34	5.36	0.14
						1" Ice	7.17	6.64	0.26
(2) NHH-65C-R2B w/	Α	From Leg	4.00	0.0000	440.00	2" Ice	44.65	A =-	
Mount Pipe	~	rom Leg	4.00 0.00	0.0000	140.00	No Ice	11.63	9.79	0.08
moont ipe			0.00			1/2"	12.35	11.31	0.17
			0.00			Ice	13.07	12.85	0.27
						1" Ice	14.44	15.19	0.51
(2) NHH-65C-R2B w/	В	From Leg	4.00	0.0000	140.00	2" Ice No Ice	11 62	מל מ	Λ 00
Mount Pipe	_		0.00	0.0000	1-10.00	1/2"	11.63 12.35	9.79 11.31	0.08
•			0.00			lce	13.07	12.85	0.17
						100	15.07	12.00	0.27

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement ft	-	C _A A _A Front ft ²	CaAa Side ft²	Weight K
			ft ft						
			ft		, <u></u>	1" Ice	14.44	15.19	0.51
(O) NULL OFO DOD. (_					2" Ice			
(2) NHH-65C-R2B w/ Mount Pipe	С	From Leg	4.00 0.00	0.0000	140.00	No ice	11.63	9.79	0.08
Would Tipe			0.00			1/2" Ice	12.35 13.07	11.31 12.85	0.17
			0.00			1" Ice	14.44	15.19	0.27 0.51
						2" Ice	17,77	10.10	0.51
DB-T1-6Z-8AB-0Z	Α	From Leg	4.00	0.0000	140.00	No Ice	4.80	2.00	0.04
			0.00			1/2"	5.07	2.19	0.08
			0.00			Ice	5.35	2.39	0.12
						1" Ice 2" Ice	5.93	2.81	0.21
(3) RFV01U-D2A	Α	From Leg	4.00	0.0000	140.00	No Ice	1.88	1.01	0.07
		Ū	0.00			1/2"	2.05	1.14	0.09
			0.00			Ice	2.22	1.28	0.11
						1" Ice	2.60	1.59	0.15
(3) RFV01U-D1A	В	From Leg	4.00	0.0000	440.00	2" Ice	4.00	4.00	
(6) KI 7010-BIA	ь	1 Toni Leg	0.00	0.0000	140.00	No Ice 1/2"	1.88 2.05	1.25	0.08
			0.00			lce	2.05	1.39 1.54	0.10 0.12
						1" Ice	2.60	1.86	0.12
Dist. 14 AND AND AND AND	_					2" Ice			5.15
Platform Mount [LP 303-1]	С	None		0.0000	140.00	No Ice	14.66	14.66	1.25
						1/2"	18.87	18.87	1.48
						Ice	23.08	23.08	1.71
						1" Ice 2" Ice	31.50	31.50	2.18
Miscellaneous [NA 507-1]	С	None		0.0000	140.00	No Ice	4.80	4.80	0.25
•					1 10.00	1/2"	6.70	6.70	0.29
						Ice	8.60	8.60	0.34
						1" Ice	12.40	12.40	0.44
(2) Miscellaneous [NA 509-	С	None		0.0000	140.00	2" Ice	44.04	44.54	
3]	C	None		0.0000	140.00	No Ice 1/2"	11.84 16.96	11.84	0.28
-,						Ice	22.08	16.96 22.08	0.30 0,32
						1" Ice	32.32	32.32	0.36
***						2" Ice	•		
TME-1900MHZ RRH	Α	Francisco	4.00	0.0000	400.00				
TME-1000MHZ KKI	A	From Leg	4.00 0.00	0.0000	132.00	No Ice	2.49	3.26	0.04
			-1.00			1/2" Ice	2.70 2.91	3.48 3.72	0.08 0.11
			.,,,,,			1" Ice	3.35	4.21	0.11
						2" Ice			0.10
TME-1900MHZ RRH	В	From Leg	4.00	0.0000	132.00	No Ice	2.49	3.26	0.04
			0.00			1/2"	2.70	3.48	0.08
			-1.00			lce	2.91	3.72	0.11
						1" ice 2" ice	3.35	4.21	0.19
TME-1900MHZ RRH	С	From Leg	4.00	0.0000	132.00	No Ice	2.49	3.26	0.04
			0.00		.02.00	1/2"	2.70	3.48	0.04
			-1.00			Ice	2.91	3.72	0.11
						1" Ice	3.35	4.21	0.19
800 EXTERNAL NOTCH	Α	Erom Log	4.00	0.0000	400.00	2" Ice			
FILTER	А	From Leg	4.00 0.00	0.0000	132.00	No Ice	0.66	0.32	0.01
			-1.00			1/2" Ice	0.76 0.87	0.40 0.48	0.02
						1" Ice	1.11	0.48	0.02 0.04
						2" Ice		0.07	5.07
800 EXTERNAL NOTCH	В	From Leg	4.00	0.0000	132.00	No Ice	0.66	0.32	0.01
FILTER			0.00			1/2"	0.76	0.40	0.02
			-1.00			ice	0.87	0.48	0.02
						1" ice	1.11	0.67	0.04
								0.07	0.0-
800 EXTERNAL NOTCH	С	From Leg	4.00	0.0000	132.00	2" Ice No Ice	0.66	0.32	0.01

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustmen t	Placement ft	.,	C _A A _A Front ft ²	CAAA Side ft ²	Weight K
	 -		ft ft ft		_				
			-1.00			1/2" Ice 1" Ice	0.87 1.11	0.48 0.67	0.02 0.04
800MHZ RRH	Α	From Leg	4.00 0.00	0.0000	132.00	2" Ice No Ice 1/2"	2.13 2.32	1. 7 7 1.95	0.05 0.07
0001117 770	_	_	-1.00			lce 1" lce 2" lce	2.51 2.92	2.13 2.51	0.10 0.16
800MHZ RRH	В	From Leg	4.00 0.00 -1.00	0.0000	132.00	No Ice 1/2" Ice	2.13 2.32 2.51	1.77 1.95 2.13	0.05 0.07 0.10
800MHZ RRH	С	From Low		0.0000		1" Ice 2" Ice	2.92	2.51	0.16
OUGHIZ KIKI	C	From Leg	4.00 0.00 -1.00	0.0000	132.00	No Ice 1/2" Ice	2.13 2.32 2.51	1.77 1.95 2.13	0.05 0.07 0.10
Pipe Mount [PM 601-3]	С	None		0.0000	132.00	1" Ice 2" Ice No Ice	2.92 4.39	2.51 4.39	0.16 0.20
				0.000	102.30	1/2" Ice	5.48 6.57	5.48 6.57	0.24 0.28
***						1" Ice 2" Ice	8.75	8.75	0.36
GPS-TMG-HR-26NCM	Α	From Leg	4.00 0.00 3.00	0.0000	130.00	No Ice 1/2" Ice	0.13 0.18 0.24	0.13 0.18 0.24	0.00 0.00 0.01
APXVSPP18-C-A20 w/	Α	From Leg	4.00	0.0000	130.00	1" Ice 2" Ice No Ice	0.37 4.60	0.37 4.01	0.01 0.10
Mount Pipe			0.00 0.00			1/2" Ice 1" Ice 2" Ice	5.05 5.50 6.44	4.45 4.89 5.82	0.16 0.23 0.42
APXVSPP18-C-A20 w/ Mount Pipe	В	From Leg	4.00 0.00 0.00	0.0000	130.00	No Ice 1/2" Ice	4.60 5.05 5.50	4.01 4.45 4.89	0.10 0.16 0.23
APXVSPP18-C-A20 w/	С	From Leg	4.00	0.0000	130,00	1" Ice 2" Ice No Ice	6.44 4.60	5.82 4.01	0.42 0.10
Mount Pipe		-	0.00 0.00			1/2" Ice 1" Ice	5.05 5.50 6.44	4.45 4.89 5.82	0.16 0.23 0.42
APXVTM14-C-120 w/ Mount Pipe	Α	From Leg	4.00 0.00 0.00	0.0000	130.00	2" Ice No Ice 1/2"	4.09 4.48	2.86 3.23	0.08 0.13
ADVI/TM14 C 400!		F				Ice 1" Ice 2" Ice	4.88 5.71	3.61 4.40	0.19 0.33
APXVTM14-C-120 w/ Mount Pipe	В	From Leg	4.00 0.00 0.00	0.0000	130.00	No Ice 1/2" Ice 1" Ice 2" Ice	4.09 4.48 4.88 5.71	2.86 3.23 3.61 4.40	0.08 0.13 0.19 0.33
APXVTM14-C-120 w/ Mount Pipe	С	From Leg	4.00 0.00 0.00	0.0000	130.00	No Ice 1/2" Ice 1" Ice	4.09 4.48 4.88 5.71	2.86 3.23 3.61 4.40	0.08 0.13 0.19 0.33
TD-RRH8X20-25	Α	From Leg	4.00 0.00 0.00	0.0000	130,00	2" Ice No Ice 1/2"	4.05 4.30	1.53 1.71	0.07 0.10
			0.00			lce 1" lce 2" lce	4.56 5.10	1.90 2.30	0.13 0.20

Description	Face	Offset	Offsets:	Azimuth	Pleasment		<u> </u>	0.4	LAZ- factor
Description	or Leg	Type	Horz Lateral Vert	Adjustmen t	Placement ft		CAAA Front ft²	CaAa Síde ft²	Weight K
			ft ft ft						
TD-RRH8X20-25	В	From Leg	4.00	0.0000	130.00	No Ice	4,05	1.53	0.07
			0.00			1/2"	4.30	1.71	0.10
			0.00			Ice	4.56	1.90	0.13
						1" ice	5.10	2.30	0.20
TD-RRH8X20-25	С	From Lea	4.00	0.0000	130.00	2" Ice No Ice	4.05	1.50	0.07
	•	1 Tolli Log	0.00	0.0000	150.00	1/2"	4.30	1.53 1.71	0.07 0.10
			0.00			lce	4.56	1.90	0.13
						1" Ice	5.10	2.30	0.20
2 27511 O.D. v. Cl. Marries Direct	•	N				2" Ice			
2.375" OD x 6' Mount Pipe	Α	None		0.0000	130.00	No Ice	1.43	1.43	0.03
						1/2" Ice	1.92 2.29	1.92 2.29	0.04
						1" Ice	3.06	3.06	0.05 0.09
						2" Ice	0.00	0.00	0.00
2.375" OD x 6' Mount Pipe	В	None		0.0000	130.00	No Ice	1.43	1.43	0.03
						1/2"	1.92	1.92	0.04
						ice	2.29	2.29	0.05
						1" Ice 2" Ice	3.06	3.06	0.09
2.375" OD x 6' Mount Pipe	С	None		0.0000	130.00	No Ice	1.43	1.43	0.03
•					,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1/2"	1.92	1.92	0.04
						lce	2.29	2.29	0.05
						1" Ice	3.06	3.06	0.09
T-Arm Mount [TA 602-3]	С	None		0.0000	120.00	2" ice	44.50	44.50	0.77
7 July Mount [174 002-0]	·	None		0.0000	130.00	No Ice 1/2"	11.59 15.44	11.59 15.44	0.77 0.99
						Ice	19.29	19.29	1.21
						1" Ice	26.99	26.99	1.64
***						2" Ice			
ERICSSON AIR 21 B2A	Α	From Leg	4.00	0.0000	122.00	No Ice	6.33	F 64	0.44
. B4P w/ Mount Pipe		r rom ecg	0.00	0.0000	122.00	1/2"	6.78	5.64 6.43	0.11 0.17
•			1.00			Ice	7.21	7.13	0.17
						1" Ice	8.12	8.59	0.38
EDICESON AID 24 D24	_	5 •	4.00			2" Ice			
ERICSSON AIR 21 B2A B4P w/ Mount Pipe	В	From Leg	4.00 0.00	0.0000	122.00	No Ice	6.33	5.64	0.11
24 W Modific ipc			1.00			1/2" Ice	6.78 7.21	6.43 7.13	0.17 0.23
			1.00			1" ice	8.12	8.59	0.23
						2" Ice		5,55	0.00
ERICSSON AIR 21 B2A	С	From Leg	4.00	0.0000	122.00	No Ice	6.33	5.64	0.11
B4P w/ Mount Pipe			0.00			1/2"	6.78	6.43	0.17
			1.00			lce 1" lce	7.21 8.12	7.13	0.23
						2" Ice	0.12	8.59	0.38
APXVAARR24_43-U-NA20	Α	From Leg	4.00	0.0000	122.00	No Ice	14.69	6.87	0.19
w/ Mount Pipe			0.00			1/2"	15.46	7.55	0.31
			1.00			Ice	16.23	8.25	0.46
						1" Ice	17.82	9.67	0.79
APXVAARR24, 43-U-NA20	В	From Leg	4.00	0.0000	122.00	2" Ice No Ice	14.69	6.87	0.19
w/ Mount Pipe	_		0.00	0.0000	122.00	1/2"	15.46	7.55	0.19
· ·			1.00			Ice	16.23	8.25	0.46
						1" Ice	17.82	9.67	0.79
ADVI/AADDO4 40 II NIAOO	_	Farm Lan	4.65			2" Ice			
APXVAARR24_43-U-NA20 w/ Mount Pipe	С	From Leg	4.00 0.00	0.0000	122.00	No ice	14.69	6.87	0.19
www.wiodift i ipe			1.00			1/2" Ice	15.46 16.23	7.55	0.31
			1,00			1" Ice	17.82	8.25 9.67	0.46 0.79
						2" Ice	,,,, <u>,,,</u>	0.01	0.10
(3) RADIO 4449 B12/B71	Α	From Leg	4.00	0.0000	122.00	No Ice	1.65	1.16	0.07
			0.00			1/2"	1.81	1.30	0.09
			1.00			Ice	1.98	1.45	0.11
						1" Ice	2.34	1.76	0.16

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustmen t	Placement ft		CAAA Front ft ²	C∆A∆ Side ff²	Weight K
T-Arm Mount [TA 702-3]	С	None		0.0000	122.00	2" Ice No Ice 1/2" Ice 1" Ice 2" Ice	5.64 6.55 7.46 9.28	5.64 6.55 7.46 9.28	0.34 0.43 0.52 0.70

Tower Pressures - No Ice

 $G_H = 1.100$

Section	Z	Kz	q_z	Ag	F	AF	AR	Aieg	Leg	CAAA	CAAA
Elevation	ft		psf	ft ²	a	ft 2	ft ²	ft ²	20g	In	Out
ft			"	"	c		"	"	70	Face	Face
					ē					ft ²	ft ²
L1 151.00-	148.48	1.106	38.88	7.757	Α	0.000	7.757	7.757	100.00	0.000	0.000
146.00				1	В	0.000	7.757	İ	100.00	0.000	0.000
			!		C	0.000	7.757		100.00	0.000	0.000
L2 146.00-	143.48	1.096	38.50	8.161	Α	0.000	8.161	8.161	100.00	0,000	0.000
141.00		!			В	0.000	8.161		100.00	0.000	0.000
					C	0.000	8.161		100.00	0.000	0.000
L3 141.00-	138.48	1.085	38.12	8.564	Α	0.000	8.564	8.564	100.00	0.000	0.000
136.00					В	0.000	8.564		100.00	0.000	0.000
1					C	0.000	8.564		100.00	0.000	0.000
L4 136.00-	133.48	1.073	37.72	8.968	Α	0.000	8.968	8.968	100.00	0.000	0.000
131.00		•		ĺ	В	0.000	8.968		100.00	0.000	0.000
	i				C	0.000	8.968		100.00	0.000	0.000
L5 131.00-	128.48	1.062	37.31	9.372	Α	0.000	9.372	9.372	100.00	0.000	0.000
126.00					В	0.000	9.372		100.00	0.000	0.000
					C	0.000	9.372		100,00	0.000	0.000
L6 126.00-	125.75	1.055	37.08	0.959	Α	0.000	0.959	0.959	100.00	0.000	0.000
125.50					В	0.000	0.959		100.00	0.000	0.000
					C	0.000	0.959		100.00	0.000	0.000
L7 125.50-	125.37	1.054	37.05	0.480	Α	0.000	0.480	0.480	100.00	0.000	0.000
125.25					В	0.000	0.480		100.00	0.000	0.000
					С	0.000	0.480		100.00	0.000	0.000
L8 125.25-	122,73	1.048	36.82	9.815	Α	0.000	9.815	9.815	100.00	3.464	0.000
120.25					В	0.000	9.815		100.00	4.836	0.000
1040005	440.0-				C	0.000	9.815		100.00	3.464	0.000
L9 120.25-	119.37	1.04	36.53	3.531	Α	0.000	3.531	3.531	100.00	2.934	0.000
118.50					В	0.000	3.531		100.00	4.306	0.000
140 440 50	440.07	4 00-7			Ç	0.000	3.531		100.00	2.934	0.000
L10 118.50-	118.37	1.037	36.45	0.506	Α	0.000	0.506	0.506	100.00	0.419	0.000
118.25	ŀ	ł			В	0.000	0.506		100.00	0.615	0.000
144 449 05	447.07	4 000	20.40	4 505	Ċ	0.000	0.506		100.00	0.419	0.000
L11 118.25- 117.50	117.87	1.036	36.40	1.525	A	0.000	1.525	1.525	100.00	1.258	0.000
117.50					В	0.000	1.525		100.00	1.846	0.000
L12 117.50-	117.37	1.035	20.20	0.544	Ç	0.000	1.525		100.00	1.258	0.000
117.25	. 117.37	1.035	36.36	0.511	A	0.000	0.511	0.511	100.00	0.419	0.000
117.23	i				ВС	0.000	0.511		100.00	0.615	0.000
L13 117.25-	114.73	1.028	36.12	10.443	_	0.000	0.511	40.440	100.00	0,419	0.000
112.25	114.73	1.020	30.12	10.443	A B	0.000	10.443	10.443	100.00	6.523	0.000
112.23	ļ	İ			C	0.000	10.443		100.00	10.443	0.000
L14 112.25-	109.73	1.015	35.67	10.848			10.443	40.040	100.00	6.523	0.000
107.25	108.73	1.010	35.67	10.048	АВ	0.000	10.848	10.848	100.00	5.000	0.000
107.23	1			i	C	0.000	10.848 10.848 i		100.00	8.920	0.000
L15 107.25-	104.74	1.001	35.19	11.253	Ă	0.000		11.050	100.00	5.000	0.000
102.25	104.74	1.001	JQ. 18	11.203	B	0.000	11.253	11.253	100.00	5.000	0.000
102.20	I		I		c	0.000	11.253		100.00	8.920	0.000
L16 102.25-	99.86	0.988	34.72	11.065	Ă		11.253	44 005	100.00	5.000	0.000
97.50	39.00	0.000	J4.12	11.005	B	0.000	11.065 11.065	11.065	100.00	5.830	0.000
٥٠,٠٥٥	ļ				c	0.000	11.065		100.00	9.554	0.000
	1	ı	ı	ı	ν I	0.000	11.005	ı	100.00	5.830	0.000

Section		Z	Kz	q_z	Ag	F	A _F	AR	Aleg	Leg	СаАа	СлАл
Elevation ft	n	ft		psf	ft²	a	ft ²	ft²	ft ²	%	In Face	Out
, "						c e	ļ				ft ²	Face ft²
L17 97.		96.71	0.979	34.40	3.707	Α	0.000	3.707	3.707	100.00	3.168	0.000
95	.92					В	0.000	3.707		100.00	4.410	0.000
L18 95,	02_	94.20	0.972	34.14	8.131	CA	0.000	3.707 8.131	8,131	100.00 100.00	3.168 6.832	0.000 0.000
	.50	34.20	0.512	34.14	0.101	lв	0.000	8.131	0,101	100.00	9.510	0.000
						C	0.000	8.131		100.00	6.832	0.000
L19 92.		92.37	0.966	33.95	0.602	Α	0.000	0.602	0.602	100.00	0.500	0.000
92	.25					B	0.000	0.602		100.00	0.696	0.000
L20 92.	25-	89.74	0.958	33.67	12.263	C	0.000	0.602 12,263	12,263	100.00 100.00	0.500 10.271	0.000 0.000
	.25	00.,	0.000	00.07	12.200	В	0.000	12.263	12.200	100.00	14.191	0.000
]						С	0.000	12.263		100.00	10,271	0.000
L21 87.		87.12	0.95	33.39	0.623	Ā	0.000	0.623	0.623	100.00	0.521	0.000
8/	.00					B	0.000	0.623 0.623		100.00 100.00	0,717 0.521	0.000 0.000
L22 87.	00-	84.49	0.942	33.10	12.676	ΙĂ	0.000	12.676	12.676	100.00	9.997	0.000
	00					В	0.000	12.676		100.00	13.917	0.000
						C	0.000	12.676		100.00	9.997	0.000
L23 82.	.00- .00	79.49	0.925	32.53	13.082	А В	0.000	13.082 13.082	13.082	100.00	5.417	0.000 0.000
I "	.00					C	0.000	13.082		100.00 100.00	9.337 5.417	0.000
L24 77.	00-	74.49	0.908	31.93	13.487	Ă	0.000	13.487	13.487	100.00	5.417	0.000
72	.00					В	0.000	13 .4 87		100.00	9.337	0.000
105.70	^^	00.40	0.004	04.00	40.000	Č	0.000	13.487	40.000	100.00	5.417	0.000
L25 72.	.00	69.49	0.891	31.30	13.892	A B	0.000	13.892 13.892	13.892	100.00 100.00	8.309 12,229	0.000 0.000
"	.00					ľċ	0.000	13.892		100.00	8.309	0.000
L26 67.		65.12	0.874	30.72	10.684	Α	0.000	10.684	10.684	100.00	8.125	0.000
63	.25					B	0.000	10.684		100.00	11.065	0.000
L27 63.	25_	63.12	0.867	30.45	0.720	CA	0.000	10.684 0.720	0.720	100.00 100.00	8.125 0.542	0.000 0.000
	.00	00.12	0.007	30.43	0.720	B	0.000	0.720	0.120	100.00	0.738	0.000
						C	0.000	0.720		100.00	0.542	0.000
L28 63.	•	60.49	0.856	30.08	14.621	Ā	0.000	14.621	14.621	100.00	11.667	0.000
58	.00					B	0.000	14.621 14.621		100.00 100.00	15.587 11.667	0.000 0.000
L29 58.	00-	57.37	0.843	29.63	3.718	Ă	0.000	3.718	3.718	100.00	3.125	0.000
	.75					В	0.000	3.718		100.00	4.105	0.000
100 50		50.00	0.54	50.50		C	0.000	3.718		100.00	3.125	0.000
L30 56.	/5- .50	56.62	0.84	29.52	0.746	A B	0.000 0.000	0.746 0.746	0.746	100.00 100.00	0.625 0.821	0.000 0.000
1 30	.50					C	0.000	0.746		100.00	0.625	0.000
L31 56.	50-	51.96	0.82	28.81	27.535	Ā	0.000	27.535	27.535	100.00	18.352	0.000
47	.50					В	0.000	27.535		100.00	25.409	0.000
122.47	_ເ ດ	47.25	0.700	28.03	1.540	Ç	0.000	27.535	1 540	100.00	18.352	0.000 0.000
L32 47.:	.00	41.23	0.798	20.03	1.540	A B	0.000 0.000	1.540 1.540	1.540	100.00 100.00	0.708 1.100	0.000
1						č	0.000	1.540		100.00	0.708	0.000
L33 47.	- 1	44.49	0.784	27.56	15.624	A	0.000	15.624	15.624	100.00	7.083	0.000
42	.00					B	0.000 0.000	15.624 15.624		100.00 100.00	11.003 7.083	0.000 0.000
L34 42.6	00-	39.49	0.758	26.63	16.029	A	0.000	16.029	16.029	100.00	11.335	0.000
	.00	,				В	0.000	16,029	. 3.023	100,00	15.255	0.000
1050-	ا ؞؞	A= A=	0.700		, , , , ,	C	0.000	16.029		100.00	11.335	0.000
L35 37.0	00- .25	35.62	0.736	25.86	8.985	A B	0.000 0.000	8.985 8.985	8.985	100.00 100.00	7.789 9.944	0.000 0.000
	ا '''					C	0.000	8.985		100.00	7.789	0.000
L36 34.:		34.12	0.727	25.55	0.823	Α	0.000	0.823	0.823	100.00	0.708	0.000
34	.00					В	0.000	0.823		100.00	0.904	0.000
L37 34,0	_{ոი-}	31.49	0.71	24.97	16.677	C A	0.000 0.000	0.823 16.677	16.677	100.00 100.00	0.708 14.167	0.000 0.000
	.00	31.48	U./ I	4.01	10.077	В	0.000	16.677	10.077	100.00	18.087	0.000
						C	0.000	16.677		100.00	14.167	0.000
L38 29.0		27.87	0.7	24.60	7.636	A	0.000	7.636	7.636	100.00	6.375	0.000
26	.75					B C	0.000 0.000	7.636 7.636		100.00 100.00	8.139 6.375	0.000 0.000
L39 26.1	₇₅₋	26,62	0.7	24.60	0.854	A	0.000	0.854	0.854	100.00	0.375	0.000
	.50					В	0.000	0.854		100.00	0.904	

Section	Z	Kz	q_z	A _G	F	A⊧	A_R	A _{leg} ft ²	Leg	СаАа	CAAA
Elevation	ft		psf	ft ²	a	ft ²	ft²	ft ²	%	ln	Out
ft					С					Face	Face
			ļ		е					ft²	ft ²
					С	0.000	0.854		100.00	0.708	0.000
L40 26.50-	23.99	0.7	24.60	17.284	Α	0.000	17.284	17.284	100.00	14.167	0.000
21.50					В	0.000	17.284		100.00	18.087	0.000
					C	0.000	17.284		100.00	14,167	0.000
L41 21.50-	19.12	0.7	24.60	16,794	Α	0.000	16,794	16.794	100.00	12.750	0.000
16.75					В	0.000	16.794		100.00	16.47 4	0.000
				j	С	0.000	16.794		100.00	7.438	0.000
L42 16.75-	16.62	0.7	24.60	0.893	Α	0.000	0.893	0.893	100.00	0.708	0.000
16.50					В	0.000	0.893		100.00	0.904	0.000
					С	0.000	0.893		100.00	0.354	0.000
L43 16.50-	15.37	0.7	24.60	8.084	Α	0.000	8.084	8.084	100.00	6.375	0.000
14.25]		В	0.000	8.084		100.00	8.139	0.000
į					С	0.000	8.084		100.00	3.188	0.000
L44 14.25-	14.12	0.7	24.60	0.903	Α	0.000	0.903	0.903	100.00	0.708	0.000
14.00					В	0.000	0.903		100.00	0.904	0.000
					С	0.000	0.903		100.00	0.354	0.000
L45 14.00-	11.49	0.7	24.60	18.284	Α	0.000	18,284	18.284	100.00	12.042	0.000
9.00					В	0.000	18.284		100.00	18.087	0.000
					С	0.000	18.284		100.00	7.083	0.000
L46 9,00-4.25	6.62	0.7	24.60	17.743	Α	0.000	17.743	17.743	100.00	6.729	0.000
·					В	0.000	17.743		100.00	17,182	0.000
					С	0.000	17.743		100.00	6.729	0.000
L47 4.25-4.00	4.12	0.7	24.60	0.945	Α	0.000	0.945	0.945	100.00	0.354	0.000
					В	0.000	0.945		100.00	0.904	0.000
					С	0.000	0.945		100.00	0.354	0.000
L48 4.00-0.00	1,99	0.7	24.60	15.254	Α	0.000	15.254	15.254	100.00	4.958	0.000
					В	0.000	15.254		100.00	13.053	0.000
					С	0.000	15.254		100.00	4.958	0.000

Tower Pressure - With Ice

G_H = 1.100

Section	Z	Kz	q_z	tz	A _G ft²	F	A⊧ ft²	AR	Aieg	Leg	CaAa	СдАд
Elevation	ft		psf	in	ft ²	а	ft²	ft²	ft ²	%	In	Out
ft			•			C	1				Face	Fac e
						е					ft ²	ft²
L1 151.00-	148.48	1.106	6.22	1.4819	8.992	Α	0.000		8.992	100.00	0.000	0.000
146.00						В	0.000	8.992		100.00	0.000	0.000
			ĺ			С	0.000	8.992		100.00	0.000	0.000
L2 146.00-	143.48	1.096	6.16	1,4769	9.392	Α	0.000	9.392	9.392	100.00	0.000	0.000
141.00						В	0.000	9.392		100.00	0.000	0.000
l						C	0.000	9.392		100.00	0.000	0.000
L3 141.00-	138.48	1.085	6,10	1.4716	9.791	Α	0.000	9.791	9.791	100.00	0.000	0.000
136.00				i		В	0.000	9.791		100.00	0.000	0.000
						С	0.000	9.791		100.00	0.000	0.000
L4 136.00-	133.48	1.073	6.03	1.4662	10.190	Α	0.000	10,190	10.190	100.00	0.000	0.000
131.00						В	0.000	10.190		100.00	0.000	0.000
		İ				C	0.000	10,190		100.00	0.000	0.000
L5 131.00-	128.48	1.062	5.97	1.4606	10.589	Α	0.000	10.589	10.589	100.00	0.000	0.000
126.00			ŀ			В	0.000	10.589		100.00	0.000	0.000
1						С	0.000	10.589		100.00	0.000	0.000
L6 126.00-	125.75	1.055	5.93	1.4575	1.081	Α	0.000	1.081	1.081	100.00	0.000	0.000
125.50						В	0.000	1.081		100.00	0.000	0.000
						С	0.000	1.081		100.00	0.000	0.000
L7 125.50-	125.37	1.054	5.93	1.4571	0.541	Α	0.000	0.541	0.541	100.00	0.000	0.000
125.25						В	0.000	0.541		100.00	0.000	0.000
						С	0.000	0.541		100.00	0.000	0.000
L8 125.25-	122.73	1.048	5.89	1,4540	11,027	Α	0.000	11.027	11.027	100.00	4.411	0.000
120.25						В	0.000	11.027		100.00	6.762	0.000
						C	0.000	11.027	1	100.00	4.411	0.000
L9 120.25-	119.37	1.04	5.85	1.4499	3,954	Α	0.000	3.954	3.954	100.00	3.763	0.000
118.50		'				В	0.000			100.00	6.112	0.000
''3,555						c	0.000	3,954		100.00	3.763	0.000
L10 118,50-	118.37	1.037	5.83	1.4487	0.567	Ā	0.000		0.567	100.00	0.537	0.000
118.25			2,00	,,,,,,,		В	0.000			100.00	0.873	0.000
						c	0.000			100.00	0.537	

Section Elevation	z ft	Kz	q _z psf	tz in	A _G ft²	F a	A _F ft²	A _R ft²	A _{leg} ft²	Leg %	C _A A _A In	C _A A _A Out
ft						c e					Face ft ²	Face ft²
L11 118.25-	117.87	1.036	5.82	1.4481	1.706	Α	0.000	1.706	1.706	100.00	1.612	0.000
117.50						ВС	0.000	1.706 1.706		100.00 100.00	2.619 1.612	0.000 0.000
L12 117.50-	117.37	1.035	5.82	1.4475	0.572	Ä	0.000	0.572	0.572	100.00	0.537	0.000
117,25						В	0.000	0.572		100.00	0.873	0.000
L13 117,25-	114.73	1.028	5.78	1.4442	11.646	C	0.000 0.000	0.572 11.646	11.646	100.00 100.00	0.537 8.378	0.000 0.000
112.25						В	0.000	11.646	******	100.00	15.084	0.000
L14 112,25-	109.73	1.015	5,71	1.4378	12.046	C A	0.000 0.000	11.646 12.046	12.046	100.00 100.00	8.378 6.438	0.000 0.000
107.25	103.73	1.013	3.71	1.4010	12.040	В	0.000	12.046	12.040	100.00	13.135	0.000
145 107 05	104.74	4 004	F 00	4 4044	40.440	Č	0.000	12.046	40.440	100.00	6.438	0.000
L15 107.25- 102.25	104.74	1.001	5.63	1.4311	12.446	A B	0.000 0.000	12.446 12.446	12.446	100.00 100.00	6.431 13.120	0.000 0.000
						Č	0.000	12.446		100.00	6.431	0.000
L16 102.25- 97.50	99.86	0.988	5.55	1.4243	12.192	A B	0.000 0.000	12.192 12.192	12.192	100.00 100.00	7. 4 65 13.812	0.000 0.000
97.30						C	0.000	12,192		100.00	7.465	0.000
L17 97.50-	96.71	0.979	5.50	1.4197	4.083	A	0.000	4.083	4.083	100.00	4.034	0.000
95.92			ļ			B C	0.000 0.000	4.083 4.083		100.00 100.00	6.150 4.034	0.000 0.000
L18 95.92-	94.20	0.972	5.46	1.4160	8.937	Ă	0.000	8.937	8.937	100.00	8.690	0.000
92.50						В	0.000	8.937	:	100.00	13.247	0.000
L19 92.50-	92.37	0.966	5.43	1.4132	0.661	C A	0.000 0.000	8.937 0.661	0.661	100.00 100.00	8.690 0.636	0.000 0.000
92.25	¥=.¥.				0.00	В	0.000	0.661	0.00.	100.00	0.969	0.000
L20 92.25-	89.74	0.958	5.39	1.4091	13.438	C	0.000	0.661	13,438	100.00	0.636	0.000
87.25	09.74	0.956	5.58	1.4091	13.438	A B	0.000 0.000	13.438 13.438	13.436	100.00 100.00	12.980 19.641	0.000 0.000
						C	0.000	13,438		100.00	12.980	0.000
L21 87.25- 87.00	87.12	0.95	5.34	1.4050	0.682	A B	0.000 0.000	0.682 0.682	0.682	100.00 100.00	0.656 0.989	0.000 0.000
07.00	i		l			Č	0.000	0.682		100.00	0.656	0.000
L22 87.00-	84.49	0.942	5.30	1.4007	13.843	Α	0.000	13.843	13.843	100.00	12.584	0.000
82.00						B	0.000 0.000	13.843 13.843		100.00 100.00	19.235 12.584	0.000 0.000
L23 82.00-	79.49	0.925	5.20	1.3922	14.242	Α	0.000	14.242	14.242	100.00	6.809	0.000
77.00						В	0.000 0.000	14.242 14.242		100.00 100.00	13.449 6.809	0.000 0.000
L24 77.00-	74.49	0.908	5.11	1.3831	14.640	Ā	0.000	14.640	14.640	100.00	6.800	0.000
72.00		i				В	0.000	14.640		100.00	13.429	0.000
L25 72.00-	69.49	0.891	5.01	1.3736	15.037	CA	0.000 0.000	14.640 15.037	15.037	100.00 100.00	6.800 10.400	0.000 0.000
67.00	30.13	0.00	0.0.	1.0100	70.001	В	0.000	15.037	10.007	100.00	17.017	0.000
126.67.00	GE 40	0.074	4 02	4 26 47	44 507	C	0.000	15.037	44 507	100.00	10.400	0.000
L26 67.00- 63.25	65.12	0.874	4.92	1.3647	11.537	A B	0.000 0.000	11.537 11.537	11.537	100.00 100.00	10.150 15.104	0.000 0.000
						С	0.000	11.537		100.00	10.150	0.000
L27 63.25- 63.00	63.12	0.867	4.87	1.3604	0.777	A B	0.000 0.000	0.777 0.777	0.777	100.00 100.00	0.676 1.006	0.000 0.000
						C	0.000	0.777	1	100.00	0.676	0.000
L28 63.00-	60.49	0.856	4.81	1.3546	15.749	A	0.000	15.749	15.749	100.00	14.348	0.000
58.00				İ		B C	0.000 0.000	15.749 15.749		100.00 100.00	20.941 14.348	0.000 0.000
L29 58.00-	57.37	0.843	4.74	1.3475	3.999	Α	0.000	3.999	3.999	100.00	3.792	0.000
56.75		j				B C	0.000 0.000	3.999 3.999		100.00 100.00	5.438 3.792	0.000 0.000
L30 56.75-	56.62	0.84	4.72	1.3457	0.802	A	0.000	0.802	0.802	100.00	3.792 0.758	0.000
56.50						В	0.000	0.802	-	100.00	1.087	0.000
L31 56.50-	51.96	0.82	4.61	1.3342	29.537	C A	0.000 0.000	0.802 29.537	29,537	100.00 100.00	0.758 22.108	0.000 0.000
47.50	31.00	0.02	01	1.5542	20.007	В	0.000	29.537	20,007	100.00	33.931	0.000
100 47 50	47.05	0.700	4 40	4 0040	4.054	Č	0.000	29.537	4.554	100.00	22.108	0.000
L32 47.50- 47.00	47.25	0.798	4.49	1.3216	1.651	A B	0.000	1.651 1.651	1.651	100.00 100.00	0.842 1.499	0.000 0.000
						С	0.000	1.651	I	100.00	0.842	0.000
L33 47.00-	44.49	0.784	4.41	1.3137	16.719	A	0.000	16.719	16.719	100.00	8,397	0.000
42.00	I	- 1	I	I	l	В	0.000	16.719	l	100.00	14.939	0.000

Section	Z	Kz	q _z	t z	Ag	F	AF	A_R	A_{leg}	Leg	CAAA	C _A A _A
Elevation	ft		psf	in	ft²	а	ft²	ft²	ft ²	%	In	Out
ft						c e					Face ft²	Face ft²
						С	0.000	16.719		100.00	8.397	0.000
L34 42,00-	39.49	0.758	4.26	1.2981	17.111	Α	0.000	17,111	17.111	100.00	13.154	0.000
37.00		ŀ				В	0.000	17.111		100.00	19.677	0.000
						С	0.000	17,111		100.00	13.154	0.000
L35 37.00-	35.62	0.736	4.14	1.2848	9.574	Α	0.000	9.574	9.574	100.00	8.969	0.000
34.25						В	0.000	9.574	i	100.00	12.546	0.000
				i		С	0.000	9.574		100.00	8.969	0.000
L36 34,25-	34.12	0.727	4.09	1.2793	0.876		0.000	0.876	0.876	100.00	0.815	0.000
34.00	i	ļ	Ī			В	0.000	0.876	ľ	100.00	1.140	0.000
		ŀ				C	0.000	0.876		100.00	0.815	0.000
L37 34.00-	31.49	0.71	3.99	1.2690	17.734	Α	0.000	17.734	17.734	100.00	16.214	0.000
29.00						В	0.000	17.734		100.00	22.776	0.000
		ļ		i		С	0.000	17.734	i	100.00	16.290	0.000
L38 29.00-	27.87	0.7	3.94	1.2537	8.106	Α	0.000	8.106	8.106	100.00	7.210	0.000
26.75						В	0.000	8.106		100.00	10.230	0.000
	i		ľ			C	0.000	8.106	ŀ	100.00	7.320	0.000
L39 26.75-	26.62	0.7	3.94	1.2479	0.906	Α	0.000	0.906	0.906	100.00	0.801	0.000
26.50						В	0.000	0.906		100.00	1,136	0.000
						С	0.000	0.906		100.00	0.813	0.000
L40 26.50-	23.99	0.7	3.94	1.2350	18.313	Α	0.000	18.313	18.313	100.00	16.003	0.000
21.50	ľ	i		i		В	0.000	18.313	- 1	100.00	22.682	0.000
						С	0.000	18.313		100.00	16.238	0.000
L41 21.50-	19.12	0.7	3,94	1.2073	17.749	Α	0.000	17.749	17,749	100.00	14.508	0.000
16.75			- 1	[В	0.000	17.749		100.00	20.807	0.000
1				.		С	0.000	17.749		100.00	8.667	0.000
L42 16.75-	16.62	0.7	3.94	1.1905	0.943	Α	0.000	0.943	0.943	100.00	0.806	0.000
16.50	I					В	0.000	0.943		100.00	1,136	0.000
	ľ			1		С	0.000	0.943		100.00	0.414	0.000
L43 16.50-	15.37	0.7	3.94	1,1812	8.527	Α	0.000	8.527	8.527	100,00	7.250	0.000
14.25			ı			В	0.000	8.527		100.00	10.213	0.000
l		ŀ				C	0.000	8.527		100.00	3.719	0.000
L44 14.25-	14.12	0.7	3.94	1.1713	0.952	Ã	0.000	0.952	0.952	100.00	0.805	0.000
14.00			'			В	0.000	0.952	5.532	100.00	1,133	0.000
					i	c	0.000	0.952		100.00	0.413	0.000
L45 14.00-9.00	11.49	0.7	3.94	1.1473	19,240	Ā	0.000	19.240	19,240	100.00	13,665	0.000
						В	0.000	19.240	.0.2.10	100.00	22.603	0.000
		1		i		č	0.000	19.240		100.00	8.231	0.000
L46 9.00-4,25	6.62	0.7	3.94	1.0857	18.603	Ă	0.000	18,603	18.603	100.00	7.606	0.000
=:::::::::::::::::::::::::::::::::::	5.52		V. V		.0.000	В	0.000	18.603	10.000	100.00	21.311	0.000
			- 1		į	Č	0.000	18.603		100.00	7.761	0.000
L47 4.25-4.00	4.12	0.7	3.94	1.0356	0.988	Ă	0.000	0.988	0.988	100.00	0.399	0.000
		٠.، ا	0.0	1.0000	0.000	B	0.000	0.988	0.500	100.00	1.115	0.000
					i	C	0.000	0.988		100.00	0.406	0.000
L48 4.00-0.00	1,99	0.7	3.94	0.9630	15.896	Ă	0.000	15.896	15.896	100.00	5.561	0.000
000 0.00	1.00	۷.,۲	5.57	0.0000	10.000	В	0.000	15.896	13.080	100.00	16.076	0.000
]		J			c	0.000	15.896		100.00	5.632	
						J	0.000	10.080		100.00	5.032	0.000

Tower Pressure - Service

 $G_H = 1.100$

Section Elevation ft	z ft	Kz	q _z psf	Ag ft²	F a c e	A _F ft ²	A _R ft²	Aleg ft ²	Leg %	C _A A _A In Face ft ²	C _A A _A Out Face ft ²
L1 151.00-	148.48	1.106	8.44	7.757	Α	0.000	7.757	7.757	100.00	0.000	0.000
146.00					В	0.000	7.757		100.00	0.000	0.000
					С	0.000	7.757	i	100.00	0.000	0.000
L2 146.00-	143.48	1.096	8.36	8.161	Α	0.000	8.161	8.161	100.00	0.000	0.000
141.00				'	В	0.000	8.161		100.00	0.000	0.000
			- 1		С	0.000	8.161		100.00	0.000	0.000
L3 141.00-	138.48	1.085	8.27	8.564	Α	0.000	8.564	8.564	100.00	0.000	0.000
136.00					В	0.000	8.564		100.00	0.000	0.000
					C	0.000	8.564		100.00	0.000	0.000
L4 136.00-	133,48	1.073	8.18	8.968	Α	0.000	8.968	8.968	100.00	0.000	0.000
131.00					В	0.000	8.968		100.00	0.000	0.000
ļ					C	0.000	8.968		100,00	0.000	0.000

Section	Z	Kz	q_z	A _G	F	A _F	A _R	Aleg	Leg	CAAA	C _A A _A
Elevation ft	ft		psf	ft²	a c	ft²	ft²	ft²	%	In Face	Out Face
"					e					ft ²	ft ²
L5 131.00-	128.48	1.062	8.10	9.372	Α	0.000	9.372	9.372	100.00	0.000	0.000
126.00					В	0.000	9.372		100.00	0.000	0.000
L6 126.00-	125.75	1.055	8.05	0.959	C	0.000	9.372 0.959	0.959	100.00 100.00	0.000 0.000	0.000 0.000
125.50	120.10	1.000	0.00	0.000	В	0.000	0.959	0.000	100.00	0.000	0.000
					C	0.000	0.959		100.00	0.000	0.000
L7 125,50-	125.37	1.054	8.04	0.480	Α	0.000	0.480	0.480	100.00	0.000	0.000
125.25					В	0.000	0.480		100.00	0.000	0.000
L8 125.25-	122.73	1.048	7.99	9,815	C	0.000	0.480 9.815	9.815	100.00 100.00	0.000 3.464	0.000 0.000
120.25	122.70	1.040	7.00	0.010	В	0.000	9.815	3.013	100.00	4.836	0.000
					Ċ	0.000	9.815		100.00	3.464	0.000
L9 120.25-	119.37	1.04	7.93	3.531	A	0.000	3.531	3.531	100.00	2.934	0.000
118.50					B	0.000	3.531 3.531		100.00 100.00	4.306 2.934	0,000 000.0
L10 118.50-	118.37	1.037	7.91	0.506	A	0.000	0.506	0.506	100.00	0.419	0.000
118,25	110.01	1.007	7.01	0.000	В	0.000	0.506	0.000	100.00	0.615	0.000
]					С	0.000	0.506		100.00	0.419	0.000
L11 118.25-	117.87	1.036	7.90	1.525	A	0.000	1.525	1.525	100.00	1.258	0.000
117.50					B	0.000	1.525 1.525		100,00 100.00	1.846 1.258	0.000 0.000
L12 117.50-	117.37	1.035	7.89	0.511	Ã	0.000	0.511	0.511	100.00	0.419	0.000
117.25					В	0.000	0,511		100.00	0.615	0.000
					С	0.000	0.511		100.00	0,419	0.000
L13 117.25-	114.73	1.028	7.84	10.443	A	0.000	10.443	10.443	100.00	6.523	0.000
112.25					B	0.000 0.000	10.443 10.443		100.00 100.00	10.443 6.523	0.000
L14 112.25-	109.73	1.015	7.74	10.848	Ā	0.000	10.848	10.848	100.00	5.000	0.000
107.25					В	0.000	10.848		100.00	8.920	0.000
					С	0.000	10.848		100.00	5.000	0.000
L15 107.25-	104.74	1.001	7.64	11.253	A	0.000	11.253	11.253	100.00	5.000	0.000
102.25					B	0.000 0.000	11.253 11.253		100.00 100.00	8.920 5.000	0.000 0.000
L16 102.25-	99.86	0.988	7.53	11.065	Ă	0.000	11.065	11.065	100.00	5.830	0.000
97.50					В	0.000	11.065		100.00	9.554	0.000
					Ç	0.000	11.065		100.00	5.830	0.000
L17 97.50- 95.92	96.71	0.979	7.46	3.707	A B	0.000 0.000	3.707 3.707	3.707	100.00 100.00	3.168 4.410	0.000 0.000
95.92					C	0.000	3.707		100.00	3.168	0.000
L18 95.92-	94.20	0.972	7.41	8.131	Ā	0.000	8.131	8.131	100.00	6.832	0.000
92.50					В	0.000	8.131		100.00	9.510	0.000
140.00.50	00.07	0.000	7.77	0.000	Č	0.000	8.131	0.000	100.00	6.832	0.000
L19 92.50- 92,25	92.37	0.966	7.37	0.602	A B	0.000 0.000	0.602 0.602	0.602	100.00 100.00	0.500 0.696	0.000
02,20					č	0.000	0.602		100.00	0.500	0.000
L20 92.25-	89.74	0.958	7.31	12.263	Α	0.000	12.263	12.263	100.00	10.271	0.000
87.25					В	0.000	12.263		100.00	14.191	0.000
L21 87.25-	87.12	0.95	7.25	0.623	C A	0.000 0.000	12.263 0.623	0.623	100.00 100.00	10.271 0.521	0.000 0.000
87.00	01.12	0.90	,.24	5.023	В	0.000	0.623	0.020	100.00	0.717	0.000
					С	0.000	0.623		100.00	0.521	0.000
L22 87.00-	84.49	0.942	7.18	12.676	A	0.000	12.676	12.676	100.00	9.997	0.000
82.00					B	0.000 0.000	12.676 12.676		100.00 100.00	13.917 9.997	0.000
L23 82.00-	79.49	0.925	7.06	13.082	A	0.000	13.082	13.082	100.00	5.417	0.000
77.00	, 5, 10	=0			В	0.000	13.082		100.00	9.337	0.000
					C	0.000	13.082		100.00	5.417	0.000
L24 77.00-	74.49	0.908	6.93	13.487	A	0.000	13.487	13.487	100.00	5.417	0.000
72.00					B	0.000 0.000	13.487 13.487		100.00 100.00	9.337 5.417	0.000
L25 72.00-	69,49	0.891	6.79	13.892	Ā	0.000	13.892	13.892	100.00	8.309	0.000
67.00	-5,.5				В	0.000	13.892		100.00	12.229	0.000
					Ç	0.000	13.892		100.00	8.309	0.000
L26 67.00-	65,12	0.874	6.67	10.684	A	0.000	10.684	10.684	100.00	8.125	0.000
63.25					B	0.000 0.000	10.68 4 10.68 4		100.00 100.00	11.065 8.125	0.000
L27 63.25-	63.12	0.867	6.61	0.720	Ā	0.000	0.720	0.720	100.00	0.542	0.000
63.00					В	0.000		l .	100.00		0.000

Elevation ft	Section	Z	Kz	q_z	Ag	F	A _F	AR	Aleg	Leg	CAAA	CAAA
Face Face		ft	'~	psf	ft ²		ft ²	ft ²				
L28 63,00				,,			"			, -	1	
L28 83.00						e	! i				ft²	ft²
58.00						С	0.000	0.720		100.00	0,542	0.000
L29 58.00	L28 63.00-	60.49	0.856	6.53	14.621	Α		14.621	14.621		11.667	0.000
L29 58.00 S6.75 S6.87 S6.87 S6.82 O.84 S.41 O.746 B O.000 O.746 O.000	58.00		!									0.000
Section Sect												0.000
L30 56.75		57.37	0.843	6,43	3.718				3.718			0.000
L30 56.75 56.62 0.84 6.41 0.746 A 0.000 0.746 0.746 100.00 0.625 0.000	56.75											0.000
S6.50	100 50 75	50.00	0.04		0 740							0.000
C		56.62	0.84	6.41	0.746				0.746			
L31 56.50	50.50											0.000
A7.50	131 56 50-	51.06	กลว	6.25	27 535				27 535			
C		31.50	0.02	0.20	27.000				27.000			0.000
L32 47.50- 47.25 0.798 6.08 1.540 A 0.000 1.540 1.540 100.00 0.708 0.000	-77.55											
47.00	L32 47.50-	47.25	0.798	6.08	1.540				1,540			0.000
C												
L33 47.00						C						0.000
42.00	L33 47.00-	44.49	0,784	5.98	15.624	Α	0.000	15.624	15.624	100.00	7.083	0.000
1.34 42.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 37.00 35.62 0.736 5.61 8.985 C 0.000 16.029 100.00 11.335 0.000 0.000 37.00 34.25 C 0.000 8.985 8.985 100.00 7.789 0.000 0.000 34.25 0.000 0.8985 0.000 0	42.00					В	0.000				11,003	0.000
37.00						C	0.000			100.00		0.000
L35 37.00		39.49	0.758	5.78	16.029				16.029			0.000
L35 37.00	37.00											0.000
34.25						ı						0.000
L36 34.25		35.62	0.736	5.61	8.985				8.985			
L36 34.25	34.25											
34.00	100 04 05	24.40	0.707	F E 4	0.000	ı			0.000			
L37 34.00- 29.00 L37 34.00- 29.00 L38 29.00- 27.87 O.7 5.34 7.636 A O.000 16.677 C 0.000 16.677 D 0.000 14.167 D 0.000 14.167 D 0.000 L38 29.00- 26.75 C 0.000 7.636 D 0.000 7.636 D 0.000 7.636 D 0.000 7.636 D 0.000 0.854 D 0.000 0.		34,12	Ų./Z/	5.54	0.823				0.823			0.000
L37 34.00-	34.00											
29.00	1373400-	31 40	0.71	5.42	16 677				16 677			
L38 29.00- 26.75 26.75 26.62 27.87 26.62 26.60 27.87 26.50 26.50 26.50 27.87 26.50 28.80 27.87 28.80 2		01.43	0.71	J.72	10.077				10.077			
L38 29.00- 27.87)	0.000
C	L38 29.00-	27.87	0.7	5.34	7.636				7.636			
L39 26.75						В						0.000
C						С				100.00	6.375	0.000
L40 26.50- 21.50 23.99 0.7 5.34 17.284 A 0.000 17.284 17.284 100.00 14.167 0.000 14.167 0.000 14.167 0.000 16.794 100.00 14.167 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.474 0.000 16.794 100.00 16.474 0.000 16.474 0.000 16.474 0.000 16.474 0.000 0.893 0.893 0.893 100.00 0.904 0.000 0.893 100.00 0.904 0.000 0.893 100.00 0.354 0.000 0.893 100.00 0.354 0.000 0.893 0.000 0.893 0.000 0.893 0.000 0.893 0.000 0.354 0.000 0.354 0.000 0.903 0.903 100.00 0.3188 0.000 0.903 100.00 0.904 0.000 0.903 100.00 0.904 0.000 0.904 0.000 0.903 100.00 0.904 0.000 0.904 0.000 0.903 0.903 100.00 0.904 0.000 0.904 0.000 0.904 0.000 0.904 0.000 0.903 0.903 100.00 0.904 0.000 0.	L39 26.75-	26.62	0.7	5.34	0.854	Α	0.000	0.854	0.854	100.00		0.000
L40 26.50- 23.99 0.7 5.34 17.284 A 0.000 17.284 17.284 100.00 14.167 0.000 0	26.50			-								0.000
21.50												
L41 21,50- 19,12 0.7 5,34 16,794 A 0.000 17,284 16,794 100,00 12,750 0.000 16,794 16,794 100,00 12,750 0.000 16,794 100,00 12,750 0.000 16,794 100,00 7,438 0.000 16,794 100,00 7,438 0.000 16,794 100,00 7,438 0.000 16,794 100,00 7,438 0.000 18,794 100,00 7,438 0.000 18,794 100,00 0.708 0.000 16,794 100,00 0.708 0.000 0.893 100,00 0.904 0.000 0.893 100,00 0.904 0.000 0.893 100,00 0.904 0.000 0.893 100,00 0.354 0.000 14,25 10,000 18,284 100,00 0.318 0.000 0.318 0.000 0.904 100,00 0.318 0.000 0.904 100,00 0.318 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.0000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.903 100,00 0.708 0.000 0.904 0.000 0.90		23.99	0.7	5.34	17.284				17.284			
L41 21.50- 16.75 19.12 16.75 0.7 5.34 5.34 16.794 16.794 B B C C C D.000 16.794 16.794 16.794 100.00 12.750 100.00 0.000 16.474 0.000 0.000 16.474 0.000 0.000 16.474 0.000 100.00 100.00 16.474 0.000 0.000 0.000 0.000 0.893 100.00 0.7438 0.000 0.000 0.904 0.000 0.000 0.893 100.00 0.708 0.000 0.000 0.904 0.000 0.000 0.893 100.00 0.904 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.354 0.000 0.000 0.903 0.	21.50											
16.75	144.04.50	40.40			40.704				40 770 4			
L42 16.75- 16.62 0.7 5.34 0.893 A 0.000 0.893 0.893 100.00 0.708 0.000 0.000 0.893 0.893 100.00 0.708 0.000 0.893 0.893 100.00 0.708 0.000 0.893 0.893 100.00 0.904 0.000 0.893 0.893 100.00 0.904 0.000 0.893 0.893 100.00 0.904 0.000 0.893 0.893 100.00 0.904 0.000 0.893 0.893 0.893 100.00 0.904 0.000 0.893 0.893 0.893 100.00 0.904 0.000 0.893 0.893 0.893 100.00 0.903 0.903 100.00 0.354 0.000 0.893 0.893 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.894 0.994 0.894 0.9		19,12	0.7	5.34	16.794				16.794			
L42 16.75- 16.50 16.62 0.7 5.34 0.893 A 0.000 0.893 0.893 100.00 0.708 0.000 L43 16.50- 14.25 15.37 0.7 5.34 8.084 A 0.000 8.084 8.084 100.00 0.354 0.000 L44 14.25- 14.00 14.12 0.7 5.34 0.903 A 0.000 8.084 100.00 6.375 0.000 L44 14.25- 14.00 14.12 0.7 5.34 0.903 A 0.000 0.903 0.903 100.00 0.708 0.000 L45 14.00- 9.00 11.49 0.7 5.34 18.284 A 0.000 0.903 0.903 100.00 0.354 0.000 L46 9.00-4.25 6.62 0.7 5.34 17.743 A 0.000 18.284 18.284 100.00 12.042 0.000 L47 4.25-4.00 4.12 0.7 5.34 17.743 A 0.000 17.743 17.743 100.00 0.354	10./5											
16.50	42 16 75	16.62	0.7	5 34	U 803				U 803			
L43 16.50- 14.25 L44 14.25- 14.10 L45 14.00- 9.00 L46 9.00-4.25 C 0.7 5.34 C 0.000 C 0		10.02	0,7	0.54	0.000				0,083			
L43 16.50- 14.25 15.37 14.25 0.7 5.34 5.34 8.084 A B C C C D.000 B B B D.000 C C D.000 B B D.000 D.903 D.903 D.903 D.900 D.900 D.903 D.900 D.900 D.903 D.900 D.90	10.00											0.000
14.25	L43 16.50-	15.37	0.7	5.34	8.084	_			8.084			0.000
L44 14.25- 14.12												0.000
L44 14.25- 14.00 14.12 0.7 5.34 0.903 A 0.000 0.903 0.903 0.903 100.00 100.00 0.708 0.904 0.000 0.903 0.903 L45 14.00- 9.00 11.49 0.7 5.34 18.284 A 0.000 0.903 18.284 100.00 100.00 100.00 12.042 0.000 0.000 0.903 L45 14.00- 9.00 11.49 0.7 5.34 18.284 A 0.000 0.903 18.284 100.00 100.00 12.042 0.000 0.903 L46 9.00-4.25 6.62 0.7 5.34 17.743 A 0.000 0.900 17.743 17.743 100.00 17.743 6.729 100.00 0.000 0.945 L47 4.25-4.00 4.12 0.7 5.34 0.945 0.945 A 0.000 0.945 0.000 0.945 0.945 100.00 0.935 0.900 0.354 0.000 0.935 0.000 0.000 0.935 0.000 L48 4.00-0.00 1.99 0.7 5.34 15.254 0.900 A 0.000 0.945 0.000 15.254 0.000 15.254 0.000 100.00 0.935 0.000 13.053 0.000 0.900 0.935 0.000												0.000
L45 14.00- 9.00		14.12	0.7	5.34	0.903		0.000		0.903			0.000
L45 14.00- 9.00 11.49 9.00 5.34 18.284 A 0.000 18.284 B 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 18.284 C 0.000 17.743 100.00 6.729 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 17.743 C 0.000 0.000 17.743 C 0.000 0.000 17.743 C 0.000 0.000 17.743 C 0.000 0.00	14.00							0.903		100.00	0.904	0.000
9.00 B B 0.000 18.284 100.00 18.087 0.000 14.69 0.000 18.087 0.000 0.0				_								0.000
L46 9.00-4.25		11.49	0.7	5.34	18.284				18.284			
L46 9.00-4.25 6.62 0.7 5.34 17.743 A 0.000 17.743 17.743 100.00 6.729 0.000 L47 4.25-4.00 4.12 0.7 5.34 0.945 A 0.000 0.945 0.945 100.00 6.729 0.000 L48 4.00-0.00 1.945 0.945 0.945 0.945 100.00 0.354 0.000 L48 4.00-0.00 1.99 0.7 5.34 15.254 A 0.000 15.254 15.254 100.00 4.958 0.000 B 0.000 15.254 15.254 100.00 13.053 0.000	9.00											
L47 4.25-4.00	14600010			ایم	47740				477.5			
L47 4.25-4.00	L40 9.00-4.25	6,62	0.7	5.34	17.743		I I		17.743			
L47 4.25-4.00				l								
L48 4.00-0.00 1.99 0.7 5.34 15.254 A 0.000 15.254 15.254 100.00 13.053 0.000 B 0.000 15.254 100.00 13.053 0.000	1474 25-4 00	A 12	02	5 2/	0 045				LOVE			
L48 4.00-0.00 1.99 0.7 5.34 15.254 A 0.000 15.254 15.254 100.00 13.053 0.000 B 0.000 15.254 15.254 100.00 13.053 0.000	LT: T.20-4.00	4.12	0.7	J.J4	ს,შუმ		1 1		U,840			
L48 4.00-0.00 1.99 0.7 5.34 15.254 A 0.000 15.254 15.254 100.00 4.958 0.000 B 0.000 15.254 100.00 13.053 0.000					•							
B 0.000 15.254 100.00 13.053 0.000	L48 4.00-0.00	1.99	0.7	5.34	15,254				15 254			0.000
, , , , , , , , , , , , , , , , , , ,				,			0.000				13.053	0.000
[Ċ	0,000	15,254		100.00	4.958	0.000

Load Combinations

C	Depositéen
Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 60 deg - No Ice
7	0.9 Dead+1.0 Wind 60 deg - No Ice
8	1.2 Dead+1.0 Wind 90 deg - No Ice
9	0.9 Dead+1.0 Wind 90 deg - No Ice
10	1.2 Dead+1.0 Wind 120 deg - No Ice
11	0.9 Dead+1.0 Wind 120 deg - No Ice
12	1.2 Dead+1.0 Wind 150 deg - No Ice
13	0.9 Dead+1.0 Wind 150 deg - No Ice
14	1.2 Dead+1.0 Wind 180 deg - No Ice
15	0.9 Dead+1.0 Wind 180 deg - No Ice
16	1.2 Dead+1.0 Wind 210 deg - No Ice
17	0.9 Dead+1.0 Wind 210 deg - No Ice
18	1.2 Dead+1.0 Wind 240 deg - No Ice
19	0.9 Dead+1.0 Wind 240 deg - No Ice
20	1.2 Dead+1.0 Wind 270 deg - No Ice
21	0.9 Dead+1.0 Wind 270 deg - No Ice
22	1.2 Dead+1.0 Wind 300 deg - No Ice
23	0.9 Dead+1.0 Wind 300 deg - No Ice
24	1.2 Dead+1.0 Wind 330 deg - No Ice
25	0.9 Dead+1.0 Wind 330 deg - No Ice
26	1.2 Dead+1.0 Ice+1.0 Temp
27	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp
29	1.2 Dead+1.0 Wind 60 ded+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
31	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
33	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1,2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1,2 Dead+1,0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Maximum Member Forces

Sectio n No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	151 - 146	Pole	Max Tension	39	0.00	0.00	0.00
			Max. Compression	26	-8.36	-0.72	2.26
			Max. Mx	8	-3.02	-19.53	0.19
			Max. My	2	-3.02	-0.31	19.53
			Max. √y	8	5.20	-19.53	0.19
			Max, Vx	2	-5.20	-0.31	19.53
			Max. Torque	10			2.22
L2	146 - 141	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-8.89	-0.75	2.31

						- Airi	
Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n No	ft	Type		Load	K	Moment	Moment
<u>No.</u>			Max. Mx	Comb.	0.00	kip-ft	kip-ft
			Max. My	8 2	-3.33 -3.33	-46.41	0.21
			Max. Vy	8	-3.33 5.56	-0.33 -46.41	46.42 0.21
			Max. Vx	2	-5.56	-0.33	46.42
			Max. Torque	10	-0.00	-0.55	2.22
L3	141 - 136	Pole	Max Tension	1	0.00	0.00	0.00
	**** 100	. 0.0	Max. Compression	26	-17.00	-2.85	4.08
			Max. Mx	8	-6.95	-97.05	0.83
			Max. My	2	-6.92	-1.38	97.24
			Max. Vv	8	11.11	-97.05	0.83
			Max. Vx	2	-11.27	-1.38	97.24
			Max. Torque	10			3.05
L4	136 - 131	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-18.98	-2.90	4.16
			Max. Mx	8	-7.91	-153.75	0.72
			Max. My	2	-7.88	-1.26	154.72
			Max. Vy	8	12.25	-153.75	0.72
			Max. Vx	2	-12.40	-1.26	154,72
			Max. Torque	10			3.05
L5	131 - 126	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-23.81	-2.95	4.30
			Max. Mx	8	-10.14	-223.28	0.62
			Max. My	2	-10.11	-1.14	225.04
			Max. Vy	8	14.46	-223.28	0.62
			. Max. Vx	2	-14.62	-1.14	225.04
1.6	100 100 5	D-I-	Max. Torque	10	0.00		3.07
L6	126 - 125.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	<i>-</i> 23.88	-2.95	4.31
			Max. Mx	8	-10.19 -10.46	-230.51	0.61
			Max, My	2	-10.16	-1.12	232.36
			Max. Vy Max. Vx	8 2	14.49 -14.65	-230.51 -1.12	0.61 232.36
			Max. Torque	10	-14.05	-1.12	3.07
L7	125.5 -	Pole	Max. Torque Max Tension	1	0.00	0.00	0.00
	125.25	1 010	Wax Tellololl	•	0.00	0.00	0.00
			Max. Compression	26	-23.92	-2.96	4.31
			Max. Mx	8	-10.23	-234.14	0.60
			Max. My	2	-10.20	-1.12	236.02
			Max. Vý	8	14.51	-234.14	0.60
			Max. Vx	2	-14.67	-1.12	236.02
			Max. Torque	10			3.07
L8	125.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	120.25						
			Max. Compression	26	-28.99	-3.04	6.56
			Max, Mx	8	<i>-</i> 12.45	-313.13	1,69
			Max. My	2	-12.41	-1.00	317.24
			Max. Vy	20	-17.15	310.04	2.84
			Max. Vx	2	-17.26	-1.00	317.24
			Max. Torque	10			3.54
L9	120.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	118.5						
			Max. Compression	26	-29.45	-3.09	6.61
			Max. Mx	8	-12.70	-343.11	1.66
			Max. My	2	-12.66	-0.96	347.65
			Max. Vy Max. Vx	20	-17.34	340.20	2.91
			Max. Vx Max. Torque	2	-17.51	-0.96	347.65
L10	118,5 -	Pole	Max. Forque Max Tension	10	0.00	0.00	3.54
LIG	118.25	rule	IVIAX TEHSIOH	1	0.00	0.00	0.00
	110.20		Max. Compression	26	-29.54	-3.10	6.62
			Max. Mx	8	-29.5 4 -12.76	-3.10 -347.42	1.66
			Max. My	2	-12.70 -12.72	-347.42 -0.96	352.03
			Max. Vy	20	-17.36	-0.90 344.54	2.92
			Max. Vx	20	-17.53	-0.96	352.03
			Max. Torque	10	11.00	0.00	3.54
L11	118.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	117.5			-			
			Max. Compression	26	-29.79	-3.12	6.64
			Max. Mx	8	-12.92	-360.40	1.64

Sectio	Elevation	Component	Condition	Gov.	0	84-1 4	16
n	ft	Туре	Condition	Load	Axial K	Major Axis Moment	Minor Axis Moment
No	_			Comb.		kip-ft	kip-ft
	"		Max. My	2	-12.88	-0.94	365.22
			Max. Vy	20	-17.46	357.59	2.95
			Max. Vx	2	-17.65	-0.94	365.22
			Max. Torque	10			3.54
L12	117.5 - 117.25	Pole	Max Tension	1	0.00	0.00	0.00
	777.22		Max. Compression	26	-29.87	-3.13	6.65
			Max, Mx	8	-12.97	-364,74	1.64
			Мах. Му	2	-12.92	-0.94	369.64
			Max. Vy	20	-17.48	361.96	2.96
			Max. Vx	2	-17.68	-0.94	369.64
			Max. Torque	10			3.54
L13	117.25 - 112.25	Pole	Max Tension	1	0.00	0.00	0.00
	112120		Max, Compression	26	-31.30	-3.28	6.79
			Max, Mx	8	-13.87	-453.10	1.54
			Max. My	2	-13.82	-0.83	459.72
			Max, Vý	20	-18.04	450,73	3.15
			Max. Vx	2	-18.36	-0.83	459.72
			Max. Torque	10			3.54
L14	112.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	107.25						
			Max. Compression	26	-32.69	-3.44	6.94
			Max. Mx	8	-14.80	-544.31	1.44
			Max. My	2	-14.76	-0.73	552.80
			Max. Vy	20	-18.57	542.20	3.34
			Max, Vx	2	-18.89	-0.73	552.80
L15	107.25 -	Pole	Max. Torque Max Tension	10	0.00	0.00	3.54
LIS	107.25 -	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-34,10	-3.59	7.08
			Max. Mx	8	-15.76	-638.36	1.33
			Max. My	2	-15.72	-0.62	648.54
			Max. Vy	20	-19.10	636.32	3.53
			Max. Vx	2	-19.42	-0.62	648.54
			Max. Torque	10			3.54
L16	102.25 - 97.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-34.49	-3.64	7.11
			Max. Mx	8	-16.01	-663.93	1.30
			Max. My	2	-15.98	-0.60	674.52
			Max. Vy	8	19.25	-663.93	1.30
			Max. Vx	14	19.56	-2.87	-669.54
			Max. Torque	10			3.53
L17	97.5 - 95.916	Pole	Max Tension	1	0.00	0.00	0.00
	33.510		Max. Compression	26	-36.85	-3.79	7.25
			Max. Mx	8	-17.63	-761.84	1.20
			Max. My	2	-17.60	-0.49	773.89
			Max. Vy	8	19.91	-761.84	1.20
			Max. Vx	14	20.21	-3.06	-768.92
	•		Max. Torque	10			3.53
L18	95.916 - 92.5	Pole	Max Tension	1	0.00	0.00	0.00
	92.5		Max. Compression	26	-38.06	-3.90	7.34
			Max. Mx	8	-18.43	-830.54	1.12
			Max. My	2	-18.40	-0.42	843.49
			Max. Vy	8	20.32	-830.54	1.12
			Max. Vx	14	20.62	-3.19	-838.60
			Max. Torque	10		* · · · ·	3.53
L19	92.5 - 92.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-38,15	-3.91	7.35
			Max. Mx	8	-18.49	-835.62	1.12
			Max. My	2	-18.46	-0.42	848.63
			Max. Vy	8	20.35	-835.62	1.12
			Max. Vx	14	20.64	-3.20	-843.76
1.00	00.00		Max. Torque	10			3.53
L20	92.25 -	Pole	Max Tension	1	0.00	0.00	0.00
	87.25						

No. No.	Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
Max. Compression		π	Type			K		
Max. My	710.			Max. Compression		-39.95		
Max. My 2 1-19.63 -0.31 -963.45 -0.31 -963.45 -0.31 -0.34 -0.44.55 -0.38 -948.45 -0.38 -948.45 -0.38 -948.45 -0.38 -948.45 -0.38 -948.45 -0.28 -0.								
L21 87.25 - 87 Pole Max Torque 10 10 10 10 10 10 10 1				Max. My	2			
Max Torque 10								
L21 87.25 - 87						21.26	-3.38	
Max. Compression 26 40,05 40,07 7,49	1.04	07.05 07	Dele			0.00	0.00	
Max. My	LZI	87.25 - 87	Pole					
Max. My								
Max. Vy 8 20.99								
Max Tension 1				•				
L22				Max. Vx	14	21.28	-3.39	-953.77
Max. Compression 26				•				
Max Mx	L22	87 - 82	Pole					
Max My				·				
L23								
Max. Vix								
Max Torque								
Max. Compression								
Max. My 2 -22.38 -1160.14 0.78	L23	82 - 77	Pole	Max Tension	1	0.00	0.00	0.00
Max. My								
Max. Vy								
Max								
L24								
L24						22.45	~3.10	
Max. Compression	1 24	77 - 72	Pole			0.00	0.00	
Max. My			. 0,0					
Max. Vy								
Max. Vx				Max. My	2	-23.76	0.02	1289.07
L25								
Pole						22.99	-3.95	
Max. Compression	LOF	70 67	D-1-	•		0.00	0.00	
Max. Mx	L25	12-61	Pole					
Max. My								
Max. Vý								
L26				-				
L26					14	23.56		-1402.36
Max. Compression								
Max. Mx	L26	67 - 63.25	Pole					
Max. My								
Max. Vý								
Max. Vx				-				
L27								
Max. Compression 26				Max. Torque	10			3.52
Max. Mx 8	L27	63.25 - 63	Pole					
Max. My				-				
Max. Vy								
L28 63 - 58 Pole Max. Vx 14 24.04 -4.28 -1497.51 Max. Torque 10 3.52 Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.34 -5.00 8.21 Max. Mx 8 -27.75 -1602.97 0.35 Max. My 2 -27.75 0.32 1620.15 Max. Vy 8 24.44 -1602.97 0.35 Max. Vx 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98				•				
L28 63 - 58 Pole Max. Torque Max. Torque Max. Torque Max. Compression 26 -51.34 -5.00 8.21 Max. Mx 8 -27.75 -1602.97 0.35 Max. My 2 -27.75 0.32 1620.15 Max. Vy 8 24.44 -1602.97 0.35 Max. Vy 8 24.44 -1602.97 0.35 Max. Vy 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 Max. Torque 10 3.52 Max. Torque 10 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98								
L28 63 - 58 Pole Max Tension Max. Compression 26 (Max. Compression 26 (Max. Mx) (M						24.04	7.20	
Max. Mx 8 -27.75 -1602.97 0.35 Max. My 2 -27.75 0.32 1620.15 Max. Vy 8 24.44 -1602.97 0.35 Max. Vx 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98	L28	63 - 58	Pole	•		0.00	0.00	
Max. My 2 -27.75 0.32 1620.15 Max. Vy 8 24.44 -1602.97 0.35 Max. Vx 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98				Max. Compression	26	-51.34	-5,00	8,21
Max. Vý 8 24.44 -1602.97 0.35 Max. Vx 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98				Max. Mx			-1602.97	0.35
Max. Vx 14 24.63 -4.46 -1619.11 Max. Torque 10 3.52 L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vy 14 24.78 -4.51 -1649.98								
L29 58 - 56.75 Pole Max Torque Max Torque Max Tension 1 0.00								
L29 58 - 56.75 Pole Max Tension 1 0.00 0.00 0.00 Max. Compression 26 -51.87 -5.04 8.24 Max. Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vx 14 24.78 -4.51 -1649.98						24.63	-4.46	
Max. Compression 26 -51.87 -5.04 8.24 Max, Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vx 14 24.78 -4.51 -1649.98	1 20	58 - 56 75	Dolo	•		0.00	0.00	
Max, Mx 8 -28.12 -1633.60 0.32 Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vx 14 24.78 -4.51 -1649.98	LZŰ	JU - JU./ J	ruie					
Max. My 2 -28.11 0.34 1650.77 Max. Vy 8 24.59 -1633.60 0.32 Max. Vx 14 24.78 -4.51 -1649.98								
Max. Vy 8 24.59 -1633.60 0.32 Max. Vx 14 24.78 -4.51 -1649.98								
				_				0.32
Max. Torque 10 3.52						24.78	-4.5 1	
				Max. Torque	10			3.52

	F1:						
Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n No.	ft	Type		Load	K	Moment	Moment
L30	56.75 - 56.5	Pole	Max Tension	Comb. 1	0.00	kip-ft	kip-ft
L30	30.73 - 30.3	FUIC	Max. Compression	26	-51.99	0.00 -5.05	0.00 8.25
			Max, Mx	8	-28.21	-1639.75	0.32
			Max. My	2	-28.21	0.35	1656.91
			Max. Vy	8	24.61	-1639,75	0.32
			Max. Vx	14	24.80	-4.52	-1656.17
			Max. Torque	10	24.00	7.02	3.52
L31	56.5 -	Pole	Max Tension	1	0.00	0.00	0.00
	47.49 9			-			
			Max. Compression	26	-53.98	-5.20	8.35
			Max. Mx	8	-29.66	-1751,73	0.21
			Max. My	14	-29.64	-4.68	-1768.90
			Max. Vy	8	25.15	-1751.73	0.21
			Max. Vx	14	25.32	-4.68	-1768.90
			Max. Torque	10			3,52
L32	47.499 -	Pole	Max Tension	1	0.00	0.00	0.00
	46.999						
			Max. Compression	26	-57.86	-5.36	8.46
			Max. Mx	8	-32.64	-1879.19	0.10
			Max. My	14	-32.63	-4.86	-1897.09
			Max. Vy	8	25.83	-1879.19	0.10
			Max. Vx	14	25.97	-4 .86	-1897.09
L33	46.999 -	Pole	Max. Torque Max Tension	10 1	0.00	0.00	3.52
LOO	41.999	ruie	Wax rension	•	0.00	0.00	0.00
	41.000		Max. Compression	26	- 6 0.15	-5.52	8.57
			Max. Mx	8	-34.43	-2009.70	-0.02
			Max. My	14	-34,42	-5.05	-2028.16
			Max. Vy	8	26.38	-2009.70	-0.02
			Max. Vx	14	26.48	-5.05	-2028.16
			Max. Torque	10		3.55	3.52
L34	41.999 -	Pole	Max Tension	1	0.00	0.00	0.00
	36.999						
			Max. Compression	26	-62.57	-5.68	8.68
			Max. Mx	8	-36.25	-2142.93	-0.13
			Max. My	14	-36.24	-5.23	-2161.80
			Max. Vy	8	26.93	-2142.93	-0.13
			Max. Vx	14	27.01	-5.23	-2161.80
105	00.000		Max. Torque	10			3,52
L35	36.999 -	Pole	Max Tension	1	0.00	0.00	0.00
	34.25		M O	00	00.00		0.74
			Max. Compression	26	-63.96	-5.77	8.74
			Max. Mx	8	-37.26	-2217.34	-0.20
			Max. My	14 8	-37.25	-5.33	-2236.42
			Max. Vy Max. Vx	14	27.23 27.32	-2217.34 -5.33	-0.20 - 2236.42
			Max. Torque	10	21.32	-0.33	3.52
L36	34,25 - 34	Pole	Max Tension	1	0.00	0.00	0.00
200	011.20 01	. 0.0	Max. Compression	26	-64.08	-5.78	8.75
			Max. Mx	8	-37.36	-2224.15	-0.20
			Max, My	14	-37.36	-5.34	-2243.25
			Max. Vy	8	27.24	-2224.15	-0.20
			Max. Vx	14	27.33	-5.34	-2243.25
			Max. Torque	10			3.52
L37	34 - 29	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	- 66 .61	-5.92	8.83
			Max. Mx	8	-39.22	-2361.68	-0.32
			Max. My	14	-39.22	-5.52	-2381.14
			Max. Vy	8	27.77	-2361.68	-0.32
			Max. Vx	14	27.86	-5.52	-2381.14
1.00	00 00 ==	5.1	Max. Torque	10			3.52
L38	29 - 26.75	Pole	Max Tension	1	0.00	0.00	0.00
			Max, Compression	26	-67.75	-5.98	8.87
			Max. Mx	8	-40.07	-2424.42	-0.37
			Max. My	14	-40.07	-5.60	-2444.04
			Max. Vy Max. Vx	8 14	28.01	-2424.42 5.60	-0.37
			Max. Vx Max. Torque	14 10	28.09	-5.60	-2444.04 3.52
L39	26.75 - 26.5	Pole	Max Tension	1	0.00	0.00	0.00
_50	_00 _20,0	1 010	Max i Gildion	•	0.00	0.00	0.00

Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n	ft	Type		Load	К	Moment	Moment
No.			May Campagaian	Comb.	-67.88	kip-ft -5.99	kip-ft
			Max. Compression Max, Mx	26 8	-07.88 -40.18	-5.99 -2431,42	8.88 -0.38
			Max. My	14	-40.16 -40.17	-2451,42 -5.61	-2451.06
			Max. Vy	8	28.02	-2431.42	-0.38
			Max. Vx	14	28.11	-2451.42 -5.61	-2451.06
			Max. Torque	10	20,11	-0.01	3.52
L40	26.5 - 21.5	Pole	Max Tension	1	0.00	0.00	0.00
LHU	20.5 - 21.5	I VIC	Max. Compression	26	-70.43	-6.13	8.95
			Max. Mx	8	-4 2.07	-2572.81	-0.50
			Max. My	14	-4 2.07	-5.78	-2592.80
			Max. Vy	8	28.54	-2572.81	-0.50
			Max. Vx	14	28.62	-5.78	-2592.80
			Max. Torque	10	20.02	01,0	3.52
L41	21.5 - 16.75	Pole	Max Tension	1	0.00	0.00	0.00
	21.0 10.10	. 0.0	Max. Compression	26	-72,81	-6.24	9.17
			Max. Mx	8	-43.91	-2709,49	-0.61
			Max. My	14	-43.91	-5.95	-2729.81
			Max. Vy	8	29.03	-2709,49	-0.61
			Max. Vx	14	29.11	-5,95	-2729.81
			Max. Torque	10			3.52
L42	16.75 - 16.5	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-72,96	-6.24	9.19
			Max. Mx	8	-44.04	-2716.75	-0.61
			Max. My	14	-44.03	-5.96	-2737.08
			Max. Vy	8	29.04	-2716.75	-0.61
			Max. Vx	14	29.12	-5.96	-2737.08
			Max. Torque	10			3,51
L43	16.5 - 14.25	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	<i>-</i> 74.28	-6.28	9.30
			Max. Mx	8	-45.10	-2782.37	-0.67
			Max. My	14	-45.09	- 6.04	-2802.85
			Max. Vy	8	29.29	-2782.37	- 0.67
			Max. Vx	14	29.37	-6.04	-2802.85
			Max. Torque	10			3.51
L44	14.25 - 14	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-74.42	-6.29	9.32
			Max. Mx	8	-45.21	-2789.69	-0.67
			Max. My	14	-45.21	-6.05	-2810.19
			Max. Vy	8	29.31	-2789.69	-0.67
			Max. Vx	14	29.39	-6.05	-2810.19
			Max. Torque	10			3.51
L45	14 - 9	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-77.13	-6.40	9.55
			Max. Mx	8	-47.38	-2937.55	-0.79
			Max. My	14	-47.38	-6.23	-2958.37
			Max. Vy	8	29.84	-2937.55	-0.79
			Max. Vx	14	29.91	-6.23	-2958.37
			Max. Torque	10			3.51
L46	9 - 4.25	Pole	Max Tension	1	0.00	0.00	0.00
	•		Max. Compression	26	-79.67	-6.55	9.71
			Max. Mx	8	-49,47	-3080.35	-0.90
			Max. My	14	- 4 9.47	-6.39	-3101.48
			Max. Vy	8	30.31	-3080.35	-0.90
			Max. Vx	14	30.39	-6.39	-3101.48
			Max. Torque	10		0.00	3.51
L47	4.25 - 4	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-79.79	-6.56	9.72
			Max. Mx	8	-49.58	-3087.93	-0.91
			Max. My	14	-49.58	-6.40	-3109.07
			Max. Vy	8	30.32	-3087.93	-0.91
			Max. Vx	14	30.39	-6.40	-3109.07
1.40	4 ^	D-I+	Max, Torque	10	0.00	0.00	3.51
L48	4 - 0	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-81.70	-6.67	9.83
			Max. Mx	8	-51.19 51.10	-3209.95	-1.00
			Max. My	14	-51.19	-6.54	-3231.34
			Max. Vy	8	30.70	-3209.95	-1.00
			Max. Vx	14 10	30.77	-6.54	-3231.34 3,51
			iviax. Forque	טו			10,6
			Max. Torque	10	V 0	0.0.	

Sectio	Elevation	Component	Condition	Gov.	Axial	Major Axis	Minor Axis
n	ft	Type		Load	K	Moment	Moment
No.				Comb.		kip-ft	kip-ft

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, 2 K
Pole	Max. Vert	26	81.70	0.00	-0.00
	Max. H _x	21	38.40	29.46	0.03
	Max. H _z	2	51.20	0.03	29.79
	Max. M _x	2	3209.26	0.03	29.79
	Max. M _z	8	3209.95	-30.68	-0.03
	Max, Torsion	10	3.51	-25.94	-15.09
	Min. Vert	3	38.40	0.03	29.79
	Min. H _x	8	51.20	-30.68	-0.03
	Min. H _z	15	38.40	-0.03	-30.75
	Min. M _x	14	-3231.34	-0.03	-30.75
	Min. M _z	20	-3163.87	29.46	0.03
	Min. Torsion	22	-3.51	25,72	14.96

Tower Mast Reaction Summary

Load Combination	Vertical K	Shear _x K	Shear _z K	Overturning Moment, M _x kip-ft	Overturning Moment, M₂ kip-ft	Torque kip-ft
Dead Only	42.67	-0.00	0.00	-2.31	-1.92	0.00
1.2 Dead+1.0 Wind 0 deg -	51.20	-0.03	-29.79	- 3209.26	1.52	1.60
No Ice						
0.9 Dead+1.0 Wind 0 deg -	38.40	-0.03	-29.79	-3169.51	2.13	1.56
No Ice						
1.2 Dead+1.0 Wind 30 deg -	51.20	14.70	-25.67	-2767.59	-1582.21	-0.21
No Ice						
0.9 Dead+1.0 Wind 30 deg -	38.40	14.70	- 25.67	-2733.20	-1562.37	-0.24
No Ice	E4 00	00.47	45.40	4004.04	0750.04	4.04
1.2 Dead+1.0 Wind 60 deg -	51.20	26.17	-15.19	-1601.24	-2750.31	-1.94
No Ice	38.40	26.17	-15.19	-1581.10	-2716.43	-1.94
0.9 Dead+1.0 Wind 60 deg - No Ice	30.40	20.17	-10.18	-1361,10	-27 10.43	-1.84
1.2 Dead+1.0 Wind 90 deg -	51.20	30.68	0.03	1.00	-3209.95	-3.15
No Ice	31.20	30.00	0.03	1.00	-0203.33	-0.10
0.9 Dead+1.0 Wind 90 deg -	38.40	30.68	0.03	1.75	-3170.61	-3.12
No Ice	00.10	00.00	0.00		0170.01	02
1,2 Dead+1,0 Wind 120 deg	51.20	25.94	15.09	1591.45	-2735.79	-3.51
- No Ice						
0.9 Dead+1.0 Wind 120 deg	38.40	25.94	15.09	1572.92	-2702.00	-3.47
- No Ice						
1.2 Dead+1.0 Wind 150 deg	51.20	15.06	26.24	2770.78	-1592.20	-2.93
- No Ice						
0.9 Dead+1.0 Wind 150 deg	38.40	15.06	26.24	2737.95	-1572.27	-2.88
- No Ice						
1.2 Dead+1.0 Wind 180 deg	51.20	0.03	30.75	3231,34	-6.54	-1.60
- No Ice						
0.9 Dead+1.0 Wind 180 deg	38.40	0.03	30.75	3193.07	- 5.82	-1.56
- No Ice	54.00	-15.32	20.72	2707.04	1597.68	0.22
1.2 Dead+1.0 Wind 210 deg - No Ice	51.20	-15.32	26.73	2797.04	1997.00	0.22
0.9 Dead+1.0 Wind 210 deg	38.40	<i>-</i> 15.32	26.73	2764.08	1579.07	0.25
- No Ice	30,40	-13.32	20.73	2704.00	1078.07	0.20
1.2 Dead+1.0 Wind 240 deg	51,20	-25.85	15.01	1583.93	2725.78	1.95
- No Ice	01.20	20,00	10,01	1000.00	2.20.70	1.50
0.9 Dead+1.0 Wind 240 deg	38.40	-25.85	15.01	1565.49	2693.39	1.95
- No Ice	22.10	25.50		,	_	
1.2 Dead+1.0 Wind 270 deg	51.20	-29.46	-0.03	-7.06	3163.87	3.15
- No Ice		· -				

Load Combination	Vertical K	Shear _x K	Shear₂ K	Overturning Moment, M _x kip-ft	Overturning Moment, Mz kip-ft	Torque kip-ft
0.9 Dead+1.0 Wind 270 deg - No Ice	38.40	-29.46	-0.03	-6.20	3126.12	3.12
1.2 Dead+1.0 Wind 300 deg - No Ice	51.20	-25.72	-14.96	-1605.71	2744.97	3.51
0.9 Dead+1.0 Wind 300 deg - No Ice	38.40	-25.72	-14.96	-1585.49	2712.39	3.46
1.2 Dead+1.0 Wind 330 deg - No ice	51.20	-15.33	-26.69	-2806.17	1604.11	2.93
0.9 Dead+1.0 Wind 330 deg - No Ice	38.40	-15.33	-26,69	-2771.53	1585.40	2.88
1.2 Dead+1.0 Ice+1.0 Temp	81.70	-0.00	0.00	-9.83	-6.67	0.00
1.2 Dead+1.0 Wind 0	81.70	-0.01	-6.77	-835.35	-5.79	0.72
deg+1.0 lce+1.0 Temp						
1.2 Dead+1.0 Wind 30	81.70	3.33	-5.82	-718.60	-412.05	0.14
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 60	81.70	5.85	-3.39	-420.11	-712.43	-0.46
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 90	81.70	6,83	0.01	-8.99	- 828.02	-0.94
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 120	81.70	5.81	3.38	399.96	-710.08	-1.17
deg+1.0 Ice+1.0 Temp	04.77					
1.2 Dead+1.0 Wind 150	81.70	3.36	5.85	700.04	-413.93	-1.08
deg+1.0 lce+1.0 Temp 1.2 Dead+1.0 Wind 180	04.70	0.04	0.07	040.07	774	0.70
deg+1.0 Ice+1.0 Temp	81,70	0.01	6.87	819.87	-7.71	-0.72
1.2 Dead+1.0 Wind 210	81.70	-3.41	5.95	706.49	402.05	0.44
deg+1.0 lce+1.0 Temp	01.70	-3.41	5.95	700.49	403.05	-0.14
1.2 Dead+1.0 Wind 240	81.70	-5.79	3.36	398,20	695.45	0.47
dea+1.0 ce+1.0 Temp	01110	5.70	0.00	000.20	000.40	0.47
1.2 Dead+1.0 Wind 270	81.70	-6.68	-0.01	-10.92	805,49	0.95
deg+1.0 Ice+1.0 Temp						2.20
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp	81.70	-5.84	-3.39	-4 21.65	699.67	1.17
1.2 Dead+1.0 Wind 330	81.70	-3.42	-5.95	-727.20	404.62	1.08
deg+1.0 Ice+1.0 Temp						
Dead+Wind 0 deg - Service	42.67	-0.01	-6.46	-693.42	-1.21	0,35
Dead+Wind 30 deg - Service	42.67	3.19	-5.57	-598.38	-342.56	-0.05
Dead+Wind 60 deg - Service	42.67	5.68	-3.30	-347.00	-594.34	-0.43
Dead+Wind 90 deg - Service	42.67	6.66	0.01	-1.65	-693.35	-0.69
Dead+Wind 120 deg -	42.67	5.63	3.27	341.13	- 591.17	-0.77
Service						
Dead+Wind 150 deg -	42.67	3.27	5.69	595.35	-344.73	-0.64
Service						
Dead+Wind 180 deg -	42.67	0.01	6.67	694.47	-2.95	-0.35
Service Dead+Wind 210 deg -	42.67	-3.32	5.80	604.03	242.04	0.05
Service	42.07	-3.32	5.60	601.03	342.84	0.05
Dead+Wind 240 deg - Service	42.67	-5.61	3.26	339.50	585.93	0.43
Dead+Wind 270 deg -	42.67	-6.39	-0.01	-3.39	680.31	0.69
Service Dead+Wind 300 deg -	42.67	-5.58	-3.25	-347.96	590.11	0.77
Service Dead+Wind 330 deg - Service	42.67	-3.33	-5.79	-606.74	344,22	0.64

Solution Summary

	Sun	n of Applied Force	es		Sum of Reaction	าร	
Load	PX	PY	PΖ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-42.67	0.00	0.00	42.67	-0.00	0.003%
2	-0.03	-51.20	-29.79	0.03	51.20	29.79	0.001%
3	-0.03	-38.40	- 29.79	0.03	38.40	29.79	0.001%
4	14.70	-51.20	-25.67	-14.70	51.20	25.67	0.000%
5	14.70	-38.40	-25.67	-14.70	38.40	25.67	0.000%
6	26,17	-51.20	-15.19	-26.17	51.20	15.19	0.000%

	Sun	n of Applied Force	es ·		Sum of Reaction	ns	
Load	PX	 PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	κ	K	K	K	
7	26.17	-38.40	-15.19	-26.17	38.40	15.19	0.000%
8	30.68	-51.20	0.03	-30.68	51.20	-0.03	0.000%
9	30.68	-38.40	0.03	-30.68	38.40	-0.03	0.001%
10	25.94	-51.20	15.09	-25.94	51.20	-15.09	0.000%
11	25.94	-38.40	15.09	-25.94	38.40	-15.09	0.000%
12	15.06	-51,20	26.24	-15,06	51.20	-26.24	0.000%
13	15.06	-38.40	26.24	-15.06	38.40	-26.24	0.000%
14	0.03	-51,20	30.75	-0.03	51.20	-30.75	0.001%
15	0.03	-38.40	30.75	-0.03	38.40	-30.75	0.001%
16	-15.32	-51.20	26.73	15.32	51.20	-26.73	0.000%
17	-15,32	-38.40	26.73	15.32	38.40	-26.73	0.000%
18	-25.85	-51.20	15.01	25.85	51.20	-15.01	0.000%
19	-25,85	-38.40	15.01	25.85	38.40	-15.01	0.000%
20	-29.46	-51.20	-0.03	29.46	51.20	0.03	0.000%
21	-29.46	-38.40	-0.03	29.46	38.40	0.03	0.000%
22	-25.72	-51,20	-14.96	25.72	51.20	14.96	0.000%
23	-25.72	-38.40	-14.96	25.72	38.40	14.96	0.000%
24	-15.33	-51,20	-26.69	15.33	51.20	26.69	0.000%
25	-15.33	-38.40	-26.69	15.33	38.40	26.69	0.000%
26	0.00	-81.70	0.00	0.00	81.70	-0.00	0.000%
27	-0.01	-81.70	-6.77	0.01	81.70	6.77	0.000%
28	3,33	-81.70	-5.82	-3.33	81.70	5,82	0.000%
29	5.85	-81.70	-3.39	-5.85	81.70	3.39	0.000%
30	6,83	-81.70	0.01	-6.83	81.70	-0.01	0.000%
31	5.81	-81,70	3.38	-5.81	81.70	-3.38	0.000%
32	3.36	-81.70	5.85	-3.36	81.70	-5.85	0.000%
33	0.01	-81.70	6.87	-0.01	81.70	- 6.87	0.000%
34	-3.41	-81.70	5.95	3.41	81,70	-5.95	0.000%
35	-5.79	-81.70	3.36	5.79	81.70	-3.36	0.000%
36	-6.68	-81,70	-0.01	6.68	81.70	0.01	0.000%
37	-5.84	-81.70	-3,39	5.84	81.70	3,39	0.000%
38	-3.42	-81.70	-5.95	3.42	81.70	5.95	0.000%
39	-0.01	-42.67	-6.46	0.01	42,67	6.46	0.004%
40	3.19	-42.67	-5,57	-3.19	42.67	5,57	0.001%
41	5.68	-42.67	-3.30	-5.68	42.67	3.30	0.001%
42	6.66	-42.67	0.01	-6.66	42.67	-0.01	0.002%
43	5.63	-42.67	3.27	-5.63	42.67	-3.27	0.001%
44	3.27	-42.67	5.69	-3.27	42.67	-5.69	0.001%
45	0.01	-42.67	6.67	-0.01	42.67	- 6.67	0.004%
46	-3.32	-42.67	5.80	3.32	42.67	-5.80	0.001%
47	-5.61	-42.67	3.26	5.61	42.67	-3.26	0.001%
48	-6.39	-42.67	-0.01	6.39	42.67	0.01	0.002%
49	-5.58	-42.67	-3.25	5.58	42.67	3.25	0.001%
50	-3.33	-42.67	-5.79	3.33	42.67	5.79	0.001%

Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	6	0.00000001	0.00001463
2	Yes	21	0.00000001	0.00009815
3	Yes	20	0.00000001	0.00013660
4	Yes	26	0.00000001	0.00008232
5	Yes	25	0.00000001	0.00011116
6	Yes	26	0.00000001	0.00008416
7	Yes	25	0.00000001	0.00011385
8	Yes	22	0.00000001	0.00010202
9	Yes	21	0.00000001	0.00014525
10	Yes	25	0.00000001	0.00014896
11	Yes	25	0.00000001	0.00010451
12	Yes	26	0.00000001	0.00008642
13	Yes	25	0.00000001	0.00011706
14	Yes	21	0.00000001	0.00011144
15	Yes	21	0.00000001	0.00008209
16	Yes	26	0.00000001	0.00008222
17	Yes	25	0.00000001	0.00011132
18	Yes	25	0.00000001	0.00014993
19	Yes	25	0.00000001	0.00010540
20	Yes	22	0.00000001	0.00010900
21	Yes	22	0.00000001	0.00008142
22	Yes	26	0.00000001	0.00008643
23	Yes	25	0.00000001	0.00011716
24	Yes	26	0.00000001	0.00007981
25	Yes	25	0.00000001	0.00010768
26	Yes	15	0.00000001	0.00014859
27	Yes	23	0.00000001	0.00008508
28	Yes	23	0.00000001	0.00010860
29	Yes	23	0.00000001	0.00010917
30	Yes	23	0.00000001	0.00008402
31	Yes	23	0.00000001	0.00010201
32	Yes	23	0.00000001	0.00010637
33	Yes	22	0.00000001	0.00014614
34	Yes	23	0.00000001	0.00010124
35	Yes	23	0.00000001	0.00009945
36	Yes	22	0.00000001	0.00014562
37	Yes	23	0.00000001	0.00010845
38	Yes	23	0.00000001	0.00010525
39	Yes	16	0.00014670	0.00013332
40	Yes	19	0.00000001	0.00009556
41	Yes	19	0.00000001	0.00010833
42	Yes	17	0.00000001	0.00013208
43	Yes	18	0.00000001	0.00014859
44	Yes	19	0.00000001	0.00011465
45	Yes	16	0.00014645	0.00013443
46	Yes	19	0.00000001	0.00009387
47	Yes	18	0.00000001	0.00014854
48	Yes	17	0.00000001	0.00013168
4 9	Yes	19	0.00000001	0.00011846
50	Yes	19	0.00000001	0.00008491

Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt	Twist
L1	151 - 146	22.3859	39	1.3829	0.0120
L2	146 - 141	20.9386	39	1.3793	0.0114
L3	141 - 136	19.5025	39	1.3619	0.0099
L4	136 - 131	18.0915	39	1.3298	0.0083
L5	131 - 126	16,7238	39	1.2800	0.0069
L6	126 - 125.5	15.4161	39	1.2150	0.0056
L7	125.5 - 1 25.25	15.2892	39	1.2078	0.0054
L8	125.25 - 120.25	15.2261	39	1.2055	0.0054
L9	120.25 - 118.5	13.9897	39	1.1544	0.0047

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.	ft	Deflection	Load	Φ	0
		in	Comb.		
L10	118.5 - 118.25	13.5701	39	1.1348	0.0044
L11	118.25 - 117.5	13.5107	39	1.1332	0.0044
L12	117.5 - 117.25	13,3332	39	1.1281	0.0043
L13	117.25 - 112.25	13.2742	39	1.1259	0.0043
L14	112.25 - 107.25	12.1198	39	1.0781	0.0038
L15	107.25 - 102. 25	11.0184	39	1.0250	0.0033
L16	102.25 - 97.5	9.9750	39	0.9672	0.0029
L17	100.916 - 95.916	9.7070	39	0.9514	0.0028
L18	95.916 - 92,5	8.7269	39	0.9149	0.0026
L19	92.5 - 92.25	8.0857	39	0.8775	0.0024
L20	92.25 - 87.25	8.0398	39	0.8748	0.0024
L21	87.25 - 87	7.1553	50	0.8180	0.0021
L.22	87 - 82	7.1126	50	0.8155	0.0021
L23	82 - 77	6.2870	50	0.7646	0.0019
L24	77 - 72	5.5149	50	0.7125	0.0017
L25	72 - 67	4.7 977	50	0.6591	0.0015
L26	67 - 63.25	4.1364	50	0.6048	0.0013
L27	63.25 - 63	3.6775	50	0.5641	0.0012
L28	63 - 58	3.6480	50	0.5614	0.0012
L29	58 - 56.75	3.0889	50	0.5066	0.0010
L30	56.75 - 56.5	2.9580	50	0.4931	0.0010
L31	56.5 - 47.499	2,9322	50	0.4907	0.0009
L32	51.999 - 46.999	2.4902	50	0.4473	0.0008
L33	46.999 - 41.999	2,0341	50	0.4215	0.0008
L34	41.999 - 36.999	1.6171	50	0.3750	0.0007
L35	36.999 - 34.25	1.2488	50	0.3283	0.0006
L36	34.25 - 34	1.0672	50	0.3029	0.0005
L37	34 - 29	1.0514	50	0.3005	0.0005
L38	29 - 26.75	0.7611	50	0.2539	0.0004
L39	26.75 - 26.5	0.6463	50	0.2332	0.0004
L40	26.5 - 21.5	0.6341	50	0.2309	0.0004
L41	21.5 - 16.75	0.4167	50	0.1844	0.0003
L42	16.75 - 16.5	0.2550	50	0.1409	0.0002
L43	16.5 - 14.25	0.2476	50	0.1389	0.0002
L44	14.25 - 14	0.1863	50	0.1214	0.0002
L45	14 - 9	0.1800	50	0.1194	0.0002
L46	9 - 4.25	0.0765	50	0.0783	0.0001
L47	4.25 - 4	0.0177	50	0.0399	0.0001
L48	4-0	0.0157	50	0.0376	0.0001

Critical Deflections and Radius of Curvature - Service Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt	Twist	Radius of Curvature ft
148.00	(2) AM-X-CD-16-65-00T-RET w/ Mount Pipe	39	21.5168	1.3819	0.0117	26203
140.00	DB854DG65ESX w/ Mount Pipe	39	19.2177	1.3568	0.0096	10242
132.00	TME-1900MHZ RRH	39	16.9930	1,2910	0.0071	5215
130.00	GPS-TMG-HR-26NCM	39	16.4569	1.2687	0.0066	4705
122.00	ERICSSON AIR 21 B2A B4P w/	39	14.4163	1,1749	0.0050	5466
	Mount Pipe					

Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt	Twist
L1	151 - 146	103.2916	2	6.3641	0.0551
L2	146 - 141	96.6437	2	6.3487	0.0522
L3	141 - 136	90.0449	2	6.2709	0.0455
L4	136 - 131	83.5713	14	6.1279	0.0381
L5	131 - 126	77.2976	14	5.9029	0.0313
L6	126 - 125.5	71.2913	14	5.6063	0.0254
L7	125.5 - 125.25	70,7083	14	5.5730	0.0248

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.	ft	Deflection	Load	o o	•
		in	Comb.		
L8	125.25 - 120.25	70.4179	14	5.5626	0.0247
L9	120,25 - 118.5	64.7326	14	5.3294	0.0213
L10	118.5 - 118.25	62.8017	14	5.2402	0.0201
L11	118.25 - 117.5	62.5284	14	5.2325	0.0200
L12	117.5 - 117.25	61.7108	14	5.2094	0,0197
L13	117.25 - 112.25	61.4392	14	5.1994	0.0196
L14	112.25 - 107.25	56.1214	14	4.9811	0.0173
L15	107.25 - 102.25	51.0424	14	4.7376	0.0153
L16	102.25 - 97.5	46,2268	14	4,4722	0.0133
L17	100.916 - 95.916	44.9890	14	4.3993	0.0129
L18	95.916 - 92.5	40.4608	14	4.2316	0.0119
L19	92.5 - 92.25	37.4969	14	4.0605	0.0109
L20	92.25 - 87.25	37.2848	14	4.0479	0.0109
L21	87.25 - 87	33.1851	14	3.7873	0.0096
L22	87 - 82	32.9873	14	3.7759	0.0095
L23	82 - 77	29.1579	14	3.5422	0.0085
L24	77 - 7 2	25.5763	14	3.3020	0.0076
L25	72 - 67	22.2489	14	3.0561	0.0067
L26	67 - 63.25	19,1813	14	2,8052	0.0059
L27	63.25 - 63	17.0525	14	2.6175	0.0053
L28	63 - 58	16.9159	14	2.6050	0.0053
L29	58 - 56.75	14.3220	14	2.3506	0.0045
L30	56.75 - 56.5	13.7150	14	2.2879	0.0044
L31	56.5 - 47.499	13.5955	14	2.2766	0.0043
L32	51,999 - 46,999	11.5450	14	2.0749	0.0038
L33	46.999 - 41.999	9.4299	14	1.9553	0.0035
L34	41,999 - 36,999	7.4959	14	1.7394	0.0030
L35	36.999 - 34.25	5.7889	24	1.5224	0.0026
L36	34.25 - 34	4.9466	24	1.4042	0.0023
L37	34 - 29	4.8734	24	1.3935	0.0023
L38	29 - 26.75	3,5277	24	1,1774	0.0019
L39	26.75 - 26.5	2.9956	24	1.0811	0.0017
L40	26.5 - 21.5	2.9393	24	1,0704	0.0017
L41	21.5 - 16.75	1,9315	24	0.8549	0.0013
L42	16.75 - 16.5	1.1817	24	0.6530	0.0010
L43	16.5 - 14.25	1,1477	24	0.6440	0.0010
L44	14.25 - 14	0.8634	24	0.5627	0.0008
L45	14 - 9	0.8342	24	0.5533	0.0008
L46	9 - 4.25	0.3546	24	0.3630	0.0005
L47	4.25 - 4	0.0822	24	0.1850	0.0003
L48	4-0	0.0728	24	0.1741	0.0002

Critical Deflections and Radius of Curvature - Design Wind

Elevation ft	Appurtenance	Gov. Load Comb.	Deflection in	Tilt	Twist	Radius of Curvature ft
148.00	(2) AM-X-CD-16-65-00T-RET w/ Mount Pipe	2	99.2999	6.3600	0.0539	6214
140.00	DB854DG65ESX w/ Mount Pipe	2	88.7361	6.2481	0.0442	2400
132.00	TME-1900MHZ RRH	14	78.5334	5.9526	0.0329	1190
130.00	GPS-TMG-HR-26NCM	14	76.0724	5.8515	0.0304	1065
122.00	ERICSSON AIR 21 B2A B4P w/ Mount Pipe	14	66.6950	5.4225	0.0228	1223

Compression Checks Pole Design Data

Section No.	Elevation ft	Size	L ft	L _v ft	Kl/r	A in²	Pu K
L1	151 - 146 (1)	TP18.5255x17.59x0.2188	5.00	0.00	0.0	12.897 7	-3.02
L2	146 - 141 (2)	TP19.461x18.5255x0.218	5.00	0.00	0.0	13,556	-3.33

Section	Eleveties	Si	,	•	W17	Α	
Section No.	Elevation ft	Size	L ft	L _u ft	KI/r	A in²	P⊔ K
L3	141 - 136 (3)	TP20.3965x19.461x0.218	5.00	0.00	0.0	14.215	-6.93
L4	136 - 131 (4)	8 TP21.3321x20.3965x0.21 88	5.00	0.00	0.0	9 14.875 0	-7.88
L5	131 - 126 (5)	TP22.2676x21.3321x0.21 88	5.00	0.00	0.0	15.534 2	-10.11
L6	126 - 125.5 (6)	TP22.3611x22,2676x0,21 88	0.50	0.00	0.0	15.600 1	-10.16
L7	125.5 - 125.25 (7)	TP22.4079x22,3611x0,36	0.25	0.00	0.0	25.736 0	-10.20
L.8	125.25 - 120.25 (8)	TP23.3434x22.4079x0.35 63	5.00	0.00	0.0	26.372 8	-12.41
L9	120.25 - 118.5 (9)	TP23.6708x23.3434x0.35 63	1.75	0.00	0.0	26.748 4	-12.66
L10	118.5 - 118.25 (10)	TP23.7176x23.6708x0.64 38	0.25	0.00	0.0	47.832 9	-12.72
L11	118.25 - 117.5 (11)	TP23.8579x23,7176x0.64 38	0.75	0.00	0.0	48.123 8	-12.88
L12	117.5 - 117.25 (12)	TP23.9047x23.8579x0.49 38	0.25	0.00	0.0	37.224 2	- 12.92
L13	117.25 - 112.25 (13)	TP24.8402x23.9047x0.48 13	5.00	0.00	0.0	37.751 1	-13.82
L14	112,25 - 107.25 (14)	TP25.7757x24.8402x0.46 88	5.00	0.00	0.0	38,201 7	-14.76
L15	107,25 - 102.25 (15)	TP26.7113x25.7757x0.45 63	5.00	0.00	0.0	38.576 0	-15.72
L16	102.25 - 97.5 (16)	TP27.6x26.7113x0.4563	4.75	0.00	0.0	38.942 8	-15.98
L17	97.5 - 95.916 (17)	TP27.4588x26.5233x0.55	5.00	0.00	0.0	47.655 5	-17.60
L18	95.916 - 92.5 (18)	TP28.098x27.4588x0,55	3.42	0.00	0.0	48.787 4	-18.40
L19	92.5 - 92.25 (19)	TP28.1447x28.098x0.55	0.25	0.00	0.0	48.870 3	-18.46
L20	92.25 - 87.25 (20)	TP29.0803x28.1447x0.53 75	5.00	0.00	0.0	49.400 4	-19.63
L21	87.25 - 87 (21)	TP29.1271x29.0803x0.62	0.25	0.00	0.0	57.360 4	-19.71
L22	87 - 82 (22)	TP30.0626x29.1271x0.61	5.00	0.00	0.0	58.082 9	-21.03
L23	82 - 77 (23)	TP30.9981x30.0626x0.6	5.00	0.00	0.0	58.729 2	-22.38
L24	77 - 72 (24)	TP31.9337x30.9981x0.58	5.00	0.00	0.0	59.299 1	-23.76
L25	72 - 67 (25)	TP32.8692x31.9337x0.57	5.00	0.00	0.0	59.792 7	-25.16
L26	67 - 63.25 (26)	TP33.5709x32.8692x0.57	3.75	0.00	0.0	61.091 8	-26.23
L27	63. 25 - 63 (27)	TP33.6176x33.5709x0.57	0.25	00,0	0.0	61.178	-26.31
L28	63 - 58 (28)	TP34.5532x33.6176x0.56	5.00	0.00	0.0	61.565 6	-27.75
L29	58 - 56.75 (29)	TP34.7871x34.5532x0.56 25	1.25	0.00	0.0	61.989 2	-28.11
L30	56.75 - 56.5 (30)	TP34.8338x34.7871x0.63	0.25	0.00	0.0	70.196 5	-28.21
L31	56.5 - 47.499 (31)	TP36.518x34.8338x0.637	9.00	0.00	0.0	71.925 3	-29.64
L32	47.499 - 46.999 (32)	TP35.9865x35.051x0.7	5.00	0.00	0.0	79.535 8	-32.63
L33	46.999 - 41.999 (33)	TP36.922x35.9865x0.687 5 TP37.8575v36.033v0.675	5.00	0.00	0.0	80.214 1	-34.42
L34	41.999 - 36.999 (34)	TP37.8575x36.922x0.675	5.00	0.00	0.0	80.816 2	-36.24
L35	36.999 - 34.25 (35)	TP38.3718x37.8575x0.67 5	2.75	0.00	0.0	81.934 1	-37.25
L36	34,25 - 34 (36)	TP38.4186x38.3718x0.67	0.25	0.00	0.0	82.035 8	-37.36
L37	34 - 29 (37)	TP39.3541x38.4186x0.66 25	5.00	0.00	0.0	82,538 9	-39.22

Section	Elevation	Size	L	L _u	KI/r	A tu²	P _u
No.	ft		ft	ft		in ²	<u> </u>
L38	29 - 26.75 (38)	TP39.7751x39.3541x0.66 25	2.25	0.00	0.0	83.436 9	-40.07
L39	26.75 - 26.5 (39)	TP39.8219x39.7751x0.66 25	0.25	0.00	0,0	83.536 7	-40.17
L40	26.5 - 21.5 (40)	TP40.7574x39.8219x0.65	5.00	0.00	0.0	83.944 7	-42.07
L41	21.5 - 16.75 (41)	TP41.6461x40.7574x0.65	4.75	0.00	0.0	85.804 8	-43.90
L42	16.75 - 16.5 (42)	TP41.6929x41.6461x0.76 25	0.25	0.00	0.0	100.49 40	-44.03
L43	16.5`- 14.25 (43)	TP42.1138x41.6929x0.76 25	2.25	0.00	0.0	101.52 80	-45.09
L44	14.25 - 14 (44)	TP42.1606x42.1138x0.72 5	0.25	0.00	0.0	96.731 4	-45.21
L45	14 - 9 (45)	TP43.0961x42.1606x0.71 25	5.00	0.00	0.0	97.238 6	-47.38
L46	9 - 4.25 (46)	TP43.9848x43.0961x0.71 25	4.75	0.00	0.0	99.277 5	-49.47
L47	4.25 - 4 (47)	TP44.0316x43.9848x0.6	0,25	0.00	0.0	83.909 9	-49.58
L48	4 - 0 (48)	TP44.78x44.0316x0.6	4.00	0.00	0.0	85.355 8	-51.19

Pole Bending Design Data

<u> </u>			
Section	Elevation	Size	M_{ux}
No.	ft	TD40 F0FF 4F F0 0 0 0 0 0	kip-ft
L1	151 - 146 (1)		19.68
L2	146 - 141 (2)	TP19.461x18.5255x0.218 8	46.55
L3	141 - 136 (3)	TP20.3965x19.461x0.218 8	97.62
L4	136 - 131 (4)	_	154.72
L5	131 - 12 6 (5)		225.05
L6	126 - 125.5 (6)	TP22.3611x22.2676x0.21	232.36
L7	125.5 -	TP22.4079x22.3611x0.36	236.03
L8	125.25 (7) 125.25 -	TP23.3434x22.4079x0.35	31 7.24
L9	120.25 (8) 120.25 -	63 TP23.6708x23.3434x0.35	347.65
L10	118.5 (9) 118.5 -	63 TP23.7176x23.6708x0.64	352.03
L11	118.25 (10) 118.25 -	38 TP23.8579x23.7176x0.64	365.22
L12	117.5 (11) 117.5 -	38 TP23.9047x23.8579x0 .4 9	369,64
	117.25 (12)	38	
L13	117.25 - 112.25 (13)	TP24.8402x23.9047x0.48 13	459.72
L14	112.25 - 107.25 (14)	TP25.7757x24.8402x0.46 88	552.80
L15	107.25 -	TP26.7113x25.7757x0.45	648.54
L16	102.25 (15) 102.25 - 97.5	63 TP27.6x26.7113x0.4563	674.52
L.17	(16) 97.5 - 95.916	TP27.4588x26.5233x0,55	773.89
L18	(17) 95.916 - 92.5 (18)	TP28.098x27.4588x0.55	843.48
L19	92.5 - 92.25 (19)	TP28.1447x28.098x0.55	848.63
L20	92.25 - 87.25 (20)	TP29.0803x28.1447x0.53	953.05
L21	87.25 - 87 (21)	75 TP29.1271x29.0803x0.62 5	958.34

Section	Elevation	Size	Mux
No.	ft	3126	kip-ft
L22	87 - 82 (22)	TP30.0626x29.1271x0.61	1065.79
	(/	25	
L23	82 - 77 (23)	TP30.9981x30.0626x0.6	1176.07
L24	77 - 72 (24)	TP31.9337x30.9981x0.58	1289.08
		75	
L25	72 - 67 (25)	TP32.8692x31.9337x0.57	1404.81
L26	67 - 63.25	5 TP33.5709x32.8692x0.57	1493.43
LZU	(26)	5	1400.40
L27	63.25 - 63	TP33.6176x33.5709x0.57	1499.40
	(27)	5	
L28	63 - 58 (28)	TP34.5532x33.6176x0.56	1620.15
		25	
L29	58 - 56.75	TP34.7871x34.5532x0.56	1650.77
	(29)	25	4050.00
L30	56.75 - 56.5	TP34.8338x34.7871x0.63 75	1656.92
L31	(30) 56.5 - 47.499	TP36.518x34.8338x0.637	1768.91
LUI	(31)	5	1700.51
L32	47,499 -	TP35.9865x35.051x0.7	1897.10
	46.999 (32)		
L33	46.999 -	TP36.922x35.9865x0.687	2028.17
	41.999 (33)	5	
L34	41.999 -	TP37.8575x36.922x0.675	2161.81
L35	36.999 (34)	TP38.3718x37.8575x0.67	2236.43
LJJ	36.999 - 34.25 (35)	1730,3710X37,0373XU.07	2230.43
L36	34.25 (33)	TP38.4186x38.3718x0.67	2243.25
200	(36)	5	
L37	34 - 29 (37)	TP39.3541x38.4186x0.66	2381.14
	` .	25	
L38	29 - 26.75	TP39.7751x39.3541x0.66	2444.04
	(38)	25	0.454.07
L39	26.75 - 26.5	TP39.8219x39.7751x0.66	2451.07
L40	(39) 26.5 - 21.5	25 TP40,7574x39.8219x0.65	2592.81
L40	(40)	11-40.7574855.621586.65	2392.01
· L41	21.5 - 16.75	TP41.6461x40.7574x0.65	2730.09
	(41)		
L42	16.75 - 16.5	TP41.6929x41.6461x0.76	2737.38
	(42)	25	
L43	16.5 - 14.25	TP42.1138x41.6929x0.76	2803.30
1.44	(43)	25	2040.66
L44	14.25 - 14 (44)	TP42.1606x42.1138x0.72 5	2810.66
L45	14 - 9 (45)	TP43,0961x42.1606x0.71	2959.05
0	0 (-0)	25	2000.00
L46	9 - 4.25 (46)	TP43.9848x43.0961x0.71	3102.31
	` '	25	
L47	4.25 - 4 (47)	TP44.0316x43.9848x0.6	3109.91
L48	4 - 0 (48)	TP44.78x44.0316x0.6	3232.29

Pole Shear Design Data

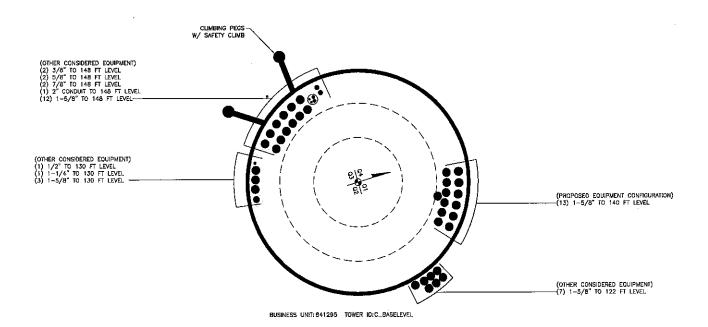
Section	Elevation	Size	Actual	Actual
No.	ft		V_u	T_{u}
			K	kip-ft
L1	151 - 1 46 (1)	TP18.5255x17.59x0.2188	5.20	1.28
L2	146 - 141 (2)	TP19.461x18.5255x0.218	5.56	1.28
		8		
L3	141 - 136 (3)	TP20.3965x19.461x0.218	11.20	0.07
		8		
L4	136 - 131 (4)	TP21.3321x20.3965x0.21	12.40	1.58
		88		
L5	131 - 126 (5)	TP22.2676x21.3321x0.21	14.62	1.58
		88		
L6	126 - 125.5	TP22,3611x22.2676x0.21	14.65	1.58
	(6)	88		

Continu	Flavorian	C/	0 mt cml	Antoni
Section No.	Elevation ft	Síze	Actual Vu	Actual Tu
			ĸ	kip-ft
L7	125.5 - 125.25 (7)	TP22.4079x22.3611x0.36 26	14.67	1.58
L8	125.25`- [′] 120.25 (8)	TP23.3434x22.4079x0.35 63	17.26	1.58
L9	120.25 - 118.5 (9)	TP23.6708x23.3434x0.35 63	17.51	1.59
L10	118.5 -	TP23.7176x23.6708x0.64	17.53	1.59
L11	118.25 (10) 118.25 -	38 TP23.8579x23.7176x0.64	17.65	1.59
L12	117.5 (11) 117.5 -	38 TP23.9047x23.8579x0.49	17.68	1.59
L13	117.25 (12) 117.25 -	38 TP24.8402x23.9047x0.48	18.36	1.62
L14	112.25 (13) 112.25 -	13 TP25.7757x24.8402x0.46	18.89	1.61
L15	107.25 (14) 107.25 -	88 TP26.7113x25.7757x0.45	19.42	1.61
L16	102,25 (15) 102,25 - 97,5	63 TP27.6x26.7113x0.4563	19.56	1.61
L17	(16) 97.5 - 95.916	TP27.4588x26.5233x0.55	20.19	1.61
L18	(17) 95.916 - 92.5	TP28.098x27.4588x0.55	20.58	1.61
L19	(18) 92.5 - 92.25	TP28.1447x28.098x0.55	20.60	1.61
L20	(19) 92.25 - 87.25	TP29.0803x28.1447x0.53	21.18	1.61
L21	(20) 87.25 - 87	75 TP29.1271x29.0803x0.62	21.20	1.61
L22	(21) 87 - 82 (22)	5 TP30.0626x29.1271x0.61	21.79	1.61
L23	82 - 77 (23)	25 TP30.9981x30.0626x0.6	22.34	1.61
L24	77 - 72 (24)	TP31.9337x30.9981x0.58	22.88	1.61
L25	72 - 67 (25)	TP32.8692x31.9337x0.57 5	23.43	1.61
L26	67 - 63.25 (26)	TP33.5709x32.8692x0.57 5	23.86	1.61
L27	63.25 - 63 (27)	TP33.6176x33.5709x0.57 5	23.88	1.61
L28	63 - 58 (28)	TP34.5532x33.6176x0.56 25	24.44	1.61
L29	58 - 56.75 (29)	TP34.7871x34.5532x0.56 25	24.58	1.61
L30	56.75 - 56.5 (30)	TP34.8338x34.7871x0.63 75	24.60	1.61
L31	56.5 - 47.499 (31)	TP36.518x34.8338x0.637 5	25.32	1.60
L32	47.499 - 46.999 (32)	TP35.9865x35.051x0.7	25.97	1.60
L33	46.999 - 41.999 (33)	TP36.922x35.9865x0.687 5	26.48	1.60
L34	41.999 - ´ 36.999 (34)	TP37.8575x36.922x0.675	27.01	1.60
L35	36.999 - [′] 34.25 (35)	TP38.3718x37.8575x0.67 5	27.32	1.60
L36	34.25 - 34 (36)	TP38.4186x38.3718x0.67 5	27.33	1.60
L37	34 - 29 (37)	TP39.3541x38.4186x0.66	27.86	1.60
L38	29 - 26.75 (38)	TP39,7751x39,3541x0,66 25	28.09	1.60
L39	26.75 - 26.5 (39)	TP39.8219x39.7751x0.66	28.11	1.60
L 4 0	26.5 - 21.5 (40)	TP40.7574x39.8219x0.65	28.62	1.60
L 4 1	21.5 - 16.75 (41)	TP41.6461x40.7574x0.65	29.18	2.93

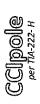
151 Ft Monopole Tower Structural Analysis Project Number 37519-2490.001.7805, Order 492710, Revision 0

Section No.	Elevation ft	Size	Actual V _u K	Actual Tu kip-ft
L42	16.75 - 16.5 (42)	TP41.6929x41.6461x0.76 25	29.19	2.93
L43	16.5 - 14.25 (43)	TP42.1138x41.6929x0.76 25	29,42	2.93
L44	14,25 - 14 (44)	TP42.1606x42.1138x0.72 5	29.44	2.93
L45	14 - 9 (45)	TP43.0961x42.1606x0.71 25	29.94	2.93
L46	9 - 4.2 5 (46)	TP43.9848x43.0961x0.71 25	30.41	2.93
L47 L48	4.25 - 4 (47) 4 - 0 (48)	TP44,0316x43.9848x0.6 TP44.78x44.0316x0.6	30.42 30.80	2.93 2.93
	, ,			

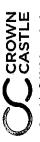
APPENDIX B BASE LEVEL DRAWING



APPENDIX C ADDITIONAL CALCULATIONS



Site BU: 841295 Work Order:



Copyright © 2019 Crown Castle Pole Material A572-65 A572-65 A572-65
 Wall Thickness (in)
 Bend Radius (in)

 0.2188
 Auto

 0.3125
 Auto
 Bottom Diameter (In) 27.6 36.518 44.78 Top Diameter (in) 17.59 26.52 35.05 Number of Sides Lap Splice Length (ft) 3.416 Section Length (ft) 53.5 53.417 51.999 Pole Height Above Base (ft) 1 151 2 100.916 3 51.999 Pole Geometry

Reinforcement Configuration

12											. 0%	
11			0	.		ु		0		, T		
10	. 0				0		, 0		868			
9			0							(a)		
80										٥	0	
7				្ល		. 0		, o				
9		a			0		0	,	. 0			
r,									- 1.	0.0		
4										0	ō	
ES.				್ರಾ		9		ે ં		o.	2.00	
2		٥		191	୍ତ		.0	92.11	0	, O		
1								_	-21,	0	_	
			-									
Number	1	2	2	3	3	3	3	3	3	8	3	
Model	MS-850 (1.1875")	MS-850 (1.1875")	MS-850 (1.1875")	MS-850 (1.1875")	MS-850 (1,1875")	MS-650 (1.1875")	("2781.1) 029-2M	MS-600 (1.1875")	("3781.1) 009-SW	FP 1.25 x 3.125_1	(1.1875")	
Туре	plate	plate	plate	plate	plate	płate	plate	plate	plate	plate	channel	
Top Effective Elevation (ft)	26.75	26.75	16.75	34.25	56.75	63.25	87.25	92.5	118.5	4.25	125.5	
Bottom Effective Elevation (ft)	14.25	4,25	4.25	26.75	34.25	56.75	63.25	87.25	92.5	0	117.5	
	1	2	'n	4	2	9	7	8	6	10	11	12

Reinforcement Details

		_	\neg										_
	Reinforcement	Material	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65	A572-65
		Bolt Hole Size (in)	1.1875	1.1875	1.1875	1.1875	1.1875	1.1875	1.1875	1.1875	1.1875	0.0000	1.1875
		Net Area (in")	9.063	9.063	9.063	9.063	9.063	6.563	6.563	4.750	4.750	3.906	2,545
		L" (in)	17.250	17.250	17.250	17,250	17.250	19.250	19,250	16.375	16.375	000'0	18.000
Тор	Termination	Length (in)	45.000	45.000	45.000	45.000	45.000	33.000	33.000	24.000	24.000	n/a	14.000
Bottom	Termination	Length (in)	45.000	45.000	45,000	45.000	45.000	33.000	33.000	24.000	24.000	e/u	14.000
	Pole Face to	Centroid (in)	0.625	0.625	0.625	0.625	0.625	0.625	0.625	0.5	0.5	1.5625	0.59
		Gross Area (In")	10.625	10.625	10.625	10,625	10.625	8.125	8.125	9	9	3.90625	2:92
	.;	H (in)	1.25	1.25	1.25	1.25	1.25	1.25	1.25	1	1	3,125	1.57
		B (in)	8.5	8.5	8.5	8.5	8.5	6.5	6.5	9	9	1.25	4.06
			.1	7	3	4	5	9	7	.00	6	10	11

Page 1

TNX Geometry Input

	rement (ft): 5		Lap Splice Length		l	Bottom Diameter	-	Tapered Pole	Weight
	Section Height (ft)	Section Length (ft)	(ft)	Number of Sides	Top Diameter (in)	(in)	Wall Thickness (in)	Grade	Multiplier
1	151 - 146	5	1.4	12	17.590	18,526	0.2188	A572-65	1.000
2	146 - 141	5		12	18.526	19.461	0.2188	A572-65	1.000
3	141 - 136	5		12	19.461	20.397	0.2188	A572-65	1.000
4	136 - 131	5		12	20.397	21.332	0.2188	A572-65	1.000
5	131 - 126	5		12	21.332	22,268	0.2188	A572-65	1.000
6	126 - 125.5	0.5		12	22.268	22.361	0.2188	A572-65	1.000
ᆉ	125.5 - 125.25	0.25		12	22.361	22.408	0.36255	AS72-65	0.948
8	125,25 - 120,25	5		12	22.408	23.343	0.3563	AS72-65	0.950
9	120,25 - 118.5	1.75		12	23.343	23.671	0.3563	AS72-65	0.946
10	118.5 - 118.25	0.25		12	23.671	23.718	0.6438	A572-65	0.906
11	118.25 - 117.5	0.75		12	23.718	23.858	0,6438	A572-65	0.903
12	117.5 - 117.25	0.25		12	23.858	23.905	0.4938	A572-65	0.933
13	117.25 - 112.25	5		12	23.905	24.840	0.4813	A572-65	0.937
14	112.25 - 107.25	5		12	24.840	25.776	0.4688	A572-65	0.943
15	107.25 - 102.25	5		12	25.776	26.711	0.4563	A572-65	0.951
16	107.25 - 102.25	4.75	3.416	12	26.711	27.600	0.4563	A572-65	0.947
17	100.916 - 95.916	5		12	26.523	27.459	0.55	A572-65	0.951
18	95.916 - 92.5	3.416		12	27.459	28.098	0.55	A572-65	0.943
19	92.5 - 92.25	0.25		12	28.098	28.145	0.55	A572-65	0.942
20	92.25 - 87.25	5		12	28.145	29.080	0.5375	A572-65	0.951
21	87.25 - 87	0.25	<u> </u>	12	29.080	29.127	0.625	A572-65	0.931
22	87 - 82	5		12	29.127	30.063	0.6125	A572-65	0.936
23	82 - 77	. 5		: 12	30.063	30,998	0.6	A572-65	0.941
24	77 - 72	5		12	30,998	31,934	0.5875	AS72-65	0.948
25	72 - 67	5	<u>-</u>	12	31,934	32.869	0.575	A572-65	0.956
26	67 - 63.25	3.75		12	32.869	33,571	0.575	A572-65	0.947
27	63,25 - 63	0.25		12	33.571	33.618	0.575	A572-65	0.947
28	63 - 58	5		12	33.618	34.553	0.5625	A572-65	0.956
29	58 - 56.75	1.25		12	34.553	34.787	0.5625	A572-65	0.953
30	56.75 - 56.5	0.25		12	34,787	34.834	0.6375	A572-65	0.950
31	56.5 - 51.999	9.001	4.5	12	34.834	36.518	0.6375	A572-65	0.939
32	51.999 - 46.999	5		12	35.051	35.987	0.7	A572-65	0.942
33	46.999 - 41.999	5		12	35.987	36.922	0,6875	A572-65	0.948
34	41.999 - 36.999	5		12	36.922	37.858	0.675	A572-65	0.955
35	36.999 - 34.25	2.749		. 12	37.858	38.372	0.675	A572-65	0.950
36	34.25 - 34	0.25		12	38.372	38.419	0.675	A572-65	0.949
37	34 - 29	5		12	38.419	39.354	0.6625	A572-65	0.957
38	29 - 26.75	2.25		12	39.354	39.775	0.6625	A572-65	0.953
39	26.75 - 26.5	0.25		12	39.775	39.822	0.6625	A572-65	. 0.952
40	26.5 - 21.5	5		12	39.822	40.757	0.65	A572-65	0.961
41	21.5 - 16.75	4,75		12	40,757	41.646	0.65	A572-65	0.953
42	16.75 - 16.5	0.25		12	41.646	41.693	0.7625	A572-65	1:026
43	16.5 - 14.25	2.25		12	41.693	42.114	0.7625	A572-65	1.020
44	14.25 - 14	0.25		12	42.114	42.161	0.725	A572-65	0,962
45	14 - 9	5		12	42.161	43.096	0.7125	A572-65	0.968
46	9 - 4.25	4.75		12	43.096	43.985	0.7125	A572-65	0.959
47	4.25 - 4	0.25		12	43.985	44.032	0.6	A572-65	1.001
48	4 - 0	4		12	44.032	44,780	0.6	A572-65	0.995

TNX Section Forces

lne	crement (ft):	5		NX Outpu	ıt
	A CHICAT (10).	1 3 1		M _{ux} (kip-	V _u
	Section He	ight (ft)	P _u (K)	ft)	(K)
1	151 -	146	3.02	19.68	5.20
2	146 -	141	3.33	46,56	5.56
3	141 -	136	6.93	97.62	11.20
4	136 -	131	7.89	154.77	12.34
5	131 -	126	10.11	225.05	14.62
6	126 -	125.5	10.16	232.36	14.65
7	125.5 -	125.25	10.20	236.03	14.67
8	125.25 -	120.25	12.41	317.24	17.26
9	120.25 -	118.5	12.66	347.65	17.51
10	118.5 -	118.25	12.72	352.03	17.53
11	118.25 -	117.5	12.88	365.22	17.65
12	117.5 -	117.25	12.92	369.64	17.68
13	117.25 -	112.25	13.82	459.72	18.36
14	112,25 -	107.25	14.76	552.80	18.89
15	107.25 -	102.25	15.72	648.54	19.42
16	102.25 -	100.916	15.98	674.52	19.56
17	100.916 -	95.916	17.60	773.89	20.19
18	95.916 -	92.5	18.40	843.49	20.58
19	92.5 -	92.25	18.46	848.63	20.60
20	92.25 -	87.25	19.63	953.05	21.18
21	87.25 -	87	19.71	958,34	21.20
22	87 -	82	21.03	1065.79	21.79
23	82 -	77	22.38	1176.07	22.34
24	77 -	72	23.76	1289.07	22.88
25	72 -	67	25.16	1404.81	23.43
26	67 -	63.25	26.23	1493.44	23.86
27	63.25 -	63	26.31	1499.40	23.88
28	63 -	58	27.75	1620.15	24.44
29	58 -	56.75	28.11	1650.77	24.58
30	56.75 -	56.5	28.21	1656. 9 1	24.60
31	56.5 -	51.999	29.64	1768.90	25.32
32	51.999 -	46.999	32.63	1897.10	25.97
33	46.999 -	41.999	34.42	2028.16	26.48
34	41.999 -	36.999	36.24	2161.81	27.01
35	36.999 -	34.25	37.25	2236.42	27.32
36	34.25 -	34	37.36	2243.25	27.33
37	34 -	29	39.22	2381.15	27.86
38	29 -	26.75	40.07	2444.04	28.09
39	26.75 -	26.5	40.17	2451.06	28.11
40	26.5 -	21.5	42.07	2592.81	28.62
41	21.5 -	16.75	43.90	2730.09	29.18
42	16.75 -	16.5	44.03	2737.39	29.19
43	16.5 -	14.25	45.09	2803.30	29.42
44	14.25 -	14	45.21	2810.66	29.44
45	14 -	9	47.38	2959.05	29.94
46	. 9 -	4.25	49.47	3102.30	30.41
47	4.25 -	4	49.58	3109.91	30.42
48	4 -	0	51.19	3232.30	30.80
I					

Analysis Results

Elevation (ft)	Component Type	Size	Critical Element	% Capacity	Pass / Fail
151 - 146	Pole	TP18.526x17.59x0.2188	Pole	5.6%	Pass
146 - 141	Pole	TP19.461x18.526x0.2188	Pole	11.9%	Pass
141 - 136	Pole	TP20.397x19.461x0.2188	Pole	23.1%	Pass
136 - 131	Pole	TP21.332x20.397x0.2188	Pole	33.7%	Pass
131 - 126	Pole	TP22.268x21.332x0.2188	Pole	45.6%	Pass
126 <i>-</i> 125.5	Pole	TP22.361x22.268x0.2188	Pole	46.7%	Pass
125.5 - 125.25	Pole + Reinf.	TP22.408x22.361x0.3626	Reinf. 11 Tension Rupture	40.8%	Pass
125.25 - 120.25	Pole + Reinf.	TP23.343x22.408x0.3563	Reinf. 11 Tension Rupture	51.2%	Pass
120.25 - 118.5	Pole + Reinf.	TP23.671x23.343x0.3563	Reinf. 11 Tension Rupture	54.8%	Pass
118.5 - 118.25	Pole + Reinf.	TP23.718x23.671x0.6438	Reinf. 9 Bolt-Shaft Bearing	33.5%	Pass
118.25 - 117.5	Pole + Reinf.	TP23.858x23.718x0.6438	Reinf. 9 Tension Rupture	33.7%	Pass
117.5 - 117.25	Pole + Reinf.	TP23.905x23.858x0.4938	Reinf. 9 Tension Rupture	42.9%	Pass
117.25 - 112.25	Pole + Reinf.	TP24.84x23.905x0.4813	Reinf. 9 Tension Rupture	50.4%	Pass
112.25 - 107.25	Pole + Reinf.	TP25.776x24.84x0.4688	Reinf. 9 Tension Rupture	57.4%	Pass
107.25 - 102.25	Pole + Reinf.	TP26.711x25.776x0.4563	Reinf. 9 Tension Rupture	63.8%	Pass
102.25 - 100.92	Pole + Reinf.	TP27.6x26.711x0.4563	Reinf. 9 Tension Rupture	65.4%	Pass
100.92 - 95.92	Pole + Reinf.	TP27.459x26.523x0.55	Reinf. 9 Tension Rupture	60.5%	Pass
95.92 - 92.5	Pole + Reinf.	TP28.098x27.459x0.55	Reinf. 9 Tension Rupture	63.6%	Pass
92.5 - 92.25	Pole + Reinf.	TP28.145x28.098x0.55	Reinf. 8 Tension Rupture	63.8%	Pass
92.25 - 87.25	Pole + Reinf.	TP29.08x28.145x0.5375	Reinf. 8 Tension Rupture	67.9%	Pass
87.25 - 87	Pole + Reinf.	TP29.127x29.08x0.625	Reinf. 7 Tension Rupture	58.4%	Pass
87 - 82	Pole + Reinf.	TP30.063x29.127x0.6125		61.9%	Pass
Salvationes to take more annut more in as id one to define			Reinf. 7 Tension Rupture	65.2%	Pass
82 - 77	Pole + Reinf.	TP30.998x30.063x0.6	Reinf. 7 Tension Rupture	and the second s	
77 - 72	Pole + Reinf.	TP31.934x30.998x0.5875	Reinf. 7 Tension Rupture	68.2%	Pass
72 - 67	Pole + Reinf.	TP32.869x31.934x0.575	Reinf. 7 Tension Rupture	71.1%	Pass
67 - 63.25	Pole + Reinf.	TP33.571x32.869x0.575	Reinf. 7 Tension Rupture	73.1%	Pass
63.25 - 63	Pole + Reinf.	TP33.618x33.571x0.575	Reinf. 6 Tension Rupture	73.3%	Pass
63 - 58	Pole + Reinf.	TP34.553x33.618x0.5625	Reinf. 6 Tension Rupture	75.8%	Pass
58 - 56.75	Pole + Reinf.	TP34.787x34.553x0.5625	Reinf. 6 Tension Rupture	76.4%	Pass
56.75 - 56.5	Pole + Reinf.	TP34.834x34.787x0.6375	Reinf. 5 Bolt Shear	66.4%	Pass
56.5 - 52	Pole + Reinf.	TP36.518x34.834x0.6375	Reinf. 5 Compression	66.1%	Pass
52 - 47	Pole + Reinf.	TP35.987x35.051x0.7	Reinf. 5 Compression	63.6%	Pass
47 - 42	Pole + Reinf.	TP36.922x35.987x0.6875	Reinf. 5 Compression	65.4%	Pass
42 - 37	Pole + Reinf.	TP37.858x36.922x0.675	Reinf. 5 Compression	67.0%	Pass
37 - 34.25	Pole + Reinf.	TP38.372x37.858x0.675	Reinf. 5 Bolt Shear	70.3%	Pass
34.25 - 34	Pole + Reinf.	TP38.419x38.372x0.675	Reinf. 4 Bolt Shear	70.4%	Pass
34 - 29	Pole + Reinf.	TP39.354x38.419x0.6625	Reinf. 4 Compression	69.4%	Pass
29 - 26.75	Pole + Reinf.	TP39.775x39.354x0.6625	Reinf. 4 Bolt Shear	72.6%	Pass
26.75 - 26.5	Pole + Reinf.	TP39.822x39.775x0.6625	Reinf. 1 Bolt Shear	72.7%	Pass
26.5 - 21.5	Pole + Reinf.	TP40.757x39.822x0.65	Reinf. 1 Compression	71.5%	Pass
21.5 - 16.75	Pole + Reinf.	TP41.646x40.757x0.65	Reinf. 1 Compression	72.8%	Pass
16.75 - 16 <i>.</i> 5	Pole + Reinf.	TP41.693x41.646x0.7625	Reinf. 2 Compression	66.9%	Pass
16.5 - 14.25	Pole + Reinf.	TP42.114x41.693x0.7625	Reinf. 2 Compression	67.5%	Pass
14.25 - 14	Pole + Reinf.	TP42.161x42.114x0.725	Reinf. 2 Compression	67.9%	Pass
14 - 9	Pole + Reinf.	TP43.096x42.161x0.7125	Reinf. 2 Compression	69.1%	Pass
9 - 4.25	Pole + Reinf.	TP43.985x43.096x0.7125	Reinf. 2 Bolt Shear	72.7%	Pass
4.25 - 4	Pole + Reinf.	TP44.032x43.985x0.6	Reinf. 10 Connection	74.0%	Pass
4 - 0	Pole + Reinf. I P44.032x43.985x0.6 Pole + Reinf. TP44.78x44.032x0.6		Reinf. 10 Connection	74.8%	Pass
	TOTAL TOTAL	111 ONT 1.002AU.0	reservations are a secured to the secure of	Summary	
		unter de la comparte del la comparte del la comparte del la comparte de la comparte de la comparte del la comparte de la comparte del la comparte del la comparte del la comparte del la comparte del la comparte del la comparte del la comparte del la comparte del	Pole	64.6%	Pass
TO SERVICE STATE OF THE SERVIC	TOTAL STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET, STREET,		Reinforcement	76.4%	Pass
			Overall	76.4%	Pass

Additional Calculations

Section	Mom	ent of Inertia	a (In ⁴)		Area (in²)						9	6 Capaci	ty*					
Elevation (ft)	Pole	Reinf.	Total	Pale	Reinf.	Total	Pole	R1	R2	R3	R4	R5	R6	R7	RB	RÝ	R10	R11
151 - 146	. 552	n/a	552	12.88	n/a	12.88	5.6%											
146 - 141	642	n/a	642	13.54	n/a	13.54	11.9%											
141 - 135	740	n/a	740	14.20	n/a	14.20	23.1%											
136 - 131	848	n/a	848	14.85	n/a	14.85	33.7%											
131 - 125	965	n/a	965	15.51	n/a	15.51	45.6%					1						
126 - 125.5	978	n/a	978	15.58	n/a	15.58	46.7%											
125.5 - 125.25	984	612	1596	15.61	8.76	24.37	28.3%									- 1		40.89
125.25 - 120.25	1114	661	1775	16.27	8.76	25.03	36.1%											51.29
120.25 - 118.5	1161	679	1840	16.50	8,76	25.26	38.9%									1000		54.89
118.5 - 118.25	1168	2084	3252	16.53	26.76	43.29	22.4%									33.5%		31.59
118.25 - 117.5	1190	2107	3297	16.63	26.75	43.39	23.1%					•				33.7%		32.45
117.5 - 117.25	1197	1423	2620	16.66	18.00	34.66	29.5%									42.9%		
117.25 - 112.25	1344	1530	2874 .	17.32	18.00	35.32	35.2%									50.4%		
112.25 - 107.25	1503	1641	3144	17.98	18.00	35.98	40.8%									57.4%		
107.25 - 102.25	1674	1756	3430	18.64	18.00	36.64	46.2%								ì	63.8%		
102.25 - 100.92	1722	1787	3509	18.81	18.00	36.81	47.7%									85.4%		
100.92 - 95.92	2573	1850	4423	27.28	18.00	45.28	38.5%									60.5%		
95.92 - 92.5	2759	1933	4692	27.92	18.00	45.92	40.8%									63.6%		
92.5 - 92.25	2773	1939	4712	27.97	18.00	45.97	40.9%								63.8%			
92.25 - 87.25	3062	2064	5126	28.91	18.00	46.91	44.1%								67,9%			
87.25 • 87	3077	2856	5933	28.95	24.38	53.33	38.4%	1.1						58.4%				
87 - 82	3385	3032	6418	29.89	24.38	54.27	41.2%							61.9%				
82 - 77	3716	3213	6929	30.83	24.38	55.21	43.9%							65.2%				
77 - 72	4066	3400	7466	31.77	24.38	56.15	48.6%							68.2%				
72 - 67	4438	3591	8030	32.71	24.38	57.09	49.1%							71.1%				
67 - 63.25	4731	3739	8470	33.42	24.38	57.79	51.0%							73.1%				
63.25 - 63	4751	3749	8500	33.47	24.38	57.84	51.1%	·					73.3%	i				
63 - 58	5163	3950	9113	34.41	24.38	58.78	53,6%						75.8%					
58 - 56.75	5270	4001	9271	34.54	24.38	59.02	54.2%						76.4%					
56.75 - 56.5	5291	5286	10577	34,59	31.88	66.56	47.B%			-		66.4%		i				
56.5 - 52	5688	5531	11219	35.53	31.88	67.41	49.8%	7				66.1%						
52 - 47	6970	5623	12593	42.94	31.88	74.81	44.7%					63.6%						
47 - 42	7534	5904	13438	44.07	31.88	75.94	46,4%	-				65.4%						
42 - 37	8127	6192	14319	45.20	31.88	77.07	48.1%					67.0%						
37 - 34.25	8456	6353	14820	45.82	31.88	77.69	49.0%					70.3%						
34.25 - 34	8498	535B	14866	45.87	31.88	77.75	49.0%				70.4%							
34 - 29	9140	6667	15807	47.00	31.88	78.87	50.6%	_			69,4%							
29 - 26.75	9440	6804	16244	47.51	31.88	79.38	51.3%				72.6%							
26.75 - 26.5	9473	6819	16292	47.56	31.88	79.44	51.4%	72.7%	72.7%									
26.5 - 21.5	10163	7129	17292	48.69	31.88	80.57	53.0%	71.5%	71.5%									
21.5 - 16.75	10849	7430	18279	49.76	31.88	81.64	54.4%	72.8%	72.8%									
16.75 - 16.5	11070	10638	21707	49,82	53.13	102.94	50.2%	45.5%	66.9%	51.6%								
16.5 - 14.25	11409	10846	22255	50.33	53.13	103.45	50.8%	47.6%	67.5%	50.3%				.				
14.25 - 14	11315	9986	21301	50.38	42.50	92,88	52.3%	.,,,=10	67.9%	60.8%								
14.25 - 14	12090	10417	22507	51.51	42.50	94.01	53.8%		69.1%	61.9%					-			
9-4.25	12859	10835	23694	52.58	42.50	95.08	55.2%	-	72.7%	65.2%		_						
4.25 - 4	12848	7526	20374	52.64	31.25	83.89	63.3%										74.0%	<u> </u>
4.25 - 4	13520	7767	21287	53.54	31.25	84.79	64.6%	_						\vdash			74.8%	†

Note: Section capacity checked in 5 degree Increments.
Rating per TIA-222-H Section 15.5.

Monopole Base Plate Connection

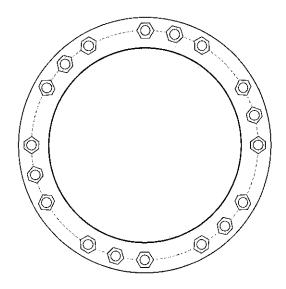


Site Info	
BU#	841295
Site Name	Bethany
Order#	

Analysis Considerations	
TIA-222 Revision	Н
Grout Considered:	No
l _{ar} (in)	0

Applied Loads	
Moment (kip-ft)	3232.30
Axial Force (kips)	51.19
Shear Force (kips)	30.80

^{*}TIA-222-H Section 15.5 Applied



Connection Properties	Α	nalysis Results	
Anchor Rod Data	Anchor Rod Summary	(u	nits of kips, kip-in)
GROUP 1: (12) 2-1/4" ø bolts (A615-75 N; Fy=75 ksi, Fu=100 ksi) on 52.75" BC	GROUP 1:		
GROUP 2: (6) 2-1/4" ø bolts (Williams N; Fy=120 ksi, Fu=125 ksi) on 52.75" BC	Pu_c = 154.73	φPn_c = 243.75	Stress Rating
	Vu = 2.57	φVn = 73.13	60.6%
Base Plate Data	Mu = n/a	фМn = n/a	Pass
58.75" OD x 3" Plate (A572-50; Fy=50 ksi, Fu=65 ksi)			
	GROUP 2:		
Stiffener Data	Pu_c = 188.89	$\Phi Pn_c = 489.6$	Stress Rating
N/A	Vu = 0	φVn = 146.88	36.7%
	Mư = n/a	φMn = n/a	Pass
Pole Data			
44.78" x 0.375" 12-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)	Base Plate Summary		
	Max Stress (ksi):	26.72	(Flexural)
	Allowable Stress (ksi):	45	
	Stress Rating:	56.6%	Pass

CCIplate - version 3.6.0 Analysis Date: 6/7/2019

Pier and Pad Foundation

BU # : 841295
Site Name: Bethany
App. Number:



TIA-222 Revision:	H
Tower Type:	Мопороје

Top & Bot. Pad Rein. Different?:	T
Block Foundation?:	

Superstructure Analysis	Reaction	าร
Compression, P _{comp} :	51.19	kips
Base Shear, Vu_comp:	30.8	kips
Moment, M _u :	3232.3	ft-kips
Tower Height, H:	150	ft
BP Dist. Above Fdn, bp _{dist} :	3.75	in

Foundation Analysis Checks						
	Capacity	Demand	Rating*	Check		
Lateral (Sliding) (kips)	482.94	30.80	6.1%	Pass		
Bearing Pressure (ksf)	22.50	1.84	7.8%	Pass		
Overturning (kip*ft)	10947.31	3534.53	32.3%	Pass		
Pier Flexure (Comp.) (kip*ft)	6585.19	3263.10	47.2%	Pass		
Pier Compression (kip)	22913.28	57.67	0.2%	Pass		
Pad Flexure (kip*ft)	7614.39	1351.62	16.9%	Pass		
Pad Shear - 1-way (kips)	3225.07	81.25	2.4%	Pass		
Pad Shear - 2-way (Comp) (ksi)	0.190	0.005	2.4%	Pass		
Flexural 2-way (Comp) (kip*ft)	15228.77	1957.86	12.2%	Pass		

Pier Propertie	S	
Pier Shape:	Square	
Pier Diameter, dpier:	6	ft
Ext. Above Grade, E:	0.4	ft
Pier Rebar Size, Sc :	10	
Pier Rebar Quantity, mc :	40	
Pier Tie/Spiral Size, St:	4	
Pier Tie/Spiral Quantity, mt:		
Pier Reinforcement Type:	Tie	
Pier Clear Cover, cc _{pler} :	2.5	in

*Rating per TIA-222-H Section 15.5

Pad Properties					
Depth, D :	9.1	ft			
Pad Width, W :	29	ft			
Pad Thickness, T:	8.5	ft			
Pad Rebar Size (Bottom), Sp:	7				
Pad Rebar Quantity (Bottom), mp:	29	<u> </u>			
Pad Clear Cover, cc _{nad} :	3	in			

Soil Rating*:	32.3%
Structural Rating*:	47.2%

Material Properties			
Rebar Grade, Fy :	60	ksi	
Concrete Compressive Strength, F'c:	4	ksi	
Dry Concrete Density, δ c :	150	pcf	

Soil Properties		
Total Soil Unit Weight, γ :	110	pcf
Ultimate Gross Bearing, Qult:	30.000	ksf
Cohesion, Cu:	0.000	ksf
Friction Angle, $arphi$:	30	degrees
SPT Blow Count, Nolows:	69	

Base Friction, μ :

Neglected Depth, N:

Foundation Bearing on Rock?

Groundwater Depth, gw:

0.5

3.30

No

<--Toggle between Gross and Net



ASCE 7 Hazards Report

Address:

No Address at This Location

Standard:

ASCE/SEI 7-10

Elevation: 741.6 ft (NAVD 88)

Latitude:

41.442758

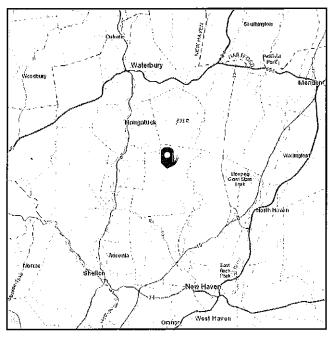
Risk Category: □

Soil Class:

D - Stiff Soil

Longitude: -72.992461





Wind

Results:

Wind Speed:

122 Vmph

10-year MRI

76 Vmph

25-year MRI

86 Vmph

50-year MRI

93 Vmph

100-year MRI

99 Vmph

Data Source:

ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of

March 12, 2014

Date Accessed:

Wed Jun 05 2019

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.



[ce

Results:

Ice Thickness:

0.75 in.

Concurrent Temperature:

15 F

Gust Speed:

50 mph

Data Source:

Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8

Date Accessed:

Wed Jun 05 2019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 50-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

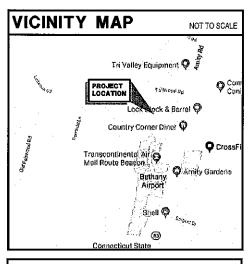
The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

Veriza BETHANY NO

CROWN CASTLE B 719 AMITY R BETHANY, CT



DO NOT SCALE DRAWINGS

CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE LESSEE/LICENSEE REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

CONSULTANT TEAM

APPLICANT:

VERIZON WIRELESS 20 ALEXANDER DRIVE WALLINGFORD, CT 06492 CONTACT: JAMES O'DONNELL

APPLICANT'S CONTACT:

JAMES O'DONNELL (413) 575-2626

ARCHITECT:

JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE

5TH FLOOR

BOSTON, MA 02116

STRUCTURAL ENGINEER: JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE

5TH FLOOR

BOSTON, MA 02116

ELECTRICAL ENGINEER:

JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE

5TH FLOOR BOSTON, MA 02116

PROJECT SUMMARY

VERIZON SITE NAME:

BETHANY NORTH C

CROWN CASTLE SITE NAME: BETHANY

TOWER OWNER:

CROWN CASTLE LL 67 SHARP STREET HINGHAM, MA 02043

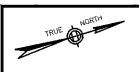
COORDINATES:

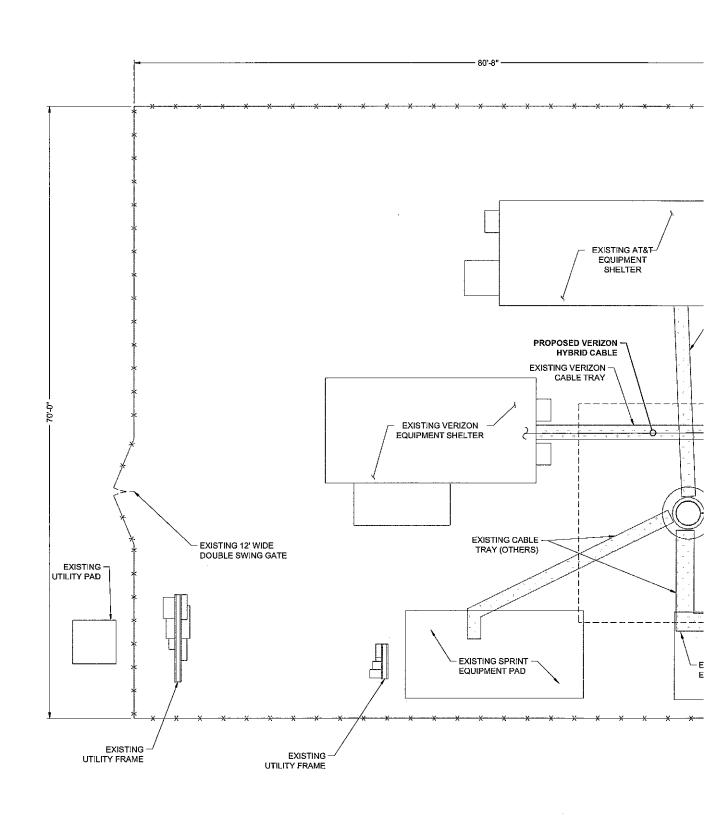
N 41° 26' 33.93" W 72° 59' 32,86"

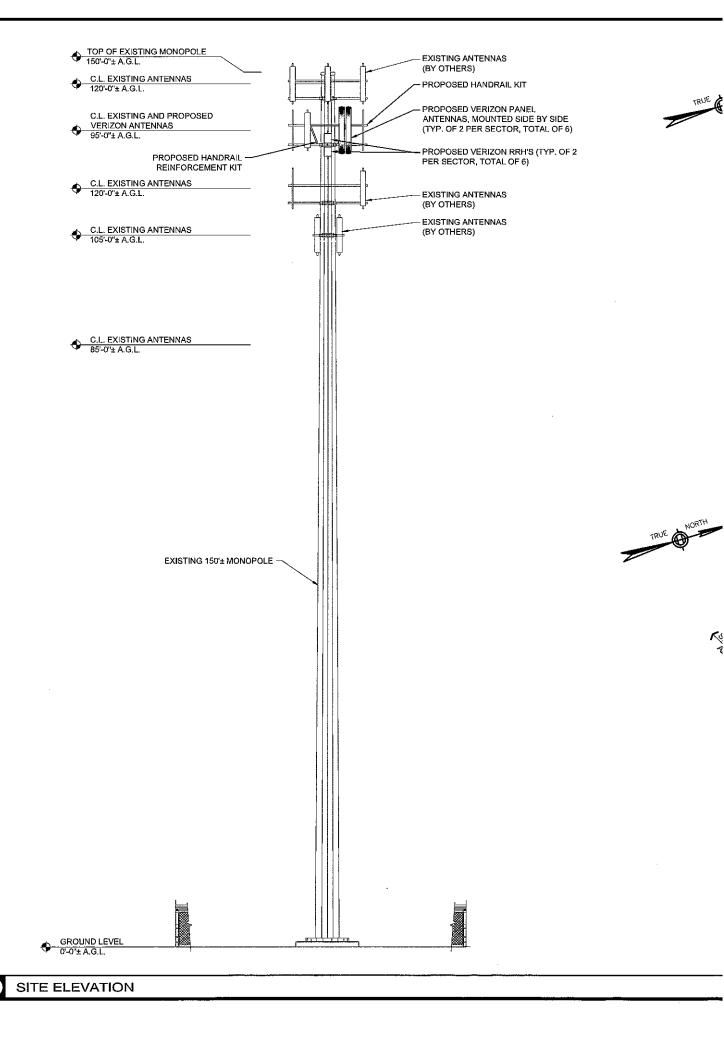
APPLICANT:

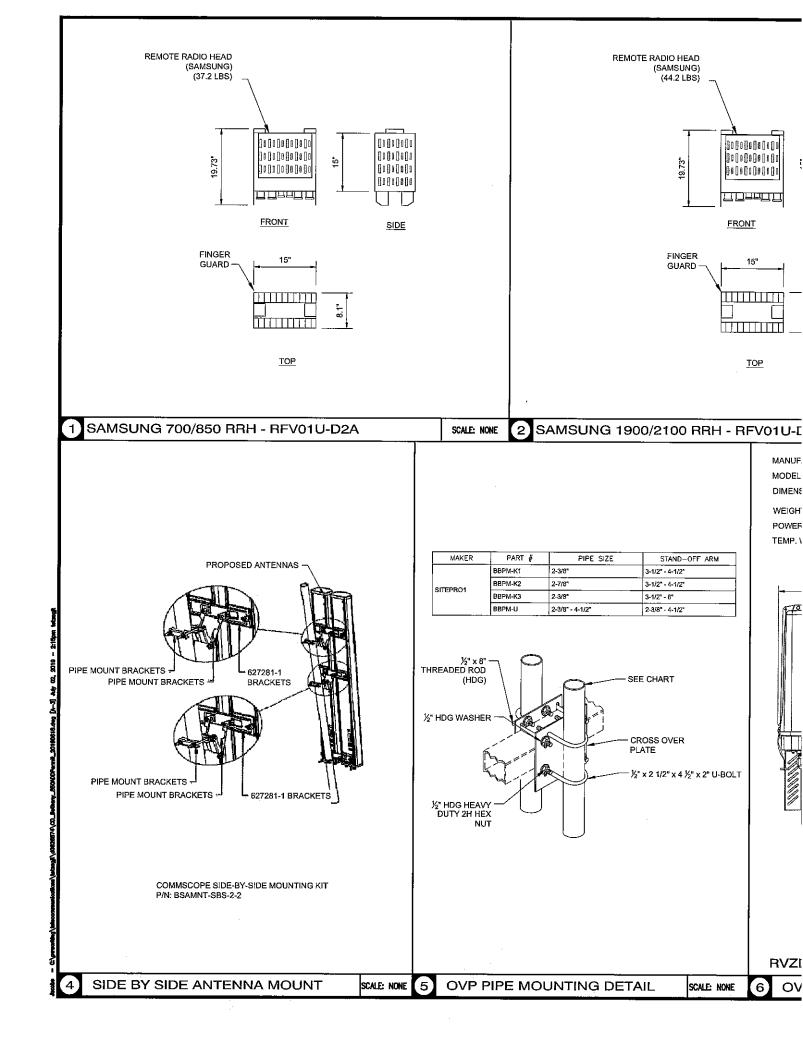
VERIZON WIRELESS 20 ALEXANDER DRI

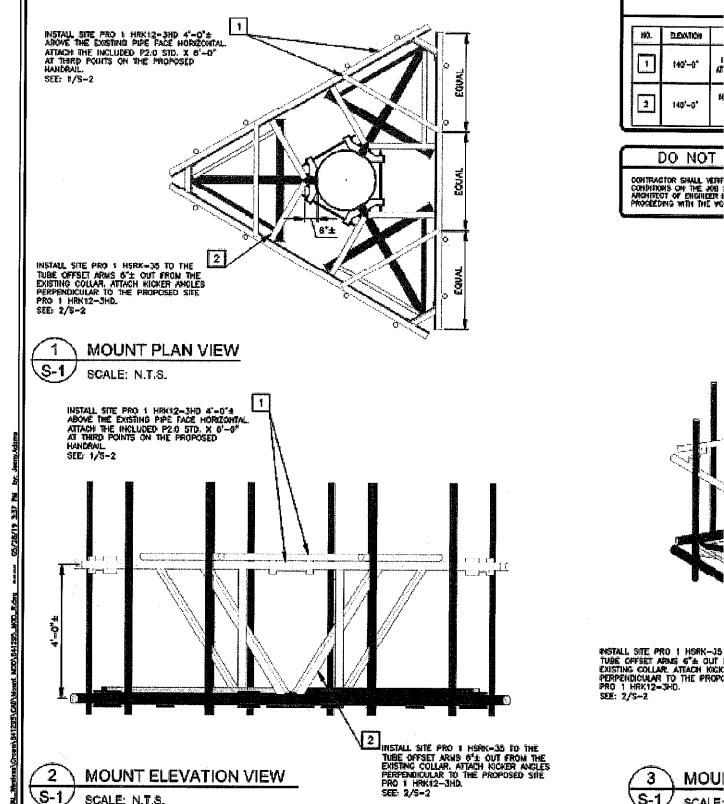
WALLINGFORD, CT











MOUI SCALE:

Æ

Kimley » Horn

421 FAYETTEVILLE STREET, SUITE 600 RALEIGH, NC 27601 PHONE: 919-677-2000 WWW.KIMLEY-HORN.COM

MOUNT MODIF

BETHANY

CROWN CASTLE BU#: 8
VERIZON SITE#: 1043

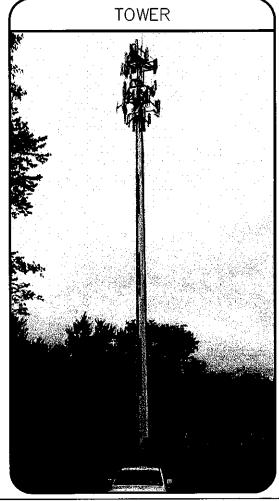
STRUCTURE INFORM

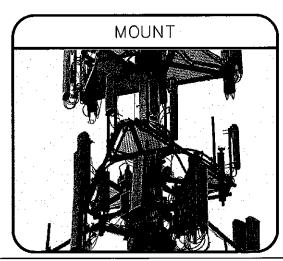
150' MONOPOLE TOW LOW PROFILE PLATFO

SITE ADDRESS

719 AMITY ROAD BETHANY, CT 0652 NEW HAVEN COUNT LATITUDE: N 41° 26' 33

LONGITUDE: W 72° 59' 3





OF ALL TRADES AND SHALL CHECK ALL DIMENSIONS. ALL DISCREPANCIES SHALL BE CALLED TO THE ATTENTION OF THE PROJECT MANAGER AND/OR ENGINEER AND BE RESOLVED BEFORE PROCEEDING WITH WORK WHERE THERE IS A CONFLICT BETWEEN DRAWING AND SPECIFICATIONS.

1.03 ALL INFORMATION SHOWN ON THE DRAWINGS RELATIVE TO EXISTING CONDITIONS IS GIVEN AS THE BEST PRESENT KNOWLEDGE, BUT WITHOUT GUARANTEE OF ACCURACY. WHERE ACTUAL CONDITIONS CONFLICT WITH THE DRAWINGS, THEY SHALL BE REPORTED TO THE PROJECT MANAGER AND/OR ENGINEER OF RECORD SO THAT PROPER REVISIONS MAY BE MADE. MODIFICATION OF DETAILS OR CONSTRUCTION SHALL NOT BE MADE WITHOUT WRITTEN APPROVAL OF THE PROJECT MANAGER AND/OR ENGINEER OF RECORD.

1.04 CONTRACTOR SHALL REVIEW AND BE FAMILIAR WITH SITE CONDITIONS AS

SHOWN ON THE ATTACHED SITE PLAN AND/OR SURVEY DRAWINGS.

1.05 CONTRACTOR TO PROVIDE DUMPSTER AND PORTABLE TOILET FACILITY

DURING CONSTRUCTION.

1.06 CONSTRUCTION WASTE MAY NEITHER BE BURNED NOR BURIED AND MUST BE TAKEN TO AN APPROVED LANDFILL.
 1.07 SECURITY TO THE SITE SHALL BE MAINTAINED AT ALL TIMES.

2.00 STRUCTURAL STEEL NOTES

2.01 STRUCTURAL STEEL SHALL COMPLY WITH THE FOLLOWING SPECIFICATIONS

A. STRUCTURAL STEEL SHAPES, PLATES AND BARS. (EXPECT W-SHAPES) - ASTM A36, Fy=36 KSI.
B. PIPE - ASTM A53, GRADE B, Fy=35 KSI.
C. HSS-SHAPES - ATSM A500, GRADE B,

Fy = 42 KSI (ROUND)

Fy = 46 KSI (RECTANGLE)

D. ANCHOR RODS - ASTM F1554, GRADE 55

E. ALL THREAD RODS - ASTM F1554, GRADE 105

F. STRUCTURAL BOLTS 1/2" AND LARGER - ASTM A325

G. STRUCTURAL BOLTS SMALLER THAN 2000

DIMENSIONS: ASME B18.2.1

MATERIAL SAE J429 GRADE 5
THREADING: ASME B1.1, UNC, CLASS 2A
FINISH: HOT—DIP GALVANIZED OR ZINC—PLATED

H. NUTS FOR BOLTS/ALL-THREAD - ASTM A563 (THREADING TO

USING ASTM A780 PROCEDURES WITH A ZINC RICH PAINT (SUCH AS ZRC GALVILITE) FOR GALVANIZING DAMAGED BY HANDLING, TRANSPORTING, CUTTING, WELDING, OR BOLTING. DO NOT HEAT SURFACES TO WHICH REPAIR PAINT HAS BEEN APPLIED. CALL OUT HOLES REQUIRED FOR HOT-DIP GALVANIZING ON SHOP DRAWINGS.

2.04 WELDING SHALL BE IN ACCORDANCE WITH AWS D1.1 "STRUCTURAL WELDING CODE - STEEL". WELD ELECTRODES SHALL BE E80XX. UNLESS OTHERWISE NOTED PROVIDE CONTINUOUS FILLET WELDS WITH MINIMUM SIZE OF $\frac{2}{3}$ 6° OR OF A SIZE EQUAL TO THE THICKNESS OF THE THINNER WELD LEG SIZE SHALL BE ADJUSTED AS REQUIRED TO MAINTAIN THE EFFECTIVE THROAT OF

A 3/6" FILLET WELD IN A 90' JOINT. ALL WELD SIZES SHOWN IN INCHES.

2.05 PRIOR TO WELDING, THE CONTRACTOR SHALL SUBMIT CERTIFICATION FOR EACH WELDER STATING THE TYPE OF WELDING AND POSITIONS QUALIFIED FOR, THE CODE AND PROCEDURE QUALIFIED UNDER, STATE QUALIFIED, AND THE FIRM AND INDIVIDUAL CERTIFYING THE QUALIFICATION TESTS. THIS INFORMATION SHALL BE SUBMIT TO THE MODIFICATION INSPECTOR (SEE SHEET N-3) AS WELL AS ANY THIRD-PARTY CERTIFIED WELD INSPECTOR

2.06 MEMBERS SHALL BE SHOP-FABRICATED AND WELDED TO THE EXTENT PRACTICABLE IN ORDER TO REDUCE FIELD INSTALLATION COSTS.

3.00 MODIFICATION NOTES
3.01 THESE MODIFICATIONS HAVE BEEN DESIGNED IN ACCORDANCE WITH GOVERNING PROVISIONS OF TIA/EIA-222, ASCE 7, AWS, ACI, AND AMATERIALS AND SERVICES PROVIDED BY THE CONTRACTOR SHALL (TO THE ABOVE MENTIONED CODES AND CONTRACT SPECIFICATIONS. 3.02 ALL MATERIALS UTILIZED FOR THIS PROJECT MUST BE NEW AND FROM THE ABOVE MENTIONED CODES AND CONTRACT SPECIFICATIONS.

ANY DEFECTS

3.03 ALL PRODUCT OR MATERIAL SUBSTITUTIONS PROPOSED BY THE CONTRACTOR SHALL BE APPROVED IN WRITING BY THE ENGINEER C RECORD. CONTRACTOR SHALL PROVIDE DOCUMENTATION TO ENGINE SUITABLE TO DETERMINE IF THE SUBSTITUTE IS ACCEPTABLE FOR L
MEETS THE ORIGINAL DESIGN CRITERIA. DIFFERENCES FROM THE OR
DESIGN, INCLUDING; MAINTENANCE, REPAIR, AND REPLACEMENT, SH
NOTED. ESTIMATES OF COSTS/CREDITS ASSOCIATED WITH THE SUBS (INCLUDING RE-DESIGN COSTS AND COSTS TO SUB-CONTRACTORS)
BE PROVIDED TO THE ENGINEER. CONTRACTOR SHALL PROVIDE ADD
DOCUMENTATION AND/OR SPECIFICATION TO THE ENGINEER AS REQ

3.04 PROVIDE STRUCTURAL STEEL SHOP DRAWINGS(S) TO THE ENGINEER RECORD FOR APPROVAL PRIOR TO FABRICATION.
3.05 UNLESS NOTED OTHERWISE, ALL NEW MEMBERS AND REINFORCING SMAINTAIN THE EXISTING MEMBER WORK AND NOT INTRODUCE

ECCENTRICITIES INTO THE STRUCTURE.

3.06 ANY CONTRACTOR—CAUSED DAMAGE TO PROPERTY OF THE LAND C PROPERTY OF THE CUSTOMER, SITE FENCING OR GATES, ANY AND UTILITY AND/OR SERVICE LINES, SHOWN OR NOT SHOWN ON THE P SHALL BE REPAIRED OR REPLACED AT THE SOLE COST OF THE CONTRACTOR AND SHALL BE ADDRESSED BY THE CONTRACTOR WIT COMPANIES THAT OWN THE DAMAGED ITEMS.

4.00 CONTRACTOR NOTES

PRIOR TO BEGINNING CONSTRUCTION, ALL CONTRACTORS AND SUBCONTRACTORS MUST ACKNOWLEDGE IN WRITING TO STRUCTURE O THAT THEY HAVE OBTAINED, UNDERSTAND, AND WILL FOLLOW STRUC OWNER STANDARDS OF PRACTICE, CONSTRUCTION GUIDELINES, ALL PRODUCT LIMITATIONS AND INSTALLATION PROCEDURES USED ON SITE, AND PROPOSED MODIFICA DESCRIBED RECEIPT OF ACKNOWLEDGEMENT MUST OCCUR PRIOR TO BEGINNING CONSTRUCTION OF CLIMBING. IT IS THE RESPONSIBILITY OF GENERAL CONTRACTOR TO PROVIDE THE DOCUMENTATION FOR STRUC OWNER ON COMPANY LETTERHEAD AND THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO OBTAIN THIS DOCUMENTATION FROM ANY SUBCONTRACTORS (ON SUBCONTRACTOR LETTERHEAD) AND DELIVER THE STRUCTURE OWNER.

4.02 IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT AR REPRESENTED ON THESE DRAWINGS, OR ANY CONDITIONS THAT AN REPRESENTED ON THESE DRAWINGS, OR ANY CONDITIONS THAT WOUL INTERFERE WITH THE INSTALLATION OF THE MODIFICATIONS, THE ENGINEERED SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE SIGNI OF THE DEVIATION.

OF THE DEVIATION.

4.03 THE CONTRACTOR SHALL SOLICIT AND HIRE THE SERVICES OF A QUAMODIFICATIONS INSPECTOR PRIOR TO BEGINNING CONSTRUCTION, THE MODIFICATION INSPECTOR MAY BE AN EMPLOYEE OF THE CONTRACTOR HOWEVER, THE INSPECTOR'S ONLY DUTIES SHALL BE INSPECTION, TES AND REPORT CREATION AS REQUIRED ON THE "MODIFICATION INSPECTOR'S SHEET, IT IS ALSO ACCEPTABLE FOR THE CONTRACTOR TO SUBCONTRACT THE MODIFICATION INSPECTOR DUTIES TO A THIRD PAINTED THE ABOVE REQUIREMENTS.

MATCH BOLT)

I. WASHERS FOR BOLTS/ALL THREADS — ASTM F436

J. W & WT SHAPES — ASTM A36 — Fy—36 KSI.

ALTERNATE SPEC: ASTM (IF OTHER SPEC IS UNAVAILABLE).

2.02 STRUCTURAL BOLTS SHALL CONFORM TO THIS NOTE. ALL BOLT HOLES
SHALL BE STANDARD SIZE BOLT HOLES PER AISC 360, UNLESS OTHERWISE
NOTED. ALL HOLES SHALL BE SHOP DRILLED OR SUB—PUNCHED AND
REAMED. BURNING OF HOLES IS NOT PERMITTED, WHERE SLOTTED OR
OVERSIZE HOLES ARE SPECIFIED ON THE DRAWINGS, EXTRA—THICK ASTM
F436 PLATE WASHERS SHALL BE USED (% MINIMUM THICKNESS) WITH A
DIAMETER SUITABLE TO COVER THE EXTENTS OF THE SLOT OF HOLE. BOLTS
SHALL BE HEAVY—HEX WHERE AVAILABLE IN THE SIZE AND GRADE
SPECIFIED.

2.03 ALL STEEL HARDWARE, INCLUDING ADHESIVE OR EMBEDDED ANCHOR BOLTS
THEIR ACCESSORIES, SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES, SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES, SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BE HOT—DIP GALVANIZED IN ACCORDANCE

**MOTHER ACCESSORIES BY SHALL BY THE RIP BY THE ENGINEER OF RECORD AND THE STRUCTURE OWNER WHE

**MOTHER ACCESSORIES BY SHALL BY THE RIP BY THE ENGINEER OF RECORD AND THE STRUCTURE OWNER WHE

**MOTHER ACCESSORIES BY SHALL BY THE RIP BY THE ACCESSORIES BY SHALL BY THE RIP BY THE ACCESSORIES BY SHALL BY THE ACCESSORIES NOTIFY THE ENGINEER OF RECORD AND THE STRUCTURE OWNER WHE WORK HAS BEEN COMPLETED WITHIN 2 BUSINESS DAYS OF THE COM OF THE WORK AND ASSOCIATED MODIFICATION INSPECTIONS & TESTINIT IS ASSUMED THAT ANY STRUCTURAL MODIFICATION WORK SPECIFIED THESE PLANS WILL BE ACCOMPLISHED BY KNOWLEDGEABLE WORKMEN.

THESE PLANS WILL BE ACCOMPLISHED BY KNOWLEDGEABLE WORKMEN TOWER/BUILDING CONSTRUCTION EXPERIENCE. THIS INCLUDES PROVID NECESSARY CERTIFICATIONS TO THE STRUCTURE OWNER AND ENGINE INCLUDING BUT NOT LIMITED TO QUALIFIED WELDER CERTIFICATES, CE WELDING INSPECTOR CREDENTIALS, ET CETERA.

4.06 THESE DRAWINGS DO NOT INDICATE THE METHOD OF CONSTRUCTION, CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL SOLELY RESPONSIBLE FOR ALL CONSTRUCTION METHODS, MEANS, TECHNIQUES, SEQUENCES AND PROCEDURES.

4.07 CONTRACTOR SHALL WORK WITHIN THE LIMITS OF THE STRUCTURE OF PROPERTY OF LEASE AREA AND APPROVED EASEMENT. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY WORK IS WITHIN THE

PROPERTY OF LEASE AREA AND APPROVED EASEMENT. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY WORK IS WITHIN THI BOUNDARIES. CONTRACTOR SHALL EMPLOY A SURVEYOR AS REQUIRE WORK OUTSIDE THESE BOUNDARIES SHALL BE APPROVED IN WRITING LAND OWNER PRIOR TO MOBILIZATION. CONSTRUCTION STAKING AND BOUNDARY MARKING IS THE RESPONSIBILITY OF THE CONTRACTOR. DO NOT SCALE DRAWINGS. CONTRACTOR SHALL VERIFY ALL PLANS, DIMENSIONS, CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY THE ARCHITECT OR ENGINEER IN WRITING OF ANY DISCREPANCIES BE

PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR THE SAME.

1.00 GENERAL INSPECTION NOTES

1.01 THE POST-MODIFICATION INSPECTION IS A VISUAL EXAMINATION OF STRUCTURE MODIFICATIONS AND A REVIEW OF ANY REQUIRED CONSTRUCTION INSPECTIONS, TESTING, AND OTHER DATA TO VERITY THAT THE MODIFICATIONS ARE INSTALLED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS AS DESIGNED BY THE ENGINEER OF RECORD. THE CONTRACTOR DOCUMENTS INCLUDE THESE MODIFICATION DRAWINGS, ANY PROJECT SPECIFICATION REFERENCED TO IN THE PROJECT NOTES OR OTHERWISE PROVIDED WITH THE DRAWINGS, AND OTHER DOCUMENTS OR DRAWINGS PROVIDED WITH THE MODIFICATION DRAWINGS WITH THE INTENT THEY BE USED AS A DESIGN AND OR GUILDELING FOR CONSTRUCTION

USED AS A DESIGN AID OR GUIDELINE FOR CONSTRUCTION.
THE POST-MODIFICATION INSPECTION SHALL CONFIRM INSTALLATION
CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A QUALITATIVE REVIEW OF
THE ENGINEERING ASPECTS OF THE DESIGN OR THE DESIGN DRAWINGS. THE
MODIFICATION INSPECTOR IS NOT TAKING OWNERSHIP OF THE MODIFICATION DESIGN
IN THE PERFORMANCE OF THEIR DUTIES. OWNERSHIP OF THE MODIFICATION DESIGN'S EFFECTIVENESS AND INTENT, AS WELL AS ALL ASSOCIATED RISK, LIED

WITH THE ENGINEER OF RECORD AT ALL TIMES.

TO ENSURE THE REQUIREMENTS OF THE POST—MODIFICATION INSPECTION ARE MET,

IT IS ESSENTIAL COORDINATION BETWEEN THE PRIME CONTRACTOR AND THE

MODIFICATION INSPECTOR BEING AS SOON AS THE PROJECT IS FUNDED AND WORK

ENTERS THE PLANNING STAGE. THE PRIME CONTRACTOR AND MODIFICATION INSPECTOR SHALL BE PROACTIVE IN IDENTIFYING CONSTRUCTION ISSUES AND COMMUNICATE THESE ISSUES TO EACH OTHER AND THE ENGINEER OF RECORD AND STRUCTURE OWNER & CUSTOMER, AS REQUIRED.

2.00 INSPECTION & REPORT RECOM'S
2.01 THE FOLLOWING ARE PROVIDED WITH THE INTENT OF ENHANCING THE EFFECTIVENESS OF THE MODIFICATION INSPECTIONS AND IMPROVING THE EFFICIENCY OF THE PROCESS OF COLLECTING AND COMPILING THE INFORMATION INTO A USEABLE REPORT:

2.01.1 IT IS RECOMMENDED THE PRIME CONTRACTOR PROVIDE THE MODIFICATION INSPECTOR AT LEAST 5 BUSINESS DAYS NOTICE FOR WHEN THE SITE WILL BE READY FOR THE MODIFICATION INSPECTION.

INSPECTION.

2.01.2 THE PRIME CONTRACTOR AND THE MODIFICATION INSPECTOR SHALL COORDINATE CLOSELY THROUGHOUT THE ENTIRE PROJECT.

2.01.3 THE PRIME CONTRACTOR AND MODIFICATION INSPECTION SHALL BOTH BE PRESENT DURING THE INITIAL INSPECTIONS IN ORDER TO ALLOW FOR THE REMEDIATION OF DEFICIENCIES DURING THE INSPECTIONS, AS PRACTICABLE. IT MAY BE PREFERABLE TO KEEP WORK CREWS AND THEIR EQUIPMENT ON—SITE TO REMEDIATE DEFICIENCIES DURING INSPECTIONS.

3.00 INSPECTION RESCHEDULE & CANCEL
3.01 IF THE PRIME CONTRACTOR AND MODIFICATION INSPECTOR HAVE AGREED UPON A TIME AND DATE FOR A GIVEN INSPECTION AND EITHER PARTY RESCHEDULES OR CANCELS THE INSPECTION, THE STRUCTURE OWNER SHALL NOT BE RESPONSIBLE FOR COSTS, FEES, LOST DEPOSITS, OR OTHER EXPENSES INCURRED BY THE PRIME CONTRACTOR, THEIR SUBCONTRACTOR(S), OR THE MODIFICATION INSPECTOR DUE TO THESE SCHEDULING CHANGES. EXCEPTIONS MAY BE MADE IN THE EVENT OF UNCONTROLLABLE SITUATIONS SUCH AS NATURAL DISASTERS, SEVERE WEATHER, OR OTHER CONDITIONS THAT COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.

4.00 REMEDIATION OF FAILING INSPECTION

- 4.01 IN THE EVENT ANY PORTION OF THE MODIFICATION WORK IS DETERMINED TO BE UNSATISFACTORY BY THE MODIFICATION INSPECTOR, THE PRIME CONTRACTOR SHALL WORK WITH THE MODIFICATION INSPECTOR TO CREATE A PLAN OF ACTION THAT WILL EITHER:
 - REPAIR THE DEFICIENT WORK TO SATISFACTORY CONDITION AND INCLUDE A SUBSEQUENT RE-INSPECTION OF THE WORK TO VERIFY IT IS SATISFACTORY.
 - 4.01.2 OR, WITH THE PERMISSION OF THE STRUCTURE OWNER AND/OR CUSTOMER, THE PRIME CONTRACTOR MAY WORK WITH THE ENGINEER OF RECORD TO REVIEW THE AS-BUILT CONDITION OF THE MODIFICATION TO DETERMINE IF IT IS STRUCTURALLY ACCEPTABLE, IF THE ACTION US NOT ACCEPTABLE TO ANY PARTY, THE PRIME CONTRACTOR SHALL PROCEED TO REPAIR THE DEFICIENT WORK TO A SATISFACTORY CONDITION.

5.00 OWNER INSPECTIONS
5.01 THE STRUCTURE OWNER MAY CONDUCT INSPECTIONS TO VERIFY THE QUALITY AND COMPLETENESS OF THE PREVIOUSLY COMPLETED MODIFICATION INSPECTIONS REPORTS OR THE MODIFICATION INSTALLATION WORK.
5.02 INSPECTIONS MAY BE COMPLETED BY A 3RD-PARTY FIRM OF THE STRUCTURE

OWNER'S CHOOSING AFTER A MODIFICATION PROJECT IS COMPLETED AND A PASSING MODIFICATION INSPECTION REPORT IS ISSUED.

6.00 MOD INSPECTOR'S RESPONSIBILITIES
6.01 THE MODIFICATION INSPECTOR SHALL CONTACT THE F
AS THE HAVE RECEIVED A PURCHASE ORDER OR PA'
THE MODIFICATION INSPECTOR SHALL REVIEW THE RE'
INSPECTION CHECKLIST, SHALL WORK WITH THE PRIME
SCHEDULE OF NECESSARY ON-SITE INSPECTIONS, AN
SITE-SPECIFIC INSPECTION REQUIREMENTS OF OTHER
6.02 THE MODIFICATION INSPECTOR IS RESPONSIBLE FOR (
CONTRACTOR INSPECTION AND TEST REPORTS (INCLU-

CONTRACTOR INSPECTION AND TEST REPORTS (INCLU SUB-CONTRACTORS), SHALL REVIEW THE REPORTS FOR CONTRACT DOCUMENTS, SHALL CONDUCT THE NECESS AND SHALL COMPILE AND SUBMIT THE MODIFICATION

7.00 PRIME CONTRACTOR RESPONSIBILIT
7.01 THE PRIME CONTRACTOR SHALL CONTACT THE MODIFIC AS THEY HAVE RECEIVED A PURCHASE ORDER OR PAMODIFICATION INSTALLATION. THE PRIME CONTRACTOR REQUIREMENTS OF THE MODIFICATION INSPECTION CHIT THE MODIFICATION INSPECTOR TO DEVELOP A SCHEDL INSPECTIONS, AND SHALL DISCUSS SPECIFIC INSPECTI REQUIREMENTS WITH THE MODIFICATION INSPECTOR IN UNDERSTANDING OF THE REQUIRED INSPECTION AND
7.02 THE PRIME CONTRACTOR SHALL PERFORM AND RECOI INSPECTION RESULTS IN ACCORDANCE WITH THE REQUINDED TO THE REQUIREMENTS WITH THE REQUIREMENTS.

8.00 PHOTOGRAPHY REQUIREMENTS

8.01 THE PRIME CONTRACTOR AND MODIFICATION INSPECTS
EFFORTS OF BOTH PARTIES AND THEIR EMPLOYED PE
PHOTOGRAPHS WITH THE INSPECTION REPORT TO INC
A GENERAL SITE PHOTOGRAPHS PRE—CONSTRUCTION
B MODIFICATION INSTALLATION PHOTOGRAPHS DURING CONSTRUCTION/ERECTION OPERATIONS AND INSPECTION
B.1 RAW MATERIALS

B.2 PHOTOS OF DETAILED WORK REQUIRED ON THE DRAWINGS (CONNECTIONS, WELDMENTS,

FIELD/FABRICATED MEMBERS, ETC.)

B.3 WELD PREPARATION AND COMPLETED WELD

INSPECTION (INCLUDING A FILLET WELD SIZE G. B.4 BOLT INSTALLATION AND TORQUE/PRETENSION.

B.5 FINAL INSTALLED CONDITION (AFTER DEFICIENT

CONDITIONS, IF ANY, ARE REMEDIATED). B.6 REPAIR OF SURFACE COATINGS (INCLUDING

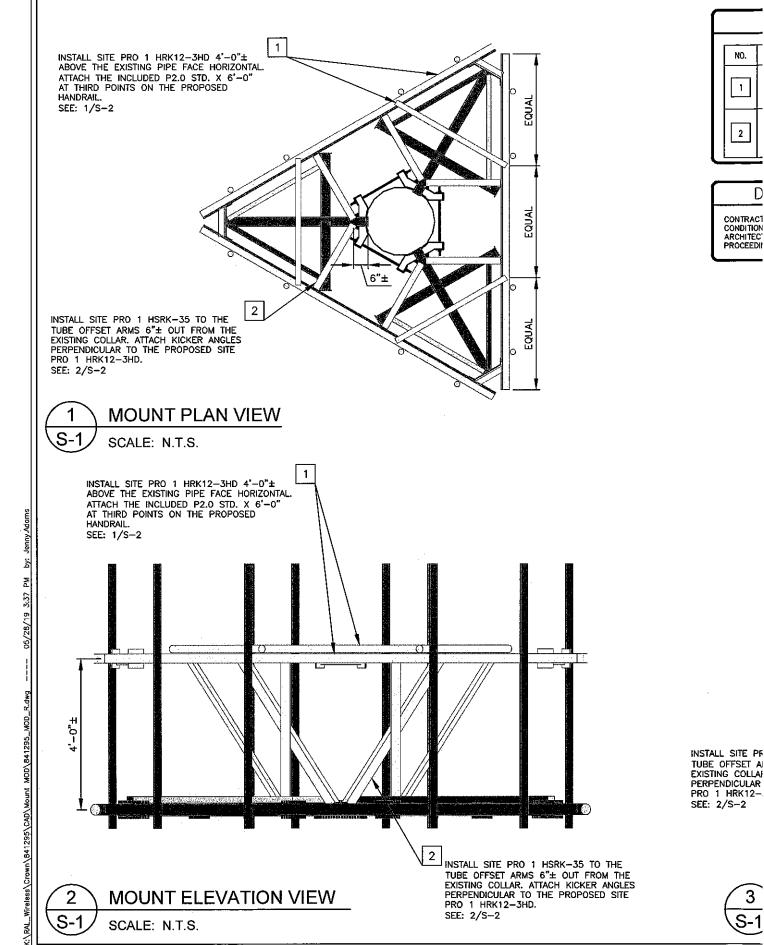
GALVANIZING AND/OR PAINT COATING).

C. POST-MODIFICATION PHOTOGRAPHS OF THE SITE & D. PHOTOGRAPHS OF THE SITE WORK BY THE PRIME CONTRACTOR, ASSOCIATED SITE MODIFICATION INSPECTOR.

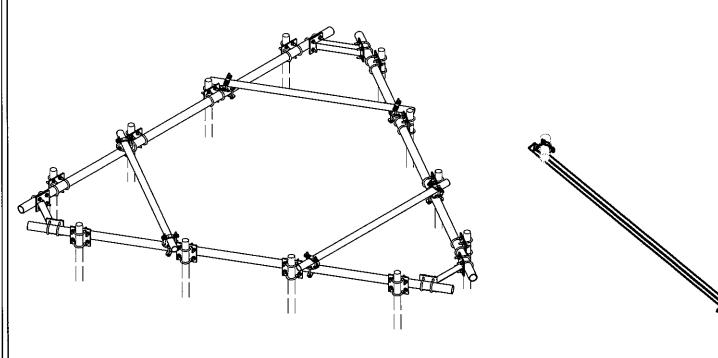
E. OTHER PHOTOS MAY BE INCLUDED AT PRIME CONTRACTOR.

INSPECTOR'S DISCRETION.

NOTE: PHOTOS OF MODIFICATIONS INSTALLED ON THE STR ELEVATION OF 20' SHALL REQUIRE PHOTOS TAKE FROWELL AS OVERALL PHOTOGRAPHS OF THE MODIFICATI GROUND.



This document, together with the concepts and designs presented herein, as an instrument of service, is intended only for the specific purpose and client for which it was prepared. Reuse of and improper reliance on this document without



SITE PRO 1 HRK12-3HD SCALE: N.T.S.

SITE PR

SCALE: N.T