Crown Castle<br>3 Corporate Park Drive, Suite 101

July 18, 2019

Melanie A. Bachman<br>Acting Executive Director<br>Connecticut Siting Council<br>10 Franklin Square<br>New Britain, CT 06051

## RE: Notice of Exempt Modification for Verizon Wireless: $\mathbf{8 4 1 2 9 5}$ <br> Verizon Site ID:104335 <br> 719 Amity Rd. Bethany, CT 06524 <br> Latitude: $\mathbf{4 1}^{\circ}-26^{\prime} 33.93^{\prime \prime} /$ Longitude: $-72^{\circ}-59^{\prime} 32.86^{\prime \prime}$

Dear Ms. Bachman:
Verizon currently maintains nine (9) antennas at the 95 -foot level of the existing 150 -foot monopole tower at 719 Amity Road, Bethany CT 06524. The tower is owned by Crown Castle and the Town of Bethany is the property owner. Verizon now intends to replace six (6) antennas with new antennas. Verizon also intends to add three (3) new remote radios, replace three (3) remote radios with new, add one (1) hybrid cable and one (1) OVP box as well as a handrail kit for the antenna mount.

This facility was approved by the Connecticut Siting Council in Docket No. 168 on June 6, 1995. This approval included the condition that:

1. The self-supporting monopole tower shall be no taller than necessary to provide the proposed communication service and the tower shall not exceed a total height of 150 feet above ground level (AGL).

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16$50 \mathrm{j}-73$, for construction that constitutes an exempt modification pursuant to R.C.S.A. § $16-50 \mathrm{j}-72$ (b) (2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to First-Selectwoman - Ms. Paula Cofrancesco, Town of Bethany and Land Use Administrator/Zoning Enforcement - Isabel Kearns, Town of Bethany. The property owner is the Town of Bethany and Crown Castle is the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

Melanie A. Bachman
December 10, 2018
Page 2
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, Verizon respectfully submits that the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Jeffrey Barbadora.


Jeffrey Barbadora
Real Estate Specialist
12 Gill Street, Suite 5800, Woburn, MA 01801
781-729-0053

## Jeff.Barbadora@crowncastle.com

Attachments:
Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes
Tab 2: Exhibit-2: Structural Modification Report
Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

First-Selectwoman - Ms. Paula Cofrancesco<br>Town of Bethany<br>40 Peck Road<br>203-393-2100 ext. 1100<br>Land Use Administrator/Zoning Enforcement - Isabel Kearns<br>Town of Bethany<br>40 Peck Road<br>203-393-2100 ext. 1135<br>Town of Bethany, Land Owner<br>Crown Castle, Tower Owner

DOCKET NO. 168 - An application of Springwich Cellular Limited Partnership for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telecommunications facility located on the former site of the Bethany Airport, 719 Amity Road (Route 63) in Bethany, Connecticut.
\} Connecticut
\} Siting
\} Council
\} July 6, 1995

## DECISION AND ORDER

Pursuant to the foregoing Findings of Fact, and Opinion, the Connecticut Siting Council (Council) finds that the effects associated with the construction, operation, and maintenance of a cellular telecommunications tower and equipment building at the proposed site in Bethany, Connecticut, including effects on the natural environment; ecological integrity and balance; public health and safety; scenic, historic, and recreational values; forests and parks; air and water purity; and fish and wildlife are not disproportionate either alone or cumulatively with other effects when compared to need, are not in conflict with the policies of the State concerning such effects, and are not sufficient reason to deny the application and therefore directs that a Certificate of Environmental Compatibility and Public Need, as provided by General Statutes $\boldsymbol{\$} 16-50 \mathrm{k}$, be issued to Springwich Cellular Linited Partnership (Springwich), for the construction, operation, and maintenance of a cellular telecommunications tower, associated equipment, and building at the proposed site located at the Bethany Airport, 719 Amity Road, Bethany, Comnecticut.

The facility shall be constructed, operated, and maintained substantially as specified in the Council's record in this matter, and subject to the following conditions:

1. The self-supporting monopole tower shall be no taller than necessary to provide the proposed communications service and the tower shall not exceed a total height of 150 feet above ground level (AGL).
2. The Certificate Folder shall prepare a Development and Management (D\&M) Plan for this site in compliance with Sections $16-50 \mathrm{j}-75$ through $16-50 \mathrm{j}-77$ of the Regulations of Connecticut State Agencies. The D\&M Plan shall be submitted to and approved by the Council prior to the commencement of facility construction and shall include detailed plans for the tower location and tower foundation; the placement of all antennas to be attached to this tower; equipment building, access road, utility line, and security fence; site clearing and tree trimming; and water drainage and erosion and sedimentation controls consistent with the Connecticut Guidelines for Soil Erosion and Sedimentation Control, as amended.
3. Upon the establishment of any new State or federal radio frequency standards applicable to frequencies of this facility, the facility granted herein shall be brought into compliance with such standards.
4. The Certificate Holder shall provide the Council a recalculated report of electromagnetic radio frequency power density if and when circumstances in operation cause a change in power density above the levels originally calculated and provided in the application.
5. The Certificate Holder shall permit public or private entities to share space on the proposed tower for fair consideration, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing.
6. If the facility does not initially provide, or permanently ceases to provide cellular services following completion of construction, this Decision and Order shall be void, and the Certificate Holder shall dismantle the tower and remove all associated equipment or reapplication for any continued or new use shall be made to the Council before any such use is made.
7. Unless otherwise approved by the Council, this Decision and Order shall be void if all construction authorized herein is not completed within three years of the effective date of this Decision and Order or within three years after all appeals to this Decision and Order have been resolved.
8. The Certificate Holder shall notify the Council upon completion of construction and provide the final cost to construct the facility.

Pursuant to General Statutes $\$ 16-50$ p, we hereby direct that a copy of the Findings of Fact, Opinion, and Decision and Order be served on each person listed below, and notice of issuance shall be published in The New Haven Register and Beth-Wood News.

By this Decision and Order, the Council disposes of the legal rights, duties, and privileges of each party named or admitted to the proceeding in accordance with Section $16-50 \mathrm{j}-17$ of the Regulations of Connecticut State Agencies.

The parties and intervenors to this proceeding are:

## applicaitt

Springwich Cellular Limited Partnership

INTERVENOR
Metro Mobile CTS of Hartford, Inc.

## ITS REPRESEITAÁTIVES

Peter J. Tyrrell, Esq.
Springwich Cellular Limited Partnership
227 Church Street
New Haven, CT 06510

## ITS REPRESENTATIVES

Metro Mobile CTS of Hartford, Inc.
20 Alexander Drive
Wallingford, CT 06492
Attn: David S. Malko, P.E., Manager
Engineering \& Regulatory Services
Robinson \& Cole
One Commercial Plaza
Hartford, CT 06103-3597
Attn: Brian C.S. Freeman, Esq.

## CERTIFICATION

The Undersigned members of the Connecticut Siting Council (Council) hereby certify that they have heard this case, or read the record thereof, in Docket No. 168 - An application of Springwich Cellular Limited Partnership for a Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a cellular telecommunications facility located on the former site of the Bethany Airport, 719 Amity Road (Route 63) in Bethany, Connecticut, and voted as follows:

## Council Members

Hodmen 4 Geom
Vote Cast

YES
Mortimer A. Gelston
Chairman
(0)

Commissioner Regina td J. Smith
Designed. Gerald J. Heffernan


YES
Commissioner Sidney J. Holbrook
Designed: Fred Reese


YES

ABSENT

YES

ABSTAIN
Colin C. Wait

> Edward S. Wilensky


YES

Dated at New Britain, Connecticut, July 6, 1995.

STATE OF CONNECTICUT \}
ss. New Britain, Connecticut \} COUNTY OF HARTFORD
STATE OF CONNECTICUT $\} \quad$ July 7, 1995

I hereby certify that the foregoing is a true and correct copy of the Findings of Fact, Opinion, and Decision and Order issued by the Connecticut Siting Council, State of Connecticut.

## ATTEST:



I certify that a copy of the Findings of Fact, Opinion, and Decision and Order in Docket No. 168 have been forwarded by Certified First Class Return Receipt Requested mail on July 7, 1995, to all parties and intervenors of record as listed on the attached service list, dated April 10, 1995.

ATTEST:


Gloria B. Owens
Administrative Assistant
Connecticut Siting Council

The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at $70 \%$ of the estimated market value of real property at the time of the last revaluation which was 2013.


Information on the Property Records for the Municipality of Bethany was last updated on 9/20/2017.

## Property Summary Information

Parcel Data And Values Building $\nabla$ Outbuildings Google Map

## Parcel Information

| Location: | 755 AMITY RD | Property Use: Public Use | Primary Use: | Fire Station - |
| :--- | :--- | :--- | :--- | :--- | :--- |
| Volunteer |  |  |  |  |

## Value Information

|  | Appraised Value | 70\% Assessed Value |
| :--- | :---: | :---: |
| Land | $1,476,000$ | $1,033,200$ |
| Buildings | $1,740,164$ | $1,218,110$ |


|  | Appraised Value | 70\% Assessed Value |
| :--- | :--- | :--- |
| Detached Outbuildings | 159,624 | 111,740 |
| Total | $3,375,788$ | $2,363,050$ |
|  | Owner's Information |  |

Owner's Data<br>BETHANY TOWN OF 40 PECK RD<br>BETHANY CT 06524

; Back To Search (JavaScript:window.history.back(1);)
Print View (PrintPage.aspx?towncode $=008 \&$ uniqueid $=00016500$ )

Information Published With Permission From The Assessor

Town of Bethany, Connecticut Assessment Parcel Map

Parcel: 00016500 Address: 755 AMITY RD


Map Produced: Aug 2017

## Site Name: Bethany North CT

## Cumulative Power Density

| Operator | Operating Frequency | Number of Trans | ERP Per Trans. |  | Distance to Farget | $\begin{aligned} & \text { Calculted } \\ & \text { Eower } \\ & \text { Bensity } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | (MHz) |  | (watts) | (watts) | (feet) | $\left(\mathrm{mW} / \mathrm{cm}^{\wedge} 2\right)$ |
| VZW PCS | 1970 | 4 | 1104 | 4416.28 | 110 | 0.1313 |
| VZW Cellular CDMA | 869 | 2 | 289 | 578.16 | 110 | 0.0172 |
| VZW Cellular LTE | 880 | 4 | 463 | 1853.76 | 110 | 0.0551 |
| VZW AWS | 2145 | 4 | 1225 | 4898.44 | 110 | 0.1456 |
| VZW 700 | 746 | 4 | 492 | 1968 | 100 | 0.0708 |

Total Percentage of Maximum Permissible Exposure
*Guidelines adopted by the FCC on August 1, 1996, 47 CFR Section 1.13101 based on NCRP Report 86, 19
$\mathrm{MHz}=$ Megahertz
$\mathrm{mW} / \mathrm{cm}^{\wedge 2}$ = milliwatts per square centimeter ERP = Effective Radiated Power

Absolute worst case maximum values used, including the following assumptions:

1. closest accessible point is distance from antenna to base of pole;
2. continuous transmission from all available channels at full power for indefinite time period; and, 3. all RF energy is assumed to be directed solely to the base of the pole.

| Maximum Permissible Exposure | Fraction of MPE |
| :---: | :---: |
| (mW/cm ${ }^{\wedge}$ 2) | (\%) |
| 1.0 | 13.13\% |
| 0.579333333 | 2.97\% |
| 0.586666667 | 9.39\% |
| 1.0 | 14.56\% |
| 0.497333333 | 14.23\% |

86 and generally on ANSI/IEEE C95.1-1992

The Assessor's office is responsible for the maintenance of records on the ownership of properties. Assessments are computed at $70 \%$ of the estimated market value of real property at the time of the last revaluation which was 2018.


Information on the Property Records for the Municipality of Bethany was last updated on 7/18/2019.

## Property Summary Information



## Value Information

## Appraised Value

1,421,200
Assessed Value
Land

|  | Appraised Value | Assessed Value |
| :--- | :--- | :--- |
| Buildings | $1,878,616$ | $1,315,030$ |
| Detached Outbuildings | 150,924 | 105,650 |
| Total | $3,450,740$ | $2,415,520$ |
|  | Owner's Information |  |
|  | Owner's Data |  |
|  | BETHANY TOWN OF |  |
| 40 PECK RD |  |  |
| BETHANY, CT 06524 |  |  |

Back To Search (JavaScript:window.history.back(1);)
Print View (PrintPage.aspx?towncode=008\&uniqueid=00016500)

Information Published With Permission From The Assessor

Town of Bethany, Connecticut Assessment Parcel Map

Parcel: 00016500
Address: 755 AMITY RD




| ORIGINID:BEDA JEFF BARBADORA CROUN CASTLE 12 GILL STREET SUITE 5800 WOBURN MA O1801 UNITED STATES US | (781) 970-0053 | SHIP DATE: 18JUL 19 ACTWGT:0.50 LB CAD: 104924191/IMET4160 <br> BLLL SENDER |
| :---: | :---: | :---: |
| To LAND USE/ZONE ENF. ISABEL KEARNS |  |  |
| TOWN OF BETHANY |  |  |
| 40 PECK ROAD |  |  |

```
(203) 393-2100\times1135
                                    REF: 1766.6600
```

| $\mathbb{N}:$ |
| :--- |
| $\mathrm{PO}:$ |



FRI - 19 JUL 10:30A
Trkसt 775777076160
PRIORITY OVERNIGHT
EB EFBA
06524 cт.us BDL



FRI-19 JUL 10:30A
TRK\# 775777051682
PRIORITY OVERNIGHT EB EFBA ${ }^{\text {and }}$


Kevin Morrow
Crown Castle
3530 Toringdon Way, Suite 300
Charlotte, NC 28277
(704) 405-6619

Kimley»)Horn
Kimley-Horn and Associates, Inc.
421 Fayetteville Street, Suite 600
Raleigh, NC 27601
(919) 677-2000

CrownMounts@kimley-horn.com

## Subject:

## Carrier Designation:

Crown Castle Designation:

Mount Modification Report
Verizon Wireless Equipment Change-Out Carrier Site Number: 104335
Carrier Site Name: Bethany North CT

Crown Castle BU Number: 841295
Crown Castle Site Name: BETHANY
Crown Castle JDE Job Number: 574490
Crown Castle Order Number: 492710 , Rev. 0

Engineering Firm Designation: Kimley-Horn Report Designation: 019558041
Site Data:
719 Amity Road, Bethany, New Haven County, CT 06524
Latitude $41^{\circ} 26^{\prime} 33.93^{\prime \prime}$ Longitude $-72^{\circ} 59^{\prime} 32.86^{\prime \prime}$

Structure Information:
Tower Height \& Type:
150 ft Monopole
Mount Elevation: 140 ft
Mount Type:
12.5 ft Low Profile Platform

Dear Charles McGuirt,

Kimley-Horn is pleased to submit this "Mount Modification Report" to determine the structural integrity of Verizon Wireless's antenna mounting system with the proposed appurtenance and equipment addition on the abovementioned supporting tower structure. Analysis of the existing supporting tower structure is to be completed by others and therefore is not part of this analysis. Analysis of the antenna mounting system as a tie-off point for fall protection or rigging is not part of this document.

The purpose of the analysis is to determine acceptability of the mount stress level. Based on our analysis we have determined the mount stress level to be:

## Low Profile Platform

## Sufficient

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2015 International Building Code. Applicable Standard references and design criteria are listed in Section 2 - Analysis Criteria.

Mount analysis prepared by: Greg VanMaaren, E.l. under the supervision of Steven C. Ball, P.E., S.E.


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4) ANALYSIS RESULTS

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Mount Modification Design Drawings (MDD)

## 1) INTRODUCTION

The mounting configuration consists of existing 12.5 ft Low Profile Platform.
2) ANALYSIS CRITERIA

| Building Code: | $2015 \mathrm{IBC}, 2018$ Connecticut State Building Code |
| :--- | :--- |
| TIA-222 Revision: | TIA-222-H |
| Risk Category: | II |
| Ultimate Wind Speed: | 125 mph |
| Exposure Category: | C |
| Topographic Factor at Base: | 1.0 |
| Topographic Factor at Mount: | 1.0 |
| Ice Thickness: | 0.75 in |
| Wind Speed with Ice: | 50 mph |
| Live Loading Wind Speed: | 30 mph |
| Man Live Load at Mount Pipes: | 500 lb |

Table 1 - Proposed Equipment Configuration

| Elevation (ft) |  | K, Me, Me, Antennas |  |
| :---: | :---: | :---: | :---: |
| Mount | Centerline | \# \# \% |  |
| 140 | 140 | 6 | CommScope $\mathrm{NHH}-65 \mathrm{C}-\mathrm{R} 2 \mathrm{~B}$ |
|  |  | 3 | decibel (cci) DB854DG65ESX |
|  |  | 1 | rfs celwave DB-T1-6Z-8AB-0Z |
|  |  | 3 | samsung telecommunications RFV01U-D1A |
|  |  | 3 | samsung telecommunications RFV01U-D2A |

## 3) ANALYSIS PROCEDURE

Table 2 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Photos | - | - | CCISites |
| Mount Analysis | Kimley-Horn | 8418942 | CCISites |

## 3.1) Analysis Method

RISA-3D (version 16.00), a commercially available analysis software package, was used to create a three-dimensional model of the antenna mounting system and calculate member stresses for various loading cases.

A proprietary tool internally developed by Kimley-Horn and Associates, Inc. was used to calculate wind loading on all appurtenances, dishes and mount members for various load cases. Selected output from the analysis is included in Appendix B.

This analysis was performed in accordance with Crown Castle's ENG-SOW-10208 Tower Mount Analysis (Revision B).

## 3.2) Assumptions

1) The antenna mounting system was properly fabricated, installed and maintained in good condition in accordance with its original design and manufacturer's specifications.
2) The configuration of antennas, mounts, and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
3) All member connections are assumed to have been designed to meet or exceed the load carrying capacity of the connected member unless otherwise specified in this report.
4) Steel grades have been assumed as follows, unless noted otherwise:

| Channel, Solid Round, Angle, Plate | ASTM A36 (Gr. 36) |
| :--- | :--- |
| HSS (Rectangular) | ASTM A36 (Gr. 36) |
| Pipe | ASTM A53 (Gr. B-35) |
| Threaded Rods | ASTM A36 (Gr. 36) |
| Connection Bolts | ASTM A325 |

This analysis may be affected if any assumptions are not valid or have been made in error. Kimley-Horn should be notified to determine the effect on the structural integrity of the antenna mounting system.

## 4) ANALYSIS RESULTS

Table 3 - Mount Component Stresses vs. Capacity

| Component | \% Capacity | Pass $/$ Fail |
| :---: | :---: | :---: |
| Connections | $87 \%$ | Pass |
| Stand Off Horizontals | $53 \%$ | Pass |
| Mount Pipes | $39 \%$ | Pass |
| Corner Plates | $39 \%$ | Pass |
| Face Horizontals | $20 \%$ | Pass |


|  |
| :---: |
|  |  |

## 4.1) Recommendations

According to our structural analysis, the mounting configuration has been found to PASS PENDING MODIFICATIONS. The mounting configuration considered in this analysis will be capable of supporting the referenced loading pursuant to referenced standards once the referenced modifications are installed.

This analysis incorporates modifications per Kimley-Horn, dated 05/28/19.

## APPENDIX A

WIRE FRAME AND RENDERED MODELS



## APPENDIX B

## SOFTWARE INPUT CALCULATIONS



| Exposure Category | C |
| :---: | :---: |
| Topographic Factor， $\mathrm{K}_{2}$ ： | 1.00 |
| Strucilie Base Elev：（AMSL），$z_{3}(t)$ | 741.00 |
| Ground Effect Factor， $\mathrm{K}_{\mathrm{p}}$ | 0.97 |



| Whid Direction Probability Factor， $\mathbf{K}_{\mathbf{d}}$ | 0.95 |
| :---: | :---: |
| Gust Efiect Factor， $\mathbf{S}_{\mathbf{n}}$ | 1 |
| Shielding Factor，$K_{\text {a }}$（antenna） | 0.9 |
| Sthielding Factor， $\mathrm{K}_{\mathbf{a}}$（mount） | 0.9 |


| Whasimmary |  |
| :---: | :---: |
| Basic Wind Speed W／o leo，V（ （riph） | 125.09 |
| Velocity Pressure Coeff， $\mathbf{K}_{\mathbf{z}}$ ． | 1.36 |
| Velocily Prosscire， $\mathbf{q}_{2}$（w／o lce） （psf） | 50.26 |


| Baslc Wind Speed w／ice， $\mathrm{V}_{1}$（mph） | 50，00 |
| :---: | :---: |
| Destgn lce Thick．（ASCE 7－10）； $\mathbf{t}_{\text {（in）}}$ ） | 0.75 |
| Velocily Pressuife，$q_{z}$（wllce）（psf） | 8.04 |
| Escalated loe Thick，© Mounit tig（ $(\mathrm{n}$ ） | 1.73 |


|  |  |
| :---: | :---: |
| Spectral Respoise（Short Periods），$S_{5}$ | － |
| Spectral Response $\{$ i－Sec．Peiod $)$ ， $\mathbf{S}_{1}$ | － |
| Site Class | － |
| Seismic Design Calegory | － |
| Seismic Risk Category | － |



## Kimley»）Horn

| Date | May 28，2019 |
| :--- | :--- |
| Client | Crown Castla |
| Site\＃ | 841295 |
| Site Name | BETHANY |
| Project\＃ | 19558041 |


| Antenna $N$ ainc | ONoy | Shape |  |  |  |  |  | Mha |  |  |  |  |  |  | Hent | Side |  | Wisiod |  | $\square$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| NHH－65C－R2E | 3 | Flat | 96 | 11.9 | 7.1 | 51.6 | N1212B | N12108 | N1228B | N12268 | N1220日 | N12188 | 0 | 0 | 1139 | 7.66 | 529．14 | ${ }^{\text {Sigig }}$ | 108.6 | Sidide |
| NHH－65C－R2B | 3 | Flat | 96 | 11.9 | 7.1 | 51.6 | N2211B | N12098 | N12278 | N12258 | N1219日 | N1217B | 0 | 0 | 11.39 | 7.68 | 529.14 | 355.69 | 108.62 | 80．32 |
| D8854DG65ESX | 3 | Flat | 48 | 12.6 | 5.7 | 18.5 | N1232日 | N1231B | N1240C | N1239C | N1236日 | N12358 | 0 | 0 | 5.28 | 2.75 | 245.5 | 12777 | 525 | 80.32 <br> 32.6 |
| DB－T1－6Z．9AB－0Z | 1 | Flat | 24 | 24 | 10 | 44 | N124SE | B | 0 | 0 | 0 | 0 | 0 | 0 | 2.4 | 2 | 111.51 | 92.92 | 23.37 | 22.91 |
| RFV01U－D1A | 2 | Flat | 15 | 15 | 10 | 94.4 | 0 | 0 | N1251C | N1250C | 0 | 0 | 0 | 0 | 0,94 | 1.25 | 43.56 | 8 | 10.56 | 5.41 |
| RFVV11－D2A | 2 | Flat | 15 | 15 | 8.1 | 70.3 | N1245B | N1244C | 0 | 0 | 0 | 0 | 0 | 0 | 0.84 | 1.01 | 43.56 | 47.04 | 10.56 | 13.23 |
| RFV01U－D1A | 1 | Flat | 15 | 15 | 10 | 84.4 | 0 | 0 | N1252A | 0 | 0 | 0 | 0 | 0 | 0.94 | 1.25 | 43.56 | 58，08 | 10.56 | 15.41 |
| RFV01U－02A | 1 | Flat | 15 | 15 | 8.1 | 70.3 | N1248E | ， | 0 | 0 | 0 | 0 | 0 | 0 | 0.94 | 1.01 | 43．56 | 47.04 | 10.56 | 13.23 |

## APPENDIX C

## SOFTWARE ANALYSIS OUTPUT

## Basic Load Cases

|  | BLC Description | Category | $X$ Gravity | Y Gravity | Z Gravity | Joint | Point | Distributed | Area/Me.. | Surface(P.. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| , | Dead | DL |  |  | -1 | 25 |  |  |  |  |
| 2 | Dead of lce. | T. RL | , | N, | am | 25 |  | 51 | 4, | W, |
| 4. | Structure Wind (0) | None | NW ${ }^{\text {a }}$, | $\cdots \times$ | W | , ${ }^{2}$, | NTSM | 402 | \% |  |
| 5 | Structure Wind (30) | None |  |  |  |  |  | 102 |  |  |
| 6. | Structure Wind (45) | None | $\cdots$ | 2 | 13, |  | \% | 102 | W\% ${ }^{\text {a }}$ |  |
| 7. | Structure Wind (60) | None |  |  |  |  |  | 102 |  |  |
| 8 | Structure Wind (90) | None | WVY4. | Fera | 12\% 4 , | 34, | \% \% ${ }^{\text {a }}$ | 102 | W, |  |
| 9 | Structure Wind (120) | None |  |  |  |  |  | 102 |  |  |
| 10 | Structure Wind (135) | None. | N-Tさ? | , , , | - , $\times$, | Wry | - | 102. | 3-7 |  |
| 11 | Structüre Wind (150) | None |  |  |  |  |  | 102 |  |  |
| 12 | Structure Wind w/ lce . | None | , | *, | 4...... |  | V, - | 102 | , , \% | , |
| 13 | Structure Wind w/ lce ... | None |  |  |  |  |  | 102 |  |  |
| 14 | Structure Wind w/ lce. | - None. |  | , , , , | Nay | $\cdots$ | 4* | 102 | man | \#, \% |
| 15 | Structure Wind w/ Ice ... | None |  |  |  |  |  | 102 |  |  |
| 16 | Structure Wind w/ Ice. | None. | \% ${ }^{2}$ | , | W, | M ${ }^{\text {a }}$ | 4, +, ${ }^{\text {as, }}$ | 102 |  | , |
| 17 | Structure Wind w/ Ice . | None |  |  |  |  |  | 102 |  |  |
| 18 | Structure Wind w/lce. | None | , , + | $\ldots$ | $3 \times$ |  |  | 102 | \% $\times$, | $\cdots$ |
| $\frac{19}{20}$ | Structure Wind w/ lce ... | None |  |  |  |  |  | 102 |  |  |
| 20 | Antenna Wind (0) | None., |  |  |  | 50 | , | 102 | 2, | \% |
| 21 | Antenna Wind (30) | None |  |  |  | 50 |  |  |  |  |
| 22. | Antenna Wind (45) | None. | 4 | \% |  | 50 |  | 2, \% ${ }^{\text {a }}$ |  |  |
| 23 | Antenna Wind (60) | None |  |  |  | 50 |  |  |  |  |
| 24 | Antenna Wind (90) | None. |  |  |  | 50 |  | \% |  |  |
| 25 | Antenna Wind (120) | None |  |  |  | 50 |  |  |  |  |
| 26. | Antenna Wind (135) | None. |  |  | . | , 50, | 줓 | 4 | 4, ${ }^{2}$ |  |
| 27. | Antenna Wind (150) | None |  |  |  | 50 |  |  |  |  |
| 28. | Antenna Wind w/Ice... | None, | $\cdots$ |  | , | 50 |  |  | , |  |
| 29. | Antenna Wind w/ Ice (... | None |  |  |  | 50 |  |  |  |  |
| 30. | Antenna Wind w/lee? | None | W. ${ }^{\text {a }}$ | ¢ |  | 50 | - |  |  |  |
| 31. | Antenna Wind w/ Ice (.). | None |  |  |  | 50 |  |  |  |  |
| 32. | Antenna Wind w/ Ice,. | None, |  | $\cdots$ |  | - 50 |  | $\cdots$, | , | W, |
| 33. | Antenna Wind w/ Ice (... | None |  |  |  | 50 |  |  |  |  |
| 34 | Antenna Wind w/lce.. | None. |  | ¢ ${ }^{\text {a }}$ | + | 50 |  | 4, | $\cdots$ | \% |
| 35 | Antenria Wind w/ Ice (... | None |  |  |  | 50 |  |  |  |  |
| 36 | Maintenance Live Lm. | - OL1. |  | $\wedge$ | W ${ }^{\text {a }}$ | -1. | W\% | , $\times 2$ | \% |  |
| 37 38 | Maintenance Live Lm .. | OL2 |  |  |  | 1 |  |  |  |  |
| -38 | Maintenance Live Lm. | $\cdots \mathrm{OL} 3$ | $\cdots$ | W, | W\% | 1 | \% ${ }^{\text {a }}$ | W, \% | , $\times$, |  |
| 39 | Maintenance Live Lm.r. | OL4 |  |  |  | 1 |  |  |  |  |

## Load Combinations



## Load Combinations (Continued)

|  | Descripti... | PDelta |  |  |  |  | CFac. |  |  |  |  |  |  |  |  |  | Fa |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 14 | $12 \mathrm{D}+1$ Yes | Y Y , |  |  |  | 7. |  |  | - 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 15 | 1.2D $+1 .$. Yes | Y |  | DL | 1.2 | 8 | -1 | 24 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| -16. | 12D + / Y Yes |  |  | D ${ }^{\text {d }}$ | 12 | 9 | $\underline{1}$ | 25 | $-1$ |  | , | , | , | - | * | 䜌 | , | , | \% |  | , | , | , |
| 17 | 1.2D + 1...Yes | Y |  |  | 1.2 | 10 | -1 | 26 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| $\underline{18}$ | 120 +1, Yes | , $\mathrm{Y}^{\mathbf{Y}}$, |  | DL | 1.2 | 11 | 1 | 27 | -1 | 洨 | \% | , | , | \% | TY | " | , ${ }^{\text {a }}$ | , | * | + | W | , | , |
| 19 | 1,2D + 1...Yes | Y |  | DL | 1.2 | RL | 1 | 12 | 1 |  | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 20 | 12D +1. Yes | , Y |  | DL | 12 | RL | 1 | 13 | 1 | 29 | 1 |  |  | * | +2\% | , | * | 1, | 1. |  | 24x |  |  |
| 21 | 1.2D $+1 . . . Y$ Yes | Y |  |  | 1.2 | RL | 1 | 14 | 1 | 30 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 22 | 120+1. Ves | Y Y, |  |  | 1.2 | RL | 1 | 15 | 1 | 31 | 1 | - | 3 | , | * | , | + | 4 | , | " | - |  |  |
| 23 | 1:2D + 1...Yes | $Y$ |  |  | 1.2 | RL | 1 | 16 | 1 | 32 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 24 | $12 \mathrm{D}+1, \mathrm{Yes}$ | V $V$ |  | DL | 1.2 | RL | 1 | 17 | 1 | 33 | 1 |  | 5, | 4 | , | , |  |  |  | , | $\cdots$ |  |  |
| 25 | 1.2D $+1 .$. Yes | Y |  |  | 1.2 | RL | 1 | 18 | 1 | 34 | 1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 26. | 120 + 1, Yes | Y |  | DL | 1.2 | RL | 1 | 19 | 1 | 35 | 1 | 2 |  | * | 1 |  |  |  | , | , |  |  |  |
| 27 | 1.2D $+1 .$. Yes | $Y$ |  | DL | 1.2 | RL | 1 | 12 | -1 | 28 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 28. | $1.20+1, \mathrm{Yes}$ | , Y |  | DH | 1.2 | RL | 1 | 13 | 1 | 39. | -1 | , | \% | 4 | $\stackrel{\square}{ }$ | , |  | 4 |  |  |  | \% |  |
| 29 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | $Y$ |  |  | 1.2 | RL | 1 | 14 | -1 | 30 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 30. | 12D $+1 . \mathrm{Yes}$ | Y $Y$ |  | DL | 1.2 | RL | 1 | 15 | -1 | 31 | -1 |  | $\cdots$ | . | , |  | 1, |  |  | , |  | 4 |  |
| 31 | 1.2D $+1 .$. Yes | Y |  |  | 1.2 | RL | 1 | 16 | -1 | 32 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 32. | 120 +1., Yes | Y |  | DL 1 | 1.2 | R | 1 | 17 | 4 | 33 | -1 | , | Y | * | * | $\cdots$ | , |  |  |  |  | , | , |
| 33. | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | Y |  |  | 1.2 | RL | 1 | 18 | -1 | 34 | -1 |  |  |  |  |  |  |  |  |  |  |  |  |
| 34 | $12 \mathrm{D}+1 . \mathrm{Yes}$ | Y |  | DL 1 | 1.2 | RL | 1 | 19. | 1 | 35 | -1 |  | L |  | \% |  |  | \% | , | 4 | , | , |  |
| 35 | 1.2D + $1 .$. Yes | Y |  |  | 1.2 | 4 | . 058 | 20 | . 058 |  | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 36. | 12D $+1 . \mathrm{Yes}$ | , Y |  | DL 1 | 1.2 | 5 | 058 | 21 | 058 |  | 1.5 | , |  | - | , | + |  |  |  |  | , |  |  |
| 37 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | Y |  |  | 1.2 | 6 | . 058 | 22 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 38. | 12D +1.Yes | $\cdots$ |  | DL 1 | 1.2 | 7 | 058 | 23 | 058 |  | 1.5 |  |  |  | $\cdots$ |  | $\cdots$ |  | $\cdots$ |  |  | * |  |
| 39 | $1.2 \mathrm{D}+1 \ldots$ Yes | Y |  |  | 1.2 | 8 | . 058 | 24 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 40 | $1.2 \mathrm{D}+1 . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 9 | 058 | 25. | 058 | OL1 | 1.5 |  |  | 4 | $\cdots$ | , | 1*, |  |  | , |  |  |  |
| 41 | $1.2 \mathrm{D}+1 \ldots . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 10 | . 058 | 26 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 42 | $12 \mathrm{D}+1 \ldots \mathrm{Yes}$ | Y $\mathbf{Y}$ |  | DL1 | 1.2 | 11 | 058 | 27 | 058 | 0 C | 1.5 |  |  |  | , |  | , |  | , |  |  |  |  |
| 43 | $1.2 \mathrm{D}+1 .$. Yes | Y |  |  | 1.2 |  | -. 058 | 20 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 44 | $12 \mathrm{D}+1 . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 5 | -058 | 21 | 058 | OL | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 45 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 6 | -. 058 | 22 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 46 | 12D +1. Yes | Y |  | DL1 | 1.2 | 7. | . 058 | 23 | , 058 | OL | 1.5 |  |  |  |  | $\checkmark$ |  | . |  |  | . | , |  |
| 47 | 1.2D + 1... Yes- | Y |  | DL 1 | 1.2 | 8 | -. 058 | 24 | . 058 | OL1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 48 | 12D+1. Yes | Y $Y$ |  | DL 1 | 1.2 | 9 | 058 | 25 | 058 | OL1 | 1.5 | , |  |  |  |  | , |  | , |  |  |  |  |
| 49 | 1.2D + 1...Yes | $Y$ |  | DL 1 | 1.2 | 10. | . 058 | 26 | . 058 | OLT 1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 50 | $12 \mathrm{D}+1 . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 11 | -058 |  | .058 |  | 1.5 |  |  |  |  |  |  |  | \% |  |  |  |  |
| 51 | 1.2D+1.. Yes | $Y$ |  | DL 1 | 1.2 | 4 | . 058 | 20 | . 058 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 52 | $12 \mathrm{D}+1 . \mathrm{Yes}$ |  |  | DL 1 | 1.2 | 5 | 058 | 21 | 058 |  | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 53 | 1.2D + 1...Yes | Y |  | DL 1 | 1.2 | 6 | . 058 | 22 | . 0580 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 54 | $1.2 \mathrm{D}+1 . \mathrm{Yes}$ | Q Y |  | DL 1 | 1.2 | 7 | 058 | 23 | 058 | OL2 | 1.5 |  | 5 |  |  |  |  |  |  |  |  |  |  |
| 55 | 1.2D + 1...Yes | Y |  | DL 1 | 1.2 | 8 | . 058 | 24 | . 058 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 56 | 12D+1. Yes | , $\mathbf{Y}^{\text {P }}$ |  | DL 1 | 12 | 9 | 058 | 25 | . 058 | OL 2 | 1.5 |  |  |  | , |  |  | , |  | , |  | \% |  |
| 57 | $1.2 \mathrm{D}+1 \ldots \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 10. | . 058 | 26 | . 058 | OL 2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 58 | 1.2D +1. Yes | , Y |  | DL 1 | 1.2 | 11. | 058 | 27. | 058 | OL2 | 1.5 | , | 4 |  |  |  |  |  |  |  | 4 |  |  |
| -59 | 1.2D $+1 . . . Y$ Yes | Y |  | DL 1 | 1.2 | 4. | -058 | 20 | . 058 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 60 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 |  | 058 | 21. | . 058 | OL 2 | 1.5 |  | $\stackrel{1}{2}$ |  |  |  |  |  |  |  |  | $\times$ |  |
| 61 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 6. | -. 058 | 22 | . 058 | OL2 1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 62 | 12D+1. Yes | Y |  | DL 1 | 1.2 | 7 . | 058 | 23. | 058 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 63 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | Y |  | DL 1 |  | 8. | -058 | 24 | . 0580 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 64 | 12D + $1 . \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 9 | . 058 | 25 | . 058 | OL2 | 1.5 |  |  |  |  | 4 |  |  |  |  |  |  |  |
| 65 | $1.2 \mathrm{D}+1 . . \mathrm{Yes} \mid$ | Y |  | DL. 1 | 1.2 | 10. | . 058 | 26 | . 058 | OL2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 66. | 12D + 1. Yes | Y |  | DL 1 | 1.2 | 11. | . 0582 | 27 | . 058 | 0 L 2 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 67 | 1:2D $+1 \ldots Y$ | Y |  | DL 1 | 1.2 | 4 | . 058 | 20 | . 058 | OL3 1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 68 | $122+1 . Y \mathrm{Yes}$ | $Y$ |  | DL 1 | 1.2 | 5 | 058 | 21 | 058 | OLS | 1.5 |  |  |  |  | , |  |  |  |  |  |  |  |
| 69 | 1.2D + 1...Yes | Y |  | DL 1 | 1.2 | 6 | . 058 | 22 | . 058 | OL3 1 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 70 | 122D +1..Yes | Y |  | DL1 | 1.2 | 7 | 0582 | 23 | 058 | 0L31 | 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |

## Load Combinations (Continued)

|  | Descripti...So | PDel |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 71 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | Y |  | DL 1.2 | 8 | [.058 | 24 | . 058 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 72 | 12D +1. Yes | Y | 2. | DL 1.2 | 9 | 058 | 25 | 1058 | OL3 1.5 |  | , | , | , | 12, |  |  | ** |  |  | 4 |  |
| 73 | 1.2D + 1...Yes | Y |  | DL 1.2 | 10 | . 058 | 26 | . 058 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 74 | $12 \mathrm{D}+11 \mathrm{Yes}$ | , Y |  | B41.2 | 11 | 058 | 27 | 058 | © 41.5 |  | \% |  | 1, | , |  |  | , |  |  |  |  |
| 75 | 1.2D $+1 . .$. Yes | Y |  | DL 1.2 | 4 | -. 058 | 20 | - 058 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 76 | 12D + 11, Yes | Y, Y |  | DL 1.2 | 5 | 058 | 21 | . 058 | OL31.5 |  |  |  | $\cdots$ |  |  |  |  |  |  | a |  |
| 77 | 1.2D + 1...Yes | Y |  | DL 1.2 | 6 | -. 058 | 22 | -. 058 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 78. | 12D + 1 Yes | U@ Y |  | DU 1.2 | V | 0.58 | 23. | . 058 | OL3 1.5 |  |  |  | , |  |  |  |  |  |  |  |  |
| 79 | $1.2 \mathrm{D}+1 \ldots \mathrm{Yes}$ | Y |  | DL 1.2 | 8 | -. 058 | 24 | . 058 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 80 | $12 \mathrm{D}+14 \mathrm{Yes}$ | Y-Y |  | DL 1.2 |  | . 058 | 25 | -0580 | 0131.5 | , |  |  | (a) |  |  | , | , |  |  |  |  |
| 81. | 1.2D + 1...Yes | Y |  | DL 1.2 | 10. | -. 058 | 26 | -. 0580 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 82. | $12 \mathrm{D}+11 \mathrm{Yes}$ | W | , | DL 12 | 11. | .058 | 27. | 0558 | OL3 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 83. | 1:2D + 1...Yes | $Y$ |  | DL 1.2 | 4 | . 058 | 20 | . 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 84 | $12 \mathrm{t}+1 . \mathrm{Yes}$ | $\cdots$ | , | DL1.2 | 5 | 058. | 21 | . 0580 | 0.41 .5 |  |  |  |  |  | 4 |  |  |  |  |  |  |
| 85 | 1.2D + 1...Yes | Y |  | DL 1.2 | 6 | . 058 | 22 | . 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 86 | 12D +1. Yes | $\cdots$ |  | DL 1.2 | 7. | 058 | 23. | 0580 | 0 L 41.5 |  |  |  |  |  |  |  |  |  |  | - |  |
| 87 | 1.2D + 1...Yes | $Y$ |  | DL 1.2 | 8 | . 058 | 24 | . 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 88. | 12D + $1 . \mathrm{Yes}$ | $\cdots$ |  | DL1.2 | 9 | . 058 | 25 | 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 89 | 1.2D + 1...Yes | Y |  | DL 1.2 | 10. | . 058 | 26 | . 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 90 | 12D+1.4Vs | $Y$ |  | DL 1.2 | 11. | 058 | 27 | 058 | OL4 1.5 |  | , |  | 4 | , |  |  |  |  | * |  | \% |
| 91. | 1.2D + 1...Yes | Y |  | DL 1.2 | 4 | -. 058 | 20 | -. 0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 92 | 122D+1. Yes | Y |  | D 41.2 | 5. | . 058 | 21. | -0580 | 0.41 .5 |  | \% | * | , |  | W |  |  |  | , |  |  |
| 93 | 1.2D + 1...Yes | Y |  | DL 1.2 | 6. | -. 058 | 22. | -.0580 | OL4 1.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 94 | 12D + 1. Yes | , Y |  | DL 1.2 | 7. | 058 | 23. | -0580 | 0.41 .5 |  |  | $\cdots$ |  |  | , |  |  |  |  |  |  |
| 95 | $1.2 \mathrm{D}+1 . . \mathrm{Yes}$ | $Y$ |  | DL 1.2 | 8 | -. 058 |  | -. 0580 | OL. 41.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 96. | 1.2D + 1. Yes | , Y |  | DL 1.2 | 9 . | . 058 | 25. | . 0580 | 01.415 | : | , |  |  |  |  | 4 |  | * | 4. |  | $\cdots$ |
| 97 | 1.2D $+1 . .$. Yes | $Y$ |  | DL 1.2 | 10 | . 058 |  | -. 0580 | OL. 41.5 |  |  |  |  |  |  |  |  |  |  |  |  |
| 98 | 122+1.. Yes | \% $Y$ |  | DL 1.2 | 11. | .058. |  | . 0580 | OL4 1.5 |  |  | , |  |  | $\cdots$ |  |  |  | , |  |  |

## Hot Rolled Steel Properties

| Label |  | E [ksi] | G [ksi] | Nu | Therm (11E.. Densitylkft. |  | Yieldiksi] |  | Fulksi] | Rt |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | A36 Gr. 36 | 29000 | 11154 | . 3 | . 65 | . 49 | 36 | 1.5 | 58 | 1.2 |
| 2 | A572 Gr. 50 | 29000 | 11154 | 4. 3 | +. 65 | . $\quad .49$ | 50 | . 1.1 | 65 | 1.1 |
| 3 | A992 | 29000 | 11154 | . 3 | . 65 | . 49 | 50 | 1.1 | 65 | 1.1 |
| 4. | A500 Gr, B RND | 29000 | 11154 | 3 | . 6.65 | . 527 | $\square 42$ | 1.4 | 58 | 1.3 |
| 5 | A500 Gr.B Rect | 29000 | 11154 | . 3 | . 65 | 527 | 46 | 1.4 | 58 | 1.3 |
| 6 | A53 Gr.B | 29000 | 11154 | $\square$ | . 65 | . 49 | 35. | 1.6 | 60 | 1.2 |
| 7 | A1085 | 29000 | 11154 | . 3 | .65 | . 49 | 50 | 1.4 | 65 | 1.3 |

## Hot Rolled Steel Section Sets

| Label |  | Shape | Type | Design List | Material | Design Rules A [in2] |  | IWv [in4] | Izz [in4] | J [in4] |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Platform Horzont. | PIPE 3.0 | Beam | Pipe | A53 Gr.B | Typical | 2.07 | 2.85 | 2.85 | 5.69 |
| 2 | Offsett Tube | HSS $4 \times 4 \times 4$ | Beam | SquareTube | A36 Gr. 36 | Typical | 3.37 | 7.8 | 7.8 | 12.8 |
| 3 | Offset Side Plate | $0.38 \times 6$ Pla... | Beam | RECT | A36 Gr. 36 | Typical | 2.28 | 027 | 6.84 | . 105 |
| 4 | Grating Angle | $12 \times 2 \times 3$ | Beam | Single Angle | A36 Gr 36 | Typical | 722 | . 271 | . 271 | 009 |
| 5 | Mount Pipe | PIPE 2.0 | Beam | Pipe | A53 Gr.B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 6. | Ofset End Plate | $0.5 \times 6$ Plate | Beam | RECT | A36 Gr 36 | Typical | 3 | . 063 | 9 | 237 |
| 7 | MOD HRK12-3HD | PIPE 2.5 | Beam | Pipe | A53 Gr.B | Typical | 1.61 | 1.45 | 1.45 | 2.89 |
| 8. | MODHRK12-3H... | $0.38 \times 6$ Pla. | Beam | RECT | A 36 Gr .36 | Typical | 2.28 | . 027 | 6.84 | 105 |
| 9 | MOD HRK12-3H... | L2.5x2.5x4 | Beam | Single Angle | A36 Gr. 36 | Typical | 1.19 | . 692 | . 692 | . 026 |
| 10 | MOD HRK12-3H. | PIPE 2.0 | Beam. | Pipe, | $A 53 \mathrm{Gr}$ B | Typical | 1.02 | . 627 | . 627 | 1.25 |
| 11 | MOD HSRK-35 | L3×3×4 | Beam | Pipe | A36 Gr. 36 | Typical | 1.44 | 1.23 | 1.23 | . 031 |


|  |  |  | 23007 | Lbyylin] | Lbzz[in] | Lcomp toplin |  |  | Kyy | Kzz | Cb | Function |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | M51 | Offseft Tube | 63.007 |  |  |  |  |  |  |  |  | Lateral |
| 2 | - M60 | Offselt Tube | 30,438 | , +3. | , | Lbyy | 3, |  | 縟 | $\cdots$ | \% | Lateral |
| 3 | M63 | Offsett Tube | 30.437 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 4 | M69. | Platiorm Ho: | 150 | , | W+ | Libys |  |  | 4 | , | W | Lateral |
| 5 | M72 | Platform Ho.. | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 6 | M75 | Platorm Ho. | 150 |  |  | Lbyy | \% | \% | , | $\checkmark$ | , | Lateral |
| 7 | M92 | Grating Angle | 50.542 |  |  | Lbviv |  |  |  |  |  | Lateral |
| 8 | M94 | Grating Angle | 50.542 | - |  | Liby | 2.x. | W24.3 |  | \% |  | Leieral |
| 9 | M98 | Grating Angle | 50.542 |  |  | Lbuy |  |  |  |  |  | Lateral |
| 10 | M100 | Grating Angle | 50.542 |  | WW. | Lbyy | 4 | 4. | 2. | W | \% | Cateral |
| 11 | M104 | Grating Angle | 50.542 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 12 | M106 | Gratiting Angle | 50.542 |  |  | Lbyy, | s. |  |  |  |  | Lateral |
| 13 | M160 | Mount Pipe | 84 |  |  | Lbyv |  |  |  |  |  | Lateral |
| 14 | M161 | Mount Pipe | 84 | \% | 3, | Lbyy | $3 \times$ | $\cdots$ | \% | $\cdots$ |  | Lateral |
| 15 | M162 | Mount Pipe | 84 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 16 | M163 | Mount Pipe | 84 | + |  | Lbyy | ${ }^{3}$ | , | 3 |  |  | Lateral |
| 17 | M245A | Offsett Tube | 30.438 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 18 | M246A | Offsett Tube | 30.437 | * | $\cdots$ | Lby | $4 \times$ |  | ${ }^{3}$ |  | \% | Lateral |
| 19 | M279 | Offsett Tube | 30.438 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 20 | M280 | Offsett Tưbe | 30:437 | 4 | W, | Lbyy | , | $\cdots$ | \% | $\cdots$ |  | Lateral |
| 21 | M242A | Offsett Tube | 63.007 |  |  | Lby | - |  |  |  |  | Lateral |
| 22 | M243A | Offsetr Tube | 63.007 | $\cdots$ | $\cdots$ | Weray |  | $\cdots$ | . |  |  | Lateral |
| 23 | M232A | Mount Pipe | 84 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 24 | M233A | Mount Pipe | 84 |  | + | Lbyy |  | , |  | * |  | Lateral |
| 25. | M234A | Mount Pipe | 84 |  |  | Lbyv |  |  |  |  |  | Lateral |
| 26. | M235A | Mount Pipe | 84 |  | $\cdots$ | Lbyy |  |  |  |  |  | Lateral |
| 27. | M240A | Mount Pipe | 84 |  |  | Lbyv |  |  |  |  |  | Lateral |
| 28. | M241A | Mount Pipe | 84 | , | $\cdots$ | Lbyy | T ${ }^{2}$ | \% | 4 |  |  | Lateral |
| 29 | M242B | Mount Pipe | 84 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 30 | M243B | Mount Pripe | 84 | M, |  | Lbyy | \% ${ }^{\text {a }}$ |  | . | , |  | Lateral |
| 31 | M272A | MOD HRK1..) | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 32 | M275A | MOD HRK1. | 5 | - | 4 | Lbyy. | , |  | . | $\cdots$ |  | Lateral |
| 33 | M278A | MOD HRK1... | 5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 34 | M283A | MOD HRK1, | 150 |  |  | Lbyy |  |  | $\checkmark$ |  |  | Lateral |
| 35 | M286A | MOD HRK1.. | 5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 36. | M289A | MOD HRK1. | 5 |  |  | Lbyy |  |  |  |  | . | Lateral |
| 37. | M294A | MOD HRK1.. | 150 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 38. | M297A | MOD HRK1. | 5 | W. | 4. | Lbyy |  |  |  | $\triangle$ |  | Lateral |
| 39 | M300B | MOD HRK1.. | 5 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 40. | M301B | MOD HRK1. | 13.155 | - |  | Lbyy |  |  | ${ }^{4}$ | . |  | Lateraial |
| 41 | M302B | MOD HRK1. | 13.155 |  |  | Lbyy |  |  |  |  |  | Lateral |
| 42 | M303B | MOD HRK1. | 13.155 | 4 | W, \% | Lbyy | N | , |  |  | T | Lateral |
| 43 | M310B | MOD HRK1.. | 56.619 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 44. | M311B | MOD HRK1. | 56.619 |  | $\cdots$ | Lbyy |  | $\cdots$ | $\checkmark$ |  |  | Lateral |
| 45 | M312B | MOD HRK1.. | 56.619 |  |  | Lbiy |  |  |  |  |  | Lateral |
| 46 | M320. | MOD HSRK. | 56.759 | 27) | $\cdots$ | Lbyy | $4 \times$ |  |  |  |  | Lateral |
| 47 | M322 | MOD HSRK. | 56.759 |  |  | Lbuy |  |  |  |  |  | Lateral |
| 48. | M324 | MOD HSRK. | 56.759 |  |  | Lbyy | , | * |  |  |  | Lateral |
| 49 | M326 | MOD HSRK.. | 56,759 |  |  | Lbvy |  |  |  |  |  | Lateral |
| 50 | M328 | MOD HSRK. | 56.759 |  | , | Lbyy | \% | $\cdots$ |  |  |  | Lateral |
| 51 | M330 | MOD HSRK... | 56.759 |  |  | Lbyy |  |  |  |  |  | Lateral |


|  | Joint |  | $\times$ [ [b] | LC | Y $[1 \mathrm{lb]}$ |  | Z [ilb] | LC | MX [lib-ft] | LC |  | LC | MZ [lib-ft]. | LC |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | N88 | max | 2363.215 | 3 | 1743.592 | 15 | 2895.693 | 19 | 2091.225 | 7 | 6207.49 | 3 | 1496.137 | 7 |
| 2 | - | min | -3253.827 | 17 | 1745.306 | 7 | -721.06 | 11 | 2327.94 | 15 | 4303.569 | 11 | -1524.983 | 15 |
| 3 | N1203B | max | 2233.289 | 3 | 2012.2 | 14 | 3303.292 | 30 | 3419.442 | 6 | 2606.576 | 4 | 1680.908 | 18 |
| 4 | ${ }^{1}$ | min | -1769.594 | 11. | -2775.58 | 6 | -485.694 | 6. | -5675.354 | 14 | -3951.803 | 12 | -1697.422 | 10 |
| 5 | N1205B | max | 1897.733 | 3 | 2874.979 | 16 | 2996.068 | 24 | 5291.557 | 8 | 2625.067 | 18 | 1653.475 | 12 |
| 6. | $\stackrel{1}{ }$ | min. | -1470.811 | 11. | 2108.08 | 8 | -764.717 | 16. | -3815.503 | 16 | $-3678.112$ | 10 | -1657.214 | 4 |
| 7 | Totals: | max | 6494.237 | 3 | 6464.203 | 15 | 7944.743 | 20 |  |  |  |  |  |  |
| 8. | Nax | min | -6494.233 | 11 | -6464.239 | 7. | 2355.688 | 1. | 23N M M |  |  | +1. | W, | \% |

## Envelope AISC 14th(360-10): LRFD Steel Code Checks

| 1 Member |  | Shape Code Check |  | Loc[in] |  | Shear Che .271 | $\frac{\text { Loclin_DirLC }}{2} \frac{\mathrm{z}}{10}$ |  | Cphi*Pnc...phi*Pnt ...phi* ${ }^{\text {Mn }}$...phi* Mn ...Cb Eqn |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | HSS4x4x4 | . 532 | 0 | 14 |  |  |  | 99760.9.1 109188 | 12663 | 12663 2. | 2.. $\mathrm{H} 1-1 \mathrm{~b}$ |
| 2 | M243A. | HSS $4 \times 4 \times 4$ | 508 | 0 | 8. | 278 | 0 | z 12 | 299760.9.109188 | 12663 | 12663 | H1-1b |
| 3 | M51 | HSS4x4x4 | . 508 | 0 | 3. | . 276 | 0 | z 15 | 99760.9.1109188 | 12663 | 126632 | H1-1b |
| 4 | M240A | PIPE 2.0 | . .391 | 77,368 | 12 | . 075 | 28.7. | 6 | 17855.0. 32130 | 1871.62 | 1871.6252 | . 111 l |
| 5 | M160 | PIPE 2:0 | . 380 | 77.368 | 7 | . 075 | 28.7... | 16 | 17855.0.. 32130 | 1871.62 | 1871.6252 | H1-1b |
| 6. | M161 | PIPE 2.0 | 365 | 77.368 | 15 | . 062 | 77.3. | 17 | 17855.0.. 32130 | 1871.6 | 1871.6252 | 1b |
| 7 | M232A | PIPE 2.0 | . 360 | 77.368 | 18 | . 075 | 28.7... |  | 117855.0 .32130 | 1871.6 | 1871.625 2 | 1 b |
| 8. | M241A. | PIPE 20 | . 352 | 77.368 | 4. | 059 | 77.3. | 6 | 17855.0. 32130 | 1871.6 | 1871.6252 | -111 |
| 9 | M233A | PIPE 2.0 | . 346 | 77.368 | 9 | . 058 | 77.3... | 11 | 177855.0 .132130 | 1871.6 | 1871.6252. | H1-1b |
| 10 | M243B | PIPE 2.0 | . 301 | 77,368 | 13 | 073 | 77.3.\% | 14 | 178550.32130 | 1871.6 | 18716252 | H1-1b |
| 11 | M163 | PIPE 2.0 | 300 | 77.368 | 8 | . 075 | 77.3... | 9 | 17855.0. 32130 | 1871.6 | 1871.6252. | H1-1b |
| 12 | M162 | PIPE 20 | 290 | 77,368 | 14. | 075 | 28.7. | 6 | 17855.0. 32130 | 187162 | 1871,6252. | .11-1b |
| 13 | M235A | PIPE 2.0 | 289 | 77.368 | 3 | . 075 | 77.3... | 3 | 17855.0.. 32130 | 1871.62 | 1871.6252. | $\ldots+1-1 b$ |
| 14 | M294A. | PIPE 2.5 | 276 | 47.368 | 11 | 146 | 55.2 | 9. | 14558.7. 50715 | 3596.25 | 3596.252. | H1-1b |
| 15 | M245A | HSS $4 \times \times 4 \times 4$ | . 276 | 30.438 | 13 | . 100 | 3.204 | z 3 | 106911... 109188 | 12663 | 12663 1.. | H1-1b |
| 16 | M272A | PIPE 2.5 | . 272 | 47.368 | 6 | 151 | 55.2. | 4. | 14558.7 .50715 | 3596.25 | 3596,252. | . 11.16 |
| 17 | M242B | PIPE 2.0 | 267 | 77.368 | 3 | . 075 | 28.7... | 11 | 17855.0., 32130 | 1871.62 | 1871.6252. | H1-1b |
| 18 | M283A. | PIPE 2.5 | 266 | 47.368 | 16 | 146 | 55.2 | 15 | 14558.7. 50715 | 3596.25 | 3596.252 | , 1 1-1b |
| 19 | M246A | HSS $4 \times 4 \times 4$ | 264 | 0 | 15 | . 095 | 27.2. | z 9 | 106911... 109188 | 12663 | 126631. | H1-1b |
| 20 | M60 | HSS $4 \times 4 \times 4$ | 263 | 30.438 | 18 | . 094 | 3.204 | Z. 8 | 106911.109188 | 12663 | 126631. | H1-1b |
| 21 | M279 | HSS $4 \times 4 \times 4$ | 258 | 30.438 | 7 | . 104 | 3.204 |  | 106911...109188 | 12663 | 12663 1.. | . $\mathrm{H} 1-1 \mathrm{~b}$ |
| 22 | M280 | HSS $4 \times 4 \times 4$ | 255 | 0 | 9 | . 092 | 27.2. | 23 | 106911.409188 | 12663 | 126631. | H1-1b |
| 23 | M63 | HSS $4 \times 4 \times 4$ | . 252 | 0 | 4 | . 095 | 27.2 |  | 106911...109188 | 12663 | 126631. | H1-1b |
| 24 | M234A | PIPE 2.0 | . 248 | 77,368 | 8 | . 075 | 28.7. |  | 17855.0. 32130 | 1871.625 | 1871.625 2 | 1-1b |
| 25 | M75 | PIPE 3.0 | . 204 | 90.789 | 13 | . 086 | 90.7 |  | 28250.5.. 65205 | 5748.75 | 5748.75 2. | H1-1b |
| 26 | M72 | PIPE 3.0 | . 191 | 90.789 | 3 | 085 | 59.2 |  | 28250.5.65205 | 5748.75 | 5748.752 | 11-16 |
| 27. | M69 | PJPE 3.0 | . 185 | 90.789 | 8 | . 089 | 134... | 3 | 28250.5., 65205 | 5748.75 | 5748.75 2... | H1-1b |
| 28 | M104 | L2 $2 \times 2 \times 3$ | 158 | 0 | 16. | 007 | 0 | 28 | 9618,888 233928 | 557.717 | 1196.2131. | H 2 l |
| 29 | M100 | L2x2x3 | 156 | 0 | 11 | . 008 | 0 | v 3 | 9618.956 23392.8 | 557.717 | 1178.909 $1 .$. | H2-1 |
| 30 | M92 | L2×2×3 | - 152 | 0 | 11 | . 007 | 0 | 23 | 9618.888823392 .8 | 557.717 | 163.9311. | H 21 |
| 31. | M98 | $12 \times 2 \times 3$ | . 147 | 0 | 6 | . 007 | 0 | z 6 | 9618.888823392 .8 | 557.717 | $1171.4171 .$. | H2-1 |
| 32 | M106 | L2x2×3 | 141 | 0 | 6 | . 007 | 0 | y 14 | 9618.95623392 .8 | 557.717 | 146,161. | $\mathrm{H} 2-1$ |
| 33 | M94 | L2x2x | 141 | 0 | 16 | . 007 | 0 | V 8 | 9618.956 23392.8 | 557.717 | 1133.0261 .. | H2-1 |
| 34. | M301B | 12.5×2.5x4 | 130 | 13.155 | 18. | . 044 | 0 | y 4 | 37073,2, 38556 | 1113,554 | 25373881. | H2-1 |
| 35 | M289A | $0.38 \times 6$ PI... | . 130 | 2.5 | 18 | . 019 | 1.053 | z 18 | 66218.6.. 73872 | 584.82 | 9234 1.. | . H 1-1b |
| 36. | M302B | $12.5 \times 2.5 \times 4$ | 128 | 0 | 9 | . 043 | 0 | $\bigcirc 7$ | 37073,2, 38556 | 1113.554 | 2537,3881 | H2-1 |
| 37 | M286A | $0.38 \times 6 \mathrm{Pl} .$. | . 126 | 2.5 | 9 | . 019 | 1.053 | z 9 | 66218.6 .173872 | 584.82 | 9234 1... | H2-1b |
| 38. | M303B | $2.5 \times 2.5 \times 4$ | 1117 | 0 | 4 | . 040 | 0 | Y 10 | 37073.2. 38556 | 1113.554 | 2537.3881. | H 21 |
| 39 | M297A | $0.38 \times 6 \mathrm{Pl} . .$. | . 116 | 2.5 | 4 | . 018 | 1.053 | $z 4$ | 66218.6. 73872 | 584.82 | 9234 1.. | H1-1b |
| 40. | M278A | $0.38 \times 6 \mathrm{Pl}$. | 110 | 2.5 | 7 | 017 | 1.053 | 27 | 66218.6. 73872 | 584.82 | 9234.1. | H1-1b |
| 41 | M275A | $0.38 \times 6$ Pl... | . 103 | 2.5 | 14 | . 015 | 1.053 | z 14 | 66218.6 .173872 | 584.82 | 92341. | H1-1b |
| 42 | M300B | $0.38 \times 6 \mathrm{P}$. | 102 | 2.5 | 13 | . 016 | 1.053 | z113 | 66218.6. 73872 | 584.82 | 9234, 1. | H1-1b |
| 43 | M322 | L $3 \times 3 \times 4$ | . 066 | 26.886 | 3 | . 009 | 0 | y 15 | 28423.7.. 46656 | 1688.138 | 3426.651 $1 .$. | H2-1 |


| Member |  | Shape | Code Check Lociin] |  |  | $\begin{aligned} & \text { Shear Che } \\ & 0.009 \end{aligned}$ | $\frac{\mathrm{Loc} / \mathrm{in}}{} \mathrm{O}$ | $\begin{aligned} & \text { DirLC phi*Pnc. } \\ & y 10284237 . \end{aligned}$ |  | $\frac{\text { phi*Pnt }}{46656}$ | phi* Mn ...phi* Mn ...Cb Ean 1688.1383426.651 11. H2-1 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 44 | M326 | $43 \times 3 \times 4$ | 1. 064 | 26.886 | 14 |  |  |  |  |  |  |  |
| 45 | M330 | L $3 \times 3 \times 4$ | . 063 | 26.886 | 8 | . 0.009 | - | v 4 | 4 28423.7.. | 4 | 1688.138 3426.6511. |  |
| 46 | M328 | $13 \times 3 \times 4$ | . 062 | 28.38 | 11 | . 010 | 0 |  | 228423.7 . | 46656 | 1688.1383426 .6511 | - |
| 47. | M324 | $13 \times 3 \times 4$ | . 061 | 28.38 | 17 | . 010 | 56.7... | z 18 | 828423.7.1. | 46656 | 1688.138 3426.6511. | H2-1 |
| $\frac{48}{49}$ | M320 | L13x3x4 | 059 | 28.38 | 6. | . 010 | 1, 0 |  | 28423.7. | 46656 | 1688.1383426.6511. | $\xrightarrow{\mathrm{H} 2-1}$ |
| 49 | M310B | PIPE 2.0 | 036 | 28.31 | 22 | . 022 | 0 |  | 8124603.0. | 32130 | 1871.6251871.6251. | H1-1b |
|  |  | PIPE 2.0 | 035 | 28.31 | 32 | . 020 | 56.6. |  | 24603.0. | 32130 | 1871.6251871.6251. | 1-1b |
| 5 | M311B | PIPE_2.0 | . 035 | 28.31 | 27 | . 022 | 0 |  | 24603.0., | 32130 | 1871.625/1871.625/1.. | H1-1b |

## Envelope Plate/Shell Principal Stresses

| Plate |  |  | Sigma1 [ksi] LC |  |  | $\frac{\text { Sigma2 [ksi] }}{1.103}$ | 0 | $\frac{\text { Tau Max }[\mathrm{ksi]}}{6.016}$ |  | Angle [rad] | LC Von Mises [ksil LC |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1. | P726 | max | T | 11.178 | 10 |  |  |  |  | 2.081 | 74 | 12.718 | 18 |
| 2. | , | min |  | -1.339 | 82 | -13.308 | 18 | W. 092 | 25 | 2. 367 | 27 | 212.718 | 25 |
| 3 |  | max | B | 7.395 | 18 | 1.542 | 18 | 2.926 | 18 | 2.297 | 53 | 6.757 | 18 |
| 4 | \% | min |  | 1,328 | 10 | 6. 6.355 | 10 | . 0.097 | 25 | $\underline{4.771}$ | 52 | 236. | $\frac{18}{25}$ |
| 5 | P531 | max | T | 14.286 | 14 | 4.41 | 14 | 4.938 | 14 | 2.13 | 19 | 12.671 | 14 |
| $\begin{array}{r}6 \\ \hline 7\end{array}$ |  | min |  | -4.016 | 6. | -12.974 | 6 | W. 024 | 50 | . 559 | 28 | 12,042 | 50 |
| 8 |  | max | B | 15.002 | 6 | 4.351 | 6 | 5.841 | 14 | 2.307 | 55 | 14.67 | 14 |
| 8 | 30 | min |  | -4.782 | 14 | 16.464 | 14 | 038. | 19 | 4.751 | 53 | . 08 | 53 |
| 9 | P436 | max | T | 14.104 | 3 | 4.35 | 3 | 4.877 | 3 | 1.634 | 24 | 12.51 | 3. |
| 10 |  | min |  | -4.099 | 11 | -13.223 | 11 | 02 | 48 | -195 | 7. | . 034 | 48 |
| 11 |  | max | B | 15.42 | 11 | 4.468 | 11 | 5.68 | 3 | 1.642 | 31 | 14.287 | 3 |
| $\frac{12}{13}$ |  | min |  | -4.681 | 3 | -16.04 | 3. | 075 | 65 | $\cdot 167$ | 15 | . 131 | 65 |
| $\frac{13}{14}$ | P798 | max | T | 9.64 | 4 | 748 | 4 | 5.886 | 13 | 2.142 | 9 | 12.322 | 13 |
| 14 |  | min. |  | -1.043 | 12 | -12.807 | 13. | 524 | 18 | -4.48 | 8 | 951 | 18 |
| 16. |  | $\max$ | B | 6.76 | 13 | 1.316 | 12 | 2.725 | 13 | 1.901 | 3 | 6.21 | 13 |
| 17 | P627 | max | T | $\underline{.963}$ | 4 | -5.105 | 5 | 196 | 69 | . 102 | 18 | 413 | 69 |
| 18 |  | min |  | 4.255 | 8 | 4.037 | 8 | 4.76 | 16 | 2.298 | 52 | 12.216 | 16 |
| 19 |  | max | B | 15.83 | 16 | -13. | 16 | , ,024 | 87. | 4.767 | 45 | 044 | 87 |
| 20 |  | min. |  | 4.401 | 8 | $\frac{4.586}{15.258}$ | 16 | 5.622 | 16 | 2.337 | 35 | 14.107 | 16 |
| 21 | P515 | max | T | 13.319 | 14 | 4.098 | 14 | 1.022 4.61 | 91 | 4.686 | 47. | . 044 | 91 |
| 22. | , + ${ }^{\text {a }}$ | min. |  | -3.732 | 6 | -12.103 | 6. | 4.61 | 14 | 2.121 | 19 | 11.815 | 14 |
| 23 |  | max | B | 12.798 | 6 | 3.905 | 6 |  | 54. | -23 | 28 | . 07 | 54 |
| 24. |  | min |  | 4.295 | 14 | -14.053 | 14 | 03 | 14 | 2.204 | 50 | 12.473 | 14 |
| 25 | P655 | max | T | 10.945 | 15 | . 946 | 15 | 5.557 | 19 | -. 591 | 42. | . 078 | 19 |
| 26 |  | min |  | -1.218 | 7 | -12.332 | 7 | 5.557 | 7 | 2.201 | 63 | 11.77 | 7 |
| 27. |  | max | B | 6.911 | 7 | 1.46 | 7 | 2.726 | 84 | -68 | 82 | ,066 | 84 |
| 28. |  | min |  | -1.179 | 15 | -5.864 | 15 | 2.7206 | 72 | 2.218 | 83 | 6.31 | 7 |
| 29 | P526 | max | T | 13.171 | 14 | 4.076 | 14 | 4.548 | 32 | -75 | 93 | 077 | 84. |
| 30 |  | min |  | -3.675 | 6 | -11.877 | 6 |  | 14 | 2.271 | 18 | 11.68 | 14 |
| 31 |  | $\max$ | B | 13.972. | 6 | 4.014 | 6 | 78 | 35 | . 049 | 17 | 0116 | 35 |
| 32 |  | min |  | -4.463 | 14 | -15.419 | 14 |  | 14 | 2.163 | 40 | 13.742 | 14 |
| 33 | P622 | max | T | 13.072 | 8 | 4.041 | 8 | . 07.3 | 35. | - 556 | 9 | 139 | 35 |
| 34 |  | min. |  | -3.717 | 16 | -11.971 | 16 | 4.516 | 8 | 2.126 | 12 | 11.592 | 8 |
| 35 |  | $\max$ | B | 14.251 | 16 | 4.096 | 16 | 021 | 81. | -693 | 80 | 036 | 81 |
| 36 | P $\quad$, | min |  | 4.382 | 8 | 115.052 | 8 |  | 8 | 2.176 | 29 | 13.409 | 8 |
| 37 | P420 | max | T | 12.974 | 3 | 3.994 | 3 | 4.49 | $\frac{90}{3}$ | -484 | 86 | 066 | 78. |
| 38 | $\cdots$ | min |  | -3.806 | 11 | -12.355 | 11 |  | $\frac{3}{54}$ | 1.6 | 24 | 11.509 | 3 |
| 39 |  | max | B | 13.096 | 11 | 3.998 | 11 |  | $\frac{54}{3}$ | -193 | 7 | 007 | 54. |
| 40 |  | min |  | -4.173 | 3 | -13.657 | 3 | 4.742 | 3 | 1.66 | 31 | 12.121 | 3 |
| 41 | P611 | $\max$ | T | 12.462 | 8 | 3.833 | 8 | 4.46 | 67 | -321 | 15 | . 054 | 67 |
| 42 | , | min |  | -3.982 | 16 | -12.903 | 16 | 017 | $\frac{16}{68}$ | 2.353 | 46 | 11.444 | 16 |
| 43 |  | max | B | 13.604 | 16 | -12.903 | 16 | 4.727 | 68 | $\frac{-753}{2.31}$ | 44 | 12032 | $\frac{68}{16}$ |
| 44 | 凹, , | min | , 1 | 4.021 | 8 | -13.156 | 8 | . 022 | 53 | $\begin{array}{r}2.31 \\ \hline 753\end{array}$ | 36 | 12.076 | $\frac{16}{53}$ |

## APPENDIX D

## ADDITIONAL CALCUATIONS



$\stackrel{14}{ }$



4. .


## APPENDIX E

MOUNT MODIFICATION DESIGN DRAWINGS (MDD) / SUPPLEMENTAL DRAWINGS



## MOUNT MODIFICATION <br> DRAWINGS




BETHANY
$\begin{gathered}\text { CROWN CASTLE BU\#: } 84295 \\ \text { VERIZON SITE\#: 104335 }\end{gathered}$
STRUCTURE INFORMATION
150' MONOPOLE TOWER
LOW PROFILE PLATFORM


द5नान

$$
\begin{gathered}
\text { SITE ADDRESS } \\
\text { 719 AMITY ROAD } \\
\text { BETHANY, CT O6524 } \\
\text { NEW HAVEN COUNTY } \\
\text { LATITUDE: N } 41^{\circ} 26^{\prime} 33.93^{\prime \prime} \pm \\
\text { LONGITUDE: } 72^{\circ} 59^{\prime} 32.86^{\prime \prime} \pm
\end{gathered}
$$







## DJ PAUL J. FORD \& COMPANY

Date: June 06, 2019
Denise Nicholson
Crown Castle
3 Corporate Dr, Suite 101
Clifton Park, NY 12065

Paul J. Ford and Company 250 East Broad St., Suite 600 Columbus, OH 43215 (614) 221-6679

Subject:
Carrier Designation:

Crown Castle Designation:

Engineering Firm Designation:
Site Data:


Dear Denice Nicholson,
Paul J. Ford and Company is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

## LC7: Proposed Equipment Configuration

## Sufficient Capacity (73.9\%)

This analysis utilizes an ultimate 3-second gust wind speed of 125 mph as required by the 2018 Connecticut State Building Code and Appendix N. Applicable Standard references and design criteria are listed in Section 2 Analysis Criteria.

Respectfully submitted by:


Aaron E. Pike, E.I.
Structural Designer apike@pauljford.com


06/07/2019

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## 1) INTRODUCTION

This tower is a 151 ft Monopole tower designed by VALMONT and mapped by FDH in March of 2016.
The tower has been modified per reinforcement drawings prepared by B+T in February of 2012. Reinforcement consist of flat plate reinforcing, post-installed anchor rods, and foundation augmentation.
The tower has been modified per reinforcement drawings prepared by B+T in July of 2012. Reinforcement consist of shaft reinforcing.
2) ANALYSIS CRITERIA

TIA-222 Revision:
Risk Category:
Wind Speed:
Exposure Category:
Topographic Factor:
Ice Thickness:
Wind Speed with Ice:
Service Wind Speed:

TIA-222-H
II
125 mph
B
1
1.5 in

50 mph
60 mph

Table 1 - Proposed Equipment Configuration

| Mounting Level (ft) | Center Line Elevation (ft) | $\left\|\begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array}\right\|$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | $\left\|\begin{array}{c} \text { Feed } \\ \text { Line } \\ \text { Size }(\text { in) } \end{array}\right\|$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 140.0 | 140.0 | 6 | commscope | NHH-65C-R2B w/ Mount Pipe | 13 | 1-5/8 |
|  |  | 3 | decibel | DB854DG65ESX w/ Mount Pipe |  |  |
|  |  | 1 | rfs celwave | DB-T1-6Z-8AB-0Z |  |  |
|  |  | 3 | samsung telecommunications | RFV01U-D1A |  |  |
|  |  | 3 | $\begin{array}{\|c\|} \hline \text { samsung } \\ \text { telecommunications } \end{array}$ | RFV01U-D2A |  |  |
|  |  | 1 | tower mounts | 12.5 ft Low Profile Platform |  |  |
|  |  | 1 | site pro 1 | Handrail Kit [HRK12-3HD] |  |  |
|  |  | 3 | site pro 1 | Kicker Kit [HSRK-35] |  |  |

Table 2-Other Considered Equipment

| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{gathered} \begin{array}{c} \text { Number } \\ \text { of } \\ \text { Antennas } \end{array} \end{gathered}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | $\begin{aligned} & \text { Feed } \\ & \text { Line } \\ & \text { Size (in) } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 148.0 | 160.0 | 1 | dbspectra | DS1F03F36D-N | $\begin{gathered} 12 \\ 2 \\ 2 \\ 2 \\ 2 \end{gathered}$ | $\begin{gathered} 1-5 / 8 \\ 7 / 8 \\ 5 / 8 \\ 3 / 8 \\ 2^{\prime \prime} \text { cond. } \end{gathered}$ |
|  | 149.0 | 6 | adc | CG-1900DD-FULL-DIN |  |  |
|  |  | 6 | communication components inc. | DTMABP7819VG12A |  |  |
|  |  | 6 | ericsson | RRUS-11 |  |  |
|  |  | 3 | kathrein | 80010121 w/ Mount Pipe |  |  |
|  |  | 3 | kathrein | 86010025 |  |  |
|  |  | 6 | $\begin{gathered} \mathrm{kmw} \\ \text { communications } \end{gathered}$ | $\begin{aligned} & \text { AM-X-CD-16-65-00T-RET w/ } \\ & \text { Mount Pipe } \end{aligned}$ |  |  |
|  |  | 12 | powerwave technologies | LGP21901 |  |  |
|  |  | 1 | raycap | DC6-48-60-18-8F |  |  |
|  | 148.0 | 1 | tower mounts | Platform Mount [LP 602-1] |  |  |


| Mounting Level (ft) | Center Line Elevation (ft) | $\begin{gathered} \text { Number } \\ \text { of } \\ \text { Antennas } \end{gathered}$ | Antenna Manufacturer | Antenna Model | Number of Feed Lines | Feed Line Size (in) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 132.0 | 132.0 | 1 | tower mounts | Pipe Mount [PM 601-3] | -- | -- |
|  | 131.0 | 3 | alcatel lucent | 800 EXTERNAL NOTCH FILTER |  |  |
|  |  | 3 | alcatel lucent | 800MHZ RRH |  |  |
|  |  | 3 | alcatel lucent | TME-1900MHZ RRH |  |  |
| 130.0 | 133.0 | 1 | pctel | GPS-TMG-HR-26NCM | $\begin{aligned} & 1 \\ & 3 \\ & 1 \end{aligned}$ | $\begin{gathered} 1 / 2 \\ 1-5 / 8 \\ 1-1 / 4 \end{gathered}$ |
|  | 130.0 | 3 | alcatel lucent | TD-RRH8X20-25 |  |  |
|  |  | 3 | rfs celwave | APXVSPP18-C-A20 w/ Mount Pipe |  |  |
|  |  | 3 | rfs celwave | APXVTM14-C-120 w/ Mount Pipe |  |  |
|  |  | 1 | tower mounts | T-Arm Mount [TA 602-3] |  |  |
| 122.0 | 123.0 | 3 | ericsson | ERICSSON AIR 21 B2A B4P w/ Mount Pipe | 7 | 1-5/8 |
|  |  | 3 | ericsson | RADIO 4449 B12/B71 |  |  |
|  |  | 3 | rfs celwave | APXVAARR24_43-U-NA20 w/ Mount Pipe |  |  |
|  | 122.0 | 1 | tower mounts | T-Arm Mount [TA 702-3] |  |  |

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| 4-GEOTECHNICAL REPORTS | FDH, 15BBNL1600, 2/18/2016 | 6133952 | CCISITES |
| 4-TOWER FOUNDATION <br> DRAWINGS/DESIGN/SPECS | FDH, 16BBMT1500, 2/17/2016 <br> (mapped) | 6133920 | CCISITES |
| 4-TOWER MANUFACTURER <br> DRAWINGS | FDH, 16BBMW1500, 3/11/2016 <br> (mapped) | 6133951 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | B+T, 83154.003A, 2/21/2012 | 5135907 | CCISITES |
| 4-POST-MODIFICATION <br> INSPECTION | B+T, 83154.004, 8/3/2012 | 5135928 | CCISITES |
| 4-TOWER REINFORCEMENT <br> DESIGN/DRAWINGS/DATA | B+T, 84427.0002, 7/19/2012 | 4945157 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 8.0.5.0), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases.
Selected output from the analysis is included in Appendix A.
tnxTower was used to determine the loads on the modified structure. Additional calculations were performed to determine the stresses in the pole and in the reinforcing elements. These calculations are presented in Appendix C.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
4) Tower was modified in accordance with the referenced modification documents.
5) The rebar in the pad portion of the original foundation is unknown. In this analysis, it is assumed that the rebar at the top and bottom of the pad is consistent with the rebar added per PMI document \#5135928 (\#7 spaced 12" O.C.).
6) The monopole manufacturer drawings are not available at the time of this analysis. Therefore, we have assumed the steel yield strength(s) (Fy) as per the following:
a) Anchor rods: ASTM A615 (Fu = $100 \mathrm{ksi}, \mathrm{Fy}=75 \mathrm{ksi}$ )
b) Pole Shaft: ASTM A572 Gr 65
c) Base Plate: ASTM A572 Gr 50
7) The existing base plate grout was considered in this analysis. Grout must be maintained and inspected periodically and must be replaced if damaged or cracked. Refer to Crown Castle document ENG-PRC-10012, Base Plate Grout Repair.
This analysis may be affected if any assumptions are not valid or have been made in error. Paul J. Ford and Company should be notified to determine the effect on the structural integrity of the tower.
8) ANALYSIS RESULTS

Table 4 - Section Capacity (Summary)

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 151-146 | Pole | TP18.526×17.59x0.2188 | Pole | 5.6\% | Pass |
| 146-141 | Pole | TP19.461×18.526x0.2188 | Pole | 11.9\% | Pass |
| 141-136 | Pole | TP20.397x19.461x0.2188 | Pole | 23.1\% | Pass |
| 136-131 | Pole | TP21.332×20.397×0.2188 | Pole | 33.7\% | Pass |
| 131-126 | Pole | TP22.268×21.332x0.2188 | Pole | 45.6\% | Pass |
| 126-125.5 | Pole | TP22.361x22.268x0.2188 | Pole | 46.7\% | Pass |
| 125.5-125.25 | Pole + Reinf. | TP22.408×22.361x0.3626 | Reinf. 11 Tension Rupture | 40.8\% | Pass |
| 125.25-120.25 | Pole + Reinf. | TP23.343x22.408x0.3563 | Reinf. 11 Tension Rupture | 51.2\% | Pass |
| 120.25-118.5 | Pole + Reinf. | TP23.671x23.343x0.3563 | Reinf. 11 Tension Rupture | 54.8\% | Pass |
| 118.5-118.25 | Pole + Reinf. | TP23.718x23.671x0.6438 | Reinf. 9 Bolt-Shaft Bearing | 33.5\% | Pass |
| 118.25-117.5 | Pole + Reinf. | TP23.858×23.718x0.6438 | Reinf. 9 Tension Rupture | 33.7\% | Pass |
| 117.5-117.25 | Pole + Reinf. | TP23.905×23.858×0.4938 | Reinf. 9 Tension Rupture | 42.9\% | Pass |
| 117.25-112.25 | Pole + Reinf. | TP24.84×23.905×0.4813 | Reinf. 9 Tension Rupture | 50.4\% | Pass |
| 112.25-107.25 | Pole + Reinf. | TP25.776x24.84x0.4688 | Reinf. 9 Tension Rupture | 57.4\% | Pass |
| 107.25-102.25 | Pole + Reinf. | TP26.711 $25.776 \times 0.4563$ | Reinf. 9 Tension Rupture | 63.8\% | Pass |
| 102.25-100.92 | Pole + Reinf. | TP27.6x26.711×0.4563 | Reinf. 9 Tension Rupture | 65.4\% | Pass |
| 100.92-95.92 | Pole + Reinf | TP27.459x26.523x0.55 | Reinf. 9 Tension Rupture | 60.5\% | Pass |
| 95.92-92.5 | Pole + Reinf. | TP28.098×27.459x0.55 | Reinf. 9 Tension Rupture | 63.6\% | Pass |
| 92.5-92.25 | Pole + Reinf. | TP28.145x28.098×0.55 | Reinf. 8 Tension Rupture | 63.8\% | Pass |
| 92.25-87.25 | Pole + Reinf. | TP29.08×28.145x0.5375 | Reinf. 8 Tension Rupture | 67.9\% | Pass |
| 87.25-87 | Pole + Reinf. | TP29.127×29.08×0.625 | Reinf. 7 Tension Rupture | 58.4\% | Pass |
| 87-82 | Pole + Reinf. | TP30.063×29.127×0.6125 | Reinf. 7 Tension Rupture | 61.9\% | Pass |
| 82-77 | Pole + Reinf. | TP30.998×30.063×0.6 | Reinf. 7 Tension Rupture | 65.2\% | Pass |
| 77-72 | Pole + Reinf. | TP31.934×30.998×0.5875 | Reinf. 7 Tension Rupture | 68.2\% | Pass |
| 72-67 | Pole + Reinf. | TP32.869×31.934×0.575 | Reinf. 7 Tension Rupture | 71.1\% | Pass |


| Elevation ( ft ) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 67-63.25 | Pole + Reinf | TP33.571×32.869×0.575 | Reinf. 7 Tension Rupture | 73.1\% | Pass |
| 63.25-63 | Pole + Reinf. | TP33.618x33.571x0.575 | Reinf. 6 Tension Rupture | 73.3\% | Pass |
| 63-58 | Pole + Reinf. | TP34.553×33.618×0.5625 | Reinf. 6 Tension Rupture | 75.8\% | Pass |
| 58-56.75 | Pole + Reinf. | TP34.787x34.553x0.5625 | Reinf. 6 Tension Rupture | 76.4\% | Pass |
| 56.75-56.5 | Pole + Reinf. | TP34.834×34.787x0.6375 | Reinf. 5 Bolt Shear | 66.4\% | Pass |
| 56.5-52 | Pole + Reinf. | TP36.518x34.834×0.6375 | Reinf. 5 Compression | 66.1\% | Pass |
| 52-47 | Pole + Reinf. | TP35.987×35.051×0.7 | Reinf. 5 Compression | 63.6\% | Pass |
| 47-42 | Pole + Reinf. | TP36.922x35.987x0.6875 | Reinf. 5 Compression | 65.4\% | Pass |
| 42-37 | Pole + Reinf. | TP37.858×36.922×0.675 | Reinf. 5 Compression | 67.0\% | Pass |
| 37-34.25 | Pole + Reinf. | TP38.372x37.858×0.675 | Reinf. 5 Bolt Shear | 70.3\% | Pass |
| 34.25-34 | Pole + Reinf. | TP38.419×38.372×0.675 | Reinf. 4 Bolt Shear | 70.4\% | Pass |
| 34-29 | Pole + Reinf. | TP39.354×38.419x0.6625 | Reinf. 4 Compression | 69.4\% | Pass |
| 29-26.75 | Pole + Reinf. | TP39.775x39.354×0.6625 | Reinf. 4 Bolt Shear | 72.6\% | Pass |
| 26.75-26.5 | Pole + Reinf. | TP39.822x39.775×0.6625 | Reinf. 1 Bolt Shear | 72.7\% | Pass |
| 26.5-21.5 | Pole + Reinf. | TP40.757x39.822x0.65 | Reinf. 1 Compression | 71.5\% | Pass |
| 21.5-16.75 | Pole + Reinf. | TP41.646x40.757x0.65 | Reinf. 1 Compression | 72.8\% | Pass |
| 16.75-16.5 | Pole + Reinf. | TP41.693x41.646x0.7625 | Reinf. 2 Compression | 66.9\% | Pass |
| 16.5-14.25 | Pole + Reinf. | TP42.114×41.693×0.7625 | Reinf. 2 Compression | 67.5\% | Pass |
| 14.25-14 | Pole + Reinf. | TP42.161×42.114×0.725 | Reinf. 2 Compression | 67.9\% | Pass |
| 14-9 | Pole + Reinf. | TP43.096x42.161×0.7125 | Reinf. 2 Compression | 69.1\% | Pass |
| 9-4.25 | Pole + Reinf. | TP43.985x43.096x0.7125 | Reinf. 2 Bolt Shear | 72.7\% | Pass |
| 4.25-4 | Pole + Reinf. | TP44.032×43.985×0.6 | Reinf. 10 Connection | 74.0\% | Pass |
| 4-0 | Pole + Reinf. | TP44.78×44.032×0.6 | Reinf. 10 Connection | 74.8\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 64.6\% | Pass |
|  |  |  | Reinforcement | 76.4\% | Pass |
|  |  |  | Overall | 76.4\% | Pass |

Table 5 - Tower Component Stresses vs. Capacity - LC7

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 60.6 | Pass |  |  |
| 1 | Base Plate | 0 | 56.6 | Pass |  |  |
| $\mathbf{1}$ | Base Foundation Steel | 0 | 47.2 | Pass |  |  |
| $\mathbf{1}$ | Base Foundation Soil Interaction | 0 | 32.3 | Pass |  |  |
| Structure Rating (max from all components) |  |  |  |  |  | $\mathbf{7 6 . 4 \%}$ |

Notes:

- All structural ratings are per TIA-222-H Section 15.5

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The tower and its foundation have sufficient capacity to carry the proposed load configuration. No modifications are required at this time.

## APPENDIX A

 TNXTOWER OUTPUT

## Tower Input Data

The tower is a monopole.
This tower is designed using the TIA-222-H standard.
The following design criteria apply:

1) Tower is located in New Haven County, Connecticut.
2) Tower base elevation above sea level: 741.00 ft .
3) Basic wind speed of 125.00 mph .
4) Risk Category II.
5) Exposure Category B.
6) Simplified Topographic Factor Procedure for wind speed-up calculations is used.
7) Topographic Category: 1.
8) Crest Height: 0.00 ft .
9) Nominal ice thickness of 1.5000 in .
10) Ice thickness is considered to increase with height.
11) Ice density of 56.00 pcf.
12) A wind speed of 50.00 mph is used in combination with ice.
13) Temperature drop of $50.00^{\circ} \mathrm{F}$.
14) Deflections calculated using a wind speed of 60.00 mph .
15) TIA-222-H Annex S.
16) A non-linear (P-delta) analysis was used.
17) Pressures are calculated at each section.
18) Stress ratio used in pole design is 1.05 .
19) Tower analysis based on target reliabilities in accordance with Annex $S$.
20) Load Modification Factors used: $\mathrm{K}_{\mathrm{es}}\left(\mathrm{F}_{\mathrm{w}}\right)=0.95$, $\mathrm{K}_{\mathrm{es}}\left(\mathrm{t}_{\mathrm{i}}\right)=0.85$.
21) Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

Consider Moments - Legs
Consider Moments - Horizontals
Consider Moments - Diagonals
Use Moment Magnification
Use Code Stress Ratios
$\sqrt{ }$ Use Code Safety Factors - Guys
Escalate Ice
Always Use Max Kz
Use Special Wind Profile
Include Bolts In Member Capacity
Leg Bolts Are At Top Of Section Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided)
SR Members Have Cut Ends
SR Members Are Concentric

## Distribute Leg L.oads As Uniform

Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ } \sqrt{ }$ Use Clear Spans For Wind Area
Use Clear Spans For KL/r Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt.
Autocalc Torque Arm Areas
Add IBC .6D+W Combination
Sort Capacity Reports By Component
Triangulate Diamond Inner Bracing Treat Feed Line Bundles As Cylinder Ignore KL./ry For 60 Deg. Angle Legs

Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces
Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\checkmark$ Consider Feed Line Torque
Include Angle Block Shear Check
Use TIA-222-H Bracing Resist.
Exemption
Use TIA-222-H Tension Splice
Exemption
$\sqrt{ }$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow
Use Top Mounted Sockets
Pole Without Linear Attachments
Pole With Shroud Or No
Appurtenances
Outside and Inside Corner Radii Are
Known

## Tapered Pole Section Geometry

| Section | Elevation <br> ft | Section <br> Length <br> ft | Splice <br> Length <br> ft | Number <br> of <br> Sides | Top <br> Diameter <br> in | Bottom <br> Diameter <br> in | Wall <br> Thickness <br> in | Bend <br> Radius <br> in | Pole Grade |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L 1 | $151.00-146.00$ | 5.00 | 0.00 | 12 | 17.5900 | 18.5255 | 0.2188 | 0.8752 | A572-65 <br> $(65 \mathrm{ksi})$ |  |
| L2 | $146.00-141.00$ | 5.00 | 0.00 | 12 | 18.5255 | 19.4610 | 0.2188 | 0.8752 | A572-65 <br> $(65 \mathrm{ksi})$ |  |
| L3 | $141.00-136.00$ | 5.00 | 0.00 | 12 | 19.4610 | 20.3965 | 0.2188 | 0.8752 | A572-65 <br> $(65 \mathrm{ksi})$ |  |
| L4 | $136.00-131.00$ | 5.00 | 0.00 | 12 | 20.3965 | 21.3321 | 0.2188 | 0.8752 | A572-65 |  |
|  |  |  |  |  |  |  |  |  |  |  |
| $(65 \mathrm{ksi})$ |  |  |  |  |  |  |  |  |  |  |

151 Ft Monopole Tower Structural Analysis

| Section | Elevation ft | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L5 | 131.00-126.00 | 5.00 | 0.00 | 12 | 21.3321 | 22.2676 | 0.2188 | 0.8752 | $\begin{gathered} \hline \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L6 | 126.00-125.50 | 0.50 | 0.00 | 12 | 22.2676 | 22.3611 | 0.2188 | 0.8752 | A572-65 <br> ( 65 ksi ) |
| L7 | 125.50-125.25 | 0.25 | 0.00 | 12 | 22.3611 | 22.4079 | 0.3625 | 1.4502 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L8 | 125.25-120.25 | 5.00 | 0.00 | 12 | 22.4079 | 23.3434 | 0.3563 | 1.4252 | A572-65 <br> ( 65 ksi ) |
| L9 | 120.25-118.50 | 1.75 | 0.00 | 12 | 23.3434 | 23.6708 | 0.3563 | 1.4252 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L10 | 118.50-118.25 | 0.25 | 0.00 | 12 | 23.6708 | 23.7176 | 0.6438 | 2.5752 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L11 | 118.25-117.50 | 0.75 | 0.00 | 12 | 23.7176 | 23.8579 | 0.6438 | 2.5752 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L12 | 117.50-117.25 | 0.25 | 0.00 | 12 | 23.8579 | 23.9047 | 0.4938 | 1.9752 | A572-65 <br> ( 65 ksi ) |
| L13 | 117.25-112.25 | 5.00 | 0.00 | 12 | 23.9047 | 24.8402 | 0.4813 | 1.9252 | A572-65 <br> ( 65 ksi ) |
| L14 | 112.25-107.25 | 5.00 | 0.00 | 12 | 24.8402 | 25.7757 | 0.4688 | 1.8752 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L15 | 107.25-102.25 | 5.00 | 0.00 | 12 | 25.7757 | 26.7113 | 0.4563 | 1.8252 | A572-65 <br> ( 65 ksi ) |
| L16 | 102.25-97.50 | 4.75 | 3.42 | 12 | 26.7113 | 27.6000 | 0.4563 | 1.8252 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L17 | 97.50-95.92 | 5.00 | 0.00 | 12 | 26.5233 | 27.4588 | 0.5500 | 2.2000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L. 18 | 95.92-92.50 | 3.42 | 0.00 | 12 | 27.4588 | 28.0980 | 0.5500 | 2.2000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L19 | 92.50-92.25 | 0.25 | 0.00 | 12 | 28.0980 | 28.1447 | 0.5500 | 2.2000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L20 | 92.25-87.25 | 5.00 | 0.00 | 12 | 28.1447 | 29.0803 | 0.5375 | 2.1500 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L21 | 87.25-87.00 | 0.25 | 0.00 | 12 | 29.0803 | 29.1271 | 0.6250 | 2.5000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L22 | 87.00-82.00 | 5.00 | 0.00 | 12 | 29.1271 | 30.0626 | 0.6125 | 2.4500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L23 | 82.00-77.00 | 5.00 | 0.00 | 12 | 30.0626 | 30.9981 | 0.6000 | 2.4000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L24 | 77.00-72.00 | 5.00 | 0.00 | 12 | 30.9981 | 31.9337 | 0.5875 | 2.3500 | A572-65 <br> ( 65 ksi ) |
| L25 | 72.00-67.00 | 5.00 | 0.00 | 12 | 31.9337 | 32.8692 | 0.5750 | 2.3000 | A572-65 <br> ( 65 ksi ) |
| L26 | 67.00-63.25 | 3.75 | 0.00 | 12 | 32.8692 | 33.5709 | 0.5750 | 2.3000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L27 | 63.25-63.00 | 0.25 | 0.00 | 12 | 33.5709 | 33.6176 | 0.5750 | 2.3000 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L28 | 63.00-58.00 | 5.00 | 0.00 | 12 | 33.6176 | 34.5532 | 0.5625 | 2.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L29 | 58.00-56.75 | 1.25 | 0.00 | 12 | 34.5532 | 34.7871 | 0.5625 | 2.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L30 | 56.75-56.50 | 0.25 | 0.00 | 12 | 34.7871 | 34.8338 | 0.6375 | 2.5500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L31 | 56.50-47.50 | 9.00 | 4.50 | 12 | 34.8338 | 36.5180 | 0.6375 | 2.5500 | A572-65 <br> ( 65 ksi ) |
| L32 | 47.50-47.00 | 5.00 | 0.00 | 12 | 35.0510 | 35.9865 | 0.7000 | 2.8000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L33 | 47.00-42.00 | 5.00 | 0.00 | 12 | 35.9865 | 36.9220 | 0.6875 | 2.7500 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L34 | 42.00-37.00 | 5.00 | 0.00 | 12 | 36.9220 | 37.8575 | 0.6750 | 2.7000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L35 | 37.00-34.25 | 2.75 | 0.00 | 12 | 37.8575 | 38.3718 | 0.6750 | 2.7000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L36 | 34.25-34.00 | 0.25 | 0.00 | 12 | 38.3718 | 38.4186 | 0.6750 | 2.7000 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L37 | 34.00-29.00 | 5.00 | 0.00 | 12 | 38.4186 | 39.3541 | 0.6625 | 2.6500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L38 | 29.00-26.75 | 2.25 | 0.00 | 12 | 39.3541 | 39.7751 | 0.6625 | 2.6500 | $\begin{aligned} & \text { A572-65 } \\ & (65 \mathrm{ksi}) \end{aligned}$ |
| L39 | 26.75-26.50 | 0.25 | 0.00 | 12 | 39.7751 | 39.8219 | 0.6625 | 2.6500 | A572-65 |

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| Section | Elevation $f t$ | Section Length ft | Splice Length ft | Number of Sides | Top Diameter in | Bottom Diameter in | Wall <br> Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L40 | 26.50-21.50 | 5.00 | 0.00 | 12 | 39.8219 | 40.7574 | 0.6500 | 2.6000 | (65 ksi) |
|  |  |  |  |  |  |  |  |  | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L41 | 21.50-16.75 | 4.75 | 0.00 | 12 | 40.7574 | 41.6461 | 0.6500 | 2.6000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L. 42 | 16.75-16.50 | 0.25 | 0.00 | 12 | 41.6461 | 41.6929 | 0.7625 | 3.0500 | A572-65 |
|  |  |  |  |  |  |  |  |  | ( 65 ksi ) |
| L43 | 16.50-14.25 | 2.25 | 0.00 | 12 | 41.6929 | 42.1138 | 0.7625 | 3.0500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L44 | 14.25-14.00 | 0.25 | 0.00 | 12 | 42.1138 | 42.1606 | 0.7250 | 2.9000 | A572-65 |
|  |  |  |  |  |  |  |  |  | ( 65 ksi ) |
| L45 | 14.00-9.00 | 5.00 | 0.00 | 12 | 42.1606 | 43.0961 | 0.7125 | 2.8500 | A572-65 |
|  |  |  |  |  |  |  |  |  | ( 65 ksi ) |
| L46 | 9.00-4.25 | 4.75 | 0.00 | 12 | 43.0961 | 43.9848 | 0.7125 | 2.8500 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L47 | 4.25-4.00 | 0.25 | 0.00 | 12 | 43.9848 | 44.0316 | 0.6000 | 2.4000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |
| L48 | 4.00-0.00 | 4.00 |  | 12 | 44.0316 | 44.7800 | 0.6000 | 2.4000 | A572-65 |
|  |  |  |  |  |  |  |  |  | (65 ksi) |

## Tapered Pole Properties

| Section | Tip Dia. in | Area $i n^{2}$ | $\frac{1}{i n^{4}}$ | $\begin{gathered} r \\ \text { in } \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \text { in } \end{aligned}$ | $\frac{1 / C}{i n^{3}}$ | $\begin{gathered} J \\ i n^{4} \end{gathered}$ | $\begin{aligned} & 1 / / Q \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 18.1333 | 12.2386 | 471.3881 | 6.2189 | 9.1116 | 51.7348 | 955.1601 | 6.0235 | 4.1277 | 18.865 |
|  | 19.1018 | 12.8977 | 551.7220 | 6.5538 | 9.5962 | 57.4937 | 1117.9384 | 6.3479 | 4.3785 | 20.011 |
| L2 | 19.1018 | 12.8977 | 551.7220 | 6.5538 | 9.5962 | 57.4937 | 1117.9384 | 6.3479 | 4.3785 | 20.011 |
|  | 20.0704 | 13.5568 | 640.7007 | 6.8887 | 10.0808 | 63.5565 | 1298.2334 | 6.6723 | 4.6292 | 21.157 |
| 13 | 20.0704 | 13.5568 | 640.7007 | 6.8887 | 10.0808 | 63.5565 | 1298.2334 | 6.6723 | 4.6292 | 21.157 |
|  | 21.0389 | 14.2159 | 738.7659 | 7.2236 | 10.5654 | 69.9231 | 1496.9400 | 6.9967 | 4.8799 | 22.303 |
| 14 | 21.0389 | 14.2159 | 738.7659 | 7.2236 | 10.5654 | 69.9231 | 1496.9400 | 6.9967 | 4.8799 | 22.303 |
|  | 22.0074 | 14.8750 | 846.3593 | 7.5585 | 11.0500 | 76.5936 | 1714.9535 | 7.3210 | 5.1306 | 23.449 |
| 15 | 22.0074 | 14.8750 | 846.3593 | 7.5585 | 11.0500 | 76.5936 | 1714.9535 | 7.3210 | 5.1306 | 23.449 |
|  | 22.9759 | 15.5342 | 963.9228 | 7.8935 | 11.5346 | 83.5679 | 1953.1689 | 7.6454 | 5.3813 | 24.595 |
| 16 | 22.9759 | 15.5342 | 963.9228 | 7.8935 | 11.5346 | 83.5679 | 1953.1689 | 7.6454 | 5.3813 | 24.595 |
|  | 23.0728 | 15.6001 | 976.2445 | 7.9270 | 11.5831 | 84.2821 | 1978.1360 | 7.6779 | 5.4064 | 24.709 |
| L7 | 23.0220 | 25.6814 | 1586.3287 | 7.8755 | 11.5831 | 136.9525 | 3214.3320 | 12.6396 | 5.0211 | 13.85 |
|  | 23.0705 | 25.7360 | 1596.4693 | 7.8922 | 11.6073 | 137.5402 | 3234.8795 | 12.6665 | 5.0337 | 13.884 |
| L8 | 23.0727 | 25.2995 | 1570.2825 | 7.8945 | 11.6073 | 135.2842 | 3181.8181 | 12.4516 | 5.0504 | 14.175 |
|  | 24.0412 | 26.3728 | 1778.7333 | 8.2294 | 12.0919 | 147.1014 | 3604.1959 | 12.9799 | 5.3012 | 14.878 |
| L9 | 24.0412 | 26.3728 | 1778.7333 | 8.2294 | 12.0919 | 147.1014 | 3604.1959 | 12.9799 | 5.3012 | 14.878 |
|  | 24.3802 | 26.7484 | 1855.8303 | 8.3466 | 12.2615 | 151.3543 | 3760.4153 | 13.1648 | 5.3889 | 15.125 |
| L. 10 | 24.2787 | 47.7359 | 3230.7786 | 8.2437 | 12.2615 | 263.4898 | 6546.4334 | 23.4942 | 4.6184 | 7.174 |
|  | 24.3272 | 47.8329 | 3250.5071 | 8.2604 | 12.2857 | 264.5759 | 6586.4086 | 23.5419 | 4.6309 | 7.193 |
| L11 | 24.3272 | 47.8329 | 3250.5071 | 8.2604 | 12.2857 | 264.5759 | 6586.4086 | 23.5419 | 4.6309 | 7.193 |
|  | 24.4725 | 48.1238 | 3310.1739 | 8.3107 | 12.3584 | 267.8478 | 6707.3098 | 23.6850 | 4.6685 | 7.252 |
| L12 | 24.5254 | 37.1498 | 2588.4664 | 8.3644 | 12.3584 | 209.4497 | 5244.9346 | 18.2840 | 5.0705 | 10.268 |
|  | 24.5738 | 37.2242 | 2604.0441 | 8.3811 | 12.3826 | 210.2979 | 5276.4993 | 18.3206 | 5.0831 | 10.294 |
| L13 | 24.5782 | 36.3013 | 2542.1934 | 8.3856 | 12.3826 | 205.3029 | 5151.1730 | 17.8664 | 5.1166 | 10.631 |
|  | 25.5467 | 37.7511 | 2859.1208 | 8.7205 | 12.8672 | 222.2015 | 5793.3538 | 18.5800 | 5.3673 | 11.152 |
| L14 | 25.5511 | 36.7896 | 2789.1550 | 8.7250 | 12.8672 | 216.7640 | 5651.5843 | 18.1067 | 5.4008 | 11.52 |
|  | 26.5196 | 38.2017 | 3122.8328 | 9.0599 | 13.3518 | 233.8879 | 6327.7058 | 18.8017 | 5.6515 | 12.055 |
| L15 | 26.5241 | 37.2015 | 3044.0724 | 9.0644 | 13.3518 | 227.9890 | 6168.1159 | 18.3095 | 5.6850 | 12.459 |
|  | 27.4926 | 38.5760 | 3394.1142 | 9.3993 | 13.8364 | 245.3027 | 6877.3957 | 18.9860 | 5.9357 | 13.008 |
| L. 16 | 27.4926 | 38.5760 | 3394.1142 | 9.3993 | 13.8364 | 245.3027 | 6877.3957 | 18.9860 | 5.9357 | 13.008 |
|  | 28.4127 | 39.8819 | 3750.5886 | 9.7174 | 14.2968 | 262.3376 | 7599.7094 | 19.6286 | 6.1739 | 13.53 |
| L17 | 27.9266 | 45.9986 | 3960.8075 | 9.2984 | 13.7390 | 288.2884 | 8025.6699 | 22.6391 | 5.6342 | 10.244 |
|  | 28.2334 | 47.6555 | 4404.4058 | 9.6333 | 14.2237 | 309.6536 | 8924.5203 | 23.4546 | 5.8850 | 10.7 |
| L18 | 28.2334 | 47.6555 | 4404.4058 | 9.6333 | 14.2237 | 309.6536 | 8924.5203 | 23.4546 | 5.8850 | 10.7 |
|  | 28.8951 | 48.7874 | 4725.7713 | 9.8622 | 14.5547 | 324.6895 | 9575.6939 | 24.0117 | 6.0563 | 11.011 |
| L19 | 28.8951 | 48.7874 | 4725.7713 | 9.8622 | 14.5547 | 324.6895 | 9575.6939 | 24.0117 | 6.0563 | 11.011 |
|  | 28.9436 | 48.8703 | 4749.8856 | 9.8789 | 14.5790 | 325.8039 | 9624.5559 | 24.0525 | 6.0688 | 11.034 |
| L20 | 28.9480 | 47.7812 | 4648.2446 | 9.8834 | 14.5790 | 318.8321 | 9418.6039 | 23.5165 | 6.1023 | 11.353 |
|  | 29.9165 | 49.4004 | 5136.9910 | 10.2183 | 15.0636 | 341.0206 | $\begin{gathered} 10408.936 \\ 5 \end{gathered}$ | 24.3134 | 6.3530 | 11.82 |
| L21 | 29.8856 | 57.2662 | 5918.4793 | 10.1870 | 15.0636 | 392.8999 | $\begin{gathered} 11992.443 \\ 6 \end{gathered}$ | 28.1847 | 6.1185 | 9.79 |


| Section | Tip Dia. in | Area $i n^{2}$ | $\begin{gathered} i n^{4} \end{gathered}$ | $\begin{gathered} r \\ i n \end{gathered}$ | $\begin{aligned} & \mathrm{C} \\ & \text { in } \end{aligned}$ | $\begin{aligned} & I / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{aligned} & I t / Q \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & w \\ & i n \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L22 | 29.9341 | 57.3604 | 5947.7151 | 10.2037 | 15.0878 | 394.2066 | $\begin{gathered} 12051.683 \\ 2 \end{gathered}$ | 28.2310 | 6.1310 | 9.81 |
|  | 29.9385 | 56.2378 | 5836.4330 | 10.2082 | 15.0878 | 386.8310 | $\begin{gathered} 11826.195 \\ 6 \end{gathered}$ | 27.6785 | 6.1645 | 10.065 |
| L23 | 30.9070 | 58.0829 | 6429.9530 | 10.5431 | 15.5724 | 412.9064 | $\begin{gathered} 13028.827 \\ 9 \end{gathered}$ | 28.5867 | 6.4153 | 10.474 |
|  | 30.9114 | 56.9217 | 6306.7533 | 10.5476 | 15.5724 | 404.9950 | $\begin{gathered} 12779.191 \\ 9 \end{gathered}$ | 28.0151 | 6.4488 | 10.748 |
| L24 | 31.8800 | 58.7292 | 6926.8161 | 10.8825 | 16.0570 | 431.3883 | $\begin{gathered} 14035.607 \\ 4 \end{gathered}$ | 28.9047 | 6.6995 | 11.166 |
|  | 31.8844 | 57.5293 | 6790.8780 | 10.8870 | 16.0570 | 422.9224 | $\begin{gathered} 13760.159 \\ 9 \end{gathered}$ | 28.3142 | 6.7330 | 11.46 |
| L. 25 | 32.8529 | 59.2991 | 7437.0912 | 11.2219 | 16.5416 | 449.5982 | $\begin{gathered} 15069.563 \\ 2 \end{gathered}$ | 29.1852 | 6.9837 | 11.887 |
|  | 32.8573 | 58.0606 | 7287.5666 | 11.2264 | 16.5416 | 440.5589 | $\begin{gathered} 14766.585 \\ 6 \end{gathered}$ | 28.5756 | 7.0172 | 12.204 |
| L26 | 33.8259 | 59.7927 | 7959.4601 | 11.5613 | 17.0263 | 467.4817 | $\begin{gathered} 16128.024 \\ 0 \end{gathered}$ | 29.4282 | 7.2679 | 12.64 |
|  | 33.8259 | 59.7927 | 7959.4601 | 11.5613 | 17.0263 | 467.4817 | $\begin{gathered} 16128.024 \\ 0 \end{gathered}$ | 29.4282 | 7.2679 | 12.64 |
| L27 | 34.5523 | 61.0918 | 8489.6181 | 11.8125 | 17.3897 | 488.1979 | $\begin{gathered} 17202.267 \\ 9 \end{gathered}$ | 30.0675 | 7.4560 | 12.967 |
|  | 34.5523 | 61.0918 | 8489.6181 | 11.8125 | 17.3897 | 488.1979 | $\begin{gathered} 17202.267 \\ 9 \end{gathered}$ | 30.0675 | 7.4560 | 12.967 |
| L28 | 34.6007 | 61.1784 | 8525.7755 | 11.8293 | 17.4139 | 489.5949 | $\begin{gathered} 17275.532 \\ 7 \end{gathered}$ | 30.1102 | 7.4685 | 12.989 |
|  | 34.6051 35.5737 | 59.8711 | 8349.9017 | 11.8337 | 17.4139 | 479.4953 | $\begin{gathered} 16919.164 \\ 6 \end{gathered}$ | 29.4667 | 7.5020 | 13.337 |
| L29 | 35.5737 35.5737 | 61.5656 | 9079.1230 | 12.1687 | 17.8985 | 507.2547 | $\begin{gathered} 18396.764 \\ 7 \end{gathered}$ | 30.3007 | 7.7528 | 13.783 |
|  | 35.5737 | 61.5656 | 9079.1230 | 12.1687 | 17.8985 | 507.2547 | $\begin{gathered} 18396.764 \\ 7 \end{gathered}$ | 30.3007 | 7.7528 | 13.783 |
| L30 | 35.8158 | 61.9892 | 9267.8319 | 12.2524 | 18.0197 | 514.3167 | $\begin{gathered} 18779.140 \\ 1 \end{gathered}$ | 30.5092 | 7.8154 | 13.894 |
|  | 35.7893 35.8378 | 70.1005 70.1065 | $\begin{gathered} 10434.641 \\ 4 \end{gathered}$ | 12.2255 | 18.0197 | 579.0686 | $\begin{gathered} 21143.412 \\ 5 \end{gathered}$ | 34.5013 | 7.6144 | 11.944 |
| L31 | 35.8378 | 70.1965 | $\begin{gathered} 10477.579 \\ 3 \end{gathered}$ | 12.2423 | 18.0439 | 580.6706 | $\begin{gathered} 21230.416 \\ 2 \end{gathered}$ | 34.5486 | 7.6270 | 11.964 |
|  | 35.8378 | 70.1965 | $\begin{gathered} 10477.579 \\ 3 \end{gathered}$ | 12.2423 | 18.0439 | 580.6706 | $\begin{gathered} 21230.416 \\ 2 \end{gathered}$ | 34.5486 | 7.6270 | 11.964 |
| L32 | 37.5813 | 73.6537 | $\begin{gathered} 12103.123 \\ 6 \end{gathered}$ | 12.8452 | 18.9163 | 639.8243 | $\begin{gathered} 24524.209 \\ 8 \end{gathered}$ | 36.2501 | 8.0783 | 12.672 |
|  | 36.9122 | 77.4272 | $\begin{gathered} 11661.611 \\ 3 \end{gathered}$ | 12.2977 | 18.1564 | 642.2856 | $\begin{gathered} 23629.586 \\ 1 \end{gathered}$ | 38.1073 | 7.5177 | 10.74 |
| L33 | 37.0090 | 79.5358 | $\begin{gathered} 12640.552 \\ 2 \end{gathered}$ | 12.6326 | 18.6410 | 678.1044 | $\begin{gathered} 25613.185 \\ 9 \end{gathered}$ | 39.1451 | 7.7684 | 11.098 |
|  | 37.0135 | 78.1432 | $\begin{gathered} 12428.026 \\ 4 \end{gathered}$ | 12.6370 | 18.6410 | 666.7034 | $\begin{gathered} 25182.550 \\ 8 \end{gathered}$ | 38.4597 | 7.8019 | 11.348 |
| L34 | 37.9820 | 80.2141 | $\begin{gathered} 13442.550 \\ 4 \end{gathered}$ | 12.9720 | 19.1256 | 702.8564 | $\begin{gathered} 27238.251 \\ 5 \end{gathered}$ | 39.4790 | 8.0526 | 11.713 |
|  | 37.9864 | 78.7829 | $\begin{gathered} 13211.804 \\ 2 \end{gathered}$ | 12.9764 | 19.1256 | 690.7916 | $\begin{gathered} 26770.697 \\ 1 \end{gathered}$ | 38.7745 | 8.0861 | 11.979 |
| L35 | 38.9549 | 80.8162 | $\begin{gathered} 14261.381 \\ 0 \end{gathered}$ | 13.3113 | 19.6102 | 727.2434 | $\begin{gathered} 28897.424 \\ 4 \end{gathered}$ | 39.7753 | 8.3368 | 12.351 |
|  | 38.9549 | 80.8162 | $\begin{gathered} 14261.381 \\ 0 \end{gathered}$ | 13.3113 | 19.6102 | 727.2434 | $\begin{gathered} 28897.424 \\ 4 \end{gathered}$ | 39.7753 | 8.3368 | 12.351 |
| L36 | 39.4873 | 81.9341 | $\begin{gathered} 14861.427 \\ 8 \end{gathered}$ | 13.4955 | 19.8766 | 747.6841 | $\begin{gathered} 30113.281 \\ 9 \end{gathered}$ | 40.3255 | 8.4747 | 12.555 |
|  | 39.4873 | 81.9341 | $\begin{gathered} 14861.427 \\ 8 \end{gathered}$ | 13.4955 | 19.8766 | 747.6841 | $\begin{gathered} 30113.281 \\ 9 \end{gathered}$ | 40.3255 | 8.4747 | 12.555 |
| L37 | 39.5358 | 82.0358 | $\begin{gathered} 14916.817 \\ 4 \end{gathered}$ | 13.5122 | 19.9008 | 749.5570 | $\begin{gathered} 30225.516 \\ 2 \end{gathered}$ | 40.3755 | 8.4872 | 12.574 |
|  | 39.5402 | 80.5432 | $\begin{gathered} 14655.131 \\ 0 \end{gathered}$ | 13.5167 | 19.9008 | 736.4075 | $\begin{gathered} 29695.268 \\ 5 \end{gathered}$ | 39.6409 | 8.5207 | 12.861 |
| L38 | 40.5087 | 82.5389 | $\begin{gathered} 15771.691 \\ 9 \end{gathered}$ | 13.8516 | 20.3854 | 773.6747 | $\begin{gathered} 31957.723 \\ 8 \end{gathered}$ | 40.6231 | 8.7714 | 13.24 |
|  | 40.5087 | 82.5389 | $\begin{gathered} 15771.691 \\ 9 \end{gathered}$ | 13.8516 | 20.3854 | 773.6747 | $\begin{gathered} 31957.723 \\ 8 \end{gathered}$ | 40.6231 | 8.7714 | 13.24 |
|  | 40.9445 | 83.4369 | $\begin{gathered} 16292.112 \\ 5 \end{gathered}$ | 14.0023 | 20.6035 | 790.7450 | $\begin{gathered} 33012.236 \\ 9 \end{gathered}$ | 41.0651 | 8.8842 | 13.41 |

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| Section | Tip Dia. in | Area $i n^{2}$ | $1$ | in | $\begin{aligned} & C \\ & \text { in } \end{aligned}$ | $\begin{aligned} & 1 / C \\ & i n^{3} \end{aligned}$ | $\underset{i n^{4}}{J}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | W/t |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L39 | 40.9445 | 83.4369 | $\begin{gathered} 16292.112 \\ 5 \end{gathered}$ | 14.0023 | 20.6035 | 790.7450 | $\begin{gathered} 33012.236 \\ 9 \end{gathered}$ | 41.0651 | 8.8842 | 13.41 |
|  | 40.9929 | 83.5367 | $\begin{gathered} 16350.633 \\ 8 \end{gathered}$ | 14.0191 | 20.6277 | 792.6533 | $\begin{gathered} 33130.816 \\ 9 \end{gathered}$ | 41.1142 | 8.8968 | 13.429 |
| L40 | 40.9973 | 81.9867 | $\begin{gathered} 16057.498 \\ 5 \end{gathered}$ | 14.0235 | 20.6277 | 778.4425 | $\begin{gathered} 32536.845 \\ 3 \end{gathered}$ | 40.3514 | 8.9303 | 13.739 |
|  | 41.9658 | 83.9447 | $\begin{gathered} 17235.641 \\ 4 \end{gathered}$ | 14.3584 | 21.1123 | 816.3786 | $\begin{gathered} 34924.082 \\ 2 \end{gathered}$ | 41.3150 | 9.1810 | 14.125 |
| L41 | 41.9658 | 83.9447 | $\begin{gathered} 17235.641 \\ 4 \end{gathered}$ | 14.3584 | 21.1123 | 816.3786 | $\begin{gathered} 34924.082 \\ 2 \end{gathered}$ | 41.3150 | 9.1810 | 14.125 |
|  | 42.8859 | 85.8048 | $\begin{gathered} 18406.969 \\ 6 \end{gathered}$ | 14.6766 | 21.5727 | 853.2541 | $\begin{gathered} 37297.510 \\ 8 \end{gathered}$ | 42.2305 | 9.4192 | 14.491 |
| L42 | 42.8462 | 100.3794 | $\begin{gathered} 21415.516 \\ 1 \end{gathered}$ | 14.6363 | 21.5727 | 992.7151 | $\begin{gathered} 43393.641 \\ 7 \end{gathered}$ | 49.4037 | 9.1177 | 11.958 |
|  | 42.8946 | 100.4943 | $\begin{gathered} 21489.104 \\ 6 \end{gathered}$ | 14.6531 | 21.5969 | 995.0087 | $\begin{gathered} 43542.752 \\ 0 \end{gathered}$ | 49.4602 | 9.1302 | 11.974 |
| L43 | 42.8946 | 100.4943 | $\begin{gathered} 21489.104 \\ 6 \end{gathered}$ | 14.6531 | 21.5969 | 995.0087 | $\begin{gathered} 43542.752 \\ 0 \end{gathered}$ | 49.4602 | 9.1302 | 11.974 |
|  | 43.3305 | 101.5279 | $\begin{gathered} 22159.001 \\ 9 \end{gathered}$ | 14.8038 | 21.8150 | 1015.7707 | $\begin{gathered} 44900.145 \\ 6 \end{gathered}$ | 49.9689 | 9.2430 | 12.122 |
| L44 | 43.3437 | 96.6222 | $\begin{gathered} 21126.587 \\ 6 \end{gathered}$ | 14.8172 | 21.8150 | 968.4447 | $\begin{gathered} 42808.194 \\ 3 \end{gathered}$ | 47.5545 | 9.3435 | 12.888 |
|  | 43.3921 | 96.7314 | $\begin{gathered} 21198.296 \\ 2 \end{gathered}$ | 14.8339 | 21.8392 | 970.6538 | $\begin{gathered} 42953.495 \\ 2 \end{gathered}$ | 47.6083 | 9.3560 | 12.905 |
| L45 | 43.3965 | 95.0923 | $\begin{gathered} 20851.668 \\ 1 \end{gathered}$ | 14.8384 | 21.8392 | 954.7819 | $\begin{gathered} 42251.132 \\ 7 \end{gathered}$ | 46.8015 | 9.3895 | 13.178 |
|  | 44.3650 | 97.2386 | $\begin{gathered} 22295.661 \\ 5 \end{gathered}$ | 15.1733 | 22.3238 | 998.7403 | $\begin{gathered} 45177.054 \\ 9 \end{gathered}$ | 47.8579 | 9.6403 | 13.53 |
| L46 | 44.3650 | 97.2386 | $\begin{gathered} 22295.661 \\ 5 \end{gathered}$ | 15.1733 | 22.3238 | 998.7403 | $\begin{gathered} 45177.054 \\ 9 \end{gathered}$ | 47.8579 | 9.6403 | 13.53 |
|  | 45.2851 | 99.2775 | $\begin{gathered} 23727.798 \\ 7 \end{gathered}$ | 15.4915 | 22.7841 | 1041.4173 | $\begin{gathered} 48078.953 \\ 0 \end{gathered}$ | 48.8614 | 9.8784 | 13.864 |
| L47 | 45.3248 | 83.8195 | $\begin{gathered} 20137.552 \\ 7 \end{gathered}$ | 15.5318 | 22.7841 | 883.8408 | $\begin{gathered} 40804.141 \\ 3 \end{gathered}$ | 41.2534 | 10.1799 | 16.967 |
|  | 45.3732 | 83.9099 | $\begin{gathered} 20202.756 \\ 1 \end{gathered}$ | 15.5485 | 22.8084 | 885.7606 | $\begin{gathered} 40936.261 \\ 2 \end{gathered}$ | 41.2979 | 10.1925 | 16.987 |
| L48 | 45.3732 | 83.9099 | $\begin{gathered} 20202.756 \\ 1 \end{gathered}$ | 15.5485 | 22.8084 | 885.7606 | $\begin{gathered} 40936.261 \\ 2 \end{gathered}$ | 41.2979 | 10.1925 | 16.987 |
|  | 46.1480 | 85.3558 | $\begin{gathered} 21265.236 \\ 0 \\ \hline \end{gathered}$ | 15.8164 | 23.1960 | 916.7615 | $\begin{gathered} 43089.133 \\ 4 \end{gathered}$ | 42.0095 | 10.3930 | 17.322 |

$\left.\begin{array}{cccccc}\hline \begin{array}{c}\text { Tower } \\ \text { Elevation } \\ \text { ft }\end{array} & \begin{array}{c}\text { Gusset } \\ \text { Area } \\ \text { (per face) } \\ f^{2}\end{array} & \begin{array}{c}\text { Gusset } \\ \text { Thickness } \\ \text { in }\end{array} & \text { Gusset GradeAdjust. Factor }\end{array} \begin{array}{c}\text { Adjust. } \\ \text { Factor }\end{array}\right)$

| Tower Elevation ft | Gusset Area (perface) $f^{2}$ | Gusset Thickness in | Gusset Grade Adjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Boit Spacing Diagonals in | Double Angie Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { L12 117.50- } \\ 117.25 \end{gathered}$ |  |  | 1 | 1 | 0.932549 |  |  |  |
| $\begin{gathered} \text { L13 117.25- } \\ 112.25 \end{gathered}$ |  |  | 1 | 1 | 0.936991 |  |  |  |
| $\begin{gathered} \text { L14 112.25- } \\ 107.25 \end{gathered}$ |  |  | 1 | 1 | 0.943192 |  |  |  |
| $\begin{gathered} \text { L15 107.25- } \\ 102.25 \end{gathered}$ |  |  | 1 | 1 | 0.951126 |  |  |  |
| $\begin{gathered} \text { L16 102.25- } \\ 97.50 \end{gathered}$ |  |  | 1 | 1 | 0.946685 |  |  | . |
| $\begin{gathered} \mathrm{L} 1797.50- \\ 95.92 \end{gathered}$ |  |  | 1 | 1 | 0.951449 |  |  |  |
| $\begin{gathered} \text { L18 95.92- } \\ 92.50 \end{gathered}$ |  |  | 1 | 1 | 0.942557 |  |  |  |
| $\begin{gathered} \text { L19 92.50- } \\ 92.25 \end{gathered}$ |  |  | 1 | 1 | 0.941922 |  |  |  |
| $\begin{gathered} \mathrm{L} 2092.25- \\ 87.25 \end{gathered}$ |  |  | 1 | 1 | 0.95087 |  |  |  |
| $\begin{gathered} \text { L21 87.25- } \\ 87.00 \end{gathered}$ |  |  | 1 | 1 | 0.931036 |  |  |  |
| $\begin{gathered} \text { L22 87.00- } \\ 82.00 \end{gathered}$ |  |  | 1 | 1 | 0.935662 |  |  |  |
| $\begin{gathered} \llcorner 2382.00- \\ 77.00 \end{gathered}$ |  |  | 1 | 1 | 0.941395 |  |  |  |
| $\begin{gathered} \text { L24 77.00- } \\ 72.00 \end{gathered}$ |  |  | 1 | 1 | 0.948222 |  |  |  |
| $\begin{gathered} \text { L25 72.00- } \\ 67.00 \end{gathered}$ |  |  | 1 | 1 | 0.956139 |  |  |  |
| $\begin{gathered} \text { L26 } 67.00- \\ 63.25 \end{gathered}$ |  |  | 1 | 1 | 0.947363 |  |  |  |
| $\begin{gathered} \text { L27 63.25- } \\ 63.00 \end{gathered}$ |  |  | 1 | 1 | 0.946792 |  |  |  |
| $\begin{gathered} \mathrm{L} 2863.00- \\ 58.00 \end{gathered}$ |  |  | 1 | 1 | 0.956128 |  |  |  |
| $\begin{gathered} \mathrm{L} 2958.00- \\ 56.75 \end{gathered}$ |  |  | 1 | 1 | 0.953391 |  |  |  |
| $\begin{gathered} \text { L30 } 56.75- \\ 56.50 \end{gathered}$ |  |  | 1 | 1 | 0.949588 |  |  |  |
| $\begin{gathered} \text { L31 } 56.50- \\ 47.50 \end{gathered}$ |  |  | 1 | 1 | 0.938546 |  |  |  |
| $\begin{gathered} \text { L32 } 47.50- \\ 47.00 \end{gathered}$ |  |  | 1 | 1 | 0.941986 |  |  |  |
| $\begin{gathered} \text { L33 } 47.00- \\ 42.00 \end{gathered}$ |  |  | 1 | 1 | 0.948102 |  |  |  |
| $\begin{gathered} \mathrm{L} 3442.00- \\ 37.00 \end{gathered}$ |  |  | 1 | 1 | 0.955017 |  |  |  |
| $\begin{gathered} \text { L35 } 37.00- \\ 34.25 \end{gathered}$ |  |  | 1 | 1 | 0.949567 |  |  |  |
| $\begin{gathered} \text { L36 } 34.25- \\ 34.00 \end{gathered}$ |  |  | 1 | 1 | 0.949078 |  |  |  |
| $\begin{gathered} \mathrm{L} 3734.00- \\ 29.00 \end{gathered}$ |  |  | 1 | 1 | 0.956979 |  |  |  |
| $\begin{gathered} \text { L38 } 29.00- \\ 26.75 \end{gathered}$ |  |  | 1 | 1 | 0.952771 |  |  |  |
| $\begin{gathered} \text { L39 } 26.75- \\ 26.50 \end{gathered}$ |  |  | 1 | 1 | 0.952309 |  |  |  |
| $\begin{gathered} \text { L40 } 26.50- \\ 21.50 \end{gathered}$ |  |  | 1 | 1 | 0.961137 |  |  |  |
| $\begin{gathered} \text { L41 } 21.50- \\ 16.75 \end{gathered}$ |  |  | 1 | 1 | 0.952808 |  |  |  |
| $\begin{gathered} \text { L42 16.75- } \\ 16.50 \end{gathered}$ |  |  | 1 | 1 | 1.02585 |  |  |  |
| $\begin{gathered} \text { L43 16.50- } \\ 14.25 \end{gathered}$ |  |  | 1 | 1 | 1.02042 |  |  |  |
| $\begin{gathered} \text { L44 14.25- } \\ 14.00 \end{gathered}$ |  |  | 1 | 1 | 0.961601 |  |  |  |

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| Tower Elevation ft | Gusset Area (perface) $f{ }^{2}$ | Gusset Thickness in | Gusset GradeAdjust. Factor $A_{f}$ | Adjust. Factor $A_{r}$ | Weight Mult. | Double Angle Stitch Bolt Spacing Diagonals in | Double Angle Stitch Bolt Spacing Horizontals in | Double Angle Stitch Bolt Spacing Redundants in |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{gathered} \hline \text { L45 14.00- } \\ 9.00 \end{gathered}$ |  |  | 1 | 1 | 0.968203 |  |  |  |
| L46 9.00-4.25 |  |  | 1 | 1 | 0.959127 |  |  |  |
| L47 4.25-4.00 |  |  | 1 | 1 | 1.0012 |  |  |  |
| L48 4.00-0.00 |  |  | 1 | 1 | 0.994823 |  |  |  |

Feed Line/Linear Appurtenances - Entered As Round Or Flat


| Description | Sector | Exclude From Torque Calculation | $\begin{gathered} \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement $f t$ | Total Number | Number Per Row | Start/En <br> $d$ <br> Position | Width or Diamete $r$ in | $\begin{gathered} \text { Perimete } \\ r \\ \text { in } \end{gathered}$ | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MP3-03 (L) | B | No | $\begin{gathered} \text { Surface Af } \\ (\mathrm{CaAa}) \end{gathered}$ | $\begin{gathered} 125.00- \\ 115.00 \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.250 \\ & -0.250 \end{aligned}$ | 4.0600 | 11.2600 | 0.00 |
| MP3-03 (L) | A | No | Surface Af (CaAa) | $\begin{gathered} 125.00- \\ 115.00 \\ \hline \end{gathered}$ | 1 | 1 | $\begin{aligned} & -0.250 \\ & -0.250 \\ & \hline \end{aligned}$ | 4.0600 | 11.2600 | 0.00 |

Feed Line/Linear Appurtenances - Entered As Area

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Allow Shield | Exclude From Torque Calculation | $\begin{gathered} \hline \text { Componen } \\ t \\ \text { Type } \end{gathered}$ | Placement ft | Total Number |  | $\begin{aligned} & C_{A} A_{A} \\ & f^{2} / f t \end{aligned}$ | Weight plf |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $* * *$$* * * * * * * * * * * * * * * * * * * *$$* * * * * * * * *$ |  |  |  |  |  |  |  |  |  |
|  |  |  |  |  |  |  |  |  |  |
| LDF2-50(3/8) | C | No | No | Inside Pole | 148.00-0.00 | 2 | No lce | 0.00 | 0.08 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.08 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.08 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.08 |
| 9776(5/8) | C | No | No | Inside Pole | 148.00-0.00 | 2 | No lce | 0.00 | 0.28 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.28 |
|  |  |  |  |  |  |  | 1 ' Ice | 0.00 | 0.28 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.28 |
| LDF7-50A(1-5/8) | C | No | No | Inside Pole | 148.00-0.00 | 12 | No lce | 0.00 | 0.82 |
|  |  |  |  |  |  |  | $1 / 2^{1} \text { Ice }$ | 0.00 | 0.82 |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |
| 2" (Nominal) Conduit | C | No | No | Inside Pole | 148.00-0.00 | 1 | No Ice | 0.00 | 0.72 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.72 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.72 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.72 |
| 810921-001(7/8) | C | No | No | Inside Pole | 148.00-0.00 | 2 | No Ice | 0.00 | 0.40 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.40 |
|  |  |  |  |  |  |  | 1" lce | 0.00 | 0.40 |
|  |  |  |  |  |  |  | 2" lce | 0.00 | 0.40 |
| *** |  |  |  |  |  |  |  |  |  |
| L.DF7-50A(1-5/8) | C | No | No | Inside Pole | 140.00-0.00 | 12 |  | 0.00 | 0.82 |
|  |  |  |  |  |  |  | $1 / 2^{\prime \prime} \text { lce }$ | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |
| $\begin{aligned} & \text { HB158-1-08U8- } \\ & \text { S8J18(1-5/8) } \end{aligned}$ | C | No | No | Inside Pole | 140.00-0.00 | 1 | No lce | 0.00 | 1.30 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.30 |
|  |  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 0.00 | 1.30 |
|  |  |  |  |  |  |  | 2 ' Ice | 0.00 | 1.30 |
| *** ${ }^{*}$ |  |  |  |  |  |  |  |  |  |
| LDF4-50A(1/2) | C | No | No | Inside Pole | 130.00-0.00 | 1 |  | 0.00 | $0.15$ |
|  |  |  |  |  |  |  | $1 / 2^{1 "} \text { Ice }$ | 0.00 | 0.15 |
|  |  |  |  |  |  |  | 1" Ice | 0.00 | 0.15 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.15 |
| LDF7-50A(1-5/8) | C | No | No | Inside Pole | 130.00-0.00 | 3 | No lce | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 0.00 | 0.82 |
|  |  |  |  |  |  |  | 2" Ice | 0.00 | 0.82 |
| $\begin{aligned} & \text { HB114-21U3M12- } \\ & \text { XXXF(1-1/4) } \end{aligned}$ | C | No | No | Inside Pole | 130.00-0.00 | 1 | No Ice | 0.00 | 1.22 |
|  |  |  |  |  |  |  | 1/2" Ice | 0.00 | 1.22 |
|  |  |  |  |  |  |  | $1^{\prime \prime}$ Ice | 0.00 | 1.22 |
|  |  |  |  |  |  |  | 2" ice | 0.00 | 1.22 |

## Feed Line/Linear Appurtenances Section Areas

| Tower Sectio n | Tower Elevation ft | Face | $\begin{gathered} \overline{A_{R}} \\ f^{2} \end{gathered}$ | $\overline{A_{F}}$ | $\begin{gathered} C_{A} A_{A} \\ \text { In } F a c e \\ f f t^{2} \\ \hline \end{gathered}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ \text { ft }^{2} \end{gathered}$ | $\begin{gathered} \text { Weight } \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 151.00-146.00 | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |

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| Tower Sectio $n$ | Tower Elevation ft | Face | $\begin{gathered} A_{R} \\ f^{2} \end{gathered}$ | $A_{F}$ $f^{2}$ | $\begin{gathered} C_{A} A_{A} \\ \text { In Face } \\ f^{2} \end{gathered}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ {f t^{2}}^{2} \end{gathered}$ | Weight $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L2 | 146.00-141.00 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.02 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L.3 | 141.00-136.00 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.06 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L4 | 136.00-131.00 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.10 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L5 | 131.00-126.00 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.12 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L6 | 126.00-125.50 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.13 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L7 | 125.50-125.25 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
| L8 | 125.25-120.25 | C | 0.000 | 0.000 | 0.000 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 3.464 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 4.836 | 0.000 | 0.01 |
| L9 | 120.25-118.50 | C | 0.000 | 0.000 | 3.464 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 2.934 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 4.306 | 0.000 | 0.01 |
| L10 | 118.50-118.25 | C | 0.000 | 0.000 | 2.934 | 0.000 | 0.05 |
|  |  | A | 0.000 | 0.000 | 0.419 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.615 | 0.000 | 0.00 |
| L11 | 118.25-117.50 | C | 0.000 | 0.000 | 0.419 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 1.258 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 1.846 | 0.000 | 0.00 |
| L12 | 117.50-117.25 | C | 0.000 | 0.000 | 1.258 | 0.000 | 0.02 |
|  |  | A | 0.000 | 0.000 | 0.419 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.615 | 0.000 | 0.00 |
| 1.13 | 117.25-112.25 | C | 0.000 | 0.000 | 0.419 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 6.523 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 10.443 | 0.000 | 0.02 |
| L14 | 112.25-107.25 | C | 0.000 | 0.000 | 6.523 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 5.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 8.920 | 0.000 | 0.02 |
| L15 | 107.25-102.25 | C | 0.000 | 0.000 | 5.000 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 5.000 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 8.920 | 0.000 | 0.02 |
| L16 | 102.25-97.50 | C | 0.000 | 0.000 | 5.000 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 5.830 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 9.554 | 0.000 | 0.02 |
| L17 | 97.50-95.92 | C | 0.000 | 0.000 | 5.830 | 0.000 | 0.13 |
|  |  | A | 0.000 | 0.000 | 3.168 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 4.410 | 0.000 | 0.01 |
| L18 | 95.92-92.50 | C | 0.000 | 0.000 | 3.168 | 0.000 | 0.04 |
|  |  | A | 0.000 | 0.000 | 6.832 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 9.510 | 0.000 | 0.01 |
| L19 | 92.50-92.25 | C | 0.000 | 0.000 | 6.832 | 0.000 | 0.09 |
|  |  | A | 0.000 | 0.000 | 0.500 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.696 | 0.000 | 0.00 |
| L20 | 92.25-87.25 | C | 0.000 | 0.000 | 0.500 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 10.271 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 14.191 | 0.000 | 0.02 |
| L21 | 87.25-87.00 | C | 0.000 | 0.000 | 10.271 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 0.521 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.717 | 0.000 | 0.00 |
| 122 | 87.00-82.00 | C | 0.000 | 0.000 | 0.521 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 9.997 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 13.917 | 0.000 | 0.02 |
| L23 | 82.00-77.00 | C | 0.000 | 0.000 | 9.997 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 5.417 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 9.337 | 0.000 | 0.02 |
| L24 | 77.00-72.00 | C | 0.000 | 0.000 | 5.417 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 5.417 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 9.337 | 0.000 | 0.02 |

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| Tower Sectio $n$ | Tower Elevation ft | Face | $\begin{gathered} A_{R} \\ f t^{2} \end{gathered}$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ |  | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ f^{2} \end{gathered}$ | $\begin{gathered} \text { Weight } \\ K \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L25 | 72.00-67.00 | C | 0.000 | 0.000 | 5.417 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 8.309 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 12.229 | 0.000 | 0.02 |
| L26 | 67.00-63.25 | C | 0.000 | 0.000 | 8.309 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 8.125 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 11.065 | 0.000 | 0.01 |
| L27 | 63.25-63.00 | C | 0.000 | 0.000 | 8.125 | 0.000 | 0.10 |
|  |  | A | 0.000 | 0.000 | 0.542 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.738 | 0.000 | 0.00 |
| L28 | 63.00-58.00 | C | 0.000 | 0.000 | 0.542 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 11.667 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 15.587 | 0.000 | 0.02 |
| L29 | 58.00-56.75 | C | 0.000 | 0.000 | 11.667 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 3.125 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 4.105 | 0.000 | 0.00 |
| L30 | 56.75-56.50 | C | 0.000 | 0.000 | 3.125 | 0.000 | 0.03 |
|  |  | A | 0.000 | 0.000 | 0.625 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.821 | 0.000 | 0.00 |
| L31 | 56.50-47.50 | C | 0.000 | 0.000 | 0.625 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 18.352 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 25.409 | 0.000 | 0.03 |
| L32 | 47.50-47.00 | C | 0.000 | 0.000 | 18.352 | 0.000 | 0.24 |
|  |  | A | 0.000 | 0.000 | 0.708 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 1.100 | 0.000 | 0.00 |
| L33 | 47.00-42.00 | C | 0.000 | 0.000 | 0.708 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 7.083 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 11.003 | 0.000 | 0.02 |
| L34 | 42.00-37.00 | C | 0.000 | 0.000 | 7.083 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 11.335 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 15.255 | 0.000 | 0.02 |
| L35 | 37.00-34.25 | C | 0.000 | 0.000 | 11.335 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 7.789 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 9.944 | 0.000 | 0.01 |
| L36 | 34.25-34.00 | C | 0.000 | 0.000 | 7.789 | 0.000 | 0.07 |
|  |  | A | 0.000 | 0.000 | 0.708 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.904 | 0.000 | 0.00 |
| L37 | 34.00-29.00 | C | 0.000 | 0.000 | 0.708 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 14.167 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 18.087 | 0.000 | 0.02 |
| L38 | 29.00-26.75 | C | 0.000 | 0.000 | 14.167 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 6.375 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 8.139 | 0.000 | 0.01 |
| L39 | 26.75-26.50 | C | 0.000 | 0.000 | 6.375 | 0.000 | 0.06 |
|  |  | A | 0.000 | 0.000 | 0.708 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.904 | 0.000 | 0.00 |
| L40 | 26.50-21.50 | C | 0.000 | 0.000 | 0.708 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 14.167 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 18.087 | 0.000 | 0.02 |
| L41 | 21.50-16.75 | C | 0.000 | 0.000 | 14.167 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 12.750 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 16.474 | 0.000 | 0.02 |
| L42 | 16.75-16.50 | C | 0.000 | 0.000 | 7.438 | 0.000 | 0.13 |
|  |  | A | 0.000 | 0.000 | 0.708 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.904 | 0.000 | 0.00 |
| L43 | 16.50-14.25 | C | 0.000 | 0.000 | 0.354 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 6.375 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 8.139 | 0.000 | 0.01 |
| 144 | 14.25-14.00 | C | 0.000 | 0.000 | 3.188 | 0.000 | 0.06 |
|  |  | A | 0.000 | 0.000 | 0.708 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.904 | 0.000 | 0.00 |
| L45 | 14.00-9.00 | C | 0.000 | 0.000 | 0.354 | 0.000 | 0.01 |
|  |  | A | 0.000 | 0.000 | 12.042 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 18.087 | 0.000 | 0.02 |
| L46 | $9.00-4.25$ | C | 0.000 | 0.000 | 7.083 | 0.000 | 0.14 |
|  |  | A | 0.000 | 0.000 | 6.729 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 17.182 | 0.000 | 0.02 |
| L47 | 4.25-4.00 | C | 0.000 | 0.000 | 6.729 | 0.000 | 0.13 |
|  |  | A | 0.000 | 0.000 | 0.354 | 0.000 | 0.00 |
|  |  | B | 0.000 | 0.000 | 0.904 | 0.000 | 0.00 |

[^1]| Tower <br> Sectio | Tower <br> Elevation <br> $n$ | Face | $A_{R}$ <br> $f^{2}$ | $A_{F}$ | $C_{A} A_{A}$ <br> In Face | $C_{A} A_{A}$ <br> Out Face <br> $f l^{2}$ | Weight <br> $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | $f^{2}$ | $f^{2}$ |  |  |
|  |  |  | C | 0.000 | 0.000 | 0.354 | 0.000 |
|  | $4.00-0.00$ | A | 0.000 | 0.000 | 4.958 | 0.000 | 0.01 |
|  |  | B | 0.000 | 0.000 | 13.053 | 0.000 | 0.01 |
|  |  | C | 0.000 | 0.000 | 4.958 | 0.000 | 0.11 |

Feed Line/Linear Appurtenances Section Areas - With Ice

| Tower Sectio <br> $n$ | Tower Elevation ft | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | lce Thickness in | $\begin{gathered} A_{R} \\ f^{2} \end{gathered}$ | $A_{F}$ $f^{2}$ |  | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ f^{2} \end{gathered}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 151.00-146.00 | A | 1.482 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.02 |
| L2 | 146.00-141.00 | A | 1.477 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.06 |
| L3 | 141.00-136.00 | A | 1.472 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.10 |
| L4 | 136.00-131.00 | A | 1.466 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.12 |
| L5 | 131.00-126.00 | A | 1.461 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.13 |
| L6 | 126.00-125.50 | A | 1.458 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.01 |
| L7 | 125.50-125.25 | A | 1.457 | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.00 |
|  |  | C |  | 0.000 | 0.000 | 0.000 | 0.000 | 0.01 |
| L8 | 125.25-120.25 | A | 1.454 | 0.000 | 0.000 | 4.411 | 0.000 | 0.05 |
|  |  | B |  | 0.000 | 0.000 | 6.762 | 0.000 | 0.08 |
|  |  | C |  | 0.000 | 0.000 | 4.411 | 0.000 | 0.18 |
| L. 9 | 120.25-118.50 | A | 1.450 | 0.000 | 0.000 | 3.763 | 0.000 | 0.04 |
|  |  | B |  | 0.000 | 0.000 | 6.112 | 0.000 | 0.07 |
|  |  | C |  | 0.000 | 0.000 | 3.763 | 0.000 | 0.08 |
| L10 | 118.50-118.25 | A | 1.449 | 0.000 | 0.000 | 0.537 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 0.873 | 0.000 | 0.01 |
|  |  | C |  | 0.000 | 0.000 | 0.537 | 0.000 | 0.01 |
| L11 | 118.25-117.50 | A | 1.448 | 0.000 | 0.000 | 1.612 | 0.000 | 0.02 |
|  |  | B |  | 0.000 | 0.000 | 2.619 | 0.000 | 0.03 |
|  |  | C |  | 0.000 | 0.000 | 1.612 | 0.000 | 0.04 |
| L12 | 117.50-117.25 | A | 1.447 | 0.000 | 0.000 | 0.537 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 0.873 | 0.000 | 0.01 |
|  |  | C |  | 0.000 | 0.000 | 0.537 | 0.000 | 0.01 |
| 113 | 117.25-112.25 | A | 1.444 | 0.000 | 0.000 | 8.378 | 0.000 | 0.08 |
|  |  | B |  | 0.000 | 0.000 | 15.084 | 0.000 | 0.18 |
|  |  | C |  | 0.000 | 0.000 | 8.378 | 0.000 | 0.21 |
| L14 | 112.25-107.25 | A | 1.438 | 0.000 | 0.000 | 6.438 | 0.000 | 0.05 |
|  |  | B |  | 0.000 | 0.000 | 13.135 | 0.000 | 0.15 |
|  |  | C |  | 0.000 | 0.000 | 6.438 | 0.000 | 0.19 |
| L15 | 107.25-102.25 | A | 1.431 | 0.000 | 0.000 | 6.431 | 0.000 | 0.05 |
|  |  | B |  | 0.000 | 0.000 | 13.120 | 0.000 | 0.15 |
|  |  | C |  | 0.000 | 0.000 | 6.431 | 0.000 | 0.19 |
| L16 | 102.25-97.50 | A | 1.424 | 0.000 | 0.000 | 7.465 | 0.000 | 0.06 |
|  |  | B |  | 0.000 | 0.000 | 13.812 | 0.000 | 0.16 |
|  |  | C |  | 0.000 | 0.000 | 7.465 | 0.000 | 0.19 |
| L17 | 97.50-95.92 | A | 1.420 | 0.000 | 0.000 | 4.034 | 0.000 | 0.03 |
|  |  | B |  | 0.000 | 0.000 | 6.150 | 0.000 | 0.07 |
|  |  | C |  | 0.000 | 0.000 | 4.034 | 0.000 | 0.08 |
| L. 18 | 95.92-92.50 | A | 1.416 | 0.000 | 0.000 | 8.690 | 0.000 | 0.07 |
|  |  | B |  | 0.000 | 0.000 | 13.247 | 0.000 | 0.14 |
|  |  | C |  | 0.000 | 0.000 | 8.690 | 0.000 | 0.17 |
| L19 | 92.50-92.25 | A | 1.413 | 0.000 | 0.000 | 0.636 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 0.969 | 0.000 | 0.01 |
|  |  | C |  | 0.000 | 0.000 | 0.636 | 0.000 | 0.01 |
| L20 | 92.25-87.25 | A | 1.409 | 0.000 | 0.000 | 12.980 | 0.000 | 0.11 |

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| Tower Sectio <br> $n$ | Tower Elevation ft | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \\ \hline \end{gathered}$ | Ice Thickness in | $\begin{gathered} A_{R} \\ {f t^{2}}^{2} \end{gathered}$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\mathrm{C}_{A} A_{A}$ $\ln$ Face $f^{2}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Out Face } \\ {f t^{2}}^{2} \end{gathered}$ | Weight $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L21 | 87.25-87.00 | B | 1.405 | 0.000 | 0.000 | 19.641 | 0.000 | 0.21 |
|  |  | C |  | 0.000 | 0.000 | 12.980 | 0.000 | 0.24 |
|  |  | A |  | 0.000 | 0.000 | 0.656 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 0.989 | 0.000 | 0.01 |
| L22 | 87.00-82.00 | C | 1.401 | 0.000 | 0.000 | 0.656 | 0.000 | 0.01 |
|  |  | A |  | 0.000 | 0.000 | 12.584 | 0.000 | 0.10 |
|  |  | B |  | 0.000 | 0.000 | 19.235 | 0.000 | 0.20 |
| L23 | 82.00-77.00 | C | 1.392 | 0.000 | 0.000 | 12.584 | 0.000 | 0.24 |
|  |  | A |  | 0.000 | 0.000 | 6.809 | 0.000 | 0.06 |
|  |  | B |  | 0.000 | 0.000 | 13.449 | 0.000 | 0.15 |
| L24 | 77.00-72.00 | C | 1.383 | 0.000 | 0.000 | 6.809 | 0.000 | 0.19 |
|  |  | A |  | 0.000 | 0.000 | 6.800 | 0.000 | 0.06 |
|  |  | B |  | 0.000 | 0.000 | 13.429 | 0.000 | 0.15 |
| L25 | 72.00-67.00 | C | 1.374 | 0.000 | 0.000 | 6.800 | 0.000 | 0.19 |
|  |  | A |  | 0.000 | 0.000 | 10.400 | 0.000 | 0.08 |
|  |  | B |  | 0.000 | 0.000 | 17.017 | 0.000 | 0.18 |
| L26 | 67.00-63.25 | C | 1.365 | 0.000 | 0.000 | 10.400 | 0.000 | 0.22 |
|  |  | A |  | 0.000 | 0.000 | 10.150 | 0.000 | 0.08 |
|  |  | B |  | 0.000 | 0.000 | 15.104 | 0.000 | 0.15 |
| L27 | 63.25-63.00 | C | 1.360 | 0.000 | 0.000 | 10.150 | 0.000 | 0.18 |
|  |  | A |  | 0.000 | 0.000 | 0.676 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.006 | 0.000 | 0.01 |
| L28 | 63.00-58.00 | C | 1.355 | 0.000 | 0.000 | 0.676 | 0.000 | 0.01 |
|  |  | A |  | 0.000 | 0.000 | 14.348 | 0.000 | 0.11 |
|  |  | B |  | 0.000 | 0.000 | 20.941 | 0.000 | 0.21 |
| L29 | 58.00-56.75 | C | 1.348 | 0.000 | 0.000 | 14.348 | 0.000 | 0.25 |
|  |  | A |  | 0.000 | 0.000 | 3.792 | 0.000 | 0.03 |
|  |  | B |  | 0.000 | 0.000 | 5.438 | 0.000 | 0.05 |
| L30 | 56.75-56.50 | C | 1.346 | 0.000 | 0.000 | 3.792 | 0.000 | 0.06 |
|  |  | A |  | 0.000 | 0.000 | 0.758 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.087 | 0.000 | 0.01 |
| L31 | 56.50-47.50 | C | 1.334 | 0.000 | 0.000 | 0.758 | 0.000 | 0.01 |
|  |  | A |  | 0.000 | 0.000 | 22.108 | 0.000 | 0.17 |
|  |  | B |  | 0.000 | 0.000 | 33.931 | 0.000 | 0.34 |
| L32 | 47.50-47.00 | C | 1.322 | 0.000 | 0.000 | 22.108 | 0.000 | 0.41 |
|  |  | A |  | 0.000 | 0.000 | 0.842 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.499 | 0.000 | 0.02 |
| L33 | 47.00-42.00 | C | 1.314 | 0.000 | 0.000 | 0.842 | 0.000 | 0.02 |
|  |  | A |  | 0.000 | 0.000 | 8.397 | 0.000 | 0.06 |
|  |  | B |  | 0.000 | 0.000 | 14.939 | 0.000 | 0.15 |
| L34 | 42.00-37.00 | C | 1.298 | 0.000 | 0.000 | 8.397 | 0.000 | 0.20 |
|  |  | A |  | 0.000 | 0.000 | 13.154 | 0.000 | 0.10 |
|  |  | B |  | 0.000 | 0.000 | 19.677 | 0.000 | 0.19 |
| L35 | 37.00-34.25 | C | 1.285 | 0.000 | 0.000 | 13.154 | 0.000 | 0.23 |
|  |  | A |  | 0.000 | 0.000 | 8.969 | 0.000 | 0.07 |
|  |  | B |  | 0.000 | 0.000 | 12.546 | 0.000 | 0.12 |
| L36 | 34.25-34.00 | C | 1.279 | 0.000 | 0.000 | 8.969 | 0.000 | 0.14 |
|  |  | A |  | 0.000 | 0.000 | 0.815 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.140 | 0.000 | 0.01 |
| L37 | 34.00-29.00 | C | 1.269 | 0.000 | 0.000 | 0.815 | 0.000 | 0.01 |
|  |  | A |  | 0.000 | 0.000 | 16.214 | 0.000 | 0.12 |
|  |  | B |  | 0.000 | 0.000 | 22.776 | 0.000 | 0.21 |
| L38 | 29.00-26.75 | C | 1.254 | 0.000 | 0.000 | 16.290 | 0.000 | 0.26 |
|  |  | A |  | 0.000 | 0.000 | 7.210 | 0.000 | 0.05 |
|  |  | B |  | 0.000 | 0.000 | 10.230 | 0.000 | 0.09 |
| L39 | 26.75-26.50 | C | 1.248 | 0.000 | 0.000 | 7.320 | 0.000 | 0.11 |
|  |  | A |  | 0.000 | 0.000 | 0.801 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.136 | 0.000 | 0.01 |
| L40 | 26.50-21.50 | C | 1.235 | 0.000 | 0.000 | 0.813 | 0.000 | 0.01 |
|  |  | A |  | 0.000 | 0.000 | 16.003 | 0.000 | 0.12 |
|  |  | B |  | 0.000 | 0.000 | 22.682 | 0.000 | 0.20 |
| L. 41 | 21.50-16.75 | C | 1.207 | 0.000 | 0.000 | 16.238 | 0.000 | 0.25 |
|  |  | A |  | 0.000 | 0.000 | 14.508 | 0.000 | 0.10 |
|  |  | B |  | 0.000 | 0.000 | 20.807 | 0.000 | 0.18 |
| L42 | 16.75-16.50 | C | 1.191 | 0.000 | 0.000 | 8.667 | 0.000 | 0.19 |
|  |  | A |  | 0.000 | 0.000 | 0.806 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.136 | 0.000 | 0.01 |
|  |  | C |  | 0.000 | 0.000 | 0.414 | 0.000 | 0.01 |
| 143 | 16.50-14.25 | A | 1.181 | 0.000 | 0.000 | 7.250 | 0.000 | 0.05 |

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| Tower Sectio $n$ $\qquad$ | Tower Elevation ft | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Ice <br> Thickness in | $\begin{gathered} A_{R} \\ f^{2} \end{gathered}$ | $A F$ $f^{2}$ |  | $\qquad$ | Weight $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L44 | 14.25-14.00 | B | 1.171 | 0.000 | 0.000 | 10.213 | 0.000 | 0.09 |
|  |  | C |  | 0.000 | 0.000 | 3.719 | 0.000 | 0.09 |
|  |  | A |  | 0.000 | 0.000 | 0.805 | 0.000 | 0.01 |
|  |  | B |  | 0.000 | 0.000 | 1.133 | 0.000 | 0.01 |
|  | 14.00-9.00 | C | 1.147 | 0.000 | 0.000 | 0.413 | 0.000 | 0.01 |
| L45 |  | A |  | 0.000 | 0.000 | 13.665 | 0.000 | 0.09 |
|  |  | B |  | 0.000 | 0.000 | 22.603 | 0.000 | 0.19 |
|  | $9.00-4.25$ | C | 1.086 | 0.000 | 0.000 | 8.231 | 0.000 | 0.19 |
| 146 |  | A |  | 0.000 | 0.000 | 7.606 | 0.000 | 0.05 |
|  |  | B |  | 0.000 | 0.000 | 21.311 | 0.000 | 0.17 |
|  | 4.25-4.00 | C | 1.036 | 0.000 | 0.000 | 7.761 | 0.000 | 0.18 |
| L47 |  | A |  | 0.000 | 0.000 | 0.399 | 0.000 | 0.00 |
|  |  | B |  | 0.000 | 0.000 | 1.115 | 0.000 | 0.01 |
|  | 4.00-0.00 | C | 0.963 | 0.000 | 0.000 | 0.406 | 0.000 | 0.01 |
| L48 |  | A |  | 0.000 | 0.000 | 5.561 | 0.000 | 0.03 |
|  |  | B |  | 0.000 | 0.000 | 16.076 | ${ }^{\prime} 0.000$ | 0.12 |
|  |  | C |  | 0.000 | 0.000 | 5.632 | 0.000 | 0.14 |

Feed Line Center of Pressure

| Section | Elevation ft | $\begin{gathered} C P_{X} \\ \text { in } \end{gathered}$ | $\begin{gathered} C P_{Z} \\ \text { in } \end{gathered}$ | $\begin{gathered} C P_{X} \\ \text { ice } \\ \text { in } \end{gathered}$ | $\begin{aligned} & C P_{Z} \\ & \text { ice } \end{aligned}$ in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 151.00-146.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L2 | 146.00-141.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L3 | 141.00-136.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L4 | 136.00-131.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L5 | 131.00-126.00 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L6 | 126.00-125.50 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L7 | 125.50-125.25 | 0.0000 | 0.0000 | 0.0000 | 0.0000 |
| L8 | 125.25-120.25 | 0.8201 | -0.2585 | 1.0168 | -0.3205 |
| L9 | 120.25-118.50 | 1.2210 | -0.3849 | 1.5547 | -0.4901 |
| L10 | 118.50-118.25 | 1.2281 | -0.3871 | 1.5640 | -0.4930 |
| L11 | 118.25-117.50 | 1.2309 | -0.3880 | 1.5680 | -0.4943 |
| L12 | 117.50-117.25 | 1.2330 | -0.3887 | 1.5713 | -0.4953 |
| L13 | 117.25-112.25 | 1.4506 | -0.4573 | 1.8337 | -0.5780 |
| L14 | 112.25-107.25 | 1.7041 | -0.5372 | 2.1397 | -0.6745 |
| L.15 | 107.25-102.25 | 1.7340 | -0.5466 | 2.1849 | -0.6887 |
| L16 | 102.25-97.50 | 1.5879 | -0.5005 | 2.0217 | -0.6373 |
| L17 | 97.50-95.92 | 1.1925 | -0.3759 | 1.5437 | -0.4866 |
| L18 | 95.92-92.50 | 1.2047 | -0.3798 | 1.5607 | -0.4920 |
| L19 | 92.50-92.25 | 1.2137 | -0.3826 | 1.5734 | -0.4960 |
| L20 | 92.25-87.25 | 1.2053 | -0.3799 | 1.5702 | -0.4950 |
| L21 | 87.25-87.00 | 1.2070 | -0.3805 | 1.5770 | -0.4971 |
| L22 | 87.00-82.00 | 1.2519 | -0.3946 | 1.6353 | -0.5155 |
| L23 | 82.00-77.00 | 1.7937 | -0.5654 | 2.3132 | -0.7292 |
| L24 | 77.00-72.00 | 1.8193 | -0.5735 | 2.3523 | -0.7415 |
| L25 | 72.00-67.00 | 1.4749 | -0.4649 | 1.9307 | -0.6086 |
| L26 | 67.00-63.25 | 1.2744 | -0.4017 | 1.6801 | -0.5296 |
| L27 | 63.25-63.00 | 1.2830 | -0.4044 | 1.6923 | -0.5334 |
| L28 | 63.00-58.00 | 1.2344 | -0.3891 | 1.6453 | -0.5186 |
| L29 | 58.00-56.75 | 1.1924 | -0.3759 | 1.6046 | -0.5058 |
| L30 | 56.75-56.50 | 1.1957 | -0.3769 | 1.6091 | -0.5072 |
| L31 | 56.50-47.50 | 1.3803 | -0.4351 | 1.8562 | -0.5851 |
| L32 | 47.50-47.00 | 1.7003 | -0.5360 | 2.2817 | -0.7192 |
| L33 | 47.00-42.00 | 1.7124 | -0.5398 | 2.2972 | -0.7241 |
| L34 | 42.00-37.00 | 1.3295 | -0.4191 | 1.8264 | -0.5757 |
| L35 | 37.00-34.25 | 1.1648 | -0.3672 | 1.6161 | -0.5094 |
| L36 | 34.25-34.00 | 1.1702 | -0.3689 | 1.6233 | -0.5117 |
| L37 | 34.00-29.00 | 1.1796 | -0.3718 | 1.6389 | -0.4952 |
| L38 | 29.00-26.75 | 1.1925 | -0.3759 | 1.6626 | -0.4542 |
| L39 | 26.75-26.50 | 1.1969 | -0.3773 | 1.6682 | -0.4564 |
| 1.40 | 26.50-21.50 | 1.2061 | -0.3802 | 1.6797 | -0.4612 |
| L41 | 21.50-16.75 | -2.2376 | -3.4202 | -1.5447 | -3.3731 |
| L42 | 16.75-16.50 | -3.4048 | -4.4732 | -2.4634 | -4.1150 |
| L43 | 16.50-14.25 | -3.4203 | -4.4922 | -2.4769 | -4.1323 |
| L44 | 14.25-14.00 | -3.4354 | -4.5108 | -2.4905 | -4.1494 |
| L45 | 14.00-9.00 | -3.5337 | -3.7808 | -2.5467 | -3.4886 |

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| Section | Elevation <br> $f t$ | $C P_{x}$ <br> in | $C P_{z}$ <br> in | $C P x$ <br> lce <br> in | $C P_{z}$ <br> Ice <br> in |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{L46}$ | $9.00-4.25$ | -3.7736 | -1.7841 | -2.6823 | -1.7114 |
| $\mathrm{L47}$ | $4.25-4.00$ | -3.8044 | -1.7970 | -2.7225 | -1.7294 |
| L 48 | $4.00-0.00$ | -3.3723 | -1.7824 | -2.2882 | -1.7233 |

Note: For pole sections, center of pressure calculations do not consider feed line shielding.
Shielding Factor Ka

| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No lce } \end{gathered}$ | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L8 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 120.25- \\ 122.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 46 | MS-600 (L) | $\begin{array}{r} 120.25- \\ 120.50 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 47 | MS-600 (L) | $120.25-$ 120.50 | 1.0000 | 1.0000 |
| L8 | 48 | MS-600 (L) | $120.25-$ 120.50 | 1.0000 | 1.0000 |
| L8 | 50 | MP3-03 (L) | $120.25-$ 125.00 | 1.0000 | 1.0000 |
| L8 | 51 | MP3-03 (L) | $\begin{array}{r} 120.25- \\ 125.00 \end{array}$ | 1.0000 | 1.0000 |
| L8 | 52 | MP3-03 (L) | $\begin{array}{r} 120.25- \\ 12500 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 24 | AL.7-50(1-5/8) | $\begin{array}{r} 118.50- \\ 120.25 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 46 | MS-600 (L) | $\begin{array}{r} 118.50- \\ 120.25 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 47 | MS-600 (L) | $\begin{array}{r} 118.50- \\ 120.25 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 48 | MS-600 (L) | $\begin{array}{r} 118.50- \\ 120.25 \end{array}$ | 1.0000 | 1.0000 |
| L9 | 50 | MP3-03 (L) | $118.50-$ 120.25 | 1.0000 | 1.0000 |
| L9 | 51 | MP3-03 (L) | $118.50-$ 120.25 | 1.0000 | 1.0000 |
| L9 | 52 | MP3-03 (L) | $\begin{array}{r} 118.50- \\ 120.25 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L. 10 | 46 | MS-600 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 47 | MS-600 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 48 | MS-600 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 50 | MP3-03 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 51 | MP3-03 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L10 | 52 | MP3-03 (L) | $\begin{array}{r} 118.25- \\ 118.50 \end{array}$ | 1.0000 | 1.0000 |
| L.11 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L. 11 | 46 | MS-600 (L) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 47 | MS-600 (L) | $\begin{array}{r} 117.50= \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 48 | MS-600 (L) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 50 | MP3-03 (L) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 51 | MP3-03 (L) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L11 | 52 | MP3-03 (L) | $\begin{array}{r} 117.50- \\ 118.25 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 117.25 \\ 117.50 \end{array}$ | 1.0000 | 1.0000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { lce } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L12 | 46 | MS-600 (L) | $\begin{array}{r} \hline 117.25- \\ 117.50 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 47 | MS-600 (L) | $\begin{array}{r} 117.25- \\ 117.50 \end{array}$ | 1.0000 | 1.0000 |
| L12 | 48 | MS-600 (L) | $117.25-$ 117.50 | 1.0000 | 1.0000 |
| L12 | 50 | MP3-03 (L) | $117.25-$ 117.50 | 1.0000 | 1.0000 |
| L12 | 51 | MP3-03 (L) | $117.25-$ 117.50 | 1.0000 | 1.0000 |
| L12 | 52 | MP3-03 (L) | $\begin{array}{r} 117.25- \\ 117.50 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 112.25= \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 46 | MS-600 (L) | $\begin{array}{r} 112.25- \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 47 | MS-600 (L) | $\begin{array}{r} 112.25= \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 48 | MS-600 (L) | $\begin{array}{r} 112.25 \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 50 | MP3-03 (L) | $\begin{array}{r} 115.00- \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 51 | MP3-03 (L) | $\begin{array}{r} 115.00- \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L13 | 52 | MP3-03 (L) | $\begin{array}{r} 115.00- \\ 117.25 \end{array}$ | 1.0000 | 1.0000 |
| L14 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 107.25- \\ 112.25 \end{array}$ | 1.0000 | 1.0000 |
| L14 | 46 | MS-600 (L) | 107.25- | 1.0000 | 1.0000 |
| L14 | 47 | MS-600 (L) | $\begin{array}{r} 107.25 \\ 112.25 \end{array}$ | 1.0000 | 1.0000 |
| L14 | 48 | MS-600 (L) | $\begin{array}{r} 107.25- \\ 112.25 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 102.25- \\ 107.25 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 46 | MS-600 (L) | $\begin{array}{r} 102.25- \\ 107.25 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 47 | MS-600 (L) | $\begin{array}{r} 102.25- \\ 107.25 \end{array}$ | 1.0000 | 1.0000 |
| L15 | 48 | MS-600 (L) | $\begin{array}{r} 102.25- \\ 107.25 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 24 | AL7-50(1-5/8) | $\begin{aligned} & 97.50- \\ & 102.25 \end{aligned}$ | 1.0000 | 1.0000 |
| L16 | 43 | MS-600 (L) | $\begin{array}{r} 97.50- \\ 98.58 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 44 | MS-600 (L) | $\begin{array}{r} 97.50- \\ 98.58 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 45 | MS-600 (L) | $\begin{array}{r} 97.50- \\ 98.58 \end{array}$ | 1.0000 | 1.0000 |
| L16 | 46 | MS-600 (L) | $\begin{aligned} & 97.50- \\ & 102.25 \end{aligned}$ | 1.0000 | 1.0000 |
| L.16 | 47 | MS-600 (L) | $\begin{aligned} & 97.50- \\ & 102.25 \end{aligned}$ | 1.0000 | 1.0000 |
| L16 | 48 | MS-600 (L) | $\begin{aligned} & 97.50- \\ & 102.25 \end{aligned}$ | 1.0000 | 1.0000 |
| L18 | 24 | AL7-50(1-5/8) | $92.50-$ 95.92 | 1.0000 | 1.0000 |
| L18 | 43 | MS-600 (L) | $\begin{array}{r} 92.50- \\ 95.92 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 44 | MS-600 (L) | 92.50-1 | 1.0000 | 1.0000 |
| L18 | 45 | MS-600 (L) | $\begin{array}{r} 92.50- \\ 95.92 \end{array}$ | 1.0000 | 1.0000 |
| L18 | 46 | MS-600 (L) | $92.50-$ 95.92 | 1.0000 | 1.0000 |
| L18 | 47 | MS-600 (L) | $\begin{array}{r} 92.50- \\ 95.92 \end{array}$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { Ice } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L18 | 48 | MS-600 (L) | $\begin{array}{r} 92.50 \\ 95.92 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 92.25- \\ 92.50 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 43 | MS-600 (L) | $92.25-$ 92.50 | 1.0000 | 1.0000 |
| L19 | 44 | MS-600 (L) | $92.25-$ 92.50 | 1.0000 | 1.0000 |
| L19 | 45 | MS-600 (L) | $\begin{array}{r} 92.25- \\ 92.50 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 46 | MS-600 (L) | $\begin{array}{r} 92.25- \\ 92.50 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 47 | MS-600 (L) | $\begin{array}{r} 92.25- \\ 92.50 \end{array}$ | 1.0000 | 1.0000 |
| L19 | 48 | MS-600 (L) | $\begin{array}{r} 92.25- \\ 92.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 87.25- \\ 92.25 \end{array}$ | 1.0000 | 1.0000 |
| 1.20 | 40 | MS-650 (L) | $\begin{array}{r} 87.25 \\ 90.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 41 | MS-650 (L) | $\begin{array}{r} 87.25- \\ 90.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 42 | MS-650 (L) | $\begin{array}{r} 87.25- \\ 90.50 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 43 | MS-600 (L) | $\begin{array}{r} 87.25- \\ 92.25 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 44 | MS-600 (L) | $\begin{array}{r} 87.25- \\ 92.25 \end{array}$ | 1.0000 | 1.0000 |
| L20 | 45 | MS-600 (L) | $87.25-$ 92.25 | 1.0000 | 1.0000 |
| L20 | 46 | MS-600 (L) | 90.50- | 1.0000 | 1.0000 |
| L20 | 47 | MS-600 (L) | $90.50-$ 92.25 | 1.0000 | 1.0000 |
| L20 | 48 | MS-600 (L) | $90.50-$ 92.25 | 1.0000 | 1.0000 |
| L21 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 40 | MS-650 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 41 | MS-650 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 42 | MS-650 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 43 | MS-600 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 44 | MS-600 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| L21 | 45 | MS-600 (L) | $\begin{array}{r} 87.00- \\ 87.25 \end{array}$ | 1.0000 | 1.0000 |
| 422 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 82.00- \\ 87.00 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 40 | MS-650 (L) | $82.00-$ 87.00 | 1.0000 | 1.0000 |
| L22 | 41 | MS-650 (L) | $82.00-$ 87.00 | 1.0000 | 1.0000 |
| L22 | 42 | MS-650 (L) | $\begin{array}{r} 82.00- \\ 87.00 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 43 | MS-600 (L) | $82.42-$ 87.00 | 1.0000 | 1.0000 |
| L22 | 44 | MS-600 (L) | $\begin{array}{r} 82.42- \\ 87.00 \end{array}$ | 1.0000 | 1.0000 |
| L22 | 45 | MS-600 (L) | $\begin{array}{r} 82.42- \\ 87.00 \end{array}$ | 1.0000 | 1.0000 |
| L23 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 77.00- \\ 82.00 \end{array}$ | 1.0000 | 1.0000 |
| 123 | 40 | MS-650 (L) | $\begin{array}{r} 77.00- \\ 82.00 \end{array}$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No lce } \end{gathered}$ | $\begin{aligned} & \hline K_{a} \\ & \text { lce } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L23 | 41 | MS-650 (L) | $\begin{array}{r} 77.00- \\ 82.00 \end{array}$ | 1.0000 | 1.0000 |
| 123 | 42 | MS-650 (L) | 77.00 82.00 | 1.0000 | 1.0000 |
| L. 24 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 72.00- \\ 77.00 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 40 | MS-650 (L) | $72.00-$ 77.00 | 1.0000 | 1.0000 |
| L24 | 41 | MS-650 (L) | $\begin{array}{r} 72.00- \\ 77.00 \end{array}$ | 1.0000 | 1.0000 |
| L24 | 42 | MS-650 (L) | $\begin{array}{r} 72.00- \\ 77.00 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 67.00- \\ 72.00 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 37 | MS-650 (L) | $\begin{array}{r} 67.00- \\ 69.67 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 38 | MS-650 (L) | $\begin{array}{r} 67.00- \\ 69.67 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 39 | MS-650 (L) | $\begin{array}{r} 67.00- \\ 69.67 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 40 | MS-650 (L) | $\begin{array}{r} 67.00- \\ 72.00 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 41 | MS-650 (L) | $\begin{array}{r} 67.00 \\ 72.00 \end{array}$ | 1.0000 | 1.0000 |
| L25 | 42 | MS-650 (L) | $\begin{array}{r} 67.00- \\ 72.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 37 | MS-650 (L) | $63.25-1$ 67.00 | 1.0000 | 1.0000 |
| L26 | 38 | MS-650 (L) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 39 | MS-650 (L) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 40 | MS-650 (L) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 41 | MS-650 (L) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L26 | 42 | MS-650 (L) | $\begin{array}{r} 63.25- \\ 67.00 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 37 | MS-650 (L) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 38 | MS-650 (L) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 39 | MS-650 (L) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 40 | MS-650 (L) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 41 | MS-650 (L) | $\begin{array}{r} 63.00- \\ 63.25 \end{array}$ | 1.0000 | 1.0000 |
| L27 | 42 | MS-650 (L) | $63.00-$ 63.25 | 1.0000 | 1.0000 |
| L28 | 24 | AL7-50(1-5/8) | 58.00 63.00 | 1.0000 | 1.0000 |
| L28 | 34 | MS-850 (L) | $\begin{array}{r} 58.00- \\ 60.50 \end{array}$ | 1.0000 | 1.0000 |
| 1.28 | 35 | MS-850 (L) | $58.00-$ 60.50 | 1.0000 | 1.0000 |
| L28 | 36 | MS-850 (L) | $\begin{array}{r} 58.00- \\ 60.50 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 37 | MS-650 (L) | $\begin{array}{r} 58.00- \\ 63.00 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 38 | MS-650 (L) | 58.00- | 1.0000 | 1.0000 |
| L28 | 39 | MS-650 (L) | $\begin{array}{r} 58.00- \\ 63.00 \end{array}$ | 1.0000 | 1.0000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{a} \\ \text { No lee } \end{gathered}$ | $K_{B}$ Ice |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 128 | 40 | MS-650 (L) | $\begin{array}{r} 60.50- \\ 63.00 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 41 | MS-650 (L) | $\begin{array}{r} 60.50 \\ 63.00 \end{array}$ | 1.0000 | 1.0000 |
| L28 | 42 | MS-650 (L) | $60.50-$ 63.00 | 1.0000 | 1.0000 |
| L29 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 56.75- \\ 58.00 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 34 | MS-850 (L) | $\begin{array}{r} 56.75- \\ 58.00 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 35 | MS-850 (L) | $\begin{array}{r} 56.75- \\ 58.00 \end{array}$ | 1.0000 | 1.0000 |
| L29 | 36 | MS-850 (L) | $56.75-$ 58.00 | 1.0000 | 1.0000 |
| L29 | 37 | MS-650 (L) | $56.75-$ 58.00 | 1.0000 | 1.0000 |
| L29 | 38 | MS-650 (L) | $56.75-$ $58.00$ | 1.0000 | 1.0000 |
| L29 | 39 | MS-650 (L) | $\begin{array}{r} 50.00 \\ 56.75 \\ 58.00 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 56.50- \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 34 | MS-850 (L) | $\begin{array}{r} 56.50 \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 35 | MS-850 (L) | $\begin{array}{r} 56.50 \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 36 | MS-850 (L) | $\begin{array}{r} 56.50- \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 37 | MS-650 (L) | $\begin{array}{r} 56.50 \\ 56.50 \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 38 | MS-650 (L) | $\begin{array}{r} 56.50- \\ 56.75 \end{array}$ | 1.0000 | 1.0000 |
| L30 | 39 | MS-650 (L) | $56.50-$ 56.75 | 1.0000 | 1.0000 |
| L. 31 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 50.10 \\ 47.50- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 34 | MS-850 (L) | $\begin{array}{r} 20.50 \\ 47.50- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 35 | MS-850 (L) | $\begin{array}{r} 47.50- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 36 | MS-850 (L) | $\begin{array}{r} 50.00 \\ 47.50- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 37 | MS-650 (L) | $\begin{array}{r} 51.33- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 38 | MS-650 (L) | $\begin{array}{r} 50.30 \\ 51.33- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L31 | 39 | MS-650 (L) | $\begin{array}{r} 51.33- \\ 56.50 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 42.00- \\ 47.00 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 34 | MS-850 (L) | $\begin{array}{r} 47.00 \\ 42.00- \\ 47.00 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 35 | MS-850 (L) | $\begin{array}{r} 42.00- \\ 47.00 \end{array}$ | 1.0000 | 1.0000 |
| L33 | 36 | MS-850 (L) | $\begin{array}{r} 42.00- \\ 47.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 47.00 \\ 42.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 31 | MS-850 (L) | $\begin{array}{r} 42.00 \\ 40.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 32 | MS-850 (L) | $\begin{array}{r} 37.00- \\ 40.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 33 | MS-850 (L) | $\begin{array}{r} 37.00- \\ 40.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 34 | MS-850 (L) | $\begin{array}{r} 37.00 \\ 42.00 \end{array}$ | 1.0000 | 1.0000 |
| L34 | 35 | MS-850 (L) | 37.00 42.00 | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ No lce | $\begin{aligned} & K_{a} \\ & \text { lce } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L34 | 36 | MS-850 (L) | $\begin{array}{r} 37.00- \\ 42.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 34.25- \\ 37.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 31 | MS-850 (L) | $\begin{array}{r} 34.25 \\ 37.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 32 | MS-850 (L) | $\begin{array}{r} 34.25- \\ 37.00 \end{array}$ | 1.0000 | 1.0000 |
| L35 | 33 | MS-850 (L) | $34.25-$ 37.00 | 1.0000 | 1.0000 |
| 135 | 34 | MS-850 (L) | $34.25-$ 37.00 | 1.0000 | 1.0000 |
| L35 | 35 | MS-850 (L) | $34.25-$ 37.00 | 1.0000 | 1.0000 |
| L35 | 36 | MS-850 (L) | $34.25-$ 37.00 | 1.0000 | 1.0000 |
| L36 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 34.00- \\ 34.25 \end{array}$ | 1.0000 | 1.0000 |
| 136 | 31 | MS-850 (L) | $\begin{array}{r} 34.00- \\ 34.25 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 32 | MS-850 (L) | $\begin{array}{r} 34.00- \\ 34.25 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 33 | MS-850 (L) | $\begin{array}{r} 34.00 \\ 34.00- \\ 34.25 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 34 | MS-850 (L) | $34.00-$ 34.25 | 1.0000 | 1.0000 |
| L36 | 35 | MS-850 (L) | $\begin{array}{r} 34.00- \\ 34.25 \end{array}$ | 1.0000 | 1.0000 |
| L36 | 36 | MS-850 (L) | 34.00-1 | 1.0000 | 1.0000 |
| L37 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 29.00- \\ 34.00 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 26 | MS-850 (L) | $\begin{array}{r} 29.00- \\ 30.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 27 | MS-850 (L) | $\begin{array}{r} 29.00- \\ 30.50 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 28 | MS-850 (L) | $29.00-$ 30.50 | 1.0000 | 1.0000 |
| L37 | 31 | MS-850 (L) | $29.00-$ 34.00 | 1.0000 | 1.0000 |
| L37 | 32 | MS-850 (L) | $39.00-$ 34.00 | 1.0000 | 1.0000 |
| L37 | 33 | MS-850 (L) | $29.00-$ 34.00 | 1.0000 | 1.0000 |
| L37 | 34 | MS-850 (L) | $\begin{array}{r} 30.50- \\ 34.00 \end{array}$ | 1.0000 | 1.0000 |
| L37 | 35 | MS-850 (L) | $30.50-$ 34.00 | 1.0000 | 1.0000 |
| L37 | 36 | MS-850 (L) | $30.50-$ 34.00 | 1.0000 | 1.0000 |
| L38 | 24 | AL7-50(1-5/8) | $26.75-$ 29.00 | 1.0000 | 1.0000 |
| L38 | 26 | MS-850 (L) | $\begin{array}{r} 26.75- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 27 | MS-850 (L) | $26.75-$ 29.00 | 1.0000 | 1.0000 |
| L38 | 28 | MS-850 (L) | $\begin{array}{r} 26.75- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 31 | MS-850 (L) | $\begin{array}{r} 26.75- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 32 | MS-850 (L) | $\begin{array}{r} 26.75- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L38 | 33 | MS-850 (L) | $\begin{array}{r} 26.75- \\ 29.00 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 26 | MS-850 (L) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |

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| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $K_{a}$ Nolce | $\begin{aligned} & K_{a} \\ & \text { lce } \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L39 | 27 | MS-850 (L) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 28 | MS-850 (L) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 31 | MS-850 (L) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L39 | 32 | MS-850 (L) | $\begin{array}{r} 26.50-1 \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L. 39 | 33 | MS-850 (L) | $\begin{array}{r} 26.50- \\ 26.75 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 21.50- \\ 26.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 26 | MS-850 (L) | $\begin{array}{r} 21.50- \\ 26.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 27 | MS-850 (L) | $21.50-$ 26.50 | 1.0000 | 1.0000 |
| L40 | 28 | MS-850 (L) | $\begin{array}{r} 21.50- \\ 26.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 31 | MS-850 (L) | $\begin{array}{r} 21.50- \\ 26.50 \end{array}$ | 1.0000 | 1.0000 |
| L40 | 32 | MS-850 (L) | 21.50-1 | 1.0000 | 1.0000 |
| L40 | 33 | MS-850 (L) | $21.50-$ 26.50 | 1.0000 | 1.0000 |
| L41 | 24 | AL.7-50(1-5/8) | $\begin{array}{r} 16.75 \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 26 | MS-850 (L) | $16.75-$ 21.50 | 1.0000 | 1.0000 |
| L41 | 27 | MS-850 (L) | $\begin{array}{r} 16.75- \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| $\llcorner 41$ | 28 | MS-850 (L) | $\begin{array}{r} 16.75- \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 29 | MS-850 (L) | $16.75-$ 20.50 | 1.0000 | 1.0000 |
| $\llcorner 41$ | 30 | MS-850 (L) | $\begin{array}{r} 16.75- \\ 20.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 31 | MS-850 (L) | $\begin{array}{r} 21.00- \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 32 | MS-850 (L) | $\begin{array}{r} 21.00- \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| L41 | 33 | MS-850 (L) | $\begin{array}{r} 21.00- \\ 21.50 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 16.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 26 | MS-850 (L) | $16.50-$ 16.75 | 1.0000 | 1.0000 |
| L42 | 27 | MS-850 (L) | $16.50-$ 16.75 | 1.0000 | 1.0000 |
| $\llcorner 42$ | 28 | MS-850 (L) | $\begin{array}{r} 16.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 29 | MS-850 (L) | $\begin{array}{r} 16.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L42 | 30 | MS-850 (L) | $\begin{array}{r} 16.50- \\ 16.75 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 14.25- \\ 16.50 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 26 | MS-850 (L) | $\begin{array}{r} 14.25-5 \\ 16.50 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 27 | MS-850 (L) | $\begin{array}{r} 14.25- \\ 16.50 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 28 | MS-850 (L) | $\begin{array}{r} 14.25- \\ 16.50 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 29 | MS-850 (L) | $\begin{array}{r} 14.25- \\ 16.50 \end{array}$ | 1.0000 | 1.0000 |
| L43 | 30 | MS-850 (L) | $14.25-$ 16.50 | 1.0000 | 1.0000 |
| 144 | 24 | AL7-50(1-5/8) | $\begin{array}{r} 14.00- \\ 14.25 \end{array}$ | 1.0000 | 1.0000 |


| Tower Section | Feed Line Record No. | Description | Feed Line Segment Elev. | $\begin{gathered} K_{\mathrm{a}} \\ \text { No Ice } \end{gathered}$ | $\begin{gathered} K_{a} \\ \text { Ice } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L44 | 26 | MS-850 (L) | $14.00-$ 14.25 | 1.0000 | 1.0000 |
| L44 | 27 | MS-850 (L) | $14.00-$ 14.25 | 1.0000 | 1.0000 |
| L44 | 28 | MS-850 (L) | $14.00-$ 14.25 | 1.0000 | 1.0000 |
| L44 | 29 | MS-850 (L) | $14.00-$ 14.25 | 1.0000 | 1.0000 |
| L44 | 30 | MS-850 (L) | $14.00-$ 14.25 | 1.0000 | 1.0000 |
| $\llcorner 45$ | 24 | AL7-50(1-5/8) | 9.00-14.00 | 1.0000 | 1.0000 |
| L45 | 26 | MS-850 (L) | $10.50-$ 14.00 | 1.0000 | 1.0000 |
| L45 | 27 | MS-850 (L) | 9.00-14.00 | 1.0000 | 1.0000 |
| L45 | 28 | MS-850 (L) | 9.00-14.00 | 1.0000 | 1.0000 |
| L45 | 29. | MS-850 (L) | 9.00-14.00 | 1.0000 | 1.0000 |
| L45 | 30 | MS-850 (L) | 9.00-14.00 | 1.0000 | 1.0000 |
| L46 | 24 | AL7-50(1-5/8) | 4.25-9.00 | 1.0000 | 1.0000 |
| L46 | 27 | MS-850 (L) | 4.25-9.00 | 1.0000 | 1.0000 |
| L46 | 28 | MS-850 (L) | 4.25-9.00 | 1.0000 | 1.0000 |
| L46 | 29 | MS-850 (L) | $4.25-9.00$ | 1.0000 | 1.0000 |
| L46 | 30 | MS-850 (L) | 4.25-9.00 | 1.0000 | 1.0000 |
| L47 | 24 | AL7-50(1-5/8) | $4.00-4.25$ | 1.0000 | 1.0000 |
| L47 | 27 | MS-850 (L) | 4.00-4.25 | 1.0000 | 1.0000 |
| L47 | 28 | MS-850 (L) | 4.00-4.25 | 1.0000 | 1.0000 |
| L47 | 29 | MS-850 (L) | 4.00-4.25 | 1.0000 | 1.0000 |
| L47 | 30 | MS-850 (L) | 4.00-4.25 | 1.0000 | 1.0000 |
| L48 | 24 | AL7-50(1-5/8) | 0.00-4.00 | 1.0000 | 1.0000 |
| L48 | 27 | MS-850 (L) | 0.50-4.00 | 1.0000 | 1.0000 |
| L48 | 28 | MS-850 (L) | 0.50-4.00 | 1.0000 | 1.0000 |
| L48 | 29 | MS-850 (L) | 0.50-4.00 | 1.0000 | 1.0000 |
| L48 | 30 | MS-850 (L) | 0.50-4.00 | 1.0000 | 1.0000 |

Discrete Tower Loads

| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ | Placement ft |  | $C_{A} A_{A}$ Front $t t^{2}$ | $C_{A} A_{A}$ Side $f^{2}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (2) AM-X-CD-16-65-00TRET w/ Mount Pipe | A | From Leg | 4.00 | 0.0000 | 148.00 | No lce | 4.63 | 3.27 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 5.06 | 3.69 | 0.13 |
|  |  |  | 1.00 |  |  | Ice | 5.51 | 4.12 | 0.20 |
|  |  |  |  |  |  | 1 " Ice | 6.43 | 5.00 | 0.38 |
| (2) AM-X-CD-16-65-00TRET w/ Mount Pipe | B |  |  |  |  | $2^{\prime \prime}$ Ice |  |  |  |
|  |  | From Leg | 4.00 | 0.0000 | 148.00 | No lce | 4.63 | 3.27 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 5.06 | 3.69 | 0.13 |
|  |  |  | 1.00 |  |  | Ice | 5.51 | 4.12 | 0.20 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" Ice } \\ & 2^{\prime \prime} \text { Ice } \end{aligned}$ | 6.43 | 5.00 | 0.38 |
| (2) AM-X-CD-16-65-00TRET w/ Mount Pipe | C | From Leg | 4.00 | 0.0000 | 148.00 | No Ice | 4.63 | 3.27 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 5.06 | 3.69 | 0.13 |
|  |  |  | 1.00 |  |  | Ice | 5.51 | 4.12 | 0.20 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 6.43 | 5.00 | 0.38 |
|  |  |  |  |  |  | 2" lce |  |  |  |
| 80010121 w/ Mount Pipe | A | From Leg | 4.00 | 0.0000 | 148.00 | No Ice | 5.74 | 4.95 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 6.34 | 6.02 | 0.12 |
|  |  |  | 1.00 |  |  | lce | 6.86 | 6.81 | 0.18 |
|  |  |  |  |  |  | 1 I' Ice | 7.91 | 8.41 | 0.32 |
|  |  |  |  |  |  | 2 " Ice |  |  |  |
| 80010121 w/ Mount Pipe | B | From Leg | 4.00 | 0.0000 | 148.00 | No Ice | 5.74 | 4.95 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 6.34 | 6.02 | 0.12 |
|  |  |  | 1.00 |  |  | Ice | 6.86 | 6.81 | 0.18 |
|  |  |  |  |  |  | 1" Ice | 7.91 | 8.41 | 0.32 |
|  |  |  |  |  |  | $2^{\prime \prime} \text { Ice }$ |  |  |  |
| 80010121 w/ Mount Pipe | C | From Leg | 4.00 | 0.0000 | 148.00 | No Ice | 5.74 | 4.95 | 0.07 |
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151 Ft Monopole Tower Structural Analysis
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| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: Horz Lateral Vert ft ft $f t$ | Azimuth Adjustmen ! | Placement $f t$ |  | $C_{A} A_{A}$ Front $f^{2}$ | $C_{A} A_{A}$ Side $f^{2}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| (2) $\mathrm{NHH}-65 \mathrm{C}-\mathrm{R} 2 \mathrm{~B}$ w Mount Pipe | C | From Leg |  | 0.0000 | 140.00 | $\begin{aligned} & \text { 1" Ice } \\ & 2 " \text { Ice } \end{aligned}$ | 14.44 | 15.19 | 0.51 |
|  |  |  | $\begin{aligned} & 4.00 \\ & 0.00 \end{aligned}$ |  |  | No lce 1/2" lce | 11.63 12.35 13.07 | 9.79 11.31 | 0.08 0.17 |
|  |  |  | 0.00 |  |  | Ice | 13.07 | 12.85 | 0.27 |
| DB-T1-6Z-8AB-0Z | A | From Leg |  | 0.0000 | 140.00 | $\begin{aligned} & 1^{\prime \prime} \text { Ice } \\ & 2^{\prime \prime} \text { Ice } \end{aligned}$ | 14.44 | 15.19 | 0.51 |
|  |  |  | 4.00 |  |  | No Ice | 4.80 | 2.00 | 0.04 |
|  |  |  | 0.00 |  |  | 1/2" | 5.07 | 2.19 | 0.08 |
|  |  |  | 0.00 |  |  | Ice | 5.35 | 2.39 | 0.12 |
| (3) RFV01U-D2A | A | From Leg |  | 0.0000 | 140.00 | $\begin{aligned} & 1 " \text { Ice } \\ & 2 " \text { Ice } \end{aligned}$ | 5.93 | 2.81 | 0.21 |
|  |  |  | 4.00 |  |  | No Ice | 1.88 | 1.01 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 2.05 | 1.14 | 0.09 |
|  |  |  | 0.00 |  |  | Ice | 2.22 | 1.28 | 0.11 |
| (3) RFV01U-D1A | B | From Leg |  | 0.0000 | 140.00 | $\begin{aligned} & 1^{\prime \prime} \text { Ice } \\ & 2^{\prime \prime} \text { Ice } \end{aligned}$ | 2.60 | 1.59 | 0.15 |
|  |  |  | 4.00 |  |  | No Ice | 1.88 | 1.25 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 2.05 | 1.39 | 0.10 |
|  |  |  | 0.00 |  |  | Ice | 2.22 | 1.54 | 0.12 |
| Platform Mount [LP 303-1] | C | None |  | 0.0000 | 140.00 | 1" Ice | 2.60 | 1.86 | 0.18 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
|  |  |  |  |  |  | No Ice | 14.66 | 14.66 | 1.25 |
|  |  |  |  |  |  | 1/2" | 18.87 | 18.87 | 1.48 |
|  |  |  |  |  |  | Ice | 23.08 | 23.08 | 1.71 |
| Miscellaneous [NA 507-1] | C | None |  | 0.0000 |  | $1{ }^{\prime \prime}$ Ice | 31.50 | 31.50 | 2.18 |
|  |  |  |  |  | 140.00 | 2"Ice |  |  |  |
|  |  |  |  |  |  | No Ice | 4.80 | 4.80 | 0.25 |
|  |  |  |  |  |  | 1/2" | 6.70 | 6.70 | 0.29 |
|  |  |  |  |  |  | Ice | 8.60 | 8.60 | 0.34 |
| (2) Miscellaneous [NA 5093] | C | None |  | 0.0000 | 140.00 | 1" Ice | 12.40 | 12.40 | 0.44 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
|  |  |  |  |  |  | No Ice | 11.84 | 11.84 | 0.28 |
|  |  |  |  |  |  | 1/2" | 16.96 | 16.96 | 0.30 |
|  |  |  |  |  |  | Ice | 22.08 | 22.08 | 0.32 |
|  |  |  |  |  |  | 1 1'Ice | 32.32 | 32.32 | 0.36 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| TME-1900MHZ RRH | A | From Leg | 4.00 | 0.0000 | 132.00 | No Ice | 2.49 | 3.26 | 0.04 |
|  |  |  | 0.00 |  |  | 1/2" | 2.70 | 3.48 | 0.08 |
|  |  |  | -1.00 |  |  | Ice | 2.91 | 3.72 | 0.11 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 3.35 | 4.21 | 0.19 |
| TME-1900MHZ RRH | B | From Leg |  | 0.0000 | 132.00 | 2"Ice |  |  |  |
|  |  |  | 4.00 |  |  | No Ice | 2.49 | 3.26 | 0.04 |
|  |  |  | 0.00 |  |  | 1/2" | 2.70 | 3.48 | 0.08 |
|  |  |  | -1.00 |  |  | Ice | 2.91 | 3.72 | 0.11 |
|  | C | From Leg |  | 0.0000 | 132.00 | 1" Ice | 3.35 | 4.21 | 0.19 |
| TME-1900MHZ RRH |  |  |  |  |  | 2" Ice |  |  |  |
|  |  |  | 4.00 |  |  | No Ice | 2.49 | 3.26 | 0.04 |
|  |  |  | 0.00 |  |  | 1/2" | 2.70 | 3.48 | 0.08 |
|  |  |  | -1.00 |  |  | Ice | 2.91 | 3.72 | 0.11 |
|  |  |  |  |  |  | 1 I' Ice | 3.35 | 4.21 | 0.19 |
| 800 EXTERNAL NOTCH <br> FILTER |  |  |  |  |  | 2"Ice |  |  |  |
|  | A | From Leg | 4.00 | 0.0000 | 132.00 | No Ice | 0.66 | 0.32 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2" | 0.76 | 0.40 | 0.02 |
|  |  |  | -1.00 |  |  | Ice | 0.87 | 0.48 | 0.02 |
|  |  |  |  |  |  | $1^{\prime \prime}$ Ice | 1.11 | 0.67 | 0.04 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| 800 EXTERNAL NOTCH FILTER | $B$ | From Leg | 4.00 | 0.0000 | 132.00 | No Ice | 0.66 | 0.32 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2" | 0.76 | 0.40 | 0.02 |
|  |  |  | -1.00 |  |  | ice | 0.87 | 0.48 | 0.02 |
|  |  |  |  |  |  | 1' Ice | 1.11 | 0.67 | 0.04 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| 800 EXTERNAL NOTCH <br> FILTER | C | From Leg | 4.00 | 0.0000 | 132.00 | No Ice | 0.66 | 0.32 | 0.01 |
|  |  |  | 0.00 |  |  |  | 0.76 | 0.40 | 0.02 |

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| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ | Placement ft |  | $C_{A} A_{A}$ Front $f^{2}$ | $C_{A} A_{A}$ Side $f^{2}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 800MHZ RRH | A | From Leg | -1.00 | 0.0000 | 132.00 | 1/2" | 0.87 | 0.48 | 0.02 |
|  |  |  |  |  |  | Ice | 1.11 | 0.67 | 0.04 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" Ice } \\ & \text { 2" Ice } \end{aligned}$ |  |  |  |
|  |  |  | 4.00 |  |  | No Ice | 2.13 | 1.77 | 0.05 |
|  |  |  | 0.00 |  |  | 1/2" | 2.32 | 1.95 | 0.07 |
|  |  |  | -1.00 |  |  | Ice | 2.51 | 2.13 | 0.10 |
|  | B | From Leg |  | 0.0000 | 132.00 | $1{ }^{\prime \prime}$ Ice | 2.92 | 2.51 | 0.16 |
| 800MHZ RRH |  |  |  |  |  | 2" Ice |  |  |  |
|  |  |  | 4.00 |  |  | Nolce | 2.13 | 1.77 | 0.05 |
|  |  |  | 0.00 |  |  | 1/2' | 2.32 | 1.95 | 0.07 |
|  |  |  | -1.00 |  |  | Ice | 2.51 | 2.13 | 0.10 |
|  | C | From Leg |  | 0.0000 | 132.00 | 1 Ice | 2.92 | 2.51 | 0.16 |
| 800MHZ RRH |  |  |  |  |  | 2 " Ice |  |  |  |
|  |  |  | 4.00 |  |  | No lce | 2.13 | 1.77 | 0.05 |
|  |  |  | 0.00 |  |  | 1/2" | 2.32 | 1.95 | 0.07 |
|  |  |  | -1.00 |  |  | Ice | 2.51 | 2.13 | 0.10 |
|  | C | None |  | 0.0000 | 132.00 | 1 Ice | 2.92 | 2.51 | 0.16 |
| Pipe Mount [PM 601-3] |  |  |  |  |  | 2" Ice |  |  |  |
|  |  |  |  |  |  | No Ice | 4.39 | 4.39 | 0.20 |
|  |  |  |  |  |  | 1/2" | 5.48 | 5.48 | 0.24 |
|  |  |  |  |  |  | Ice | 6.57 | 6.57 | 0.28 |
|  |  |  |  |  |  | 1" Ice | 8.75 | 8.75 | 0.36 |
| *** |  |  |  |  |  | 2" Ice |  |  |  |
| GPS-TMG-HR-26NCM | A | From Leg | $4.00$ | 0.0000 | 130.00 | No Ice | 0.13 | 0.13 | 0.00 |
|  |  |  | 0.00 |  |  | 1/2" | 0.18 | 0.18 | 0.00 |
|  |  |  | 3.00 |  |  | Ice | 0.24 | 0.24 | 0.01 |
|  |  |  |  |  |  | 1" Ice | 0.37 | 0.37 | 0.01 |
| APXVSPP18-C-A20 w/ Mount Pipe |  |  |  |  |  | 2" Ice |  |  |  |
|  | A | From Leg |  | 0.0000 | 130.00 | No Ice | 4.60 | 4.01 | 0.10 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ | 5.05 | 4.45 | 0.16 |
|  |  |  | 0.00 |  |  | Ice | 5.50 | 4.89 | 0.23 |
|  |  |  |  |  |  | 1 1" Ice | 6.44 | 5.82 | 0.42 |
| APXVSPP18-C-A20 wl Mount Pipe |  |  |  |  | 130.00 | 2" Ice |  |  |  |
|  | B | From Leg | 4.00 | 0.0000 |  | No lce | 4.60 | 4.01 | 0.10 |
|  |  |  | 0.00 |  |  | $1 / 2^{\prime \prime}$ | 5.05 | 4.45 | 0.16 |
|  |  |  | 0.00 |  |  | Ice | 5.50 | 4.89 | 0.23 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 6.44 | 5.82 | 0.42 |
| APXVSPP18-C-A20 w/ Mount Pipe |  | From Leg |  |  |  | $2^{\prime \prime}$ Ice |  |  |  |
|  | C |  | 4.00 | 0.0000 | 130.00 | No Ice | 4.60 | 4.01 | 0.10 |
|  |  |  | 0.00 |  |  | 1/2" | 5.05 | 4.45 | 0.16 |
|  |  |  | 0.00 |  |  | ice | 5.50 | 4.89 | 0.23 |
|  |  |  |  |  |  | 1 Ice | 6.44 | 5.82 | 0.42 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| APXVTM14-C-120 w/ Mount Pipe | A | From Leg | 4.00 | 0.0000 | 130.00 | No Ice | 4.09 | 2.86 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 4.48 | 3.23 | 0.13 |
|  |  |  | 0.00 |  |  | Ice | 4.88 | 3.61 | 0.19 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ lce | 5.71 | 4.40 | 0.33 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| APXVTM14-C-120 wl Mount Pipe | B | From Leg | 4.00 | 0.0000 | 130.00 | No Ice | 4.09 | 2.86 | 0.08 |
|  |  |  | $0.00$ |  |  | 1/2" | 4.48 | 3.23 | 0.13 |
|  |  |  | 0.00 |  |  | Ice | 4.88 | 3.61 | 0.19 |
|  |  |  |  |  |  | 1 1' Ice | 5.71 | 4.40 | 0.33 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| APXVTM14-C-120 w/ Mount Pipe | C | From Leg | 4.00 | 0.0000 | 130.00 | No Ice | 4.09 | 2.86 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" | 4.48 | 3.23 | 0.13 |
|  |  |  | 0.00 |  |  | Ice | 4.88 | 3.61 | 0.19 |
|  |  |  |  |  |  | 1" Ice | 5.71 | 4.40 | 0.33 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| TD-RRH8X20-25 | A | From Leg | 4.00 | 0.0000 | 130.00 | No Ice | 4.05 | 1.53 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 4.30 | 1.71 | 0.10 |
|  |  |  | 0.00 |  |  | Ice | 4.56 | 1.90 | 0.13 |
|  |  |  |  |  |  | 1" Ice | 5.10 | 2.30 | 0.20 |
|  |  |  |  |  |  | 2" Ice |  |  |  |

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| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset Type | Offsets: Horz Lateral Vert ft ft ft | Azimuth Adjustmen $t$ | Placement ft |  | $C_{A} A_{A}$ Front $f^{2}$ | $\begin{gathered} \hline C_{A} A_{A} \\ \text { Side } \\ {f t^{2}}^{2} \end{gathered}$ | Weight $K$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| TD-RRH8X20-25 | B | From Leg | 4.00 | 0.0000 | 130.00 | No Ice | 4.05 | 1.53 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 4.30 | 1.71 | 0.10 |
|  |  |  | 0.00 |  |  | Ice | 4.56 | 1.90 | 0.13 |
|  |  |  |  |  |  | $\begin{aligned} & \text { 1" Ice } \\ & 2 " \text { Ice } \end{aligned}$ | 5.10 | 2.30 | 0.20 |
| TD-RRH8X20-25 | C | From Leg | 4.00 | 0.0000 | 130.00 | No lce | 4.05 | 1.53 | 0.07 |
|  |  |  | 0.00 |  |  | 1/2" | 4.30 | 1.71 | 0.10 |
|  |  |  | 0.00 |  |  | Ice | 4.56 | 1.90 | 0.13 |
|  |  |  |  |  |  | $1^{\prime \prime} \text { Ice }$ $2 " \text { Ice }$ | 5.10 | 2.30 | 0.20 |
| 2.375" OD x $6^{\prime}$ Mount Pipe | A | None |  | 0.0000 | 130.00 | No Ice | 1.43 | 1.43 | 0.03 |
|  |  |  |  |  |  | 1/2" | 1.92 | 1.92 | 0.04 |
|  |  |  |  |  |  | Ice | 2.29 | 2.29 | 0.05 |
|  |  |  |  |  |  | 1" Ice | 3.06 | 3.06 | 0.09 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| 2.375" OD x 6 ' Mount Pipe | B | None |  | 0.0000 | 130.00 | Nolce | 1.43 | 1.43 | 0.03 |
|  |  |  |  |  |  | 1/2" | 1.92 | 1.92 | 0.04 |
|  |  |  |  |  |  | Ice | 2.29 | 2.29 | 0.05 |
|  |  |  |  |  |  | $1{ }^{\prime \prime}$ Ice | 3.06 | 3.06 | 0.09 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| 2.375" OD x 6 ' Mount Pipe | C | None |  | 0.0000 | 130.00 | No Ice | 1.43 | 1.43 | 0.03 |
|  |  |  |  |  |  | 1/2" | 1.92 | 1.92 | 0.04 |
|  |  |  |  |  |  | Ice | 2.29 | 2.29 | 0.05 |
|  |  |  |  |  |  | 1" Ice | 3.06 | 3.06 | 0.09 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| T-Arm Mount [TA 602-3] | C | None |  | 0.0000 | 130.00 | No Ice | 11.59 | 11.59 | 0.77 |
|  |  |  |  |  |  | 1/2" | 15.44 | 15.44 | 0.99 |
|  |  |  |  |  |  | Ice | 19.29 | 19.29 | 1.21 |
|  |  |  |  |  |  | 1 " Ice | 26.99 | 26.99 | 1.64 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| ERICSSON AIR 21 B2A | A | From Leg | 4.00 | 0.0000 | 122.00 | No Ice | 6.33 | 5.64 | 0.11 |
| B4P w/ Mount Pipe |  |  | $0.00$ |  |  | 1/2" | 6.78 | 6.43 | 0.17 |
|  |  |  | 1.00 |  |  | Ice | 7.21 | 7.13 | 0.23 |
|  |  |  |  |  |  | $1{ }^{1 \prime}$ Ice | 8.12 | 8.59 | 0.38 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| ERICSSON AIR 21 B2A | B | From Leg | 4.00 | 0.0000 | 122.00 | No Ice | 6.33 | 5.64 | 0.11 |
| B4P w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" | 6.78 | 6.43 | 0.17 |
|  |  |  | 1.00 |  |  | Ice | 7.21 | 7.13 | 0.23 |
|  |  |  |  |  |  |  | 8.12 | 8.59 | 0.38 |
|  |  |  |  |  |  | $2^{\prime \prime} \text { Ice }$ |  |  |  |
| ERICSSON AIR 21 B2A | C | From Leg |  | 0.0000 | 122.00 | No Ice | 6.33 | 5.64 | 0.11 |
| B4P w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" | 6.78 | 6.43 | 0.17 |
|  |  |  | 1.00 |  |  | Ice | 7.21 | 7.13 | 0.23 |
|  |  |  |  |  |  | 1"Ice | 8.12 | 8.59 | 0.38 |
|  |  |  |  |  |  | 2"Ice |  |  |  |
| APXVAARR24_43-U-NA20 | A | From Leg | 4.00 | 0.0000 | 122.00 | No lce | 14.69 | 6.87 | 0.19 |
| w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" | 15.46 | 7.55 | 0.31 |
|  |  |  | 1.00 |  |  | Ice | 16.23 | 8.25 | 0.46 |
|  |  |  |  |  |  | 1" Ice | 17.82 | 9.67 | 0.79 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| APXVAARR24_43-U-NA20 | B | From Leg | 4.00 | 0.0000 | 122.00 | No Ice | 14.69 | 6.87 | 0.19 |
| w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" | 15.46 | 7.55 | 0.31 |
|  |  |  | 1.00 |  |  | Ice | 16.23 | 8.25 | 0.46 |
|  |  |  |  |  |  | 1"Ice | 17.82 | 9.67 | 0.79 |
|  |  |  |  |  |  | 2" Ice |  |  |  |
| APXVAARR24_43-U-NA20 | C | From Leg | 4.00 | 0.0000 | 122.00 | No Ice | 14.69 | 6.87 | 0.19 |
| w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" | 15.46 | 7.55 | 0.31 |
|  |  |  | 1.00 |  |  | Ice | 16.23 | 8.25 | 0.46 |
|  |  |  |  |  |  | 1" Ice | 17.82 | 9.67 | 0.79 |
| (3) RADIO 4449 B12/B71 | A |  |  |  |  | 2" Ice |  |  |  |
|  |  | From Leg | 4.00 | 0.0000 | 122.00 | $\begin{gathered} \text { No Ice } \\ \text { 1/2" } \\ \text { Ice } \\ \text { 1" Ice } \end{gathered}$ | 1.65 | 1.16 | 0.07 |
|  |  |  | 0.00 |  |  |  | 1.81 | 1.30 | 0.09 |
|  |  |  | 1.00 |  |  |  | 1.98 | 1.45 | 0.11 |
|  |  |  |  |  |  |  | 2.34 | 1.76 | 0.16 |

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| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> ft <br> ft <br> ft | Azimuth Adjustmen ! | $\begin{gathered} \text { Placement } \\ f t \end{gathered}$ |  | $C_{A} \mathcal{A}_{A}$ Front $f^{2}$ | $\begin{gathered} C_{A} A_{A} \\ \text { Side } \\ f^{2} \end{gathered}$ | Weight K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| T-Arm Mount [TA 702-3] | C | None |  | 0.0000 | 122.00 | 2" Ice |  |  |  |
|  |  |  |  |  |  | No lce | 5.64 | 5.64 | 0.34 |
|  |  |  |  |  |  | 1/2" | 6.55 | 6.55 | 0.43 |
|  |  |  |  |  |  | lce | 7.46 | 7.46 | 0.52 |
|  |  |  | . |  |  | 1" Ice | 9.28 | 9.28 | 0.70 |
|  |  |  |  |  |  | 2" Ice |  |  |  |

## Tower Pressures - No Ice

$G_{H}=1.100$

| Section Elevation ft | $z$ | $K z$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $A_{G}$ $\boldsymbol{H}^{2}$ | F a $c$ e | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f^{2} \end{aligned}$ | $\overline{A_{i e g}}$ $f^{2}$ | $\begin{gathered} \mathrm{Leg} \\ \% \end{gathered}$ | $\begin{gathered} C_{A} A_{A} \\ \text { In } \\ \text { Face } \\ f^{2} \\ \hline \end{gathered}$ | $C_{A} A_{A}$ Out Face $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 151.00- | 148.48 | 1.106 | 38.88 | 7.757 | A | 0.000 | 7.757 | 7.757 | 100.00 | 0.000 | 0.000 |
| 146.00 |  |  |  |  | B | 0.000 | 7.757 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 7.757 |  | 100.00 | 0.000 | 0.000 |
| L2 146.00- | 143.48 | 1.096 | 38.50 | 8.161 | A | 0.000 | 8.161 | 8.161 | 100.00 | 0.000 | 0.000 |
| 141.00 |  |  |  |  | B | 0.000 | 8.161 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.161 |  | 100.00 | 0.000 | 0.000 |
| L3 141.00- | 138.48 | 1.085 | 38.12 | 8.564 | A | 0.000 | 8.564 | 8.564 | 100.00 | 0.000 | 0.000 |
| $136.00$ |  |  |  |  | B | 0.000 | 8.564 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.564 |  | 100.00 | 0.000 | 0.000 |
| L4 136.00- | 133.48 | 1.073 | 37.72 | 8.968 | A | 0.000 | 8.968 | 8.968 | 100.00 | 0.000 | 0.000 |
| $131.00$ |  |  |  |  | B | 0.000 | 8.968 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.968 |  | 100.00 | 0.000 | 0.000 |
| L5 131.00- | 128.48 | 1.062 | 37.31 | 9.372 | A | 0.000 | 9.372 | 9.372 | 100.00 | 0.000 | 0.000 |
| $126.00$ |  |  |  |  | B | 0.000 | 9.372 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 9.372 |  | 100.00 | 0.000 | 0.000 |
| L6 126.00 | 125.75 | 1.055 | 37.08 | 0.959 | A | 0.000 | 0.959 | 0.959 | 100.00 | 0.000 | 0.000 |
| $125.50$ |  |  |  |  | B | 0.000 | 0.959 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.959 |  | 100.00 | 0.000 | 0.000 |
| L7 125.50- | 125.37 | 1.054 | 37.05 | 0.480 | A | 0.000 | 0.480 | 0.480 | 100.00 | 0.000 | 0.000 |
| 125.25 |  |  |  |  | B | 0.000 | 0.480 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.480 |  | 100.00 | 0.000 | 0.000 |
| L8 125.25- | 122.73 | 1.048 | 36.82 | 9.815 | A | 0.000 | 9.815 | 9.815 | 100.00 | 3.464 | 0.000 |
| $120.25$ |  |  |  |  | B | 0.000 | 9.815 |  | 100.00 | 4.836 | 0.000 |
|  |  |  |  |  | C | 0.000 | 9.815 |  | 100.00 | 3.464 | 0.000 |
| L. 120.25- | 119.37 | 1.04 | 36.53 | 3.531 | A | 0.000 | 3.531 | 3.531 | 100.00 | 2.934 | 0.000 |
| $118.50$ |  |  |  |  | B | 0.000 | 3.531 |  | 100.00 | 4.306 | 0.000 |
|  |  |  |  |  | C | 0.000 | 3.531 |  | 100.00 | 2.934 | 0.000 |
| L10 118.50- | 118.37 | 1.037 | 36.45 | 0.506 | A | 0.000 | 0.506 | 0.506 | 100.00 | 0.419 | 0.000 |
| $118.25$ |  |  |  |  | B | 0.000 | 0.506 |  | 100.00 | 0.615 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.506 |  | 100.00 | 0.419 | 0.000 |
| L11 118.25- | 117.87 | 1.036 | 36.40 | 1.525 | A | 0.000 | 1.525 | 1.525 | 100.00 | 1.258 | 0.000 |
| $117.50$ |  |  |  |  | B | 0.000 | 1.525 |  | 100.00 | 1.846 | 0.000 |
|  |  |  |  |  | C | 0.000 | 1.525 |  | 100.00 | 1.258 | 0.000 |
| L12 117.50- | 117.37 | 1.035 | 36.36 | 0.511 | A | 0.000 | 0.511 | 0.511 | 100.00 | 0.419 | 0.000 |
| $117.25$ |  |  |  |  | B | 0.000 | 0.511 |  | 100.00 | 0.615 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.511 |  | 100.00 | 0.419 | 0.000 |
| L13 117.25- | 114.73 | 1.028 | 36.12 | 10.443 | A | 0.000 | 10.443 | 10.443 | 100.00 | 6.523 | 0.000 |
| $112.25$ |  |  |  |  | B | 0.000 | 10.443 |  | 100.00 | 10.443 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.443 |  | 100.00 | 6.523 | 0.000 |
| L14 112.25- | 109.73 | 1.015 | 35.67 | 10.848 | A | 0.000 | 10.848 | 10.848 | 100.00 | 5.000 | 0.000 |
| 107.25 |  |  |  |  | B | 0.000 | 10.848 |  | 100.00 | 8.920 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.848 |  | 100.00 | 5.000 | 0.000 |
| L15 107.25- | 104.74 | 1.001 | 35.19 | 11.253 | A | 0.000 | 11.253 | 11.253 | 100.00 | 5.000 | 0.000 |
| $102.25$ |  |  |  |  | B | 0.000 | 11.253 |  | 100.00 | 8.920 | 0.000 |
|  |  |  |  |  | C | 0.000 | 11.253 |  | 100.00 | 5.000 | 0.000 |
| L16 102.25- | 99.86 | 0.988 | 34.72 | 11.065 | A | 0.000 | 11.065 | 11.065 | 100.00 | 5.830 | 0.000 |
| 97.50 |  |  |  |  | B | 0.000 | 11.065 |  | 100.00 | 9.554 | 0.000 |
|  |  |  |  |  | C | 0.000 | 11.065 |  | 100.00 | 5.830 | 0.000 |

[^2]| Section Elevation ft | $\begin{aligned} & \mathbf{z} \\ & f t \end{aligned}$ | $K_{z}$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & A_{G} \\ & {f t^{2}}^{2} \end{aligned}$ | $F$ $a$ $c$ $e$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f t^{2} \end{aligned}$ | $A_{\log }$ $f^{2}$ | $\begin{gathered} \mathrm{Leg} \\ \% \end{gathered}$ | $\begin{gathered} C_{A} A_{A} \\ \text { In } \\ \text { Face } \\ {f t^{2}}^{2} \end{gathered}$ | $C_{A} A_{A}$ Out Face ft ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L17 97.50- | 96.71 | 0.979 | 34.40 | 3.707 | A | 0.000 | 3.707 | 3.707 | 100.00 | 3.168 | 0.000 |
| 95.92 |  |  |  |  | B | 0.000 | 3.707 |  | 100.00 | 4.410 | 0.000 |
|  |  |  |  |  | C | 0.000 | 3.707 |  | 100.00 | 3.168 | 0.000 |
| L18 95.92- | 94.20 | 0.972 | 34.14 | 8.131 | A | 0.000 | 8.131 | 8.131 | 100.00 | 6.832 | 0.000 |
| 92.50 |  |  |  |  | B | 0.000 | 8.131 |  | 100.00 | 9.510 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.131 |  | 100.00 | 6.832 | 0.000 |
| L19 92.50- | 92.37 | 0.966 | 33.95 | 0.602 | A | 0.000 | 0.602 | 0.602 | 100.00 | 0.500 | 0.000 |
| 92.25 |  |  |  |  | B | 0.000 | 0.602 |  | 100.00 | 0.696 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.602 |  | 100.00 | 0.500 | 0.000 |
| L20 92.25- | 89.74 | 0.958 | 33.67 | 12.263 | A | 0.000 | 12.263 | 12.263 | 100.00 | 10.271 | 0.000 |
| 87.25 |  |  |  |  | B | 0.000 | 12.263 |  | 100.00 | 14.191 | 0.000 |
|  |  |  |  |  | C | 0.000 | 12.263 |  | 100.00 | 10.271 | 0.000 |
| L21 87.25- | 87.12 | 0.95 | 33.39 | 0.623 | A | 0.000 | 0.623 | 0.623 | 100.00 | 0.521 | 0.000 |
| 87.00 |  |  |  |  | B | 0.000 | 0.623 |  | 100.00 | 0.717 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.623 |  | 100.00 | 0.521 | 0.000 |
| L22 87.00- | 84.49 | 0.942 | 33.10 | 12.676 | A | 0.000 | 12.676 | 12.676 | 100.00 | 9.997 | 0.000 |
| 82.00 |  |  |  |  | B | 0.000 | 12.676 |  | 100.00 | 13.917 | 0.000 |
|  |  |  |  |  | C | 0.000 | 12.676 |  | 100.00 | 9.997 | 0.000 |
| L23 82.00- | 79.49 | 0.925 | 32.53 | 13.082 | A | 0.000 | 13.082 | 13.082 | 100.00 | 5.417 | 0.000 |
| 77.00 |  |  |  |  | B | 0.000 | 13.082 |  | 100.00 | 9.337 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.082 |  | 100.00 | 5.417 | 0.000 |
| L24 77.00- | 74.49 | 0.908 | 31.93 | 13.487 | A | 0.000 | 13.487 | 13.487 | 100.00 | 5.417 | 0.000 |
| $72.00$ |  |  |  |  | B | 0.000 | 13.487 |  | 100.00 | 9.337 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.487 |  | 100.00 | 5.417 | 0.000 |
| L25 72.00- | 69.49 | 0.891 | 31.30 | 13.892 | A | 0.000 | 13.892 | 13.892 | 100.00 | 8.309 | 0.000 |
| 67.00 |  |  |  |  | B | 0.000 | 13.892 |  | 100.00 | 12.229 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.892 |  | 100.00 | 8.309 | 0.000 |
| L26 67.00- | 65.12 | 0.874 | 30.72 | 10.684 | A | 0.000 | 10.684 | 10.684 | 100.00 | 8.125 | 0.000 |
| $63.25$ |  |  |  |  | B | 0.000 | 10.684 |  | 100.00 | 11.065 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.684 |  | 100.00 | 8.125 | 0.000 |
| L27 63.25- | 63.12 | 0.867 | 30.45 | 0.720 | A | 0.000 | 0.720 | 0.720 | 100.00 | 0.542 | 0.000 |
| 63.00 |  |  |  |  | B | 0.000 | 0.720 |  | 100.00 | 0.738 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.720 |  | 100.00 | 0.542 | 0.000 |
| L28 63.00- | 60.49 | 0.856 | 30.08 | 14.621 | A | 0.000 | 14.621 | 14.621 | 100.00 | 11.667 | 0.000 |
| $58.00$ |  |  |  |  | B | 0.000 | 14.621 |  | 100.00 | 15.587 | 0.000 |
|  |  |  |  |  | C | 0.000 | 14.621 |  | 100.00 | 11.667 | 0.000 |
| L29 58.00- | 57.37 | 0.843 | 29.63 | 3.718 | A | 0.000 | 3.718 | 3.718 | 100.00 | 3.125 | 0.000 |
| 56.75 |  |  |  |  | B | 0.000 | 3.718 |  | 100.00 | 4.105 | 0.000 |
|  |  |  |  |  | C | 0.000 | 3.718 |  | 100.00 | 3.125 | 0.000 |
| L30 56.75- | 56.62 | 0.84 | 29.52 | 0.746 | A | 0.000 | 0.746 | 0.746 | 100.00 | 0.625 | 0.000 |
| $56.50$ |  |  |  |  | B | 0.000 | 0.746 |  | 100.00 | 0.821 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.746 |  | 100.00 | 0.625 | 0.000 |
| L31 56.50- | 51.96 | 0.82 | 28.81 | 27.535 | A | 0.000 | 27.535 | 27.535 | 100.00 | 18.352 | 0.000 |
| 47.50 |  |  |  |  | B | 0.000 | 27.535 |  | 100.00 | 25.409 | 0.000 |
|  |  |  |  |  | C | 0.000 | 27.535 |  | 100.00 | 18.352 | 0.000 |
| L32 47.50- | 47.25 | 0.798 | 28.03 | 1.540 | A | 0.000 | 1.540 | 1.540 | 100.00 | 0.708 | 0.000 |
| 47.00 |  |  |  |  | B | 0.000 | 1.540 |  | 100.00 | 1.100 | 0.000 |
|  |  |  |  |  | C | 0.000 | 1.540 |  | 100.00 | 0.708 | 0.000 |
| 133 47.00- | 44.49 | 0.784 | 27.56 | 15.624 | A | 0.000 | 15.624 | 15.624 | 100.00 | 7.083 | 0.000 |
| $42.00$ |  |  |  |  | B | 0.000 | 15.624 |  | 100.00 | 11.003 | 0.000 |
|  |  |  |  |  | C | 0.000 | 15.624 |  | 100.00 | 7.083 | 0.000 |
| L34 42.00- | 39.49 | 0.758 | 26.63 | 16.029 | A | 0.000 | 16.029 | 16.029 | 100.00 | 11.335 | 0.000 |
| $37.00$ |  |  |  |  | B | 0.000 | 16.029 |  | 100.00 | 15.255 | 0.000 |
|  |  |  |  |  | C | 0.000 | 16.029 |  | 100.00 | 11.335 | 0.000 |
| L35 37.00- | 35.62 | 0.736 | 25.86 | 8.985 | A | 0.000 | 8.985 | 8.985 | 100.00 | 7.789 | 0.000 |
| 34.25 |  |  |  |  | B | 0.000 | 8.985 |  | 100.00 | 9.944 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.985 |  | 100.00 | 7.789 | 0.000 |
| L. $3634.25-$ | 34.12 | 0.727 | 25.55 | 0.823 | A | 0.000 | 0.823 | 0.823 | 100.00 | 0.708 | 0.000 |
| 34.00 |  |  |  |  | B | 0.000 | 0.823 |  | 100.00 | 0.904 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.823 |  | 100.00 | 0.708 | 0.000 |
| L37 34.00- | 31.49 | 0.71 | 24.97 | 16.677 | A | 0.000 | 16.677 | 16.677 | 100.00 | 14.167 | 0.000 |
| 29.00 |  |  |  |  | B | 0.000 | 16.677 |  | 100.00 | 18.087 | 0.000 |
|  |  |  |  |  | C | 0.000 | 16.677 |  | 100.00 | 14.167 | 0.000 |
| L38 29.00- | 27.87 | 0.7 | 24.60 | 7.636 | A | 0.000 | 7.636 | 7.636 | 100.00 | 6.375 | 0.000 |
| 26.75 |  |  |  |  | B | 0.000 | 7.636 |  | 100.00 | 8.139 | 0.000 |
|  |  |  |  |  | C | 0.000 | 7.636 |  | 100.00 | 6.375 | 0.000 |
| L39 26.75- | 26.62 | 0.7 | 24.60 | 0.854 | A | 0.000 | 0.854 | 0.854 | 100.00 | 0.708 | 0.000 |
| 26.50 |  |  |  |  | B | 0.000 | 0.854 |  | 100.00 | 0.904 | 0.000 |


| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | $K_{z}$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $A_{G}$ $f^{2}$ | F $a$ $c$ $e$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f^{2} \end{aligned}$ | $A_{\text {leg }}$ $f^{2}$ | $\begin{gathered} \operatorname{Leg} \\ \% \end{gathered}$ | $\begin{aligned} & C_{A} A_{A} \\ & \text { In } \\ & \text { Face } \\ & f^{2} \end{aligned}$ | $C_{A} A_{A}$ <br> Out <br> Face <br> ff ${ }^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \text { L40 } 26.50- \\ 21.50 \end{array}$ | 23.99 | 0.7 | 24.60 | 17.284 | C | 0.000 | 0.854 | 17.284 | 100.00 | 0.708 | 0.000 |
|  |  |  |  |  | A | 0.000 | 17.284 |  | 100.00 | 14.167 | 0.000 |
|  |  |  |  |  | B | 0.000 | 17.284 |  | 100.00 | 18.087 | 0.000 |
|  |  | 0.7 |  |  | C | 0.000 | 17.284 | 16.794 | 100.00 | 14.167 | 0.000 |
| $\begin{array}{r} \text { L41 } 21.50- \\ 16.75 \end{array}$ | 19.12 |  | 24.60 | 16.794 | A | 0.000 | 16.794 |  | 100.00 | 12.750 | 0.000 |
|  |  |  |  |  | B | 0.000 | 16.794 |  | 100.00 | 16.474 | 0.000 |
|  | 16.62 | 0.7 | 24.60 | 0.893 | C | 0.000 | 16.794 | 0.893 | 100.00 | 7.438 | 0.000 |
| $\begin{array}{r} \text { L42 16.75- } \\ 16.50 \end{array}$ |  |  |  |  | A | 0.000 | 0.893 |  | 100.00 | 0.708 | 0.000 |
|  |  |  |  |  | B | 0.000 | 0.893 |  | 100.00 | 0.904 | 0.000 |
|  | 15.37 | 0.7 | 24.60 | 8.084 | C | 0.000 | 0.893 | 8.084 | 100.00 | 0.354 | 0.000 |
| $\begin{array}{r} \text { L. } 4316.50- \\ 14.25 \end{array}$ |  |  |  |  | A | 0.000 | 8.084 |  | 100.00 | 6.375 | 0.000 |
|  |  |  |  |  | B | 0.000 | 8.084 |  | 100.00 | 8.139 | 0.000 |
|  | 14.12 | 0.7 | 24.60 | 0.903 | C | 0.000 | 8.084 | 0.903 | 100.00 | 3.188 | 0.000 |
| $\begin{array}{r} \text { L44 14.25- } \\ 14.00 \end{array}$ |  |  |  |  | A | 0.000 | 0.903 |  | 100.00 | 0.708 | 0.000 |
|  |  |  |  |  | B | 0.000 | 0.903 |  | 100.00 | 0.904 | 0.000 |
|  | 11.49 | 0.7 | 24.60 | 18.284 | C | 0.000 | 0.903 | 18.284 | 100.00 | 0.354 | 0.000 |
| L45 14.00- |  |  |  |  | A | 0.000 | 18.284 |  | 100.00 | 12.042 | 0.000 |
| 9.00 |  |  |  |  | B | 0.000 | 18.284 |  | 100.00 | 18.087 | 0.000 |
|  | 6.62 | 0.7 | 24.60 | 17.743 | C | 0.000 | 18.284 | 17.743 | 100.00 | 7.083 | 0.000 |
| L46 9.00-4.25 |  |  |  |  | A | 0.000 | 17.743 |  | 100.00 | 6.729 | 0.000 |
|  |  |  |  |  | B | 0.000 | 17.743 |  | 100.00 | 17.182 | 0.000 |
|  |  | 0.7 | 24.60 | 0.945 | C | 0.000 | 17.743 | 0.945 | 100.00 | 6.729 | 0.000 |
| L47 4.25-4.00 | 4.12 |  |  |  | A | 0.000 | 0.945 |  | 100.00 | 0.354 | 0.000 |
|  |  |  |  |  | B | 0.000 | 0.945 |  | 100.00 | 0.904 | 0.000 |
|  |  | 0.7 | 24.60 | 15.254 | C | 0.000 | 0.945 | 15.254 | 100.00 | 0.354 | 0.000 |
| L48 4.00-0.00 | 1.99 |  |  |  | A | 0.000 | 15.254 |  | 100.00 | 4.958 | 0.000 |
|  |  |  |  |  | B | 0.000 | 15.254 |  | 100.00 | 13.053 | 0.000 |
|  |  |  |  |  | C | 0.000 | 15.254 |  | 100.00 | 4.958 | 0.000 |

Tower Pressure - With Ice
$G_{H}=1.100$

| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | $K z$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & \overline{t z} \\ & i n \end{aligned}$ | $\begin{aligned} & A_{G} \\ & f^{2} \end{aligned}$ | $F$ $a$ $c$ $e$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f^{2} \end{aligned}$ | $A_{\text {leg }}$ $f^{2}$ | $\begin{gathered} \operatorname{Leg} \\ \% \end{gathered}$ | $C_{A} A_{A}$ <br> in <br> Face <br> $f^{2}$ | $C_{A} A_{A}$ Out Face $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \hline \text { L1 } 151.00- \\ 146.00 \end{array}$ | 148.48 | 1.106 | 6.22 | 1.4819 | 8.992 | A | 0.000 | 8.992 | 8.992 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 8.992 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 8.992 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L2 } 146.00- \\ 141.00 \end{array}$ | 143.48 | 1.096 | 6.16 | 1.4769 | 9.392 | A | 0.000 | 9.392 | 9.392 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 9.392 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 9.392 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L3 } 141.00- \\ 136.00 \end{array}$ | 138.48 | 1.085 | 6.10 | 1.4716 | 9.791 | A | 0.000 | 9.791 | 9.791 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 9.791 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 9.791 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L4 } 136.00- \\ 131.00 \end{array}$ | 133.48 | 1.073 | 6.03 | 1.4662 | 10.190 | A | 0.000 | 10.190 | 10.190 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 10.190 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 10.190 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L5 } 131.00- \\ 126.00 \end{array}$ | 128.48 | 1.062 | 5.97 | 1.4606 | 10.589 | A | 0.000 | 10.589 | 10.589 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 10.589 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 10.589 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L6 } 126.00- \\ 125.50 \end{array}$ | 125.75 | 1.055 | 5.93 | 1.4575 | 1.081 | A | 0.000 | 1.081 | 1.081 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 1.081 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 1.081 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} L 7125.50- \\ 125.25 \end{array}$ | 125.37 | 1.054 | 5.93 | 1.4571 | 0.541 | A | 0.000 | 0.541 | 0.541 | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 0.541 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.541 |  | 100.00 | 0.000 | 0.000 |
| $\begin{array}{r} \text { L8 } 125.25- \\ 120.25 \end{array}$ | 122.73 | 1.048 | 5.89 | 1.4540 | 11.027 | A | 0.000 | 11.027 | 11.027 | 100.00 | 4.411 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 11.027 |  | 100.00 | 6.762 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 11.027 |  | 100.00 | 4.411 | 0.000 |
| $\begin{array}{r} \text { L9 120.25- } \\ 118.50 \end{array}$ | 119.37 | 1.04 | 5.85 | 1.4499 | 3.954 | A | 0.000 | 3.954 | 3.954 | 100.00 | 3.763 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 3.954 |  | 100.00 | 6.112 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 3.954 |  | 100.00 | 3.763 | 0.000 |
| $\begin{array}{r} \text { L10 } 118.50- \\ 118.25 \end{array}$ | 118.37 | 1.037 | 5.83 | 1.4487 | 0.567 | A | 0.000 | 0.567 | 0.567 | 100.00 | 0.537 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 0.567 |  | 100.00 | 0.873 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.567 |  | 100.00 | 0.537 | 0.000 |


| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | $K_{z}$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & \mathrm{tz} \\ & \mathrm{in} \end{aligned}$ | $\begin{aligned} & A_{G} \\ & f^{2} \end{aligned}$ | $F$ $a$ $c$ $e$ | $\begin{aligned} & A_{F} \\ & {f t^{2}}^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f^{2} \end{aligned}$ | $\overline{A_{i e g}}$ $\pi t^{2}$ | $\begin{gathered} \operatorname{Leg} \\ \% \end{gathered}$ | $C_{A} A_{A}$ <br> In <br> Face <br> $f t^{2}$ | $C_{A} A_{A}$ Out Face $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L11 118.25- | 117.87 | 1.036 | 5.82 | 1.4481 | 1.706 | A | 0.000 | 1.706 | 1.706 | 100.00 | 1.612 | 0.000 |
| 117.50 |  |  |  |  |  | B | 0.000 | 1.706 |  | 100.00 | 2.619 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 1.706 |  | 100.00 | 1.612 | 0.000 |
| L12 117.50- | 117.37 | 1.035 | 5.82 | 1.4475 | 0.572 | A | 0.000 | 0.572 | 0.572 | 100.00 | 0.537 | 0.000 |
| 117.25 |  |  |  |  |  | B | 0.000 | 0.572 |  | 100.00 | 0.873 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.572 |  | 100.00 | 0.537 | 0.000 |
| L13 117.25- | 114.73 | 1.028 | 5.78 | 1.4442 | 11.646 | A | 0.000 | 11.646 | 11.646 | 100.00 | 8.378 | 0.000 |
| 112.25 |  |  |  |  |  | B | 0.000 | 11.646 |  | 100.00 | 15.084 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 11.646 |  | 100.00 | 8.378 | 0.000 |
| L14 112.25- | 109.73 | 1.015 | 5.71 | 1.4378 | 12.046 | A | 0.000 | 12.046 | 12.046 | 100.00 | 6.438 | 0.000 |
| 107.25 |  |  |  |  |  | B | 0.000 | 12.046 |  | 100.00 | 13.135 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 12.046 |  | 100.00 | 6.438 | 0.000 |
| L15 107.25- | 104.74 | 1.001 | 5.63 | 1.4311 | 12.446 | A | 0.000 | 12.446 | 12.446 | 100.00 | 6.431 | 0.000 |
| 102.25 |  |  |  |  |  | B | 0.000 | 12.446 |  | 100.00 | 13.120 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 12.446 |  | 100.00 | 6.431 | 0.000 |
| L16 102.25- | 99.86 | 0.988 | 5.55 | 1.4243 | 12.192 | A | 0.000 | 12.192 | 12.192 | 100.00 | 7.465 | 0.000 |
| 97.50 |  |  |  |  |  | B | 0.000 | 12.192 |  | 100.00 | 13.812 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 12.192 |  | 100.00 | 7.465 | 0.000 |
| L17 97.50- | 96.71 | 0.979 | 5.50 | 1.4197 | 4.083 | A | 0.000 | 4.083 | 4.083 | 100.00 | 4.034 | 0.000 |
| $95.92$ |  |  |  |  |  | B | 0.000 | 4.083 |  | 100.00 | 6.150 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 4.083 |  | 100.00 | 4.034 | 0.000 |
| L18 95.92- | 94.20 | 0.972 | 5.46 | 1.4160 | 8.937 | A | 0.000 | 8.937 | 8.937 | 100.00 | 8.690 | 0.000 |
| $92.50$ |  |  |  |  |  | B | 0.000 | 8.937 |  | 100.00 | 13.247 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 8.937 |  | 100.00 | 8.690 | 0.000 |
| L19 92.50- | 92.37 | 0.966 | 5.43 | 1.4132 | 0.661 | A | 0.000 | 0.661 | 0.661 | 100.00 | 0.636 | 0.000 |
| 92.25 |  |  |  |  |  | B | 0.000 | 0.661 |  | 100.00 | 0.969 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.661 |  | 100.00 | 0.636 | 0.000 |
| L20 92.25- | 89.74 | 0.958 | 5.39 | 1.4091 | 13.438 | A | 0.000 | 13.438 | 13.438 | 100.00 | 12.980 | 0.000 |
| 87.25 |  |  |  |  |  | B | 0.000 | 13.438 |  | 100.00 | 19.641 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 13.438 |  | 100.00 | 12.980 | 0.000 |
| L21 87.25- | 87.12 | 0.95 | 5.34 | 1.4050 | 0.682 | A | 0.000 | 0.682 | 0.682 | 100.00 | 0.656 | 0.000 |
| 87.00 |  |  |  |  |  | B | 0.000 | 0.682 |  | 100.00 | 0.989 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.682 |  | 100.00 | 0.656 | 0.000 |
| L22 87.00- | 84.49 | 0.942 | 5.30 | 1.4007 | 13.843 | A | 0.000 | 13.843 | 13.843 | 100.00 | 12.584 | 0.000 |
| 82.00 |  |  |  |  |  | B | 0.000 | 13.843 |  | 100.00 | 19.235 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 13.843 |  | 100.00 | 12.584 | 0.000 |
| L23 82.00- | 79.49 | 0.925 | 5.20 | 1.3922 | 14.242 | A | 0.000 | 14.242 | 14.242 | 100.00 | 6.809 | 0.000 |
| 77.00 |  |  |  |  |  | B | 0.000 | 14.242 |  | 100.00 | 13.449 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 14.242 |  | 100.00 | 6.809 | 0.000 |
| L24 77.00- | 74.49 | 0.908 | 5.11 | 1.3831 | 14.640 | A | 0.000 | 14.640 | 14.640 | 100.00 | 6.800 | 0.000 |
| 72.00 |  |  |  |  |  | B | 0.000 | 14.640 |  | 100.00 | 13.429 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 14.640 |  | 100.00 | 6.800 | 0.000 |
| L25 72.00- | 69.49 | 0.891 | 5.01 | 1.3736 | 15.037 | A | 0.000 | 15.037 | 15.037 | 100.00 | 10.400 | 0.000 |
| 67.00 |  |  |  |  |  | B | 0.000 | 15.037 |  | 100.00 | 17.017 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 15.037 |  | 100.00 | 10.400 | 0.000 |
| L26 67.00- | 65.12 | 0.874 | 4.92 | 1.3647 | 11.537 | A | 0.000 | 11.537 | 11.537 | 100.00 | 10.150 | 0.000 |
| 63.25 |  |  |  |  |  | B | 0.000 | 11.537 |  | 100.00 | 15.104 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 11.537 |  | 100.00 | 10.150 | 0.000 |
| L27 63.25- | 63.12 | 0.867 | 4.87 | 1.3604 | 0.777 | A | 0.000 | 0.777 | 0.777 | 100.00 | 0.676 | 0.000 |
| 63.00 |  |  |  |  |  | B | 0.000 | 0.777 |  | 100.00 | 1.006 | 0.000 |
| - |  |  |  |  |  | C | 0.000 | 0.777 |  | 100.00 | 0.676 | 0.000 |
| L28 63.00- | 60.49 | 0.856 | 4.81 | 1.3546 | 15.749 | A | 0.000 | 15.749 | 15.749 | 100.00 | 14.348 | 0.000 |
| 58.00 |  |  |  |  |  | B | 0.000 | 15.749 |  | 100.00 | 20.941 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 15.749 |  | 100.00 | 14.348 | 0.000 |
| L29 58.00- | 57.37 | 0.843 | 4.74 | 1.3475 | 3.999 | A | 0.000 | 3.999 | 3.999 | 100.00 | 3.792 | 0.000 |
| 56.75 |  |  |  |  |  | B | 0.000 | 3.999 |  | 100.00 | 5.438 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 3.999 |  | 100.00 | 3.792 | 0.000 |
| L30 56.75- | 56.62 | 0.84 | 4.72 | 1.3457 | 0.802 | A | 0.000 | 0.802 | 0.802 | 100.00 | 0.758 | 0.000 |
| 56.50 |  |  |  |  |  | B | 0.000 | 0.802 |  | 100.00 | 1.087 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.802 |  | 100.00 | 0.758 | 0.000 |
| L31 56.50- | 51.96 | 0.82 | 4.61 | 1.3342 | 29.537 | A | 0.000 | 29.537 | 29.537 | 100.00 | 22.108 | 0.000 |
| 47.50 |  |  |  |  |  | B | 0.000 | 29.537 |  | 100.00 | 33.931 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 29.537 |  | 100.00 | 22.108 | 0.000 |
| L32 47.50- | 47.25 | 0.798 | 4.49 | 1.3216 | 1.651 | A | 0.000 | 1.651 | 1.651 | 100.00 | 0.842 | 0.000 |
| 47.00 |  |  |  |  |  | B | 0.000 | 1.651 |  | 100.00 | 1.499 | 0.000 |
| - |  |  |  |  |  | C | 0.000 | 1.651 |  | 100.00 | 0.842 | 0.000 |
| L33 47.00- | 44.49 | 0.784 | 4.41 | 1.3137 | 16.719 | A | 0.000 | 16.719 | 16.719 | 100.00 | 8.397 | 0.000 |
| 42.00 |  |  |  |  |  | B | 0.000 | 16.719 |  | 100.00 | 14.939 | 0.000 |


| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | Kz | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & t_{z} \\ & i n \end{aligned}$ | $A_{G}$ $t^{2}$ | $F$ $a$ $c$ $e$ | $\begin{aligned} & A_{F} \\ & f^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f t^{2} \end{aligned}$ | $\begin{gathered} A_{l e g} \\ f^{2} \end{gathered}$ | $\begin{gathered} \mathrm{Leg} \\ \% \end{gathered}$ | $\begin{aligned} & \mathrm{C}_{A} A_{A} \\ & \text { In } \\ & \text { Face } \\ & {f t^{2}}^{2} \end{aligned}$ | $C_{A} A_{A}$ Out Face $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  |  |  | C | 0.000 | 16.719 |  | 100.00 | 8.397 | 0.000 |
| L34 42.00- | 39.49 | 0.758 | 4.26 | 1.2981 | 17.111 | A | 0.000 | 17.111 | 17.111 | 100.00 | 13.154 | 0.000 |
| 37.00 |  |  |  |  |  | B | 0.000 | 17.111 |  | 100.00 | 19.677 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 17.111 |  | 100.00 | 13.154 | 0.000 |
| L35 37.00- | 35.62 | 0.736 | 4.14 | 1.2848 | 9.574 | A | 0.000 | 9.574 | 9.574 | 100.00 | 8.969 | 0.000 |
| 34.25 |  |  |  |  |  | B | 0.000 | 9.574 |  | 100.00 | 12.546 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 9.574 |  | 100.00 | 8.969 | 0.000 |
| L36 34.25- | 34.12 | 0.727 | 4.09 | 1.2793 | 0.876 | A | 0.000 | 0.876 | 0.876 | 100.00 | 0.815 | 0.000 |
| 34.00 |  |  |  |  |  | B | 0.000 | 0.876 |  | 100.00 | 1.140 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.876 |  | 100.00 | 0.815 | 0.000 |
| L37 34.00- | 31.49 | 0.71 | 3.99 | 1.2690 | 17.734 | A | 0.000 | 17.734 | 17.734 | 100.00 | 16.214 | 0.000 |
| 29.00 |  |  |  |  |  | B | 0.000 | 17.734 |  | 100.00 | 22.776 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 17.734 |  | 100.00 | 16.290 | 0.000 |
| $L 3829.00-$ | 27.87 | 0.7 | 3.94 | 1.2537 | 8.106 | A | 0.000 | 8.106 | 8.106 | 100.00 | 7.210 | 0.000 |
| 26.75 |  |  |  |  |  | B | 0.000 | 8.106 |  | 100.00 | 10.230 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 8.106 |  | 100.00 | 7.320 | 0.000 |
| L.39 26.75- | 26.62 | 0.7 | 3.94 | 1.2479 | 0.906 | A | 0.000 | 0.906 | 0.906 | 100.00 | 0.801 | 0.000 |
| 26.50 |  |  |  |  |  | B | 0.000 | 0.906 |  | 100.00 | 1.136 | 0.000 |
| . |  |  |  |  |  | C | 0.000 | 0.906 |  | 100.00 | 0.813 | 0.000 |
| L40 $26.50-$ | 23.99 | 0.7 | 3.94 | 1.2350 | 18.313 | A | 0.000 | 18.313 | 18.313 | 100.00 | 16.003 | 0.000 |
| 21.50 |  |  |  |  |  | B | 0.000 | 18.313 |  | 100.00 | 22.682 | 0.000 |
| - 21.50 |  |  |  |  |  | C | 0.000 | 18.313 |  | 100.00 | 16.238 | 0.000 |
| L41 21.50- | 19.12 | 0.7 | 3.94 | 1.2073 | 17.749 | A | 0.000 | 17.749 | 17.749 | 100.00 | 14.508 | 0.000 |
| 16.75 |  |  |  |  |  | B | 0.000 | 17.749 |  | 100.00 | 20.807 | 0.000 |
| - 10.75 |  |  |  |  |  | C | 0.000 | 17.749 |  | 100.00 | 8.667 | 0.000 |
| L42 16.75-\| | 16.62 | 0.7 | 3.94 | 1.1905 | 0.943 | A | 0.000 | 0.943 | 0.943 | 100.00 | 0.806 | 0.000 |
| $16.50$ |  |  |  |  |  | B | 0.000 | 0.943 |  | 100.00 | 1.136 | 0.000 |
| . 10.50 |  |  |  |  |  | C | 0.000 | 0.943 |  | 100.00 | 0.414 | 0.000 |
| L43 16.50- | 15.37 | 0.7 | 3.94 | 1.1812 | 8.527 | A | 0.000 | 8.527 | 8.527 | 100.00 | 7.250 | 0.000 |
| $14.25$ |  |  |  |  |  | B | 0.000 | 8.527 |  | 100.00 | 10.213 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 8.527 |  | 100.00 | 3.719 | 0.000 |
| L44 14.25- | 14.12 | 0.7 | 3.94 | 1.1713 | 0.952 | A | 0.000 | 0.952 | 0.952 | 100.00 | 0.805 | 0.000 |
| $14.00$ |  |  |  |  |  | B | 0.000 | 0.952 |  | 100.00 | 1.133 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.952 |  | 100.00 | 0.413 | 0.000 |
| L45 14.00-9.00 | 11.49 | 0.7 | 3.94 | 1.1473 | 19.240 | A | 0.000 | 19.240 | 19.240 | 100.00 | 13.665 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 19.240 |  | 100.00 | 22.603 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 19.240 |  | 100.00 | 8.231 | 0.000 |
| L46 9.00-4.25 | 6.62 | 0.7 | 3.94 | 1.0857 | 18.603 | A | 0.000 | 18.603 | 18.603 | 100.00 | 7.606 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 18.603 |  | 100.00 | 21.311 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 18.603 |  | 100.00 | 7.761 | 0.000 |
| L47 4.25-4.00 | 4.12 | 0.7 | 3.94 | 1.0356 | 0.988 | A | 0.000 | 0.988 | 0.988 | 100.00 | 0.399 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 0.988 |  | 100.00 | 1.115 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 0.988 |  | 100.00 | 0.406 | 0.000 |
| L48 4.00-0.00 | 1.99 | 0.7 | 3.94 | 0.9630 | 15.896 | A | 0.000 | 15.896 | 15.896 | 100.00 | 5.561 | 0.000 |
|  |  |  |  |  |  | B | 0.000 | 15.896 |  | 100.00 | 16.076 | 0.000 |
|  |  |  |  |  |  | C | 0.000 | 15.896 |  | 100.00 | 5.632 | 0.000 |

## Tower Pressure - Service

| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | $K z$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & A_{G} \\ & f^{2} \end{aligned}$ | F $a$ $c$ e | $\begin{aligned} & A_{F} \\ & {f t^{2}}^{2} \end{aligned}$ | $\begin{aligned} & A_{R} \\ & f^{2} \end{aligned}$ | $\begin{gathered} A_{\text {ieg }} \\ f^{2} \end{gathered}$ | $\begin{gathered} \text { Leg } \\ \% \end{gathered}$ | $\begin{aligned} & C_{A} A_{A} \\ & \text { In } \\ & \text { Face } \\ & f^{2} \\ & \hline \end{aligned}$ | $C_{A} A_{A}$ <br> Out <br> Face <br> $f t^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 151.00- | 148.48 | 1.106 | 8.44 | 7.757 | A | 0.000 | 7.757 | 7.757 | 100.00 | 0.000 | 0.000 |
| 146.00 |  |  |  |  | B | 0.000 | 7.757 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 7.757 |  | 100.00 | 0.000 | 0.000 |
| L2 146.00- | 143.48 | 1.096 | 8.36 | 8.161 | A | 0.000 | 8.161 | 8.161 | 100.00 | 0.000 | 0.000 |
| 141.00 |  |  |  |  | B | 0.000 | 8.161 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.161 |  | 100.00 | 0.000 | 0.000 |
| L3 141.00- | 138.48 | 1.085 | 8.27 | 8.564 | A | 0.000 | 8.564 | 8.564 | 100.00 | 0.000 | 0.000 |
| 136.00 |  |  |  |  | B | 0.000 | 8.564 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.564 |  | 100.00 | 0.000 | 0.000 |
| $L 4$ 136.00- | 133.48 | 1.073 | 8.18 | 8.968 | A | 0.000 | 8.968 | 8.968 | 100.00 | 0.000 | 0.000 |
| 131.00 |  |  |  |  | B | 0.000 | 8.968 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.968 |  | 100.00 | 0.000 | 0.000 |


| Section Elevation ft | $\begin{aligned} & z \\ & f t \end{aligned}$ | $K z$ | $\begin{gathered} q_{z} \\ p s f \end{gathered}$ | $\begin{aligned} & \hline A_{G} \\ & f^{2} \end{aligned}$ | F a c e | $\begin{aligned} & A_{F} \\ & f t^{2} \end{aligned}$ | $\begin{aligned} & \hline A_{R} \\ & {f t^{2}}^{2} \end{aligned}$ | $\overline{A_{i e g}}$ $\mathrm{ft}^{2}$ | $\begin{gathered} \operatorname{Leg} \\ \% \end{gathered}$ | $C_{A} A_{A}$ <br> In <br> Face <br> ft | $C_{A} A_{A}$ <br> Out <br> Face <br> $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L5 131.00- | 128.48 | 1.062 | 8.10 | 9.372 | A | 0.000 | 9.372 | 9.372 | 100.00 | 0.000 | 0.000 |
| 126.00 |  |  |  |  | B | 0.000 | 9.372 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 9.372 |  | 100.00 | 0.000 | 0.000 |
| L6 126.00- | 125.75 | 1.055 | 8.05 | 0.959 | A | 0.000 | 0.959 | 0.959 | 100.00 | 0.000 | 0.000 |
| 125.50 |  |  |  |  | B | 0.000 | 0.959 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.959 |  | 100.00 | 0.000 | 0.000 |
| L7 125.50- | 125.37 | 1.054 | 8.04 | 0.480 | A | 0.000 | 0.480 | 0.480 | 100.00 | 0.000 | 0.000 |
| 125.25 |  |  |  |  | B | 0.000 | 0.480 |  | 100.00 | 0.000 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.480 |  | 100.00 | 0.000 | 0.000 |
| L8 125.25- | 122.73 | 1.048 | 7.99 | 9.815 | A | 0.000 | 9.815 | 9.815 | 100.00 | 3.464 | 0.000 |
| 120.25 |  |  |  |  | B | 0.000 | 9.815 |  | 100.00 | 4.836 | 0.000 |
|  |  |  |  |  | C | 0.000 | 9.815 |  | 100.00 | 3.464 | 0.000 |
| L9 120.25- | 119.37 | 1.04 | 7.93 | 3.531 | A | 0.000 | 3.531 | 3.531 | 100.00 | 2.934 | 0.000 |
| 118.50 |  |  |  |  | B | 0.000 | 3.531 |  | 100.00 | 4.306 | 0.000 |
|  |  |  |  |  | C | 0.000 | 3.531 |  | 100.00 | 2.934 | 0.000 |
| L10 118.50- | 118.37 | 1.037 | 7.91 | 0.506 | A | 0.000 | 0.506 | 0.506 | 100.00 | 0.419 | 0.000 |
| 118.25 |  |  |  |  | B | 0.000 | 0.506 |  | 100.00 | 0.615 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.506 |  | 100.00 | 0.419 | 0.000 |
| L11 118.25- | 117.87 | 1.036 | 7.90 | 1.525 | A | 0.000 | 1.525 | 1.525 | 100.00 | 1.258 | 0.000 |
| 117.50 |  |  |  |  | B | 0.000 | 1.525 |  | 100.00 | 1.846 | 0.000 |
|  |  |  |  |  | C | 0.000 | 1.525 |  | 100.00 | 1.258 | 0.000 |
| L12 117.50- | 117.37 | 1.035 | 7.89 | 0.511 | A | 0.000 | 0.511 | 0.511 | 100.00 | 0.419 | 0.000 |
| 117.25 |  |  |  |  | B | 0.000 | 0.511 |  | 100.00 | 0.615 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.511 |  | 100.00 | 0.419 | 0.000 |
| L13 117.25- | 114.73 | 1.028 | 7.84 | 10.443 | A | 0.000 | 10.443 | 10.443 | 100.00 | 6.523 | 0.000 |
| 112.25 |  |  |  |  | B | 0.000 | 10.443 |  | 100.00 | 10.443 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.443 |  | 100.00 | 6.523 | 0.000 |
| L14 112.25- | 109.73 | 1.015 | 7.74 | 10.848 | A | 0.000 | 10.848 | 10.848 | 100.00 | 5.000 | 0.000 |
| 107.25 |  |  |  |  | B | 0.000 | 10.848 |  | 100.00 | 8.920 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.848 |  | 100.00 | 5.000 | 0.000 |
| L15 107.25- | 104.74 | 1.001 | 7.64 | 11.253 | A | 0.000 | 11.253 | 11.253 | 100.00 | 5.000 | 0.000 |
| 102.25 |  |  |  |  | B | 0.000 | 11.253 |  | 100.00 | 8.920 | 0.000 |
|  |  |  |  |  | C | 0.000 | 11.253 |  | 100.00 | 5.000 | 0.000 |
| L16 102.25- | 99.86 | 0.988 | 7.53 | 11.065 | A | 0.000 | 11.065 | 11.065 | 100.00 | 5.830 | 0.000 |
| 97.50 |  |  |  |  | B | 0.000 | 11.065 |  | 100.00 | 9.554 | 0.000 |
|  |  |  |  |  | C | 0.000 | 11.065 |  | 100.00 | 5.830 | 0.000 |
| L17 97.50- | 96.71 | 0.979 | 7.46 | 3.707 | A | 0.000 | 3.707 | 3.707 | 100.00 | 3.168 | 0.000 |
| 95.92 |  |  |  |  | B | 0.000 | 3.707 |  | 100.00 | 4.410 | 0.000 |
|  |  |  |  |  | C | 0.000 | 3.707 |  | 100.00 | 3.168 | 0.000 |
| L18 95.92- | 94.20 | 0.972 | 7.41 | 8.131 | A | 0.000 | 8.131 | 8.131 | 100.00 | 6.832 | 0.000 |
| 92.50 |  |  |  |  | B | 0.000 | 8.131 |  | 100.00 | 9.510 | 0.000 |
|  |  |  |  |  | C | 0.000 | 8.131 |  | 100.00 | 6.832 | 0.000 |
| L19 92.50- | 92.37 | 0.966 | 7.37 | 0.602 | A | 0.000 | 0.602 | 0.602 | 100.00 | 0.500 | 0.000 |
| 92.25 |  |  |  |  | B | 0.000 | 0.602 |  | 100.00 | 0.696 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.602 |  | 100.00 | 0.500 | 0.000 |
| L20 92.25- | 89.74 | 0.958 | 7.31 | 12.263 | A | 0.000 | 12.263 | 12.263 | 100.00 | 10.271 | 0.000 |
| 87.25 |  |  |  |  | B | 0.000 | 12.263 |  | 100.00 | 14.191 | 0.000 |
|  |  |  |  |  | C | 0.000 | 12.263 |  | 100.00 | 10.271 | 0.000 |
| L21 87.25- | 87.12 | 0.95 | 7.25 | 0.623 | A | 0.000 | 0.623 | 0.623 | 100.00 | 0.521 | 0.000 |
| 87.00 |  |  |  |  | B | 0.000 | 0.623 |  | 100.00 | 0.717 | 0.000 |
|  |  |  |  |  | C | 0.000 | 0.623 |  | 100.00 | 0.521 | 0.000 |
| L22 87.00- | 84.49 | 0.942 | 7.18 | 12.676 | A | 0.000 | 12.676 | 12.676 | 100.00 | 9.997 | 0.000 |
| 82.00 |  |  |  |  | B | 0.000 | 12.676 |  | 100.00 | 13.917 | 0.000 |
|  |  |  |  |  | C | 0.000 | 12.676 |  | 100.00 | 9.997 | 0.000 |
| L23 82.00- | 79.49 | 0.925 | 7.06 | 13.082 | A | 0.000 | 13.082 | 13.082 | 100.00 | 5.417 | 0.000 |
| 77.00 |  |  |  |  | B | 0.000 | 13.082 |  | 100.00 | 9.337 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.082 |  | 100.00 | 5.417 | 0.000 |
| L24 77.00- | 74.49 | 0.908 | 6.93 | 13.487 | A | 0.000 | 13.487 | 13.487 | 100.00 | 5.417 | 0.000 |
| 72.00 |  |  |  |  | B | 0.000 | 13.487 |  | 100.00 | 9.337 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.487 |  | 100.00 | 5.417 | 0.000 |
| L25 72.00- | 69.49 | 0.891 | 6.79 | 13.892 | A | 0.000 | 13.892 | 13.892 | 100.00 | 8.309 | 0.000 |
| 67.00 |  |  |  |  | B | 0.000 | 13.892 |  | 100.00 | 12.229 | 0.000 |
|  |  |  |  |  | C | 0.000 | 13.892 |  | 100.00 | 8.309 | 0.000 |
| L26 67.00- | 65.12 | 0.874 | 6.67 | 10.684 | A | 0.000 | 10.684 | 10.684 | 100.00 | 8.125 | 0.000 |
| 63.25 |  |  |  |  | B | 0.000 | 10.684 |  | 100.00 | 11.065 | 0.000 |
|  |  |  |  |  | C | 0.000 | 10.684 |  | 100.00 | 8.125 | 0.000 |
| L27 63.25- | 63.12 | 0.867 | 6.61 | 0.720 | A | 0.000 | 0.720 | 0.720 | 100.00 | 0.542 | 0.000 |
| 63.00 |  |  |  |  | B | 0.000 | 0.720 |  | 100.00 | 0.738 | 0.000 |


| Section Elevation ft | $\begin{aligned} & z \\ & f \end{aligned}$ | $K z$ | $\begin{gathered} q_{2} \\ p s f \end{gathered}$ | $\begin{aligned} & A_{G} \\ & f^{2} \end{aligned}$ | $F$ $a$ $c$ $e$ | $A_{F}$ $f t^{2}$ | $A_{R}$ $f^{2}$ | $\begin{aligned} & A_{\text {leg }} \\ & f^{2} \end{aligned}$ | $\begin{gathered} \mathrm{Leg} \\ \% \end{gathered}$ | $\begin{gathered} \mathrm{C}_{A} A_{A} \\ \text { in } \\ \text { Face } \\ {f t^{2}}^{2} \end{gathered}$ | $C_{A} A_{A}$ <br> Out <br> Face <br> $f^{2}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\begin{array}{r} \mathrm{L} 28 \text { 63.00- } \\ 58.00 \end{array}$ | 60.49 | 0.856 | 6.53 | 14.621 | C | 0.000 | 0.720 | 14.621 | 100.00 | 0.542 | 0.000 |
|  |  |  |  |  | A | 0.000 | 14.621 |  | 100.00 | 11.667 | 0.000 |
|  |  |  |  |  | B | 0.000 | 14.621 |  | 100.00 | 15.587 | 0.000 |
|  | 57.37 |  |  |  | C | 0.000 | 14.621 | 3.718 | 100.00 | 11.667 | 0.000 |
| L29 58.00- |  | 0.843 | 6.43 | 3.718 | A | 0.000 | 3.718 |  | 100.00 | 3.125 | 0.000 |
| 56.75 |  |  |  |  | B | 0.000 | 3.718 |  | 100.00 | 4.105 | 0.000 |
|  | 56.62 | 0.84 | 6.41 | 0.746 | C | 0.000 | 3.718 | 0.746 | 100.00 | 3.125 | 0.000 |
| L30 56.75- |  |  |  |  | A | 0.000 | 0.746 |  | 100.00 | 0.625 | 0.000 |
| 56.50 |  |  |  |  | B | 0.000 | 0.746 |  | 100.00 | 0.821 | 0.000 |
|  | 51.96 | 0.82 | 6.25 | 27.535 | C | 0.000 | 0.746 | 27.535 | 100.00 | 0.625 | 0.000 |
| L31 56.50- |  |  |  |  | A | 0.000 | 27.535 |  | 100.00 | 18.352 | 0.000 |
| 47.50 |  |  |  |  | B | 0.000 | 27.535 |  | 100.00 | 25.409 | 0.000 |
|  | 47.25 | 0.798 | 6.08 | 1.540 | C | 0.000 | 27.535 | 1.540 | 100.00 | 18.352 | 0.000 |
| L32 47.50- |  |  |  |  | A | 0.000 | 1.540 |  | 100.00 | 0.708 | 0.000 |
| 47.00 |  |  |  |  | B | 0.000 | 1.540 |  | 100.00 | 1.100 | 0.000 |
|  |  | 0.784 | 5.98 | 15.624 | C | 0.000 | 1.540 | 15.624 | 100.00 | 0.708 | 0.000 |
| L33 47.00- | 44.49 |  |  |  | A | 0.000 | 15.624 |  | 100.00 | 7.083 | 0.000 |
| 42.00 |  |  |  |  | B | 0.000 | 15.624 |  | 100.00 | 11.003 | 0.000 |
|  | 39.49 | 0.758 | 5.78 | 16.029 | C | 0.000 | 15.624 | 16.029 | 100.00 | 7.083 | 0.000 |
| L.34 42.00- |  |  |  |  | A | 0.000 | 16.029 |  | 100.00 | 11.335 | 0.000 |
| 37.00 |  |  |  |  | B | 0.000 | 16.029 |  | 100.00 | 15.255 | 0.000 |
|  | 35.62 | 0.736 | 5.61 | 8.985 | C | 0.000 | 16.029 | 8.985 | 100.00 | 11.335 | 0.000 |
| L35 37.00- |  |  |  |  | A | 0.000 | 8.985 |  | 100.00 | 7.789 | 0.000 |
| 34.25 |  |  |  |  | B | 0.000 | 8.985 |  | 100.00 | 9.944 | 0.000 |
|  | 34.12 | 0.727 | 5.54 | 0.823 | C | 0.000 | 8.985 | 0.823 | 100.00 | 7.789 | 0.000 |
| L36 34.25- |  |  |  |  | A | 0.000 | 0.823 |  | 100.00 | 0.708 | 0.000 |
| 34.00 |  |  |  |  | B | 0.000 | 0.823 |  | 100.00 | 0.904 | 0.000 |
|  | 31.49 | 0.71 | 5.42 | 16.677 | C | 0.000 | 0.823 | 16.677 | 100.00 | 0.708 | 0.000 |
| L37 34.00- |  |  |  |  | A | 0.000 | 16.677 |  | 100.00 | 14.167 | 0.000 |
| 29.00 |  |  |  |  | B | 0.000 | 16.677 |  | 100.00 | 18.087 | 0.000 |
|  | 27.87 | 0.7 | 5.34 | 7.636 | C | 0.000 | 16.677 | 7.636 | 100.00 | 14.167 | 0.000 |
| L38 29.00- |  |  |  |  | A | 0.000 | 7.636 |  | 100.00 | 6.375 | 0.000 |
| 26.75 |  |  |  |  | B | 0.000 | 7.636 |  | 100.00 | 8.139 | 0.000 |
|  | 26.62 | 0.7 | 5.34 | 0.854 | C | 0.000 | 7.636 | 0.854 | 100.00 | 6.375 | 0.000 |
| L39 26.75- |  |  |  |  | A | 0.000 | 0.854 |  | 100.00 | 0.708 | 0.000 |
| 26.50 |  |  |  |  | B | 0.000 | 0.854 |  | 100.00 | 0.904 | 0.000 |
|  | 23.99 | 0.7 | 5.34 | 17.284 | C | 0.000 | 0.854 | 17.284 | 100.00 | 0.708 | 0.000 |
| L40 26.50- |  |  |  |  | A | 0.000 | 17.284 |  | 100.00 | 14.167 | 0.000 |
| 21.50 |  |  |  |  | B | 0.000 | 17.284 |  | 100.00 | 18.087 | 0.000 |
|  | 19.12 | 0.7 | 5.34 | 16.794 | C | 0.000 | 17.284 | 16.794 | 100.00 | 14.167 | 0.000 |
| L41 21.50- |  |  |  |  | A | 0.000 | 16.794 |  | 100.00 | 12.750 | 0.000 |
| 16.75 |  |  |  |  | B | 0.000 | 16.794 |  | 100.00 | 16.474 | 0.000 |
|  | 16.62 | 0.7 | 5.34 | 0.893 | C | 0.000 | 16.794 | 0.893 | 100.00 | 7.438 | 0.000 |
| L42 16.75- |  |  |  |  | A | 0.000 | 0.893 |  | 100.00 | 0.708 | 0.000 |
| 16.50 |  |  |  |  | B | 0.000 | 0.893 |  | 100.00 | 0.904 | 0.000 |
|  | 15.37 | 0.7 | 5.34 | 8.084 | C | 0.000 | 0.893 | 8.084 | 100.00 | 0.354 | 0.000 |
| L43 16.50- |  |  |  |  | A | 0.000 | 8.084 |  | 100.00 | 6.375 | 0.000 |
| 14.25 |  |  |  |  | B | 0.000 | 8.084 |  | 100.00 | 8.139 | 0.000 |
|  | 14.12 | 0.7 | 5.34 |  | C | 0.000 | 8.084 | 0.903 | 100.00 | 3.188 | 0.000 |
| L44 14.25- |  |  |  | 0.903 | A | 0.000 | 0.903 |  | 100.00 | 0.708 | 0.000 |
| 14.00 |  |  |  |  | B | 0.000 | 0.903 |  | 100.00 | 0.904 | 0.000 |
|  | 11.49 | 0.7 | 5.34 |  | C | 0.000 | 0.903 | 18.284 | 100.00 | 0.354 | 0.000 |
| L45 14.00- |  |  |  | 18.284 | A | 0.000 | 18.284 |  | 100.00 | 12.042 | 0.000 |
| 9.00 |  |  |  |  | B | 0.000 | 18.284 |  | 100.00 | 18.087 | 0.000 |
|  | 6.62 | 0.7 | 5.34 |  | C | 0.000 | 18.284 |  | 100.00 | 7.083 | 0.000 |
| L46 9.00-4.25 |  |  |  | 17.743 | A | 0.000 | 17.743 | 17.743 | 100.00 | 6.729 | 0.000 |
|  |  |  |  |  | B | 0.000 | 17.743 |  | 100.00 | 17.182 | 0.000 |
|  | 4.12 |  | 5.34 |  | C | 0.000 | 17.743 |  | 100.00 | 6.729 | 0.000 |
| L47 4.25-4.00 |  | 0.7 |  | 0.945 | A | 0.000 | 0.945 | 0.945 | 100.00 | 0.354 | 0.000 |
|  |  |  |  |  | B | 0.000 | 0.945 |  | 100.00 | 0.904 | 0.000 |
|  | 1.99 |  | 5.34 |  | C | 0.000 | 0.945 | 15.254 | 100.00 | 0.354 | 0.000 |
| L.48 4.00-0.00 |  | 0.7 |  | 15.254 | A | 0.000 | 15.254 |  | 100.00 | 4.958 | 0.000 |
|  |  |  |  |  | B | 0.000 | 15.254 |  | 100.00 | 13.053 | 0.000 |
|  |  |  |  |  | C | 0.000 | 15.254 |  | 100.00 | 4.958 | 0.000 |

## Load Combinations

| Comb. No. | Description |
| :---: | :---: |
| 1 | Dead Only |
| 2 | 1.2 Dead+1.0 Wind 0 deg - No Ice |
| 3 | 0.9 Dead+1.0 Wind 0 deg - No Ice |
| 4 | 1.2 Dead+1.0 Wind 30 deg - No Ice |
| 5 | 0.9 Dead+1.0 Wind 30 deg - No Ice |
| 6 | 1.2 Dead+1.0 Wind 60 deg - No Ice |
| 7 | 0.9 Dead+1.0 Wind 60 deg - No Ice |
| 8 | 1.2 Dead+1.0 Wind 90 deg - No Ice |
| 9 | 0.9 Dead+1.0 Wind 90 deg - No Ice |
| 10 | 1.2 Dead+1.0 Wind 120 deg - No Ice |
| 11 | 0.9 Dead+1.0 Wind 120 deg - No Ice |
| 12 | 1.2 Dead+1.0 Wind 150 deg - No Ice |
| 13 | 0.9 Dead+1.0 Wind 150 deg - No Ice |
| 14 | 1.2 Dead+1.0 Wind 180 deg - No Ice |
| 15 | 0.9 Dead+1.0 Wind 180 deg - No Ice |
| 16 | 1.2 Dead+1.0 Wind 210 deg - No Ice |
| 17 | 0.9 Deadt 1.0 Wind 210 deg - No Ice |
| 18 | 1.2 Dead+1.0 Wind 240 deg - No Ice |
| 19 | 0.9 Dead+1.0 Wind 240 deg - No Ice |
| 20 | 1.2 Dead+1.0 Wind 270 deg - No Ice |
| 21 | 0.9 Dead+1.0 Wind 270 deg - No Ice |
| 22 | 1.2 Dead+1.0 Wind 300 deg - No Ice |
| 23 | 0.9 Dead+1.0 Wind 300 deg - No Ice |
| 24 | 1.2 Dead +1.0 Wind 330 deg - No Ice |
| 25 | 0.9 Dead+1.0 Wind 330 deg - No Ice |
| 26 | 1.2 Dead+1.0 Ice+1.0 Temp |
| 27 | 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp |
| 28 | 1.2 Dead+1.0 Wind $30 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 29 | 1.2 Dead+1.0 Wind 60 deg+1.0 Ice +1.0 Temp |
| 30 | 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp |
| 31 | 1.2 Dead+1.0 Wind $120 \mathrm{deg}+1.0$ Ice +1.0 Temp |
| 32 | 1.2 Dead +1.0 Wind $150 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 33 | 1.2 Dead+1.0 Wind $180 \mathrm{deg}+1.0$ Ice+1.0 Temp |
| 34 | 1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp |
| 35 | 1.2 Dead +1.0 Wind $240 \mathrm{deg}+1.0$ Ice +1.0 Temp |
| 36 | 1.2 Dead+1.0 Wind 270 deg +1.0 Ice+1.0 Temp |
| 37 | 1.2 Dead+1.0 Wind $300 \mathrm{deg}+1.0 \mathrm{Ice}+1.0$ Temp |
| 38 | 1.2 Dead+1.0 Wind $330 \mathrm{deg}+1.0$ lce+1.0 Temp |
| 39 | Dead+Wind 0 deg - Service |
| 40 | Dead+Wind 30 deg - Service |
| 41 | Dead+Wind 60 deg - Service |
| 42 | Dead+Wind 90 deg - Service |
| 43 | Dead+Wind 120 deg - Service |
| 44 | Dead+Wind 150 deg - Service |
| 45 | Dead+Wind 180 deg - Service |
| 46 | Dead+Wind 210 deg - Service |
| 47 | Dead+Wind 240 deg - Service |
| 48 | Dead+Wind 270 deg - Service |
| 49 | Dead+Wind 300 deg - Service |
| 50 | Dead+Wind 330 deg-Service |

Maximum Member Forces

| $\begin{gathered} \hline \text { Sectio } \\ n \\ \text { No. } \\ \hline \end{gathered}$ | Elevation ft | Component Type | Condition | Gov. Load Comb | Axial $K$ | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 151-146 | Pole | Max Tension | 39 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -8.36 | -0.72 | 2.26 |
|  |  |  | Max. Mx | 8 | -3.02 | -19.53 | 0.19 |
|  |  |  | Max. My | 2 | -3.02 | -0.31 | 19.53 |
|  |  |  | Max. Vy | 8 | 5.20 | -19.53 | 0.19 |
|  |  |  | Max. Vx | 2 | -5.20 | -0.31 | 19.53 |
|  |  |  | Max. Torque | 10 |  |  | 2.22 |
| L2 | 146-141 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -8.89 | -0.75 | 2.31 |



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151 Ft Monopole Tower Structural Analysis
CCI BU No 841295
Project Number 37519-2490.001.7805, Order 492710, Revision 0

| $\begin{gathered} \text { Sectio } \\ n \\ \text { No. } \\ \hline \end{gathered}$ | Elevation ft | Component Type | Condition | Gov. Load Comb. | Axial K | Major Axis Moment kip-ft | Minor Axis Moment kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L30 | 56.75-56.5 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -51.99 | -5.05 | 8.25 |
|  |  |  | Max. Mx | 8 | -28.21 | -1639.75 | 0.32 |
|  |  |  | Max. My | 2 | -28.21 | 0.35 | 1656.91 |
|  |  |  | Max. Vy | 8 | 24.61 | -1639.75 | 0.32 |
|  |  |  | Max. Vx | 14 | 24.80 | -4.52 | -1656.17 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L31 | $\begin{gathered} 56.5- \\ 47.499 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -53.98 | -5.20 | 8.35 |
|  |  |  | Max. Mx | 8 | -29.66 | -1751.73 | 0.21 |
|  |  |  | Max. My | 14 | -29.64 | -4.68 | -1768.90 |
|  |  |  | Max. Vy | 8 | 25.15 | -1751.73 | 0.21 |
|  |  |  | Max. Vx | 14 | 25.32 | -4.68 | -1768.90 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| 132 | $\begin{gathered} 47.499- \\ 46.999 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -57.86 | -5.36 | 8.46 |
|  |  |  | Max. Mx | 8 | -32.64 | -1879.19 | 0.10 |
|  |  |  | Max. My | 14 | -32.63 | -4.86 | -1897.09 |
|  |  |  | Max. Vy | 8 | 25.83 | -1879.19 | 0.10 |
|  |  |  | Max. Vx | 14 | 25.97 | -4.86 | -1897.09 |
|  |  |  | Max. Torque | 10 |  |  | $3.52$ |
| L33 | $\begin{gathered} 46.999 \\ 41.999 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -60.15 | -5.52 | 8.57 |
|  |  |  | Max. Mx | 8 | -34.43 | -2009.70 | -0.02 |
|  |  |  | Max. My | 14 | -34.42 | -5.05 | -2028.16 |
|  |  |  | Max. Vy | 8 | 26.38 | -2009.70 | -0.02 |
|  |  |  | Max. Vx | 14 | 26.48 | -5.05 | -2028.16 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L34 | $\begin{gathered} 41.999- \\ 36.999 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | $-62.57$ | $-5.68$ | $8.68$ |
|  |  |  | Max. Mx | 8 | -36.25 | $-2142.93$ | $-0.13$ |
|  |  |  | Max. My | 14 | -36.24 | -5.23 | -2161.80 |
|  |  |  | Max. Vy | 8 | 26.93 | -2142.93 | -0.13 |
|  |  |  | Max. Vx | 14 | 27.01 | -5.23 | -2161.80 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L35 | $\begin{gathered} 36.999- \\ 34.25 \end{gathered}$ | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -63.96 | $-5.77$ | 8.74 |
|  |  |  | Max. Mx | 8 | -37.26 | $-2217.34$ | -0.20 |
|  |  |  | Max. My | 14 | -37.25 | -5.33 | -2236.42 |
|  |  |  | Max. Vy | 8 | 27.23 | -2217.34 | -0.20 |
|  |  |  | Max. Vx | 14 | 27.32 | -5.33 | -2236.42 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L36 | 34.25-34 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -64.08 | -5.78 | 8.75 |
|  |  |  | Max. Mx | 8 | -37.36 | -2224.15 | -0.20 |
|  |  |  | Max. My | 14 | -37.36 | -5.34 | -2243.25 |
|  |  |  | Max. Vy | 8 | 27.24 . | -2224.15 | -0.20 |
|  |  |  | Max. Vx | 14 | 27.33 | -5.34 | -2243.25 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L37 | 34-29 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -66.61 | -5.92 | 8.83 |
|  |  |  | Max. Mx | 8 | -39.22 | -2361.68 | -0.32 |
|  |  |  | Max. My | 14 | -39.22 | -5.52 | -2381.14 |
|  |  |  | Max. Vy | 8 | 27.77 | -2361.68 | -0.32 |
|  |  |  | Max. Vx | 14 | 27.86 | -5.52 | -2381.14 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L38 | 29-26.75 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |
|  |  |  | Max. Compression | 26 | -67.75 | -5.98 | 8.87 |
|  |  |  | Max. Mx | 8 | -40.07 | -2424.42 | -0.37 |
|  |  |  | Max. My | 14 | -40.07 | -5.60 | -2444.04 |
|  |  |  | Max. Vy | 8 | 28.01 | -2424.42 | -0.37 |
|  |  |  | Max. Vx | 14 | 28.09 | -5.60 | -2444.04 |
|  |  |  | Max. Torque | 10 |  |  | 3.52 |
| L39 | 26.75-26.5 | Pole | Max Tension | 1 | 0.00 | 0.00 | 0.00 |

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| Sectio <br> $n$ <br> No. | Elevation <br> ft | Component <br> Type | Condition | Gov. <br> Load <br> Comb. | Axial <br> K | Major Axis <br> Moment <br> kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |

## Maximum Reactions

| Location | Condition | Gov. Load Comb. | Vertical K | $\begin{gathered} \text { Horizontal, X } \\ K \end{gathered}$ | Horizontal, Z K |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Pole | Max. Vert | 26 | 81.70 | 0.00 | -0.00 |
|  | Max. $\mathrm{H}_{\mathrm{x}}$ | 21 | 38.40 | 29.46 | 0.03 |
|  | Max. $\mathrm{Hz}_{\mathrm{z}}$ | 2 | 51.20 | 0.03 | 29.79 |
|  | Max. $\mathrm{M}_{\mathrm{x}}$ | 2 | 3209.26 | 0.03 | 29.79 |
|  | Max. $\mathrm{M}_{\mathbf{z}}$ | 8 | 3209.95 | -30.68 | -0.03 |
|  | Max. Torsion | 10 | 3.51 | -25.94 | -15.09 |
|  | Min. Vert | 3 | 38.40 | 0.03 | 29.79 |
|  | Min. $\mathrm{H}_{\mathrm{x}}$ | 8 | 51.20 | -30.68 | -0.03 |
|  | Min. $\mathrm{H}_{\mathbf{z}}$ | 15 | 38.40 | -0.03 | -30.75 |
|  | Min. $\mathrm{M}_{\mathrm{x}}$ | 14 | -3231.34 | -0.03 | -30.75 |
|  | Min. $\mathrm{M}_{\mathbf{z}}$ | 20 | -3163.87 | 29.46 | 0.03 |
|  | Min. Torsion | 22 | -3.51 | 25.72 | 14.96 |

## Tower Mast Reaction Summary

| Load Combination | Vertical $K$ | Shear <br> $K$ | Shearz $K$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Dead Only | 42.67 | -0.00 | 0.00 | -2.31 | -1.92 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg No lce | 51.20 | -0.03 | -29.79 | -3209.26 | 1.52 | 1.60 |
| $\begin{aligned} & \text { 0.9 Dead+1.0 Wind } 0 \text { deg - } \\ & \text { No Ice } \end{aligned}$ | 38.40 | -0.03 | -29.79 | -3169.51 | 2.13 | 1.56 |
| 1.2 Dead+1.0 Wind 30 deg No lce | 51.20 | 14.70 | -25.67 | -2767.59 | -1582.21 | -0.21 |
| 0.9 Dead+1.0 Wind 30 deg No lce | 38.40 | 14.70 | -25.67 | -2733.20 | -1562.37 | -0.24 |
| 1.2 Dead+1.0 Wind 60 deg No Ice | 51.20 | 26.17 | -15.19 | -1601.24 | -2750.31 | -1.94 |
| 0.9 Dead+1.0 Wind 60 deg No lce | 38.40 | 26.17 | -15.19 | -1581.10 | -2716.43 | -1.94 |
| 1.2 Dead+1.0 Wind 90 deg No Ice | 51.20 | 30.68 | 0.03 | 1.00 | -3209.95 | -3.15 |
| 0.9 Dead +1.0 Wind 90 deg No Ice | 38.40 | 30.68 | 0.03 | 1.75 | -3170.61 | -3.12 |
| 1.2 Dead+1.0 Wind 120 deg <br> - No Ice | 51.20 | 25.94 | 15.09 | 1591.45 | -2735.79 | -3.51 |
| 0.9 Dead+1.0 Wind 120 deg <br> - No Ice | 38.40 | 25.94 | 15.09 | 1572.92 | -2702.00 | -3.47 |
| 1.2 Dead+1.0 Wind 150 deg <br> - No Ice | 51.20 | 15.06 | 26.24 | 2770.78 | -1592.20 | -2.93 |
| 0.9 Dead+1.0 Wind 150 deg <br> - No Ice | 38.40 | 15.06 | 26.24 | 2737.95 | -1572.27 | -2.88 |
| 1.2 Dead+1.0 Wind 180 deg <br> - No lce | 51.20 | 0.03 | 30.75 | 3231.34 | -6.54 | -1.60 |
| 0.9 Dead+1.0 Wind 180 deg <br> - No Ice | 38.40 | 0.03 | 30.75 | 3193.07 | -5.82 | -1.56 |
| 1.2 Dead+1.0 Wind 210 deg <br> - No Ice | 51.20 | -15.32 | 26.73 | 2797.04 | 1597.68 | 0.22 |
| 0.9 Dead+1.0 Wind 210 deg <br> - No Ice | 38.40 | -15.32 | 26.73 | 2764.08 | 1579.07 | 0.25 |
| 1.2 Dead+1.0 Wind 240 deg <br> - No lce | 51.20 | -25.85 | 15.01 | 1583.93 | 2725.78 | 1.95 |
| 0.9 Dead+1.0 Wind 240 deg <br> - No Ice | 38.40 | -25.85 | 15.01 | 1565.49 | 2693.39 | 1.95 |
| 1.2 Dead+1.0 Wind 270 deg | 51.20 | -29.46 | -0.03 | -7.06 | 3163.87 | 3.15 |


| Load Combination | Vertical K | Shear ${ }_{x}$ $K$ | Shearz $K$ | Overturning Moment, $M_{x}$ kip-ft | Overturning Moment, $M_{z}$ kip-ft | Torque kip-ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 0.9 Dead +1.0 Wind 270 deg <br> - No Ice | 38.40 | -29.46 | -0.03 | -6.20 | 3126.12 | 3.12 |
| 1.2 Dead+1.0 Wind 300 deg <br> - No Ice | 51.20 | -25.72 | -14.96 | -1605.71 | 2744.97 | 3.51 |
| 0.9 Dead +1.0 Wind 300 deg <br> - No Ice | 38.40 | -25.72 | -14.96 | -1585.49 | 2712.39 | 3.46 |
| 1.2 Dead+1.0 Wind 330 deg <br> - No lce | 51.20 | -15.33 | -26.69 | -2806.17 | 1604.11 | 2.93 |
| 0.9 Dead+1.0 Wind 330 deg <br> - No ice | 38.40 | -15.33 | -26.69 | -2771.53 | 1585.40 | 2.88 |
| 1.2 Dead+1.0 Ice+1.0 Temp | 81.70 | -0.00 | 0.00 | -9.83 | -6.67 | 0.00 |
| 1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp | 81.70 | -0.01 | -6.77 | -835.35 | -5.79 | 0.72 |
| 1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp | 81.70 | 3.33 | -5.82 | -718.60 | -412.05 | 0.14 |
| 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp | 81.70 | 5.85 | -3.39 | -420.11 | -712.43 | -0.46 |
| 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp | 81.70 | 6.83 | 0.01 | -8.99 | -828.02 | -0.94 |
| 1.2 Dead +1.0 Wind 120 deg+1.0 Ice+1.0 Temp | 81.70 | 5.81 | 3.38 | 399.96 | -710.08 | -1.17 |
| 1.2 Dead +1.0 Wind 150 deg+1.0 lce +1.0 Temp | 81.70 | 3.36 | 5.85 | 700.04 | -413.93 | -1.08 |
| 1.2 Dead+1.0 Wind 180 deg+1.0 Ice +1.0 Temp | 81.70 | 0.01 | 6.87 | 819.87 | -7.71 | -0.72 |
| 1.2 Dead+1.0 Wind 210 deg+1.0 Ice +1.0 Temp | 81.70 | -3.41 | 5.95 | 706.49 | 403.05 | -0.14 |
| 1.2 Dead+1.0 Wind 240 deg+1.0 Ice +1.0 Temp | 81.70 | -5.79 | 3.36 | 398.20 | 695.45 | 0.47 |
| 1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp | 81.70 | -6.68 | -0.01 | -10.92 | 805.49 | 0.95 |
| 1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp | 81.70 | -5.84 | -3.39 | -421.65 | 699.67 | 1.17 |
| 1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp | 81.70 | -3.42 | -5.95 | -727.20 | 404.62 | 1.08 |
| Dead+Wind 0 deg - Service | 42.67 | -0.01 | -6.46 | -693.42 | -1.21 | 0.35 |
| Dead+Wind 30 deg - Service | 42.67 | 3.19 | -5.57 | -598.38 | -342.56 | -0.05 |
| Dead+Wind 60 deg - Service | 42.67 | 5.68 | -3.30 | -347.00 | -594.34 | -0.43 |
| Dead+Wind 90 deg - Service | 42.67 | 6.66 | 0.01 | -1.65 | -693.35 | -0.69 |
| Dead+Wind 120 deg Service | 42.67 | 5.63 | 3.27 | 341.13 | -591.17 | -0.77 |
| Dead+Wind 150 deg Service | 42.67 | 3.27 | 5.69 | 595.35 | -344.73 | -0.64 |
| Dead+Wind 180 deg Service | 42.67 | 0.01 | 6.67 | 694.47 | -2.95 | -0.35 |
| Dead+Wind 210 deg Service | 42.67 | -3.32 | 5.80 | 601.03 | 342.84 | 0.05 |
| Dead + Wind 240 deg Service | 42.67 | -5.61 | 3.26 | 339.50 | 585.93 | 0.43 |
| Dead+Wind 270 deg Service | 42.67 | -6.39 | -0.01 | -3.39 | 680.31 | 0.69 |
| Dead+Wind 300 deg Service | 42.67 | -5.58 | -3.25 | -347.96 | 590.11 | 0.77 |
| Dead+Wind 330 deg Service | 42.67 | -3.33 | -5.79 | -606.74 | 344.22 | 0.64 |

Solution Summary

|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | $P Y$ | $P Z$ | $P X$ | $P Y$ | $P Z$ | \% Error |
| Comb. | $K$ | $K$ | $K$ | $K$ | $K$ | $K$ |  |
| 1 | 0.00 | -4.67 | 0.00 | 0.00 | 42.67 | -0.00 | $0.003 \%$ |
| 2 | -0.03 | -51.20 | -29.79 | 0.03 | 51.20 | 29.79 | $0.001 \%$ |
| 3 | -0.03 | -38.40 | -29.79 | 0.03 | 38.40 | 29.79 | $0.001 \%$ |
| 4 | 14.70 | -51.20 | -25.67 | -14.70 | 51.20 | 25.67 | $0.000 \%$ |
| 5 | 14.70 | -38.40 | -25.67 | -14.70 | 38.40 | 25.67 | $0.000 \%$ |
| 6 | 26.17 | -51.20 | -15.19 | -26.17 | 51.20 | 15.19 | $0.000 \%$ |

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|  | Sum of Applied Forces |  |  | Sum of Reactions |  |  | \% Error |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Load | $P X$ | PY | PZ | $P X$ | PY | PZ |  |
| Comb. | K | K | $K$ | K | K | K |  |
| 7 | 26.17 | -38.40 | -15.19 | -26.17 | 38.40 | 15.19 | 0.000\% |
| 8 | 30.68 | -51.20 | 0.03 | -30.68 | 51.20 | -0.03 | 0.000\% |
| 9 | 30.68 | -38.40 | 0.03 | -30.68 | 38.40 | -0.03 | 0.001\% |
| 10 | 25.94 | -51.20 | 15.09 | -25.94 | 51.20 | -15.09 | 0.000\% |
| 11 | 25.94 | -38.40 | 15.09 | -25.94 | 38.40 | -15.09 | 0.000\% |
| 12 | 15.06 | -51.20 | 26.24 | -15.06 | 51.20 | -26.24 | 0.000\% |
| 13 | 15.06 | -38.40 | 26.24 | -15.06 | 38.40 | -26.24 | 0.000\% |
| 14 | 0.03 | -51.20 | 30.75 | -0.03 | 51.20 | -30.75 | 0.001\% |
| 15 | 0.03 | -38.40 | 30.75 | -0.03 | 38.40 | -30.75 | 0.001\% |
| 16 | -15.32 | -51.20 | 26.73 | 15.32 | 51.20 | -26.73 | 0.000\% |
| 17 | -15.32 | -38.40 | 26.73 | 15.32 | 38.40 | -26.73 | 0.000\% |
| 18 | -25.85 | -51.20 | 15.01 | 25.85 | 51.20 | -15.01 | 0.000\% |
| 19 | -25.85 | -38.40 | 15.01 | 25.85 | 38.40 | -15.01 | 0.000\% |
| 20 | -29.46 | -51.20 | -0.03 | 29.46 | 51.20 | 0.03 | 0.000\% |
| 21 | -29.46 | -38.40 | -0.03 | 29.46 | 38.40 | 0.03 | 0.000\% |
| 22 | -25.72 | -51.20 | -14.96 | 25.72 | 51.20 | 14.96 | 0.000\% |
| 23 | -25.72 | -38.40 | -14.96 | 25.72 | 38.40 | 14.96 | 0.000\% |
| 24 | -15.33 | -51.20 | -26.69 | 15.33 | 51.20 | 26.69 | 0.000\% |
| 25 | -15.33 | -38.40 | -26.69 | 15.33 | 38.40 | 26.69 | 0.000\% |
| 26 | 0.00 | -81.70 | 0.00 | 0.00 | 81.70 | -0.00 | 0.000\% |
| 27 | -0.01 | -81.70 | -6.77 | 0.01 | 81.70 | 6.77 | 0.000\% |
| 28 | 3.33 | -81.70 | -5.82 | -3.33 | 81.70 | 5.82 | 0.000\% |
| 29 | 5.85 | -81.70 | -3.39 | -5.85 | 81.70 | 3.39 | 0.000\% |
| 30 | 6.83 | -81.70 | 0.01 | -6.83 | 81.70 | -0.01 | 0.000\% |
| 31 | 5.81 | -81.70 | 3.38 | -5.81 | 81.70 | -3.38 | 0.000\% |
| 32 | 3.36 | -81.70 | 5.85 | -3.36 | 81.70 | -5.85 | 0.000\% |
| 33 | 0.01 | -81.70 | 6.87 | -0.01 | 81.70 | -6.87 | 0.000\% |
| 34 | -3.41 | -81.70 | 5.95 | 3.41 | 81.70 | -5.95 | 0.000\% |
| 35 | -5.79 | -81.70 | 3.36 | 5.79 | 81.70 | -3.36 | 0.000\% |
| 36 | -6.68 | -81.70 | -0.01 | 6.68 | 81.70 | 0.01 | 0.000\% |
| 37 | -5.84 | -81.70 | -3.39 | 5.84 | 81.70 | 3.39 | 0.000\% |
| 38 | -3.42 | -81.70 | -5.95 | 3.42 | 81.70 | 5.95 | 0.000\% |
| 39 | -0.01 | -42.67 | -6.46 | 0.01 | 42.67 | 6.46 | 0.004\% |
| 40 | 3.19 | -42.67 | -5.57 | -3.19 | 42.67 | 5.57 | 0.001\% |
| 41 | 5.68 | -42.67 | -3.30 | -5.68 | 42.67 | 3.30 | 0.001\% |
| 42 | 6.66 | -42.67 | 0.01 | -6.66 | 42.67 | -0.01 | 0.002\% |
| 43 | 5.63 | -42.67 | 3.27 | -5.63 | 42.67 | -3.27 | 0.001\% |
| 44 | 3.27 | -42.67 | 5.69 | -3.27 | 42.67 | -5.69 | 0.001\% |
| 45 | 0.01 | -42.67 | 6.67 | -0.01 | 42.67 | -6.67 | 0.004\% |
| 46 | -3.32 | -42.67 | 5.80 | 3.32 | 42.67 | -5.80 | 0.001\% |
| 47 | -5.61 | -42.67 | 3.26 | 5.61 | 42.67 | -3.26 | 0.001\% |
| 48 | -6.39 | -42.67 | -0.01 | 6.39 | 42.67 | 0.01 | 0.002\% |
| 49 | -5.58 | -42.67 | -3.25 | 5.58 | 42.67 | 3.25 | 0.001\% |
| 50 | -3.33 | -42.67 | -5.79 | 3.33 | 42.67 | 5.79 | 0.001\% |

## Non-Linear Convergence Results

| Load Combination | Converged? | Number of Cycles | Displacement Tolerance | Force Tolerance |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Yes | 6 | 0.00000001 | 0.00001463 |
| 2 | Yes | 21 | 0.00000001 | 0.00009815 |
| 3 | Yes | 20 | 0.00000001 | 0.00013660 |
| 4 | Yes | 26 | 0.00000001 | 0.00008232 |
| 5 | Yes | 25 | 0.00000001 | 0.00011116 |
| 6 | Yes | 26 | 0.00000001 | 0.00008416 |
| 7 | Yes | 25 | 0.00000001 | 0.00011385 |
| 8 | Yes | 22 | 0.00000001 | 0.00010202 |
| 9 | Yes | 21 | 0.00000001 | 0.00014525 |
| 10 | Yes | 25 | 0.00000001 | 0.00014896 |
| 11 | Yes | 25 | 0.00000001 | 0.00010451 |
| 12 | Yes | 26 | 0.00000001 | 0.00008642 |
| 13 | Yes | 25 | 0.00000001 | 0.00011706 |
| 14 | Yes | 21 | 0.00000001 | 0.00011144 |
| 15 | Yes | 21 | 0.00000001 | 0.00008209 |
| 16 | Yes | 26 | 0.00000001 | 0.00008222 |
| 17 | Yes | 25 | 0.00000001 | 0.00011132 |
| 18 | Yes | 25 | 0.00000001 | 0.00014993 |
| 19 | Yes | 25 | 0.00000001 | 0.00010540 |
| 20 | Yes | 22 | 0.00000001 | 0.00010900 |
| 21 | Yes | 22 | 0.00000001 | 0.00008142 |
| 22 | Yes | 26 | 0.00000001 | 0.00008643 |
| 23 | Yes | 25 | 0.00000001 | 0.00011716 |
| 24 | Yes | 26 | 0.00000001 | 0.00007981 |
| 25 | Yes | 25 | 0.00000001 | 0.00010768 |
| 26 | Yes | 15 | 0.00000001 | 0.00014859 |
| 27 | Yes | 23 | 0.00000001 | 0.00008508 |
| 28 | Yes | 23 | 0.00000001 | 0.00010860 |
| 29 | Yes | 23 | 0.00000001 | 0.00010917 |
| 30 | Yes | 23 | 0.00000001 | 0.00008402 |
| 31 | Yes | 23 | 0.00000001 | 0.00010201 |
| 32 | Yes | 23 | 0.00000001 | 0.00010637 |
| 33 | Yes | 22 | 0.00000001 | 0.00014614 |
| 34 | Yes | 23 | 0.00000001 | 0.00010124 |
| 35 | Yes | 23 | 0.00000001 | 0.00009945 |
| 36 | Yes | 22 | 0.00000001 | 0.00014562 |
| 37 | Yes | 23 | 0.00000001 | 0.00010845 |
| 38 | Yes | 23 | 0.00000001 | 0.00010525 |
| 39 | Yes | 16 | 0.00014670 | 0.00013332 |
| 40 | Yes | 19 | 0.00000001 | 0.00009556 |
| 41 | Yes | 19 | 0.00000001 | 0.00010833 |
| 42 | Yes | 17 | 0.00000001 | 0.00013208 |
| 43 | Yes | 18 | 0.00000001 | 0.00014859 |
| 44 | Yes | 19 | 0.00000001 | 0.00011465 |
| 45 | Yes | 16 | 0.00014645 | 0.00013443 |
| 46 | Yes | 19 | 0.00000001 | 0.00009387 |
| 47 | Yes | 18 | 0.00000001 | 0.00014854 |
| 48 | Yes | 17 | 0.00000001 | 0.00013168 |
| 49 | Yes | 19 | 0.00000001 | 0.00011846 |
| 50 | Yes | 19 | 0.00000001 | 0.00008491 |

## Maximum Tower Deflections - Service Wind

| Section <br> No. | Elevation <br> ft | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt <br> 0 | Twist <br> o |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $151-146$ | 22.3859 | 39 | 1.3829 | 0.0120 |
| L2 | $146-141$ | 20.9386 | 39 | 1.3793 | 0.0114 |
| L3 | $141-136$ | 19.5025 | 39 | 1.3619 | 0.0099 |
| L4 | $136-131$ | 18.0915 | 39 | 1.3298 | 0.0083 |
| L5 | $131-126$ | 16.7238 | 39 | 1.2800 | 0.0069 |
| L6 | $126-125.5$ | 15.4161 | 39 | 1.2150 | 0.0056 |
| L7 | $125.5-125.25$ | 15.2892 | 39 | 1.2078 | 0.0054 |
| L8 | $125.25-120.25$ | 15.2261 | 39 | 1.2055 | 0.0054 |
| L9 | $120.25-118.5$ | 13.9897 | 39 | 1.1544 | 0.0047 |


| Section | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tit |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L10 | $118.5-118.25$ | 13.5701 | 39 | 1.1348 | Twist |
| L11 | $118.25-117.5$ | 13.5107 | 39 | 1.1332 | 0.0044 |
| L12 | $117.5-117.25$ | 13.3332 | 39 | 1.1281 | 0.0044 |
| L13 | $117.25-112.25$ | 13.2742 | 39 | 1.1259 | 0.0043 |
| L14 | $112.25-107.25$ | 12.1198 | 39 | 1.0781 | 0.0043 |
| L15 | $107.25-102.25$ | 11.0184 | 39 | 1.0250 | 0.0038 |
| L16 | $102.25-97.5$ | 9.9750 | 39 | 0.9672 | 0.0033 |
| L17 | $100.916-95.916$ | 9.7070 | 39 | 0.9514 | 0.0029 |
| L18 | $95.916-92.5$ | 8.7269 | 39 | 0.9149 | 0.0028 |
| L19 | $92.5-92.25$ | 8.0857 | 39 | 0.8775 | 0.0026 |
| L.20 | $92.25-87.25$ | 8.0398 | 39 | 0.8748 | 0.0024 |
| L21 | $87.25-87$ | 7.1553 | 50 | 0.8180 | 0.0024 |
| L22 | $87-82$ | 7.1126 | 50 | 0.8155 | 0.0021 |
| L23 | $82-77$ | 6.2870 | 50 | 0.7646 | 0.0021 |
| L24 | $77-72$ | 5.5149 | 50 | 0.7125 | 0.0019 |
| L25 | $72-67$ | 4.7977 | 50 | 0.6591 | 0.0017 |
| L26 | $67-63.25$ | 4.1364 | 50 | 0.6048 | 0.0015 |
| L27 | $63.25-63$ | 3.6775 | 50 | 0.5641 | 0.0013 |
| L28 | $63-58$ | 3.6480 | 50 | 0.5614 | 0.0012 |
| L29 | $58-56.75$ | 3.0889 | 50 | 0.5066 | 0.0012 |
| L30 | $56.75-56.5$ | 2.9580 | 50 | 0.4931 | 0.0010 |
| L31 | $56.5-47.499$ | 2.9322 | 50 | 0.4907 | 0.0010 |
| L32 | $51.999-46.999$ | 2.4902 | 50 | 0.4473 | 0.0009 |
| L33 | $46.999-41.999$ | 2.0341 | 50 | 0.4215 | 0.0008 |
| L34 | $41.999-36.999$ | 1.6171 | 50 | 0.3750 | 0.0008 |
| L35 | $36.999-34.25$ | 1.2488 | 50 | 0.3283 | 0.0007 |
| L36 | $34.25-34$ | 1.0672 | 50 | 0.3029 | 0.0006 |
| L37 | $34-29$ | 1.0514 | 50 | 0.3005 | 0.0005 |
| L38 | $29-26.75$ | 0.7611 | 50 | 0.2539 | 0.0005 |
| L39 | $26.75-26.5$ | 0.6463 | 50 | 0.2332 | 0.0004 |
| L40 | $26.5-21.5$ | 0.6341 | 50 | 0.2309 | 0.0004 |
| L41 | $21.5-16.75$ | 0.4167 | 50 | 0.1844 | 0.0004 |
| L42 | $16.75-16.5$ | 0.2550 | 50 | 0.1409 | 0.0003 |
| L43 | $16.5-14.25$ | 0.2476 | 50 | 0.1389 | 0.0002 |
| L44 | $14.25-14$ | 0.1863 | 50 | 0.1214 | 0.0002 |
| L45 | $14-9$ | 0.1800 | 50 | 0.1194 | 0.0002 |
| L46 | $9-4.25$ | 0.0765 | 50 | 0.0783 | 0.0002 |
| L47 | $4.25-4$ | 0.0177 | 50 | 0.0399 | 0.0001 |
| L48 | $4-0$ | 0.0157 | 50 | 0.0376 | 0.0001 |
|  |  |  |  |  | 0.0001 |
|  |  |  |  |  |  |

## Critical Deflections and Radius of Curvature - Service Wind

| Elevation f | Appurtenance | Gov. Load Comb. | Deflection in | $\underset{\substack{\text { Tilt }}}{ }$ | Twist | Radius of Curvature ft |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 148.00 | (2) AM-X-CD-16-65-00T-RET wf Mount Pipe | 39 | 21.5168 | 1.3819 | 0.0117 | 26203 |
| 140.00 | DB854DG65ESX w/ Mount Pipe | 39 | 19.2177 | 1.3568 | 0.0096 | 10242 |
| 132.00 | TME-1900MHZ RRH | 39 | 16.9930 | 1.2910 | 0.0071 | 5215 |
| 130.00 | GPS-TMG-HR-26NCM | 39 | 16.4569 | 1.2687 | 0.0066 | 4705 |
| 122.00 | ERICSSON AIR 21 B2A B4P wl Mount Pipe | 39 | 14.4163 | 1.1749 | 0.0050 | 5466 |

Maximum Tower Deflections - Design Wind

| Section <br> No. | Elevation <br> ft | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt <br> 0 | Twist <br> 0 |
| :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | $151-146$ | 103.2916 | 2 | 6.3641 | 0.0551 |
| L2 | $146-141$ | 96.6437 | 2 | 6.3487 | 0.0522 |
| L3 | $141-136$ | 90.0449 | 2 | 6.2709 | 0.0455 |
| L4 | $136-131$ | 83.5713 | 14 | 6.1279 | 0.0381 |
| L5 | $131-126$ | 77.2976 | 14 | 5.9029 | 0.0313 |
| L6 | $126-125.5$ | 71.2913 | 14 | 5.6063 | 0.0254 |
| L7 | $125.5-125.25$ | 70.7083 | 14 | 5.5730 | 0.0248 |


| Section | Elevation | Horz. <br> Deflection <br> in | Gov. <br> Load <br> Comb. | Tilt | Twist |
| :---: | :---: | :---: | :---: | :---: | :---: |
| No. |  | Ct | 14 |  |  |
| L8 | $125.25-120.25$ | 70.4179 | 5.5626 | 0.0247 |  |
| L9 | $120.25-118.5$ | 64.7326 | 14 | 5.3294 | 0.0213 |
| L10 | $118.5-118.25$ | 62.8017 | 14 | 5.2402 | 0.0201 |
| L11 | $118.25-117.5$ | 62.5284 | 14 | 5.2325 | 0.0200 |
| L12 | $117.5-117.25$ | 61.7108 | 14 | 5.2094 | 0.0197 |
| L13 | $117.25-112.25$ | 61.4392 | 14 | 5.1994 | 0.0196 |
| L14 | $112.25-107.25$ | 56.1214 | 14 | 4.9811 | 0.0173 |
| L15 | $107.25-102.25$ | 51.0424 | 14 | 4.7376 | 0.0153 |
| L16 | $102.25-97.5$ | 46.2268 | 14 | 4.4722 | 0.0133 |
| L17 | $100.916-95.916$ | 44.9890 | 14 | 4.3993 | 0.0129 |
| L18 | $95.916-92.5$ | 40.4608 | 14 | 4.2316 | 0.0119 |
| L19 | $92.5-92.25$ | 37.4969 | 14 | 4.0605 | 0.0109 |
| L20 | $92.25-87.25$ | 37.2848 | 14 | 4.0479 | 0.0109 |
| L21 | $87.25-87$ | 33.1851 | 14 | 3.7873 | 0.0096 |
| L22 | $87-82$ | 32.9873 | 14 | 3.7759 | 0.0095 |
| L23 | $82-77$ | 29.1579 | 14 | 3.5422 | 0.0085 |
| L24 | $77-72$ | 25.5763 | 14 | 3.3020 | 0.0076 |
| L25 | $72-67$ | 22.2489 | 14 | 3.0561 | 0.0067 |
| L26 | $67-63.25$ | 19.1813 | 14 | 2.8052 | 0.0059 |
| L27 | $63.25-63$ | 17.0525 | 14 | 2.6175 | 0.0053 |
| L28 | $63-58$ | 16.9159 | 14 | 2.6050 | 0.0053 |
| L29 | $58-56.75$ | 14.3220 | 14 | 2.3506 | 0.0045 |
| L30 | $56.75-56.5$ | 13.7150 | 14 | 2.2879 | 0.0044 |
| L31 | $56.5-47.499$ | 13.5955 | 14 | 2.2766 | 0.0043 |
| L32 | $51.999-46.999$ | 11.5450 | 14 | 2.0749 | 0.0038 |
| L33 | $46.999-41.999$ | 9.4299 | 14 | 1.9553 | 0.0035 |
| L34 | $41.999-36.999$ | 7.4959 | 14 | 1.7394 | 0.0030 |
| L35 | $36.999-34.25$ | 5.7889 | 24 | 1.5224 | 0.0026 |
| L36 | $34.25-34$ | 4.9466 | 24 | 1.4042 | 0.0023 |
| L37 | $34-29$ | 4.8734 | 24 | 1.3935 | 0.0023 |
| L38 | $29-26.75$ | 3.5277 | 24 | 1.1774 | 0.0019 |
| L39 | $26.75-26.5$ | 2.9956 | 24 | 1.0811 | 0.0017 |
| L40 | $26.5-21.5$ | 2.9393 | 24 | 1.0704 | 0.0017 |
| L41 | $21.5-16.75$ | 1.9315 | 24 | 0.8549 | 0.0013 |
| L42 | $16.75-16.5$ | 1.1817 | 24 | 0.6530 | 0.0010 |
| L43 | $16.5-14.25$ | 1.1477 | 24 | 0.6440 | 0.0010 |
| L44 | $14.25-14$ | 0.8634 | 24 | 0.5627 | 0.0008 |
| L45 | $14-9$ | 0.8342 | 24 | 0.5533 | 0.0008 |
| L46 | $9-4.25$ | 0.3546 | 24 | 0.3630 | 0.0005 |
| L47 | $4.25-4$ | 0.0822 | 24 | 0.1850 | 0.0003 |
| L48 | $4-0$ | 0.0728 | 24 | 0.1741 | 0.0002 |
|  |  |  |  |  |  |

## Critical Deflections and Radius of Curvature - Design Wind

| Elevation <br> $f t$ | Appurtenance | Gov. <br> Load <br> Comb. | Deflection <br> in | Tilt <br> 0 | Twist <br> 0 | Radius of <br> Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 4 |  |  |  |  |  |  |


|  |  | Compression Checks Pole Design Data |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section No. | $\begin{aligned} & \text { Elevation } \\ & \text { ft } \end{aligned}$ | Size | $\begin{aligned} & \mathrm{L} \\ & \mathrm{ft} \\ & \hline \end{aligned}$ | $\begin{aligned} & L_{u} \\ & f t \end{aligned}$ | K/Vr | $\begin{gathered} A \\ i n^{2} \end{gathered}$ | $\begin{aligned} & \hline P_{u} \\ & K \\ & \hline \end{aligned}$ |
| L1 | 151-146 (1) | TP18.5255x17.59x0.2188 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 12.897 \\ 7 \end{gathered}$ | -3.02 |
| L2 | 146-141 (2) | TP19.461×18.5255×0.218 8 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 13.556 \\ 8 \end{gathered}$ | -3.33 |


| Section No. | $\begin{gathered} \text { Elevation } \\ \mathrm{ft} \end{gathered}$ | Size | $\begin{aligned} & \mathrm{L} \\ & \mathrm{f} \end{aligned}$ | $\begin{aligned} & L_{u} \\ & \mathrm{ft} \\ & \hline \end{aligned}$ | KI/r | $\begin{aligned} & \bar{A} \\ & i n^{2} \end{aligned}$ | $\begin{aligned} & P_{u} \\ & K \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L3 | 141-136 (3) | TP20.3965 ${ }_{8} 19.461 \times 0.218$ | 5.00 | 0.00 | 0.0 | $\frac{14.215}{9}$ | -6.93 |
| L4 | 136-131 (4) | TP21.3321×20.3965×0.21 | 5.00 | 0.00 | 0.0 | $\stackrel{14.875}{0}$ | -7.88 |
| L5 | 131-126 (5) | $\begin{gathered} \text { TP22.2676×21.3321×0.21 } \\ 88 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 15.534 \\ 2 \end{gathered}$ | -10.11 |
| L6 | $126-125.5$ <br> (6) | TP22.3611×22.2676x0.21 88 | 0.50 | 0.00 | 0.0 | $\begin{gathered} 15.600 \\ 1 \end{gathered}$ | -10.16 |
| L7 | $\begin{gathered} 125.5- \\ 125.25(7) \end{gathered}$ | TP22.4079×22.3611×0.36 | 0.25 | 0.00 | 0.0 | $\underset{0}{25.736}$ | -10.20 |
| L. 8 | $\begin{gathered} 125.25- \\ 120.25(8) \end{gathered}$ | TP23.3434×22.4079×0.35 63 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 26.372 \\ 8 \end{gathered}$ | -12.41 |
| L. 9 | $\begin{aligned} & 120.25- \\ & 118.5 \text { (9) } \end{aligned}$ | TP23.6708×23.3434×0.35 | 1.75 | 0.00 | 0.0 | $\begin{gathered} 26.748 \\ 4 \end{gathered}$ | -12.66 |
| L10 | $\begin{gathered} 118.5- \\ 118.25(10) \end{gathered}$ | TP23.7176×23.6708×0.64 38 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 47.832 \\ 9 \end{gathered}$ | -12.72 |
| L11 | $\begin{gathered} 118.25- \\ 117.5(11) \end{gathered}$ | TP23.8579×23.7176x0.64 38 | 0.75 | 0.00 | 0.0 | $\begin{gathered} 48.123 \\ 8 \end{gathered}$ | -12.88 |
| L12 | $\begin{gathered} 117.5- \\ 117.25(12) \end{gathered}$ | $\mathrm{TP} 23.9047 \times 23.8579 \times 0.49$ 38 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 37.224 \\ 2 \end{gathered}$ | -12.92 |
| L13 | $\begin{gathered} 117.25- \\ 112.25(13) \end{gathered}$ | TP24.8402×23.9047×0.48 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 37.751 \\ 1 \end{gathered}$ | -13.82 |
| L14 | $\begin{array}{r} 112.25- \\ 107.25(14) \end{array}$ | TP25.7757×24.8402×0.46 88 | 5.00 | 0.00 | 0.0 | $\underset{7}{38.201}$ | -14.76 |
| L15 | $\begin{gathered} 107.25- \\ 102.25(15) \end{gathered}$ | TP26.7113×25.7757×0.45 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 38.576 \\ 0 \end{gathered}$ | -15.72 |
| L16 | $\begin{gathered} 102.25-97.5 \\ \text { (16) } \end{gathered}$ | TP27.6x26.7113x0.4563 | 4.75 | 0.00 | 0.0 | $\begin{gathered} 38.942 \\ 8 \end{gathered}$ | -15.98 |
| L17 | $\begin{gathered} 97.5-95.916 \\ (17) \end{gathered}$ | TP27.4588×26.5233×0.55 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 47.655 \\ 5 \end{gathered}$ | -17.60 |
| L18 | $95.916-92.5$ | TP28.098x27.4588x0.55 | 3.42 | 0.00 | 0.0 | $\begin{gathered} 48.787 \\ 4 \end{gathered}$ | -18.40 |
| L19 | $\begin{gathered} 92.5-92.25 \\ (19) \end{gathered}$ | TP28.1447x28.098×0.55 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 48.870 \\ 3 \end{gathered}$ | -18.46 |
| L20 | $\begin{gathered} 92.25-87.25 \\ \text { (20) } \end{gathered}$ | TP29.0803×28.1447×0.53 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 49.400 \\ 4 \end{gathered}$ | -19.63 |
| L21 | $\underset{(21)}{87.25-87}$ | TP29.1271 $\times 29.0803 \times 0.62$ 5 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 57.360 \\ 4 \end{gathered}$ | -19.71 |
| 122 | 87-82 (22) | TP30.0626×29.1271×0.61 25 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 58.082 \\ 9 \end{gathered}$ | -21.03 |
| L23 | 82-77 (23) | TP30.9981x30.0626x0.6 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 58.729 \\ 2 \end{gathered}$ | -22.38 |
| L24 | 77-72 (24) | $\mathrm{TP} 31.9337 \times 30.9981 \times 0.58$ 75 | 5.00 | 0.00 | 0.0 | $\underset{1}{59.299}$ | -23.76 |
| L25 | 72-67 (25) | TP32.8692×31.9337×0.57 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 59.792 \\ 7 \end{gathered}$ | -25.16 |
| L26 | $\begin{gathered} 67-63.25 \\ (26) \end{gathered}$ | TP33.5709×32.8692×0.57 | 3.75 | 0.00 | 0.0 | $\begin{gathered} 61.091 \\ 8 \end{gathered}$ | -26.23 |
| L27 | $63.25-63$ | TP33.6176×33.5709×0.57 5 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 61.178 \\ 4 \end{gathered}$ | -26.31 |
| L28 | 63-58(28) | TP34.5532 25 $25.6176 \times 0.56$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 61.565 \\ 6 \end{gathered}$ | -27.75 |
| L29 | $\begin{gathered} 58-56.75 \\ (29) \end{gathered}$ | $\underset{25}{\text { TP34.7871 }} \underset{25453 \times 0.56}{ }$ | 1.25 | 0.00 | 0.0 | $\begin{gathered} 61.989 \\ 2 \end{gathered}$ | -28.11 |
| L30 | $\begin{gathered} 56.75-56.5 \\ (30) \end{gathered}$ | TP34.8338×34.7871×0.63 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 70.196 \\ 5 \end{gathered}$ | -28.21 |
| L31 | $\begin{gathered} 56.5-47.499 \\ (31) \end{gathered}$ | TP36.518×34.8338×0.637 | 9.00 | 0.00 | 0.0 | $\begin{gathered} 71.925 \\ 3 \end{gathered}$ | -29.64 |
| L32 | $\begin{gathered} 47.499- \\ 46.999(32) \end{gathered}$ | TP35.9865x35.051x0.7 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 79.535 \\ 8 \end{gathered}$ | -32.63 |
| L33 | $\begin{gathered} 46.999- \\ 41.999(33) \end{gathered}$ | TP36.922×35.9865×0.687 5 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 80.214 \\ 1 \end{gathered}$ | -34.42 |
| L.34 | $\begin{gathered} 41.999- \\ 36.999(34) \end{gathered}$ | TP37.8575 $\times 36.922 \times 0.675$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 80.816 \\ 2 \end{gathered}$ | -36.24 |
| L35 | $\begin{gathered} 36.999- \\ 34.25(35) \end{gathered}$ | TP38.3718×37.8575×0.67 | 2.75 | 0.00 | 0.0 | $\begin{gathered} 81.934 \\ 1 \end{gathered}$ | -37.25 |
| L36 | $\begin{gathered} 34.25-34 \\ (36) \end{gathered}$ | TP $38.4186 \times 38.3718 \times 0.67$ | 0.25 | 0.00 | 0.0 | $\begin{gathered} 82.035 \\ 8 \end{gathered}$ | -37.36 |
| L37 | 34-29(37) | TP39.3541×38.4186×0.66 25 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 82.538 \\ 9 \end{gathered}$ | -39.22 |

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| Section No. | Elevation ft | Size | $\begin{aligned} & L \\ & f t \end{aligned}$ | $\begin{aligned} & L_{u} \\ & f t \end{aligned}$ | KI/r | $\begin{gathered} A \\ i n^{2} \end{gathered}$ | $\begin{aligned} & P_{u} \\ & K \end{aligned}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L38 | $\begin{gathered} 29-26.75 \\ (38) \end{gathered}$ | $\begin{aligned} & \text { TP39.7751×39.3541×0.66 } \\ & 25 \end{aligned}$ | 2.25 | 0.00 | 0.0 | $\begin{gathered} 83.436 \\ 9 \end{gathered}$ | -40.07 |
| L39 | $\begin{gathered} 26.75-26.5 \\ (39) \end{gathered}$ | $\begin{gathered} \text { TP39.8219×39.7751×0.66 } \\ 25 \end{gathered}$ | 0.25 | 0.00 | 0.0 | $\begin{gathered} 83.536 \\ 7 \end{gathered}$ | -40.17 |
| L40 | $\begin{gathered} 26.5-21.5 \\ (40) \end{gathered}$ | TP40.7574×39.8219×0.65 | 5.00 | 0.00 | 0.0 | $\begin{gathered} 83.944 \\ 7 \end{gathered}$ | -42.07 |
| L41 | $\begin{gathered} 21.5-16.75 \\ (41) \end{gathered}$ | TP41.6461×40.7574×0.65 | 4.75 | 0.00 | 0.0 | $\begin{gathered} 85.804 \\ 8 \end{gathered}$ | -43.90 |
| L42 | $\begin{gathered} 16.75-16.5 \\ (42) \end{gathered}$ | $\begin{gathered} \text { TP41.6929x41.6461x0.76 } \\ 25 \end{gathered}$ | 0.25 | 0.00 | 0.0 | $\begin{gathered} 100.49 \\ 40 \end{gathered}$ | -44.03 |
| L43 | $16.5-14.25$ <br> (43) | TP42.1138×41.6929×0.76 25 | 2.25 | 0.00 | 0.0 | $\begin{gathered} 101.52 \\ 80 \end{gathered}$ | -45.09 |
| L44 | $\begin{gathered} 14.25-14 \\ (44) \end{gathered}$ | TP42.1606×42.1138×0.72 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 96.731 \\ 4 \end{gathered}$ | -45.21 |
| L45 | 14-9 (45) | $\begin{gathered} \text { TP43.0961×42.1606×0.71 } \\ 25 \end{gathered}$ | 5.00 | 0.00 | 0.0 | $\begin{gathered} 97.238 \\ 6 \end{gathered}$ | -47.38 |
| L46 | 9-4.25 (46) | TP43.9848×43.0961×0.71 25 | 4.75 | 0.00 | 0.0 | $\begin{gathered} 99.277 \\ 5 \end{gathered}$ | -49.47 |
| L47 | 4.25-4 (47) | TP44.0316x43.9848×0.6 | 0.25 | 0.00 | 0.0 | $\begin{gathered} 83.909 \\ 9 \end{gathered}$ | -49.58 |
| L48 | 4-0(48) | TP44.78×44.0316×0.6 | 4.00 | 0.00 | 0.0 | $\begin{gathered} 85.355 \\ 8 \end{gathered}$ | -51.19 |

## Pole Bending Design Data

| Section No. | Elevation ft | Size | $\begin{gathered} M_{u x} \\ \text { kip-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| L1 | 151-146 (1) | TP18.5255x17.59x0.2188 | 19.68 |
| L2 | 146-141 (2) | TP $19.461 \times 18.5255 \times 0.218$ 8 | 46.55 |
| L3 | 141-136 (3) | $\begin{gathered} \text { TP20.3965×19.461×0.218 } \\ 8 \end{gathered}$ | 97.62 |
| L4 | 136-131 (4) | $\begin{gathered} \text { TP21.3321×20.3965×0.21 } \\ 88 \end{gathered}$ | 154.72 |
| L5 | 131-126 (5) | $\begin{gathered} \text { TP22.2676×21.3321x0.21 } \\ 88 \end{gathered}$ | 225.05 |
| L6 | $\begin{gathered} 126-125.5 \\ \text { (6) } \end{gathered}$ | TP22.3611×22.2676×0.21 88 | 232.36 |
| L7 | $\begin{gathered} 125.5- \\ 125.25(7) \end{gathered}$ | TP22.4079×22.3611×0.36 26 | 236.03 |
| L8 | $\begin{gathered} 125.25- \\ 120.25(8) \end{gathered}$ | $\begin{gathered} \text { TP23.3434×22.4079×0.35 } \\ 63 \end{gathered}$ | 317.24 |
| L9 | $\begin{gathered} 120.25- \\ 118.5(9) \end{gathered}$ | $\begin{gathered} \text { TP23.6708×23.3434×0.35 } \\ 63 \end{gathered}$ | 347.65 |
| L10 | $\begin{gathered} 118.5- \\ 118.25(10) \end{gathered}$ | $\begin{gathered} \text { TP23.7176×23.6708×0.64 } \\ 38 \end{gathered}$ | 352.03 |
| L11 | $\begin{gathered} 118.25- \\ 117.5(11) \end{gathered}$ | $\begin{gathered} \text { TP23.8579×23.7176x0.64 } \\ 38 \end{gathered}$ | 365.22 |
| L12 | $\begin{gathered} 117.5- \\ 117.25(12) \end{gathered}$ | $\begin{gathered} \text { TP23.9047×23.8579×0.49 } \\ 38 \end{gathered}$ | 369.64 |
| L13 | $\begin{gathered} 117.25- \\ 112.25(13) \end{gathered}$ | $\begin{gathered} \text { TP24.8402x23.9047×0.48 } \\ 13 \end{gathered}$ | 459.72 |
| L14 | $\begin{gathered} 112.25- \\ 107.25(14) \end{gathered}$ | $\begin{gathered} \text { TP25.7757×24.8402x0.46 } \\ 88 \end{gathered}$ | 552.80 |
| L15 | $\begin{gathered} 107.25- \\ 102.25(15) \end{gathered}$ | TP26.7113 $\times 25.7757 \times 0.45$ 63 | 648.54 |
| L16 | $\begin{gathered} 102.25-97.5 \\ (16) \end{gathered}$ | TP27.6x26.7113x0.4563 | 674.52 |
| L. 17 | $\begin{gathered} 97.5-95.916 \\ (17) \end{gathered}$ | TP27.4588×26.5233×0.55 | 773.89 |
| L18 | $\begin{gathered} 95.916-92.5 \\ (18) \end{gathered}$ | TP28.098x27.4588×0.55 | 843.48 |
| L19 | $92.5-92.25$ (19) | TP28.1447x28.098x0.55 | 848.63 |
| L20 | $\begin{gathered} 92.25-87.25 \\ (20) \end{gathered}$ | $\begin{gathered} \text { TP29.0803×28.1447×0.53 } \\ 75 \end{gathered}$ | 953.05 |
| L21 | $\begin{gathered} 87.25-87 \\ (21) \end{gathered}$ | $\underset{5}{\mathrm{TP} 29.1271 \times 29.0803 \times 0.62}$ | 958.34 |

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| Section No. | Elevation ft | Size | $\begin{gathered} M u x \\ \text { kip-ft } \end{gathered}$ |
| :---: | :---: | :---: | :---: |
| L22 | 87-82 (22) | $\begin{gathered} \text { TP30.0626×29.1271x0.61 } \\ 25 \end{gathered}$ | 1065.79 |
| L23 | 82-77 (23) | TP30.9981×30.0626x0.6 | 1176.07 |
| L24 | 77-72 (24) | $\begin{gathered} \text { TP31.9337×30.9981×0.58 } \\ 75 \end{gathered}$ | 1289.08 |
| L25 | 72-67(25) | $\begin{gathered} \text { TP32.8692x31.9337x0.57 } \\ 5 \end{gathered}$ | 1404.81 |
| L26 | $\begin{gathered} 67-63.25 \\ (26) \end{gathered}$ | TP33.5709×32.8692×0.57 | 1493.43 |
| L27 | $\begin{gathered} 63.25-63 \\ (27) \end{gathered}$ | TP33.6176×33.5709×0.57 5 | 1499.40 |
| L28 | 63-58(28) | TP34.5532×33.6176x0.56 25 | 1620.15 |
| L29 | $\begin{gathered} 58-56.75 \\ (29) \end{gathered}$ | TP34.7871×34.5532×0.56 25 | 1650.77 |
| L30 | $\begin{gathered} 56.75-56.5 \\ (30) \end{gathered}$ | TP34.8338×34.7871×0.63 75 | 1656.92 |
| L31 | $\begin{gathered} 56.5-47.499 \\ (31) \end{gathered}$ | TP36.518×34.8338×0.637 5 | 1768.91 |
| L32 | $\begin{gathered} 47.499- \\ 46.999(32) \end{gathered}$ | TP35.9865x35.051x0.7 | 1897.10 |
| L33 | $\begin{gathered} 46.999- \\ 41.999(33) \end{gathered}$ | TP36.922×35.9865×0.687 5 | 2028.17 |
| L34 | $\begin{gathered} 41.999- \\ 36.999(34) \end{gathered}$ | TP37.8575x36.922x0.675 | 2161.81 |
| L35 | $\begin{gathered} 36.999- \\ 34.25(35) \end{gathered}$ | TP38.3718×37.8575×0.67 5 | 2236.43 |
| L36 | $\begin{gathered} 34.25-34 \\ (36) \end{gathered}$ | TP38.4186×38.3718×0.67 5 | 2243.25 |
| L37 | 34-29(37) | $\begin{gathered} \text { TP39.3541×38.4186x0.66 } \\ 25 \end{gathered}$ | 2381.14 |
| L38 | $\begin{gathered} 29-26.75 \\ (38) \end{gathered}$ | TP39.7751×39.3541×0.66 25 | 2444.04 |
| L39 | $\begin{gathered} 26.75-26.5 \\ (39) \end{gathered}$ | $\begin{gathered} \text { TP39.8219×39.7751×0.66 } \\ 25 \end{gathered}$ | 2451.07 |
| L40 | $\begin{gathered} 26.5-21.5 \\ (40) \end{gathered}$ | TP40.7574×39.8219x0.65 | 2592.81 |
| L41 | $\begin{gathered} 21.5-16.75 \\ (41) \end{gathered}$ | TP41.6461×40.7574×0.65 | 2730.09 |
| L42 | $\begin{gathered} 16.75-16.5 \\ (42) \end{gathered}$ | TP41.6929×41.6461×0.76 25 | 2737.38 |
| L43 | $\begin{gathered} 16.5-14.25 \\ (43) \end{gathered}$ | $\begin{gathered} \text { TP42.1138×41.6929×0.76 } \\ 25 \end{gathered}$ | 2803.30 |
| L44 | $\begin{gathered} 14.25-14 \\ (44) \end{gathered}$ | $\begin{gathered} \text { TP42.1606×42.1138×0.72 } \\ 5 \end{gathered}$ | 2810.66 |
| 145 | 14-9(45) | $\begin{gathered} \text { TP43.0961×42.1606x0.71 } \\ 25 \end{gathered}$ | 2959.05 |
| 146 | 9-4.25 (46) | TP43.9848×43.0961×0.71 25 | 3102.31 |
| L47 | 4.25-4 (47) | TP44.0316x43.9848×0.6 | 3109.91 |
| L48 | 4-0 (48) | TP44.78×44.0316x0.6 | 3232.29 |

## Pole Shear Design Data

| Section No. | Elevation ft | Size | Actual $V_{u}$ <br> $K$ | Actual $T_{s}$ kip-ft |
| :---: | :---: | :---: | :---: | :---: |
| L1 | 151-146 (1) | TP18.5255x17.59x0.2188 | 5.20 | 1.28 |
| L2 | 146-141 (2) | TP19.461×18.5255×0.218 8 | 5.56 | 1.28 |
| L3 | 141-136 (3) | TP20.3965×19.461×0.218 8 | 11.20 | 0.07 |
| L4 | 136-131 (4) | TP21.3321×20.3965×0.21 88 | 12.40 | 1.58 |
| L5 | 131-126 (5) | $\begin{gathered} \text { TP22.2676x21.3321×0.21 } \\ 88 \end{gathered}$ | 14.62 | 1.58 |
| L6 | $126-125.5$ <br> (6) | $\begin{gathered} \text { TP22.3611×22.2676×0.21 } \\ 88 \end{gathered}$ | 14.65 | 1.58 |

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| Section No. | Elevation $f t$ | Size | Actual $V_{u}$ <br> $K$ | Actual $T_{u}$ kip-ft |
| :---: | :---: | :---: | :---: | :---: |
| L7 | $\begin{gathered} 125.5- \\ 125.25(7) \end{gathered}$ | $\begin{gathered} \text { TP22.4079×22.3611×0.36 } \\ 26 \end{gathered}$ | 14.67 | 1.58 |
| L8 | $\begin{gathered} 125.25- \\ 120.25(8) \end{gathered}$ | TP23.3434×22.4079×0.35 63 | 17.26 | 1.58 |
| L9 | $\begin{gathered} 120.25- \\ 118.5(9) \end{gathered}$ | TP23.6708×23.3434×0.35 63 | 17.51 | 1.59 |
| L10 | $\begin{gathered} 118.5- \\ 118.25(10) \end{gathered}$ | TP23.7176×23.6708×0.64 38 | 17.53 | 1.59 |
| L11 | $\begin{gathered} 118.25- \\ 117.5(11) \end{gathered}$ | $\begin{gathered} \text { TP23.8579x23.7176x0.64 } \\ 38 \end{gathered}$ | 17.65 | 1.59 |
| L. 12 | $\begin{gathered} 117.5- \\ 117.25(12) \end{gathered}$ | $\begin{gathered} \text { TP23.9047×23.8579×0.49 } \\ 38 \end{gathered}$ | 17.68 | 1.59 |
| L13 | $\begin{gathered} 117.25- \\ 112.25(13) \end{gathered}$ | $\begin{gathered} \text { TP24.8402×23.9047×0.48 } \\ 13 \end{gathered}$ | 18.36 | 1.62 |
| L14 | $\begin{gathered} 112.25- \\ 107.25(14) \end{gathered}$ | TP25.7757×24.8402×0.46 88 | 18.89 | 1.61 |
| L15 | $\begin{gathered} 107.25- \\ 102.25(15) \end{gathered}$ | $\begin{gathered} \text { TP26.7113×25.7757×0.45 } \\ 63 \end{gathered}$ | 19.42 | 1.61 |
| L16 | $\begin{gathered} 102.25-97.5 \\ (16) \end{gathered}$ | TP27.6x26.7113×0.4563 | 19.56 | 1.61 |
| L17 | $\begin{gathered} 97.5-95.916 \\ (17) \end{gathered}$ | TP27.4588×26.5233x0.55 | 20.19 | 1.61 |
| L18 | $\begin{gathered} 95.916-92.5 \\ (18) \end{gathered}$ | TP28.098x27.4588×0.55 | 20.58 | 1.61 |
| L19 | $92.5-92.25$ <br> (19) | TP28.1447x28.098×0.55 | 20.60 | 1.61 |
| L20 | $\begin{gathered} 92.25-87.25 \\ (20) \end{gathered}$ | $\begin{gathered} \text { TP29.0803×28.1447×0.53 } \\ 75 \end{gathered}$ | 21.18 | 1.61 |
| L21 | $\begin{gathered} 87.25-87 \\ (21) \end{gathered}$ | TP29.1271 $\times 29.0803 \times 0.62$ 5 | 21.20 | 1.61 |
| L22 | 87-82 (22) | TP30.0626 $25.1271 \times 0.61$ 25 | 21.79 | 1.61 |
| L23 | 82-77 (23) | TP30.9981×30.0626x0.6 | 22.34 | 1.61 |
| L24 | 77-72 (24) | TP31.9337×30.9981×0.58 75 | 22.88 | 1.61 |
| L25 | 72-67(25) | TP32.8692×31.9337×0.57 5 | 23.43 | 1.61 |
| L26 | $\begin{gathered} 67-63.25 \\ (26) \end{gathered}$ | TP33.5709×32.8692x0.57 5 | 23.86 | 1.61 |
| L27 | $\begin{gathered} 63.25-63 \\ (27) \end{gathered}$ | TP33.6176×33.5709×0.57 5 | 23.88 | 1.61 |
| L28 | 63-58(28) | TP34.5532×33.6176×0.56 25 | 24.44 | 1.61 |
| L29 | $\begin{gathered} 58-56.75 \\ (29) \end{gathered}$ | TP34.7871×34.5532×0.56 25 | 24.58 | 1.61 |
| 130 | $\begin{gathered} 56.75-56.5 \\ (30) \end{gathered}$ | TP34.8338×34.7871×0.63 75 | 24.60 | 1.61 |
| L31 | $\begin{gathered} 56.5-47.499 \\ (31) \end{gathered}$ | TP $36.518 \times 34.8338 \times 0.637$ 5 | 25.32 | 1.60 |
| L32 | $\begin{gathered} 47.499- \\ 46.999(32) \end{gathered}$ | TP35.9865x35.051x0.7 | 25.97 | 1.60 |
| L33 | $\begin{gathered} 46.999- \\ 41.999(33) \end{gathered}$ | TP36.922×35.9865×0.687 5 | 26.48 | 1.60 |
| L34 | $\begin{gathered} 41.999- \\ 36.999(34) \end{gathered}$ | TP37.8575x36.922x0.675 | 27.01 | 1.60 |
| L35 | $\begin{gathered} 36.999- \\ 34.25(35) \end{gathered}$ | TP38.3718×37.8575×0.67 5 | 27.32 | 1.60 |
| L36 | $\begin{gathered} 34.25-34 \\ (36) \end{gathered}$ | TP38.4186×38.3718×0.67 5 | 27.33 | 1.60 |
| L37 | 34-29(37) | TP39.3541×38.4186×0.66 25 | 27.86 | 1.60 |
| L38 | $\begin{gathered} 29-26.75 \\ (38) \end{gathered}$ | TP39.7751×39.3541×0.66 25 | 28.09 | 1.60 |
| L39 | $\begin{gathered} 26.75-26.5 \\ (39) \end{gathered}$ | TP39.8219×39.7751x0.66 25 | 28.11 | 1.60 |
| L40 | $\begin{gathered} 26.5-21.5 \\ (40) \end{gathered}$ | TP40.7574×39.8219x0.65 | 28.62 | 1.60 |
| L41 | $\begin{gathered} 21.5-16.75 \\ (41) \end{gathered}$ | TP41.6461×40.7574×0.65 | 29.18 | 2.93 |


| Section No. | Elevation ft | Size | Actual $V_{u}$ <br> K | Actual $T_{u}$ kip-ft |
| :---: | :---: | :---: | :---: | :---: |
| L42 | $\begin{gathered} 16.75-16.5 \\ (42) \end{gathered}$ | $\begin{gathered} \text { TP41.6929×41.6461×0.76 } \\ 25 \end{gathered}$ | 29.19 | 2.93 |
| L43 | $\begin{gathered} 16.5-14.25 \\ (43) \end{gathered}$ | $\begin{gathered} \text { TP42.1138×41.6929×0.76 } \\ 25 \end{gathered}$ | 29.42 | 2.93 |
| L44 | $\begin{gathered} 14.25-14 \\ (44) \end{gathered}$ | TP42.1606×42.1138×0.72 5 | 29.44 | 2.93 |
| 145 | 14-9(45) | $\begin{gathered} \text { TP43.0961×42.1606x0.71 } \\ 25 \end{gathered}$ | 29.94 | 2.93 |
| L46 | 9-4.25 (46) | $\begin{gathered} \text { TP } 43.9848 \times 43.0961 \times 0.71 \\ 25 \end{gathered}$ | 30.41 | 2.93 |
| L47 | 4.25-4 (47) | TP44.0316x43.9848x0.6 | 30.42 | 2.93 |
| L48 | 4-0(48) | TP44.78x44.0316x0.6 | 30.80 | 2.93 |

## APPENDIX B

## BASE LEVEL DRAWING



## APPENDIX C

## ADDITIONAL CALCULATIONS


$0_{2}=$ an



TNX Geometry Input
Increment (f): 5

|  | Section | Height ( ft ) | Section Length ( ft ) | Lap Splice Length <br> ( ft ) | Number of Sides | Top Diameter (in) | Bottom Diameter (in) | Wall Thickness (in) | Tapered Pole Grade | Weight Multiplier |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 151 | - 146 | 5 |  | 12 | 17.590 | 18.526 | 0.2188 | A572-65 | 1.000 |
| 2 | 146 | - 141 | 5 |  | 12 | 18.526 | 19.461 | 0.2188 | A572-65 | 1.000 |
| 3 | 141 | - 136 | 5 |  | 12 | 19.461 | 20.397 | 0.2188 | A572-65 | 1.000 |
| 4 | 136 | - 131 | 5 |  | 12 | 20.397 | 21.332 | 0.2188 | A572-65 | 1.000 |
| 5 | 131 | - 126 | 5 | . | 12 | 21.332 | 22.268 | 0.2188 | A572-65 | 1.000 |
| 6 | 126 | - 125.5 | 0.5 |  | 12 | 22.268 | 22.361 | 0.2188 | A572-65 | 1.000 |
| 7 | 125.5 | - 125.25 | - 0.25 |  | 12 | 22.361 | 22.408 | 0.36255 | A572-65 | 0.948 |
| 8 | 125:25 | - 120.25 | 5 |  | 12 | 22.408 | 23.343 | 0.3563 | A572-65 | 0.950 |
| 9 | 120,25 | - 118.5 | 1.75 |  | 12 | 23.343 | 23.671 | 0.3563 | A572-65 | 0.946 |
| 10 | 118.5 | - 118.25 | 0.25 |  | 12 | 23.671 | 23.718 | 0.6438 | A572-65 | 0.906 |
| 11 | 118.25 | - 117.5 | 0.75 |  | 12 | 23.718 | 23.858 | 0.6438 | A572-65 | 0.903 |
| 12 | 117.5 | - 117.25 | 0.25 |  | 12 | 23.858 | 23.905 | 0.4938 | A572-65 | 0.933 |
| 13 | 117.25 | - 112.25 | 5 |  | 12 | 23.905 | 24.840 | 0.4813 | A572-65 | 0.937 |
| 14 | 112.25 | - 107.25 | 5 |  | 12 | 24.840 | 25.776 | 0.4688 | A572-65 | 0.943 |
| 15 | 107.25 | - 102.25 | 5 |  | 12 | 25.776 | 26.711 | 0.4563 | A572-65 | 0.951 |
| 16 | 102.25 | - 100.916 | 4.75 | 3.416 | 12 | 26.711 | 27.600 | 0.4563 | A572-65 | 0.947 |
| 17 | 100.916 | - 95.916 | 5 |  | 12 | 26.523 | 27.459 | 0.55 | A572-65 | 0.951 |
| 18 | 95.916 | - 92.5 | 3.416 |  | 12 | 27.459 | 28.098 | 0.55 | A572-65 | 0.943 |
| 19 | 92.5 | - 92.25 | 0.25 |  | 12 | 28.098 | 28.145 | 0.55 | A572-65 | 0.942 |
| 20 | 92.25 | - 87.25 | 5 |  | 12 | 28.145 | 29.080 | 0.5375 | A572-65 | 0.951 |
| 21 | 87.25 | - 87 | 0.25 |  | 12 | 29.080 | 29.127 | 0.625 | A572-65 | 0.931 |
| 22 | 87 | - 82 | 5 |  | 12 | 29.127 | 30.063 | 0.6125 | A572-65 | 0.936 |
| 23 | 82 | - 77 | 5 |  | 12 | 30.063 | 30.998 | 0.6 | A572-65 | 0.941 |
| 24 | 77 | - 72 | 5 |  | 12 | 30.998 | 31.934 | 0.5875 | AS72-65 | 0.948 |
| 25 | 72 | - 67 | 5 |  | 12 | 31.934 | 32.869 | 0.575 | A572-65 | 0.956 |
| 26 | 67 | - 63.25 | 3.75 |  | 12 | 32.869 | 33.571 | 0.575 | A572-65 | 0.947 |
| 27 | 63.25 | - 63 | 0.25 |  | 12 | 33.571 | 33.618 | 0.575 | A572-65 | 0.947 |
| 28 | 63 | - 58 | 5 |  | 12 | 33.618 | 34.553 | 0.5625 | A572-65 | 0.956 |
| 29 | 58 | - 56.75 | 1.25 |  | 12 | 34.553 | 34.787 | 0.5625 | A572-65 | 0.953 |
| 30. | 56.75 | - 56.5 | 0.25 |  | 12 | 34.787 | 34.834 | 0.6375 | A572-65 | 0.950 |
| 31 | 56.5 | - 51.999 | 9.001 | 4.5 | 12 | 34.834 | 36.518 | 0.6375 | A572-65 | 0.939 |
| 32 | 51.999 | - 46.999 | 5 |  | 12 | 35.051 | 35.987 | 0.7 | A572-65 | 0.942 |
| 33 | 46.999 | - 41.999 | 5 |  | 12 | 35.987 | 36.922 | 0.6875 | A572-65 | 0.948 |
| 34 | 41.999 | - 36.999 | 5 |  | 12 | 36.922 | 37.858 | 0.675 | A572-65 | 0.955 |
| 35 | 36.999 | - 34.25 | 2.749 |  | 12 | 37.858 | 38.372 | 0.675 | A572-65 | 0.950 |
| 36 | 34.25 | - 34 | 0.25 |  | 12 | 38.372 | 38.419 | 0.675 | A572-65 | 0.949 |
| 37 | 34 | - 29 | 5 |  | 12 | 38.419 | 39.354 | 0.6525 | A572-65 | 0.957 |
| 38 | 29 | - 26.75 | 2.25 |  | 12 | 39.354 | 39.775 | 0.6625 | A572-65 | 0.953 |
| 39 | 26.75 | - 26.5 | 0.25 |  | 12 | 39.775 | 39.822 | 0.6625 | A572-65 | 0.952 |
| 40 | 26.5 | - 21.5 | 5 |  | 12 | 39.822 | 40.757 | 0.65 | A572-65 | 0.961 |
| 41 | 21.5 | - 16.75 | 4.75 |  | 12 | 40.757 | 41.646 | 0.65 | A572-65 | 0.953 |
| 42 | 16.75 | - 16.5 | 0.25 |  | 12 | 41.646 | 41.693 | 0.7625 | A572-65 | $1: 026$ |
| 43. | 16.5 | - 14.25 | 2.25 |  | 12 | 41.693 | 42.114 | 0.7625 | A572-65 | 1.020 |
| 44 | 14.25 | - 14 | 0.25 |  | 12 | 42.114 | 42.161 | 0.725 | A572-65 | 0.962 |
| 45 | 14 | - 9 | 5 |  | 12 | 42.161 | 43.096 | 0.7125 | A572-65 | 0.968 |
| 46 | 9 | - 4.25 | 4.75 |  | 12 | 43.096 | 43.985 | 0.7125 | A572-65 | 0.959 |
| 47 | 4.25 | - 4 | 0.25 |  | 12 | 43.985 | 44.032 | 0.6 | A572-65 | 1.001 |
| 48 | 4 | - 0 | 4 |  | 12 | 44.032 | 44.780 | 0.6 | A572-65 | 0.995 |

## TNX Section Forces

| Increment (ft): |  |  | 5 | TNX Output |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Section Height (ft) |  |  | $\mathrm{P}_{\mathrm{u}} \quad$ (K) | $M_{u x} \text { (kip- }$ <br> ft) | $\begin{aligned} & V_{u} \\ & (K) \end{aligned}$ |
| 1 | 151-146 |  |  | 3.02 | 19.68 | 5.20 |
| 2 | 146 - |  | - 141 | 3.33 | 46.56 | 5.56 |
| 3 | $141-136$ |  |  | 6.93 | 97.62 | 11.20 |
| 4 | 136 - |  | 131 | 7.89 | 154.77 | 12.34 |
| 5 | 131 - |  | 126 | 10.11 | 225.05 | 14.62 |
| 6 | 126 - |  | - 125 | 10.16 | 232.36 | 14.65 |
| 7 | 125.5 - |  | - 125 | 10.20 | 236.03 | 14.67 |
| 8 | 125.25 - |  | 120.25 | 12.41 | 317.24 | 17.26 |
| 9 | 120.25 - |  | 118.5 | 12.66 | 347.65 | 17.51 |
| 10 | 118.5 - |  | 118.25 | 12.72 | 352.03 | 17.53 |
| 11 | 118.25 - |  | - 117 | 12.88 | 365.22 | 17.65 |
| 12 | 117.5 - |  | - 117.2 | 12.92 | 369.64 | 17.68 |
| 13 | 117.25 - 112.25 |  |  | 13.82 | 459.72 | 18.36 |
| 14 | 112.25 - 107.25 |  |  | 14.76 | 552.80 | 18.89 |
| 15 | 107.25 - 102.25 |  |  | 15.72 | 648.54 | 19.42 |
| 16 | 102.25 - 100.916 |  |  | 15.98 | 674.52 | 19.56 |
| 17 | 100.916 - 95.916 |  |  | 17.60 | 773.89 | 20.19 |
| 18 | 95.916 - 92.5 |  |  | 18.40 | 843.49 | 20.58 |
| 19 | 92.5-92.2 |  |  | 18.46 | 848.63 | 20.60 |
| 20 | $92.25-87.25$ |  |  | 19.63 | 953.05 | 21.18 |
| 21 | 87.25 |  |  | 19.71 | 958.34 | 21.20 |
| 22. | $87-82$ |  |  | 21.03 | 1065.79 | 21.79 |
| 23 | 82 |  |  | 22.38 | 1176.07 | 22.34 |
| 24 | $77-72$ |  |  | 23.76 | 1289.07 | 22.88 |
| 25 | $72-67$ |  |  | 25.16 | 1404.81 | 23.43 |
| 26 | $67-63.25$ |  |  | 26.23 | 1493.44 | 23.86 |
| 27 | $63.25-63$ |  |  | 26.31 | 1499.40 | 23.88 |
| 28 | $63-58$ |  |  | 27.75 | 1620.15 | 24.44 |
| 29 | $58-56.75$ |  |  | 28.11 | 1650.77 | 24.58 |
| 30 | $56.75-56.5$ |  |  | 28.21 | 1656.91 | 24.60 |
| 31 | 56.5 - 51.999 |  |  | 29.64 | 1768.90 | 25.32 |
| 32 | $51.999-46.999$ |  |  | 32.63 | 1897.10 | 25.97 |
| 33 | 46.999 - 41.999 |  |  | 34.42 | 2028.16 | 26.48 |
| 34 | 41.999 - 36.999 |  |  | 36.24 | 2161.81 | 27.01 |
| 35 | 36.999 - 34.25 |  |  | 37.25 | 2236.42 | 27.32 |
| 36 | 34.25 |  |  | 37.36 | 2243.25 | 27.33 |
| 37 | 34-29 |  |  | 39.22 | 2381.15 | 27.86 |
| 38 | $29-26.7$ |  |  | 40.07 | 2444.04 | 28.09 |
| 39 | $26.75-26.5$ |  |  | 40.17 | 2451.06 | 28.11 |
| 40 | $26.5-21.5$ |  |  | 42.07 | 2592.81 | 28.62 |
| 41. | $21.5-16.75$ |  |  | 43.90 | 2730.09 | 29.18 |
| 42 | $16.75-16.5$ |  |  | 44.03 | 2737.39 | 29.19 |
| 43 | $16.5-14.25$ |  |  | 45.09 | 2803.30 | 29.42 |
| 44 | $14.25-14$ |  |  | 45.21 | 2810.66 | 29.44 |
| 45 | $14-9$ |  |  | 47.38 | 2959.05 | 29.94 |
| 46 | 9-4.25 |  |  | 49.47 | 3102.30 | 30.41 |
| 47 | 4.25 - | - | 4 | 49.58 | 3109.91 | 30.42 |
| 48 | $4-0$ |  |  | 51.19 | 3232.30 | 30.80 |

## Analysis Results

| Elevation (ft) | Component Type | Size | Critical Element | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: |
| 151-146 | Pole | TP18.526x17.59x0.2188 | Pole | 5.6\% | Pass |
| 146-141 | Pole | TP19.461×18.526x0.2188 | Pole | 11.9\% | Pass |
| 141-136 | Pole | TP20.397×19.461×0.2188 | Pole | 23.1\% | Pass |
| 136-131 | Pole | TP21.332 $20.397 \times 0.2188$ | Pole | 33.7\% | Pass |
| 131-126 | Pole | TP22.268×21.332 0.2188 | Pole | 45.6\% | Pass |
| 126-125.5 | Pole | TP22.361×22.268×0.2188 | Pole | 46.7\% | Pass |
| 125.5-125.25 | Pole + Reinf. | TP22.408×22.361×0.3626 | Reinf. 11 Tension Rupture | 40.8\% | Pass |
| 125.25-120.25 | Pole + Reinf. | TP23.343×22.408x0.3563 | Reinf. 11 Tension Rupture | 51.2\% | Pass |
| 120.25-118.5 | Pole + Reinf. | TP23.671×23.343×0.3563 | Reinf. 11 Tension Rupture | 54.8\% | Pass |
| 118.5-118.25 | Pole + Reinf. | TP23.718×23.671×0.6438 | Reinf. 9 Bolt-Shaft Bearing | 33.5\% | Pass |
| 118.25-117.5 | Pole + Reinf. | TP23.858×23.718×0.6438 | Reinf. 9 Tension Rupture | 33.7\% | Pass |
| 117.5-117.25 | Pole + Reinf. | TP23.905 $23.858 \times 0.4938$ | Reinf. 9 Tension Rupture | 42.9\% | Pass |
| 117.25-112.25 | Pole + Reinf. | TP24.84×23.905 0.4813 | Reinf. 9 Tension Rupture | 50.4\% | Pass |
| 112.25-107.25 | Pole + Reinf. | TP25.776x24.84×0.4688 | Reinf. 9 Tension Rupture | 57.4\% | Pass |
| 107.25-102.25 | Pole + Reinf. | TP26.711×25.776x0.4563 | Reinf. 9 Tension Rupture | 63.8\% | Pass |
| 102.25-100.92 | Pole + Reinf. | TP27.6×26.711×0.4563 | Reinf. 9 Tension Rupture | 65.4\% | Pass |
| 100.92-95.92 | Pole + Reinf. | TP27.459x26.523×0.55 | Reinf. 9 Tension Rupture | 60.5\% | Pass |
| 95.92-92.5 | Pole + Reinf. | TP28.098 $27.459 \times 0.55$ | Reinf. 9 Tension Rupture | 63.6\% | Pass |
| 92.5-92.25 | Pole + Reinf. | TP28.145 $28.098 \times 0.55$ | Reinf. 8 Tension Rupture | 63.8\% | Pass |
| 92.25-87.25 | Pole + Reinf. | TP29.08×28.145×0.5375 | Reinf. 8 Tension Rupture | 67.9\% | Pass |
| 87.25-87 | Pole + Reinf. | TP29.127×29.08×0.625 | Reinf. 7 Tension Rupture | 58.4\% | Pass |
| 87-82 | Pole + Reinf. | TP30.063×29.127×0.6125 | Reinf. 7 Tension Rupture | 61.9\% | Pass |
| 82-77 | Pole + Reinf. | TP30.998×30.063x0.6 | Reinf. 7 Tension Rupture | 65.2\% | Pass |
| 77-72 | Pole + Reinf. | TP31.934×30.998×0.5875 | Reinf. 7 Tension Rupture | 68.2\% | Pass |
| 72-67 | Pole + Reinf. | TP32.869×31.934×0.575 | Reinf. 7 Tension Rupture | 71.1\% | Pass |
| 67-63.25 | Pole + Reinf. | TP33.571×32.869x0.575 | Reinf. 7 Tension Rupture | 73.1\% | Pass |
| 63.25-63 | Pole + Reinf. | TP33.618×33.571×0.575 | Reinf. 6 Tension Rupture | 73.3\% | Pass |
| 63-58 | Pole + Reinf. | TP34.553×33.618×0.5625 | Reinf. 6 Tension Rupture | 75.8\% | Pass |
| 58-56.75 | Pole + Reinf. | TP34.787×34.553×0.5625 | Reinf. 6 Tension Rupture | 76.4\% | Pass |
| 56.75-56.5 | Pole + Reinf. | TP34.834×34.787×0.6375 | Reinf. 5 Bolt Shear | 66.4\% | Pass |
| 56.5-52 | Pole + Reinf. | TP36.518×34.834×0.6375 | Reinf. 5 Compression | 66.1\% | Pass |
| 52-47 | Pole + Reinf. | TP35.987×35.051×0.7 | Reinf. 5 Compression | 63.6\% | Pass |
| 47-42 | Pole + Reinf. | TP36.922x35.987×0.6875 | Reinf. 5 Compression | 65.4\% | Pass |
| 42-37 | Pole + Reinf. | TP37.858×36.922×0.675 | Reinf. 5 Compression | 67.0\% | Pass |
| 37-34.25 | Pole + Reinf. | TP38.372×37.858×0.675 | Reinf. 5 Bolt Shear | 70.3\% | Pass |
| 34.25-34 | Pole + Reinf. | TP38.419×38.372×0.675 | Reinf. 4 Bolt Shear | 70.4\% | Pass |
| 34-29 | Pole + Reinf. | TP39.354×38.419x0.6625 | Reinf. 4 Compression | 69.4\% | Pass |
| 29-26.75 | Pole + Reinf. | TP39.775 $39.354 \times 0.6625$ | Reinf. 4 Boit Shear | 72.6\% | Pass |
| 26.75-26.5 | Pole + Reinf. | TP39.822x39.775×0.6625 | Reinf. 1 Bolt Shear | 72.7\% | Pass |
| 26.5-21.5 | Pole + Reinf. | TP40.757×39.822x0.65 | Reinf. 1 Compression | 71.5\% | Pass |
| 21.5-16.75 | Pole + Reinf. | TP41.646x40.757×0.65 | Reinf. 1 Compression | 72.8\% | Pass |
| 16.75-16.5 | Pole + Reinf. | TP41.693x41.646x0.7625 | Reinf. 2 Compression | 66.9\% | Pass |
| 16.5-14.25 | Pole + Reinf. | TP42.114×41.693×0.7625 | Reinf. 2 Compression | 67.5\% | Pass |
| 14.25-14 | Pole + Reinf. | TP $42.161 \times 42.114 \times 0.725$ | Reinf. 2 Compression | 67.9\% | Pass |
| 14-9 | Pole + Reinf. | TP43.096x42.161×0.7125 | Reinf. 2 Compression | 69.1\% | Pass |
| 9-4.25 | Pole + Reinf. | TP43.985×43.096x0.7125 | Reinf. 2 Bolt Shear | 72.7\% | Pass |
| 4.25-4 | Pole + Reinf. | TP44.032 $43.985 \times 0.6$ | Reinf. 10 Connection | 74.0\% | Pass |
| 4-0 | Pole + Reinf. | TP44.78×44.032 $\times 0.6$ | Reinf. 10 Connection | 74.8\% | Pass |
|  |  |  |  | Summary |  |
|  |  |  | Pole | 64.6\% | Pass |
|  |  |  | Reinforcement | 76.4\% | Pass |
|  |  |  | Overall | 76.4\% | Pass |

## Additional Calculations

|  | Moment of Inertia $\left(\mathbf{l n}{ }^{4}\right)$ |  |  | Area ( $\mathrm{in}^{2}$ ) |  |  | \% Capacity* |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Pole | Reinf. | Total | Pole | Reint. | Total | Pole | R1 | R2 | R3 | R4 | R5 | R6 | R7 | 89 | Rg | R10 | R11 |
| 151-145 | 552 | n/a | 552 | 12.88 | $\mathrm{n} / \mathrm{a}$ | 12.88 | 5.6\% |  |  |  |  |  |  |  |  |  |  |  |
| 146-141 | 642 | n/a | 642 | 13.54 | n/a | 13.54 | 11.9\% |  |  |  |  |  |  |  |  |  |  |  |
| 141-135 | 740 | n/a | 740 | 14.20 | n/a | 14.20 | 23.1\% |  |  |  |  |  |  |  |  |  |  |  |
| 136-131 | 848 | n/a | 848 | 14.95 | n/a | 14.85 | 33.7\% |  |  |  |  |  |  |  |  |  |  |  |
| 131-126 | 965 | n/a | 965 | 15.51 | n/a | 15.51 | 45.6\% |  |  |  |  |  |  |  |  |  |  |  |
| 125-125.5 | 978 | n/a | 978 | 15.58 | n/a | 15.58 | 46.7\% |  |  |  |  |  |  |  |  |  |  |  |
| 125.5-125.25. | 984 | 612 | 1596 | 15,61 | 8.76 | 24.37 | 28.3\% |  |  | . |  |  |  |  |  | , |  | 40.8\% |
| 125.25-120.25 | 1114 | 661 | 1775 | 16.27 | 8.76 | 25,03 | 36.1\% |  |  |  |  |  |  |  |  |  |  | 51.2\% |
| 120.25-118.5 | 1161 | 679 | 1840 | 16.50 | 8.76 | 25.26 | 38.9\% |  |  |  |  |  |  |  |  | . |  | 54.8\% |
| 118.5-118.25 | 1168 | 2084 | 3252 | 16.53 | 26.76 | 43.29 | 22.4\% |  |  |  |  |  |  |  |  | 33.5\% |  | 31.5\% |
| 118.25-117.5 | 1190 | 2107 | 3297 | 16.63 | 26.75 | 43.39 | 23.1\% |  |  | . |  |  |  |  |  | 33.7\% |  | 32.4\% |
| 117.5-117.25 | 1197 | 1423 | 2620 | 16.66 | 18.00 | 34.66 | 29.5\% |  |  |  |  |  |  |  |  | 42.9\% |  |  |
| 117.25-112.25 | 1344 | 1530 | 2874 | 17.32 | 18.00 | 35.32 | 35.2\% |  |  |  |  |  |  |  |  | 50.4\% |  |  |
| 112.25-107.25 | 1503 | 1641 | 3144 | 17.98 | 18.00 | 35.98 | 40.8\% |  |  |  |  |  |  |  |  | 57.4\% |  |  |
| 107.25-102.25 | 1674 | 1756 | 3430 | 18.54 | 18.00 | 36.64 | 46.2\% |  |  |  |  |  |  |  |  | 63.8\% |  |  |
| 102.25-100.92 | 1722 | 1787 | 3509 | 18.81 | 18.00 | 36.91 | 47.7\% |  |  |  |  |  |  |  |  | 65.4\% |  |  |
| 100.92-95.92 | 2573 | 1850. | 4423 | 27.28 | 18.00 | 45.28 | 38,5\% |  |  |  |  |  |  |  |  | 60.5\% |  |  |
| 95.92-92.5 | 2759 | 1933 | 4692 | 27.92 | 18.00 | 45.92 | 40.8\% |  |  |  |  |  |  |  |  | 63.6\% |  |  |
| 92.5-92.25 | 2773 | 1939. | 4712 | 27.97 | 18.00 | 45.97 | 40.9\% |  |  |  |  |  |  |  | 63.8\% |  |  |  |
| 92.25-87.25 | 3052 | 2064 | 5126 | 28.91 | 18.00 | 46.91 | 44.1\% |  |  |  |  |  |  |  | 67,9\% |  |  |  |
| $87.25 \cdot 87$ | 3077 | 2856 | 5933 | 28.95 | 24.38 | 53.33 | 38.4\% |  |  |  |  |  |  | 58.4\% |  |  |  |  |
| 87-82 | 3386 | 3032 | 6418 | 29.89 | 24.38 | 54.27 | 41.2\% |  |  |  |  |  |  | 61.9\% |  |  |  |  |
| 82-77 | 3716 | 3213 | 6929 | 30.83 | 24.38 | 55.21 | 43.9\% |  |  |  |  |  |  | 65.2\% |  |  |  |  |
| 77-72 | 4065 | 3400 | 7466 | 31.77 | 24.38 | 56.15 | 48.6\% |  |  |  |  |  |  | 68.2\% |  |  |  |  |
| $72 \cdot 67$ | 4438 | 3591 | 8030 | 32.71 | 24.38 | 57.09. | 49.1\% |  |  |  |  |  |  | 71.1\% |  |  |  |  |
| 67-63.25 | 4731 | 3739 | 8470 | 33.42 | 24.38 | 57.79 | 51.0\% |  |  |  |  |  |  | 73.1\% |  |  |  |  |
| 63.25-63 | 4751 | 3749 | 8500 | 33.47 | 24.38 | 57.84 | 51.1\% |  |  |  |  |  | 73.3\% |  |  |  |  |  |
| 63-58 | 51.63 | 3950 | 9113 | 34.41 | 24.38 | 58.78 | 53.6\% |  |  |  |  |  | 75.8\% |  |  |  |  |  |
| 58.56.75 | 5270 | 4001 | 9271 | 34.54 | 24.38 | 59.02 | 54.2\% |  |  |  |  |  | 76.4\% |  |  |  |  |  |
| 56.75-56.5 | 5291 | 5286 | 10577 | 34.69 | 31.88 | 66.56 | 47.8\% |  |  |  |  | 66.4\% |  |  |  |  |  |  |
| 56.5-52 | 5688 | 5531 | 11219 | 35.53 | 31.88 . | 67.41 | 49.8\% |  |  |  |  | 66.1\% |  |  |  |  |  |  |
| 52-47 | 6970 | 5623 | 12593 | 42.94 | 31.88 | 74.81 | 44.7\% |  |  |  |  | 63.6\% |  |  |  |  |  |  |
| 47-42 | 7534 | 5904 | 13438 | 44.07 | 31.88 | 75.94 | 46.4\% | . |  |  |  | 65.4\% |  |  |  |  |  |  |
| 42-37 | 8127 | 6192 | 14319 | 45.20 | 31.88 | 77.07 | 48.1\% |  |  |  |  | 67.0\% |  |  |  |  |  |  |
| 37-34.25 | 8456 | 6353 . | 14820 | 45.82 | 31.88 | 77.69 | 49.0\% |  |  |  |  | 70.3\% |  |  |  |  |  |  |
| 34.25-34 | 8498 | 636B | 14856 | 45.87 | 31.88 | 77.75 | 49.0\% |  |  |  | 70.4\% |  |  |  |  |  |  |  |
| 34-29 | 9140 | 6667 | 15807 | 47.00 | 31.88 | 78.87 | 50.6\% |  |  |  | 69.4\% |  |  |  |  |  |  |  |
| 29-26.75 | 9440 | 6804 | 16244 | 47.51 | 31.88 | 79.38 | 51.3\% |  |  |  | 72.6\% |  |  |  |  |  |  |  |
| 26.75-26.5 | 9473 | 6819 | 16292 | 47.56 | 31.88 | 79.44 | 51.4\% | 72.7\% | 72.7\% |  |  |  |  |  |  |  |  |  |
| 26.5-21.5 | 10163 | 7129 | 17292 | 48.69 | 31.88 | 80.57 | 53.0\% | 71.5\% | 71.5\% |  |  |  |  |  |  |  |  |  |
| 21.5-16.75 | 10849 | 7430 | 18279 | 49.76 | 31.88 | 81.64 | 54.4\% | 72.8\% | 72.8\% |  |  |  |  |  |  |  |  |  |
| 16.75-16.5 | 11070 | 10638 | 21707 | 49.82 | 53.13 | 102.94 | 50.2\% | 45.5\% | 66.9\% | 51.6\% |  |  |  |  |  |  |  |  |
| 16.5-14.25 | 11409 | 10846 | 22255 | 50.33 | 53.13 | 103.45 | 50.8\% | 47,6\% | 67.5\% | 50.3\% |  |  |  |  |  |  |  |  |
| 14.25-14 | 11315 | 9986 | 21301 | 50.38 | 42.50 | 92.88 | 52.3\% |  | 67.9\% | 60.8\% |  |  |  |  |  |  |  |  |
| 14-9 | 12090 | 10417 | 22507 | 51.51 | 42.50 | 94.01 | 53.9\% |  | 69.1\% | 61.9\% |  |  |  |  |  |  |  |  |
| 9-4.25 | 12859 | 10835 | 23694 | 52.58 | 42.50 | 95.08 | 55.2\% |  | 72.7\% | 65.2\% |  |  |  |  |  |  |  |  |
| 4.25-4 | 12848 | 7526 | 20374 | 52.64 . | 31.25 | 83.89 | 63.3\% |  |  |  |  |  |  |  |  |  | 74.0\% |  |
| 4-0 | $135 z 0$ | 7767 | 21287 | 53.54 | 31.25 | 84.79 | 64.6\% |  |  |  |  |  |  |  |  |  | 74.8\% |  |

Rating per TAA-222-H Section 15.5.

| Site Info |  |
| ---: | :---: |
|  | BU \# |
| Site Name | 841295 |
| Order\# |  |


| Analysis Considerations |  |
| ---: | :---: |
| TIA-222 Revision | H |
| Grout Considered: | No |
| $\mathrm{l}_{\text {ar }}$ (in) | 0 |


| Applied Loads |  |
| ---: | :---: |
| Moment (kip-ft) | 3232.30 |
| Axial Force (kips) | 51.19 |
| Shear Force (kips) | 30.80 |
| ${ }^{*}$ TIA-222-H Section 15.5 Applied |  |



## Connection Properties

## Analysis Results

## Anchor Rod Data

GROUP 1: (12) 2-1/4" $\varnothing$ bolts (A615-75 $\mathrm{N} ; \mathrm{Fy}=75 \mathrm{ksi}$, Fu=100 ksi) on $52.75^{\prime \prime} \mathrm{BC}$ GROUP 2: (6) $2-1 / 4^{\prime \prime} \varnothing$ bolts (Williams $\mathrm{N} ; \mathrm{Fy}=120 \mathrm{ksi}$, Fu=125 ksi) on $52.75^{*} \mathrm{BC}$

## Base Plate Data

$58.75^{\prime \prime}$ OD x $3^{\prime \prime}$ Plate (A572-50; Fy=50 ksi, Fu=65 ksi)

Stiffener Data
N/A

Pole Data
$44.78^{\prime \prime} \times 0.375^{\prime \prime} 12$-sided pole (A572-65; Fy=65 ksi, Fu=80 ksi)
Anchor Rod Summary GROUP 1:

| $P_{U_{\_} c=154.73}$ | $\phi P n_{\_}=243.75$ | Stress Rating |
| :--- | :--- | :---: |
| $V u_{=2.57}$ | $\phi V n=73.13$ | $60.6 \%$ |
| $\mathrm{Mu}=\mathrm{n} / \mathrm{a}$ | $\phi \mathrm{Mn}=\mathrm{n} / \mathrm{a}$ | Pass |

GROUP 2:

| $P u_{-} c=188.89$ | $\phi P n_{-} c=489.6$ | Stress Rating |
| :--- | :--- | :---: |
| $V u_{=0}$ | $\phi V n=146.88$ | $36.7 \%$ |
| $M u=n / a$ | $\phi M n=n / a$ | Pass |


| Base Plate Summary |  |  |
| :--- | :--- | :---: |
| Max Stress \{ksi): | 26.72 | (Flexural) |
| Allowable Stress \{ksi): | 45 |  |
| Stress Rating: | $56.6 \%$ | Pass |

## Pier and Pad Foundation

BU \# : 841295
Site Name: Bethany App. Number: $\qquad$

| Top \& Bot. Pad Rein. Different?: | $\Gamma$ |
| ---: | :---: |
| Block Foundation?: | $\Gamma$ |


| Superstructure Analysis |  | Reactions |
| ---: | :---: | :--- |
| Compression, $\mathrm{P}_{\text {comp }}:$ | 51.19 | kips |
| Base Shear, Vu_comp: | 30.8 | kips |
|  |  |  |
|  |  |  |
| Moment, $\mathrm{M}_{\mathrm{u}}:$ | 3232.3 | ft -kips |
| Tower Height, $\mathrm{H}:$ | 150 | ft |
|  |  |  |
| BP Dist. Above Fdn, $\mathrm{bp}_{\text {dist: }}$ | 3.75 | in |


| Pier Properties |  |  |
| ---: | :---: | :--- |
| Pier Shape: | Square |  |
| Pier Diameter, dpier: | 6 | ft |
| Ext. Above Grade, E: | 0.4 | ft |
| Pier Rebar Size, Sc: | 10 |  |
| Pier Rebar Quantity, mc: | 40 |  |
| Pier Tie/Spiral Size, St: | 4 |  |
| Pier Tie/Spiral Quantity, mt: |  |  |
| Pier Reinforcement Type: | Tie |  |
| Pier Clear Cover, cc $\mathrm{cp}_{\text {pler: }}$ | 2.5 | in |


| Foundation Analysis Checks |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | Capacity | Demand | Rating* | Check |
|  |  |  |  |  |
| Lateral (Sliding) (kips) | 482.94 | 30.80 | 6.1\% | Pass |
| Bearing Pressure (ksf) | 22.50 | 1.84 | 7.8\% | Pass |
| Overtuming (kip*ti) | 10947.31 | 3534.53 | 32.3\% | Pass |
| Pier Flexure (Comp.) (kip*ti) | 6585.19 | 3263.10 | 47.2\% | Pass |
|  |  |  |  |  |
| Pier Compression (kip) | 22913.28 | 57.67 | 0.2\% | Pass |
| Pad Flexure (kip*tit) | 7614.39 | 1351.62 | 16.9\% | Pass |
| Pad Shear - 1-way (kips) | 3225.07 | 81.25 | 2.4\% | Pass |
| Pad Shear - 2-way (Comp) (ksi) | 0.190 | 0.005 | 2.4\% | Pass |
| Flexural 2-way (Comp) (kip ${ }^{\text {fif) }}$ | 15228.77 | 1957.86 | 12.2\% | Pass |

*Rating per TIA-222-H Section 15.5


| Pad Properties |  |  |
| ---: | :---: | :--- |
| Depth, D: | 9.1 | ft |
| Pad Width, W: | 29 | ft |
| Pad Thickness, T: | 8.5 | ft |
| Pad Rebar Size (Bottom), Sp: | 7 |  |
| Pad Rebar Quantity (Bottom), mp: | 29 |  |
| Pad Clear Cover, $\mathrm{cc}_{\text {pad }}$ | 3 | in |


| Material Properties |  |  |
| ---: | :---: | :---: |
| Rebar Grade, Fy: | 60 | ksi |
| Concrete Compressive Strength, F'c: | 4 | ksi |
| Dry Concrete Density, $\delta \mathrm{c}:$ | 150 | pcf |


| Soil Properties |  |  |
| ---: | :---: | :--- |
| Total Soil Unit Weight, $\gamma:$ | 110 | pcf |
| Ultimate Gross Bearing, Qult: | 30.000 | ksf |
| Cohesion, Cu: | 0.000 | ksf |
| Friction Angle, $\varphi:$ | 30 | degrees |
| SPT Blow Count, $\mathrm{N}_{\text {blows: }}$ | 69 |  |
| Base Friction, $\mu:$ | 0.5 |  |
| Neglected Depth, N: | 3.30 | ft |
| Foundation Bearing on Rock? | No |  |
| Groundwater Depth, gw: | 3.3 | ft |

<--Toggle between Gross and Net Address:
No Address at This Location

ASCE 7 Hazards Report

| Standard: | ASCE/SEI 7-10 | Elevation: |
| :--- | :--- | :--- |
| Risk Category: | II | ft (NAVD 88) |
| Soil Class: | D - Stiff Soil | Latitude: |



## Wind

Results:

Wind Speed:
10-year MRI
25-year MRI
50-year MRI
100-year MRI
Data Source:

122 Vmph
76 Vmph
86 Vmph
93 Vmph
99 Vmph
ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1-CC-4, incorporating errata of March 12, 2014

Wed Jun 052019

Date Accessed:
Value provided is 3 -second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a $7 \%$ probability of exceedance in 50 years (annual exceedance probability $=$ $0.00143, \mathrm{MRI}=700$ years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

## Results:

Ice Thickness: $\quad 0.75 \mathrm{in}$.
Concurrent Temperature: 15 F
Gust Speed: $\quad 50 \mathrm{mph}$
Data Source:
Date Accessed:
Standard ASCE/SEI 7-10, Figs. 10-2 through 10-8
Wed Jun 052019

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3 -second gust speeds, for a 50 -year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

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## $1 \times \sqrt{4}-1$

## BETHANY N(



DO NOT SCALE DRAWINGS
CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE LESSEE/LICENSEE REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

## CONSULTANT TEAM

| APPLICANT: | VERIZON WIRELESS 20 ALEXANDER DRIVE WALLINGFORD, CT 06492 CONTACT: JAMES O'DONNELL |
| :---: | :---: |
| APPLICANT'S CONTACT: | JAMES O'DONNELL <br> (413) 575-2626 |
| ARCHITECT: | JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE <br> 5TH FLOOR <br> BOSTON, MA 02116 |
| STRUCTURAL ENGINEĖR: | JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE 5TH FLOOR BOSTON, MA 02116 |
| ELECTRICAL ENGINEER: | JACOBS ENGINEERING GROUP, INC. 120 SAINT JAMES AVENUE 5TH FLOOR BOSTON, MA 02116 |

## PROJECT SUMMARY

VERIZON SITE NAME:
BETHANY NORTH C
CROWN CASTLE SITE NAME: BETHANY
TOWER OWNER:

COORDINATES:

APPLICANT:
 120 SAINT JAMES AVENUE

JACOBS ENGINEERING GROUP, INC. 5TH FLOOR
BOSTON, MA 02116





# Kimley»Horn 

421 FAYETTEVILLE STREET, SUITE 600
RALEIGH, NC 27601
PHONE: 919-677-2000
WWW.KIMLEY-HORN.COM

## MOUNT MODIF DRAWIN

## BETHANY

CROWN CASTLE BU\#: 8
VERIZON SITE\#: 1042

## STRUCTURE INFORN <br> 150' MONOPOLE TOW LOW PROFILE PLATF

## SITE ADDRES

719 AMITY ROAD BETHANY, CT 0652،
NEW HAVEN COUNT LATITUDE: N $41^{\circ} 26{ }^{\prime} 33$ LONGITUDE: W 72º 59' 3


### 1.00 GENERAL NOTES

1.01 ALL MATERIALS AND WORKMANSHIP SHALL CONFORM TO THE DRAWINGS AND SPECIFICATIONS. ALL WORK SHALL BE DONE IN ACCORDANCE WTH THE LATEST EDITION OF THE STATE, LOCAL AND NATIONAL CODES, ORDINANCES AND OR REGULATIONS APPLICABLE TO THIS PROJECT.
1.02 THE CONTRACTOR SHALL BE RESPONSIBLE FOR COORDINATING WITH WORK OF ALL TRADES AND SHALL CHECK ALL DIMENSIONS. ALL DISCREPANCIES SHALL BE CALLED TO THE ATTENTION OF THE PROJECT MANAGER AND/OR ENGINEER AND BE RESOLVED BEFORE PROCEEDING WITH WORK WHERE THERE IS A CONFLICT BETWEEN DRAWING AND SPECIFICATIONS.
1.03 ALL INFORMATION SHOWN ON THE DRAWNGS RELATIVE TO EXISTING CONDITIONS IS GIVEN AS THE BEST PRESENT KNOWLEDGE, BUT WTHOUT GUARANTEE OF ACCURACY. WHERE ACTUAL CONDITIONS CONFLICT WTH THE DRAWINGS, THEY SHALL BE REPORTED TO THE PROJECT MANAGER AND/OR ENGINEER OF RECORD SO THAT PROPER REVISIONS MAY BE MADE. MODIFICATION OF DETAILS OR CONSTRUCTION SHALL NOT BE MADE WITHOUT WRITTEN APPROVAL OF THE PROJECT MANAGER AND/OR ENGINEER OF RECORD.
1.04 CONTRACTOR SHALL REVIEW AND BE FAMILIAR WITH SITE CONDITIONS AS SHOWN ON THE ATTACHED SITE PLAN AND/OR SURVEY DRAWINGS.
1.05 CONTRACTOR TO PROVIDE DUMPSTER AND PORTABLE TOILET FACILITY DURING CONSTRUCTION.
1.06 CONSTRUCTION WASTE MAY NEITHER BE BURNED NOR BURIED AND MUST BE TAKEN TO AN APPROVED LANDFILL.
1.07 SECuRITY TO THE SITE SHALL BE MAINTAINED AT ALL TIMES.

### 2.00 STRUCTURAL STEEL NOTES

2.01 STRUCTURAL STEEL SHALL COMPLY WTH THE FOLLOWNG SPECIFICATIONS UNO:
A. STRUCTURAL STEEL SHAPES, PLATES AND BARS.
(EXPECT W-SHAPES) - ASTM A36, Fy= 36 KSI
B. PIPE - ASTM A53, GRADE B, Fy $=35 \mathrm{KSI}$.
C. HSS-SHAPES - ATSM A500, GRADE B,
$F_{y}=42 \mathrm{KSI}$ (ROUND)
$F y=46 \mathrm{KSI}$ (RECTANGLE)
D. ANCHOR RODS - ASTM F1554, GRADE 55
E. ALL THREAD RODS - ASTM F1554, GRADE 105
F. STRUCTURAL BOLTS $1 / 2$ " $\varnothing$ AND LARGER - ASTM A325
G. STRUCTURAL BOLTS SMALLER THAN $1 / 2 \eta$ DIMENSIONS:
ASME B18.2.1
MATERIAL SAE J429 GRADE 5
THREADING: ASME B1.1, UNC, CLASS 2A
FINISH: HOT-DIP GALVANIZED OR ZINC-PLATED
H. NUTS FOR BOLTS/ALL-THREAD - ASTM A563 (THREADING TO MATCH BOLT)
I. WASHERS FOR BOLTS/ALL THREADS - ASTM F436
J. $W$ \& WT SHAPES - ASTM A36 - Fy- 36 KSI.

ALTERNATE SPEC: ASTM (IF OTHER SPEC IS UNAVAILABLE).
2.02 STRUCTURAL BOLTS SHALL CONFORM TO THIS NOTE. ALL BOLT HOLES SHALL BE STANDARD SIZE BOLT HOLES PER AISC 360 , UNLESS OTHERWSE NOTED. ALL HOLES SHALL BE SHOP DRILLED OR SUB-PUNCHED AND REAMED. BURNING OF HOLES IS NOT PERMITTED, WHERE SLOTTED OR OVERSIZE HOLES ARE SPECIFIED ON THE DRAWINGS, EXTRA-THICK ASTM F436 PLATE WASHERS SHALL BE USED ( $5 / 16$ " MINIMUM THICKNESS) WTH A DIAMETER SUITABLE TO COVER THE EXTENTS OF THE SLOT OF HOLE. BOLTS SHALL BE HEAVY-HEX WHERE AVAILABLE IN THE SIZE AND GRADE SPECIFIED.
2.03 ALL STEEL HARDWARE, INCLUDING ADHESIVE OR EMBEDDED ANCHOR BOLTS AND THEIR ACCESSORIES, SHALL BE HOT-DIP GALVANIZED IN ACCORDANCE WTH ASTM A153 (EXCEPT BOLTS SMALL THAN $1 / 2^{\prime \prime}$ SHALL CONFIRM TO FE/ZN 3 AS PER ASTM F1941 WHERE HOT-DIP GALVANIZED IN ACCORDANCE WITH ASTM A123. REPAIR DAMAGE TO GALVANIZED COATINGS USING ASTM A7BO PROCEDURES WTH A ZINC RICH PAINT (SUCH AS ZRC GALVILITE) FOR GALVANIZING DAMAGED BY HANDLING, TRANSPORTING, CUTTING, WELDING, OR BOLTING. DO NOT HEAT SURFACES TO WHICH REPAIR PAINT HAS BEEN APPLIED. CALL OUT HOLES REQUIRED FOR HOT-DIP GALVANIZING ON SHOP DRAWINGS.
2.04 WELDING SHALL BE IN ACCORDANCE WITH AWS D1.1 "STRUCTURAL WELDING CODE - STEEL". WELD ELECTRODES SHALL BE E8OXX. UNLESS OTHERWISE NOTED PROVIDE CONTINUOUS FILLET WELDS WITH MINIMUM SIZE OF $3 / 1^{\prime \prime}$ OR OF A SIZE EQUAL TO THE THICKNESS OF THE THINNER WELD LEG SIZE SHALL BE ADJUSTED AS REQUIRED TO MAINTAIN THE EFFECTIVE THROAT OF A $3 / 16^{\prime \prime}$ FHLLET WELD IN A $90^{\circ}$ JOINT. ALL WELD SIZES SHOWN IN INCHES. PRIOR TO WELDING, THE CONTRACTOR SHALL SUBMIT CERTFICATION FOR EACH WELDER STATING THE TYPE OF WELDING AND POSITIONS QUALIFIED FOR, THE CODE AND PROCEDURE QUALIFIED UNDER, STATE QUALIFIED, AND THE FIRM AND INDIVIDUAL CERTIFYNG THE QUALIFICATION TESTS. THIS INFORMATION SHALL BE SUBMIT TO THE MODIFICATION INSPECTOR (SEE SHEET $N-3$ ) AS WELL AS ANY THIRD-PARTY CERTIFIED WELD INSPECTOR (CW).
2.06 MEMBERS SHALL BE SHOP-FABRICATED AND WELDED TO THE EXTENT PRACTICABLE IN ORDER TO REDUCE FIELD INSTALLATION COSTS.
3.00 MODIFICATION NOTES
3.01 THESE MODIFICATIONS HAVE BEEN DESIGNED IN ACCORDANCE WTH GOVERNING PROVISIONS OF TIA/EIA-222, ASCE 7. AWS, ACI, AND, MATERIALS AND SERVICES PROVIDED BY THE CONTRACTOR SHALL ( TO THE ABOVE MENTIONED CODES AND CONTRACT SPECIFICATIONS. 3.02 ALL MATERIALS UTILIZED FOR THIS PROJECT MUST BE NEW AND FF ANY DEFECTS.
3.03 ALL PRODUCT OR MATERIAL SUBSTITUTIONS PROPOSED BY THE

CONTRACTOR SHALL BE APPROVED IN WRITING BY THE ENGINEER C RECORD. CONTRACTOR SHALL PROVIDE DOCUMENTATION TO ENGINEI SUITABLE TO DETERMINE IF THE SUBSTITUTE IS ACCEPTABLE FOR L MEETS THE ORIGINAL DESIGN CRITERIA. DIFFERENCES FROM THE OR DESIGN, INCLUDING; MAINTENANCE, REPAIR, AND REPLACEMENT, SH NOTED. ESTIMATES OF COSTS/CREDITS ASSOCIATED WITH THE SUBS (INCLUDING RE-DESIGN COSTS AND COSTS TO SUB-CONTRACTORS) BE PROVIDED TO THE ENGINEER. CONTRACTOR SHALL PROVIDE ADD DOCUMENTATION AND/OR SPECIFICATION TO THE ENGINEER AS REQ
3.04 PROVIDE STRUCTURAL STEEL SHOP DRAWINGS(S) TO THE ENGINEER RECORD FOR APPROVAL PRIOR TO FABRICATION.
3.05 UNLESS NOTED OTHERWSE, ALL NEW MEMBERS AND REINFORCING : MAINTAIN THE EXISTING MEMBER WORK AND NOT INTRODUCE ECCENTRICITIES INTO THE STRUCTURE.
3.06 ANY CONTRACTOR-CAUSED DAMAGE TO PROPERTY OF THE LAND C PROPERTY OF THE CUSTOMER, SITE FENCING OR GATES, ANY AND UTILITY AND/OR SERVICE LINES, SHOWN OR NOT SHOWN ON THE $P$ SHALL BE REPAIRED OR REPLACED AT THE SOLE COST OF THE CONTRACTOR AND SHALL BE ADDRESSED BY THE CONTRACTOR WIT COMPANIES THAT OWN THE DAMAGED ITEMS.
4.00 CONTRACTOR NOTES
4.01 PRIOR TO BEGINNING CONSTRUCTION, ALL CONTRACTORS AND SUBCONTRACTORS MUST ACKNOWLEDGE IN WRITING TO STRUCTURE O THAT THEY HAVE OBTAINED, UNDERSTAND, AND WILL FOLLOW STRUC OWNER STANDARDS OF PRACTICE, CONSTRUCTION GUIDELINES, ALL S! STRUCTURE SAFETY PROCEDURES, ALL PRODUCT LIMITATIONS AND INSTALLATION PROCEDURES USED ON SITE, AND PROPOSED MODIFICA OESCRIBED RECEIPT OF ACKNOWLEDGEMENT MUST OCCUR PRIOR TO BEGINNING CONSTRUCTION OF CLIMBING. IT IS THE RESPONSIBILITY Of GENERAL CONTRACTOR TO PROVIDE THE DOCUMENTATION FOR STRUC OWNER ON COMPANY LETTERHEAD AND THE RESPONSIBILITY OF THE GENERAL CONTRACTOR TO OBTAIN THIS DOCUMENTATION FROM ANY SUBCONTRACTORS (ON SUBCONTRACTOR LETTERHEAD) AND DELIVER THE STRUCTURE OWNER.
4.02 IF THE CONTRACTOR DISCOVERS ANY EXISTING CONDITIONS THAT AR REPRESENTED ON THESE DRAWINGS, OR ANY CONDITIONS THAT WOUI INTERFERE WITH THE INSTALLATION OF THE MODIFICATIONS, THE ENG RECORD SHALL BE CONTACTED IMMEDIATELY TO EVALUATE THE SIGN OF THE DEVATION.
4.03 THE CONTRACTOR SHALL SOLICIT AND HIRE THE SERVICES OF A QUA MODIFICATIONS INSPECTOR PRIOR TO BEGINNING CONSTRUCTION, THE MODIFICATION INSPECTOR MAY BE AN EMPLOYEE OF THE CONTRACTC HOWEVER, THE INSPECTOR'S ONLY DUTIES SHALL BE INSPECTION, TE: AND REPORT CREATION AS REQUIRED ON THE "MODIFICATION INSPEC NOTES" SHEET. IT IS ALSO ACCEPTABLE FOR THE CONTRACTOR TO SUBCONTRACT THE MODIFICATION INSPECTOR DUTIES TO A THIRD PA MEETING THE ABOVE REQUIREMENTS.
4.04 THE CONTRACTOR SHALL NOTIFY THE ENGINEER OF RECORD AND TO OWNER OF THE PLANNED CONSTRUCTION \& INSPECTION SCHEDULE, $t$ AS ANY CHANGES TO THE SCHEDULE, WITHIN TWO BUSINESS DAYS C COMPLETION OF THE SCHEDULE REVISION BOTH PRIOR TO BEGINNING CONSTRUCTION AND DURING CONSTRUCTION AS THE SCHEDULE CHAA THE CONTRACTOR SHALL NOTFY THE ENGINEER OF RECORD WHEN PI OF CONSTRUCTION HAVE BEEN MOVED UP AND SHALL GIVE THE ENG ADEQUATE NOTICE SO THE ENGINEER OF RECORD MAY, AT THEIR DIS
INSPECT PORTIONS OF THE WORK DEEMED CRITICAL TO THE INTEGRIT INSPECT PORTIONS OF THE WORK DEEMED CRITICAL TO THE INTEGRIT
THE STRUCTURE. FALLURE TO PROVDE THIS NOTICE MAY RESULT IN REJECTION OF THE CONTRACTOR'S WORK. THE CONTRACTOR SHALL $A$ NOTIFY THE ENGINEER OF RECORD AND THE STRUCTURE OWNER WHE WORK HAS BEEN COMPLETED WITHIN 2 BUSINESS DAYS OF THE COM OF THE WORK AND ASSOCIATED MODIFICATION INSPECTIONS \& TESTII TOWER/BUILDING CONSTRUCTION EXPERIENCE. THIS INCLUDES PROVID NECESSARY CERTFICATIONS TO THE STRUCTURE OWNER AND ENGINE INCLUDING BUT NOT LIMITED TO QUALIFIED WELDER CERTIFICATES, CE WELDING INSPECTOR CREDENTIALS, ET CETERA.

> THESE DRAWNGS DO NOT INDICATE THE METHOD OF CONSTRUCTION, CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL SOLELY RESPONSLLE SUER ALI CONSTRUCTON METHODS, MEANS, TECHNIQUES, SEQUENCES AND PROCEDURES.
07 CONTRACTOR SHALL WORK WITHIN THE LIMITS OF THE STRUCTURE O' PROPERTY OF LEASE AREA AND APPROVED EASEMENT. IT IS THE RESPONSIBILITY OF THE CONTRACTOR TO VERIFY WORK IS WTHIN TH BOLUNDARIES. CONTRACTOR SHALL EMPLOY A SURVEYOR AS REQUIRE WORK OUTSIDE THESE BOUNDARIES SHALL BE APPROVED IN WRITING LAND OWNER PRIOR TO MOBILIZATION. CONSTRUCTION STAKING AND BOUNDARY MARKING IS THE RESPONSIBILITY OF THE CONTRACTOR.
4.08 DO NOT SCALE DRAWINGS. CONTRACTOR SHALL VERIFY ALL PLANS, DIMENSIONS, CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY THE ARCHITECT OR ENGINEER IN WRITING OF ANY DISCREPANCIES BE PROCEEDING WTH THE WORK OR BE RESPONSIBLE FOR THE SAME.

### 1.00 GENERAL INSPECTION NOTES

1.01 THE POST-MODIFICATION INSPECTION IS A VISUAL EXAMINATION OF STRUCTURE MODIFICATIONS AND A REVEW OF ANY REQUIRED CONSTRUCTION INSPECTIONS, TESTING, AND OTHER DATA TO VERITY THAT THE MODIFICATIONS ARE INSTALLED IN ACCORDANCE WTH THE CONTRACT DOCUMENTS AS DESIGNED BY THE ENGINEER OF RECORD. THE CONTRACTOR DOCUMENTS INCLUDE THESE MODIFICATION DRAWINGS, ANY PROJECT SPECIFICATION REFERENCED TO IN THE PROJECT NOTES OR OTHERWISE PROVIDED WTH THE DRAWNGS, AND OTHER DOCUMENTS OR DRAWINGS PROVIDED WITH THE MODIFICATION DRAWINGS WTH THE INTENT THEY BE USED AS A DESIGN AID OR GUIDELINE FOR CONSTRUCTION.
1.02 THE POST-MODIFICATION INSPECTION SHALL CONFIRM INSTALLATION CONFIGURATION AND WORKMANSHIP ONLY AND IS NOT A QUALITATIVE REVIEW OF THE ENGINEERING ASPECTS OF THE DESIGN OR THE DESIGN DRAWINGS. THE MODIFICATION INSPECTOR IS NOT TAKING OWNERSHIP OF THE MODIFICATION DESIGN IN THE PERFORMANCE OF THEIR DUTEES. OWNERSHIP OF THE MODIFICATION DESIGN'S EFFECTIVENESS AND INTENT, AS WELL AS ALL ASSOCIATED RISK, LIED WTH THE ENGINEER OF RECORD AT ALL TIMES.
1.03 TO ENSURE THE REQUIREMENTS OF THE POST-MODIFICATION INSPECTION ARE MET, IT IS ESSENTIAL COORDINATION BETWEEN THE PRIME CONTRACTOR AND THE MODIFICATION INSPECTOR BEING AS SOON AS THE PROJECT IS FUNDED AND WORK ENTERS THE PLANNING STAGE. THE PRIME CONTRACTOR AND MODIFICATION INSPECTOR SHALL BE PROACTIVE IN IDENTIFYNG CONSTRUCTION ISSUES AND COMMUNICATE THESE ISSUES TO EACH OTHER AND THE ENGINEER OF RECORD AND STRUCTURE OWNER \& CUSTOMER, AS REQUIRED.
2.00 INSPECTION \& REPORT RECOM'S
2.01 THE FOLLOWNG ARE PROVIDED WITH THE INTENT OF ENHANCING THE EFFECTIVENESS OF THE MODIFICATION INSPECTIONS AND IMPROVING THE EFFICIENCY OF THE PROCESS OF COLLECTING AND COMPILING THE INFORMATION NTO A USEABLE REPORT:
2.01.1 IT IS RECOMMENDED THE PRIME CONTRACTOR

PROVIDE THE MODIFICATION INSPECTOR AT LEAST 5 BUSINESS DAYS NOTICE FOR WHEN THE SITE WLL BE READY FOR THE MODIFICATION INSPECTION.
2.01.2 THE PRIME CONTRACTOR AND THE MODIFICATION INSPECTOR SHALL COORDINATE CLOSELY THROUGHOUT THE ENTIRE PROJECT.
2.01.3 THE PRIME CONTRACTOR AND MODIFICATION INSPECTION SHALL BOTH BE PRESENT DURING THE INITIAL INSPECTIONS IN ORDER TO ALLOW FOR THE REMEDIATION OF DEFICIENCIES DURING THE INSPECTIONS, AS PRACTICABLE. IT MAY BE PREFERABLE TO KEEP WORK CREWS AND THEIR EQUIPMENT ON-SITE TO REMEDIATE DEFICIENCIES DURING INSPECTIONS.
3.00 INSPECTION RESCHEDULE \& CANCEL
3.01 IF THE PRIME CONTRACTOR AND MODIFICATION INSPECTOR HAVE AGREED UPON A TIME AND DATE FOR A GIVEN INSPECTION AND EITHER PARTY RESCHEDULES OR CANCELS THE INSPECTION, THE STRUCTURE OWNER SHALL NOT BE RESPONSIBLE FOR COSTS, FEES, LOST DEPOSITS, OR OTHER EXPENSES INCURRED BY THE PRIME CONTRACTOR, THEIR SUBCONTRACTOR(S), OR THE MODIFICATION INSPECTOR DUE TO THESE SCHEDULING CHANGES. EXCEPTIONS MAY BE MADE IN THE EVENT OF UNCONTROLLABLE SITUATIONS SUCH AS NATURAL DISASTERS, SEVERE WEATHER, OR OTHER CONDITIONS THAT COMPROMISE THE SAFETY OF THE PARTIES INVOLVED.
4.00 REMEDIATION OF FAILING INSPECTION
4.01 IN THE EVENT ANY PORTION OF THE MODIFICATION WORK IS DETERMINED TO BE UNSATISFACTORY BY THE MODIFICATION INSPECTOR, THE PRIME CONTRACTOR SHALL WORK WITH THE MODIFICATION INSPECTOR TO CREATE A PLAN OF ACTION THAT WILL EITHER:
4.01.1 REPAIR THE DEFICIENT WORK TO SATISFACTORY CONDITION AND INCLUDE A SUBSEQUENT RE-INSPECTION OF THE WORK TO VERIFY IT IS SATISFACTORY.
4.01.2 OR, WITH THE PERMISSION OF THE STRUCTURE OWNER AND/OR CUSTOMER, THE PRIME CONTRACTOR MAY WORK WTH THE ENGINEER OF RECORD TO REVIEW THE AS-BUILT CONDITION OF THE MODIFICATION TO DETERMINE IF IT IS STRUCTURALLY ACCEPTABLE, IF THE ACTION US NOT ACCEPTABLE TO ANY PARTY, THE PRIME CONTRACTOR SHALL PROCEED TO REPAIR THE DEFICIENT WORK TO A SATISFACTORY CONDITION.
5.00 OWNER INSPECTIONS
5.01 THE STRUCTURE OWNER MAY CONDUCT INSPECTIONS TO VERIFY THE QUALITY AND COMPLETENESS OF THE PREVIOUSLY COMPLETED MODIFICATION INSPECTIONS REPORTS OR THE MODIFICATION INSTALLATION WORK.
5.02 INSPECTIONS MAY BE COMPLETED BY A 3RD-PARTY FIRM OF THE STRUCTURE OWNER'S CHOOSING AFTER A MODIFICATION PROJECT IS COMPLETED AND A PASSING MODIFICATION INSPECTION REPORT IS ISSUED.
6.00 MOD INSPECTOR'S RESPONSIBILITIE: 6.01 THE MODIFICATION INSPECTOR SHALL CONTACT THE F AS THE HAVE RECEIVED A PURCHASE ORDER OR PA THE MODIFICATION INSPECTOR SHALL REVIEW THE RE INSPECTION CHECKLIST, SHALL WORK WITH THE PRIME SCHEDULE OF NECESSARY ON-SITE INSPECTIONS, AN SITE-SPECIFIC INSPECTION REQUIREMENTS OF OTHER
6.02 THE MODIFICATION INSPECTOR IS RESPONSIBLE FOR ( CONTRACTOR INSPECTION AND TEST REPORTS (INCLU SUB-CONTRACTORS), SHALL REVEW THE REPORTS F( CONTRACT DOCUMENTS, SHALL CONDUCT THE NECES: AND SHALL COMPILE AND SUBMIT THE MODIFICATION
7.00 PRIME CONTRACTOR RESPONSIBILIT 7.01 THE PRIME CONTRACTOR SHALL CONTACT THE MODIFI AS THEY HAVE RECEIVED A PURCHASE ORDER OR P) MODIFICATION INSTALLATION. THE PRIME CONTRACTOR REQUIREMENTS OF THE MODIFICATION INSPECTION CH THE MODIFICATION INSPECTOR TO DEVELOP A SCHEDI INSPECTIONS, AND SHALL DISCUSS SPECIFIC INSPECTI REQUIREMENTS WTH THE MODIFICATION INSPECTOR IN UNDERSTANDING OF THE REQUIRED INSPECTION AND
7.02 THE PRIME CONTRACTOR SHALL PERFORM AND RECOI INSPECTION RESULTS IN ACCORDANCE WTH THE REQ MODIFICATION INSPECTION CHECKLIST.
8.00 PHOTOGRAPHY REQUIREMENTS
8.01 THE PRIME CONTRACTOR AND MODIFICATION INSPECT EFFORTS OF BOTH PARTIES AND THEIR EMPLOYED PE PHOTOGRAPHS WITH THE INSPECTION REPORT TO INC A GENERAL SITE PHOTOGRAPHS PRE-CONSTRUCTION B MODIFICATION INSTALLATION PHOTOGRAPHS DURING CONSTRUCTOON/ERECTION OPERATIONS AND INSPECTI B. 1 RAW MATERIALS
B. 2 PHOTOS OF DETAILED WORK REQUIRED ON THE DRAWINGS (CONNECTIONS, WELDMENTS, FIELD/FABRICATED MEMBERS, ETC.)
B. 3 WELD PREPARATION AND COMPLETED WELD INSPECTION (INCLUDING A FILLET WELD SIZE G, B. 4 BOLT INSTALLATION AND TORQUE/PRETENSION.
B. 5 FINAL INSTALLED CONDITION (AFTER DEFICIENT CONDITIONS, IF ANY, ARE REMEDIATED).
B. 6 REPAIR OF SURFACE COATINGS (INCLUDING GALVANIZING AND/OR PAINT COATNG).
C. POST-MODIFICATON PHOTOGRAPHS OF THE SITE d D. PHOTOGRAPHS OF THE FINAL STATE OF THE SITE WORK BY THE PRIME CONTRACTOR, ASSOCIATED SI THE MODIFICATION INSPECTOR.
E. OTHER PHOTOS MAY BE INCLUDED AT PRIME CONINSPECTOR'S DISCRETION.

NOTE: PHOTOS OF MODIFICATIONS INSTALLED ON THE STR ELEVATION OF $20^{\circ}$ SHALL REQUIRE PHOTOS TAKE FRt WELL AS OVERALL PHOTOGRAPHS OF THE MODIFICATT GROUND.

INSTALL SITE PRO 1 HRK12-3HD 4'-0"土 ABOVE THE EXISTING PIPE FACE HORIZONTAL ATTACH THE INCLUDED P2.0 STD. $\times 6^{\circ}-0^{\prime \prime}$ AT THIRD POINTS ON THE PROPOSED HANDRALL.
SEE: $1 / \mathrm{s}-2$

INSTALL SITE PRO 1 HSRK-35 TO THE TUBE OFFSET ARMS 6 " $\pm$ OUT FROM THE EXISTING COLLAR. ATTACH KICKER ANGLES PERPENDICULAR TO THE PROPOSED SITE PRO 1 HRK12-3HD.
SEE: 2/S-2


INSTALL SITE PF TUBE OFFSET A EXISTING COLLA PERPENDICULAR PRO 1 HRK 12SEE: $2 / \mathrm{S}-2$

INSTALL SITE PRO 1 HSRK-35 TO THE TUBE OFFSET ARMS 6 " $\pm$ OUT FROM THE EXISTING COLLAR. ATACH KICKER ANGLES PERPENDICULAR TO THE PROPOSED SITE PRO 1 HRK12-3HD.
SEE: 2/S-2



[^0]:    tnxTower Report - version 8.0.5.0

[^1]:    $\operatorname{tnx}$ Tower Report - version 8.0.5.0

[^2]:    tnxTower Report - version 8.0.5.0

