



New Cingular Wireless PCS, LLC 500 Enterprise Drive Rocky Hill, Connecticut 06067-3900

Phone: (860) 513-7636 Fax: (860) 513-7190

+ 49 6

EM-CING-006-051007

October 7, 2005

Ms. Pamela Katz, Chairman, and Members of the Council Connecticut Siting Council 10 Franklin Square New Britain, Connecticut 06051 OCT 07 2005
SITING COUNCIL

Re: Request by New Cingular Wireless PCS, LLC for an Order Approving Shared Use of an Approved Municipal Tower off Lopus Road, Beacon Falls

Dear Chairman Katz and Members of the Council:

Pursuant to Connecticut General Statutes (C.G.S.) Section 16-50aa, New Cingular Wireless PCS, LLC ("Cingular") hereby requests an order from the Connecticut Siting Council ("Council") for the proposed shared use by Cingular of an approved municipal tower to be located at the Beacon Falls Public Works Department garage, Lopus Road, Beacon Falls. A copy of this letter is being sent to the 1<sup>st</sup> Selectman of the Town of Beacon Falls.

#### **Approved Municipal Tower**

Under a lease agreement dated 10/23/03, AT&T Wireless agreed to construct a communications tower for the Town of Beacon Falls on the Town-owned Lopus Road site. Upon completion of construction, title to the tower would automatically transfer to the Town, and the Town would assume all responsibilities and liabilities of ownership. Thereafter, AT&T as tenant would pay rent to the Town as landlord. As a result of the merger between AT&T Wireless and Cingular, however, Cingular has assumed the role of tenant under this agreement.

In March of 2004, site plans for the tower project were comprehensively reviewed and approved by the Town of Beacon Falls Planning & Zoning Commission ("P&Z"). A copy of the P&Z's March 18, 2004 minutes are attached along with its letter to the Board of Selectmen recommending acceptance of the plans. Subsequent to the Cingular-AT&T merger, P&Z discussed the minor changes to the plans incident to converting it from an AT&T design to a Cingular design, i.e., a shelter in lieu of an equipment pad, and determined that its earlier approval would embrace either design.

The tower itself will consist of a 150 foot monopole with Town antennas at the top, and the lower levels of the tower reserved for wireless carrier use. The tower will be at the center of a 42 ft x 45 ft equipment compound surrounded by an 8-foot high chain link fence. The tower will be located adjacent to the Lopus Road Public Works garage at approximate coordinates of N 41° 26′ 00″ and W 73° 04′ 13″ (NAD 83).

#### Proposed Shared Use of the Municipal Tower

Cingular operates under licenses issued by the Federal Communications Commission ("FCC") to provide cellular and PCS mobile telephone service in New Haven County, which includes the area to be served by Cingular's proposed installation. Attached to this request are a site location map, a site plan, the tower profile, and tower design drawings. Cingular proposes to install up to twelve Powerwave 7770 dual band panel antennas, or their equivalent, approximately 55 inches in height at a centerline height of 145 feet above ground level. Cingular also proposes to place an 11½ ft x 20 ft prefabricated concrete equipment shelter at the base of the tower.

#### The Lopus Road Tower is not a Facility for purposes of Council Jurisdiction

The Town of Beacon Falls will own and operate the Lopus Road tower which is needed for emergency communications in the community. The Town owns the underlying land as well. As such, the approved tower is not a "facility" as that term is defined in Section 16-50i of the Connecticut General Statues, but rather a "municipal" tower which will continue to remain under the jurisdiction of the Town.

Given that the Lopus Road tower is an uncertificated facility for purposes of the Siting Council, Cingular respectfully requests an order pursuant to Section 16-50aa of the Connecticut General Statutes approving its shared use of the approved tower for the reasons more fully set forth below:

- A. <u>Technical Feasibility.</u> The approved tower will be structurally sound and capable of supporting the proposed shared use of the Cingular antennas at 145 feet AGL. The proposed shared use of this tower is therefore technically feasible.
- B. <u>Legal Feasibility</u>. Under C.G.S §16-50aa, the Council has been authorized to issue an order approving the proposed shared use of a tower facility such as the facility to be located at Lopus Road (C.G.S §16-50aa(c) (1)). Under the authority vested in the Council by C.G.S §16-50aa, an order approving the shared use of the Town's tower would satisfy Cingular's Siting Council obligations and permit it to obtain a building permit for the proposed installation.
- C. <u>Environmental Feasibility.</u> The proposed shared use of this tower facility would have a minimal environmental effect for the following reasons:
  - 1. The proposed installation would have an insignificant incremental visual impact

and would not cause any significant change or alteration in the physical or environmental characteristics of the property. The addition of the proposed antennas would not increase the height of the monopole tower. Cingular's equipment will be housed in an equipment shelter, and all construction will occur in the approved compound.

- 2. The proposed installation would not increase noise levels at the existing facility by six decibels or more.
- 3. Operation of the additional antennas will not increase the total radio frequency electromagnetic radiation power density, measured at the tower base, to or above the standard adopted by the State of Connecticut and the FCC. The "worst-case" exposure calculation in accordance with FCC OET Bulletin No. 65 (1997) for a point of interest at the base of the tower is as follows:

| Сотрату                | Centerline<br>Height<br>(feet) | Frequency (MHz)        | Number<br>of<br>Channels | Power Per<br>Channel<br>(Watts) | Power Density <sup>†</sup> (mW/cm <sup>2</sup> ) | Standard<br>Limits<br>(mW/cm²) | Percent<br>of<br>Limit |
|------------------------|--------------------------------|------------------------|--------------------------|---------------------------------|--------------------------------------------------|--------------------------------|------------------------|
| Town of Beacon Falls * | 155                            |                        |                          |                                 |                                                  |                                |                        |
| Cingular               | 145                            | 880-894                | 6                        | 296                             | 0.0304                                           | 0.5867                         | 5.18                   |
| Cingular               | 145                            | 1930-1935<br>1965-1970 | 3                        | 427                             | 0.0219                                           | 1.0000                         | 2.19                   |
| Total                  |                                |                        |                          |                                 |                                                  |                                | 7.37%                  |

<sup>\*</sup> Information provided by the Town of Beacon Falls.

As the table demonstrates, the "worst-case" exposure due to the Cingular transmissions would be approximately 7.4 % of the ANSI/IEEE standard, as calculated for mixed frequency sites. Cumulative power density levels resulting from Cingular's proposed use of the tower facility would thus be well within applicable ANSI/IEEE standards.

- 4. The proposed installation would not require any water or sanitary facilities, or generate air emissions or discharges to water bodies. After construction is completed (approximately four weeks), the proposed installation would not generate any vehicular traffic other than periodic maintenance visits. The proposed use of the facility would therefore have a minimal environmental effect, and is environmentally feasible.
- D. <u>Economic Feasibility.</u> Cingular has entered into an agreement with the Town of Beacon Falls to share use of the tower. The proposed facility sharing is therefore economically feasible.
- E. Public Safety Concerns. As stated above, the approved tower will be structurally

Please note that the standard power density equation provided by the Council in its memo of January 22, 2001 incorporates a ground reflection factor of 2.56 (i.e., the square of 1.6) as described in FCC OET Bulletin No. 65.

capable of supporting Cingular's proposed antennas, and radio frequency emissions fall well below State and Federal safety standards. Cingular is not aware of any other public safety concerns relative to the proposed sharing of the tower. In fact, the provision of new or improved wireless coverage in the area is expected to enhance the safety and welfare of Beacon Falls's residents.

#### Conclusion

For the reasons discussed above, the proposed shared use of the approved municipal tower off Lopus Road in the Town of Beacon Falls satisfies the criteria stated in C.G.S. §16-50aa and advances the General Assembly's and the Council's goal of preventing the proliferation of communication towers in Connecticut. Cingular therefore respectfully requests that the Council issue an order approving the proposed shared use. Thank you for your attention to this matter.

Please feel free to call me at (860) 513-7636 or Christopher Fisher, Esq. at (914) 761-1300 with questions concerning this tower sharing request. Thank you for your consideration in this matter.

Sincerely,

Steven L. Levine

Real Estate Consultant

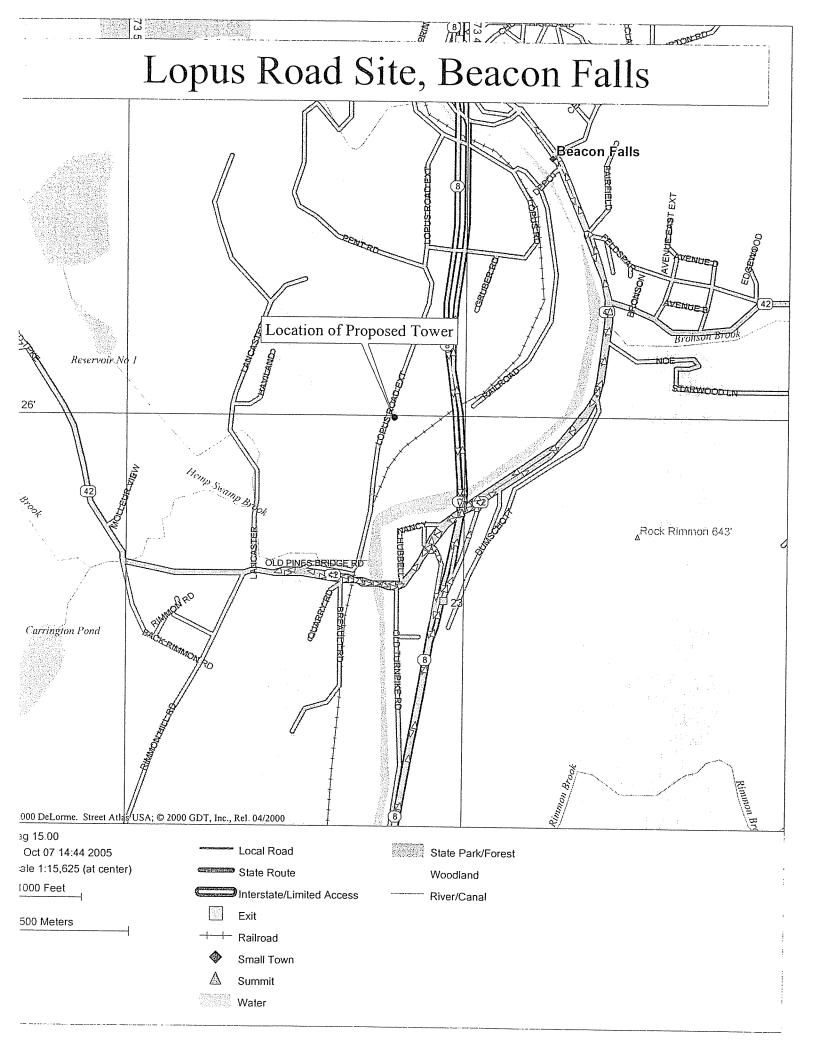
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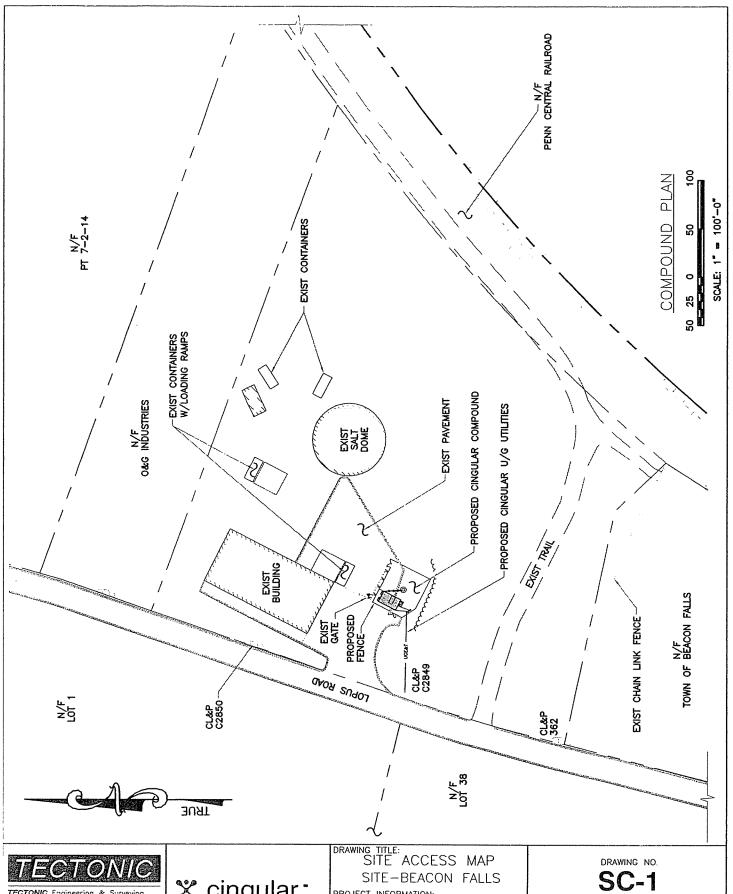
Honorable Susan Ann Cable, 1st Selectman, Town of Beacon Falls

Michele G. Briggs, Manager of Real Estate

Christopher B. Fisher, Esq.

**Enclosures** 





TECTONIC Engineering & Surveying Consultants P.C. 955 Little Britain Road New Windsor, NY 12553 Phone: (845) 567-6656 Fax: (845) 567-8703 www.tectonicengineering.com

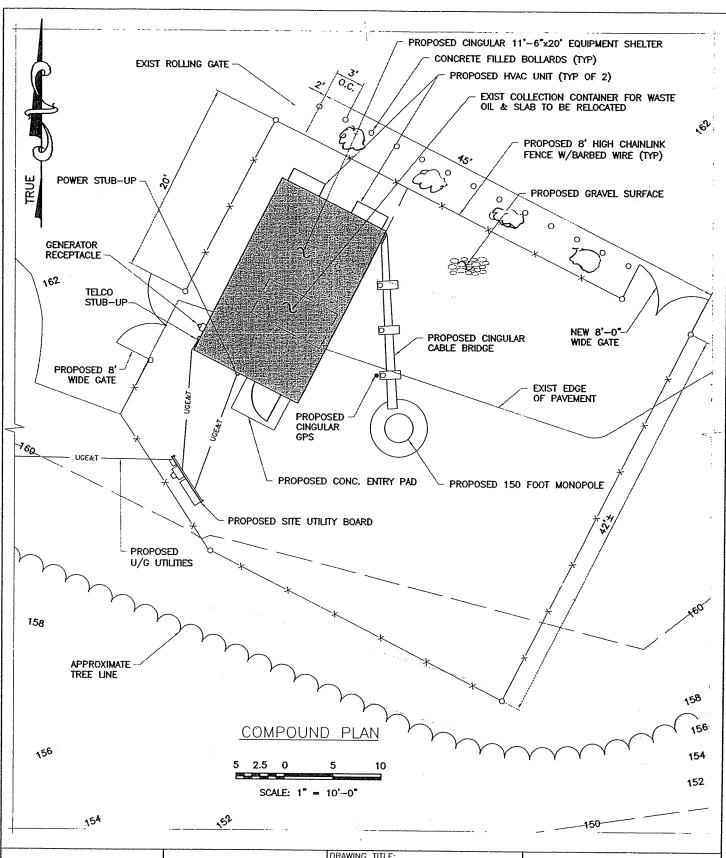
## % cingular wireless

500 ENTERPRISE DRIVE SUITE 3A ROCKY HILL, CT. 06067

SITE-BEACON FALLS

PROJECT INFORMATION:
BEACON FALLS CENTRAL
LOPUS ROAD
BEACON FALLS, CT 06403

| REVISION NO. 0                  | DRAWN BY: KAP    |  |  |  |  |
|---------------------------------|------------------|--|--|--|--|
| DATE: 8/5/05                    | CHECKED BY: CD   |  |  |  |  |
| SCALE: AS SHOWN                 | APPROVED BY: MP  |  |  |  |  |
| ISSUED FOR APPROVAL             | SHEET NO. 1 of 4 |  |  |  |  |
| WORK ORDER #: 3917-BEACON FALLS |                  |  |  |  |  |



## TECTONIC

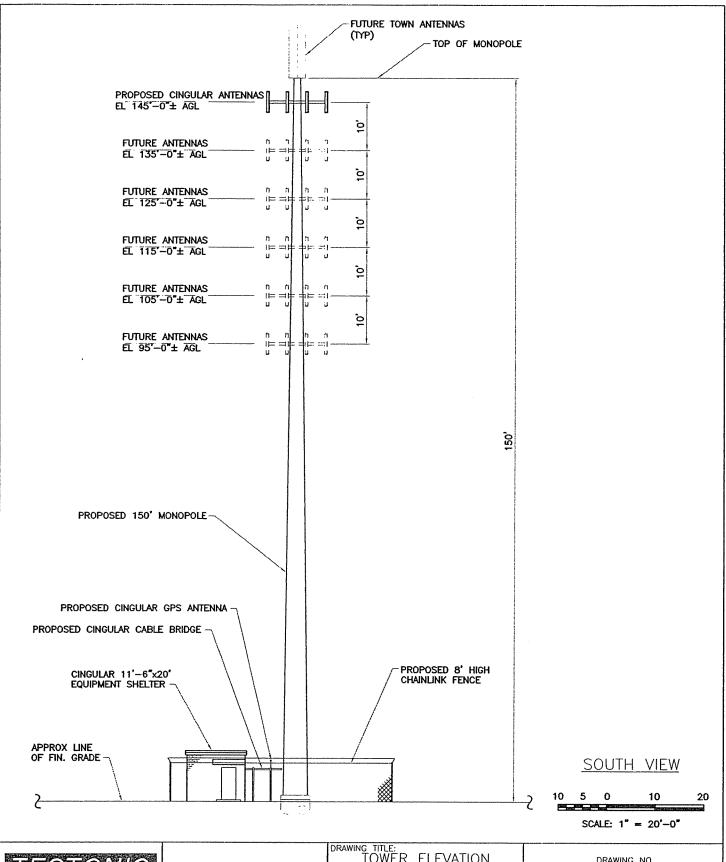
TECTONIC Engineering & Surveying Consultants P.C. 955 Little Britain Road New Windsor, NY 12553 Phone: (845) 567-6556 Fax: (645) 567-8703 www.tectonicengineering.com

## X cingular wireless

500 ENTERPRISE DRIVE SUITE JA ROCKY HILL, CT. 06067 DRAWING TITLE:
COMPOUND PLAN
SITE—BEACON FALLS
PROJECT INFORMATION:
BEACON FALLS CENTRAL
LOPUS ROAD
BEACON FALLS, CT 06403

## SC-2

| REVISION NO. 0                  | DRAWN BY: KAP    |  |  |  |  |
|---------------------------------|------------------|--|--|--|--|
| DATE: 8/5/05                    | CHECKED BY: CD   |  |  |  |  |
|                                 | APPROVED BY: MP  |  |  |  |  |
| ISSUED FOR APPROVAL             | SHEET NO. 2 of 4 |  |  |  |  |
| WORK ORDER #: 3917-BEACON FALLS |                  |  |  |  |  |





TECTONIC Engineering & Surveying Consultants P.C 955 Little Britain Road New Windsor, NY 12553

Phone: (845) 567-6656 Fox: (845) 567-8703 www.tectonicengineering.com

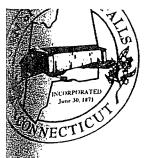


500 ENTERPRISE DRIVE SUITE 3A ROCKY HILL, CT 06067

drawing title: TOWER ELEVATION SITE-BEACON FALLS

PROJECT INFORMATION: BEACON FALLS CENTRAL LOPUS ROAD BEACON FALLS, CT 06403 DRAWING NO.

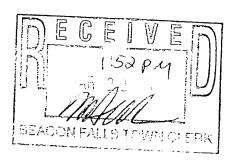
| REVISION NO 0                   | DRAWN BY: KAP    |  |  |  |  |
|---------------------------------|------------------|--|--|--|--|
| DATE: 8/5/05                    | CHECKED BY: CD   |  |  |  |  |
| SCALE: AS SHOWN                 | APPROVED BY: MP  |  |  |  |  |
| ISSUED FOR APPROVAL             | SHEET NO. 3 of 4 |  |  |  |  |
| WORK ORDER #: 3917-BEACON FALLS |                  |  |  |  |  |



# Town of BEACON FALLS onnecticut

## Planning and Zoning Commission

Board of Selectman 10 Maple Avenue Beacon Falls, CT. 06403



The Beacon Falls Planning and Zoning Commission, after review of site plan proposed by AT&T, respectfully recommends acceptance.

If you have any questions or concerns please contact Chairman Jeff Burkitt.

Mary Ellen Fernandes

Clerk, P & Z Commission

March 20, 2004



Planning and Zoning Commission
Regular Meeting Minutes
March 18, 2004
Draft Minutes Subject to Modification

#### | Call to Order

Chairman Burkitt called the regular meeting of the Beacon Falls Planning and Zoning Commission to order at 7:30 P.M.

Present: Chairman Burkitt, Commissioners Carl Vitale, Peter Betkoski, Richard

Franco, David Chadderton and Bill Abromaitis.

Absent: Kevin McDuffie

#### II Approval of Minutes

A motion to approve the minutes of the Feb 2004 regular meeting as submitted was made by Comm. Abromaitis and 2<sup>nd</sup> by Comm. Franco. All in favor. A motion to approve the minutes of Public Hearing on 6 month moratorium was made by Comm. Vitale and 2<sup>nd</sup> by Comm. Abromaitis. All in favor. A motion to approve the minutes of the Public Hearing on Pond Spring was made by Comm. Abromaitis and 2<sup>nd</sup> by Comm. Franco. All in favor.

#### III Comments from the Public

John smith, E.J. Smith Company came forward and requested a extension for filing of the mylar for application P-2003-115 Smith Farms-Section IV. Chairman Burkitt stated that this would be handled under Old Business.

#### IV Zoning Enforcement Officers Report

A written report was submitted. Discussion followed. A motion to accept report as submitted was made by Comm. Abromaitis and 2<sup>nd</sup> by Comm. McDuffie. All in favor. Charlie Edwards requested permission to have site trailer on project for 18 months. Comm. Chadderton made a motion to grant request for construction trailer for up to 18 months or more specifically September 18, 2005. Seconded by Comm. Abromaitis. All in favor.

#### V Town Engineers Report

An written report was submitted. Discussion followed. A motion to accept report as submitted was made by Comm. Abromaitis and was 2<sup>nd</sup> by Comm. Franco. All in favor.

## VI Comprehensive Plan of Conservation and Development No report.

A joint discussion between the Board of Selectman, Atty. Civitello, Planning & al Old Business Zoning and Atty. Buemi. After hearing from both attorneys, it was decided that this discussion does not belong before the Planning and Zoning Commission. 1)Application P-2003-114SP- Chatfield/Woodhaven – A motion to set a Public Hearing date for May 4, 2004 at 7:30 PM was made by Comm. Vitale and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.

3)Fawn Hill Estates – A motion to send a letter to Board of Selectman to recommend reducing the maintenance bond was made by Comm. Vitale and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.

2)Pond Spring Village – Site Plan – Accept for review.

4)E J Smith – A motion to grant request of extension to file mylar was made by Chadderton and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.

- 1) Application P-2004-120- 6 month moratorium A motion to table to April 15, VII New Business 2004 was made by Comm. Vitale and 2<sup>nd</sup> by Comm. Betkoski. All in favor.
  - 2) Joyce Van Lines Application accepted under review.
  - 3)Earth Works Application accepted under review.

### New Applications

- 1) ATT Cell Tower A motion to recommend to Board of Selectman to accept was made by Comm. Chadderton and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.
- 2) Cotton Hollow Rd Multi unit A brief discussion resulted in a motion to Table until issues are resolved was made by Comm. Chadderton and 2<sup>nd</sup> by Comm. Franco. All in favor.
- 3) Oakwood Estates A motion to set Public Hearing for May 4, 2004 at 7:00 PM was made by Comm. Abromaitis and 2<sup>nd</sup> by Comm. Franco. All in favor.
- 4) Westwind Estates Resubdivision Lot 22 & 23 Public Hearing date set
- 5) Charlie Edwards Lot Line Revisions A motion to approve was made by Comm. Chadderton and 2<sup>nd</sup> by Comm. Vitale. All in favor.

## X Correspondence and Payment of Bills

The following bills were submitted for payment:

Nafis & Young \$ 552.50 / M.E. Fernandes \$ 192.00 / Wtby Republican \$102.90 Nutmeg Printers \$394.00 / Fasano, Ipplitio & Lee \$730.00 / Karen Wilson \$115.00. A motion to accept Payment of Bills as submitted was made by Comm. Abromaitis and 2<sup>nd</sup> by Comm. Franco. All in favor. A motion to accept all correspondence and place on file was made by Comm.

Chadderton and 2nd by Comm. Franco. All in favor.

### X Executive Session

A motion to go into executive session was made by Comm. Chadderton and 2<sup>nd</sup> by Comm. Vitale. All in favor. A motion to come out of executive session was made by Comm. Vitale and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.

### XII Petitions from Commissioners

No activity

#### XII Adjournment

A motion to adjourn was made by Comm. Chadderton and 2<sup>nd</sup> by Comm. Abromaitis. All in favor.

Respectfully Submitted,

Many Ellen Lennande

Mary Ellen Fernandes Clerk, March 20, 2004

## Engineered Endeavors Inc.

7610 Jenther Drive Mentor, Ohio 44060 Tel (440) 918-1101 Fax (440) 918-1108

## Communications Structure Nonlinear Analysis and Design Program

10:07:12 10-03-2005 Revision 1.3 - 1/22/01 Engineer: NGU

Customer TECTONIC Job Name 13674

Structure 145' MONOPOLE

Location NEW HAVEN COUNTY, CT Site BEACON FALLS / 81690

| OD<br>BOT | OD NUM                           |        |                           | LENGTH<br>FT | JOINT<br>INCH |                | YIELD<br>KSI           | WEIGHT<br>LBS   | JOINT<br>HEIGHT        |
|-----------|----------------------------------|--------|---------------------------|--------------|---------------|----------------|------------------------|-----------------|------------------------|
| 43.89     | 17.50 18<br>30.13 18<br>41.35 18 | 0.3750 | 0.278<br>0.278<br>UBE WEI |              | 72.00         | SLIP<br>BASEPL | 65.0<br>65.0<br>POUNDS | 7261.<br>10193. | 94.00<br>49.75<br>0.00 |

E = 29600.0 KSI
UNIT WGT = 0.283 LBS/CU IN
AISC constants are used for stress reductions.
TUBE SECTIONS HAVE 18 SIDES AND ARE TREATED AS ROUND
Internal bend radius = 3 X T
Tube diameters are measured flat to flat.
Tube diameters are increased by 1.020 for wind across points.
Drag coefficients are increase by 1.300 for steps on the pole.
AISC Tube Shape Coefficient of 1.000 is applied.
REVISED DATA FILE NAME T:\ENG5\JOBS13\13674145





ENGINEERED ENDEAVORS INCORPORATED

The Experienced Point of View

8455678703

Customer: TECTONIC

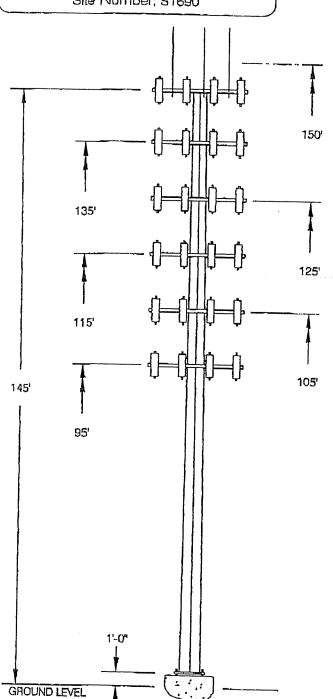
Description: 145' MONOPOLE

EEI Job Number: 13674



#### SITE INFORMATION

Location: NEW HAVEN COUNTY, CT Site Name: BEACON FALLS Site Number; \$1690



## ENGINEERED ENDEAVORS, INC.

7610 Jenther Drive • Mentor, Ohio 44060-4872 Phone: (440) 918-1101 • Phone: (888) 270-3855 Fax: (440) 918-1108 • www.engend.com

#### DESIGN INFORMATION

Designed By: N. UNGER Design Date: 10/3/2005 Status: REVISION 0

#### ANTENNA LOADING

- (12) 7770 PANEL ANTENNAS, (6) LGP2140X TMAS, (18) LGP13519 DIPLEXERS AND (3) OMNIDIRECTIONAL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 145' (CINGULAR)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 135' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 125' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 115' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 105' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 95' (FUTURE)

#### **DESIGN CRITERIA**

DESIGNED IN ACCORDANCE WITH THE TIA/EIA 222-F FOR 85 MPH FASTEST MILE WIND SPEED AND 1/2" RADIAL ICE (NON-SIMULTANEOUS)

DESIGN MEETS THE REQUIREMENTS OF SECTIONS 1609 AND 3108 OF THE 2000 AND 2003 INTERNATIONAL BUILDING CODES FOR 105 MPH 3-SECOND GUST WIND SPEED





8455678703

### **ENGINEERED ENDEAVORS INCORPORATED**

The Experienced Point of View

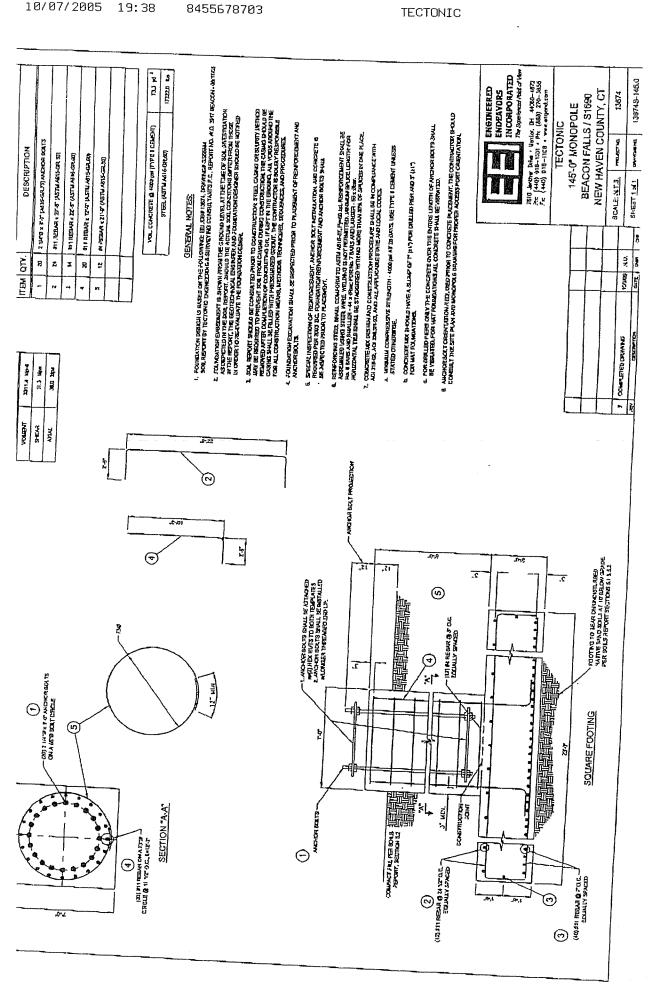
7610 Jenther Drive \* Mentor, OH 44060-4872 Ph: (440) 918-1101 \* Ph: (888) 270-3855 Fx: (440) 918-1108 \* www.engend.com

## DESIGN CALCULATIONS FOR A SPREAD FOOTER FOUNDATION

**TECTONIC** 145 ft Monopole

Beacon Falls / S1690 New Haven County, CT

EEI Project Number 13674 October 3, 2005







New Cingular Wireless PCS, LLC 500 Enterprise Drive

Rocky Hill, Connecticut 06067-3900

Phone: (860) 513-7636 Fax: (860) 513-7190

October 7, 2005

Honorable Susan Ann Cable 1<sup>st</sup> Selectman, Town of Beacon Falls Town Hall, 10 Maple Avenue Beacon Falls, Connecticut 06403

Re: Request by New Cingular Wireless PCS, LLC for an Order Approving Shared Use of an Approved Municipal Tower off Lopus Road, Beacon Falls

Dear Ms. Cable:

As you know, New Cingular Wireless PCS, LLC ("Cingular") intends to install cellular antennas and equipment at an approved wireless telecommunications tower located at the Beacon Falls Public Works Department garage off Lopus Road. Pursuant to Cingular's (formerly AT&T Wireless) lease with the Town, the tower will be owned and operated by the Town of Beacon Falls. We will be filing a building permit application within the next few days.

Pursuant to Connecticut General Statutes Section 16-50aa, Cingular has also requested an order approving shared use of the tower from the Connecticut Siting Council.

The accompanying letter fully describes Cingular's proposal. However, if you have any questions or require any further information on our plans or the Siting Council's procedures, please call me at (860) 513-7636 or Mr. Derek Phelps, Executive Director, Connecticut Siting Council at (860) 827-2935.

Sincerely

Steven L. Levine Real Estate Consultant

Enclosures

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## Communications Structure Nonlinear Analysis and Design Program

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Customer TECTONIC Job Name 13674

Structure 145' MONOPOLE

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CONNECTICUT SITING COUNCIL

| OD<br>BOT | OD NUM                           |                             |                | LENGTH<br>FT          | JOINT<br>INCH | JOINT<br>TYPE | YIELD<br>KSI | WEIGHT<br>LBS | JOINT<br>HEIGHT |
|-----------|----------------------------------|-----------------------------|----------------|-----------------------|---------------|---------------|--------------|---------------|-----------------|
| 43.89     | 17.50 18<br>30.13 18<br>41.35 18 | 0.3750<br>0.3750<br>TOTAL T | 0.278<br>0.278 | 49.54<br>52.75<br>GHT | 72.00<br>0.00 | 20873.        | 65.0         |               | 49.75           |

E = 29600.0 KSI

UNIT WGT = 0.283 LBS/CU IN

AISC constants are used for stress reductions.

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REVISED DATA FILE NAME T:\ENG5\JOBS13\13674145





ENGINEERED ENDEAVORS INCORPORATED

The Experienced Point of View

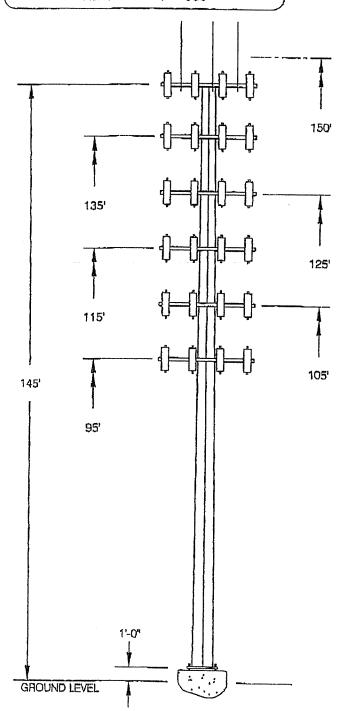
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#### SITE INFORMATION

Location: NEW HAVEN COUNTY, CT Site Name: BEACON FALLS Site Number; S1690



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#### Designed By: N. UNGER Design Date: 10/3/2005 Status: REVISION 0

DESIGN INFORMATION

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- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 135' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 125' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 115' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 105' (FUTURE)
- (12) ALP 9212 PANEL ANTENNAS MOUNTED ON A 12' LOW PROFILE PLATFORM AT 95' (FUTURE)

#### DESIGN CRITERIA

DESIGNED IN ACCORDANCE WITH THE TIA/EIA 222-F FOR 85 MPH FASTEST MILE WIND SPEED AND 1/2" RADIAL ICE (NON-SIMULTANEOUS)

DESIGN MEETS THE REQUIREMENTS OF SECTIONS 1609 AND 3108 OF THE 2000 AND 2003 INTERNATIONAL BUILDING CODES FOR 105 MPH 3-SECOND GUST WIND SPEED



## Engineered Endeavors Inc. 145' MONOPOLE 13674

#### PAGE 2

#### APPURTENANCES

#### igineered Endeavors Inc. 145' MONOPOLE 13674

PAGE 3

#### LOAD CASE 1

#### BASIC LOADING

DEAD LOAD FACTOR 1.00 WIND PSF REDUCTION 1.00 RADIAL ICE 0.00 IN.

WIND VELOCITY 85 BOTTOM 19.76 PSF TOP 29.79 PSF MAX BASE ROTATION 0.00 DEG

|                | APPLIED AP | PURTENAN | CE FORCES |
|----------------|------------|----------|-----------|
|                | ELEVATION  | WEIGHT   | MIND      |
|                | FŢ         | KIPS     | KIPS      |
| 70             | 144.00     | 0.420    | 3.310     |
| [A             | 144.00     | 0.108    | 0.262     |
| PLEXER         | 144.00     | 0.095    | 0.148     |
| W PROF. PLATF. | 144.00     | 2.100    | 0.757     |
| P 9212-N       | 134.00     | 0.324    | 2.590     |
| W PROF. PLATF. | 134.00     | 2.100    | 0.741     |
| P 9212-N       | 124.00     | 0.324    | 2.533     |
| W PROF. PLATF. | 124.00     | 2.100    | 0.725     |
| P 9212-N       | 114.00     | 0.324    | 2.473     |
| W PROF. PLATF. | 114.00     | 2.100    | 0.708     |
| P 9212-N       | 104.00     | 0.324    | 2.409     |
| W PROF. PLATF. | 104.00     | 2.100    | 0.689     |
| P 9212-N       | 94.00      | 0.324    | 2.340     |
| W PROF. PLATF. | 94.00      | 2.100    | 0.670     |
| 222            | 150.00     | 0.048    | 0.441     |

| TUBE<br>LEV<br>FT                            | PROPEI<br>DIAM<br>IN             | RTIES<br>WALL<br>IN                            |                                                     | EMBER FO<br>BENDING<br>K-FT                                       |                                                |                                      | RESSES<br>BEND.<br>KSI                    | ALLOW<br>KSI            | STRESS<br>RATIOS                     | TOTAL DEFL TILT IN DEG                                                     |
|----------------------------------------------|----------------------------------|------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------------------|------------------------------------------------|--------------------------------------|-------------------------------------------|-------------------------|--------------------------------------|----------------------------------------------------------------------------|
| 4.00<br>4.00<br>4.00<br>4.00<br>4.00<br>4.00 | 20.28<br>23.06<br>25.83<br>28.61 | 0.2500                                         |                                                     | 2.64<br>56.76<br>151.68<br>287.02<br>462.10<br>676.00<br>JOINT: S | 2.46<br>2.46<br>5.04<br>7.76<br>10.64<br>13.71 | 0.56                                 |                                           | 50.32<br>48.97          | 0.01<br>0.17<br>0.35<br>0.54<br>0.73 | 94.9 6.11<br>82.3 5.98<br>70.2 5.69<br>58.8 5.27<br>48.4 4.74<br>39.1 4.13 |
| 4.00<br>2.75<br>1.75<br>0.75<br>9.75         | 33.89<br>36.94<br>40.00<br>43.06 | 0.3750<br>0.3750<br>0.3750<br>0.3750<br>0.3750 | 25.33<br>25.33<br>26.06<br>26.80<br>27.54<br>(PE OF | 676.01                                                            | 17.76<br>17.76<br>19.44<br>21.27<br>23.23      | 0.50<br>0.45<br>0.45<br>0.46<br>0.46 | 30.19<br>35.22<br>38.36<br>40.36<br>41.59 | 51.99<br>51.00<br>49.89 | 0.59<br>0.69<br>0.76<br>0.82<br>0.86 | 39.1 4.13<br>30.0 3.61<br>22.3 3.08<br>15.7 2.57<br>10.4 2.07              |
| 9.75<br>6.00<br>4.00<br>2.00<br>0.00         | 46.00<br>49.33<br>52.67          | 0.3750<br>0.3750                               | 28.39 2<br>29.18 2<br>29.92 2                       |                                                                   | 27.46                                          | 0.51<br>0.52<br>0.52                 | 43.36<br>44.08<br>44.26<br>44.16<br>43.90 | 48.13<br>47.33<br>46.64 | 0.89<br>0.92<br>0.94<br>0.96<br>0.96 | 10.4 2.07<br>5.3 1.44<br>2.3 0.93<br>0.6 0.45<br>0.0 0.00                  |

Engineered Endeavors Inc. 145' MONOPOLE 13674

PAGE 4

| TRANSVERSE<br>SHEAR<br>0.000 | REACTION<br>VERTICAL<br>FORCE<br>36.002 | COMPONENTS<br>WIND<br>SHEAR<br>-31.24 | エエベンブルロ 人 ひどん | SOUT MOMENT<br>RSE VERTI |  | MOMENT ABOUT<br>WIND AXIS<br>0.000 |
|------------------------------|-----------------------------------------|---------------------------------------|---------------|--------------------------|--|------------------------------------|
|------------------------------|-----------------------------------------|---------------------------------------|---------------|--------------------------|--|------------------------------------|

#### igineered Endeavors Inc. 145' MONOPOLE 13674

PAGE 5

#### LOAD CASE 2

BASIC LOADING PLUS ICE

DEAD LOAD FACTOR 1.00 WIND PSF REDUCTION 0.87 RADIAL ICE 0.50 IN.

WIND VELOCITY 85 BOTTOM 17.19 PSF TOP 25.92 PSF MAX BASE ROTATION 0.00 DEG

|                | APPLIED AP | PURTENAN | CE FORCES |
|----------------|------------|----------|-----------|
|                | ELEVATION  | WEIGHT   | WIND      |
|                | FT         | KIPS     | KIPS      |
| 70             | 144.00     | 0.811    | 3.202     |
| A              | 144.00     | 0.144    | 0.278     |
| PLEXER         | 144.00     | 0.126    | 0.199     |
| W PROF. PLATF. | 144.00     | 3.250    | 0.790     |
| P 9212-N       | 134.00     | 0.660    | 2.450     |
| W PROF. PLATF. | 134.00     | 3.250    | 0.774     |
| P 9212-N       | 124.00     | 0.660    | 2.396     |
| W PROF. PLATF. | 124.00     | 3,250    | 0.757     |
| P 9212-N       | 114.00     | 0.660    | 2.339     |
| W PROF. PLATF. | 114.00     | 3.250    | 0.739     |
| P 9212-N       | 104.00     | 0.660    | 2.279     |
| W PROF. PLATF. | 104.00     | 3.250    | 0.720     |
| P 9212-N       | 94.00      | 0.660    | 2.214     |
| W PROF. PLATF. | 94.00      | 3.250    | 0.699     |
| 222            | 150.00     | 0.120    | 0.839     |

| TUBE |       | RTIES  |       | MEMBER FO |         | STI  | RESSES |       | STRESS | TOTAL     |
|------|-------|--------|-------|-----------|---------|------|--------|-------|--------|-----------|
| LEV  | DIAM  | WALL   | SHEAR | R BENDING | AXIAL   |      |        | ALLOW | RATIOS | DEFL TILT |
| FT   | IN    | IN     | K     | K-FT      | K       | KSI  | KSI    | KSI   |        | IN DEG    |
|      |       |        |       |           |         |      |        |       |        |           |
| 4.00 |       | 0.2500 |       | 5.03      | 4.07    | 0.30 | 1.05   | 51.99 | 0.02   | 96.5 6.31 |
| 4.00 |       | 0.2500 | 6.00  | 64.68     | 4.07    | 0.26 | 9.98   | 51.99 | 0.20   | 83.6 6.16 |
| 4.00 |       |        |       | 165.19    | 8.14    | 0.45 | 19.62  | 51.99 | 0.39   | 71.1 5.84 |
| 4.00 |       | 0.2500 |       | 305.83    | 12.35   |      | 28.83  |       | 0.58   | 59.4 5.38 |
| 4.00 |       | 0.2500 |       | 485.55    | 16.74   | 0.75 | 37.21  | 48.97 | 0.77   | 46.8 4.82 |
| 4.00 | 31.39 | 0.2500 |       | 703.00    |         | 0.87 | 44.66  |       | 0.95   | 39.4 4.19 |
|      |       |        | PE OF | JOINT: S  | LIP JO  | INT  |        | •     |        |           |
| 4.00 |       | 0.3750 |       | 703.00    | 26.85   | 0.75 | 31.39  | 51.99 | 0.62   | 39.4 4.19 |
| 2.75 |       | 0.3750 |       | 989.66    | 26.85   |      | 36.30  |       | 0.71   | 30.1 3.65 |
| 1.75 |       | 0.3750 |       | 1276.20   | 30.38   |      | 39.28  |       | 0.78   | 22.3 3.11 |
| 0.75 | 40.00 | 0.3750 | 27.22 | 1569.03   | 32.35   |      | 41.10  |       | 0.84   | 15.8 2.58 |
| 9.75 | 43.06 | 0.3750 | 27.22 | 1868.16   | 32.35   | 0.64 | 42.15  |       | 0.87   | 10.4 2.08 |
|      |       | T      | PE OF | JOINT: S  | LIP JOJ | NT   |        |       | 0.0.   | 2.00      |
| 9.75 | 42.18 | 0.3750 | 27.87 | 1868.16   | 36.57   |      | 43.94  | 49.19 | 0.90   | 10.4 2.08 |
| 6.00 | 46.00 | 0.3750 | 27.87 | 2251.19   | 36.57   |      | 44.42  |       | 0.94   | 5.3 1.44  |
| 4.00 | 49.33 | 0.3750 | 28.45 | 2592.48   | 38.92   |      | 44.40  |       | 0.95   | 2.3 0.93  |
| 2.00 | 52.67 | 0.3750 | 29.00 | 2940.49   | 41.28   |      | 44.13  |       | 0.96   | 0.6 0.45  |
| 0.00 | 56.00 | 0.3750 | 30.08 | 3295.68   | 45.11   |      | 43.69  |       | 0.96   | 0.0 0.00  |
|      |       |        |       |           |         |      |        |       |        | 0.00      |

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Engineered Endeavors Inc. 145' MONOPOLE 13674

PAGE 6

REACTION COMPONENTS (KIPS AND FT-KIPS) TRANSVERSE VERTICAL MOMENT ABOUT MOMENT ABOUT MOMENT ABOUT MIND SHEAR FORCE SHEAR TRANSVERSE VERTICAL 0.000 WIND AXIS 45.111 -30.076 3295.685 0.000 0.000

## ngineered Endeavors Inc. 145' MONOPOLE 13674

PAGE 7

1 BASIC LOADING

|        | SUMMARY TAB    | LE    |         |      |       |         |        |     |
|--------|----------------|-------|---------|------|-------|---------|--------|-----|
| ELEV   | STRESS RATIO   | AXIAL | BENDING | LOAD | TNG   |         |        |     |
| 144.00 | 0.02           | 4.07  | 5.0     |      |       | LOADING | חד זות | Tan |
| 134.00 | 0.20           | 4.07  | 64.7    |      |       |         |        |     |
| 124.00 | 0.39           | 8.14  | 165.2   | 2    | DAGIC | LOADING | PLUS   |     |
| 114.00 | 0.58           | 12.35 |         |      |       | LOADING |        | ÎÇE |
| 104.00 | 0.77           |       | 305.8   |      |       | LOADING |        | ICE |
| 94.00  |                | 16.74 | 485.5   | 2    | BASIC | LOADING | PLUS   | ICE |
|        | 0.95           | 21,30 | 703.0   |      |       | LOADING |        | TCE |
| 82.75  | 0.71           | 26.85 | 989.7   |      |       | LOADING |        | ICE |
| 71.75  | 0.78           | 30.38 | 1276.2  |      |       | LOADING |        |     |
| 60.75  | 0.84           | 32.35 | 1569.0  |      |       |         |        | ICE |
| 49.75  | 0.90           | 36.57 |         |      |       | LOADING | PLUS   | ICE |
| 36.00  | 0.94           | •     | 1868.2  |      |       |         | PLUS   | ICE |
| 24.00  | - <del>-</del> | 36.57 | 2251.2  | 2    | BASIC | LOADING | PLUS   | ICE |
|        | 0.95           | 38.92 | 2592.5  | 2    | BASIC | LOADING | PLIIS  | ICE |
| 12.00  | 0.96           | 41.28 | 2940.5  |      |       | LOADING |        | ICE |
| 0.00   | 0.96           | 36.00 | 3311.4  | 1    |       | LONDING | THOO   | イクロ |

3311.4

| MAXIMUM SUPPO |       |       |      | 3311.41 |
|---------------|-------|-------|------|---------|
| CORRESPONDING | AXIAL | FORCE | KIPS | 36 00   |
| CORRESPONDING | SHEAR | FORCE | KIPS | 31.25   |

36.00

## Engineered Endeavors Inc. 145' MONOPOLE 13674

#### PAGE 8

| BASE | PLATE | AT | ELEVATION | 0.00 | PEET |
|------|-------|----|-----------|------|------|
|------|-------|----|-----------|------|------|

TUBE DIAMETER DESIGN MOMENT 56.00 INCHES 3311.4 KIP FT

DESIGN MOMENT IS 0. DEGREES FROM THE WIND DIRECTION

BOLTS ARE ON THE KNUCKLES OF THE TUBE

APPLIED AXIAL FORCE 36.0 KIPS 31.25 KIPS APPLIED SHEAR

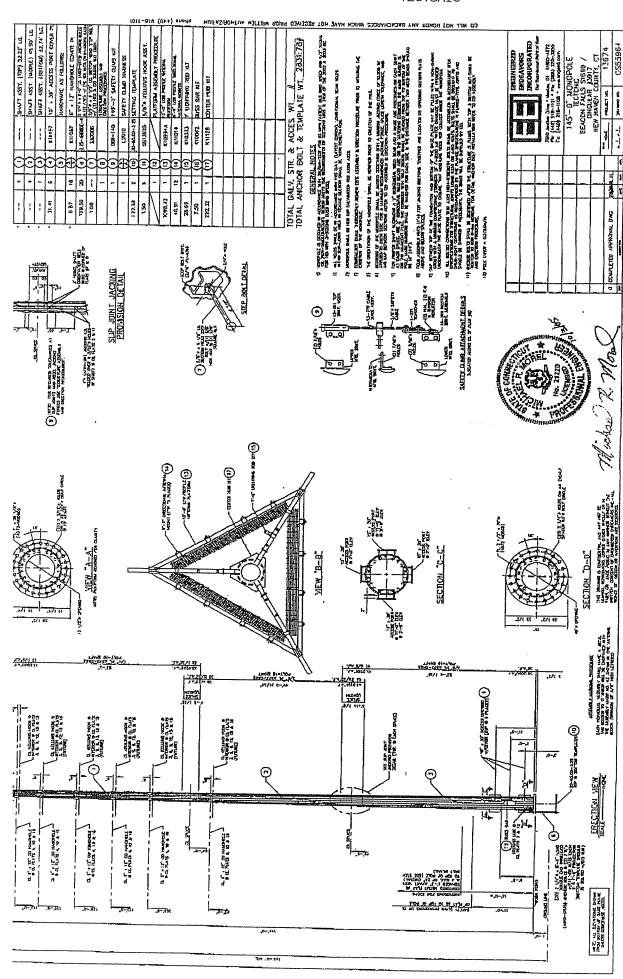
#### BOLT DATA

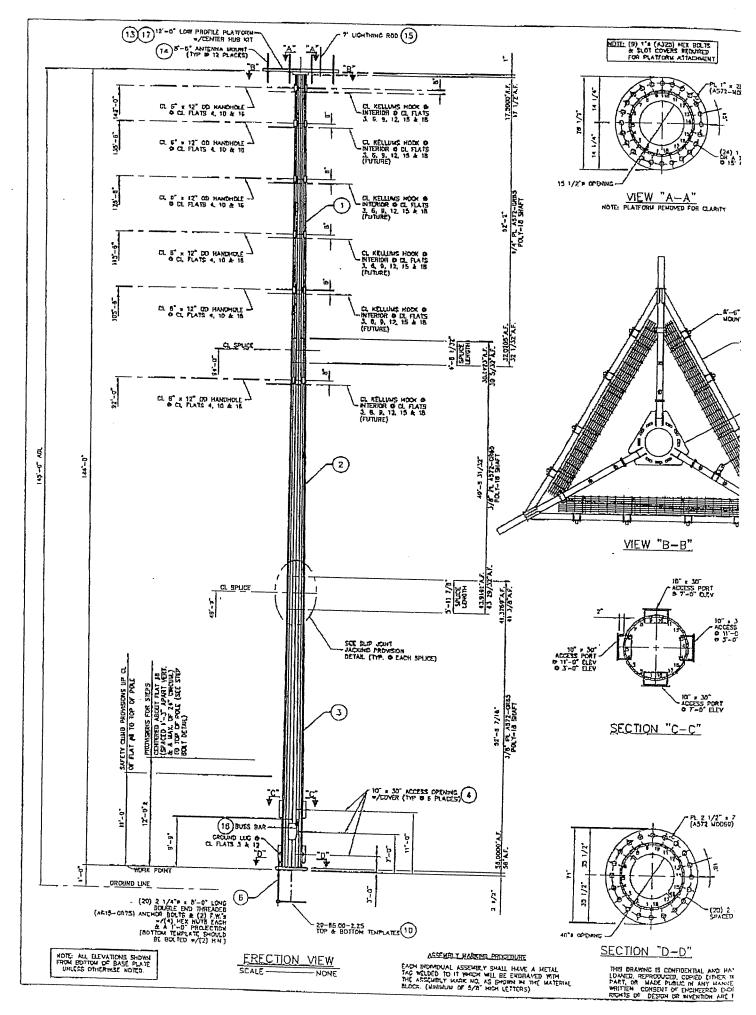
| DIAMETER EFFECTIVE AREA TOTAL LENGTH MINIMUM EMBEDMENT NUMBER OF BOLTS BOLT CIRCLE DIAMETER ALLOWABLE STRESS APPLIED AXIAL STRESS MAX BOLT FORCE BOLT BENDING STRESS COMBINED BOLT STRESS COMBINED BOLT STRESS CLEARANCE UNDER PLATE BOLT WEIGHT  2.250 INCHES C.20 INCHES C.20 EVALUATE STRESS AVAILATE STRES | BOLT TYPE<br>BOLTS ARE EVENLY SPACED                                                                                                                                                                            | A615                                                                               | GR75                                                       |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------|------------------------------------------------------------|
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | DIAMETER EFFECTIVE AREA TOTAL LENGTH MINIMUM EMBEDMENT NUMBER OF BOLTS BOLT CIRCLE DIAMETER ALLOWABLE STRESS APPLIED AXIAL STRESS MAX BOLT FORCE BOLT BENDING STRESS COMBINED BOLT STRESS CLEARANCE UNDER PLATE | 3.250<br>8.0<br>6.4<br>20<br>65.00<br>60.0<br>38.2<br>124.1<br>2.3<br>40.4<br>3.25 | SQ IN FEET FEET INCHES KSI KSI KIPS KSI KSI KSI KSI INCHES |

#### PLATE DATA

| DIAMETER OF PLATE MATERIAL PROVIDED THICKNESS REQUIRED THICKNESS BOLT HOLE DIAMETER CENTER HOLE SIZE NET WEIGHT RAW STOCK WEIGHT SURFACE AREA ALLOWABLE STRESS MAX APPLIED STRESS | 71.00<br>A572 G<br>2.500<br>1.689<br>2.625<br>46.00<br>1497.1<br>3566.5<br>29.39<br>59.99<br>27.38 | INCHES R60 INCHES INCHES INCHES POUNDS POUNDS SQ FT KSI KSI |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|-------------------------------------------------------------|
| CONCRETE STRENGTH                                                                                                                                                                 | 3000.                                                                                              | PSI                                                         |

Base Plate - use 71.00 inch ROUND x 2.500 inch A572 GR60 with (20) 2.250 diameter x 8.00 foot caged A615 GR75 bolts on a 65.00 inch bolt circle.





5) (14)

절(13)

√ kıπ(17)

4 EVENLY

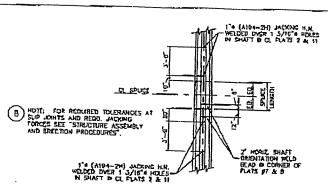
CHTHING ROD KET (15)

RECEIVED

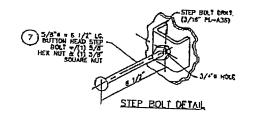
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HAVE

WASCH



## SLIP JOINT JACKING PROVISION DETAIL

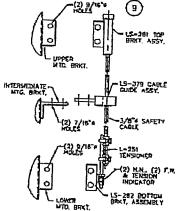


| - 1 |           |      |          |               |                                                                                               |                |
|-----|-----------|------|----------|---------------|-----------------------------------------------------------------------------------------------|----------------|
|     | GALV. WT. | QTY. | ITEM     | MK. NO.       | DESCRIPTION                                                                                   | 7              |
| ٠   |           | 17   | 0        |               | SHAFT ASSY, (TOP) 52.25' LG.                                                                  | 1              |
| ٠   |           | 1    | (2)      |               | SHAFT ASSY. (MIDDLE) 49.50' LG.                                                               | 1              |
| -   |           | 1    | (3)      |               | SHAFT ASSY. (BOTTOM) 52 74' LC.                                                               | 1              |
| ١.  | 31, 41    | E    | (4)      | K11497        | 10" x 30" ACCESS PORT COVER P                                                                 |                |
|     |           |      | (5)      |               | HARDWARE AS FOLLOWS:                                                                          | 1              |
| •   | 6,87      | 18   | (\$)     | K11097        | 8" x 12" HANDHOLE COVER PL                                                                    | 1              |
| 1   | 129.50    | 20   | (6)      | 2 25-A8800E-4 | 2 1/4"6 = 8"-0" LC. (A615-CR75) ANCHOR BOLTS<br>A (3) F.W. = / (4) HEX HUTS (A194-0876), EACH | 1              |
| [   | 1.08      |      | (7)      | \$10006       | 3/8" 4 6 1/2" LC. BUTTON HEAD STEP BOL                                                        | 1              |
|     |           | 1    | (8)      |               | STRUCTURE ASSEMBLY AND<br>ERECTION PROCEDURES                                                 | 1              |
|     |           | 1    | (9)      | DBI-140       | 140'-0" SAFETY CLIMB KIT                                                                      | 1              |
|     |           | 1    | $\oplus$ | L2010         | SAFETY CLIND HARNESS                                                                          | 1              |
| L   | 120.88    | 2    | (10)     | 20-85.00-2.25 | SETTING TEMPLATE                                                                              | ₫              |
|     | 1.50      | 6    | (11)     | C\$13825      | S/8" KELLUMS HOOK ASSY.                                                                       | 918-110        |
| L   |           | 1    | (12)     |               | PLATFORM ASSEMBLY PROCEDURE                                                                   |                |
| L   | 1098.42   | 1    | (13)     | K10994A       | IE-D' LOW PROFILE ANTENNA<br>PLATFORM                                                         | (440)          |
| L   | 40,91     | 12   | (14)     | K11014        | 8'-8" LOW PROFILE DESCRIBINAL<br>ANTENNA MOUNTS                                               |                |
|     | 28.60     | 1    | (15)     |               | 7' LICHTHING ROD KIT                                                                          | phone          |
| Ľ   | 7.50      | 1    | (16)     | K10062        | BUSS BAR KIT                                                                                  | a.             |
| Ĺ   | 292.32    | 1    | (17)     | K11128        | CENTER MUB KIT                                                                                | Z              |
| L   |           |      |          |               |                                                                                               | AU IHORIZA NON |
|     |           |      |          |               |                                                                                               | Ceriz          |
|     |           |      |          |               |                                                                                               | <u> </u>       |
| Γ   |           |      |          |               |                                                                                               |                |
| Г   |           |      |          |               |                                                                                               | MAITTEN        |
| Г   |           | 一十   |          |               |                                                                                               | Ę.             |
|     |           |      |          |               |                                                                                               |                |

140-0 MONOPOLE - BEACON FALLS STEED / DNEWAR 6/917 - 13674 - 5533964 - K II

MATERIAL REQ'D. PER ASSEMBLY

12) POLE TAPER - 0.27834/N.



SAFETY CLIMB ATTACHMENT DETAILS (LOCATED ALONG CL OF FLAT JE)

Constitution of Constitutions Michael R. Mo

| Г       |                        |           | <del></del> | <del></del>      |             |                   |                                                                  |
|---------|------------------------|-----------|-------------|------------------|-------------|-------------------|------------------------------------------------------------------|
| -<br> - |                        |           | -           |                  |             |                   | ENGINEERED ENDEAVORS INCORPORATED THE EXPERIMENTAL POINT OF VIEW |
| F       |                        |           |             |                  | Fr: (140)   | 918-1101 P        | or, OH 44080~4872<br>h: (688) 270~3855<br>mmw.chgend.com         |
|         |                        |           |             |                  | BEAC<br>NEW | TECTO<br>ON FALLS | ONOPOLE<br>NIC<br>51690 /<br>#3917<br>OUNTY, CT                  |
|         | COMPLETED APPROVAL DWG | 3/74/2015 | K J,L       |                  | HONE        | PADECT NO.        | 13674                                                            |
| PCY.    | DELCH-103              | DATE      | pres        | ~ <del>-</del> , | <u>-1+1</u> | DRAWING NO        | G\$55964                                                         |

TOTAL GALV. STR. & ACCES. WT.\_ .TOTAL ANCHOR BOLT & TEMPLATE WT. 2831.78# GENERAL NOTES MONPPOLE IS DESIGNED BY ACCORDANCE WITH TRACE-220F FOR 85 NOW FACTICE WILL WARD SPEED AND 1/7 RADIAL CE (ADM-SMULTAMEDIS). DESIGN MEETS THE RECURRENCIALS OF SECTIONS 1807 & 3108 OF the 2000 and 160 of the 2000 of the 2000 and 160 of the 2000 and 160 of the 2000 ALL MOLDS SMALL BE WI ACCORDANCE WITH AND D.I.I. (LATEST EDITION). LONGITUDHIAL SEAM WELDS WITHOUT SERVICE SECTION SHALL BE YOUZ PENETRATION. MONOPOLE SHALL BE NOT DIP CALVANIZED PER ASTM A123. CONTRACTOR SMALL INDROUGHT REVEW EETS ASSEMBLY & CRECTION PROLEDURE FROM TO INTIATING THE EROCHON OF THE MONOPOLE THE DRIENTATION OF THE MONOPOLE DAME BY VERIFIED PRIOR TO ERECTION OF THE POLE HONDR ANY BACKCHARGES ticks of the monopole small or anched tockther with a minimum accinic force of 10,000 bit leg to each soc for a maximum recommended increas force, since length tolerance and cap between sections refer to 60 assembly a execution procedure. FOR PRIPER EMAT AUCHIGHT A T MOREONTAL WELD BEAD AND A MARK ARE POSITIONED ON EACH SHAFT AT EXCH SPACE, THE 2" HORIZONTAL WELD BEADS ARE ON THE MATCHING CORNERS. THE MARK NUMBER IS NOT THE MARK NUMBER IS POLL MARK NUMBERS SHALL BE AUDIED FROM THE TO BOTTOM OF THE POLL MARK NUMBERS SHALL BE MATCHED FOR CACH SIGN. IT THE BOSTANCE BETWEEN TWO PRED BEADS SHOULD PELD ASSEMBLY NUTS (1°4) FOR JACKING SECTIONS TOOFINGS AND LOCATED ON EPPOSING SECTION FLATS 3) DAP BETWEEN TOP OF THE FOLKRATION AND BOTTON OF THE BASE PLATE MAY BE FILLED WITH A MON-SHRINK CROUT WITH A MINIMUM COMPRESSIVE STRENGTH OF F-2000 PM. WATER DRAMAGE MUST BE PROVIDED UNDERHEATH THE BASE PLATE TO ENSURE THAT MONSTURE DOES NOT COLLECT INSIDE THE MONOPOLE. ALL BOLTED CONNECTIONS WITH A 325 HOTH-STRENGTH BOLTS SMALL BE ASSEMBLED IN ACCOMMENCE WITH ASSEMBLED FOR STRUCTURAL JURITS USING A323 OR A490 BOLTS BOLTS SHALL BE BROUGHT TO SHURL-TIONS COMMENTS AS RECOMMENDED BY DRE FLANCE SPECIFICATIONS IN FLANCE-TYPE JOINTS AND SHOULD BE SHIPMED F NECESSARY. THE SHAMS WILL BE SUPPLIED BY TOL NOT ij 17) ANGJER BOLTS SHALL BE REJIENED AFTER THE STRUCTURE IS PLUMB, BOTH TOP A NOTION NUT SHALL BE NOTED TO 10-05 INDUSTRIENT, FOR DETAIL ANCHOR BOLT MISTALLATION REFER TO EEL ASSEMBLY 



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## **ENGINEERED ENDEAVORS** INCORPORATED

The Experienced Point of View

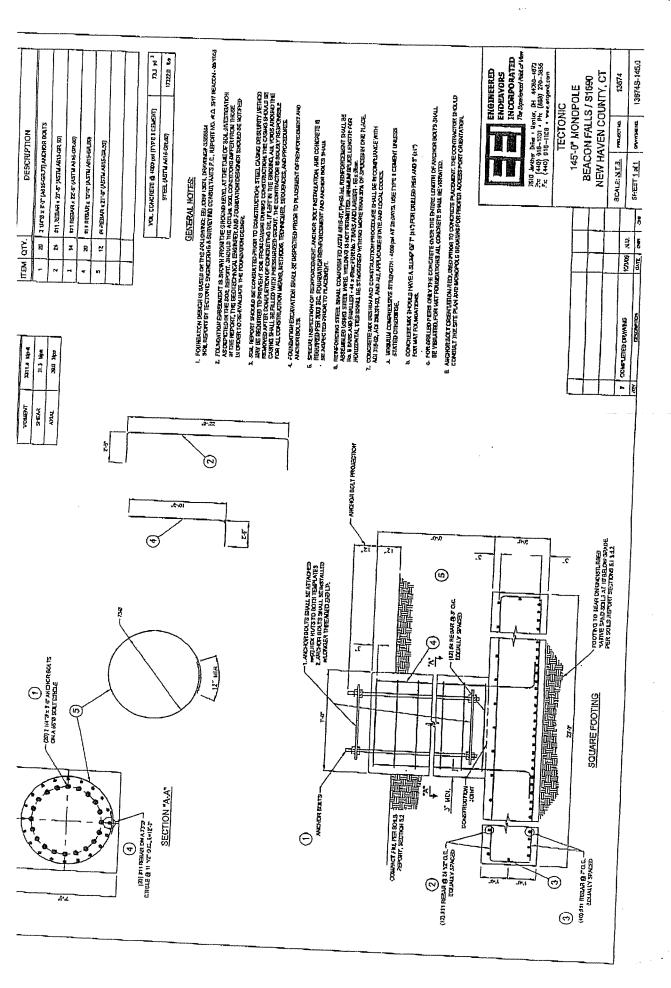
7610 Jenther Drive \* Mentor, OH 44060-4872 Ph: (440) 918-1101 + Ph: (888) 270-3855 Fx: (440) 918-1108 \* www.engend.com

## DESIGN CALCULATIONS FOR A SPREAD FOOTER FOUNDATION

**TECTONIC** 145 ft Monopole

Beacon Falls / S1690 New Haven County, CT

EEI Project Number 13674 October 3, 2005



#### FOUNDATION DESIGN CALCULATIONS FOR SPREAD FOOTING FOUNDATION

ENGINEERED ENDEAVORS INC. 7610 Jentner Drive \* Mentor, Ohio 44060 Tel:(216)918-1101 \* Fax:(216)918-1108

03-Oct-05 11:D7 AM

CUSTOMER STRUCTURE **EEI PROJECT** LOCATION SITE NAME

TECTONIC 145' MONOPOLE 13674

NEW HAVEN COUNTY, CT BEACON FALLS / \$1690

#### SERVICE LOADS AT BASE OF THE MONOPOLE

|                                                    |                 | Design Legative |                  | F 1/2/17/17/2000                           |            |
|----------------------------------------------------|-----------------|-----------------|------------------|--------------------------------------------|------------|
| Moment, kip-ft                                     |                 | Design Loading  | , ···· ··        | · · · · · · · · · · · · · · · · · · ·      | ३५ स्ट्यूप |
| Shear, klos                                        |                 | 3311.4          | W                |                                            |            |
| Axial Load, kips                                   |                 | 31.25           |                  |                                            |            |
| ANIAI COBU, NIPS                                   |                 | 36.0            |                  |                                            | i          |
| Anchor Bolts                                       | O11-1-45b.      |                 |                  |                                            |            |
| KICIOI BOILS                                       | Quantity        | 20,D            |                  | <del>4</del>                               | <u> </u>   |
|                                                    | Length, ft      | 8.0             |                  | and the second second second second second |            |
|                                                    | Circle Dia., in | 65.0            |                  |                                            |            |
|                                                    | Projection, In  | 12.0            |                  |                                            |            |
| Foundation Parameters                              |                 |                 |                  |                                            |            |
| Pedestal Min. Width, in                            |                 | 83.00           |                  |                                            |            |
| Pedestal Projection, in                            |                 | 12.0            |                  |                                            |            |
| Found, Min Height, fi                              |                 | 7.5             |                  |                                            |            |
|                                                    | Height, ft      | Width, it       | Soll Unit Wt., p | ~=                                         | 455.00     |
| Footing                                            | 3.00            | 23.00           | •                |                                            | 120.00     |
| Pedestal                                           | 8.00            | 7.00            | Concrete Unit V  |                                            | 150.00     |
|                                                    |                 | 1.00            | Slope of backfil | II, degrees                                | 0.00       |
| Foundation Weight, kips                            |                 | 296.85          |                  |                                            |            |
| Concrete, cub.yd.                                  |                 | 73.30           |                  |                                            |            |
| Soil Weight, kips                                  |                 | 403.20          | H≒               | 7.00                                       |            |
| Total Vertical Load, kips Kern of Eccentricity, ft |                 | 736.05          | B=               | 23.00                                      |            |
| •                                                  |                 | 3.83            |                  |                                            |            |
| Actual Eccentricity, ft                            |                 | 4.97            |                  |                                            |            |
| Overturning Moment, kip-ft                         |                 | 3655,15         |                  |                                            |            |
| Resisting Moment, kip-ft                           |                 | 8464,58         |                  |                                            |            |
| Allowable Gross Soil Pressure                      | , ksf           | N/A             |                  |                                            |            |
| Allowable Net Soil Pressure, k                     |                 | 6.0             |                  | (gross)                                    | (net)      |
| Gross Soil Pressure, (Service                      | Load), Kst      |                 | max q=           | 3.27                                       | 1.94       |

Safety Factor

Sf=

2.32

min q=

3.27

0.00

1.94

### ULTIMATE STRENGTH DESIGN OF FOOTING

CONCRETE, psi 3000 STEEL, KSI 60

#### SHEAR IN FOOTING

| 1. CASE I -DEAD LOAD, TWO-WAY SHEAR | U= 1.4*D |
|-------------------------------------|----------|
|-------------------------------------|----------|

Ultimate Vertical Load, kips 1030.47 Ultimate Pressure, ksf 1.95

Ultimate shear V, kips 854.67 Design shear Vn, kips 2547.57

O.K.

#### 2. CASE II - WIND LOAD, ONE-WAY SHEAR U=0.9°D+1.6°W

Ultimate Moment, klp-ft 5848.24 Ultimate Vertical Load, kips 662.45 Eccentricity, ft 8.83 Ultimate Pressure, ksf quit= 7.19 Dist, from edge to critical sect., ft 5.50 Pressure distance ft · C= 8.02 Pressure @ critical section, ksf 2.26

Actual Number of Bars

Top Steel Area, sq.in

Horizontal Spacing, in

Ultimate Shear, kips 597,21 Dasign Shear, kips 770.97 O.K.

#### FLEXURE STRENGTH DESIGN

| Ultimate Mor                                                                    | ment, kip-ft                                                                                                               | Case I                        | 1433.70                                              |             |      |
|---------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------|-------------------------------|------------------------------------------------------|-------------|------|
|                                                                                 |                                                                                                                            | Case II                       | 7049.33                                              | <b>q1</b> = | 0.01 |
| Coefficient or<br>ReInforceme<br>Min. ReInforc<br>Min. Steel Ar<br>Type of Bars | nt Ratio<br>cement Ratio                                                                                                   | Rn=<br>r=<br>r mln<br>A1<br># | 378.4<br>0.00656<br>0.00180<br>56.80                 |             |      |
| воттом                                                                          | Min. Number of Bars<br>Actual Number of Bars<br>Actual Steel Area, sq.in.<br>Steel Ratio Actual<br>Revised Coef. of Resist | Ab,in^2⇒<br>ra=<br>Rn=        | 1.56<br>36.41<br>40.00<br>62.40<br>0.00754<br>452.07 |             |      |
|                                                                                 | Design Moment, kip-ft                                                                                                      |                               | 8422,13                                              |             |      |
|                                                                                 | Horizontal Spacing, in                                                                                                     | shor=                         | 6.92                                                 |             |      |
| TOP                                                                             | Min. Steel Area, sq.in<br>Min. Number of Bars                                                                              |                               | 16.39<br>10.51                                       |             |      |

\$hor≖

10.51

12.00

18.72

24,55

| PEDE | EST | AL | DES | IGN |
|------|-----|----|-----|-----|
|------|-----|----|-----|-----|

| Pedestal Width, in          | 84     | Ultim. Moment   | 4000.0 |
|-----------------------------|--------|-----------------|--------|
| Concrete, ksi               | 3      | Chart. Worlen   | 4629,8 |
| Reinforcement, ksi          | 60     |                 |        |
| Actual Rebars , #11 Q-ty    | 20     | Asaa            |        |
| Design Rebars Q-ty          | 12     | Area, sq.in     | 1.56   |
| Minimum reinforcement ratio |        | Area, sq.in     | 2.60   |
| Actual reinforcement ratio  | 0,0044 | Rebar space, ir | 11.78  |
| Concrete cover , in         |        |                 |        |
| Rebar layout radius, in     | 4      |                 |        |
| tional layout laolus, iii   | 37.50  |                 |        |

### Bending about the major axis

| No. | Angle, deg | Coord., in | Edge Dist, in | No. | Angle, deg | Coord., in t | ≘dge Dist., in |
|-----|------------|------------|---------------|-----|------------|--------------|----------------|
| 1   | 0          | 37.50      | 4.50          | 7   | 180        | 07.00        | ***            |
| 2   | 30         | 32,48      | 9.52          | ,   |            | -37,50       | 79,50          |
| 3   | 60         | 18.75      |               | 8   | 210        | -32.48       | 74,48          |
| 4   | _          |            | 23.25         | 9   | 240        | -18.75       | 60.75          |
|     | 90         | 0.00       | 42.00         | 10  | 270        | 0.00         | 42.00          |
| 5   | 120        | -18.75     | 60.75         | 11  | 300        |              |                |
| 6   | 150        | -32,48     | 74,48         |     |            | 18.75        | 23.25          |
|     |            | 04,40      | 74.40         | 12  | 330        | 32.48        | 9.52           |

## Location of neutral axis c=, ir 7378

| Compres | ssion zone | , a=          | 6.6    |                           |           |             |                |        |                         |
|---------|------------|---------------|--------|---------------------------|-----------|-------------|----------------|--------|-------------------------|
|         |            | No.           | е      | For <del>ce</del><br>kips | Tension z | one         | No.            | е      | Force                   |
|         |            | 1             | 0.0013 | 88.73                     |           |             | 2              | 0.0007 | <i>kip</i> s<br>50.71   |
| eu=     | 0.003      |               |        |                           |           |             | 3              | 0.0007 | 156.00                  |
|         |            |               |        |                           | ey=       | 0.00207     | 4              | 0,0132 | 156.00                  |
|         |            |               |        |                           |           |             | 5              | 0.0204 | 156,00                  |
|         |            |               |        |                           |           |             | 6              | 0.0257 | 156,00                  |
|         |            |               |        |                           |           |             | 7              | 0.0277 | 156,00                  |
|         |            |               |        |                           |           |             | 8              | 0.0257 | 158,00                  |
|         |            |               |        |                           |           |             | 9              | 0.0204 | 156.00                  |
|         | Co         | oncrete, kips |        | 1416,50                   |           |             | 10             | 0.0132 | 156,00                  |
|         |            | ,,            |        | 1410,30                   |           |             | 11             | 0.0050 | 156.00                  |
|         | To         | otal compr    | ession | 1505,24                   |           | Total tensi | 12<br>on, kips | 0.0007 | 50,71<br><b>1505;41</b> |

| Moment   | due to c      | compression            |         | Moment due      | to toppia |          | •       |
|----------|---------------|------------------------|---------|-----------------|-----------|----------|---------|
| Rebars   | Force<br>klps | Mom, Arm,<br><i>In</i> | Moment  | <b>~</b> .      | orce      | Mom. Am. | Moment  |
|          | nip 2         | ""                     | k-fi    |                 | kips      | in       | k-ft    |
| 1        | 88.73         | 37.50                  | ***     | 2               | 50.71     | 32.48    | -137.23 |
| 2        | 0.00          | 07.50                  | ~~1,00  | 3               | 156.00    | 18,75    | -243.75 |
| 12       | 0.00          | 02.10                  | 0.00    | 4               | 156.00    | 0.00     | 0.00    |
| '-       | 0.00          | 32.48                  | 0.00    | 5               | 156,00    | -18.75   | 243,75  |
| Concrete | 1416.50       | 20.00                  |         | 6               | 156.00    | -32.48   | 422.19  |
|          | 1410.50       | 38,69                  | 4567.46 | 7               | 156.00    | -37.50   | 487.50  |
|          |               |                        |         | 8               | 156.00    | -32.48   | 422.19  |
|          |               |                        |         | 9               | 156,00    | -18.75   | 243,75  |
|          |               |                        |         | 10              | 156,00    | 0.00     | 0.00    |
|          |               |                        |         | 11              | 156,00    | 18.75    | -243.75 |
|          | Total in co   | ompression             | 1011    | 12              | 50.71     | 32.48    | -137,23 |
|          | i otal fil Ct | with the Region        | 4844.76 | Total In tensio | n         |          | 1057.41 |

Design moment about the major axis, kip-ff

5311.95

|  |  | a a designation of the second                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  |
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