

Filed by:

G. Scott Shepherd, Site Development Specialist II - SBA Communications 134 Flanders Rd., Suite 125, Westborough, MA 01581 508.251.0720 x 3807 - GShepherd@sbasite.com

September 21, 2020

Melanie A. Bachman Acting Executive Director Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Notice of Exempt Modification 81 Montevideo Rd., Avon, CT

Latitude: 41.803100 Longitude: -72.801300

T-Mobile Site #: CT11284A_Anchor

Dear Ms. Bachman:

T-Mobile currently maintains three (3) 600/700/1900/2500 MHz antennas at the 136-foot level of the existing 150-foot Self-Supporting Tower at **81 Montevideo Rd., Avon, CT**. The 150-foot tower is owned by SBA 2012 TC Assets, LLC. The property is owned by Monte LLC. T-Mobile now intends to install one (1) additional 2500 MHz antenna. The new antennas would be installed at the 136-foot level of the tower.

Please note: Per the Connecticut Siting Council Website: CSC COVID 19 Guidelines. In order to prevent the spread of Coronavirus and protect the health and safety of our members and staff, as of March 18, 2020, the Connecticut Siting Council shall convert to full remote operations until March 30, 2020. Please be advised that during this time period, all hard copy filing requirements will be waived in lieu of an electronic filing. Please also be advised that the March 26, 2020 regular meeting shall be held via teleconference. The Council's website is not equipped with an on-line filing fee receipt service. Therefore, filing fees and/or direct cost charges associated with matters received electronically during the above-mentioned time period will be directly invoiced at a later date.

Planned Modifications:

TOWER

Remove:

N/A



Remove and Replace:

N/A

Install New:

- (1) Ericsson AIR 6449 B41 antenna
- (1) Ericsson Radio 4415 B25 RRU
- (1) 1-5/8" fiber

Existing Equipment to Remain:

- (1) Ericsson AIR32 KRD901146-1_B66 antenna
- (1) Ericsson AIR21 KRC118023-1 antenna
- (1) RFS-APXVAARR24_43-U-NA20 antenna
- (1) Ericsson KRY112 144/2 TMA
- (1) Ericsson 4449 B71+B12 RRU
- (2) 1-5/8" coax
- (1) ½" coax for GPS (ground)
- (1) 1-5/8" fiber

Entitlements:

- (4) 1-5/8" cable
- (1) 1-1/4" hybrid cable

GROUND

Install New:

- Equipment mounted to proposed 8'x 8' x 6' concrete pad within 8' x 8' lease area in existing compound under proposed 8' x 8' weather canopy.
- Equipment inside existing 6160 equipment cabinet

Original tower was approved by Town of Avon zoning agencies, case# EM-MCM-004-070824 (enclosed), prior to statewide change in law in 2001, which brought it under the CSC's jurisdiction. Approval is for the replacement of a 150' self-support structure. The Tower was later approved by the CSC on Oct. 24, 2007, Docket# EM-MCM-004-070824 (enclosed) There were no further post construction stipulations set. Please see attached.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16.50j-72(b)(2). In accordance with R.C.S.A. § 16.50j-73, a copy of this letter is being sent to the Town of Avon's Director of Planning and Community Development, Hiram Peck III, and Town Manager, Brandon Robertson, as well as to the property owner, Monte LLC. (Separate notice is not being sent to tower owner, as it belongs to SBA.)

The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. §16.50j-72(b)(2).



- 1. The proposed modifications will not result in an increase in the height of the existing structure.
- 2. The proposed modification will not require the extension of the site boundary.
- 3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
- 4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
- 5. The proposed modification will not cause a change or alteration in the physical or environmental characteristics of the site.
- 6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-referenced telecommunication facility constitute an exempt modifications under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

G. Scott Shepherd Site Development Specialist II SBA COMMUNICATIONS CORPORATION 134 Flanders Rd., Suite 125 Westborough, MA 01581

508.251.0720 x3804 + T 508.366.2610 + F 508.868.6000 + C GShepherd@sbasite.com

Attachments

Avon Town Hall, 60 West Main St., Avon, CT 06001

Brandon Robertson, Town Manager / with attachments

Avon Town Hall, 60 West Main St., Avon, CT 06001

Brandon Robertson, Town Manager / with attachments

Avon Town Hall, 60 West Main St., Avon, CT 06001

Monte LLC / with attachments

40 Woodland St., Hartford, CT. 06105



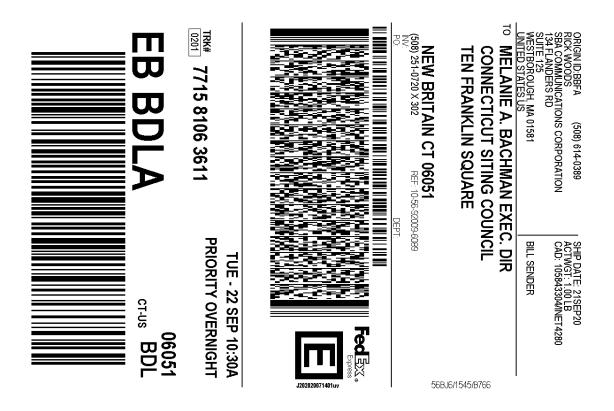
Exhibit List

Exhibit 1	Check Copy	X To Be Invoiced by CSC per Covid 19
		Guidelines
Exhibit 2	Notification Receipts	х
Exhibit 3	Property Card	х
Exhibit 4	Property Map	х
Exhibit 5	Original Zoning Approval	Town of Holland P&Z Commission 11/10/97
Exhibit 6	Construction Drawings	Chappell Engineering 9/4/20
Exhibit 7	Structural Analysis	TES dated 6/30/20
Exhibit 8	Mount Analysis	TES dated 7/8/20
Exhibit 9	EME Report	EBI Consulting 7/9/20

EXHIBIT 1

Normally, Exhibit 1 would contain a copy of the check for the filing fee.

EXHIBIT 2



- 1. Use the 'Print' button on this page to print your label to your laser or inkjet printer.
- 2. Fold the printed page along the horizontal line.
- 3. Place label in shipping pouch and affix it to your shipment so that the barcode portion of the label can be read and scanned.

Warning: Use only the printed original label for shipping. Using a photocopy of this label for shipping purposes is fraudulent and could result in additional billing charges, along with the cancellation of your FedEx account number.



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EXHIBIT 3

—Administrative Informat	: 1 on	

Owner name: MONTE LLC

Second name:

Address: 40 WOODLAND STREET

City/state: HARTFORD CT Zip: 06105

			Locati	.on	Information
Map:	015	Clerk	map:	04	104

CIEIR Map	• 04 104	
Neigh.:	Zone: RU2A	Vol: 455 Page: 057
	Exemptions	Last sale
Amount	Exempt Cat	Amount Sale date: 12-Jan-1987
140,000		Sale price: 460,000
261,560		Sale valid:
		Values
1,020		Mkt value :
2,630		Cost value: 578,871
	Utilities	Sales ratios
405,210	Water Well	Cost/sale : 1.2584
	Sewer Septic	Mkt/sale :
405,210	Gas None	Assmt/sale: .8809
	Neigh.: Amount 140,000 261,560 1,020 2,630 405,210	Neigh.: Zone: RU2A

Land Information

Type	Use	Acres/SqFt	Rate	Total	Infl Fact	Value	70% Value
PRIM	11	2.000	400,000	400,000	.50	200,000	140,000
Primary	Site	87,120					
RES	12	.500	7,500	3,750		3,750	2,625
Residual	1	21,780					
		0 500				000 550	140 605
		2.500	acres	Total	land value	203,750	142,625

Residential Dwelling Information

Subject	Code	Description	Con	ndon	ninium	
Style	02	Cape				
Exterior Walls	01	Clapboards				
Roof Material	01	Asphalt Shingles	Story	Неі	ight 1.5	
Roof Type	01	Gable				
Foundation	01	Poured Concrete	Total Rooms	8	Garage cars	3
Interior Walls	02	Drywall	Bedrooms	4	Unfinished area	
Floors	01	Hardwood	Family Rooms	1	Dormer linear f	
Heating System	02	Forced Hot Air	Full Baths	3	Masonry trim sf	
Fuel	01	Oil	Half Baths	1	Finish bsmt sz	
Attic	99	None	Addtn'l fixtures	3	Rec Room Size	1,380
Grade	40	В	Whirlpools	1	Living area	4,565
Garage	23	Attached 3 car	Saunas		# Living Units	
Area Over Gar.	03	Partial	M/F stacks			
Basement	01	Full	W/B stacks	1		
Bsmt Fin Qual	02	Rec Room w/o air	W/B openings	2		
Air Condition	01	Central Air				
Interior Cond	04	Average				
Exterior Cond	04	Average	Actual Ye	ear	Built: 1955	

Building Valuation Summary

Dwelling	Frame	1 1/2 story w/bsmt 1,671	256,410
Basement Heating	Full Yes	A/C Yes	7,770
		A/C Yes	, -
Plumbing	3 F/B	1 H/B 3 Add'l fix. 1 Wh/p Saunas	13,600
Attic	None	Attic size:	
Additions			186,962
Other Feat	ures	WB Stks RR	29,510
Sub-Total			494,252
Grade	В	Factor 1.2600	622,758
CDU		C&D Factor 1.00	622,758
Depreciati	on	40 %	373,655
		Computed cost value @ 70%	261,559

Building additions

Cat	egory	Type		Area	Value
G	Garages	FRL	Attached frame GT 65	704	23,363
L	Living Area	FATT	Full finished attic	352	9,417
L	Living Area	AIR	Air conditioning	352	793
P	Porches, Patios, Decks	FOFF	Frame open first flo	88	3,971
L	Living Area	FRFF	Frame first floor	148	12,550
L	Living Area	AIR	Air conditioning	148	333
L	Living Area	FRFF	Frame first floor	216	18,317
L	Living Area	FRUH	Frame upper half	216	8,182
L	Living Area	BSMT	Basement addition	216	2,948
L	Living Area	AIR	Air conditioning	324	730
L	Living Area	FRFF	Frame first floor	54	4,579
L	Living Area	FRUF	Frame upper full	54	3,349
L	Living Area	AIR	Air conditioning	108	243
L	Living Area	FRFF	Frame first floor	54	4,579
P	Porches, Patios, Decks	FOFF	Frame open first flo	54	2,437
L	Living Area	FRFF	Frame first floor	516	43,757
L	Living Area	FRUF	Frame upper full	516	32,003
L	Living Area	BSMT	Basement addition	516	7,043
L	Living Area	AIR	Air conditioning	1,032	2,324
P	Porches, Patios, Decks	DECK	Wood deck	308	6,044
			Total	additions	186,962

Outbuilding Information

560
1,460

EXHIBIT 4

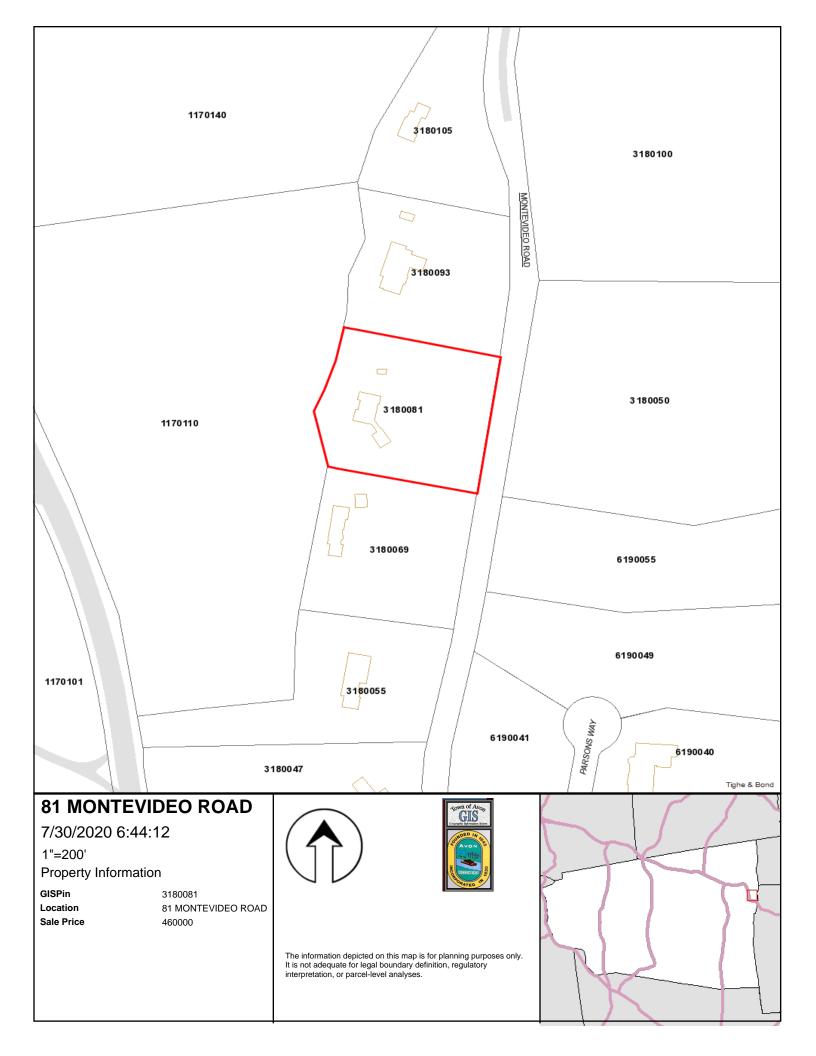


EXHIBIT 5

SITE NAME:	Avon (Montevideo)	SITE	E ID: C	Γ2207	1-A			
Transaction:	Message Center Management, Inc. (MCI	M)				Jihan/Sam Toth		
	ZONING/PERMITTING CO	MPLETIC	ON FORM	<u> </u>				
Address: 81	Montevideo Road, Avon, CT 06001					CT-06		
Jurisdiction:	Connecticut Siting Council - Zoning (current)	y) 2	Zoning Di	strict:	RU2A			
Zoning Approval	Town of Avon - Permitting Zoning Approval Type: Exempt Modification Case #: EM-MCM-004-070824							
			Case #	+ CIV	-IVICIVI-UU	14-070024		
Approval Date:	Approved Height:	150						
Removal E						<u>Yes</u> □		
Site Plan S	Submittal							
Fall Zone								
Periodic In	spections							
Periodic R	eporting							
Approval F								
Additional								
Approval is for rep of the existing tow	was approved by Town of Avon zoning agencie ight it under the Connecticut Siting Council's juri lacement of a 150 ft. guyed tower with a 150 ft. er in January of 2007 showed the existing tower e replaced to meet current & future structural sa	isdiction. self-suppo r doesn't m	ort structure	e. A rou	itine & peri	iodic inspection		
Planning/Zoning	:							
Phone:		mail:						
Bldg./Code Enfo	rcement: Susan Gatcomb							
Phone: 8		_	gatcomb	@avor	nct.gov			
Submitted by:	Satches Ostes Zoning Compliance	Date:	3/27/2	2017				
	TO BE COMPLETED BY	Y CORPO	RATE					
			Yes	No	N/A			
Zoning Approval	Attached (required)		\boxtimes					
Building Permit	Attached (required) 08-0916		⊠			Date Recd 3/24/2008		
Certificate of Oc	cupancy or Compliance (CO) attached (req	luired)	\boxtimes			11/3/2008		
Zoning Manager	Approval: Ashley Masuda				Date _	3/28/2017		

Daniel F. Caruso

Chairman

STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

Ten Franklin Square, New Britain, CT 06051 Phone: (860) 827-2935 Fax: (860) 827-2950 E-Mail: siting.council@ct.gov Internet: ct.gov/csc

October 24, 2007

Christopher B. Fisher, Esq. Cuddy & Feder LLP 445 Hamilton Avenue, 14th Floor White Plains, NY 10601

RE: EM-MCM-004-070824 – Message Center Management, Inc. notice of intent to modify an existing telecommunications facility located at 81 Montevideo Road, Avon, Connecticut.

Dear Attorney Fisher:

At a public meeting held on October 16, 2007, the Connecticut Siting Council (Council) acknowledged your notice to modify this existing telecommunications facility, pursuant to Section 16-50j-73 of the Regulations of Connecticut State Agencies with the condition that Message Center Management, Inc. will flag any trees slated for removal in the field and note the same on the construction drawings to be submitted as part of any building permit application.

The proposed modifications are to be implemented as specified here and in your notice dated August 23, 2007 and additional information dated September 28, 2007, including the placement of all necessary equipment and shelters within the tower compound. The modifications are in compliance with the exception criteria in Section 16-50j-72 (b) of the Regulations of Connecticut State Agencies as changes to an existing facility site that would not increase tower height, extend the boundaries of the tower site, increase noise levels at the tower site boundary by six decibels, and increase the total radio frequencies electromagnetic radiation power density measured at the tower site boundary to or above the standard adopted by the State Department of Environmental Protection pursuant to General Statutes § 22a-162. This facility has also been carefully modeled to ensure that radio frequency emissions are conservatively below State and federal standards applicable to the frequencies now used on this tower.

This decision is under the exclusive jurisdiction of the Council. Please be advised that the validity of this action shall expire one year from the date of this letter. Any additional change to this facility will require explicit notice to this agency pursuant to Regulations of Connecticut State Agencies Section 16-50j-73. Such notice shall include all relevant information regarding the proposed change with cumulative worst-case modeling of radio frequency exposure at the closest point of uncontrolled access to the tower base, consistent with Federal Communications Commission, Office of Engineering and Technology, Bulletin 65. Any deviation from this format may result in the Council implementing enforcement proceedings pursuant to General Statutes § 16-50u including, without limitation, imposition of expenses resulting from such failure and of civil penalties in an amount not less than one thousand dollars per day for each day of construction or operation in material violation.

Thank you for your attention and cooperation.

Daniel F. Carnes

Daniel F. Caruso

Chairman

DFC/MP/cm

c: The Honorable Richard W. Hines, Chairman Town Council, Town of Avon Steven V. Kushner, Town Planner, Town of Avon Hans Fiedler, Message Center Management, Inc.

G:\EM\MCM\Avenidc\0\607.DOC

Affirmative Action / Equal Opportunity Employer



August 23, 2007

BY FEDEX - Priority Overnight

Hon. Daniel F. Caruso, Chairman and Members of the Connecticut Siting Council 10 Franklin Square New Britain, Connecticut 06051

Re:

Message Center Management, Inc.

Notice of Exempt Modification

Replacement Tower

81 Montevideo Road, Avon, Connecticut

Dear Chairman and Members of the Council:

On behalf of Message Center Management, Inc. ("MCM"), enclosed please find its notice of exempt modification with respect to the above referenced matter together with a check in the amount of \$500, the filing fee. We respectfully request that this matter be placed on the next Council agenda for acknowledgment. In the interim, should your of the Council's staff have any questions regarding this matter, please do not hesitate to contact us. Thank you.

Very truly yours,

Christopher B. Fisher

Enclosures

cc: Phillip K. Schenck, Avon Town Manager

Steven Kushner, Town Planner

Maria Scotti, MCM Hans Fiedler, MCM

CONNECTICUT SITING COUNCIL

NOTICE OF EXEMPT MODIFICATION BY MESSAGE CENTER MANAGEMENT, INC. ("MCM") REGARDING A REPLACEMENT TOWER AT ITS EXISTING FACILITY IN AVON CONNECTICUT

Pursuant to Connecticut General Statutes § 16-50g et. seq., and Section 16-50j-72(b)(3) of the Regulations of Connecticut State Agencies adopted pursuant thereto, Message Center Management, Inc. ("MCM") hereby notifies the Connecticut Siting Council of its intent to modify an existing facility located at 81 Montevideo Road. Avon, Connecticut (the "Avon Facility") by replacing the tower to the same height.

The Existing Avon Tower Facility

The Avon Facility consists of a one hundred fifty (150') foot guyed tower (the "Tower"), building and other improvements located on sizeable parcel of property in the Town of Avon. The Avon Facility is principally used by Omnipoint Communications Inc. ("T-Mobile") and Sprint Spectrum, L.P. ("Sprint") that provide "cellular" services to the public as that term is defined and used in Section 16-50i(a)(6) of the Connecticut General Statutes. The Avon Facility was originally approved by Town of Avon zoning agencies prior to a statewide change in the law in 2001 which subsequently brought it under the Siting Council's jurisdiction.

Reasons for the proposed Tower Replacement

MCM's consulting engineers completed a routine and periodic inspection of the existing Tower in January of 2007, a copy of which is enclosed. As noted therein, the existing tower does not meet current structural standards. As such a recommendation was made to replace the tower along with other interim measures which MCM has since completed. At this time, MCM is proposing to replace the tower to meet current and future structural safety standards.

Replacement Tower

As shown on the enclosed plans prepared by URS Corporation, including a survey, site plan, and tower elevation, MCM proposes replacing the existing 150' guyed tower with a self-support lattice tower maintaining the same height and antenna locations (the "Replacement Tower"). The Replacement Tower will be located immediately adjacent to the existing Tower approximately 15' to the east and will be designed to taper to a uniform tower face for a significant portion of its height above grade. No other antenna or equipment modifications are proposed by MCM.

MCM's Tower Replacement Constitutes An Exempt Modification

The proposed replacement of the existing Tower constitutes an exempt modification of an existing facility as defined in Connecticut General Statutes Section 16-50i(d) and Council regulations promulgated pursuant thereto. Specifically 16-50j-72(b)(3) of the Council's regulations provides that, among other exempt modifications, included is a:

Replacement of an existing CATV tower or telecommunications tower and associated equipment with a tower that is no taller than the tower to be replaced....

Here the Replacement Tower is the same height as the existing Tower and as such the modification is exempt from the requirement for any further processing or approvals.

MCM's Discussions with Town Planning Officials

We note that representatives of MCM have discussed this project with Town of Avon Planning Officials regarding the structural issues and different tower replacement options. As part of those discussions MCM noted for the Town that a replacement guyed tower would require substantial tree clearing at the Avon Facility site. In lieu of same, MCM has elected to replace the tower with a self support structure which will continue to accommodate users of the site and have a minimal impact on tree clearing. For reference purposes, we have also included photosimulations of the existing Tower and proposed Replacement Tower.

Conclusion

MCM requests that the Connecticut Siting Council acknowledge that its proposed Replacement Tower at the Avon Facility meets the Council's exemption criteria specified in Section 16-72(b)(3) of its regulations. We note that no other land use or zoning approvals are required for the project pursuant to Section 16-50x of the Connecticut General Statutes. As such, upon receipt of the Council's acknowledgment, MCM intends to procure signed/sealed tower drawings from the manufacturer of the Replacement Tower and file for a building permit from the Town of Avon.

Respectfully Submitted.

Christopher B. Fisher, Esq.

On behalf of MCM

cc: Phillip K. Schenck, Avon Town Manager Steven Kushner, Town Planner Maria Scotti, MCM Hans Fiedler, MCM





TECTONIC Engineering & Surveying Consultants PC. 955 Little Britain Road New Windsor, NY 12553

(845) 567-8656 FAX: (845) 567-8703 www.tectonicengineering.com

Virginia King Message Center Management 40 Woodland Street Hartford, CT 06105

January 30, 2007

RE: W.O. 3997.07

AVON TOWER UPGRADE 81 MONTEVIDEO ROAD AVON, CT ANALYSIS RESULTS AND RECOMMENDATIONS

Dear Virginia:

As requested, Tectonic Engineering & Surveying Consultants P.C. has completed an inspection and detailed structural analysis of the existing 150' guyed tower at the above referenced site. The overall configuration of the tower is shown in Figure 1, attached.

The tower was inspected by representatives of Tectonic on 11/28/06. Based on our inspection, there are several items of concern with respect to the physical condition of the tower, as follows:

- Significant external corrosion of the tower mast, especially between the 100' and 130' levels.
- Considering the age of the tower and the use of light gauge steel tubing for the tower legs, we anticipate that internal corrosion may be present. Due to the thin walls of the tubing, even moderate corrosion can significantly reduce the structural capacity of the tower legs.
- The bracing members are very small diameter steel rods. Several are bent, which reduces their effectiveness.
- Some of the leg splice bolts are significantly corroded.
- The guys are small diameter and are generally not sufficiently taut.
- The antenna mounts at the 108' level are heavily corroded.
- Numerous existing cables are inadequately secured, and they are not efficiently bundled to minimize wind loading.

This analysis was performed using Revision G of the TIA-222 standard, as previously discussed. We find that the structure is significantly overloaded in its existing condition, despite the fact that the tower was assumed to be in "like-new" condition for the purpose



W.O. 3997.07 Page 2
Avon Tower Upgrade
Avon, CT
Analysis Results and Recommendations

January 30, 2007

of the analysis. In other words, the capacities of the tower members and guys were not adjusted (i.e. reduced) to reflect their actual condition.

As a result of our analysis, we find that:

- The existing tower is unable to withstand the required wind loading of 95 mph (3second gust) with no ice accumulation.
- The maximum wind speed that the tower can safely withstand is less than 60 mph.
- The existing tower cannot support the required ice loading, even with no wind load acting on it at all.

The primary reasons for the large degree of overstress are:

- The small size and limited capacity of the leg and bracing members, as well as the guys.
- The inclusion of a topographic factor based on the site location, as required by TIA-222-G.
- c. The larger ice thickness required by TIA-222-G, compared to the previous version of the standard.

We note that previous Structural Analysis reports by Tectonic and at least two (2) other firms show that there were problems related to the capacity of the tower under Revision F of the TIA-222 standard.

Since no information on the existing tower foundation and guy anchors was available, we could not assess their actual capacities. Based on the large overstress in the tower mast and guys, we anticipate that the existing foundations may not have sufficient capacity to resist the required loads.

The tower will need to be upgraded to satisfy the current code requirements, and to provide capacity for modified antenna configurations in the future. Reinforcement is expected to involve the installation of heavy external bracing in approximately the lower half of the tower, and replacing the guys at several levels with larger size guy wires and matching hardware. It will also involve modifications to the tower base foundation and all guy anchors.

Although upgrading the tower to meet these requirements may be technically feasible, it may be as costly and disruptive as the construction of a new replacement tower.

We recommend the installation of a new, sturdier tower on a new foundation, and relocation of all existing antennas thereto, as a better alternative. We understand that



W.O. 3997.07 Page 3
Avon Tower Upgrade
Avon, CT
Analysis Results and Recommendations

January 30, 2007

replacement of the structure does bring up other issues, but it will probably be more economical in the long run.

Anticipating that the processes for approval, procurement, and installation of a replacement tower may take a substantial amount of time, we recommend that the following corrective actions be taken as soon as possible:

- 1. Retension all of the guys to be between 8% and 10% of their breaking strength.
- Clean and repaint the deteriorated portions of the tower to minimize further corrosion.
- 3. Bundle and securely fasten the cables to the tower legs or faces.
- Perform a simple visual inspection of the structure after any severe wind or ice storm, to verify that no damage has occurred.

In closing, we foresee no problem with removing the two (2) existing T-Mobile panel antennas that are mounted at the 138' level, and reinstalling one (1) panel antenna at a lower elevation, as suggested.

Please contact me if there are any questions on the above.

Sincerely,
TECTONIC

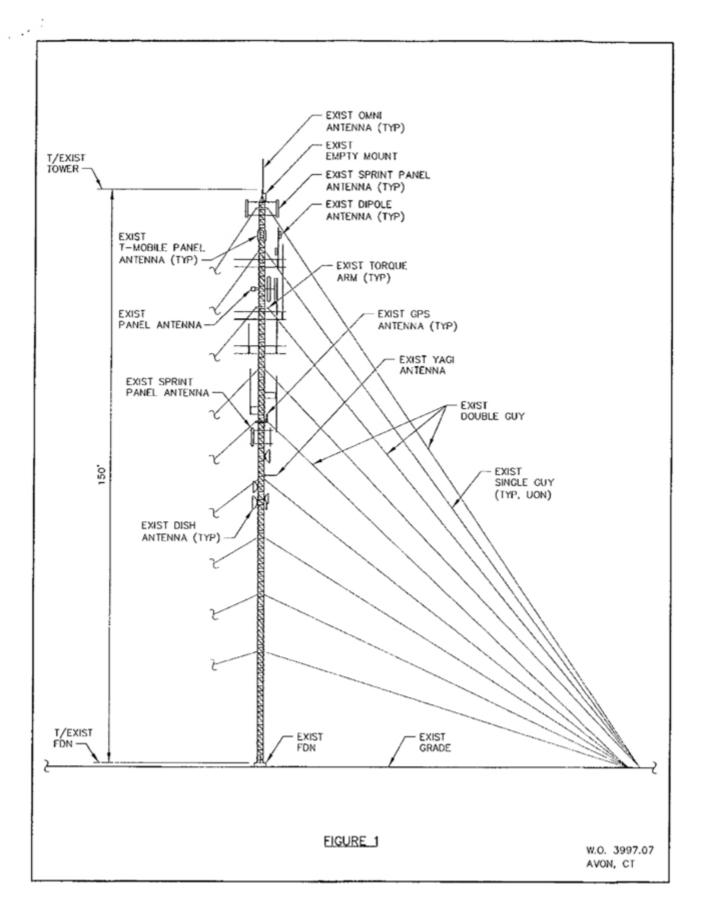
Jeffrey B. Kirby, P.E.

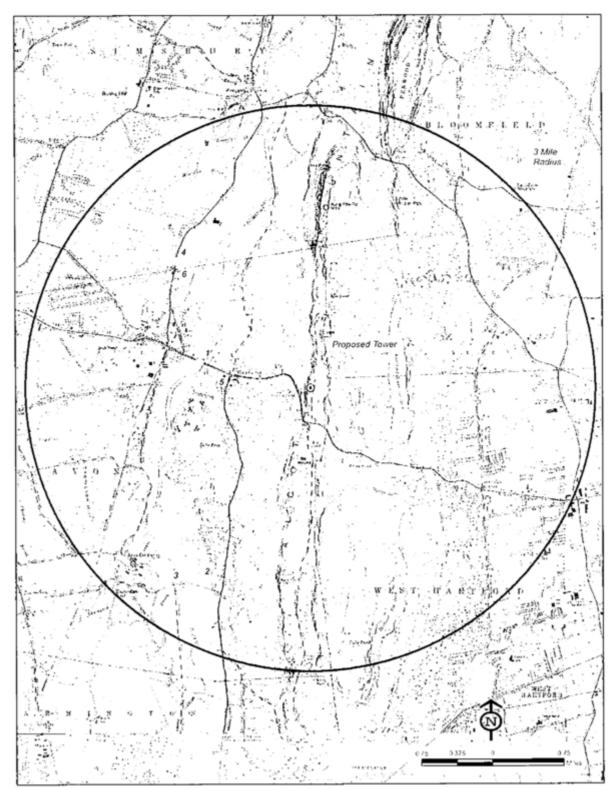
Chief Structural Engineer

No. 21291

CENSE

file AvonTowerUpgradeLtr.doc

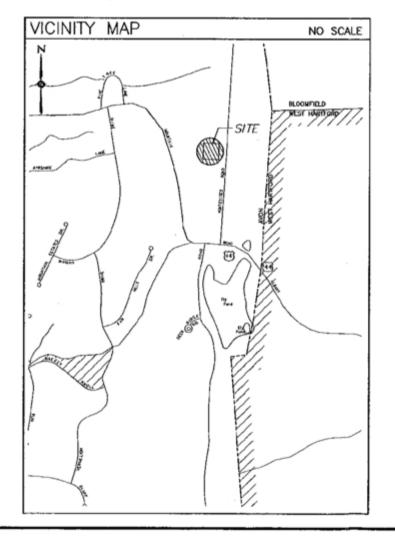




MESSAGE CENTER MANAGEMENT

AVON TOWER REPLACEMENT

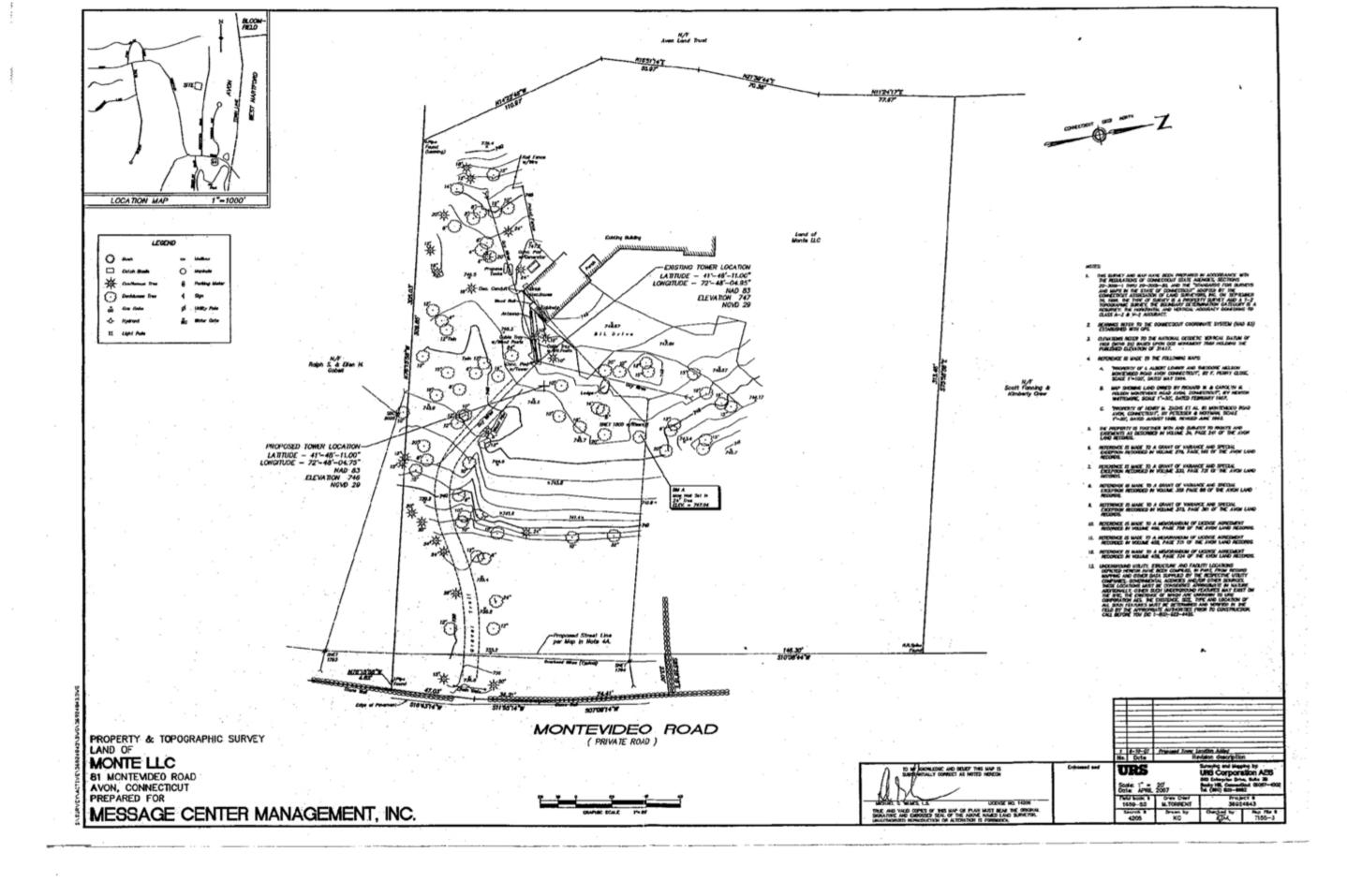
81 MONTEVIDEO ROAD AVON, CONNECTICUT



PROJECT SUMMARY MESSAGE CENTER MANAGEMENT 40 WOODLAND STREET HARTFORD, CONNECTICUT *URS CORPORATION AES* 500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT SURVEYOR: LEGEND DESCRIPTION PROJECT NO: 36924843 MCM 007 CHECKED BY: 0 08/08/07 REVIEW 1 08/10/07 FBML ABBREVIATIONS VERIFY IN RELD OH CENTER POUND/SQUARE FOOT TYPICAL FEET SQ.FI. SQUARE FEET AVON 81 MONTEVIDEO ROAD AVON, CONNECTICUT SHEET INDEX SCALE: SHT. TITLE SHEET-GENERAL NOTES TITLE SHEET - GENERAL MOTES AND LEGENDS AND LEGENDS S-1

PARTIAL SITE PLAN AND TOWER ELEVATIONS

T-1



SEDIMENTATION CONTROL FENCE SPECIFICATIONS SILT FENCES SHALL BE INSPECTED HANESWIFLY AFTER EACH RAWFALL AND AT LEAST DAILY DURING PROLONGED RAWFALL ANY REPAIRS THAT ARE REQUIRED SHALL BE MADE IMMEDIATELY. Avan Land Trust F THE FARROC ON A SILT FENCE SHOULD DECOMPOSE OR BECOME INEFFECTIVE BURNET THE EXPECTED LIFE OF THE FENCE, THE FABRIC SHALL BE REPLACED PROMPLY. SEDIMENT DEPOSITS SHOULD BE INSPECTED AFTER EVERY STORM EVENT, THE BEPOSITS SHOULD BE RICHONED WHEN THEY REACH APPROXIMATELY ONE—HALF THE HEIGHT OF THE BARRIER. SEDIMENT DEPOSITS THAT ARE REMOVED OR LEFT IN PLACE AFTER THE FAIRING HAS BEEN REMOVED SHALL BE GRADED TO CONFORM WITH THE EXISTING TOPOGRAPHY AND VEGETATION. CONSTRUCTION SEQUENCE 1. THE GEOTOCILE FARRIC SHALL WEST THE DESIGN ORIGERA FOR SLT FENCES THE FABRIC SHALL BE EMBEDGED A MINIMUM OF 8 INCHES INTO THE GROUND AND THE SOIL COMPACTED OVER THE EMBEDDED FABRIC. WOMEN WIRE FEMCES SHALL BE FASTENED SECURELY TO THE FENCE POSTS. WITH WIRE TIES OR STAPLES. FILTER CLOTH SHALL BE FASTENED SECURELY TO THE WOVEN WIRE FENCE WITH THES SPACED EVERY 24 INCHES AT THE TOP, MID—SECTION, AND BOTTON. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER, THEY SHALL BE CVENUAPPED BY 8 INCHES, FOLDED AND STAPLED. 6. FONCE POSTS SHALL BY A MINIMUM OF 35 INCHES LONG AND DRIVEN A MINIMUM OF 16 NOVIES INTO THE CROWN, WOOD POSTS SHALL BY OF SOUND QUALITY HARDWOOD AND SHALL HAVE A MINIMUM CROSS SECTIONAL AREA OF 3.0 SQUARE BICHES. MAINTENANCE SHALL BE PERFORMED AS HEEDED TO PREVIOUT BULGES IN THE SILT FENCE DUE TO DEPOSITION OF SEDIMENT. I. DURNIC CONSTRUCTION AND THEREAFTER EROSION CONTROL MEASURES ARE TO BE INPLEMENTED AS NOTED. NOT GREATER THAN BO, DOD SQ. FT. OF LAND SHALL BE EXPOSED AT ANY ONE TWO BUNNION DEVELOPMENT. MHEAL HAND IS EXPOSED DURING DEVELOPMENT, THE COPOSIDE SHOULD BE KEPT TO THE SHORTEST PRINCIPOL. PERIOD OF TIME AND SHALL HOT EXCEED BO DAYS, LAND SHOULD NOT BE LEFT DRYSCO DURING THE HINTER MONTES. EXISTING BUILDING Land of Monte LLC 簽 SILTATION FENCING SHALL BE INSTALLED WHERE SHOWN PRIOR TO ANY ON SITE GRADING OR INSTANSANCE OF EXISTING SURFACE MATERIAL, IT SHOULD BE MANTAINED DURING AND AFTER DEVELOPMENT TO REDUCE SEDMENT FROM MADDET WATER AND FROM LAND UNDERSCONE OPERLOPMENT, WHERE POSSIBLE INSTANCE INDINNECT—WAYE SHOULD BE UTBLZED AND LETT OPEN TO REMOVE EXCESS SURFACE WATER. EXISTING TOWER LOCATION LATITUDE - 41'-48'-11.00" LONGITUDE - 72'-48'-04.95" NAD 83 ELEVATION 747 ALL DISTURBED AREAS AND SIDE SLOPES WHICH ARE FINISH GRADED WITH NO FLIKTHER CONSTRUCTION TO TAKE PLACE SHALL BE LOAMED AND SEEDED. A MINIMUM OF 4" OF LOAM SHALL BE INSTALLED. CONSTRUCTION-REFER TO 2/SC-1 NGVD 29 4. ANY DISTURBED AREAS WHICH ARE TO BE LEFT TEMPORARLY, AND WHICH WILL BE REGRADED LAFER DURING CONSTRUCTION SHALL BE MACHINE HAY MULCHED AND SEEDED WITH RYS GRASS TO PREVENT EROSON. HAY OR STRAW MULCH SHALL BE APPUED IN ALL RESHALL BE LONG AT A MATE OF 2 TONS PER ACRE. BALLS SHALL BE UNSPOLLED, AR-DISED, AND FREE FROM WIED, SEEDS AND ANY COARSE MATERIA. Ralph S. & Ellen H. Gobell APPROXIMATE LOCATION OF SEPIC TANK. N/F Scott Fanning & Kimberly Crew DRAWN BY: PROPERTY LINE (TYP.) 739.3 APPROXIMATE LOCATION OF DISTRIBUTION BOX (TYP.) SEMER LINE (TYP.) R.R.Spike Found 146.30' 510'08'44"# Oranhand Wires (7)pind) ATTACH FILTER FABRIC TO THE WIRE FENCING AND EXTEND IT TO THE COMPACTED BACKFILL — MONTEVIDEO ROAD (PRIVATE ROAD) SEDIMENTATION CONTROL BARRIER - SILT FENCE SITE PLAN SC-2 SCALE: N.T.S. SC-1 SCALE: 1" = 20"-0"

MESSAGE CENTER MANAGEMENT

40 WOODLAND STREET HARTFORD, CONNECTICUT 06105

BRS CORPORATION AES

500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT

OF CONNEC

PROJECT NO: 36924843

MCM 007

RRH

CHECKED BY:

ISSUED FOR 0 08/08/07 REMEN 1 08/10/07 FINAL

AVON

81 MONTEVIDEO ROAD AYON, CONNECTICUT

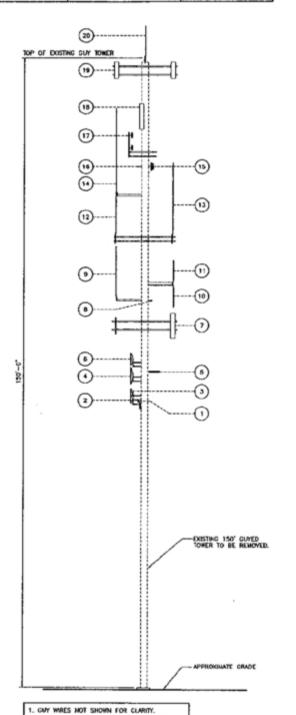
SCALE:

SITE PLAN AND SEDIMENTATION DETAILS

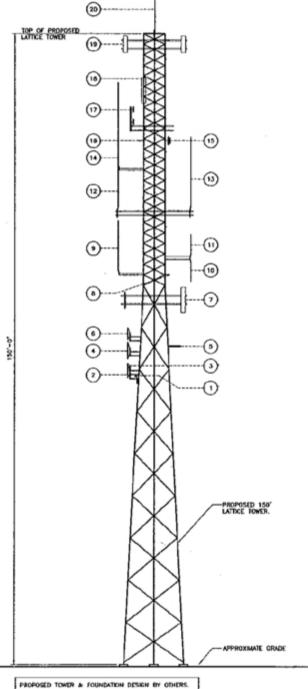
AS NOTED

SC-1

LEGEND						
DESCRIPTION	DISTING	PROPOSED				
PROPERTY LINE						
LEASE LINE						
CHAIN LINK FENCE		×				
CONTOUR LINES						
UNDERGROUND UTILITIES		E/T				
UTILITY POLE	ø	ø				
TREE LINE	**********					
SEDIMENTATION FENCE		h				







PROPOSED TOWER ELEVATION





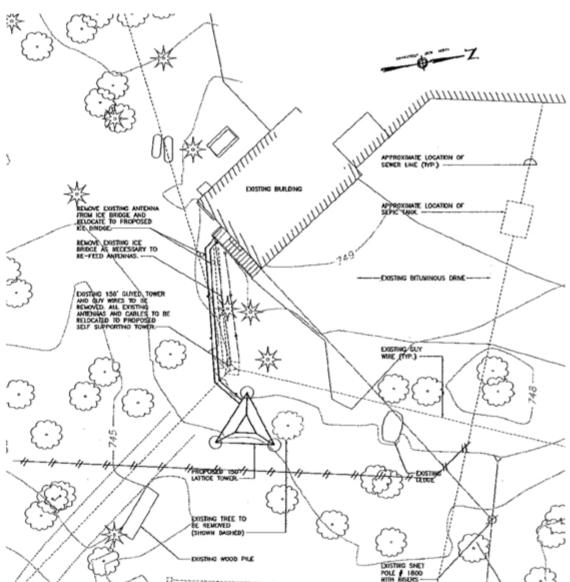
ANTENNA INFORMATION

- ANTENNA: LEG MOUNTED CPS ELEVATION: (AGL) 68'-0"
- 2 ANTENNA: 3" SOLID DISH ELEVATION: (AGL) 69"-0"
- 3 ANTENNA: 2" SOUD DISH ELEVATION: (AGL) 70"-0"
- ANTENNA: 4" SOLID DISH ELEVATION: (AGL) 74'-0"
- S ANTENNA: (1) YAGI ON 3' SIDE ARM ELEVATION: (AGL) 75"-6"
- 6 ANTENNA: 3" SOUD DISH ELEVATION: (AGL) 78"-0"
- 7 ANTENNA: (1'46') PANEL ANTENNA ON 6" SIDE ARM ELEVATION: (AGL) 86"-0"
- ANTENNA: LES MOUNTED GPS
 ELEVATION: (AGL) 92'-0"
- (9) ANTENINA: 12' WHIP ANTENINA ON A 6'-D" SIDE ARM ELEVATION: (AGL) 93'-0"
- (10) AMTERINA: 8" WHIP ANTENNA INVESTED ON EXISTING SIDE ARM
 ELEVATION: (AGL.) 96"-9"

SHOTTAMOORIN, ANKITTHA

- 11) ANTENNA: 5' WHIP ANTENNA ON A 6'-0" SIDE ARM ELEVATION: (ACL) 98'-0"
- FLENATION (ACL) 108'-0" SIDE AND FLENATION (ACL) 108'-0"
- (13) ANTENNA: 17" WHP ANTENNA ON A 6'-0" SIDE ARM ELEVATION: (ACL) 108'-0"
- ELEVATIONS (ACL) 118'-0"
- (1) DB225 ON 6' SIDE ARM ELEVATION (ACL) 124'-0"
- (1) DB871H105 PANEL ANTENNA ON 3' SIDE ARM ELEVATIONE (AGL) 124'-0"
- (17) ANTENNA: (1) DB222 ON 3' SIDE ARM ELENATION: (ACL) 130'-0"
- (B) ANTENNA: (2) APXV18-208513-C PANEL ANTENNAS ON (2) 6' SIDE ARM ELEVATION: (AGL) 136° -0"
- (19) ANTENNA: (3) 7187-05 PANEL ANTENNAS ON (3) 6" SDE ARM ELEVATION: (AGL) 147'-0"
- 20 ANTENNA: (1) 8" WHF ANTENNA (LEG MOUNTER)

NOTE: ALL MEASUREMENTS ARE ABOVE GROUND LEVEL.



PARTIAL SITE PLAN SCALE: 1" = 10'-0"



MESSAGE CENTER MANAGEMENT

40 WOODLAND STREET HARTFORD, CONNECTICUT 06105

URS CORPORATION AES

500 ENTERPRISE DRIVE ROCKY HILL, CONNECTICUT 1-(860)-629-8882



PROJECT NO: 36924843

JOB NO: MCM 007

DRAWN BY:

CHECKED BY:

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ı	0	08/08/07	REVIEW					
ı	1	08/10/07	FINAL.					
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AVON

81 MONTEVIDEO ROAD AVON, CONNECTICUT

SCALE: AS NOTED

PARTIAL SITE PLAN AND TOWER ELEVATION

SC-2

Town of Avon, Conn.

This card must be posted and visible from the road

08-0916

30.02.02

Q- Willmaner!



DISTRIBUTION:

ORIGINAL: OWNER

CERTIFICATE OF APPROVAL

TOWN OF AVON

Tel. 860.409.4316 Fax 860.409.4321 60 West Main Street Avon Connecticut 06001-3743

LOCATION OF JOB	GIS NO.	ZONE	TYPE OF PERMIT		
81 MONTEVIDEO ROAD	3180081	RU2A	BUILDING, ELECTRICAL		
OWNER	STREET		CITY	STATE & ZIPCODE	
MONTE LLC	40 WOODLAND STREET		Γ HARTFORD	CT 06105	
THIS IS TO CERTIFY THAT REPLACEMENT OF EXISTING 150FT. TELECOMMUNICATIONS TOWER AND FENCE					
DONE UNDER PERMIT #	08-1405.08-0	0916.08-0	941 ISSUED 7/3/08 3/2	4/08 3/13/08	
	377 (1105,000	0,710,000	100000 110100.512	111/0(3/13/00	
SUBSTANTIALLY COMPLIES WITH THE STATE OF CONNECTICUT BUILDING CODE IN EFFECT					
DECEMBER 31, 2005, AND IS HEREBY APPROVED.					
Decimal 1, 2003, And is tilled I All ROYED.					
CONDITIONS OF APPROVAL: NONE					
Zoning Approval Spendicus 6-30-08 FIRE MARSHAL APPROVAL MA Engineering Dept. Approval LTP 11/3/08 Wetlands Approval					

COPY: ASSESSOR

COPY: BUILDING DEPT.

Final Report of Special Inspections

Project:

Message Center Management: MCM-007 / 36924843

Location:

81 Montevideo Road, Avon, Connecticut 06001

Owner:

Message Center Management

Owner's Address:

40 Woodland Street

Hartford, CT 06105

Architect of Record: URS Corporation

Structural Engineer of Record:

Valmont Structures-Pirod, Inc.

1545 Pidco Drive, Plymouth, Indiana 46563

To the best of my information, knowledge and belief, the Special Inspections required for this project, and itemized in the Statement of Special Inspections submitted for permit, have been performed and all discovered discrepancies have been reported and resolved other than the following:

Comments:

(Attach continuation sheets if required to complete the description of corrections.)

Interim reports submitted prior to this final report form a basis for and are to be considered an integral part of this final report.

Respectfully submitted,

Valmont Structures-Pirod, Inc., 1545 Pidco Drive Plymouth, Indiana 46563

William R. Heiden III, P.E.

(Type or print name)

Date

Licensed Professional Seal

Final Report of Special Inspections

Agent's Final Report

Project:

Message Center Management: MCM-007 / 36924843

81 Montevideo Road, Avon, Connecticut 06001

Agent:

URS Corporation A.E.S., 500 Enterprise Drive, Rocky Hill, CT 06067

Special Inspector:

URS Corporation

Testing Agency:

JGI Eastern, Inc.

To the best of my information, knowledge and belief, the Special Inspections or testing required for this project, and designated for this Agent in the *Statement of Special Inspections* submitted for permit, have been performed and all discovered discrepancies have been reported and resolved other than the following:

Comments:

(Attach continuation sheets if required to complete the description of corrections.)

Interim reports submitted prior to this final report form a basis for and are to be considered an integral part of this final report.

Respectfully submitted, Agent of the Special Inspector URS Corporation, 500 Enterprise Drive – Suite 3B Rocky Hill, CT 06067

Richard Sambor, P.E.

(Type or print name)

Signature .

Date

No. 9977

Selects

Licensed Professional Seal or Certification



SPECIAL INSPECTION REPORT #1

Date: 05/29/08

Client Name:

Message center Management

Site Address:

81 Montevideo Road, Avon, CT

Site Type:

Construction of new U14.0x150' Valmont Lattice Tower

Site Visit Type:

Special Inspection

Project Number:

36924843.00000 / MCM-007

Date of Visit:

May 21, 2008

Attendees:

Jason Mead - URS Corporation

Ray Bayer - Construction Services of Branford, LLC

Rob Olah, P.E., JGI Eastern, Inc/Terracon (Testing Agency)

Weather:

520 Cloudy, 07:30am

Prepared by:

Jason Mead

Progress / Activities: Foundation Sub-grade and Material Inspection

The following was noted:

- 1. Sub-grade: Sub-grade material corresponded with that identified within the geotechnical report prepared by Clarence Welti, P.E., P.C, dated November 6th, 2007. Material consisted of moraine soils; fine to medium sand. Base was compacted with a hand-maneuvered vibratory compactor. Excavation was dry and free of deleterious materials. Contractor had installed a layer of 3/8" crushed stone at the base of the excavation, per the recommendations of the geotechnical report and was confirmed by JGI. Base of foundation excavation measured 6'-0"+/-. Finished grade shall differentiate by 1 foot vertically from East to West side of the tower base per URS design drawing C-1 and C-2 dated 01/25/08.
- 2. Rebar/Anchors: Rebar inventory was observed and found to be in conformance with the requirements of the Valmont design documents, i.e., size, quantity and material specification (ASTM A615, Grade 60), Rebar was supplied by Barker Steel Company, Inc. Anchor bolt assembly (x3) provided by the tower manufacturer (Valmont).

Virginia King - Message Center Management cc: Jim Maher - Message Center Management James Sansone - Building Official Town of Avon Ray Bayer/John Centore, Construction Services of Branford, LLC William R. Heiden III, P.E Valmont Structures

ICA/AA/CF/Book - URS

URS Corporation 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Tel: 860.529.8882 Fax: 860.529.3991



SPECIAL INSPECTION REPORT #2

Client Name:

Message center Management

Site Address:

81 Montevideo Road, Avon, CT

Site Type:

Construction of new U14.0x150' Valmont Lattice Tower

Site Visit Type:

Special Inspection

Project Number:

36924843.00000 / MCM-007

Date of Visit:

May 27, 2008

Attendees:

Jason Mead - URS Corporation

Ray Bayer - Construction Services of Branford, LLC Fred Hart - JGI Eastern, Inc/Terracon (Testing Agency)

Jim Maher - Message Center Management

James Sansone - Building Official - Town of Avon

Weather:

82⁰ Sunny, 12:00noon

Prepared by:

Jason Mead

Progress / Activities: Rebar Inspection and Concrete Placement

The following was noted:

- 1. Rebar/Anchors: Rebar installation was observed and found to be in conformance with the requirements of the Valmont design documents, i.e., size, quantity, spacing and material specification (ASTM A615, Grade 60). Rebar was supplied by Barker Steel. Precast masonry blocks were utilized to attain 3" min bottom cover. Type 26, #5 standees were utilized in accordance with the Valmont design documents to support the top temperature steel from the bottom flexural reinforcement (main bars). Twelve (12) #12 vertical L bars were installed at each pier location and secured at top with one (1) #4 tie. Remaining ties shall be installed once main footing concrete has initially cured. URS noticed that the design documents prepared by Valmont did not include a provision for a minimum of two (2) #4 ties within the top 5in of the pier/column s, per ACI 318 Section 7.10.5.6. URS contacted Valmont to discuss discrepancy. Valmont concurred with URS that an additional tie shall be required. URS notified G.C and building official of this change. Anchor bolt assemblies (x3) were in place and leveled by laser.
- Concrete Placement: Concrete specification utilized was 4000psi. Min design requirement was 3000psi. URS observed six deliveries out of a total of seven and received batch slips. First concrete delivery arrived at 1:25pm and concrete was placed approximately every 30 minutes thereafter.

URS Corporation 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Tel: 860.529.8882 Fax: 860.529.3991

Date: 05/29/08



Concrete Placement continued:

Date: 05/29/08

Concrete was vibrated and evenly distributed. Slump tests and cylinder samples were performed by JGI Eastern, results of which shall be provided under separate cover. A seventh concrete delivery was required to finish the mat pour. Concrete top surface was leveled. Finished concrete was reportedly covered with a tarpaulin to prevent anticipated rain infiltration. URS departed from site at approximately 3:30pm.

cc:

Virginia King – Message Center Management
Jim Maher – Message Center Management
James Sansone – Building Official Town of Avon
Ray Bayer/John Centore, Construction Services of Branford, LLC
William R. Heiden III, P.E Valmont Structures
ICA/AA/CF/Book - URS



SPECIAL INSPECTION REPORT #3

Date: 05/29/08

Client Name:

Message center Management

Site Address:

81 Montevideo Road, Avon, CT

Site Type:

Construction of new U14.0x150' Valmont Lattice Tower

Site Visit Type:

Special Inspection

Project Number:

36924843.00000 / MCM-007

Date of Visit:

May 28, 2008

Attendees:

Jason Mead - URS Corporation

Ray Bayer - Construction Services of Branford, LLC Jeff Chapo JGI Eastern, Inc/Terracon (Testing Agency)

Jim Maher - Message Center Management

James Sansone - Building Official - Town of Avon

Weather:

65⁰ Sunny, 11:00am

Prepared by:

Jason Mead

Progress / Activities: Concrete Placement (Three piers)

The following was noted:

Concrete Placement: Sonotube forms were installed and adjusted to maintain 3" min side cover from pier vertical rebar. Anchor bolts were checked for alignment and clearance. Two #4 binder ties installed within top 5" per ACI 318 Section 7.10.5.6 and 6" o.c thereafter, for a total of seven (7). Unitex Pro Poxy 204 medium viscosity, multi purpose two component epoxy bonding adhesive was applied to the hardened mat concrete prior to placing of pier concrete. Concrete specification utilized was 4000psi. Min design requirement was 3000psi. Concrete placement consisted of one delivery of approximately 6 cu yds. Batch slip checked for conformance and retained by G.C and JGI Eastern/Terracon. Concrete delivery arrived at 12:10pm. Concrete was placed and evenly distributed. Slump tests, cylinder samples and an air entrainment test were conducted by JGI Eastern, results of which shall be provided under separate cover. Concrete surface was floated and crowned to drain. All three pier concrete placement completed by 1:10pm. URS departed from site at 1:20pm.

cc:

Virginia King - Message Center Management Jim Maher - Message Center Management James Sansone - Building Official Town of Avon Ray Bayer/John Centore, Construction Services of Branford, LLC William R. Heiden III, P.E Valmont Structures

ICA/AA/CF/Book - URS

URS Corporation 500 Enterprise Drive, Suite 3B Rocky Hill, CT 06067 Tel: 860.529.8882 Fax: 860.529.3991

EXHIBIT 6

81 MONTEVIDEO ROAD

AVON, CT 06001

HARTFORD COUNTY

SITE NO.: CT11284A

SITE TYPE: 150' SELF-SUPPRT TOWER

RF DESIGN GUIDELINE: 67D5A992DB OUTDOOR

APPROVALS ZONING/SITE ACQ.: PROJECT MANAGER: DATE: DATE: **CONSTRUCTION:** DATE: DATE: **OPERATIONS:** RF ENGINEERING: DATE: DATE: TOWER OWNER:

-MOBILE TECHNICIAN SITE SAFETY NOTES

LOCATION SPECIAL RESTRICTIONS SECTOR A: ACCESS BY CERTIFIED CLIMBER SECTOR B: ACCESS BY CERTIFIED CLIMBER SECTOR C: ACCESS BY CERTIFIED CLIMBER SECTOR D: ACCESS BY CERTIFIED CLIMBER

GPS/LMU: UNRESTRICTED RADIO CABINETS: UNRESTRICTED PPC DISCONNECT: UNRESTRICTED MAIN CIRCUIT D/C: UNRESTRICTED NIU/T DEMARC: UNRESTRICTED

OTHER/SPECIAL: NONE

GENERAL NOTES

- THE CONTRACTOR SHALL GIVE ALL NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY, MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS, AND LOCAL AND STATE JURISDICTIONAL CODES BEARING ON THE PERFORMANCE OF THE WORK. THE WORK PERFORMED ON THE PROJECT AND THE MATERIALS INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS. AND ORDINANCES.
- THE ARCHITECT/ENGINEER HAVE MADE EVERY EFFORT TO SET FORTH IN THE CONSTRUCTION AND CONTRACT DOCUMENTS THE COMPLETE SCOPE OF WORK. THE CONTRACTOR BIDDING THE JOB IS NEVERTHELESS CAUTIONED THAT MINOR OMISSIONS OR ERRORS IN THE DRAWINGS AND OR SPECIFICATIONS SHALL NOT EXCUSE SAID CONTRACTOR FROM COMPLETING THE PROJECT AND IMPROVEMENTS IN ACCORDANCE WITH THE INTENT OF THESE DOCUMENTS.
- THE CONTRACTOR OR BIDDER SHALL BEAR THE RESPONSIBILITY OF NOTIFYING (IN WRITING) THE OMNIPOINT REPRESENTATIVE OF ANY CONFLICTS, ERRORS, OR OMISSIONS PRIOR TO THE SUBMISSION OF CONTRACTOR'S PROPOSAL OR PERFORMANCE OF WORK. IN THE EVENT OF DISCREPANCIES THE CONTRACTOR SHALL PRICE THE MORE COSTLY OR EXTENSIVE WORK, UNLESS DIRECTED IN WRITING OTHERWISE.
- THE SCOPE OF WORK SHALL INCLUDE FURNISHING ALL MATERIALS, EQUIPMENT, LABOR AND ALL OTHER MATERIALS AND LABOR DEEMED NECESSARY TO COMPLETE THE WORK/PROJECT AS DESCRIBED
- THE CONTRACTOR SHALL VISIT THE JOB SITE PRIOR TO THE SUBMISSION OF BIDS OR PERFORMING WORK TO FAMILIARIZE HIMSELF WITH THE FIELD CONDITIONS AND TO VERIFY THAT THE PROJECT CAN BE CONSTRUCTED IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.
- THE CONTRACTOR SHALL OBTAIN AUTHORIZATION TO PROCEED WITH CONSTRUCTION PRIOR TO STARTING WORK ON ANY ITEM NOT CLEARLY DEFINED BY THE CONSTRUCTION DRAWINGS/CONTRACT DOCUMENTS.
- THE CONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS ACCORDING TO THE MANUFACTURER'S/VENDOR'S SPECIFICATIONS UNLESS NOTED OTHERWISE OR WHERE LOCAL CODES OR ORDINANCES
- THE CONTRACTOR SHALL PROVIDE A FULL SET OF CONSTRUCTION DOCUMENTS AT THE SITE UPDATED WITH THE LATEST REVISIONS AND ADDENDUMS OR CLARIFICATIONS AVAILABLE FOR THE USE BY ALL PERSONNEL INVOLVED WITH THE PROJECT.
- THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE PROJECT DESCRIBED HEREIN. THE CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES AND FOR COORDINATING ALL PORTIONS OF THE WORK UNDER THE CONTRACT.
- 10. THE CONTRACTOR IS RESPONSIBLE FOR PROVIDING ALL NECESSARY CONSTRUCTION CONTROL SURVEYS, ESTABLISHING AND MAINTAINING ALL LINES AND GRADES REQUIRED TO CONSTRUCT ALL IMPROVEMENTS AS SHOWN HEREIN.

- 11. THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING ALL PERMITS AND INSPECTIONS WHICH MAY BE REQUIRED FOR THE WORK BY THE ARCHITECT/ENGINEER, THE STATE, COUNTY OR LOCAL GOVERNMENT AUTHORITY.
- 12. THE CONTRACTOR SHALL MAKE NECESSARY PROVISIONS TO PROTECT EXISTING IMPROVEMENTS, EASEMENTS, PAVING, CURBING, ETC. DURING CONSTRUCTION. UPON COMPLETION OF WORK, THE CONTRACTOR SHALL REPAIR ANY DAMAGE THAT MAY HAVE OCCURRED DUE TO CONSTRUCTION ON OR ABOUT THE PROPERTY.
- 13. THE CONTRACTOR SHALL KEEP THE GENERAL WORK AREA CLEAN AND HAZARD FREE DURING CONSTRUCTION AND DISPOSE OF ALL DIRT, DEBRIS, RUBBISH AND REMOVE EQUIPMENT NOT SPECIFIED AS REMAINING ON THE PROPERTY. PREMISES SHALL BE LEFT IN CLEAN CONDITION AND FREE FROM PAINT SPOTS, DUST, OR SMUDGES OF
- 14. THE CONTRACTOR SHALL COMPLY WITH ALL OSHA REQUIREMENTS AS THEY APPLY TO THIS PROJECT.
- 15. THE CONTRACTOR SHALL NOTIFY THE PROJECT OWNER'S REPRESENTATIVE WHERE A CONFLICT OCCURS ON ANY OF THE CONTRACT DOCUMENTS. THE CONTRACTOR IS NOT TO ORDER MATERIAL OR CONSTRUCT ANY PORTION OF THE WORK THAT IS IN CONFLICT UNTIL CONFLICT IS RESOLVED BY THE LESSEE/LICENSEE
- 16. THE CONTRACTOR SHALL VERIFY ALL DIMENSIONS, ELEVATIONS, PROPERTY LINES, ETC. ON THE JOB.
- 17. ALL UNDERGROUND UTILITY INFORMATION WAS DETERMINED FROM SURFACE INVESTIGATIONS AND EXISTING PLANS OF RECORD. THE CONTRACTOR SHALL LOCATE ALL UNDERGROUND UTILITIES IN THE FIELD PRIOR TO ANY SITE WORK.

AT LEAST 72 HOURS PRIOR TO DIGGING, THE CONTRACTOR IS **REQUIRED TO CALL DIG SAFE AT 811**



SCALE: 1" = 1000' - 0"

DO NOT SCALE DRAWINGS

CONTRACTOR SHALL VERIFY ALL PLANS AND EXISTING DIMENSIONS AND CONDITIONS ON THE JOB SITE AND SHALL IMMEDIATELY NOTIFY THE PROJECT OWNER'S REPRESENTATIVE IN WRITING OF DISCREPANCIES BEFORE PROCEEDING WITH THE WORK OR BE RESPONSIBLE FOR SAME.

SHEET INDEX

SHEET NO.	DESCRIPTION	REV. NO.
T-1	TITLE SHEET	1
GN-1	GENERAL NOTES	1
A-1	COMPOUND & EQUIPMENT PLANS	1
A-2	TOWER ELEVATION & ANTENNA PLANS	1
A-3	ANTENNA DETAILS	1
A-4	EQUIPMENT DETAILS	1
E-1	ELECTRIC & GROUNDING DETAILS	1

SPECIAL ZONING NOTE: BASED ON INFORMATION PROVIDED BY T-MOBILE REGULATORY COMPLIANCE PROFESSIONALS AND LEGAL COUNSEL, THIS TELECOMMUNICATIONS EQUIPMENT DEPLOYMENT IS CONSIDERED AN <u>ELIGIBLE FACILITY</u> UNDER THE MIDDLE CLASS TAX RELIEF AND JOB CREATION ACT OF 2012, 47 USC 1455(A), SECTION 6409(A), AND IS SUBJECT TO AN ELIGIBLE FACILITY REQUEST, EXPEDITED REVIEW, AND LIMITED/PARTIAL ZONING PRE-EMPTION FOR LOCAL DISCRETIONARY PERMITS (VARIANCE, SPECIAL PERMIT, SITE PLAN REVIEW, OR ADMINISTRATIVE REVIEW).

SITE NOTES

- THIS IS AN UNMANNED AND RESTRICTED ACCESS TELECOMMUNICATION FACILITY, AND IS NOT FOR HUMAN HABITATION. IT WILL BE USED FOR THE TRANSMISSION OF RADIO SIGNAL FOR THE PURPOSE OF PROVIDING PUBLIC CELLULAR SERVICE.
 - ADA COMPLIANCE NOT REQUIRED.
- POTABLE WATER OR SANITARY SERVICE IS NOT REQUIRED.
- NO OUTDOOR STORAGE OR ANY SOLID WASTE RECEPTACLES REQUIRED.
- ARCHITECT/ENGINEER PLACE THE RESPONSIBILITY ON THE CONTRACTOR TO CORRECT THE DISCREPANCIES AT THE CONTRACTOR'S EXPENSE.
- NEW CONSTRUCTION WILL CONFORM TO ALL APPLICABLE CODES AND ORDINANCES.
- BUILDING CODE: 2018 CONNECTICUT STATE BUILDING CODE
- ELECTRICAL CODE: 2017 NATIONAL ELECTRICAL CODE
- STRUCTURAL CODE: TIA/EIA-222-G STRUCTURAL STANDARDS FOR ANTENNA SUPPORTING STRUCTURES AND ANTÉNNAS.

PROJECT SUMMARY

SITE NUMBER:	CT11284A	L*	1	KUVI
SBA SITE NUMBER:	CT22071-A			
SBA SITE NAME:	AVON (MONTEVIDEO)	RE	₹V.	DA
SITE ADDRESS:	81 MONTEVIDEO ROAD AVON, CT 06001			
PROPERTY OWNER:	MONTE LLC. 40 WOODLAND STREET HARTFORD, CT 06105			
TOWER OWNER:	SBA TOWERS, LLC 8501 CONGRESS AVENUE BOCA RATON, FL 33487 PHONE: 561-226-9523	1	-	09/03 07/20
COUNTY:	HARTFORD			

ZONING DISTRICT: RU2A (RURAL RESIDENTAIL) STRUCTURE TYPE: SELF-SUPPRT TOWER

STRUCTURE HEIGHT: 150'±

STRUCTURAL ENGINEER:

APPLICANT: T-MOBILE NORTHEAST LLC 15 COMMERCE WAY, SUITE B NORTON, MA 02766

SBA RSM: STEPHEN ROTH PHONE: 860-539-4920

ARCHITECT: CHAPPELL ENGINEERING ASSOCIATES, LLC. 201 BOSTON POST ROAD WEST, SUITE 101

MARLBOROUGH, MA 01752 CHAPPELL ENGINEERING ASSOCIATES, LLC.

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MARLBOROUGH, MA 01752 SITE CONTROL POINT: LATITUDE: N.41.8031° (41° 48′ 11.00″)

LONGITUDE W.72.8013* (72* 48' 04.69")

201 BOSTON POST ROAD WEST, SUITE 101

T-MOBILE NORTHEAST LLC

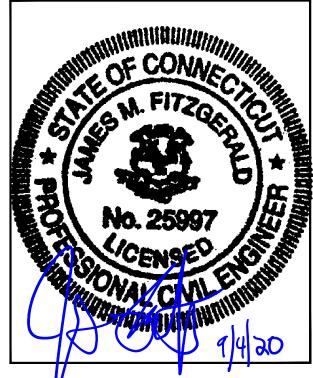
15 COMMERCE WAY, SUITE B NORTON, MA 02766 (508) 286-2700



SBA COMMUNICATIONS CORP. 134 FLANDERS ROAD, SUITE 125 WESTBOROUGH, MA 01581



201 BOSTON POST ROAD WEST, SUITE 101 MARLBOROUGH, MA 01752 (508) 481-7400 www.chappellengineering.com



CHECKED BY:

APPROVED BY:

	SUBMITTALS						
REV.	DATE	DESCRIPTION	BY				
1		ISSUED FOR CONSTRUCTION	CMC				
0	07/20/20	ISSUED FOR REVIEW	JRV				

SITE NUMBER: CT11284A

SITE ADDRESS: 81 MONTEVIDEO ROAD AVON, CT 06001

SHEET TITLE

TITLE SHEET

SHEET NUMBER

GENERAL NOTES:

- 1. FOR THE PURPOSE OF CONSTRUCTION DRAWINGS, THE FOLLOWING DEFINITIONS SHALL APPLY: CONTRACTOR - T-MOBILE SUBCONTRACTOR - GENERAL CONTRACTOR (CONSTRUCTION) OWNER - T-MOBILE
 - OEM ORIGINAL EQUIPMENT MANUFACTURER
- 2. PRIOR TO THE SUBMISSION OF BIDS, THE BIDDING SUBCONTRACTOR SHALL VISIT THE CELL SITE TO FAMILIARIZE WITH THE EXISTING CONDITIONS AND TO CONFIRM THAT THE WORK CAN BE ACCOMPLISHED AS SHOWN ON THE CONSTRUCTION DRAWINGS. ANY DISCREPANCY FOUND SHALL BE BROUGHT TO THE ATTENTION OF CONTRACTOR.
- 3. ALL MATERIALS FURNISHED AND INSTALLED SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE CODES, REGULATIONS. AND ORDINANCES. SUBCONTRACTOR SHALL ISSUE ALL APPROPRIATE NOTICES AND COMPLY WITH ALL LAWS, ORDINANCES, RULES, REGULATIONS, AND LAWFUL ORDERS OF ANY PUBLIC AUTHORITY REGARDING THE PERFORMANCE OF THE WORK.
- 4. ALL WORK CARRIED OUT SHALL COMPLY WITH ALL APPLICABLE MUNICIPAL AND UTILITY COMPANY SPECIFICATIONS AND LOCAL, STATE AND FEDERAL JURISDICTIONAL CODES, ORDINANCES AND APPLICABLE REGULATIONS.
- 5. DRAWINGS PROVIDED HERE ARE NOT TO BE SCALED AND ARE INTENDED TO SHOW OUTLINE ONLY.
- 6. UNLESS NOTED OTHERWISE, THE WORK SHALL INCLUDE FURNISHING MATERIALS, EQUIPMENT, APPURTENANCES, AND LABOR NECESSARY TO COMPLETE ALL INSTALLATIONS AS INDICATED ON THE DRAWINGS.
- 7. THE SUBCONTRACTOR SHALL INSTALL ALL EQUIPMENT AND MATERIALS IN ACCORDANCE WITH MANUFACTURER'S RECOMMENDATIONS UNLESS SPECIFICALLY STATED OTHERWISE.
- 8. IF THE SPECIFIED EQUIPMENT CANNOT BE INSTALLED AS SHOWN ON THESE DRAWINGS, THE SUBCONTRACTOR SHALL PROPOSE AN ALTERNATIVE INSTALLATION FOR APPROVAL BY THE CONTRACTOR.
- 9. SUBCONTRACTOR SHALL DETERMINE ACTUAL ROUTING OF CONDUIT, POWER, T1 CABLES AND GROUNDING CABLES AS SHOWN ON THE POWER, GROUNDING AND TELCO PLAN DRAWING. SUBCONTRACTOR SHALL UTILIZE EXISTING TRAYS AND/OR SHALL ADD NEW TRAYS AS NECESSARY, SUBCONTRACTOR SHALL CONFIRM THE ACTUAL ROUTING WITH THE CONTRACTOR AND/OR LANDLORD PRIOR TO CONSTRUCTION.
- 10. THE SUBCONTRACTOR SHALL PROTECT EXISTING IMPROVEMENTS, PAVEMENTS, CURBS, LANDSCAPING AND STRUCTURES. ANY DAMAGED PART SHALL BE REPAIRED AT SUBCONTRACTOR'S EXPENSE TO THE SATISFACTION OF THE OWNER.
- 11. SUBCONTRACTOR SHALL LEGALLY AND PROPERLY DISPOSE OF ALL SCRAP MATERIALS SUCH AS COAXIAL CABLES AND OTHER ITEMS REMOVED FROM THE EXISTING FACILITY.
- 12. SUBCONTRACTOR SHALL LEAVE PREMISES IN CLEAN CONDITION AND RETURN DISTURBED AREAS TO ORIGINAL CONDITIONS.
- 13. THE SUBCONTRACTOR SHALL SUPERVISE AND DIRECT THE PROJECT DESCRIBED HEREIN. THE SUBCONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES FOR COORDINATING ALL PORTIONS OF THE WORK UNDER THE CONTRACT.
- 14. SUBCONTRACTOR SHALL NOTIFY CHAPPELL ENGINEERING ASSOCIATES, LLC 48 HOURS IN ADVANCE OF POURING CONCRETE OR BACKFILLING TRENCHES, SEALING ROOF AND WALL PENETRATIONS AND POST DOWNS, FINISHING NEW WALLS OR FINAL ELECTRICAL CONNECTIONS FOR ENGINEERING REVIEW.
- 15. CONSTRUCTION SHALL COMPLY WITH ALL T-MOBILE STANDARDS AND SPECIFICATIONS.
- 16. SUBCONTRACTOR SHALL VERIFY ALL EXISTING DIMENSIONS AND CONDITIONS PRIOR TO COMMENCING ANY WORK. ALL DIMENSIONS OF EXISTING CONSTRUCTION SHOWN ON THE DRAWINGS MUST BE VERIFIED. SUBCONTRACTOR SHALL NOTIFY THE CONTRACTOR OF ANY DISCREPANCIES PRIOR TO ORDERING MATERIAL OR PROCEEDING WITH CONSTRUCTION.
- 17. THE EXISTING CELL SITES ARE IN FULL COMMERCIAL OPERATION. ANY CONSTRUCTION WORK BY SUBCONTRACTOR SHALL NOT DISRUPT THE EXISTING NORMAL OPERATION. ANY WORK ON EXISTING EQUIPMENT MUST BE COORDINATED WITH CONTRACTOR, ALSO, WORK SHOULD BE SCHEDULED FOR AN APPROPRIATE MAINTENANCE WINDOW USUALLY IN LOW TRAFFIC PERIODS AFTER MIDNIGHT.
- 18. IF THE EXISTING CELL SITE IS ACTIVE, ALL SAFETY PRECAUTIONS MUST BE TAKEN WHEN WORKING AROUND HIGH LEVELS OF ELECTROMAGNETIC RADIATION. EQUIPMENT SHOULD BE SHUTDOWN PRIOR TO PERFORMING ANY WORK THAT COULD EXPOSE THE WORKERS TO DANGER. PERSONAL RF EXPOSURE MONITORS ARE TO BE WORN TO ALERT OF ANY DANGEROUS EXPOSURE LEVELS.

SITE WORK GENERAL NOTES:

- 1. THE SUBCONTRACTOR SHALL CONTACT UTILITY LOCATING SERVICES PRIOR TO THE START OF CONSTRUCTION.
- 2. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY ENGINEERS. EXTREME CAUTION SHOULD BE USED BY THE SUBCONTRACTOR WHEN EXCAVATING OR DRILLING PIERS AROUND OR NEAR UTILITIES. SUBCONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE BUT NOT BE LIMITED TO A) FALL PROTECTION B) CONFINED SPACE C) ELECTRICAL SAFETY D) TRENCHING AND EXCAVATION.
- 3. ALL SITE WORK SHALL BE AS INDICATED ON THE DRAWINGS AND PROJECT SPECIFICATIONS.
- 4. IF NECESSARY, RUBBISH, STUMPS, DEBRIS, STICKS, STONES AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
- 5. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE BTS EQUIPMENT AND TOWER AREAS.
- 6. NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR EMBANKMENT.
- 7. THE SUB GRADE SHALL BE COMPACTED AND BROUGHT TO A SMOOTH UNIFORM GRADE PRIOR TO FINISHED SURFACE APPLICATION.
- 8. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF ENGINEERING, OWNER AND/OR LOCAL UTILITIES.
- 9. THE AREAS OF THE OWNERS PROPERTY DISTURBED BY THE WORK AND NOT COVERED BY THE TOWER. EQUIPMENT OR DRIVEWAY, SHALL BE GRADED TO A UNIFORM SLOPE AND STABILIZED TO PREVENT EROSION AS SPECIFIED IN THE PROJECT SPECIFICATIONS.
- 10. SUBCONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES, IF REQUIRED DURING CONSTRUCTION, SHALL BE IN CONFORMANCE WITH THE LOCAL GUIDELINES FOR EROSION AND SEDIMENT CONTROL.
- 11. THE SUBCONTRACTOR SHALL PROVIDE SITE SIGNAGE IN ACCORDANCE WITH THE T-MOBILE SPECIFICATION FOR SITE SIGNAGE.

CONCRETE AND REINFORCING STEEL NOTES:

- 1. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH THE ACI 301, ACI 318, ACI 336, ASTM A184, ASTM A185 AND THE DESIGN AND CONSTRUCTION SPECIFICATION FOR CAST-IN-PLACE CONCRETE.
- 2. ALL CONCRETE SHALL HAVE A MINIMUM COMPRESSIVE STRENGTH OF 3000 PSI AT 28 DAYS, UNLESS NOTED OTHERWISE. A HIGHER STRENGTH (400PSI) MAY BE USED. ALL CONCRETE WORK SHALL BE IN ACCORDANCE WITH THE ACI 381 CODE
- 3. REINFORCING STEEL SHALL CONFORM TO ASTM A 615. GRADE 60. DEFORMED UNLESS NOTED OTHERWISE. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A 185 WELDED STEEL WIRE FABRIC UNLESS NOTED OTHERWISE. SPLICES SHALL BE CLASS "B" AND ALL HOOKS SHALL BE STANDARD, UNO.
- 4. THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON DRAWINGS:
 - CONCRETE CAST AGAINST EARTH.......3 IN. CONCRETE EXPOSED TO EARTH OR WEATHER:
 - #6 AND LARGER2 IN.
 - #5 AND SMALLER & WWF 1½ IN. CONCRETE NOT EXPOSED TO EARTH OR WEATHER
 - OR NOT CAST AGAINST THE GROUND: SLAB AND WALL BEAMS AND COLUMNS1½ IN.
- 5. A CHAMFER 34" SHALL BE PROVIDED AT ALL EXPOSED EDGES OF CONCRETE, UNO, IN ACCORDANCE WITH ACI 301 SECTION
- 6. INSTALLATION OF CONCRETE EXPANSION/WEDGE ANCHORS SHALL BE PER MANUFACTURER'S WRITTEN RECOMMENDED PROCEDURE. THE ANCHOR BOLT, DOWEL OR ROD SHALL CONFORM TO THE MANUFACTURERS RECOMMENDATION FOR EMBEDMENT DEPTH OR AS SHOWN ON THE DRAWINGS. NO REBAR SHALL BE CUT WITHOUT PRIOR CONTRACTOR APPROVAL WHEN DRILLING HOLES IN CONCRETE. SPECIAL INSPECTIONS, REQUIRED BY GOVERNING CODES, SHALL BE PERFORMED IN ORDER TO MAINTAIN MANUFACTURER'S MAXIMUM ALLOWABLE LOADS. ALL EXPANSION/WEDGE ANCHORS SHALL BE STAINLESS STEEL OR HOT DIPPED GALVANIZED. EXPANSION BOLTS SHALL BE PROVIDED BY SIMPSON OR APPROVED EQUAL.
- 7. CONCRETE CYLINDER TIES ARE NOT REQUIRED FOR SLAB ON GRADE WHEN CONCRETE IS LESS THAN 50 CUBIC YARDS (IBC1905.6.2.3) IN THAT EVENT THE FOLLOWING RECORDS SHALL BE PROVIDED BY THE CONCRETE SUPPLIER;
- (A) RESULTS OF CONCRETE CYLINDER TEST PERFORMED AT THE SUPPLIERS PLANT.
- (B) CERTIFICATION OF MINIMUM COMPRESSIVE STRENGTH FOR THE CONCRETE GRADE SUPPLIED. FOR GREATER THAN 50 CUBIC YARDS THE GC SHALL PERFORM THE CONCRETE CYLINDER TEST.
- 8. AS AN ALTERNATIVE TO ITEM 7. TEST CYLINDERS SHALL BE TAKEN INITIALLY AND THEREAFTER FOR EVERY 50 YARDS OF CONCRETE FROM EACH DIFFERENT BATCH PLANT.
- 9. EQUIPMENT SHALL NOT BE PLACED ON NEW PADS FOR SEVEN DAYS AFTER PAD IS POURED, UNLESS IT IS VERIFIED BY CYLINDER TESTS THAT COMPRESSIVE STRENGTH HAS BEEN ATTAINED.

STRUCTURAL STEEL NOTES:

- 1. ALL STEEL WORK SHALL BE PAINTED OR GALVANIZED IN ACCORDANCE WITH THE DRAWINGS AND T-MOBILE SPECIFICATIONS UNLESS OTHERWISE NOTED. STRUCTURAL STEEL SHALL BE ASTM-A-36 UNLESS OTHERWISE NOTED ON THE SITE SPECIFIC DRAWINGS. STEEL DESIGN, INSTALLATION AND BOLTING SHALL BE IN ACCORDANCE WITH THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC) "MANUAL OF STEEL CONSTRUCTION".
- 2. ALL WELDING SHALL BE PERFORMED USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND AWS D1.1 WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION", 9TH EDITION. PAINTED SURFACES SHALL BE TOUCHED UP.
- 3. BOLTED CONNECTIONS SHALL USE BEARING TYPE ASTM A325 BOLTS (3/4") AND SHALL HAVE MINIMUM OF TWO BOLTS UNLESS NOTED OTHERWISE. ALL BOLTS SHALL BE GALVANIZED OR STAINLESS STEEL.
- 4. NON-STRUCTURAL CONNECTIONS FOR STEEL GRATING MAY USE %" DIA. ASTM A 307 BOLTS (GALV) UNLESS NOTED OTHERWISE.
- 5. CONTRACTOR SHALL SUBMIT SHOP DRAWINGS FOR ENGINEER REVIEW & APPROVAL ON PROJECTS REQUIRING STRUCTURAL
- 6. ALL STRUCTURAL STEEL WORK SHALL BE DONE IN ACCORDANCE WITH AISC SPECIFICATIONS.

SOIL COMPACTION NOTES FOR SLAB ON GRADE:

- 1. EXCAVATE AS REQUIRED TO REMOVE VEGETATION AND TOPSOIL TO EXPOSE NATURAL SUBGRADE AND PLACE CRUSHED STONE AS REQUIRED.
- 2. COMPACTION CERTIFICATION: AN INSPECTION AND WRITTEN CERTIFICATION BY A QUALIFIED GEOTECHNICAL TECHNICIAN OR ENGINEER IS ACCEPTABLE.
- 3. AS AN ALTERNATE TO INSPECTION AND WRITTEN CERTIFICATION, THE "UNDISTURBED SOIL" BASE SHALL BE COMPACTED WITH "COMPACTION EQUIPMENT". LISTED BELOW, TO AT LEAST 90% MODIFIED PROCTOR MAXIMUM DENSITY PER ASTM D 1557 METHOD C.
- 4. COMPACTED SUBBASE SHALL BE UNIFORM AND LEVELED. PROVIDE 6" MINIMUM CRUSHED STONE OR GRAVEL COMPACTED IN 3" LIFTS ABOVE COMPACTED SOIL. GRAVEL SHALL BE NATURAL OR CRUSHED WITH 100% PASSING #1 SIEVE.
- 5. AS AN ALTERNATE TO ITEMS 2 AND 3, THE SUBGRADE SOILS WITH 5 PASSES OR A MEDIUM SIZED VIBRATORY PLATE COMPACTOR (SUCH AS BOMAG BPR 30/38) OR HAND-OPERATED SINGLE DRUM VIBRATORY ROLLER (SUCH AS BOMAG BW 55E). AND SOFT AREAS THAT ARE ENCOUNTERED SHOULD BE REMOVED AND REPLACED WITH A WELL-GRADED GRANULAR FILL AND COMPACTED AS STATED ABOVE.

COMPACTION EQUIPMENT:

1. HAND OPERATED DOUBLE DRUN, VIBRATORY ROLLER, VIBRATORY PLATE COMPACTOR OR JUMPING JACK COMPACTOR.

CONSTRUCTION NOTES:

1. FIELD VERIFICATION:

- SUBCONTRACTOR SHALL FIELD VERIFY SCOPE OF WORK, T-MOBILE ANTENNA PLATFORM LOCATION AND UTILITY TRENCHWORK.
- 2. COORDINATION OF WORK:
- SUBCONTRACTOR SHALL COORDINATE RF WORK AND PROCEDURES WITH CONTRACTOR.

3. CABLE LADDER RACK:

SUBCONTRACTOR SHALL FURNISH AND INSTALL CABLE LADDER RACK, CABLE TRAY AND/OR ICE BRIDGE, AND CONDUIT AS REQUIRED TO SUPPORT CABLES TO THE NEW BTS LOCATION.

ELECTRICAL INSTALLATION NOTES:

1. WIRING, RACEWAY, AND SUPPORT METHODS AND MATERIALS SHALL COMPLY WITH THE REQUIREMENTS OF THE NEC AND TELCORDIA.

2. SUBCONTRACTOR SHALL MODIFY OR INSTALL CABLE TRAY SYSTEM AS REQUIRED TO SUPPORT RF AND TRANSPORT CABLING TO THE NEW BTS EQUIPMENT. SUBCONTRACTOR SHALL SUBMIT MODIFICATIONS TO CONTRACTOR FOR APPROVAL.

- 3. ALL CIRCUITS SHALL BE SEGREGATED AND MAINTAIN MINIMUM CABLE SEPARATION AS REQUIRED BY THE NEC AND
- 4. CABLES SHALL NOT BE ROUTED THROUGH LADDER-STYLE CABLE TRAY RUNGS.
- 5. EACH END OF EVERY POWER, GROUNDING, AND T1 CONDUCTOR AND CABLE SHALL BE LABELED WITH COLOR-CODED INSULATION OR ELECTRICAL TAPE (3M BRAND, 1/2 INCH PLASTIC ELECTRICAL TAPE WITH UV PROTECTION, OR EQUAL). THE IDENTIFICATION METHOD SHALL CONFORM WITH NEC AND OSHA, AND MATCH INSTALLATION REQUIREMENTS.
- 6. POWER PHASE CONDUCTORS (I.E., HOTS) SHALL BE LABELED WITH COLOR-CODED INSULATION OR ELECTRICAL TAPE (3M BRAND, ½ INCH PLASTIC ELECTRICAL TAPE WITH UV PROTECTION, OR EQUAL). PHASE CONDUCTOR COLOR CODES SHALL CONFORM WITH THE NEC AND OSHA.
- 7. ALL ELECTRICAL COMPONENTS SHALL BE CLEARLY LABELED WITH ENGRAVED LAMACOID PLASTIC LABELS. ALL EQUIPMENT SHALL BE LABELED WITH THEIR VOLTAGE RATING, PHASE CONFIGURATION, WIRE CONFIGURATION, POWER OR AMPACITY RATING, AND BRANCH CIRCUIT ID NUMBERS (I.E., PANELBOARD AND CIRCUIT ID'S).
- 8. PANELBOARDS (ID NUMBERS) AND INTERNAL CIRCUIT BREAKERS (CIRCUIT ID NUMBERS) SHALL BE CLEARLY LABELED WITH ENGRAVED LAMACOID PLASTIC LABELS.
- 9. ALL TIE WRAPS SHALL BE CUT FLUSH WITH APPROVED CUTTING TOOL TO REMOVE SHARP EDGES.
- 10. POWER, CONTROL, AND EQUIPMENT GROUND WIRING IN TUBING OR CONDUIT SHALL BE SINGLE CONDUCTOR (#34 AWG OR LARGER), 600 V, OIL RESISTANT THHN OR THWN-2, CLASS B STRANDED COPPER CABLE RATED FOR 90 °C (WET AND DRY) OPERATION; LISTED OR LABELED FOR THE LOCATION AND RACEWAY SYSTEM USED, UNLESS OTHERWISE
- 11. SUPPLEMENTAL EQUIPMENT GROUND WIRING LOCATED INDOORS SHALL BE SINGLE CONDUCTOR (#6 AWG OR LARGER), 600 V, OIL RESISTANT THHN OR THWN-2 GREEN INSULATION, CLASS B STRANDED COPPER CABLE RATED FOR 90 °C (WET AND DRY) OPERATION; LISTED OR LABELED FOR THE LOCATION AND RACEWAY SYSTEM USED, UNLESS OTHERWISE SPECIFIED.
- 12. SUPPLEMENTAL EQUIPMENT GROUND WIRING LOCATED OUTDOORS, OR BELOW GRADE, SHALL BE SINGLE CONDUCTOR #2 AWG SOLID TINNED COPPER CABLE, UNLESS OTHERWISE SPECIFIED.
- 13. POWER AND CONTROL WIRING, NOT IN TUBING OR CONDUIT, SHALL BE MULTI-CONDUCTOR, TYPE TC CABLE (#34 AWG OR LARGER), 600 V, OIL RESISTANT THHN OR THWN-2, CLASS B STRANDED COPPER CABLE RATED FOR 90 °C (WET AND DRY) OPERATION; WITH OUTER JACKET; LISTED OR LABELED FOR THE LOCATION USED, UNLESS OTHERWISE SPECIFIED.
- 14. ALL POWER AND GROUNDING CONNECTIONS SHALL BE CRIMP-STYLE, COMPRESSION WIRE LUGS AND WIRENUTS BY HARGER (OR EQUAL). LUGS AND WIRENUTS SHALL BE RATED FOR OPERATION AT NO LESS THAN 75°C (90°C IF AVAILABLE).
- 15. RACEWAY AND CABLE TRAY SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA, UL, ANSI/IEEE AND NEC.
- 16. NEW RACEWAY OR CABLE TRAY WILL MATCH THE EXISTING INSTALLATION WHERE POSSIBLE.
- 17. ELECTRICAL METALLIC TUBING (EMT) OR RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHEDULE 40 OR RIGID PVC SCHEDULE 80 FOR LOCATIONS SUBJECT TO PHYSICAL DAMAGE) SHALL BE USED FOR EXPOSED INDOOR LOCATIONS.
- 18. ELECTRICAL METALLIC TUBING (EMT). ELECTRICAL NONMETALLIC TUBING (ENT), OR RIGID NONMETALLIC CONDUIT (RIGID PVC, SCHEDULE 40) SHALL BE USED FOR CONCEALED INDOOR LOCATIONS.
- 19. GALVANIZED STEEL INTERMEDIATE METALLIC CONDUIT (IMC) SHALL BE USED FOR OUTDOOR LOCATIONS ABOVE
- 20. RIGID NONMETALLIC CONDUIT (I.E., RIGID PVC SCHEDULE 40 OR RIGID PVC SCHEDULE 80) SHALL BE USED UNDERGROUND; DIRECT BURIED, IN AREAS OF OCCASIONAL LIGHT VEHICLE TRAFFIC OR ENCASED IN REINFORCED CONCRETE IN AREAS OF HEAVY VEHICLE TRAFFIC.
- 21. LIQUID-TIGHT FLEXIBLE METALLIC CONDUIT (LIQUID-TITE FLEX) SHALL BE USED INDOORS AND OUTDOORS, WHERE VIBRATION OCCURS OR FLEXIBILITY IS NEEDED.
- 22. CONDUIT AND TUBING FITTINGS SHALL BE THREADED OR COMPRESSION—TYPE AND APPROVED FOR THE LOCATION
- 23. CABINETS, BOXES AND WIREWAYS SHALL BE LISTED OR LABELED FOR ELECTRICAL USE IN ACCORDANCE WITH NEMA,
- 24. CABINETS, BOXES AND WIREWAYS TO MATCH THE EXISTING INSTALLATION WHERE POSSIBLE.

USED. SETSCREW FITTINGS ARE NOT ACCEPTABLE.

UL, ANSI/IEEE AND NEC.

- 25. WIREWAYS SHALL BE EPOXY-COATED (GRAY) AND INCLUDE A HINGED COVER, DESIGNED TO SWING OPEN DOWNWARD: SHALL BE PANDUIT TYPE E (OR EQUAL): AND RATED NEMA 1 (OR BETTER) INDOORS. OR NEMA 3R (OR BETTER) OUTDOORS.
- 26. EQUIPMENT CABINETS, TERMINAL BOXES, JUNCTION BOXES, AND PULL BOXES SHALL BE GALVANIZED OR EPOXY-COATED SHEET STEEL, SHALL MEET OR EXCEED UL 50, AND RATED NEMA 1 (OR BETTER) INDOORS, OR NEMA 3R (OR BETTER) OUTDOORS.
- 27. METAL RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL BE GALVANIZED, EPOXY-COATED, OR NON-CORRODING; SHALL MEET OR EXCEED UL 514A AND NEMA OS 1; AND RATED NEMA 1 (OR BETTER) INDOORS, OR WEATHER PROTECTED (WP OR BETTER) OUTDOORS.
- 28. NONMETALLIC RECEPTACLE, SWITCH, AND DEVICE BOXES SHALL MEET OR EXCEED NEMA OS 2; AND RATED NEMA 1 (OR BETTER) INDOORS, OR WEATHER PROTECTED (WP OR BETTER) OUTDOORS.
- 29. THE SUBCONTRACTOR SHALL NOTIFY AND OBTAIN NECESSARY AUTHORIZATION FROM THE CONTRACTOR BEFORE COMMENCING WORK ON THE AC POWER DISTRIBUTION PANELS.
- 30. THE SUBCONTRACTOR SHALL PROVIDE NECESSARY TAGGING ON THE BREAKERS, CABLES AND DISTRIBUTION PANELS IN ACCORDANCE WITH THE APPLICABLE CODES AND STANDARDS TO SAFEGUARD AGAINST LIFE AND PROPERTY.
- 31. ALL ELECTRICAL WORK SHALL BE PERFORMED IN ACCORDANCE WITH THE PROJECT SPECIFICATIONS, NEC AND ALL APPLICABLE LOCAL CODES.
- 32. CONDUIT ROUTINGS ARE SCHEMATIC. SUBCONTRACTOR SHALL INSTALL CONDUITS SO THAT ACCESS TO EQUIPMENT IS NOT BLOCKED.

T-MOBILE NORTHEAST LLC

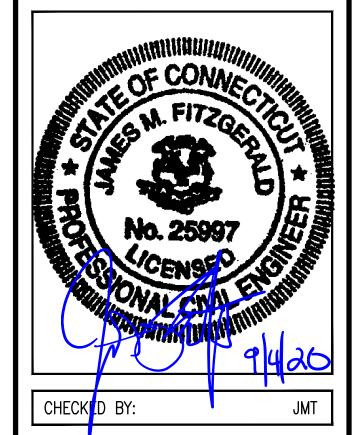
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SUBMITTALS REV. DATE RY DESCRIPTION

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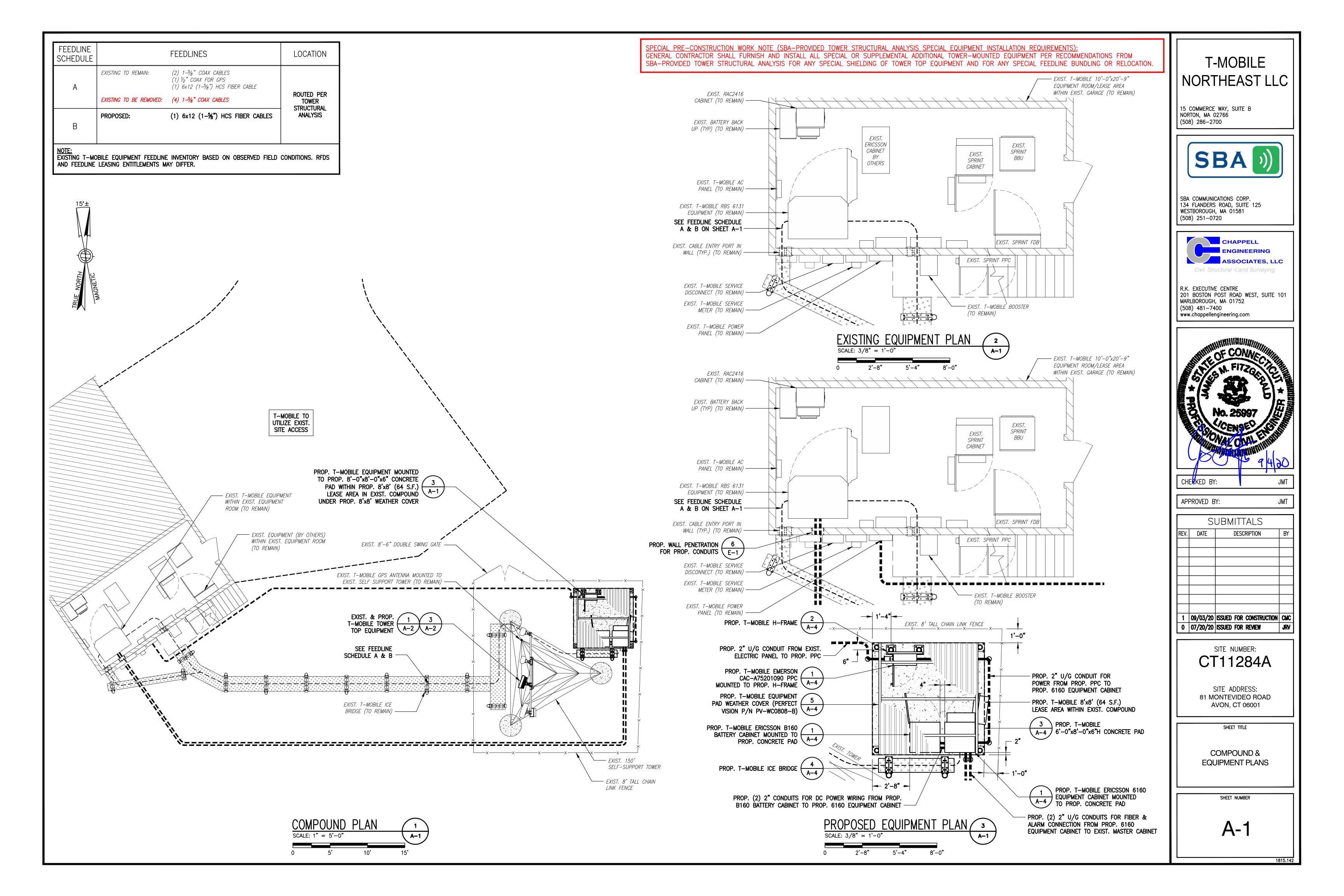
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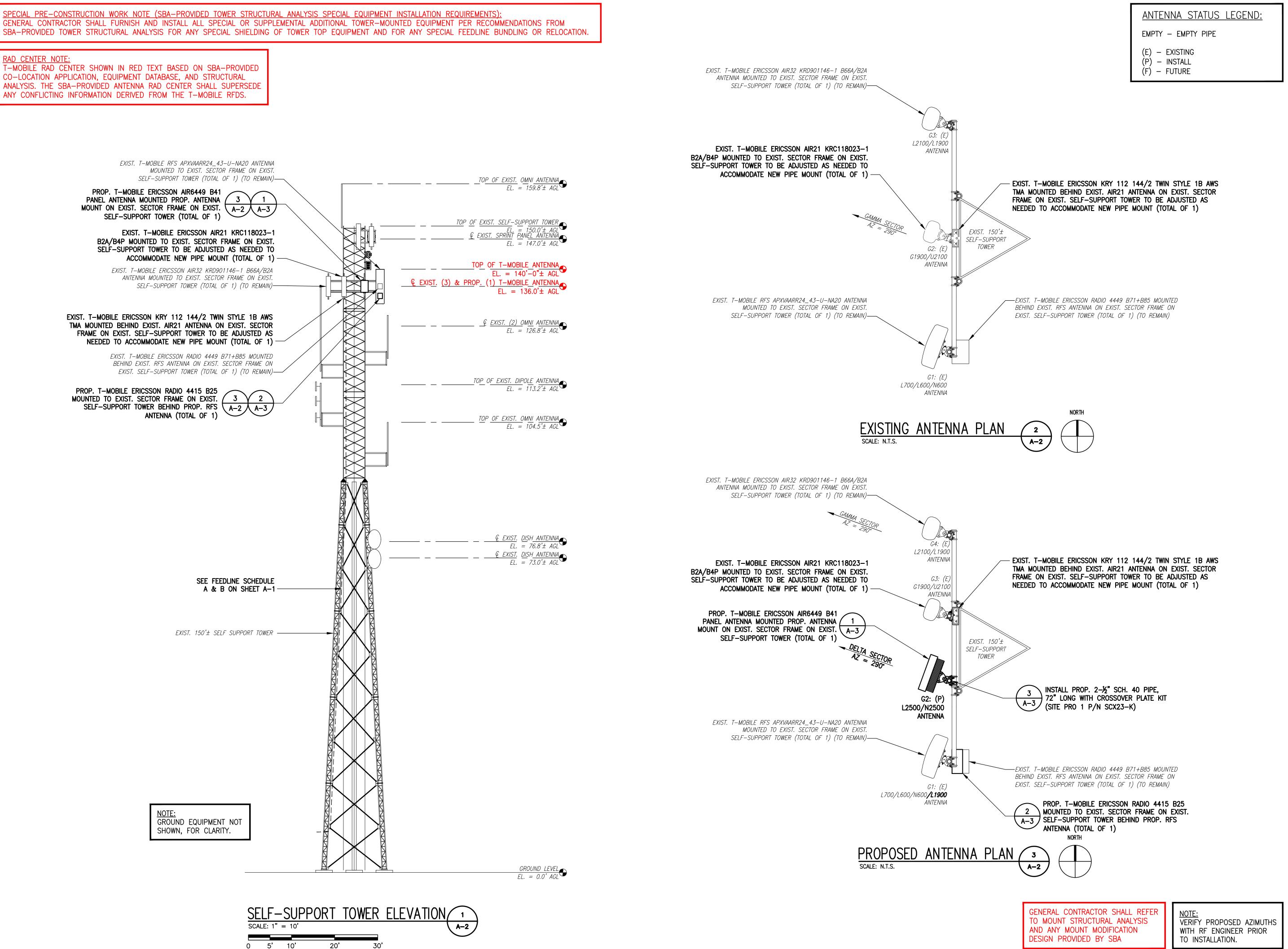
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GENERAL NOTES

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GN-1





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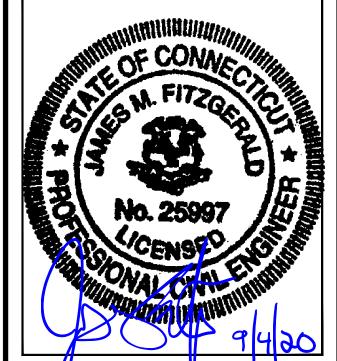
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APPROVED BY: JM

CHICKED BY:

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1 09/03/20 ISSUED FOR CONSTRUCTION CMC
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SHEET TITLE

TOWER ELEVATION & ANTENNA PLANS

SHEET NUMBER

A-2

1815.14

	FINAL ANTENNA CONFIGURATION									
SECTOR	ANTENNA	RAD CENTER	AZIMUTH (TRUE NORTH)	MECHANICAL DOWNTILT	ELECTRICAL DOWNTILT	BAND	TMA/RADIOS	CABLES		
	RFS	136'-0"± AGL	290°	<i>0°</i>	6°	L600/N600/L700	ERICSSON RADIO 4449 B71+B85			
	APXVAARR24_43-U-NA20				6°	L1900	ERICSSON RADIO 4415 B25			
GAMMA	ERICSSON M-MIMO AIR6449 B41	136'-0"± AGL	290°	0°	o•	L2500/N2500	_	(2) 1-5/8" COAX CABLES (1) 6x12 (1-5/8") HCS FIBER CABLE		
	ERICSSON AIR21 KRC118023-1 B2A/B4P	136'-0"± AGL	290°	0°	4°	G1900/U2100	ERICSSON KRY 112 144/2 TWIN STYLE 1B AWS TMA	(1) 6x12 (1-5%") HCS FIBER CABLES		
	ERICSSON AIR32 KRD901046-1 B66A/B2A	136'-0"± AGL	290°	<i>0°</i>	6°	L2100/L1900	_			

CABLE NOTE: EXISTING (4) 1-1/8" COAX CABLES TO BE REMOVED. SEE FEEDLINE SCHEDULE A & B ON SHEET A-1.

NOTE: RFDS REV6 - 05/11/20



ERICSSON M-MIMO AIR6449 B41 PANEL ANTENNA

DIMENSIONS: 33.1"H x 20.5"W x 8.3"D

WEIGHT: 103.0 lbs

QUANTITY: TOTAL OF 1





ERICSSON RADIO 4415 B25

DIMENSIONS: 16.5"H x 13.4"W x 5.9"D

WEIGHT: 46 LBS

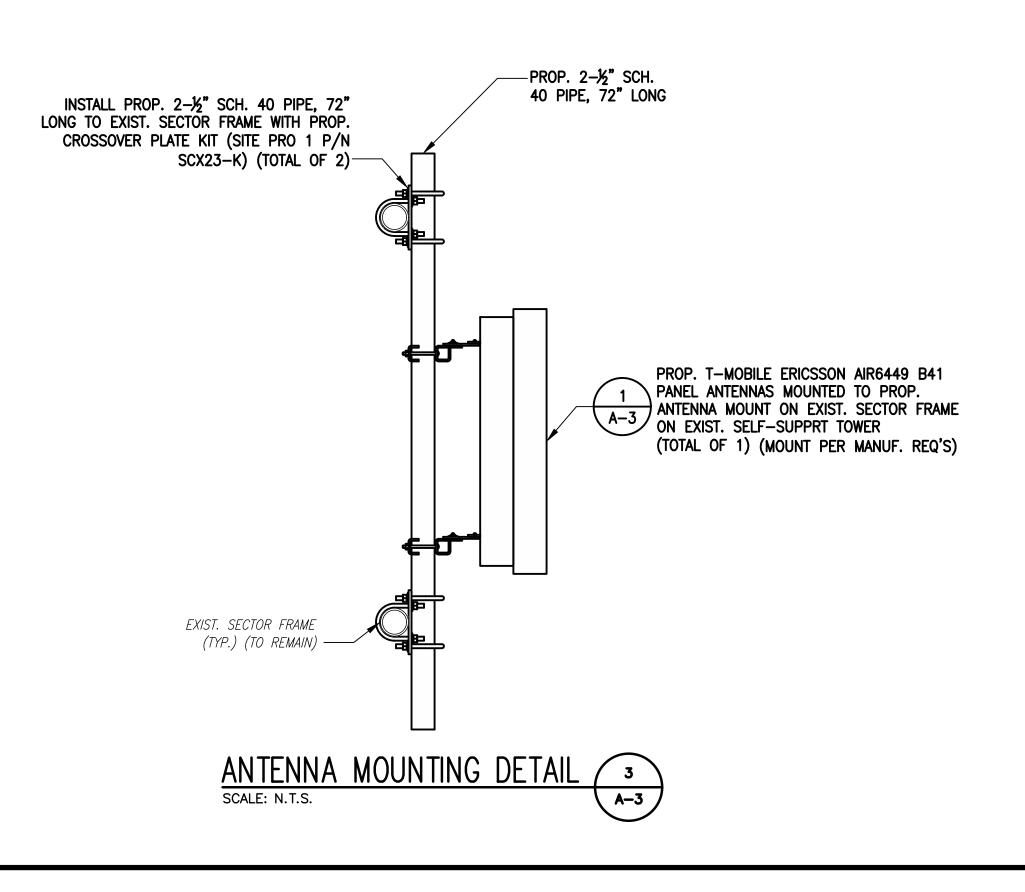
QUANTITY: TOTAL OF 1

RADIO DETAILS

SCALE: N.T.S.

2
A-3





T-MOBILE NORTHEAST LLC

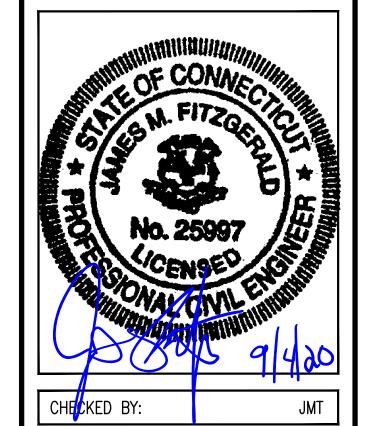
15 COMMERCE WAY, SUITE B NORTON, MA 02766 (508) 286-2700



SBA COMMUNICATIONS CORP. 134 FLANDERS ROAD, SUITE 125 WESTBOROUGH, MA 01581 (508) 251-0720



R.K. EXECUTIVE CENTRE
201 BOSTON POST ROAD WEST, SUITE 101
MARLBOROUGH, MA 01752
(508) 481-7400
www.chappellengineering.com



APPROVED BY: JMT

REV.	DATE	UBMITTALS DESCRIPTION	BY
INLV.	DAIL	DESCRIPTION	- 01
1	09/03/20	ISSUED FOR CONSTRUCTION	CM
0	07/20/20	ISSUED FOR REVIEW	JR۱

SITE NUMBER: CT11284A

SITE ADDRESS: 81 MONTEVIDEO ROAD AVON, CT 06001

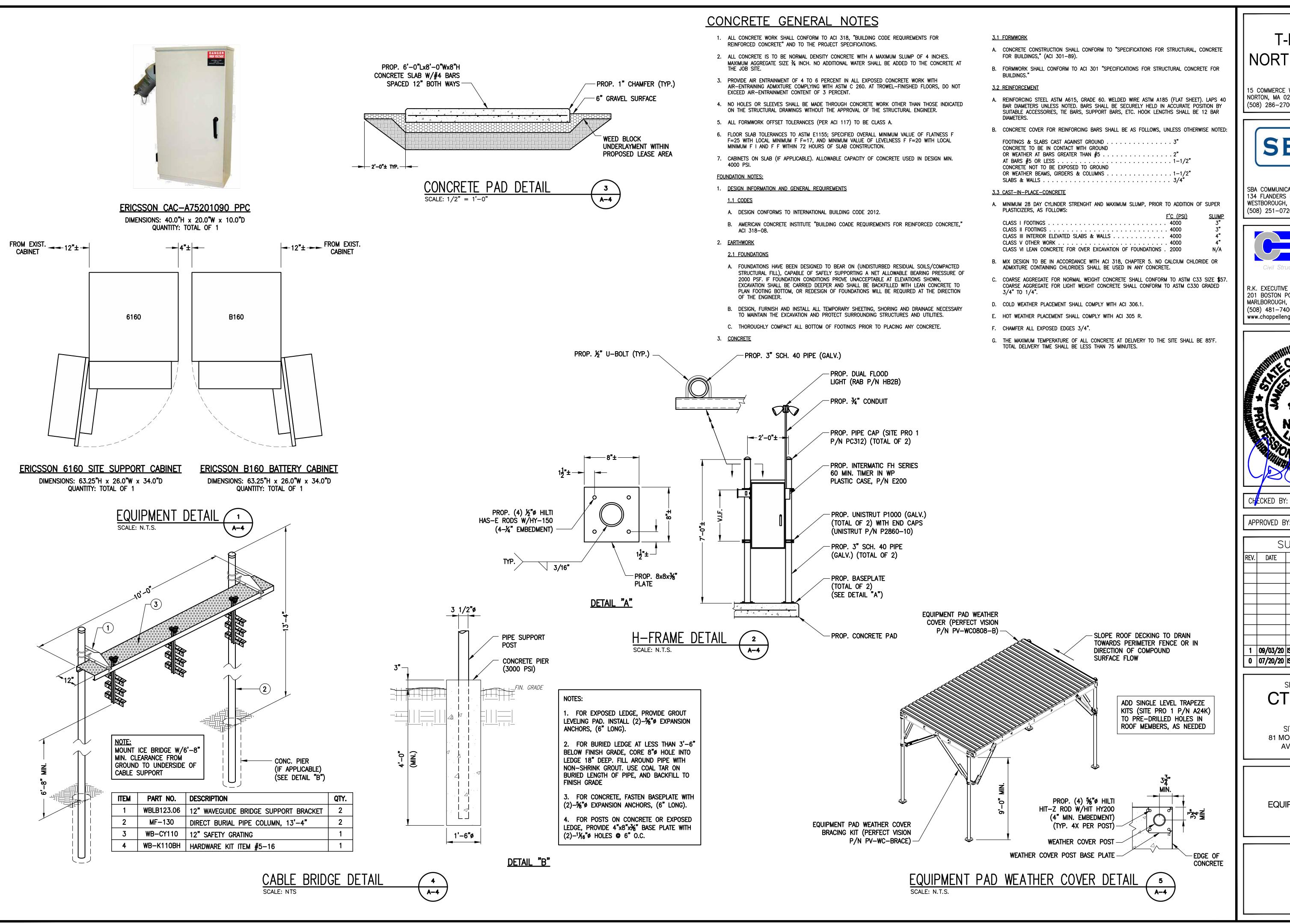
SHEET 1

ANTENNA DETAILS

SHEET NUMBER

A-3

1815.14



T-MOBILE NORTHEAST LLC

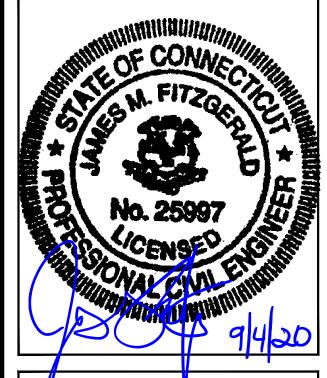
15 COMMERCE WAY, SUITE B NORTON, MA 02766 (508) 286-2700



SBA COMMUNICATIONS CORP. 134 FLANDERS ROAD, SUITE 125 WESTBOROUGH, MA 01581 (508) 251-0720



R.K. EXECUTIVE CENTRE 201 BOSTON POST ROAD WEST, SUITE 101 MARLBOROUGH, MA 01752 (508) 481-7400 www.chappellengineering.com



APPROVED BY:

	SUBMITTALS						
REV.	DATE		DESC	RIPTION	BY		
1				CONSTRUCTION	CMC		
0	07/20/20	ISSUED	FOR	REVIEW	JRV		

SITE NUMBER: CT11284A

SITE ADDRESS: 81 MONTEVIDEO ROAD AVON, CT 06001

SHEET TITLE

EQUIPMENT DETAILS

SHEET NUMBER

A-4

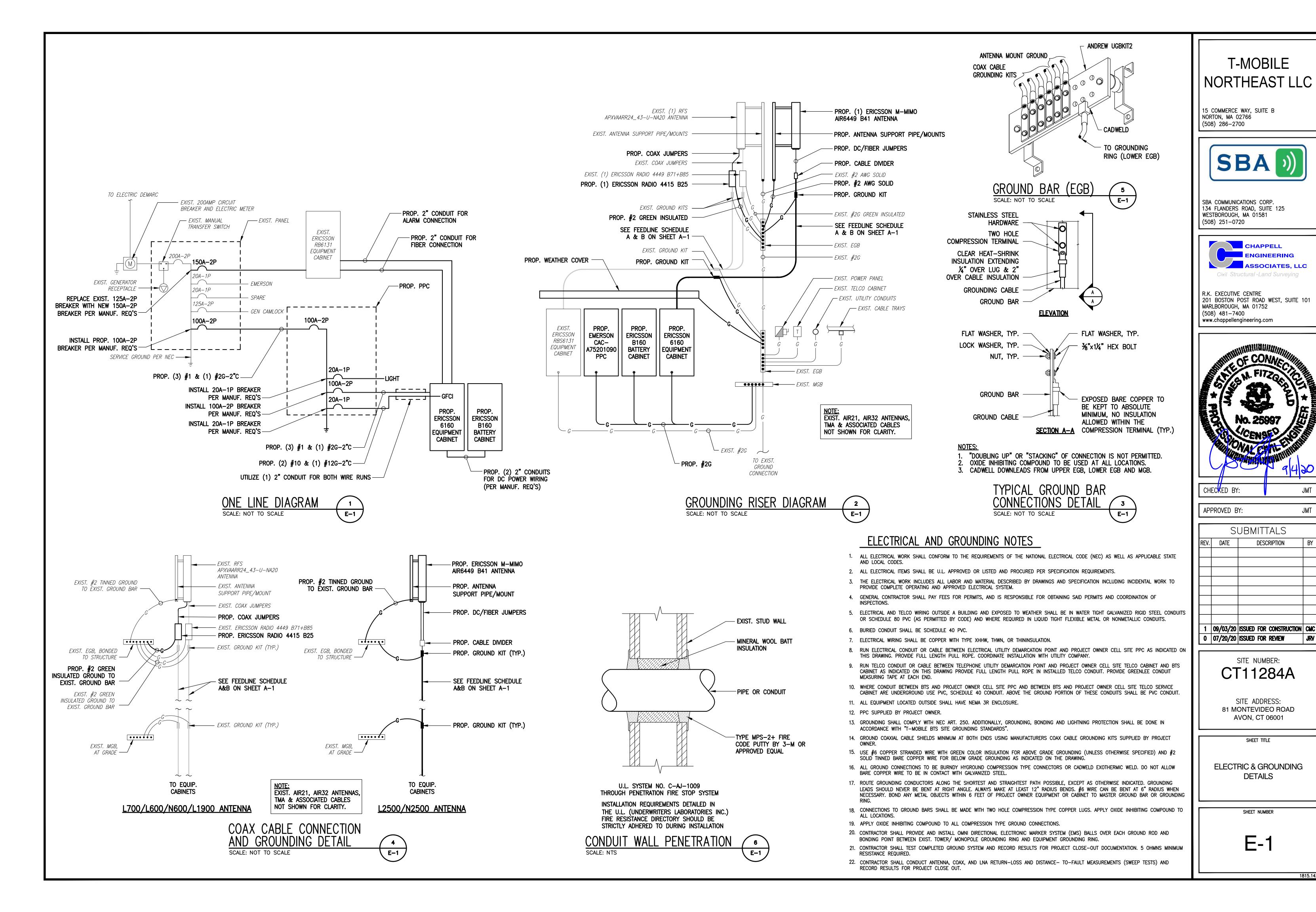


EXHIBIT 7



Tower Engineering Solutions

Phone (972) 483-0607, Fax (972) 975-9615 1320 Greenway Drive, Suite 600, Irving, Texas 75038

Structural Analysis Report

Existing 150 ft PIROD Self Supporting Tower

Customer Name: SBA Communications Corp

Customer Site Number: CT22071-A

Customer Site Name: Avon (Montevideo)

Carrier Name: T-Mobile (App#: 134550, v1)

Carrier Site ID / Name: CT11284A / SBA Avon/RT 1777

Site Location: 81 Montevideo Road

Avon, Connecticut

HARTFORD County

Latitude: 41.803100

Longitude: -72.801300



Max Structural Usage: 90.0% [Pass]

Max Foundation Usage: 75.0% [Pass]

Additional Usage Caused by New Mount/Mount Modification: N/A

Report Prepared by: Matthew Baker

Introduction

The purpose of this report is to summarize the analysis results on the 150 ft PIROD Self Supporting Tower to support the proposed antennas and transmission lines in addition to those currently installed. Any modification listed under Sources of Information was assumed completed and was included in this analysis.

Sources of Information

Tower Drawings	Valmont Eng. File # A-123251-, Archive # F-1010188, dated 11/29/2007
Foundation Drawing	Valmont Eng. File # A-123251-, Archive # F-1010188, dated 11/29/2007
Geotechnical Report	Dr. Clarence Welti, P.E., P.C Geotechnical Report (for URS Corp. Project # 36924843, Job # MCM 007), dated 11/06/2007
Modification Drawings	N/A

Analysis Criteria

The rigorous analysis was performed in accordance with the requirements and stipulations of the TIA-222-G-2. In accordance with this standard, the structure was analyzed using **TESTowers**, a proprietary analysis software. The program considers the structure as an elastic 3-D model with second-order effects and temperature effects incorporated in the analysis. The analysis was performed using multiple wind directions.

Wind Speed Used in the Analysis: Ultimate Design Wind Speed $V_{ult} = 120.0 \text{ mph (3-Sec. Gust)}/$

Nominal Design Wind Speed $V_{asd} = 93.0 \text{ mph}$ (3-Sec. Gust)

Wind Speed with Ice: 50 mph (3-Sec. Gust) with 1" radial ice concurrent

Operational Wind Speed: 60 mph + 0" Radial ice

Standard/Codes: TIA-222-G-2 / 2015 IBC / 2018 Connecticut State Building

Code

Exposure Category: B
Structure Class: II
Topographic Category: 4
Crest Height: 520 ft

Seismic Parameters: $S_S = 0.181, S_1 = 0.064$

This structural analysis is based upon the tower being classified as a Structure Class II; however, if a different classification is required subsequent to the date hereof, the tower classification will be changed to meet such requirement and a new structural analysis will be run.

Existing Antennas, Mounts and Transmission Lines

The table below summarizes the antennas, mounts and transmission lines that were considered in the analysis as existing on the tower.

Items	Elevation (ft)	Qty.	Antenna Descriptions	Mount Type & Qty.	Transmission Lines	Owner
1	159.8	1	10' Omni	Direct	(1) 7/8"	Unknown
2		2	RFS - APXVSPP18-C-A20 - Panel			
3	147.0	3	RFS - APXVSPP18-C-A20 - Panel	(3) T-Frames		Consint
4		3	Alcatel Lucent - RRH2x20-25 - RRH		(4) 1-1/4" Fiber	Sprint Nextel
5	143.7	3	Alcatel Lucent - 800 MHz RRH	Direct		Nexter
6	140.1	3	Alcatel Lucent - 1900 MHz RRH	Direct		
-		1	Ericsson - AIR 21 - Panel			
_		1	Ericsson - AIR 32 KRD901146-1_B66A -		(6) 1 5/8"	T-Mobile
	136.0		Panel	(1) Sector Frame	(2) 1 1/4"	
-	150.0	1	RFS - APXVAARR24_43-U-NA20 - Panel	(1) Sector France	Hybrid	1 WIODIIC
-		1	Ericsson - KRY 112 144/2 - TMA		TTYDITA	
-		1	Ericsson - 4449 B71 + B12 - RRH			
14	126.8	1	Omni 10'	(1) Standoff	(1) 1 1/4"	
15	120.6	1	Omni 20'	(1) Standoff	(1) 7/8"	
16	113.2	1	Dipole 10'	(1) Standoff	(1) 7/8"	
17	104.5	1	Omni 15'	(1) Standoff	(1) 7/8"	Unknown
18	99.8	1	Element 6' - Yagi	Direct	(1) 1/2"	
19	76.8	1	4.5' Parabolic Dish	(1) Standoff	(1) 1/4"	
20	73.0	1	4.5' Parabolic Dish	(1) Standoff	(1) 1/4"	
21	72.4	1	3.0"x2.5' GPS	Direct	(1) 1/2"	
22	67.3	1	3.0"x1.2' GPS	Direct	(1) 1/4"	
23	13.9	1	3.0"x1.5' GPS	(1) Standoff	(2) 1/2"	

Proposed Carrier's Final Configuration of Antennas, Mounts and Transmission Lines

Information pertaining to the proposed carrier's final configuration of antennas and transmission lines was provided by SBA Communications Corp. The proposed antennas and lines are listed below.

Items	Elevation (ft)	Qty.	Antenna Descriptions	Mount Type & Qty.	Transmission Lines	Owner
7		1	RFS - APXVAARR24_43-U-NA20 (Octa) - Panel			
8		1	Ericsson - AIR32 KRD901146-1_B66A (Octa) - Panel		(5) 1 5/8"	
9	136.0	1	Ericsson - AIR 21 - Panel	(1) Sector Frame	(3) 1 1/4"	T-Mobile
10		1	Ericsson - AIR6449 B41 - Panel		Hybrid	
11		1	Ericsson - KRY 112 144/2 - TMA			
12		1	Ericsson - Radio 4449 B71 + B12 - RRH			
13		1	Ericsson - Radio 4415 B25 - RRH			

See the attached coax layout for the line placement considered in the analysis.

Analysis Results

The results of the structural analysis, performed for the wind and ice loading and antenna equipment as defined above, are summarized as the following:

Tower Component	Legs	Diagonals	Horizontals	
Max. Usage:	90.0%	87.9%	41.8%	
Pass/Fail	Pass	Pass	Pass	

Foundations

	Compression (Kips)	Uplift (Kips)	Shear (Kips)
Analysis Reactions	278.9	255.2	27.4

The foundation has been investigated using the supplied documents and soils report and was found adequate. Therefore, no modification to the foundation will be required.

Operational Condition (Rigidity):

The maximum twist and sway of the microwave dishes under the operational wind speed as specified in the Analysis Criteria are listed in the table below:

Elevation (ft)	Antenna / Dish	Carrier	Twist (deg)	Sway (deg)
76.8	4.5' Parabolic Dish	Unknown	0.447	0.261
73.0	4.5' Parabolic Dish	Unknown	0.414	0.216

It is recommended that the carriers review the twist and sway values of the microwave dishes.

Conclusions

Based on the analysis results, the existing structure and its foundation were found to be adequate to safely support the existing and proposed equipment and meet the minimum requirements per the ANSI/TIA/EIA 222-G Standard under the design basic wind speed as specified in the Analysis Criteria.

Standard Conditions

- 1. This analysis was performed based on the information supplied to (TES) Tower Engineering Solutions, LLC. Verification of the information provided was not included in the Scope of Work for TES. The accuracy of the analysis is dependent on the accuracy of the information provided.
- 2. The structural analysis was performance based upon the evidence available at the time of this report. All information provided by the client is considered to be accurate.
- 3. The analyses will be performed based on the codes as specified by the client or based on the best knowledge of the engineering staff of TES. In the absence of information to the contrary, all work will be performed in accordance with the latest relevant revision of ANSI/TIA-222. If wind speed and/or ice loads are different from the minimum values recommended by the EIA/TIA-222 standard or other codes, TES should be notified in writing and the applicable minimum values provided by the client.
- 4. The configuration of the existing mounts, antennas, coax and other appurtenances were supplied by the customer for the current structural analysis. TES has not visited the tower site to verify the adequacy of the information provided. If there is any discrepancy found in the report regarding the existing conditions, TES should be notified immediately to evaluate the effect of the discrepancy on the analysis results.
- 5. The client will assume responsibility for rework associated with the differences in initially provided information, including tower and foundation information, existing and/or proposed equipment and transmission lines.
- 6. If a feasibility analysis was performed, final acceptance of changed conditions shall be based upon a rigorous structural analysis.

Structure: CT22071-A-SBA

Site Name: Avon (Montevideo) Code: EIA/TIA-222-G

Type:Self SupportBase Shape:TriangleBasic WS:93.00Height:150.00 (ft)Base Width:14.00Basic Ice WS:50.00

Base Elev: 0.00 (ft) Top Width: 5.00 Operational WS: 60.00 Page: 1



6/30/2020

Sect Leg Members Diagonal Members Horizontal Members
1 12B 12"BD 1.75" SAE 3X3X0.3125
2 12B 12"BD 1.75" SAE 3X3X0.1875
3 12B 12"BD 1.75" SAE 2.5X2.5X0.1875
4-5 12B 12"BD 1.5" SAE 2.5X2.5X0.1875
6 SOL 2 1/4" SOLID SOL 1" SOLID SOL 1" SOLID
7 SOL 2" SOLID SOL 7/8" SOLID SOL 7/8" SOLID
8 SOL 1 3/4" SOLID SOL 7/8" SOLID SOL 7/8" SOLID
Discrete Appurtenances
Attach Force
Elev (ft) Elev (ft) Qty Description
150.00 150.00 1 Lightning Rod
150.00 150.00 1 Beacon
150.00 159.80 1 10' Omni
147.00 147.00 3 I-Frames
147.00
147.00 147.00 3 APXV9TM14-ALU-I20
147.00 147.00 3 RRH2x20-25
143.70 143.70 3 800 MHz RRH
140.10
136.00 136.00 1 Sector Frame 136.00 136.00 1 APXVAARR24_43-U-NA20
136.00
136.00 136.00 1 AIR32 136.00 136.00 1 AIR 21
136.00 136.00 1 AIR 21 136.00 136.00 1 AIR 6449 B41
136.00 136.00 1 KRY 112 144/2
136.00 136.00 1 KKY 112 144/2 54
136.00 136.00 1 RRUS 4415 B25
119.30 119.30 1 Side Arm (M. Heavy)
119.30 126.80 1 10' Omni
116.30 116.30 1 Side Arm (M. Heavy)
116.30 126.80 1 20' Omni
106.60 106.60 1 Side Arm (M. Heavy)
106.60 113.20 1 10' Dipole
99.80 99.80 1 6' Yaqi
96.00 96.00 1 Side Arm (M. Heavy)
96.00 104.50 1 15' Omni
76.80 76.80 1 Side Arm (I Heavy)
76.80 76.80 1 4.5' Std. Dish
73.00 73.00 1 Side Arm (M. Heavy)
73.00 73.00 1 4' Std. Dish
72.40 72.40 1 3.05 x 2.5 GPS
72.40
12.30 13.90 1 Antenna Mount, 24" Short Strai
12.30 12.30 1 3.05 x 1.5 GPS
Linear Appurtenances
Elev Elev
From (ft) To (ft) Qty Description
0.00 150.00 1 7/8" Coax
0.00 147.00 4 1-1/4" Fiber
0.00 147.00 1 W/G Ladder
0.00 136.00 3 1 1/4" Coax
0.00 136.00 5 1 5/8" Coax

Structure: CT22071-A-SBA

Site Name: Avon (Montevideo) Code: EIA/TIA-222-G 6/30/2020

Type:Self SupportBase Shape:TriangleBasic WS:93.00Height:150.00 (ft)Base Width:14.00Basic Ice WS:50.00

Base Elev: 0.00 (ft) **Top Width:** 5.00 **Operational WS:** 60.00 Page: 2



0.00	13.90	2	1/2" Coax
0.00	67.30	1	1/4" Coax
0.00	72.40	1	1/2" Coax
0.00	73.00	1	1/4" Coax
0.00	76.80	1	1/4" Coax
0.00	96.00	1	7/8" Coax
0.00	99.80	1	1/2" Coax
0.00	106.60	1	7/8" Coax
0.00	116.30	1	7/8" Coax
0.00	119.30	1	1 1/4" Coax
0.00	136.00	1	W/G Ladder

Base Reactions

Overturning

39.75 (kips)

 Max Uplift:
 -255.24 (kips
 Moment:
 3268.65 (ft-kips)

 Max Down:
 278.90 (kips
 Total Down:
 27.91 (kips)

27.40 (kips Total Shear:

Leg

Max Shear:

Structure: CT22071-A-SBA

Site Name: Avon (Montevideo) Code: EIA/TIA-222-G 6/30/2020

Type:Self SupportBase Shape:TriangleHeight:150.00 (ft)Base Width:14.00Base Elev:0.00 (ft)Top Width:5.00

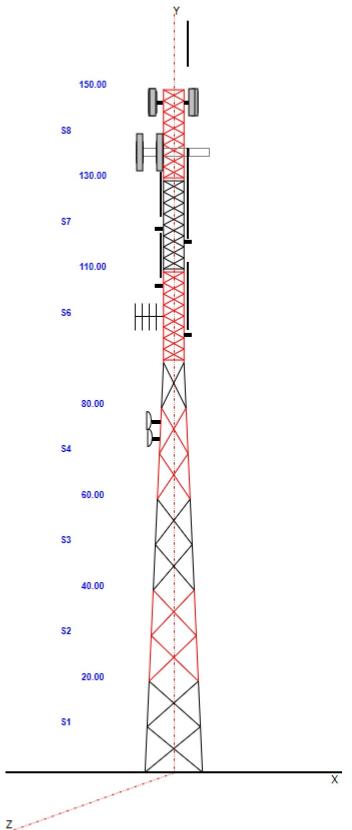
 Basic WS:
 93.00

 Basic Ice WS:
 50.00

 Operational WS:
 60.00

Page: 3





Structure: CT22071-A-SBA - Coax Line Placement

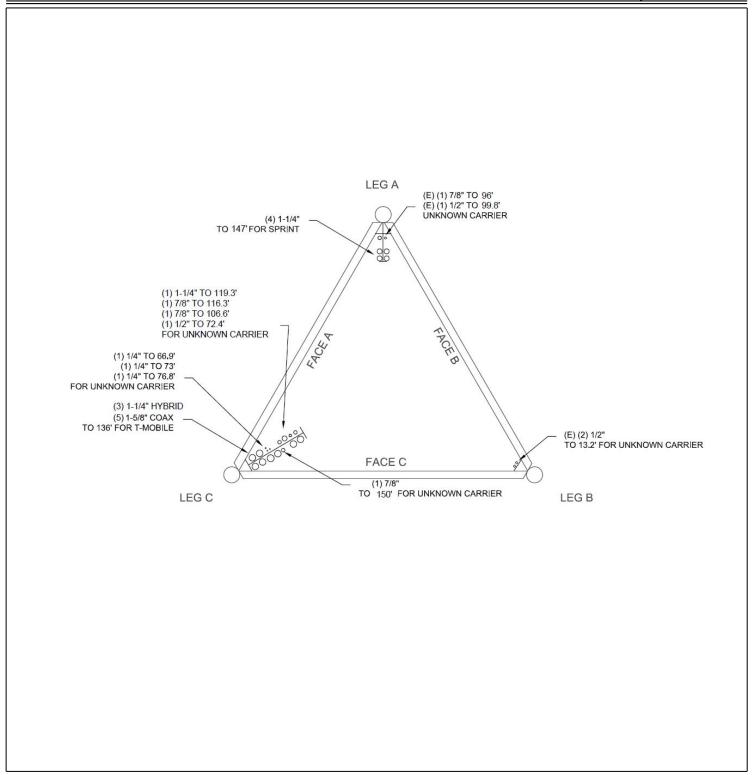
Type: Self Support 6/30/2020

Site Name: Avon (Montevideo)

Height: 150.00 (ft)

Tower Engineering Solutions

Page: 4



Loading Summary

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) Exposure: B

Height: 150.00 (ft) **Crest Height:** 520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II



Page: 5

Discrete Appurtenances Properties

	• •	_		lo Ice	lce	Э						
Attach Elev (ft)	Description	Qty	Weight (lb)	CaAa (sf)	Weight (lb)	CaAa (sf)	Len (in)	Width (in)	Depth (in)	Ka	Orientation Factor	Vert Ecc (ft)
150.00	Lightning Rod	1	5.00	0.500	40.77	3.481	72.000	1.000	1.000	1.00	1.00	0.000
150.00	Beacon	1	36.00	2.720	263.52	4.342	28.000	17.500	17.500	1.00	1.00	0.000
150.00	10' Omni	1	25.00	3.000	154.92	9.160	120.000	3.000	3.000	1.00	1.00	9.800
147.00	T-Frames	3	120.00	4.500	298.87	13.461	0.000	0.000	0.000	0.75	0.75	0.000
147.00	APXVSPP18-C-A20	2	57.00	8.020	352.26	12.792	72.000	11.800	7.000	0.80	0.83	0.000
147.00	APXV9TM14-ALU-I20	3	55.10	6.340	335.52	8.275	56.300	12.600	6.300	0.80	0.78	0.000
147.00	RRH2x20-25	3	70.00	4.050	287.75	5.514	26.100	18.600	6.700	0.80	0.67	0.000
143.70	800 MHz RRH	3	53.00	2.490	179.34	4.444	19.700	13.000	10.800	1.00	1.00	0.000
140.10	1900MHz RRH	3	44.00	3.800	230.47	6.174	23.000	13.000	17.000	1.00	1.00	0.000
136.00	Sector Frame	1	400.00	10.000	876.98	24.906	0.000	0.000	0.000	1.00	1.00	0.000
136.00	APXVAARR24_43-U-NA20	1	128.00	20.240	929.62	23.522	95.900	24.000	7.800	0.90	0.70	0.000
136.00	AIR32	1	132.20	6.510	441.18	8.459	57.000	12.900	8.700	0.90	0.86	0.000
136.00	AIR 21	1	91.00	6.090	420.30	8.051	56.000	12.100	7.900	0.90	0.85	0.000
136.00	AIR6449 B41	1	104.00	5.680	351.41	7.367	33.100	20.600	8.600	0.90	0.72	0.000
136.00	KRY 112 144/2	1	11.00	0.410	29.42	1.222	6.900	6.100	2.700	0.90	0.50	0.000
136.00	4449	1	70.00	1.650	209.00	2.640	15.000	13.200	9.300	0.90	0.67	0.000
136.00	RRUS 4415 B25	1	46.00	1.640	116.21	2.520	15.000	13.200	5.400	0.90	0.67	0.000
119.30	Side Arm (M. Heavy)	1	160.00	6.000	397.81	17.914	0.000	0.000	0.000	1.00	1.00	0.000
119.30	10' Omni	1	25.00	3.000	154.55	9.143	120.000	3.000	3.000	1.00	1.00	7.500
116.30	Side Arm (M. Heavy)	1	160.00	6.000	397.81	17.914	0.000	0.000	0.000	1.00	1.00	0.000
116.30	20' Omni	1	55.00	6.000	311.62	18.085	240.000	3.000	3.000	1.00	1.00	10.50
106.60	Side Arm (M. Heavy)	1	160.00	6.000	396.58	17.853	0.000	0.000	0.000	1.00	1.00	0.000
106.60	10' Dipole	1	30.00	3.760	219.08	13.928	120.000	3.000	3.000	1.00	1.00	6.600
99.80	6' Yagi	1	25.00	8.950	457.06	49.456	72.000	60.000	3.000	1.00	1.00	0.000
96.00	Side Arm (M. Heavy)	1	160.00	6.000	396.58	17.853	0.000	0.000	0.000	1.00	1.00	0.000
96.00	15' Omni	1	40.00	4.500	232.11	13.571	180.000	3.000	3.000	1.00	1.00	8.500
76.80	Side Arm (L. Heavy)	1	120.00	4.500	294.78	13.256	0.000	0.000	0.000	1.00	1.00	0.000
76.80	4.5' Std. Dish	1	188.00	26.000	543.97	32.392	48.000	48.000	0.000	1.00	1.00	0.000
73.00	Side Arm (M. Heavy)	1	160.00	6.000	393.04	17.675	0.000	0.000	0.000	1.00	1.00	0.000
73.00	4' Std. Dish	1	188.00	26.000	543.97	32.392	48.000	48.000	0.000	1.00	1.00	0.000
72.40	3.05 x 2.5 GPS	1	0.30	0.380	4.44	2.232	2.600	3.000	0.000	1.00	1.00	0.000
72.40	3.05 x 1.2 GPS	1	0.30	0.240	4.44	1.410	2.600	3.000	0.000	1.00	1.00	0.000
12.30	Antenna Mount, 24" Short Strai	1	50.00	1.500	175.38	4.008	0.000	0.000	0.000	1.00	1.00	1.600
12.30	3.05 x 1.5 GPS	1	0.30	0.260	3.87	1.351	2.600	3.000	0.000	1.00	1.00	0.000

Totals: 45 3,710.40 13,460.73 Number of Appurtenances : 34

Loading Summary

Structure: CT22071-A-SBA **Code**: EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) Exposure: B

Height: 150.00 (ft) **Crest Height:** 520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II Page: 6



Linear Appurtenances Properties

Elev. From (ft)	Elev. To (ft)	Description	Qty	Width (in)	Weight (lb/ft)	Pct In Block	Spread On Faces	Bundling Arrangement	Cluster Dia (in)	Out of Zone	Spacing (in)	Orientation Factor	Ka Override
0.00	150.00	7/8" Coax	1	1.11	0.52	100.00	2	Individual NR		N	0.50	1.00	
0.00	147.00	1-1/4" Fiber	4	1.25	0.95	50.00	3	Block		Ν	0.50	0.96	
0.00	147.00	W/G Ladder	1	1.00	6.00	100.00	3	Individual NR		Ν	0.50	1.00	
0.00	136.00	1 1/4" Coax	3	1.55	0.66	50.00	2	Block		Ν	0.50	1.00	
0.00	136.00	1 5/8" Coax	5	1.98	1.04	50.00	2	Block		Ν	0.50	1.00	
0.00	136.00	W/G Ladder	1	1.00	6.00	100.00	2	Individual NR		Ν	0.50	1.00	
0.00	119.30	1 1/4" Coax	1	1.55	0.66	100.00	2	Individual NR		Ν	0.50	1.00	
0.00	116.30	7/8" Coax	1	1.11	0.52	100.00	2	Individual NR		Ν	0.50	1.00	
0.00	106.60	7/8" Coax	1	1.11	0.52	100.00	2	Individual NR		Ν	0.50	1.00	
0.00	99.80	1/2" Coax	1	0.65	0.16	100.00	3	Individual NR		Ν	0.50	1.00	0
0.00	96.00	7/8" Coax	1	1.11	0.52	100.00	3	Individual NR		Ν	0.50	1.00	
0.00	76.80	1/4" Coax	1	0.25	0.04	100.00	2	Individual NR		Ν	0.50	1.00	0
0.00	73.00	1/4" Coax	1	0.25	0.04	100.00	2	Individual NR		Ν	0.50	1.00	0
0.00	72.40	1/2" Coax	1	0.65	0.16	100.00	2	Individual NR		Ν	0.50	1.00	0
0.00	67.30	1/4" Coax	1	0.25	0.04	100.00	2	Individual NR		Ν	0.50	1.00	0
0.00	13.90	1/2" Coax	2	0.65	0.16	100.00	1	Individual IR		Ν	0.50	1.00	

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II



Load Case: 1.2D + 1.6W Normal Wind - P1 1.2D + 1.6W 93 mph Wind at Normal To Face - P1

Wind Load Factor: 1.60 Wind Importance Factor: 1.00

Dead Load Factor: 1.20 lce Dead Load Factor: 0.00

Ice Importance Factor: 1.00

	Sect Seq	Wind Height (ft)	Total Flat qz Area (psf) (sqft)	Total Round Area (sqft)	Ice Round Area (sqft)	Sol Ratio	Cf	Df	Dr	Ice Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Ice Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
_	ОСЧ														• • •			
1	1	10.0	35.36 15.937	18.83	0.00	0.13	2.85	1.00	1.00	0.00	24.00	40.81	0.00	4,620.9	0.0	3290.14	1560.21	4,850.35
1	2	30.0	33.86 14.403	18.83	0.00	0.14	2.79	1.00	1.00	0.00	22.72	39.30	0.00	3,969.0	0.0	2919.06	1444.14	4,363.20
1	3	50.0	37.55 10.827	18.83	0.00	0.16	2.75	1.00	1.00	0.00	18.97	39.30	0.00	3,769.5	0.0	2661.35	1601.37	4,262.72
1	4	70.0	39.67 9.814	17.23	0.00	0.18	2.66	1.00	1.00	0.00	17.75	38.41	0.00	3,257.4	0.0	2545.55	1691.46	4,237.01
1	5	85.0	40.71 4.578	8.61	0.00	0.22	2.52	1.00	1.00	0.00	8.70	18.48	0.00	1,608.8	0.0	1214.76	867.24	2,082.00
1	6	100.0	41.42 0.000	15.46	0.00	0.15	2.78	1.00	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04 0.000	13.66	0.00	0.13	2.84	1.00	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38 0.000	12.85	0.00	0.12	2.87	1.00	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
														23,458.4	0.0	<u></u>		27,607.02

Load Case: 1.2D + 1.6W Normal Wind - P2 1.2D + 1.6W 93 mph Wind at Normal To Face - P2

Wind Load Factor: 1.60
Dead Load Factor: 1.20
Ice Dead Load Factor: 0.00
Wind Importance Factor: 1.00
Ice Importance Factor: 1.00

				i otai	i otai	ice								ice					
	Sect Seq	Wind Height (ft)		Flat Area (sqft)	Round Area (sqft)	Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	l 1	10.0	19.45	5 15.937	18.83	0.00	0.13	2.85	1.00	1.00	0.00	24.00	40.81	0.00	4,620.9	0.0	1809.58	858.12	2,667.69
1	2	30.0	18.62	2 14.403	18.83	0.00	0.14	2.79	1.00	1.00	0.00	22.72	39.30	0.00	3,969.0	0.0	1605.49	794.28	2,399.76
1	l 3	50.0	20.65	10.827	18.83	0.00	0.16	2.75	1.00	1.00	0.00	18.97	39.30	0.00	3,769.5	0.0	1463.74	880.75	2,344.50
1	l 4	70.0	21.82	9.814	17.23	0.00	0.18	2.66	1.00	1.00	0.00	17.75	38.41	0.00	3,257.4	0.0	1400.05	930.30	2,330.36
1	5	85.0	22.39	4.578	8.61	0.00	0.22	2.52	1.00	1.00	0.00	8.70	18.48	0.00	1,608.8	0.0	668.12	476.98	1,145.10
1	l 6	100.0	22.78	0.000	15.46	0.00	0.15	2.78	1.00	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	767.91	934.66	1,702.57
1	1 7	120.0	23.12	2 0.000	13.66	0.00	0.13	2.84	1.00	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	700.84	841.05	1,541.89
1	l 8	140.0	23.31	0.000	12.85	0.00	0.12	2.87	1.00	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	670.07	381.92	1,051.99
															23 458 4	0.0	<u> </u>		15.183.86

Structure: CT22071-A-SBA Code: EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) **Exposure:** В Height: 150.00 (ft) Crest Height: 520.00

C - Very Dense Soil Base Elev: 0.000 (ft) Site Class:

Gh: 0.85 Topography: 4 Struct Class: ||

1.60

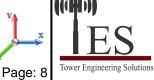
1.20

0.00

Load Case: 1.2D + 1.6W Normal Wind - P3 Wind Load Factor:

Dead Load Factor:

Ice Dead Load Factor:



1.2D + 1.6W 93 mph Wind at Normal To Face - P3

Wind Importance Factor: 1.00

> Ice Importance Factor: 1.00

Sec Sec	Wind Height (ft)	Total Flat qz Area (psf) (sqft)	Total Round Area (sqft)	Ice Round Area (sqft)	Sol Ratio	Cf	Df	Dr	Ice Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Ice Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1 1	10.0	35.36 15.937	18.83	0.00	0.13	2.85	1.00	1.00	0.00	24.00	40.81	0.00	4,620.9	0.0	3290.14	1560.21	4,850.35
1 2	30.0	33.86 14.403	18.83	0.00	0.14	2.79	1.00	1.00	0.00	22.72	39.30	0.00	3,969.0	0.0	2919.06	1444.14	4,363.20
1 3	50.0	37.55 10.827	18.83	0.00	0.16	2.75	1.00	1.00	0.00	18.97	39.30	0.00	3,769.5	0.0	2661.35	1601.37	4,262.72
1 4	70.0	39.67 9.814	17.23	0.00	0.18	2.66	1.00	1.00	0.00	17.75	38.41	0.00	3,257.4	0.0	2545.55	1691.46	4,237.01
1 5	85.0	40.71 4.578	8.61	0.00	0.22	2.52	1.00	1.00	0.00	8.70	18.48	0.00	1,608.8	0.0	1214.76	867.24	2,082.00
1 6	100.0	41.42 0.000	15.46	0.00	0.15	2.78	1.00	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1 7	120.0	42.04 0.000	13.66	0.00	0.13	2.84	1.00	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1 8	140.0	42.38 0.000	12.85	0.00	0.12	2.87	1.00	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
													23.458.4	0.	<u></u>		27.607.02

Load Case: 1.2D + 1.6W 60° Wind - P1 1.2D + 1.6W 93 mph Wind at 60° From Face - P1

Wind Load Factor: 1.60 Wind Importance Factor: 1.00 **Dead Load Factor:** 1.20 Ice Importance Factor: 1.00 Ice Dead Load Factor: 0.00

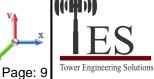
				Total	Total	Ice								Ice					
	Sect Seq	Wind Height (ft)	qz (psf)	Flat Area (sqft)	Round Area (sqft)	Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	1	10.0	35.36	5 15.937	18.83	0.00	0.13	2.85	0.80	1.00	0.00	20.82	40.81	0.00	4,620.9	0.0	2853.28	1560.21	4,413.49
1	2	30.0	33.86	3 14.403	18.83	0.00	0.14	2.79	0.80	1.00	0.00	19.83	39.30	0.00	3,969.0	0.0	2548.90	1444.14	3,993.04
1	3	50.0	37.55	5 10.827	18.83	0.00	0.16	2.75	0.80	1.00	0.00	16.80	39.30	0.00	3,769.5	0.0	2357.56	1601.37	3,958.93
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.80	1.00	0.00	15.79	38.41	0.00	3,257.4	0.0	2264.13	1691.46	3,955.59
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.80	1.00	0.00	7.78	18.48	0.00	1,608.8	0.0	1086.90	867.24	1,954.14
1	6	100.0	41.42	2 0.000	15.46	0.00	0.15	2.78	0.80	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	1 0.000	13.66	0.00	0.13	2.84	0.80	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.80	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
															23.458.4	0.	0		26.086.93

Code: 6/30/2020 Structure: CT22071-A-SBA EIA/TIA-222-G

Site Name: Avon (Montevideo) **Exposure:** В 150.00 (ft) Crest Height: 520.00 Height:

C - Very Dense Soil Base Elev: 0.000 (ft) Site Class:

Gh: 0.85 Topography: 4 Struct Class: ||



1.00

14,347.81

0.0

23,458.4

Wind Importance Factor:

Load Case: 1.2D + 1.6W 60° Wind - P2 1.2D + 1.6W 93 mph Wind at 60° From Face - P2

1.60 Wind Load Factor: **Dead Load Factor:** 1.20

0.00 Ice Importance Factor: 1.00 Ice Dead Load Factor:

Total Total Ice Ice Wind Flat Round Round Ice Eff Linear Linear Total Struct Linear **Total** Sect Height qz Area Sol Thick Area Weight Weight **Force Force Force** Area Area Area Area Seq (ft) (psf) (sqft) (sqft) (sqft) Ratio Cf Df Dr (in) (sqft) (sqft) (sqft) (lb) Ice (lb) (lb) (lb) (lb) 1 10.0 19.45 15.937 0.00 0.13 2.85 0.80 1.00 0.00 20.82 40.81 0.00 4,620.9 0.0 1569.30 858.12 2,427.42 1 18.83 1 2 30.0 18.62 14.403 18.83 0.00 0.14 2.79 0.80 1.00 0.00 19.83 39.30 0.00 3,969.0 0.0 1401.89 794.28 2,196.17 1 3 50.0 20.65 10.827 18.83 0.00 0.16 2.75 0.80 1.00 0.00 16.80 39.30 0.00 3,769.5 0.0 1296.66 880.75 2,177.41 1 4 70.0 21.82 9.814 17.23 0.00 0.18 2.66 0.80 1.00 0.00 15.79 38.41 0.00 3,257.4 0.0 1245.27 930.30 2,175.57 1 5 85.0 22.39 4.578 8.61 0.00 0.22 2.52 0.80 1.00 0.00 7.78 18.48 0.00 1,608.8 597.80 476.98 1,074.78 1 6 100.0 22.78 0.000 15.46 0.00 0.15 2.78 0.80 1.00 0.00 8.93 34.80 0.00 2,534.1 0.0 767.91 934.66 1,702.57 1 7 120.0 23.12 0.000 13.66 0.00 0.13 2.84 0.80 1.00 0.00 7.85 29.53 0.00 2,073.5 0.0 700.84 841.05 1,541.89 1 8 140.0 23.31 0.000 12.85 0.00 0.12 2.87 0.80 1.00 0.00 7.37 13.29 0.00 1,625.1 0.0 670.07 381.92 1,051.99

Load Case: 1.2D + 1.6W 60° Wind - P3 1.2D + 1.6W 93 mph Wind at 60° From Face - P3

1.60 Wind Load Factor: Wind Importance Factor: 1.00 **Dead Load Factor:** 1.20 1.00 Ice Dead Load Factor: 0.00 Ice Importance Factor:

				Total	Total	Ice								Ice					
	Sect Seq	Wind Height (ft)	qz (psf)	Flat Area (sqft)	Round Area (sqft)	Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	1	10.0	35.36	5 15.937	18.83	0.00	0.13	2.85	0.80	1.00	0.00	20.82	40.81	0.00	4,620.9	0.0	2853.28	1560.21	4,413.49
1	2	30.0	33.86	3 14.403	18.83	0.00	0.14	2.79	0.80	1.00	0.00	19.83	39.30	0.00	3,969.0	0.0	2548.90	1444.14	3,993.04
1	3	50.0	37.55	5 10.827	18.83	0.00	0.16	2.75	0.80	1.00	0.00	16.80	39.30	0.00	3,769.5	0.0	2357.56	1601.37	3,958.93
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.80	1.00	0.00	15.79	38.41	0.00	3,257.4	0.0	2264.13	1691.46	3,955.59
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.80	1.00	0.00	7.78	18.48	0.00	1,608.8	0.0	1086.90	867.24	1,954.14
1	6	100.0	41.42	2 0.000	15.46	0.00	0.15	2.78	0.80	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	1 0.000	13.66	0.00	0.13	2.84	0.80	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.80	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
															23.458.4	0.	0		26.086.93

CT22071-A-SBA Code: 6/30/2020 Structure: EIA/TIA-222-G

Site Name: Avon (Montevideo) **Exposure:** В Height: 150.00 (ft) Crest Height: 520.00

C - Very Dense Soil Base Elev: 0.000 (ft) Site Class:

Gh: 0.85 Topography: 4 Struct Class: ||



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Load Case: 1.2D + 1.6W 90° Wind - P1

1.60 Wind Load Factor:

Dead Load Factor: 1.20 Ice Dead Load Factor: 0.00

1.2D + 1.6W 93 mph Wind at 90° From Face - P1

Wind Importance Factor: 1.00

Ice Importance Factor: 1.00

				Total	Total	Ice								Ice					
		Wind		Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
	_	Height	qz	Area	Area	Area	Sol			_	Thick	Area	Area	Area	Weight	Weight	Force	Force	Force
	Seq	(ft)	(psf)	(sqft)	(sqft)	(sqft)	Ratio	Cf	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (lb)	(lb)	(lb)	(lb)
1	1	10.0	35.36	15.937	18.83	0.00	0.13	2.85	0.85	1.00	0.00	21.61	40.81	0.00	4,620.9	0.0	2962.49	1560.21	4,522.71
1	2	30.0	33.86	14.403	18.83	0.00	0.14	2.79	0.85	1.00	0.00	20.56	39.30	0.00	3,969.0	0.0	2641.44	1444.14	4,085.58
1	3	50.0	37.55	10.827	18.83	0.00	0.16	2.75	0.85	1.00	0.00	17.35	39.30	0.00	3,769.5	0.0	2433.51	1601.37	4,034.88
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.85	1.00	0.00	16.28	38.41	0.00	3,257.4	0.0	2334.49	1691.46	4,025.94
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.85	1.00	0.00	8.01	18.48	0.00	1,608.8	0.0	1118.87	867.24	1,986.10
1	6	100.0	41.42	0.000	15.46	0.00	0.15	2.78	0.85	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	0.000	13.66	0.00	0.13	2.84	0.85	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.85	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
															23,458.4	0.0	0		26,466.95

Load Case: 1.2D + 1.6W 90° Wind - P2 1.2D + 1.6W 93 mph Wind at 90° From Face - P2

Wind Load Factor: 1.60 **Dead Load Factor:** 1.20 Ice Dead Load Factor: 0.00

Wind Importance Factor: 1.00

1.00 Ice Importance Factor:

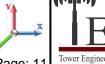
Total **Total** Ice Ice Wind Eff **Total** Flat Round Round Ice Linear Linear Total Struct Linear Sect Height Area Area Sol Thick Area Area Weight Weight **Force Force** Force αz Area Area Seq (ft) (psf) (sqft) (sqft) (sqft) Ratio Cf Df Dr (in) (sqft) (sqft) (sqft) (lb) Ice (lb) (lb) (lb) (lb) 18.83 0.85 1 10.0 19.45 15.937 0.00 0.13 2.85 1.00 0.00 21.61 40.81 0.00 4,620.9 0.0 1629.37 858.12 2,487.49 1 2 30.0 18.62 14.403 18.83 0.00 0.14 2.79 0.85 1.00 0.00 20.56 39.30 0.00 3,969.0 0.0 1452.79 794.28 2,247.07 1 3 50.0 20.65 10.827 18.83 0.00 0.16 2.75 0.85 1.00 0.00 17.35 39.30 0.00 3,769.5 0.0 1338.43 880.75 2,219.19 4 70.0 21.82 9.814 17.23 0.00 0.18 2.66 0.85 1.00 0.00 16.28 38.41 0.00 3,257.4 0.0 1283.97 930.30 2,214.27 22.39 4.578 0.00 0.22 2.52 8.01 18.48 615.38 476.98 1 5 85.0 8.61 0.85 1.00 0.00 0.00 1,608.8 0.0 1,092.36 6 100.0 22.78 0.000 15.46 0.00 0.15 2.78 0.85 1.00 0.00 8.93 34.80 0.00 2,534.1 0.0 767.91 934.66 1,702.57 1 1 7 120.0 23.12 0.000 13.66 0.00 0.13 2.84 0.85 1.00 0.00 7.85 29.53 0.00 2,073.5 0.0 700.84 841.05 1,541.89 8 140.0 23.31 0.000 12.85 0.00 0.12 2.87 0.85 1.00 0.00 7.37 13.29 0.00 1,625.1 0.0 670.07 381.92 1,051.99 23,458.4 0.0 14,556.82

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: ||



Page: 11 Tower Engineering Solutions

Wind Load Factor: 1.60 Wind Importance Factor: 1.00

Dead Load Factor: 1.20 Ice Dead Load Factor: 0.00

Ice Importance Factor: 1.00

				Total	Total	Ice								Ice					
		Wind		Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
			qz	Area	Area	Area	Sol	•	-		Thick	Area	Area	Area	Weight	3	Force	Force	Force
	Seq	(ft)	(pst)	(sqft)	(sqft)	(sqft)	Ratio	Cī	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (lb)	(lb)	(lb)	(lb)
1	1	10.0	35.36	5 15.937	18.83	0.00	0.13	2.85	0.85	1.00	0.00	21.61	40.81	0.00	4,620.9	0.0	2962.49	1560.21	4,522.71
1	2	30.0	33.86	3 14.403	18.83	0.00	0.14	2.79	0.85	1.00	0.00	20.56	39.30	0.00	3,969.0	0.0	2641.44	1444.14	4,085.58
1	3	50.0	37.55	5 10.827	18.83	0.00	0.16	2.75	0.85	1.00	0.00	17.35	39.30	0.00	3,769.5	0.0	2433.51	1601.37	4,034.88
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.85	1.00	0.00	16.28	38.41	0.00	3,257.4	0.0	2334.49	1691.46	4,025.94
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.85	1.00	0.00	8.01	18.48	0.00	1,608.8	0.0	1118.87	867.24	1,986.10
1	6	100.0	41.42	2 0.000	15.46	0.00	0.15	2.78	0.85	1.00	0.00	8.93	34.80	0.00	2,534.1	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	1 0.000	13.66	0.00	0.13	2.84	0.85	1.00	0.00	7.85	29.53	0.00	2,073.5	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.85	1.00	0.00	7.37	13.29	0.00	1,625.1	0.0	1218.32	694.40	1,912.72
															23.458.4	0.0	0		26.466.95

Load Case: 0.9D + 1.6W Normal Wind 0.9D + 1.6W 93 mph Wind at Normal To Face

Wind Load Factor: 1.60
Dead Load Factor: 0.90
Ice Dead Load Factor: 0.00
Wind Importance Factor: 1.00
Ice Importance Factor: 1.00

			Total	Total	lce								Ice					
		Wind	Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
	Sect	Height	qz Area	Area	Area	Sol				Thick	Area	Area	Area	Weight	Weight	Force	Force	Force
	Seq	(ft)	(psf) (sqft)	(sqft)	(sqft)	Ratio	Cf	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (Ib)	(lb)	(lb)	(lb)
1	1	10.0	35.36 15.93	7 18.83	0.00	0.13	2.85	1.00	1.00	0.00	24.00	40.81	0.00	3,465.7	0.0	3290.14	1560.21	4,850.35
1	2	30.0	33.86 14.40	3 18.83	0.00	0.14	2.79	1.00	1.00	0.00	22.72	39.30	0.00	2,976.7	0.0	2919.06	1444.14	4,363.20
1	3	50.0	37.55 10.82	7 18.83	0.00	0.16	2.75	1.00	1.00	0.00	18.97	39.30	0.00	2,827.2	0.0	2661.35	1601.37	4,262.72
1	4	70.0	39.67 9.81	4 17.23	0.00	0.18	2.66	1.00	1.00	0.00	17.75	38.41	0.00	2,443.1	0.0	2545.55	1691.46	4,237.01
1	5	85.0	40.71 4.57	8 8.61	0.00	0.22	2.52	1.00	1.00	0.00	8.70	18.48	0.00	1,206.6	0.0	1214.76	867.24	2,082.00
1	6	100.0	41.42 0.00	0 15.46	0.00	0.15	2.78	1.00	1.00	0.00	8.93	34.80	0.00	1,900.6	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04 0.00	0 13.66	0.00	0.13	2.84	1.00	1.00	0.00	7.85	29.53	0.00	1,555.1	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38 0.00	0 12.85	0.00	0.12	2.87	1.00	1.00	0.00	7.37	13.29	0.00	1,218.8	0.0	1218.32	694.40	1,912.72
														17,593.8	0.0	<u></u>		27,607.02

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II





Load Case: 0.9D + 1.6W 60° Wind 0.9D + 1.6W 93 mph Wind at 60° From Face

Wind Load Factor: 1.60 Wind Importance Factor: 1.00

Dead Load Factor: 0.90 Ice Dead Load Factor: 0.00

Ice Importance Factor: 1.00

				Total	Total	lce								Ice					
		Wind		Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
	Sect	Height	qz	Area	Area	Area	Sol				Thick	Area	Area	Area	Weight	Weight	Force	Force	Force
	Seq	(ft)	(psf)	(sqft)	(sqft)	(sqft)	Ratio	Cf	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (Ib)	(lb)	(lb)	(lb)
1	1	10.0	35.36	15.937	18.83	0.00	0.13	2.85	0.80	1.00	0.00	20.82	40.81	0.00	3,465.7	0.0	2853.28	1560.21	4,413.49
1	2	30.0	33.86	14.403	18.83	0.00	0.14	2.79	0.80	1.00	0.00	19.83	39.30	0.00	2,976.7	0.0	2548.90	1444.14	3,993.04
1	3	50.0	37.55	10.827	18.83	0.00	0.16	2.75	0.80	1.00	0.00	16.80	39.30	0.00	2,827.2	0.0	2357.56	1601.37	3,958.93
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.80	1.00	0.00	15.79	38.41	0.00	2,443.1	0.0	2264.13	1691.46	3,955.59
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.80	1.00	0.00	7.78	18.48	0.00	1,206.6	0.0	1086.90	867.24	1,954.14
1	6	100.0	41.42	0.000	15.46	0.00	0.15	2.78	0.80	1.00	0.00	8.93	34.80	0.00	1,900.6	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	0.000	13.66	0.00	0.13	2.84	0.80	1.00	0.00	7.85	29.53	0.00	1,555.1	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.80	1.00	0.00	7.37	13.29	0.00	1,218.8	0.0	1218.32	694.40	1,912.72
															17,593.8	0.0	0		26,086.93

Load Case: 0.9D + 1.6W 90° Wind 0.9D + 1.6W 93 mph Wind at 90° From Face

Wind Load Factor: 1.60
Dead Load Factor: 0.90
Ice Dead Load Factor: 0.00

Wind Importance Factor: 1.00
Ice Importance Factor: 1.00

				Total	Total	Ice								Ice					
	_	Wind Height	qz	Flat Area	Round Area	Round Area	Sol			_	lce Thick	Eff Area	Area	Linear Area	Total Weight	Weight	Struct Force	Linear Force	Total Force
	Seq	(ft)	(psf)	(sqft)	(sqft)	(sqft)	Ratio	Cf	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (lb)	(lb)	(lb)	(lb)
1	1	10.0	35.36	15.937	18.83	0.00	0.13	2.85	0.85	1.00	0.00	21.61	40.81	0.00	3,465.7	0.0	2962.49	1560.21	4,522.71
1	2	30.0	33.86	14.403	18.83	0.00	0.14	2.79	0.85	1.00	0.00	20.56	39.30	0.00	2,976.7	0.0	2641.44	1444.14	4,085.58
1	3	50.0	37.55	10.827	18.83	0.00	0.16	2.75	0.85	1.00	0.00	17.35	39.30	0.00	2,827.2	0.0	2433.51	1601.37	4,034.88
1	4	70.0	39.67	9.814	17.23	0.00	0.18	2.66	0.85	1.00	0.00	16.28	38.41	0.00	2,443.1	0.0	2334.49	1691.46	4,025.94
1	5	85.0	40.71	4.578	8.61	0.00	0.22	2.52	0.85	1.00	0.00	8.01	18.48	0.00	1,206.6	0.0	1118.87	867.24	1,986.10
1	6	100.0	41.42	0.000	15.46	0.00	0.15	2.78	0.85	1.00	0.00	8.93	34.80	0.00	1,900.6	0.0	1396.20	1699.39	3,095.59
1	7	120.0	42.04	0.000	13.66	0.00	0.13	2.84	0.85	1.00	0.00	7.85	29.53	0.00	1,555.1	0.0	1274.26	1529.18	2,803.43
1	8	140.0	42.38	0.000	12.85	0.00	0.12	2.87	0.85	1.00	0.00	7.37	13.29	0.00	1,218.8	0.0	1218.32	694.40	1,912.72
															17,593.8	0.0	0		26,466.95

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: ||



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Load Case: 1.2D + 1.0Di + 1.0Wi Normal Wind 1.2D + 1.0Di + 1.0Wi 50 mph Wind at Normal From Face

Wind Load Factor: 1.00 Wind Importance Factor: 1.00

Dead Load Factor: 1.20 Ice Dead Load Factor: 1.00

Ice Importance Factor: 1.00

				Total	Total	Ice								Ice					
		Wind		Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
	_	Height	qz	Area	Area	Area	Sol			_	Thick	Area	Area	Area		Weight	Force	Force	Force
	Seq	(ft)	(pst)	(sqft)	(sqft)	(sqft)	Ratio	Ct	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (lb)	(lb)	(lb)	(lb)
1	1	10.0	10.22	15.937	63.00	44.17	0.28	2.34	1.00	1.00	2.51	53.37	88.99	83.59	13,408.	8787.9	1084.49	1030.20	2,114.70
1	2	30.0	9.79	14.403	64.56	45.73	0.33	2.22	1.00	1.00	2.76	53.73	85.23	91.86	13,474.	9505.9	990.98	966.17	1,957.14
1	3	50.0	10.85	10.827	63.56	44.72	0.37	2.12	1.00	1.00	2.86	50.57	86.92	95.25	13,106.	9337.2	988.10	1072.49	2,060.58
1	4	70.0	11.47	9.814	60.41	43.18	0.44	1.98	1.00	1.00	2.91	49.45	86.96	82.29	12,146.	8888.9	956.43	1047.86	2,004.29
1	5	85.0	11.77	4.578	29.61	21.00	0.53	1.86	1.00	1.00	2.94	25.40	42.98	29.39	5,734.6	4125.8	472.80	453.34	926.14
1	6	100.0	11.97	0.000	83.90	68.44	0.74	1.78	1.00	1.00	2.96	70.62	84.09	45.54	11,571.	9037.5	1281.73	485.94	1,767.67
1	7	120.0	12.15	0.000	82.45	68.79	0.73	1.78	1.00	1.00	2.97	68.72	79.08	17.64	10,157.	8083.7	1263.75	419.52	1,683.28
1	8	140.0	12.25	0.000	81.84	68.99	0.73	1.78	1.00	1.00	2.98	68.02	39.12	9.94	8,282.0	6656.9	1260.57	217.39	1,477.96
															87,882.0	64423.0	5		13,991.75

Load Case: 1.2D + 1.0Di + 1.0Wi 60° Wind 1.2D + 1.0Di + 1.0Wi 50 mph Wind at 60° From Face

Wind Load Factor: 1.00

Dead Load Factor: 1.20

Ice Dead Load Factor: 1.00

Ice Importance Factor: 1.00

Ice Importance Factor: 1.00

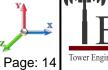
				Total	Total	Ice								Ice					
	Sect Seq	Wind Height (ft)	qz (psf)	Flat Area (sqft)	Round Area (sqft)	Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Linear Area (sqft)	Weight	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	1	10.0	10.22	15.937	63.00	44.17	0.28	2.34	0.80	1.00	2.51	50.18	88.99	83.59	13,408.	8787.9	1019.73	1030.20	2,049.93
1	2	30.0	9.79	14.403	64.56	45.73	0.33	2.22	0.80	1.00	2.76	50.85	85.23	91.86	13,474.	9505.9	937.85	966.17	1,904.02
1	3	50.0	10.85	10.827	63.56	44.72	0.37	2.12	0.80	1.00	2.86	48.41	86.92	95.25	13,106.	9337.2	945.79	1072.49	2,018.28
1	4	70.0	11.47	9.814	60.41	43.18	0.44	1.98	0.80	1.00	2.91	47.49	86.96	82.29	12,146.	8888.9	918.46	1047.86	1,966.33
1	5	85.0	11.77	4.578	29.61	21.00	0.53	1.86	0.80	1.00	2.94	24.48	42.98	29.39	5,734.6	4125.8	455.76	453.34	909.09
1	6	100.0	11.97	7 0.000	83.90	68.44	0.74	1.78	0.80	1.00	2.96	70.62	84.09	45.54	11,571.	9037.5	1281.73	485.94	1,767.67
1	7	120.0	12.15	0.000	82.45	68.79	0.73	1.78	0.80	1.00	2.97	68.72	79.08	17.64	10,157.	8083.7	1263.75	419.52	1,683.28
1	8	140.0	12.25	0.000	81.84	68.99	0.73	1.78	0.80	1.00	2.98	68.02	39.12	9.94	8,282.0	6656.9	1260.57	217.39	1,477.96
															87.882.0	64423.0	<u>-</u>		13.776.55

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II



Tower Engineering Solutions

Load Case: 1.2D + 1.0Di + 1.0Wi 90° Wind 1.2D + 1.0Di + 1.0Wi 50 mph Wind at 90° From Face

Wind Load Factor: 1.00 Wind Importance Factor: 1.00

Dead Load Factor: 1.20 Ice Dead Load Factor: 1.00

Ice Importance Factor: 1.00

		Wind	Total Flat	Total Round	Ice Round					Ice	Eff	Linear	Ice Linear	Total		Struct	Linear	Total
	Sect Seq	Height (ft)	qz Area (psf) (sqft)	Area (sqft)	Area (sqft)	Sol Ratio	Cf	Df	Dr	Thick (in)	Area (sqft)	Area (sqft)	Area (sqft)	Weight (lb)	Weight Ice (lb)	Force (lb)	Force (lb)	Force (lb)
1	1	10.0	10.22 15.937	63.00	44.17	0.28	2.34	0.85	1.00	2.51	50.98	88.99	83.59	13,408.	8787.9	1035.92	1030.20	2,066.12
1	2	30.0	9.79 14.403	64.56	45.73	0.33	2.22	0.85	1.00	2.76	51.57	85.23	91.86	13,474.	9505.9	951.13	966.17	1,917.30
1	3	50.0	10.85 10.827	63.56	44.72	0.37	2.12	0.85	1.00	2.86	48.95	86.92	95.25	13,106.	9337.2	956.37	1072.49	2,028.85
1	4	70.0	11.47 9.814	60.41	43.18	0.44	1.98	0.85	1.00	2.91	47.98	86.96	82.29	12,146.	8888.9	927.95	1047.86	1,975.82
1	5	85.0	11.77 4.578	29.61	21.00	0.53	1.86	0.85	1.00	2.94	24.71	42.98	29.39	5,734.6	4125.8	460.02	453.34	913.35
1	6	100.0	11.97 0.000	83.90	68.44	0.74	1.78	0.85	1.00	2.96	70.62	84.09	45.54	11,571.	9037.5	1281.73	485.94	1,767.67
1	7	120.0	12.15 0.000	82.45	68.79	0.73	1.78	0.85	1.00	2.97	68.72	79.08	17.64	10,157.	8083.7	1263.75	419.52	1,683.28
1	8	140.0	12.25 0.000	81.84	68.99	0.73	1.78	0.85	1.00	2.98	68.02	39.12	9.94	8,282.0	6656.9	1260.57	217.39	1,477.96
														87,882.0	64423.0	_ }		13,830.35

Load Case: 1.0D + 1.0W Normal Wind 1.0D + 1.0W 60 mph Wind at Normal To Face

Wind Load Factor: 1.00
Dead Load Factor: 1.00
Ice Dead Load Factor: 0.00

Mind Importance Factor: 1.00
Ice Importance Factor: 1.00

				Total	Total	Ice								Ice					
	Sect Seq	Wind Height (ft)	qz (psf)	Flat Area (sqft)	Round Area (sqft)	Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Linear Area (sqft)	Total Weight (lb)	Weight Ice (lb)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	1	10.0	14.72	2 15.937	18.83	0.00	0.13	2.85	1.00	1.00	0.00	25.97	40.81	0.00	3,850.8	0.0	926.12	405.88	1,332.00
1	2	30.0	14.09	14.403	18.83	0.00	0.14	2.79	1.00	1.00	0.00	24.56	39.30	0.00	3,307.5	0.0	821.15	375.69	1,196.84
1	3	50.0	15.63	3 10.827	18.83	0.00	0.16	2.75	1.00	1.00	0.00	20.85	39.30	0.00	3,141.3	0.0	761.12	416.59	1,177.71
1	4	70.0	16.51	9.814	17.23	0.00	0.18	2.66	1.00	1.00	0.00	19.26	38.41	0.00	2,714.5	0.0	718.45	440.03	1,158.47
1	5	85.0	16.94	4.578	8.61	0.00	0.22	2.52	1.00	1.00	0.00	9.37	18.48	0.00	1,340.7	0.0	340.48	225.61	566.09
1	6	100.0	17.24	1 0.000	15.46	0.00	0.15	2.78	1.00	1.00	0.00	8.93	34.80	0.00	2,111.8	0.0	363.22	442.09	805.30
1	7	120.0	17.50	0.000	13.66	0.00	0.13	2.84	1.00	1.00	0.00	7.85	29.53	0.00	1,727.9	0.0	331.49	397.81	729.30
1	8	140.0	17.64	1 0.000	12.85	0.00	0.12	2.87	1.00	1.00	0.00	7.37	13.29	0.00	1,354.2	0.0	316.94	180.65	497.58
															19.548.6	0.0	_	•	7.463.30

Structure: CT22071-A-SBA Code: EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) **Exposure:** В Height: 150.00 (ft) Crest Height: 520.00

C - Very Dense Soil **Base Elev:** 0.000 (ft) Site Class:

Gh: Struct Class: II 0.85 Topography: 4

1.00

1.00

Load Case: 1.0D + 1.0W 60° Wind

Wind Load Factor:

Dead Load Factor:



1.0D + 1.0W 60 mph Wind at 60° From Face

19,548.6

Wind Importance Factor: 1.00

0.0

7,067.85

		Ice	Dead	Load F	actor:	0.00										ice i	mportano	e Factor:	1.00
	Sect Seq	Wind Height (ft)	qz (psf)	Total Flat Area (sqft)	Total Round Area (sqft)	Ice Round Area (sqft)	Sol Ratio	Cf	Df	Dr	lce Thick (in)	Eff Area (sqft)	Linear Area (sqft)	Ice Linear Area (sqft)	Total Weight (lb)	Weight Ice (Ib)	Struct Force (lb)	Linear Force (lb)	Total Force (lb)
1	1	10.0	14.72	15.937	18.83	0.00	0.13	2.85	0.80	1.00	0.00	22.79	40.81	0.00	3,850.8	0.0	812.48	405.88	1,218.36
1	2	30.0	14.09	14.403	18.83	0.00	0.14	2.79	0.80	1.00	0.00	21.68	39.30	0.00	3,307.5	0.0	724.86	375.69	1,100.54
1	3	50.0	15.63	10.827	18.83	0.00	0.16	2.75	0.80	1.00	0.00	18.69	39.30	0.00	3,141.3	0.0	682.09	416.59	1,098.68
1	4	70.0	16.51	9.814	17.23	0.00	0.18	2.66	0.80	1.00	0.00	17.30	38.41	0.00	2,714.5	0.0	645.24	440.03	1,085.26
1	5	85.0	16.94	4.578	8.61	0.00	0.22	2.52	0.80	1.00	0.00	8.46	18.48	0.00	1,340.7	0.0	307.22	225.61	532.83
1	6	100.0	17.24	0.000	15.46	0.00	0.15	2.78	0.80	1.00	0.00	8.93	34.80	0.00	2,111.8	0.0	363.22	442.09	805.30
1	7	120.0	17.50	0.000	13.66	0.00	0.13	2.84	0.80	1.00	0.00	7.85	29.53	0.00	1,727.9	0.0	331.49	397.81	729.30
1	8	140.0	17.64	0.000	12.85	0.00	0.12	2.87	0.80	1.00	0.00	7.37	13.29	0.00	1,354.2	0.0	316.94	180.65	497.58

Load Case: 1.0D + 1.0W 90° Wind 1.0D + 1.0W 60 mph Wind at 90° From Face

Wind Load Factor: 1.00 Wind Importance Factor: 1.00 **Dead Load Factor:** 1.00 Ice Importance Factor: 1.00 Ice Dead Load Factor: 0.00

				ıotaı	ıotaı	ice								ice					
		Wind		Flat	Round	Round					Ice	Eff	Linear	Linear	Total		Struct	Linear	Total
	Sect	Height	qz	Area	Area	Area	Sol				Thick	Area	Area	Area	Weight	Weight	Force	Force	Force
	Seq	(ft)	(psf)	(sqft)	(sqft)	(sqft)	Ratio	Cf	Df	Dr	(in)	(sqft)	(sqft)	(sqft)	(lb)	Ice (Ib)	(lb)	(lb)	(lb)
1	1	10.0	14.72	15.937	18.83	0.00	0.13	2.85	0.85	1.00	0.00	23.58	40.81	0.00	3,850.8	0.0	840.89	405.88	1,246.77
1	2	30.0	14.09	14.403	18.83	0.00	0.14	2.79	0.85	1.00	0.00	22.40	39.30	0.00	3,307.5	0.0	748.93	375.69	1,124.62
1	3	50.0	15.63	10.827	18.83	0.00	0.16	2.75	0.85	1.00	0.00	19.23	39.30	0.00	3,141.3	0.0	701.84	416.59	1,118.43
1	4	70.0	16.51	9.814	17.23	0.00	0.18	2.66	0.85	1.00	0.00	17.79	38.41	0.00	2,714.5	0.0	663.54	440.03	1,103.56
1	5	85.0	16.94	4.578	8.61	0.00	0.22	2.52	0.85	1.00	0.00	8.68	18.48	0.00	1,340.7	0.0	315.53	225.61	541.14
1	6	100.0	17.24	0.000	15.46	0.00	0.15	2.78	0.85	1.00	0.00	8.93	34.80	0.00	2,111.8	0.0	363.22	442.09	805.30
1	7	120.0	17.50	0.000	13.66	0.00	0.13	2.84	0.85	1.00	0.00	7.85	29.53	0.00	1,727.9	0.0	331.49	397.81	729.30
1	8	140.0	17.64	0.000	12.85	0.00	0.12	2.87	0.85	1.00	0.00	7.37	13.29	0.00	1,354.2	0.0	316.94	180.65	497.58
															19,548.6	0.0	-	-	7,166.71

Force/Stress Compression Summary

Structure: CT22071-A-SBA Code: EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) **Exposure:** В Crest Height: 520.00 Height: 150.00 (ft)

C - Very Dense Soil Base Elev: 0.000 (ft) Site Class:

0.85 Gh: Topography: 4 Struct Class: ||



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			LEG MEMBERS									
Sect	Top Elev Member	Force (kips)	Load Case	Len (ft)	Br X	acinç Y	g % Z	KL/R	Fy (ksi)	Mem Cap (kips)	Leg Use %	Controls
1	20 12B - 12"BD 1.75"	-269.66 1.2D	+ 1.6W Normal Wind - P1	10.02	100	100	100	25.99	50.00	308.82	87.3	Member X
2	40 12B - 12"BD 1.75"	-242.62 1.2D	+ 1.6W Normal Wind - P1	10.02	100	100	100	25.99	50.00	308.82	78.6	Member X
3	60 12B - 12"BD 1.75"	-210.98 1.2D	+ 1.6W Normal Wind - P1	10.02	100	100	100	25.99	50.00	308.82	68.3	Member X
4	80 12B - 12"BD 1.5"	-176.93 1.2D	+ 1.6W Normal Wind - P1	10.02	100	100	100	30.32	50.00	222.99	79.3	Member X
5	90 12B - 12"BD 1.5"	-140.13 1.2D	+ 1.6W Normal Wind - P1	10.02	100	100	100	30.32	50.00	222.99	62.8	Member X
6	110 SOL - 2 1/4" SOLID	-132.52 1.2D	+ 1.6W Normal Wind - P1	2.42	100	100	100	51.55	50.00	147.32	90.0	Member X
7	130 SOL - 2" SOLID	-65.93 1.2D	+ 1.6W Normal Wind - P1	2.42	100	100	100	58.00	50.00	110.55	59.6	Member X
8	150 SOL - 1 3/4" SOLID	-19.89 1.2D	+ 1.6W Normal Wind - P1	2.42	100	100	100	66.28	50.00	78.50	25.3	Member X

Splices

			op Splic	e				В	ottom Sp	lice			
Sect	Top Elev	Load Case	Force (kips)		Use %	Bolt Type	Num Bolts	Load Case	Force (kips)	Cap (kips)	Use %	Bolt Type	Num Bolts
1	20	1.2D + 1.6W Normal Wind - P1	250.56	0.00	0.0			1.2D + 1.6W Normal Wind - P1	279.46	0.00			
2	40	1.2D + 1.6W Normal Wind - P1	219.60	0.00	0.0			1.2D + 1.6W Normal Wind - P1	250.56	0.00		1 A325	6
3	60	1.2D + 1.6W Normal Wind - P1	186.64	0.00	0.0			1.2D + 1.6W Normal Wind - P1	219.60	0.00		1 A325	6
4	80	1.2D + 1.6W Normal Wind - P1	150.60	0.00	0.0			1.2D + 1.6W Normal Wind - P1	186.64	0.00		1 A325	6
5	90	1.2D + 1.6W Normal Wind - P1	138.26	0.00	0.0			1.2D + 1.6W Normal Wind - P1	150.60	0.00		1 A325	6
6	110	1.2D + 1.6W Normal Wind - P1	69.66	0.00	0.0			1.2D + 1.6W Normal Wind - P1	138.26	0.00		1 A325	6
7	130	1.2D + 1.6W Normal Wind - P1	22.46	0.00	0.0			1.2D + 1.6W Normal Wind - P1	69.66	0.00			
8	150	1.2D + 1.0Di + 1.0Wi 90° Wind	0.51	0.00	0.0			1.2D + 1.6W Normal Wind - P1	22.46	0.00			

					НО	RIZO	NTAI	L ME	ИВЕГ	RS							
Sect	Top Elev	Member	Force (kips)	Load Case	•	Len (ft)	Br:	acing Y	% Z	KL/R	Fy (ksi)		Num Bolts	Num	•	Use %	Controls
1	20											0.00	0	0			
2	40											0.00	0	0			
3	60											0.00	0	0			
4	80											0.00	0	0			
5	90											0.00	0	0			
6	110	SOL - 1" SOLID	-1.12	1.2D + 1.6W 60° Win	d - P1	5.00	100	100	100	168.00	50.00	6.29	0	0		18	Member X
7	130	SOL - 7/8" SOLID	-1.54	1.2D + 1.6W Normal	Wind - P1	5.00	100	100	100	191.96	50.00	3.69	0	0		42	Member X
8	150	SOL - 7/8" SOLID	-1.15	1.2D + 1.6W Normal	Wind - P1	5.00	100	100	100	191.96	50.00	3.69	0	0		31	Member X

					D	IAGON	IAL N	/EME	BER	S	·			·				
Sect	Top Elev	Member	Force (kips)	Load C	ase	Len (ft)	Bra X	icing Y	% Z	KL/R	Fy (ksi)		Num Bolts	Num Holes		Сар	Use %	Controls
1	20	SAE - 3X3X0.3125	-7.74	1.2D + 1.6W No	rmal Wind - P1	16.80	50	50	50	171.17	36.00	13.73	1	1	31.81	29.9	56	Member Z
2	40	SAE - 3X3X0.1875	-6.15	1.2D + 1.6W 60°	Wind - P1	15.24	50	50	50	153.45	36.00	10.46	1	1	31.81	17.9	59	Member Z
3	60	SAE - 2.5X2.5X0.1875	-6.40	1.2D + 1.6W 60°	Wind - P1	13.80	50	50	50	167.23	36.00	7.29	1	1	31.81	17.9	88	Member Z
4	80	SAE - 2.5X2.5X0.1875	-6.52	1.2D + 1.6W 60°	Wind - P1	12.50	50	50	50	151.56	36.00	8.87	1	1	31.81	17.9	74	Member Z
5	90	SAE - 2.5X2.5X0.1875	-7.11	1.2D + 1.6W 90°	Wind - P1	11.42	50	50	50	138.38	36.00	10.64	1	1	31.81	17.9	67	Member Z
6	110	SOL - 1" SOLID	-6.00	1.2D + 1.6W 90°	Wind - P1	5.55	50	50	50	119.95	50.00	12.33	0	0			49	Member X
7	130	SOL - 7/8" SOLID	-4.82	1.2D + 1.6W 90°	Wind - P1	5.55	50	50	50	137.06	50.00	7.23	0	0			67	Member X
8	150	SOL - 7/8" SOLID	-3.28	1.2D + 1.6W 90°	Wind - P1	5.55	50	50	50	137.06	50.00	7.23	0	0			45	Member X

Force/Stress Tension Summary

Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

19.52

Gh: 0.85 Topography: 4 Struct Class: II



50 141.37

50 108.24



44.8 Member

18.0 Member

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						Mem		
	Top		Force		Fy	Cap	Leg	
Sect	Elev	Member	(kips)	Load Case	(ksi)	(kips)	Use %	Controls
1	20	12B - 12"BD 1.75"	247.94	0.9D + 1.6W 60° Wind	50	324.45	76.4	Member
2	40	12B - 12"BD 1.75"	224.00	0.9D + 1.6W 60° Wind	50	324.45	69.0	Member
3	60	12B - 12"BD 1.75"	195.76	0.9D + 1.6W 60° Wind	50	324.45	60.3	Member
4	80	12B - 12"BD 1.5"	164.22	0.9D + 1.6W 60° Wind	50	238.50	68.9	Member
5	90	12B - 12"BD 1.5"	130.38	0.9D + 1.6W 60° Wind	50	238.50	54.7	Member
6	110	SOL - 2 1/4" SOLID	127.92	0.9D + 1.6W 60° Wind	50	178.92	71.5	Member

63.34 0.9D + 1.6W 60° Wind

0.9D + 1.6W 60° Wind

LEG MEMBERS

Splices

150

130 SOL - 2" SOLID

SOL - 1 3/4" SOLID

			Top Spli	ce			Bottom Splice							
Sect	Top Elev	Load Case	Force (kips)	Cap (kips)	Use %	Bolt Type	Num Bolts	Load Case	Force Cap (kips) (kips)	Use %	Bolt Type	Num Bolts		
1	20	0.9D + 1.6W 60° Wind	230.20	0.00	0.0			0.9D + 1.6W 60° Wind	256.6 0.00					
2	40	0.9D + 1.6W 60° Wind	202.50	0.00	0.0			0.9D + 1.6W 60° Wind	230.2 318.06	72.4	1 A32	25 6		
3	60	0.9D + 1.6W 60° Wind	172.51	0.00	0.0			0.9D + 1.6W 60° Wind	202.5 318.06	63.7	1 A32	25 6		
4	80	0.9D + 1.6W 60° Wind	139.48	0.00	0.0			0.9D + 1.6W 60° Wind	172.5 318.06	54.2	1 A32	25 6		
5	90	0.9D + 1.6W 60° Wind	127.65	0.00	0.0			0.9D + 1.6W 60° Wind	139.4 318.06	43.9	1 A32	25 6		
6	110	0.9D + 1.6W 60° Wind	63.27	0.00	0.0			0.9D + 1.6W 60° Wind	127.6 318.06	40.1	1 A32	25 6		
7	130	0.9D + 1.6W 60° Wind	19.47	0.00	0.0			0.9D + 1.6W 60° Wind	63.27 0.00					
8	150		0.00	0.00	0.0			0.9D + 1.6W 60° Wind	19.47 0.00					

	HORIZONTAL MEMBERS											
Sect	Top Elev	Member	Force (kips)	Load Case	Fy (ksi)	Mem Cap (kips)	Num Bolts	Num Holes	Shear Cap (kips)	Bear Cap (kips)	B.S. Cap (kips)	Use % Controls
1	20	-			36	0.00	0	0				
2	40	-			36	0.00	0	0				
3	60	-			36	0.00	0	0				
4	80	-			36	0.00	0	0				
5	90	-			36	0.00	0	0				
6	110	SOL - 1" SOLID	1.52 1.	2D + 1.6W Normal W	50	35.34	0	0				4.3 Member
7	130	SOL - 7/8" SOLID	1.56 1.	.2D + 1.6W 60° Wind -	50	27.06	0	0				5.8 Member
8	150	SOL - 7/8" SOLID	1.04 1.	2D + 1.6W 60° Wind -	50	27.06	0	0				3.8 Member

	DIAGONAL MEMBERS												
Sect	Top Elev	Member	Force (kips)	Load Case	Fy (ksi)	Mem Cap (kips)	Num Bolts	Num Holes	Shear Cap (kips)	Bear Cap (kips)	B.S. Cap (kips)	Use %	Controls
1	20	SAE - 3X3X0.3125	7.52 0.9D	+ 1.6W 60° Wind	36	46.60	1	1	31.81	29.91	19.47	38.6	Blck Shear
2	40	SAE - 3X3X0.1875	6.45 0.9D	+ 1.6W 60° Wind	36	28.68	1	1	31.81	17.94	11.68	55.2	Blck Shear
3	60	SAE - 2.5X2.5X0.1875	6.49 0.9D	+ 1.6W 60° Wind	36	22.55	1	1	31.81	17.94	10.66	60.9	Blck Shear
4	80	SAE - 2.5X2.5X0.1875	7.70 0.9D	+ 1.6W 60° Wind	36	22.55	1	1	31.81	17.94	10.66	72.2	Blck Shear
5	90	SAE - 2.5X2.5X0.1875	6.88 0.9D	+ 1.6W 90° Wind	36	22.55	1	1	31.81	17.94	10.66	64.5	Blck Shear
6	110	SOL - 1" SOLID	6.40 1.2D	+ 1.6W 60° Wind	50	35.34	0	0				18.1	Member
7	130	SOL - 7/8" SOLID	4.74 1.2D	+ 1.6W 90° Wind	50	27.06	0	0				17.5	Member
8	150	SOL - 7/8" SOLID	3.34 1.2D	+ 1.6W Normal W	50	27.06	0	0				12.3	Member

Seismic Section Forces

Structure: CT22071-A-SBA Code: EIA/TIA-222-G

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II



6/30/2020



Load Case: 1.2D + 1.0E

Ke 0.0000 **Dead Load Factor** 1.20 **Sds** 0.144 **Ss** 0.1810 **Fa** 1.2000 **Seismic Load Factor** 1.00 **Sd1** 0.072 **S1** 0.0640 **Fv** 1.7000 **Kg** 0.0000 Seismic Importance Factor Vs 0.9799 **f1** 1.4514 1.00 **SA** 0.105 **R** 3.0000

	- Flank	147-				Lateral Fsz
Sect #	Elev (ft)	Wz (lb)	а	b	С	(lb)
1	10.00	3901.0	0.01	0.05	0.03	14.30
2	30.00	3307.4	0.08	0.07	0.04	23.64
3	50.00	3141.2	0.21	0.06	0.02	35.27
4	70.00	3371.1	0.41	0.01	0.01	51.64
5	85.00	1340.7	0.61	-0.06	0.02	23.29
6	100.00	2526.7	0.84	-0.12	0.07	51.58
7	120.00	2127.9	1.21	0.01	0.26	75.51
8	140.00	3542.7	1.65	0.93	0.73	273.91

Load Case: 0.9D + 1.0E **Sds** 0.144 **Ss** 0.1810 **Ke** 0.0000 **Dead Load Factor** 0.90 **Fa** 1.2000 **Seismic Load Factor Kg** 0.0000 1.00 **Sd1** 0.072 **S1** 0.0640 **Fv** 1.7000 Seismic Importance Factor Vs 0.9799 **f1** 1.4514 1.00 **R** 3.0000 **SA** 0.105

						Lateral
Sect #	Elev (ft)	Wz (lb)	а	b	С	Fsz (lb)
1	10.00	3901.0	0.01	0.05	0.03	14.30
2	30.00	3307.4	0.08	0.07	0.04	23.64
3	50.00	3141.2	0.21	0.06	0.02	35.27
4	70.00	3371.1	0.41	0.01	0.01	51.64
5	85.00	1340.7	0.61	-0.06	0.02	23.29
6	100.00	2526.7	0.84	-0.12	0.07	51.58
7	120.00	2127.9	1.21	0.01	0.26	75.51
8	140 00	3542 7	1 65	0.93	0.73	273 91

Support Forces Summary

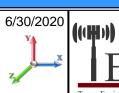
Structure: CT22071-A-SBA **Code:** EIA/TIA-222-G 6/30/2020

Site Name: Avon (Montevideo) Exposure: B

Height: 150.00 (ft) **Crest Height:** 520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: ||



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Load Case	Node	FX (kips)	FY (kips)	FZ (kips)	(-) = Uplift (+) = Down
1.2D + 1.6W Normal Wind - P1	1	-0.02	278.90	-27.40	
	1a	11.07	-125.51	-6.16	
	1b	-11.05	-125.47	-6.19	
1.2D + 1.6W Normal Wind - P2	1	-0.02	209.75	-19.57	
	1a	7.78	-90.94	-3.87	
	1b	-7.77	-90.90	-3.89	
1.2D + 1.6W Normal Wind - P3	1	-0.02	278.90	-27.40	
	1a	11.07	-125.51	-6.16	
	1b	-11.05	-125.47	-6.19	
1.2D + 1.6W 60° Wind - P1	1	-0.32	141.58	-13.63	
	1a	-11.31	139.71	7.60	
	1b	-21.48	-253.37	-13.08	
1.2D + 1.6W 60° Wind - P2		0.05	100 22	0.02	
1.2D + 1.000 60 Willia - F2	1 1a	-0.05 -7.96	108.22 106.35	-9.92 5.98	
	1b	-14.93	-186.66	-9.30	
1.2D + 1.6W 60° Wind - P3	1	-0.32	141.58	-13.63	
	1a 1b	-11.31	139.71	7.60	
		-21.48	-253.37	-13.08 	
1.2D + 1.6W 90° Wind - P1	1	-0.42	9.69	-0.71	
	1a	-19.68	237.23	12.35	
	1b	-18.51	-219.01	-11.64	
1.2D + 1.6W 90° Wind - P2	1	-0.08	9.68	-0.75	
	1a	-13.95	178.94	9.22	
	1b	-12.68	-160.71	-8.47	
1.2D + 1.6W 90° Wind - P3	1	-0.42	9.69	-0.71	
	1a	-19.68	237.23	12.35	
	1b	-18.51	-219.01	-11.64	
0.9D + 1.6W Normal Wind		-0.02	276.06	-27.19	
0.55 i i.ov Noma vina	1a	11.23	-127.59	-6.27	
	1b	-11.21	-127.54	-6.29	
0.9D + 1.6W 60° Wind			400.05		
0.9D + 1.6W 60° Wind	1 1a	-0.33 -11.14	138.95 137.22	-13.42 7.49	
	1b	-21.64	-255.24	-13.18	
0.9D + 1.6W 90° Wind	. 1	-0.43	7.27	-0.51	
	1a	-19.51	234.60	12.24	
	1b	-18.68	-220.94	-11.73 	
1.2D + 1.0Di + 1.0Wi Normal Wind	1	-0.03	165.66	-13.24	
	1a	5.17	-32.46	-2.67	
	1b	-5.14	-32.55	-2.72	
1.2D + 1.0Di + 1.0Wi 60° Wind	1	-0.02	99.70	-6.84	
	1a	-5.63	97.57	3.82	
	1b	-10.30	-96.63	-6.18	

1.2D + 1.0Di + 1.0Wi 90° Wind	1	-0.01	34.50	-0.57	
	1a	-9.67	145.35	6.05	
	1b	-8.79	-79.20	-5.48	
4.0D . 4.0E		0.00	4400	204	
1.2D + 1.0E	1	0.00	14.08	3.84	
	1a	3.84	6.92	-2.17	
	1b	-3.84	6.92	-2.17	
0.9D + 1.0E	1	0.00	11.74	4.04	
0.05 1 1.02	1a	4.02	4.59	-2.27	
	1b	-4.02	4.59	-2.27	
1.0D + 1.0W Normal Wind	1	0.00	79.11	-7.78	
	1a	2.53	-27.92	-1.42	
	1b	-2.53	-27.93	-1.43	
4.00 4.004.000.00			40.07		
1.0D + 1.0W 60° Wind	1	-0.11	42.87	-4.11	
	1a	-3.43	42.08	2.24	
	1b	-5.32	-61.70	-3.24	
1.0D + 1.0W 90° Wind	1	0.12	0.06	0.67	
1.0D + 1.0W 90 WIIIU	=	-0.13	8.06	-0.67	
	1a	-5.66	67.82	3.51	
	1b	-4.53	-52.63	-2.85	

Max Reactions

	Leg			Ov	erturning		
	Max Uplift:	-255.24	(kips)	Moment:	3268.65	(ft-kips)	
ľ	Max Down:	278.90	(kips)	Total Down:	27.91	(kips)	
N	Max Shear:	27.40	(kips)	Total Shear:	39.75	(kips)	

Analysis Summary

Site Name:Avon (Montevideo)Exposure:BHeight:150.00 (ft)Crest Height:520.00

Base Elev: 0.000 (ft) Site Class: C - Very Dense Soil

Gh: 0.85 Topography: 4 Struct Class: II Page: 21



Max Reactions

Leg	0	verturning	
Max Uplift: -255.24	(kips) Moment	3268.65	(ft-kips)
Max Down: 278.90	(kips) Total Dowr	27.91	(kips)
Max Shear: 27.40	(kips) Total Shear	39.75	(kips)

Anchor Bolts

Bolt Size (in.): 1.00 Number Bolts: 6
Yield Strength (Ksi): 105.00 Tensile Strength (Ksi): 150.00

Interaction Ratio: 0.70

Detail Type: C

Max Usages

Max Leg: 90.0% (1.2D + 1.6W Normal Wind - P1 - Sect 6)
Max Diag: 87.9% (1.2D + 1.6W 60° Wind - P1 - Sect 3)
Max Horiz: 41.8% (1.2D + 1.6W Normal Wind - P1 - Sect 7)

Max Deflection, Twist and Sway

0.9D + 1.0E - Normal To Face	10.00 70.00	0.0044	0.0000	
	70.00		0.0000	0.0135
		0.0089	-0.0004	0.0159
	80.00	0.0102	0.0000	0.0183
	95.38	0.0179	-0.0006	0.0274
	100.21	0.0186	0.0000	0.0297
	107.46	0.0225	0.0000	0.0306
	115.38	0.0291	-0.0003	0.0365
	120.21	0.0305	0.0000	0.0377
	135.38	0.0427	0.0001	0.0409
	140.21	0.0461	-0.0001	0.0404
	142.63	0.0478	-0.0001	0.0404
	147.46	0.0512	0.0000	0.0403
	150.00	0.0530	0.0000	0.0409
0.9D + 1.6W 93 mph Wind at 60° From Face	10.00	0.0116	0.2021	0.1047
'	70.00	0.4299	1.5820	0.8149
	80.00	0.5710	1.7051	0.9791
	95.38	0.8390	0.2206	1.1005
	100.21	0.9487	1.8686	1.2518
	107.46	1.1130	1.9853	1.2391
	115.38	1.3031	0.7624	1.3282
	120.21	1.4361	2.1420	1.4232
	135.38	1.8485	2.1437	1.5946
	140.21	1.9812	2.1438	1.5917
	142.63	2.0476	2.1437	1.5849
	147.46	2.1811	2.1437	1.6765
	150.00	2.2508	2.1438	1.5939

0.00 + 1.6W 93 mph Wind at 90° From Face 10.00 0.0105 0.2002 0.0191 0.0006 0.0234 1.6869 0.0234 0.0006 0.0710 1.0869 0.0960 0.0960 0.0710 1.0869 0.0960 0.0960 0.0710 1.0869 0.0960 0.0960 0.0710 0.0960 0.09						
70.00 0.4904 1.6969 0.8224 80.00 0.75710 1.8666 0.9690 95.88 0.8312 0.0261 0.9696 100.21 0.9433 1.8669 1.9690 100.21 0.9433 1.8669 1.7445 107.46 1.1.126 1.6799 1.1686 115.38 1.2090 0.0277 0.9833 120.21 1.4894 1.6782 1.1788 120.21 1.4894 1.6782 1.1788 120.21 1.4894 1.6782 1.1788 120.21 1.4896 1.6774 1.8898 120.22 1.9783 1.1774 1.8898 120.22 1.9783 1.1774 1.1764 120.00 2.2438 1.6775 1.5845 100.00 2.2438 1.6775 1.5845 100.00 0.0123 0.0030 0.9897 100.00 0.0123 0.0030 0.9870 100.00 0.9816 1.7792 0.8870 100.00 0.9816 1.7792 0.8870 100.00 0.9816 1.7792 0.8870 100.00 0.9816 1.7793 1.3746 100.00 0.9816 1.7793 1.3746 100.00 0.9816 1.7793 1.3746 100.00 0.9816 1.7793 1.3748 100.01 0.8853 1.7793 1.4157 115.38 1.8201 0.0044 1.7712 1.2736 107.46 1.1259 1.7097 1.4157 115.38 1.8201 0.0044 1.7744 120.21 1.4580 1.7099 1.7004 135.38 1.8801 1.7003 1.6218 142.63 2.0860 1.7008 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 1.1570 0.0074 140.21 0.0074 0.0074 0.0074 1.1574 140.21 0.0074 0.0074 0.0074 0.0074 140.21 0.0074 0.0	0.9D + 1.6W 93 mph Wind at 90° From Face	10.00	0.0105	0.2002	0.1019	
80.00 0.5710 1.8868 0.8980 65.38 0.8312 0.0261 0.0908 100.21 0.9483 1.8080 1.2465 100.21 0.9483 1.8080 1.2465 100.21 0.9483 1.8080 1.2465 100.21 0.9483 1.8080 1.2465 115.88 1.2000 0.0347 0.0823 115.81 1.200 0.0347 0.0823 115.81 1.200 0.0347 0.0823 115.81 1.200 0.0347 0.0823 14.24 1.9783 1.4774 1.5783 14.24 1.9783 1.4774 1.5783 14.22 1.9783 1.4774 1.5783 14.22 1.9783 1.4774 1.5783 14.22 1.9783 1.4774 1.5783 14.22 1.9783 1.4774 1.5783 14.26 1.2794 1.5784 1.6774 1.5784 1.6774 1.5784 1.6775 1.5845 1.6700 0.22438 1.6775 1.5845 1.6700 0.22438 1.6775 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.5845 1.6795 1.6845 1.679						
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142 63 2.0424 16775 1.5756 19764 19700 2.2438 16774 1.7624 150.00 2.2438 16775 1.5845 150.00 2.2438 16775 1.5845 15.000 2.2438 16775 1.5845 10.000 0.500 0.0100 0.0						
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150.00						
0.9D + 1.6W 93 mph Wind at Normal To Face 70.00 0.123 0.2033 0.1069 770.00 0.4577 1.5942 0.7571 80.00 0.5616 1.7192 0.8870 85.00 0.5616 1.7192 0.8870 85.00 0.5616 1.7192 0.8870 85.00 0.5616 1.7192 0.8870 100.21 0.0579 1.7123 1.2736 100.21 0.0579 1.7123 1.2736 100.21 10.021 1.4550 1.7067 1.4137 115.38 1.3291 0.00384 1.9744 120.21 1.4550 1.7069 1.7004 135.33 1.8801 1.7035 1.6582 140.21 1.4550 1.7069 1.7004 135.33 1.8801 1.7035 1.6582 140.21 2.0162 1.7035 1.6582 140.21 2.0162 1.7035 1.6181 147.46 2.2205 1.7032 1.6184 147.46 2.2205 1.7032 1.5184 147.46 2.2205 1.7032 1.5184 147.46 2.2205 1.7032 1.5184 147.46 1.706 1.518 147.46 1.706 1.518 147.46 1.706						
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80.00	0.9D + 1.6W 93 mph Wind at Normal To Face	10.00	0.0123	0.2033	0.1089	
95.38 0.8555 -0.0356 1.3748 100.21 0.9579 1.723 1.2736 107.46 1.1259 1.7097 1.4137 116.38 1.3291 -0.0364 1.9744 120.21 1.4550 1.7059 1.7004 136.38 1.8801 1.7033 1.8362 140.21 2.0162 1.7035 1.6218 140.21 2.0162 1.7035 1.6218 142.63 2.0840 1.7035 1.6218 147.48 2.2067 1.7035 1.6218 147.48 2.2067 1.7035 1.6119 150.00 2.2946 1.7035 1.6218 147.49 2.2067 1.7032 1.61194 150.00 2.2946 1.7035 1.6119 1.0D+1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D+1.0W 60 mph Wind at 60° From Face 10.00 0.1156 0.4494 0.2570 66.38 0.2090 0.0156 0.2841 100.21 0.2469 0.4151 0.3283 107.46 0.2930 0.4596 0.3246 11.0D+1.0W 60 mph Wind at 80° From Face 10.00 0.3779 0.4703 0.3728 11.0D+1.0W 60 mph Wind at 90° From Face 10.00 0.0300 0.5533 0.4703 0.4181 140.21 0.5740 0.4703 0.4181 140.21 0.5740 0.4703 0.4181 140.21 0.5740 0.4703 0.4181 140.21 0.5740 0.4703 0.4181 140.21 0.5723 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5932 0.4703 0.4181 140.21 0.5189 0.4473 0.3638 150.30 0.4703 0.4376 0.3638 150.30 0.3590 0.0071 0.275 100.21 0.3766 0.4376 0.3363 150.30 0.4943 0.4374 0.4388 0.4878 140.21 0.5189 0.4473 0.4493 140.21 0.5189 0.4493 0.4493 0.4493 140.21 0.5189 0.4493 0.4493 0.4493 140.21 0.5189 0.4493 0.4493 0.4493 140.21 0.5189 0.4493 0.4493 0.4493 140.21 0.5189 0.4493 0.4493 0.4493 140.21 0.5189 0.4495 0.4497 0.3623 140.24 0.5293 0.4496 0.4497 0.3493 140.25 0.3388 0.4496 0.4497 0.3493 140.21 0.3888 0.4496 0.		70.00	0.4377	1.5942	0.7571	
100.21		80.00	0.5816	1.7192	0.8870	
107.46		95.38	0.8555	-0.0356	1.3748	
115.38 1.3291 -0.0354 1.7744 120 21 1.4550 1.7004 135.38 1.8801 1.7035 1.6902 140 21 2.0162 1.7035 1.6902 140 21 2.0162 1.7035 1.6218 142 63 2.0840 1.7035 1.6181 147.48 2.2205 1.7032 1.6181 147.48 2.2205 1.7032 1.6181 150.00 2.2346 1.7039 2.5229 1.0D + 1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D + 1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0029 0.0523 0.0486 100.21 0.2499 0.4515 0.3283 107.46 0.2930 0.4596 0.3246 120.21 0.3779 0.4703 0.3246 135.38 0.4864 0.4703 0.4181 140.21 0.5231 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5249 0.0633 0.05275 150.00 0.0523 0.04703 0.4196 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.0034 0.0636 0.0636 0.0636 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.39 0.4864 0.4376 0.3063 150.30 0.5891 0.4374 0.4196 140.21 0.5891 0.4374 0.4196 140.21 0.5891 0.4374 0.4196 140.21 0.5891 0.4497 0.4496 140.21 0.5896 0.0646 0.4471 140.21 0.5896 0.0663 0.0633 150.38 0.0266 0.0663 0.0633 150.39 0.0266 0.0663 0.0673 150.00 0.1162 0.4496 0.4376 140.21 0.5896 0.0664 0.4477 140.21 0.5896 0.0466 0.4477 140.21 0.5896 0.0466 0.4477 14		100.21	0.9579	1.7123	1.2736	
115.38 1.3291 -0.0354 1.7744 120 21 1.4550 1.7004 135.38 1.8801 1.7035 1.6902 140 21 2.0162 1.7035 1.6902 140 21 2.0162 1.7035 1.6218 142 63 2.0840 1.7035 1.6181 147.48 2.2205 1.7032 1.6181 147.48 2.2205 1.7032 1.6181 150.00 2.2346 1.7039 2.5229 1.0D + 1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D + 1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0029 0.0523 0.0486 100.21 0.2499 0.4515 0.3283 107.46 0.2930 0.4596 0.3246 120.21 0.3779 0.4703 0.3246 135.38 0.4864 0.4703 0.4181 140.21 0.5231 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5233 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5234 0.4703 0.4191 140.21 0.5249 0.0633 0.05275 150.00 0.0523 0.04703 0.4196 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.0034 0.0636 0.0636 0.0636 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.38 0.4864 0.4376 0.3063 150.39 0.4864 0.4376 0.3063 150.30 0.5891 0.4374 0.4196 140.21 0.5891 0.4374 0.4196 140.21 0.5891 0.4374 0.4196 140.21 0.5891 0.4497 0.4496 140.21 0.5896 0.0646 0.4471 140.21 0.5896 0.0663 0.0633 150.38 0.0266 0.0663 0.0633 150.39 0.0266 0.0663 0.0673 150.00 0.1162 0.4496 0.4376 140.21 0.5896 0.0664 0.4477 140.21 0.5896 0.0466 0.4477 140.21 0.5896 0.0466 0.4477 14				1.7097		
120.21		115.38				
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140.21						
142.63 2.0840 1.7035 1.6181 147.46 2.2205 1.7032 1.6194 150.00 2.2846 1.7039 2.5229 1.0D+1.0W 60 mph Wind at 60° From Face 10.00 0.0029 0.0523 0.0278 1.0D+1.0W 60 mph Wind at 60° From Face 10.00 0.1136 0.4094 0.2145 80.00 0.1508 0.4110 0.2570 85.38 0.2209 0.0160 0.2884 100.21 0.2499 0.4515 0.3283 107.46 0.2830 0.4586 0.3246 115.38 0.3427 0.0530 0.3466 115.38 0.3427 0.0530 0.3466 115.38 0.3427 0.0530 0.3466 115.38 0.3427 0.0530 0.4191 140.21 0.5213 0.4703 0.4191 140.21 0.5213 0.4703 0.4191 140.21 0.5213 0.4703 0.4191 140.21 0.5213 0.4703 0.4191 140.21 0.5213 0.4703 0.4181 142.63 0.5388 0.4084 0.4703 0.4172 147.46 0.5740 0.4703 0.4172 147.46 0.5740 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5523 0.4703 0.4196 0.5000 0.5524 0.4376 0.3262 0.5000 0.500						
147.46						
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95.38						
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115.38		100.21	0.2499	0.4515	0.3283	
120.21		107.46	0.2930	0.4596	0.3246	
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140.21 0.5213 0.4703 0.4181 142.63 0.5388 0.4703 0.4172 147.46 0.5740 0.4703 0.4424 150.00 0.5923 0.4703 0.4424 150.00 0.5923 0.4703 0.4424 150.00 0.5923 0.4703 0.4196 1.0D+1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 0.1105 0.4077 0.2160 80.00 0.1504 0.4388 0.2611 95.38 0.2186 0.0063 0.2575 100.21 0.2496 0.4376 0.3262 107.46 0.2924 0.4376 0.3063 115.38 0.3390 0.0071 0.2587 120.21 0.3766 0.4376 0.3439 135.38 0.4843 0.4374 0.4156 140.21 0.5189 0.4374 0.4156 140.21 0.5189 0.4374 0.4156 140.21 0.5189 0.4374 0.4156 140.21 0.5189 0.4373 0.460 1417.46 0.5710 0.4373 0.460 1417.46 0.5710 0.4373 0.460 1417.46 0.5710 0.4373 0.460 1418 142.63 0.5505 0.4460 0.2594 0.2914 1538 0.2914 0.4137 0.4160 1418 0.5710 0.4373 0.4160 1418 0.5710 0.2536 0.4466 0.3359 100.21 0.2536 0.4466 0.3359 100.21 0.2536 0.4466 0.3359 115.38 0.3512 0.0094 0.3623 115.38 0.3512 0.0093 0.5192 120.21 0.3848 0.4465 0.3730 1515.38 0.3512 0.0093 0.5192 120.21 0.3848 0.4465 0.3359 115.38 0.3512 0.0093 0.5192 120.21 0.3848 0.4465 0.3359 115.38 0.3512 0.0093 0.5192 120.21 0.3848 0.4465 0.3359 115.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4271 142.63 0.5505 0.4460 0.4271 142.63 0.5505 0.4460 0.4271		120.21	0.3779	0.4703	0.3725	
142.63		135.38	0.4864	0.4703	0.4191	
147.46		140.21	0.5213	0.4703	0.4181	
150.00 0.5923 0.4703 0.4196 1.0D + 1.0W 60 mph Wind at 90° From Face 10.00 0.0030 0.0521 0.0270 70.00 0.1135 0.4077 0.2160 80.00 0.1504 0.4388 0.2611 95.38 0.2186 0.0063 0.2575 100.21 0.2496 0.4376 0.3262 107.46 0.2924 0.4376 0.3063 115.38 0.3390 0.0071 0.2587 120.21 0.3766 0.4376 0.3439 135.38 0.4843 0.4374 0.4156 140.21 0.5189 0.4374 0.4136 140.21 0.5189 0.4374 0.4136 142.63 0.5362 0.4374 0.4137 147.46 0.5710 0.4373 0.4622 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.0034 0.0529 0.0293 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.1162 0.4145 0.2011 80.00 0.1543 0.4471 0.2347 95.38 0.263 -0.0094 0.3623 100.21 0.2536 0.4466 0.3359 107.46 0.2979 0.4465 0.3359 107.46 0.2979 0.4466 0.3359 107.46 0.2979 0.4466 0.3359 107.46 0.2979 0.4466 0.3359 107.46 0.2979 0.4466 0.3359 107.46 0.2979 0.4466 0.3359 107.46 0.2979 0.4466 0.3359 107.47 0.3388 0.4663 0.4478 135.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4277 142.63 0.5505 0.4460 0.4277 142.63 0.5505 0.4460 0.4277		142.63	0.5388	0.4703	0.4172	
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70.00 0.1135 0.4077 0.2160 80.00 0.1504 0.4388 0.2611 95.38 0.2186 0.0063 0.2575 100.21 0.2496 0.4376 0.3262 107.46 0.2924 0.4376 0.3663 115.38 0.3390 0.0071 0.2587 120.21 0.3766 0.4376 0.3439 135.38 0.4843 0.4374 0.4156 140.21 0.5189 0.4374 0.4136 142.63 0.5362 0.4374 0.4137 147.46 0.5710 0.4373 0.4662 150.00 0.5891 0.4373 0.4662 150.00 0.5891 0.4373 0.4160 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.034 0.0529 0.0293 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.1162 0.4145 0.2011 80.00 0.1543 0.4471 0.2347 95.38 0.2263 -0.0094 0.3663 100.21 0.2536 0.4466 0.3359 107.46 0.2979 0.4465 0.3730 115.38 0.3512 -0.0093 0.5192 120.21 0.3848 0.4463 0.4478 135.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4270 142.63 0.5505 0.4460 0.4270 142.63 0.5505 0.4460 0.4270		150.00	0.5923	0.4703	0.4196	
70.00 0.1135 0.4077 0.2160 80.00 0.1504 0.4388 0.2611 95.38 0.2186 0.0063 0.2575 100.21 0.2496 0.4376 0.3262 107.46 0.2924 0.4376 0.3663 115.38 0.3390 0.0071 0.2587 120.21 0.3766 0.4376 0.3439 135.38 0.4843 0.4374 0.4156 140.21 0.5189 0.4374 0.4136 142.63 0.5362 0.4374 0.4137 147.46 0.5710 0.4373 0.4662 150.00 0.5891 0.4373 0.4662 150.00 0.5891 0.4373 0.4160 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.034 0.0529 0.0293 1.0D + 1.0W 60 mph Wind at Normal To Face 10.00 0.1162 0.4145 0.2011 80.00 0.1543 0.4471 0.2347 95.38 0.2263 -0.0094 0.3663 100.21 0.2536 0.4466 0.3359 107.46 0.2979 0.4465 0.3730 115.38 0.3512 -0.0093 0.5192 120.21 0.3848 0.4463 0.4478 135.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4270 142.63 0.5505 0.4460 0.4270 142.63 0.5505 0.4460 0.4270	1 0D + 1 0W 60 mph Wind at 90° From Face	10.00	0.0030	0.0521	0.0270	
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115.38 0.3512 -0.0093 0.5192 120.21 0.3848 0.4463 0.4478 135.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4277 142.63 0.5505 0.4460 0.4270 147.46 0.5865 0.4460 0.4271						
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135.38 0.4966 0.4461 0.4313 140.21 0.5326 0.4460 0.4277 142.63 0.5505 0.4460 0.4270 147.46 0.5865 0.4460 0.4271						
140.21 0.5326 0.4460 0.4277 142.63 0.5505 0.4460 0.4270 147.46 0.5865 0.4460 0.4271						
142.630.55050.44600.4270147.460.58650.44600.4271		135.38	0.4966	0.4461	0.4313	
147.46 0.5865 0.4460 0.4271		140.21		0.4460	0.4277	
		142.63	0.5505	0.4460	0.4270	
150.00 0.6060 0.4460 0.6624		147.46	0.5865	0.4460	0.4271	
		150.00	0.6060	0.4460	0.6624	

1.2D + 1.0Di + 1.0Wi 50 mph Wind at 60° From Face	10.00	0.0069	0.0455	0.0556	
	70.00	0.2139	0.3522	0.3877	
	80.00	0.2853	0.3787	0.4727	
	95.38	0.4224	0.0623	0.5573	
	100.21	0.4773	0.4294	0.6341	
				0.6341	
	107.46	0.5604	0.4657		
	115.38	0.6569	0.2130	0.6648	
	120.21	0.7232	0.5100	0.7098	
	135.38	0.9299	0.5108	0.7988	
	140.21	0.9966	0.5108	0.7959	
	142.63	1.0300	0.5107	0.7955	
	147.46	1.0970	0.5107	0.8480	
	150.00	1.1321	0.5108	0.8006	
4.0D + 4.0Di + 4.0Mi = 0 mmh Mind at 000 France Face	40.00	0.0000	0.0440	0.0500	
1.2D + 1.0Di + 1.0Wi 50 mph Wind at 90° From Face	10.00	0.0062	0.0448	0.0523	
	70.00	0.2120	0.3471	0.3842	
	80.00	0.2825	0.3723	0.4760	
	95.38	0.4160	0.0133	0.4872	
	100.21	0.4740	0.3708	0.6265	
	107.46	0.5559	0.3714	0.5641	
	115.38	0.6464	0.0180	0.4710	
	120.21	0.7165	0.3721	0.6441	
	135.38	0.9205	0.3719	0.7876	
	140.21	0.9861	0.3719	0.7831	
	142.63	1.0191	0.3719	0.7859	
	147.46	1.0850	0.3718	0.8883	
	150.00	1.1194	0.3719	0.7906	
1.2D + 1.0Di + 1.0Wi 50 mph Wind at Normal From Face	10.00	0.0047	0.0462	0.0486	
	70.00	0.2174	0.3595	0.3817	
	80.00	0.2906	0.3878	0.4465	
	95.38	0.4299	-0.0169	0.7076	
	100.21	0.4810	0.3873	0.6464	
	107.46	0.5663	0.3872	0.7345	
	115.38	0.6704	-0.0164	1.0178	
	120.21	0.7326	0.3870	0.8644	
	135.38	0.9453	0.3868	0.8199	
	140.21	1.0142	0.3868	0.8143	
	142.63	1.0485	0.3868	0.8133	
	147.46	1.1171	0.3867	0.8133	
	150.00	1.1538	0.3869	1.3168	
		1.1000			
1.2D + 1.0E - Normal To Face	10.00	0.0043	0.0000	0.0134	
	70.00	0.0089	-0.0004	0.0160	
	80.00	0.0103	0.0000	0.0182	
	95.38	0.0179	-0.0006	0.0275	
	100.21	0.0186	0.0000	0.0297	
	107.46	0.0226	0.0000	0.0307	
	115.38	0.0292	-0.0003	0.0366	
	120.21	0.0306	0.0000	0.0377	
	135 38	0.0428	0.0001	() ()4()9	
	135.38 140.21	0.0428	0.0001	0.0409	
	140.21	0.0462	-0.0001	0.0405	
	140.21 142.63	0.0462 0.0479	-0.0001 0.0001	0.0405 0.0405	
	140.21 142.63 147.46	0.0462 0.0479 0.0513	-0.0001 0.0001 0.0000	0.0405 0.0405 0.0404	
	140.21 142.63	0.0462 0.0479	-0.0001 0.0001	0.0405 0.0405	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46	0.0462 0.0479 0.0513	-0.0001 0.0001 0.0000	0.0405 0.0405 0.0404	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00	0.0462 0.0479 0.0513 0.0531 0.0115	-0.0001 0.0001 0.0000 0.0000	0.0405 0.0405 0.0404 0.0410 0.1047	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308	-0.0001 0.0001 0.0000 0.0000 	0.0405 0.0405 0.0404 0.0410 	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 	0.0462 0.0479 0.0513 0.0531 	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051	0.0405 0.0405 0.0404 0.0410 	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213	0.0405 0.0405 0.0404 0.0410 	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511	-0.0001 0.0001 0.0000 0.0000 	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863	0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38 120.21	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067 1.4402	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652 2.1436	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334 1.4285	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38 120.21 135.38	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067 1.4402 1.8541	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652 2.1436 2.1453	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334 1.4285 1.6006	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38 120.21 135.38 140.21	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067 1.4402 1.8541 1.9873	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652 2.1436 2.1453 2.1454	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334 1.4285 1.6006 1.5977	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38 120.21 135.38 140.21 142.63	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067 1.4402 1.8541 1.9873 2.0540	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652 2.1436 2.1453 2.1454 2.1453	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334 1.4285 1.6006 1.5977 1.5909	
1.2D + 1.6W 93 mph Wind at 60° From Face - P1	140.21 142.63 147.46 150.00 10.00 70.00 80.00 95.38 100.21 107.46 115.38 120.21 135.38 140.21	0.0462 0.0479 0.0513 0.0531 0.0115 0.4308 0.5723 0.8411 0.9511 1.1159 1.3067 1.4402 1.8541 1.9873	-0.0001 0.0001 0.0000 0.0000 0.2021 1.5820 1.7051 0.2213 1.8692 1.9863 0.7652 2.1436 2.1453 2.1454	0.0405 0.0405 0.0404 0.0410 0.1047 0.8168 0.9815 1.1043 1.2558 1.2434 1.3334 1.4285 1.6006 1.5977	

1.2D + 1.6W 93 mph Wind at 60° From Face - P2	10.00	0.0083	0.2027	0.0794	
1.25 * 1.61 66 mph ***********************************	70.00	0.3286	1.5859	0.6513	
	80.00	0.4384	1.7097	0.7823	
	95.38	0.6471	0.1783	0.8617	
	100.21	0.7362	1.8420	0.9973	
	107.46	0.8675	1.9362	0.9815	
	115.38	1.0182	0.6174	1.0604	
	120.21	1.1276	2.0631	1.1371	
	135.38	1.4621	2.0644	1.2964	
	140.21	1.5699	2.0645	1.2945	
	142.63	1.6238	2.0644	1.2890	
	147.46	1.7323	2.0643	1.3828	
	150.00	1.7889	2.0644	1.2965	
1.2D + 1.6W 93 mph Wind at 60° From Face - P3	10.00	0.0115	0.2021	0.1047	
·	70.00	0.4308	1.5820	0.8168	
	80.00	0.5723	1.7051	0.9815	
	95.38	0.8411	0.2213	1.1043	
	100.21	0.9511	1.8692	1.2558	
	107.46	1.1159	1.9863	1.2434	
	115.38	1.3067	0.7652	1.3334	
	120.21	1.4402	2.1436	1.4285	
	135.38	1.8541	2.1453	1.6006	
	140.21	1.9873	2.1454	1.5977	
	142.63	2.0540	2.1453	1.5909	
	147.46	2.1879	2.1452	1.6823	
	150.00	2.2579	2.1454	1.5999	
1.2D + 1.6W 93 mph Wind at 90° From Face - P1	10.00	0.0106	0.2002	0.1020	
	70.00	0.4312	1.5668	0.8250	
	80.00	0.5721	1.6865	0.9982	
	95.38	0.8330	0.0263	0.9841	
	100.21	0.9514	1.6808	1.2490	
	107.46	1.1152	1.6801	1.1724	
	115.38	1.2941	0.0354	0.9879	
	120.21	1.4378	1.6790	1.3158	
	135.38	1.8496	1.6777	1.5893	
	140.21	1.9818	1.6777	1.5812	
	142.63	2.0480	1.6777	1.5809	
	147.46	2.1809	1.6777	1.7677	
	150.00	2.2501	1.6777	1.5899	
4.0D 4.0M.00 L.W. L.000.5 . 5 . D0					
1.2D + 1.6W 93 mph Wind at 90° From Face - P2	10.00	0.0077	0.2013	0.0783	
	70.00	0.3287	1.5740	0.6595	
	80.00	0.4378	1.6952	0.7969	
	95.38	0.6383	0.0216	0.7381	
	100.21	0.7357	1.6908	0.9908	
	107.46	0.8659	1.6903	0.9080	
	115.38	1.0048	0.0302	0.6966	
	120.21	1.1241	1.6896	1.0226	
	135.38	1.4565	1.6885	1.2854	
	140.21	1.5632	1.6885	1.2791	
	142.63	1.6167	1.6885	1.2788	
	147.46	1.7242	1.6885	1.4662	
	150.00	1.7800	1.6885	1.2863	
1.2D + 1.6W 93 mph Wind at 90° From Face - P3	10.00	0.0106	0.2002	0.1020	
·	70.00	0.4312	1.5668	0.8250	
	80.00	0.5721	1.6865	0.9982	
	95.38	0.8330	0.0263	0.9841	
	100.21	0.9514	1.6808	1.2490	
	107.46	1.1152	1.6801	1.1724	
	115.38	1.2941	0.0354	0.9879	
	120.21	1.4378	1.6790	1.3158	
	135.38	1.8496	1.6777	1.5893	
	140.21	1.9818	1.6777	1.5812	
	142.63	2.0480	1.6777	1.5809	
	147.46	2.1809	1.6777	1.7677	
	150.00	2.2501	1.6777	1.5899	

1.2D + 1.6W 93 mph Wind at Normal To Face - P1	10.00	0.0123	0.2033	0.1092	
	70.00	0.4387	1.5942	0.7594	
	80.00	0.5831	1.7192	0.8895	
	95.38	0.8578	-0.0357	1.3788	
	100.21	0.9606	1.7123	1.2780	
	107.46	1.1291	1.7097	1.4182	
	115.38	1.3331	-0.0354	1.9799	
	120.21	1.4594	1.7059	1.7061	
	135.38	1.8862	1.7033	1.6423	
	140.21	2.0228	1.7035	1.6279	
	142.63	2.0909	1.7035	1.6243	
	147.46	2.2278	1.7032	1.6255	
	150.00	2.3023	1.7039	2.5291	
1.2D + 1.6W 93 mph Wind at Normal To Face - P2	10.00	0.0090	0.2034	0.0802	
	70.00	0.3326	1.5940	0.5898	
	80.00	0.4447	1.7191	0.6943	
	95.38	0.6601	-0.0276	1.1308	
	100.21	0.7418	1.7137	1.0173	
	107.46	0.8764	1.7118	1.1569	
	115.38	1.0401	-0.0277	1.6875	
	120.21	1.1422	1.7087	1.4097	
	135.38	1.4885	1.7066	1.3361	
	140.21	1.5995	1.7067	1.3235	
	142.63	1.6547	1.7067	1.3200	
	147.46	1.7660	1.7065	1.3218	
	150.00	1.8270	1.7070	2.2234	
1.2D + 1.6W 93 mph Wind at Normal To Face - P3	10.00	0.0123	0.2033	0.1092	
·	70.00	0.4387	1.5942	0.7594	
	80.00	0.5831	1.7192	0.8895	
	95.38	0.8578	-0.0357	1.3788	
	100.21	0.9606	1.7123	1.2780	
	107.46	1.1291	1.7097	1.4182	
	115.38	1.3331	-0.0354	1.9799	
	120.21	1.4594	1.7059	1.7061	
	135.38	1.8862	1.7033	1.6423	
	140.21	2.0228	1.7035	1.6279	
	142.63	2.0909	1.7035	1.6243	
	147.46	2.2278	1.7032	1.6255	
	150.00	2.3023	1.7039	2.5291	



Mat Foundation Design for Solf Supporting Tower				
Mat Foundation Design for Self Supporting Tower			6/30/2020	
Customer Name:	SBA Communications Corp	EIA/TIA Standard:	EIA-222-G	
Site Name:		Structure Height (Ft.):	150	
Site Nmber:	CT22071-A-SBA	Engineer Name:	M. Baker	
Engr. Number:	94598	Engineer Login ID:		

Foundation Info Obtained from:

Analysis or Design?

Number of Tower Legs:

Base Reactions (Factored):

(1). Individual Leg:

Axial Load (Kips):

Shear Force (Kips):

(2). Tower Base:

Total Vertical Load (Kips):

27.9 3268.7

4.0

23

2.50

Moment (Kips-ft):

Foundation Geometries:

Leg distance (Center-to-Center ft.): Diameter of Pier (ft.): Round

Tower center to mat center (ft):

Length of Pad (ft.):

Thickness of Pad (ft):

Drawings/Calculations

Analysis

3 Legs

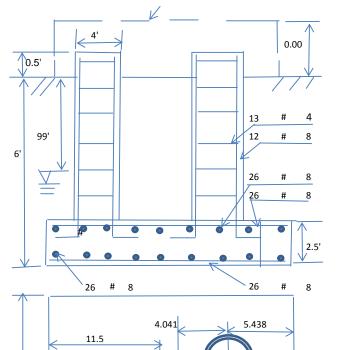
255.2 278.9 Uplift Force (Kips): 27.4

> Total Shear Force (Kips): 39.8

14.0 Mods required -Yes/No ?: No

Pier Height A. G. (ft.): 0.50 2.02083 Depth of Base BG (ft.): 6.0

Width of Pad (ft.):



Material Properties and Reabr Info:

Concrete Strength (psi):	3000	Steel Elastic Modulus:	29000	ksi
Vertical bar yield (ksi)	60	Tie steel yield (ksi):	60	
Vertical Rebar Size #:	8	Tie / Stirrup Size #:	4	
Qty. of Vertical Rebars:	12	Tie Spacing (in):	6.0	
Pad Rebar Yield (Ksi):	60	Pad Steel Rebar Size (#):	8	
Concrete Cover (in.):	3	Unit Weight of Concrete:	150.0	pcf
5 1				

Rebar at the bottom of the concrete pad:

Qty. of Rebar in Pad (L):

26

26

Rebar at the top of the concrete pad:

Qty. of Rebar in Pad (L):

Qty. of Rebar in Pad (W): 26

23

Qty. of Rebar in Pad (W): 26

(W) Mat Center

Mat Center

5.44

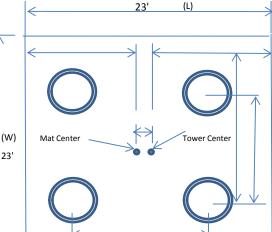
2.02

8.083

14.0

(W)

23'



12.124

Soil Design Parameters:

Soil Unit Weight (pcf):	120.0	Soil Buoyant Weight:	50.0	Pcf	
Water Table B.G.S. (ft):	99.0	Unit Weight of Water:	62.4	pcf	
Ultimate Bearing Pressure (psf):	12000	Consider ties in concrete shear st	trength:	Yes	
Consider Soil Lateral Resistance ?	Yes	Enter soil C (psf) or Phi (deg.):	30.0	Deg.	(۷
		Depth to ignor lateral resistance	1.0	Ft.	2

94598 6/30/2020 TES Engr. Number: Page 2/2 Date:

Farm dation Analysis and B	•	111:64
Apply 1.35 for e/w per G/H:	1.35	

Foundation Analysis and Design: Uplift Strength Reduction Factor:	0.75	Compression Strength Reduction Factor:	0.75		
Total Dry Soil Volume (cu. Ft.):	1719.55	Total Dry Soil Weight (Kips):	206.35		
Total Buoyant Soil Volume (cu. Ft.):	0.00	Total Buoyant Soil Weight (Kips):	0.00		
Total Effective Soil Weight (Kips):	206.35	Weight from the Concrete Block at Top (K):	0.00		
Total Dry Concrete Volume (cu. Ft.):	1473.30	Total Dry Concrete Weight (Kips):	220.99		
Total Buoyant Concrete Volume (cu. Ft.):	0.00	Total Buoyant Concrete Weight (Kips):	0.00		
Total Effective Concrete Weight (Kips):	220.99	Total Vertical Load on Base (Kips):	455.25		
Check Soil Capacities:				Load/ Capacity Ratio	
Calculated Maxium Net Soil Pressure under the base (psf):	3334.67	< Allowable Factored Soil Bearing (psf):	9000	0.37	OK!
Allowable Foundation Overturning Resistance (kips-ft.):	4744.0	> Design Factored Momont (kips-ft):	3550	0.75	OK!
Factor of Safety Against Overturning (O. R. Moment/Design Moment):	1.34	OK!			
Check the capacities of Reinforceing Concrete:					
Strength reduction factor (Flexure and axial tension):	0.90	Strength reduction factor (Shear):	0.75		
Strength reduction factor (Axial compresion):	0.65	Wind Load Factor on Concrete Design:	1.00		
(1) Concrete Pier:				Load/ Capacity Ratio	
Vertical Steel Rebar Area (sq. in./each):	0.79	Tie / Stirrup Area (sq. in./each):	0.20		
Calculated Moment Capacity (Mn,Kips-Ft):	459.6	> Design Factored Moment (Mu, Kips-Ft)	106.8	0.23	OK!
Calculated Shear Capacity (Kips):	215.1	> Design Factored Shear (Kips):	27.4	0.13	OK!
Calculated Tension Capacity (Tn, Kips):	511.9	> Design Factored Tension (Tu Kips):	255.2	0.50	OK!
Calculated Compression Capacity (Pn, Kips):	2386.9	> Design Factored Axial Load (Pu Kips):	278.9	0.12	OK!
Moment & Tension Strength Combination:	0.23	OK! Check Tie Spacing (Design/Req'd):	0.50		
Pier Reinforcement Ratio:	0.005	Reinforcement Ratio is too small			
(2).Concrete Pad:					
One-Way Design Shear Capacity (L or W Direction, Kips):	600.9	> One-Way Factored Shear (L/W-Dir Kips	155.1	0.26	OK!
One-Way Design Shear Capacity (Diagonal Dir., Kips):	511.0	> One-Way Factored Shear (Dia. Dir, Kips	189.7	0.37	OK!
Lower Steel Pad Reinforcement Ratio (L or W-Direct.):	0.0028	Lower Steel Reinf. Ratio (Dia. Dir.):	0.0025		
Lower Steel Pad Moment Capacity (L or W-Dir. Kips-ft):	2368.5	> Moment at Bottom (L-Direct. K-Ft):	498.4	0.21	OK!
Lower Steel Pad Moment Capacity (Dia. Direction,K-ft):	2291.7	> Moment at Bottom (Dia. Dir. K-Ft):	1147.3	0.50	OK!
Upper Steel Pad Reinforcement Ratio (L or W -Direction):	0.0028	Upper Steel Reinf. Ratio (Dia. Dir.):	0.0025		
Upper Steel Pad Moment Capacity (L or W-Dir., Kips-ft):	2368.5	> Moment at the top (L-Dir Kips-Ft):	194.4	0.08	OK!
Upper Steel Pad Moment Capacity (Dia. Direction, K-ft):	2291.7	> Moment at the top (Dia. Dir., K-Ft):	352.9	0.15	OK!
Punching Failure Capacity (Kips):	1019.1	> Punch. Failure Factored Shear (K):	278.9	0.27	OK!

EXHIBIT 8



Tower Engineering Solutions

Phone (972) 483-0607, Fax (972) 975-9615 1320 Greenway Drive, Suite 600, Irving, Texas 75038

Antenna Mount Analysis Report

Existing 150-Ft Self Support Tower

Customer Name: SBA Communications Corp

Customer Site Number: CT22071-A-SBA / Avon (Montevideo)

Customer Site Name: Avon (Montevideo)

Carrier Name: T-Mobile (App#: 134550, V1)

Carrier Site ID / Name: CT11284A / SBA Avon/RT 1777

Site Location: 81 Montevideo Road

Avon, Connecticut

HARTFORD County

Latitude: 41.803100

Longitude: -72.801300

Exp.01/31/2021



Analysis Result:

Max Structural Usage: 61.5%[Pass]

Report Prepared By: Neena Thapa

07/08/2020

Introduction

The purpose of this report is to summarize the analysis results on the (1) Sector Frame at 136.00' elevation to support the proposed antenna configuration. Any modification listed under Sources of Information was assumed completed and was included in this analysis.

Sources of Information

Mount Drawings	Mount Mapping by SGS, dated 6/24/2020
Antenna Loading	Provided by SBA Application #: 134550, v1, dated 6/17/2020
Modification Drawings	N/A

Analysis Criteria

Basic Wind Speed Used in the Analysis: V_{ULT} = 120 mph (3-Sec. Gust) / Equivalent to

 $V_{ASD} = 93 \text{ mph (3-Sec. Gust)}$

Basic Wind Speed with Ice: 50 mph (3-Sec. Gust) with 1" radial ice concurrent

Operational Wind Speed: 60 mph +0" Radial ice

Standard/Codes: ANSI/TIA/EIA 222-G/2015 IBC/2018 CSBC

Exposure Category: B Structure Class: II Topographic Category: 4

Topographic Category: 4 Crest Height (Ft): 135

The site is a Risk Category II structure per IBC Table 1604.5. This site does not support emergency communication equipment for first responders such as fire departments, police, hospitals, ambulance services or any of the facilities listed for Risk Categories III and IV. The scope of work detailed in this structural analysis does not include items that are a part of emergency service as the 911 or essential facility service of an emergency response system.

Mount Information

(1) Sector Frame at 136.00'

Final Antenna Configuration

- 1 RFS APXVAARR24_43-U-NA20 (Octa)
- 1 Ericsson AIR32 KRD901146-1_B66A (Octa)
- 1 Ericsson AIR 21
- 1 Ericsson AIR6449 B41
- 1 Ericsson KRY 112 144/2
- 1 Ericsson Radio 4449 B71 + B12
- 1 Ericsson Radio 4415 B25

In addition to the proposed equipment loading, a 500 lb serviceability load was also considered in this analysis in accordance with TIA requirements.

Analysis Results

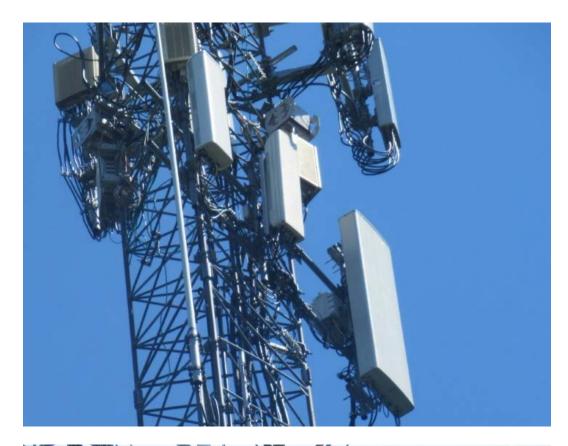
Our calculations have determined that under design wind load the existing mounts will be structurally adequate to support the proposed antenna configuration. The maximum structural usage is 61.5%, which occurs in the face horizontal. The proposed equipment must be installed as stipulated in the Final Antenna Configuration section of this report. The analysis results are void if the proposed equipment is not installed in accordance with this report.

Attachments

- 1. Mount Photos
- 2. Antenna Placement Diagram
- 3. Mount Mapping Information
- 4. Analysis Calculations

Standard Conditions

- 1. The loading configuration as analyzed in this report is as provided from the customer. Any deviation from this design shall be communicated to TES to verify deviation will not adversely impact the analysis.
- 2. The analysis is based on the presumption that the antenna mount members and components along with any existing reinforcement items have been correctly and properly designed, manufactured, installed and maintained.
- 3. All the existing structural members were assumed to be in good condition with no physical damage or deterioration associated with corrosion. The mount analysis is not a condition assessment of the mount.
- 4. The mount analysis was performed in accordance with the loading provided, and if applicable the modification required to support the additional loading.
- 5. If the mount is modified, installation must adhere to the configuration communicated in the modification drawings.
- 6. The modification drawings are not intended to convey means or methods. These are the responsibility of the installing contractor.
- 7. Rigging plan review is available if the contractor requires for a construction class IV or other if required. Review fee would apply.
- 8. The mount modification package was created based upon information provided for the mount loading. The underlying tower is assumed to provide support and sufficient rigidity to support the mount loads as a tower analysis was not part of the mount analysis.
- 9. TES is not responsible for modifications to climbing facilities unless communicated to TES in writing.





Structure: CT22071-A-SBA - Avon (Montevideo)

Sector: A

Structure Type: Self Support

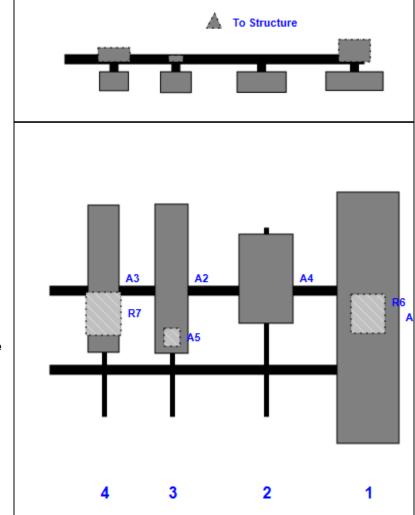
Mount Elev: 136.00

7/8/2020

Page: 1



Plan View



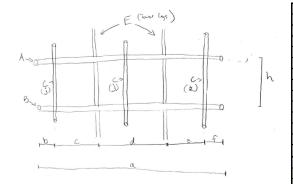
Front View
Looking Toward Structure

Ref#	Model	Height (in)	Width (in)	H Dist Left	Pipe #	Pipe Pos V	Pos	From Top	H Offset	Status	Validation
A1	RFS	95.90	24.00	122.0	1	а	Front	34.50			
R6	Ericsson Radio 4449 B71 +	15.00	13.20	122.0	1	а	Behind	33.00			
A4	Ericsson AIR6449 B41	33.90	20.60	83.00	2	а	Front	19.50			
A2	Ericsson AIR32	57.00	12.90	47.00	3	а	Front	19.50			
A5	Ericsson KRY 112 144/2	6.90	6.10	47.00	3	а	Behind	42.00			
A3	Ericsson AIR 21	56.00	12.10	21.00	4	а	Front	19.50			
R7	Ericsson Radio 4415 B25	16.50	13.40	21.00	4	а	Behind	33.00			



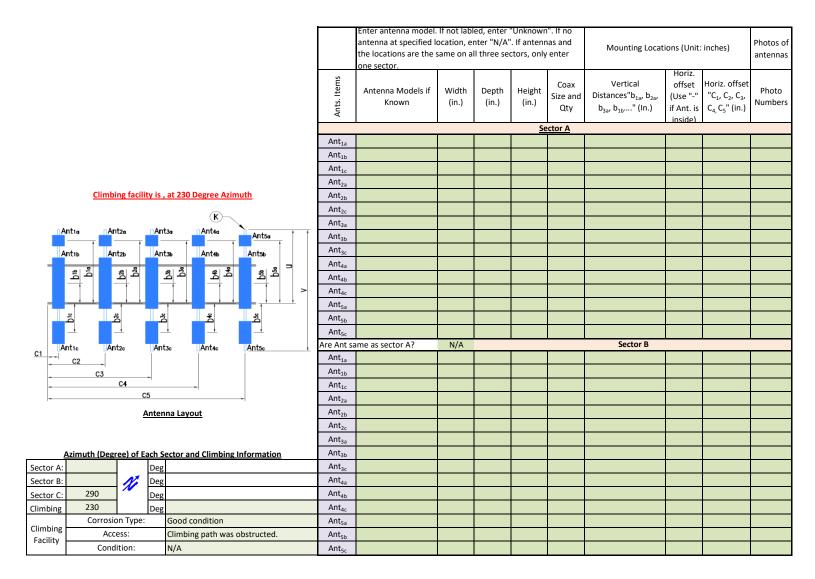
Antenna	a Mount Type "Other" Mapping Form (PA	ATENT PENDING)		Valmont Structures
Tower Owner:	SBA Communications	Mapping Date:	6/24	/20
Site Name:	Avon (Montevideo)	Structure Type:	3-Sided S.	S. Tower
Site Number or ID:	CT22071	Structure Height (Ft.):	15	0
Mapping Contractor:	SGS	Mount Height (Ft.):	13	5

This antenna mapping form is the property of TES and under PATENT PENDING. The formation contained herein is considered confidential in nature and is to be used only for the specific customer it was intended for. Reproduction, transmission, publication, modification or disclosure by any method is prohibited except by express written permission of TES. All means and methods are the responsibility of the contractor and the work shall be compliant with ANSI/ASSE A 10.48, OSHA, FCC, FAA and other safety requirements that may apply. TES is not warrantying the usability of the safety climb as it must be assessed prior to each use in compliance with OSHA requirements.

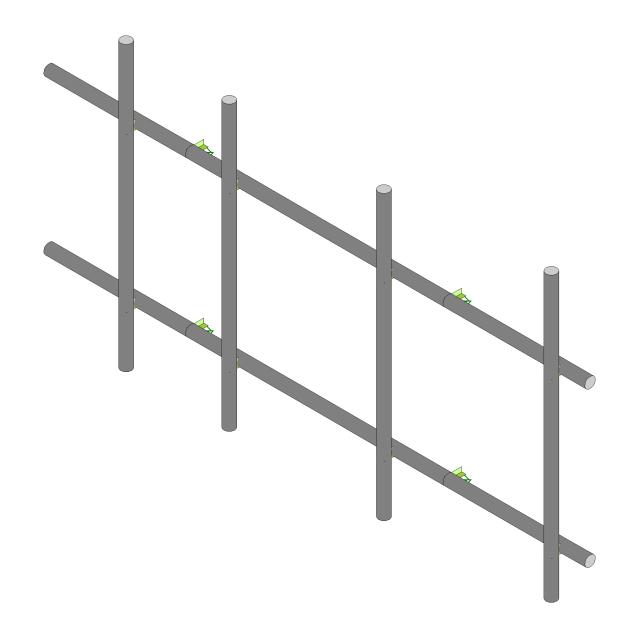


а	126	е	29	j	72	0 S						
b	21	f	4	k	96	p t						
С	12	g		m		q u*		17-21				
d	60	h	36	n		r		v *				
			Memb	ers (Unit: i	nches)	* - See Ant. Layout f	or "u", "v"	and member "	K" (pipe)			
Items	Member	Lx (O.D.)	Ly (I.D.)	T	F	Member	Lx (O.D.)	Ly (I.D.)	Т			
Α	2.375 OD x 0.154 Pipe	2.375	2.067	0.154	F							
В	2.375 OD x 0.154 Pipe	2.375	2.067	0.154	G							
С	2.375 OD x 0.218 Pipe	2.375	1.939	0.218	Н							
D					J							
E	1.75" Solid Rod	1.75	1.75	N/A	K (pipe)*							
Distance f	rom top of bottom sup	port rail t	o lowest ti	p of ant./	eqpt. of Ca	errier above. (N/A if > 2	10 ft.)		5'-4"			
Distance f	rom top of bottom sup	port rail t	o highest t	ip of ant.	eqpt. of C	arrier below. (N/A if >	10 ft.)		N/A			
	Please ente	r the infor	nation bel	ow if men	nbers can'	t be found from the dr	op down li	sts				
*Only one	mount connected to C-A	face of tow	ver at 290 d	legree azim	uths							
Tower Face	Width at the mount (ft.):	5'			Tower Leg Size at the n	nount (in.):	1.75"				

Geometries (Unit: inches)

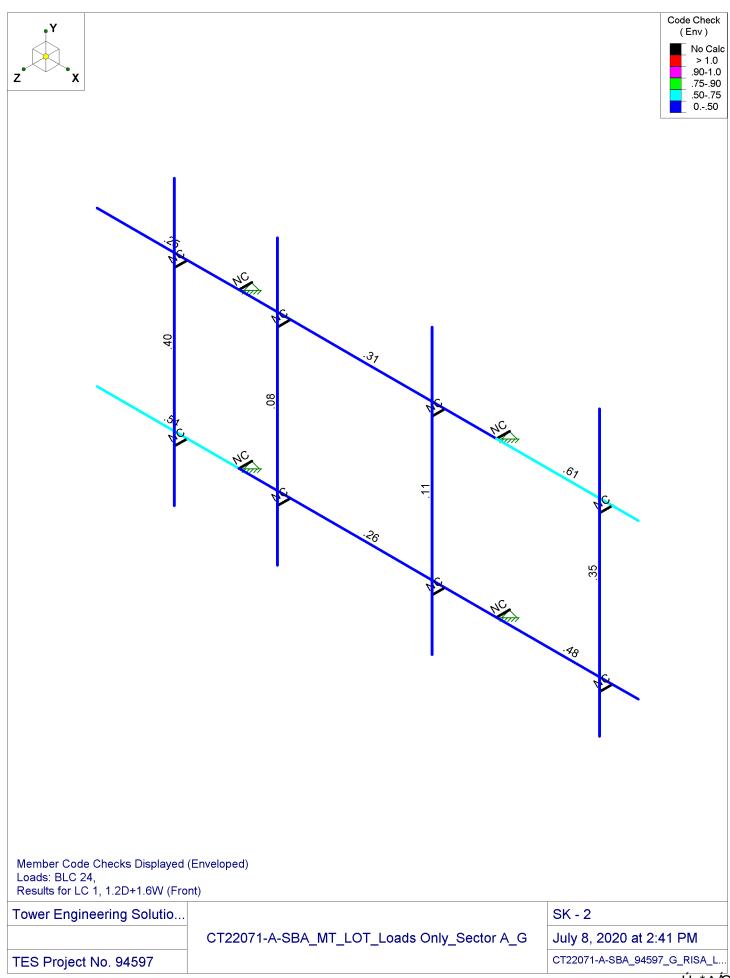


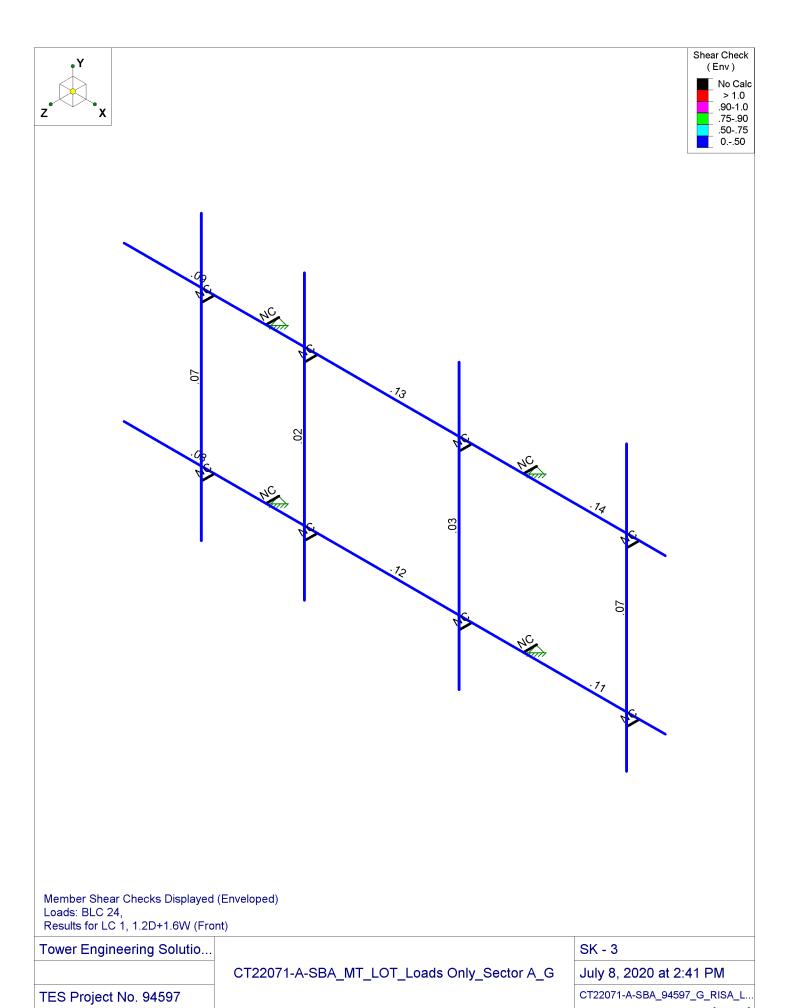




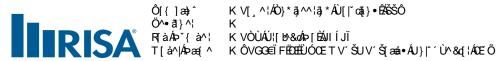
Loads: BLC 24,

Tower Engineering Solutio		SK - 1
	CT22071-A-SBA_MT_LOT_Loads Only_Sector A_G	July 8, 2020 at 2:40 PM
TES Project No. 94597		CT22071-A-SBA_94597_G_RISA_L





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	ÞF€	ĔĖ	ΙĖ̈́ΙJJ	FÈ HHH	€	
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F€	ÞFÌ	ΙĖ̈́ΙJÎΪ	ΙĖ̈́ΙJJ	F ÈHHHH	€	
FF	ÞFJ	ËĚ	FΕ̈́ί	F ÈHHHH	€	
FG	ÞŒ	ËĚ	ΙĖ̈́ΙJJ	FÈHHHH	€	
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FÌ	ÞĜ	ËFĚ	ËÍ	F ÈHHH H	€	
FJ	ÞŒŒ	ËŒ	FΕ̈́ĺ	FÈ HHH	€	
G€	ÞGGŒ	ËŒ	ΙĖ̈́ΙJJ	FÈ HHH	€	
GF	ÞGHŒ	ËŒ	FΕ̈́ĺ	€ÈHHH	€	
Œ	Þ G Œ	ËŒĬ	ΙĔΊIJ	€ÈHHH	€	
GH	ÞGHÓ	ŒĬ	FΕ̈́ĺ	FÈ HHH	€	
G	Ò D⊄	GĚ	ΙĖ̈́ΙJJ	FÈI HHH	€	
GÍ	ÞÍ Œ	GĚ	FΕ̈́ĺ	€ÈHHH	€	
Ĝ	ÞĠŒ	GĚ	ΙĖ̈́ΙJJ	€È HHHH	€	
GÏ	₽Ğ	ËHÈJJÎÏ	FΕ̈́ĺ	FÈI HHH	€	
GÌ	ÞĠ	ËHÈ JJÎÏ	ΙĖ̈́ΙJJ	FÈI HHH	€	
GJ	ÞGJ	IËIJÎÏ	FΕ̈́ĺ	FÈI HHH	€	
H€	ÞH€	IËIJÎÏ	ΙĖ̈́ΙJJ	FÈI HHH	€	
HF	ÞF	ËĖ	FΕ̈́ĺ	FÈI HHH	€	
HG	ÞHG	ËFĚ	ΙĖ̈́ΙJJ	FÈI HHH	€	
HH	ÞH	FĚ	FΕ̈́ĺ	F ÈHHHH	€	
Н	ÞH	FĚ	ΙĖ̈́ΙJJ	F ÈHHHH	€	
HÍ	ÞH	FĚ	ÎÈ	F ÈH-H-H	€	
HÎ	ÞĤ	FĚ	Ėĺ	F È₩₩ ₩	€	
ΗÏ	ÞHÏ	FĚ	FΕ̈́ĺ	FÈI HHH	€	
HÌ	ÞĤ	FĚ	ΙĔΊIJ	FÈ HHH	€	

<chFc``YX'GhYY`GYWfjcb'GYhg</pre>

	Šæà^	Ù@ ≱ ^	V^]^	Ö^∙ ã*} Æãc	Tæc∿¦ãæ¢	Ö^• ã} ÁÜÈ	È0EÄğiGá	Q^ÃŽajlá	Q:Æãjlá	RÁŽ á lá
F	TÁJĄ^	ڌӒGÈE	Ó^æ{	Úą ^	ŒÍ€€ÁÕ¦ÈÓÁÜ^&c	•] •••	FÈ€G	ĒĞ	ĒĠ	FÈGÍ
G	Ùœàãã^¦	ÚŒÓ ŒÈ	Ó^æ{	Úą ^	OÉ €€ÁÕ¦ÈÓÁÜ^&c	V^] a&ae	FÈ€G	ĒĞ	ĒĠ	FÈGÍ
Н	ØØ	ڌӒGÈE	Ó^æ{	Úą ^	OÉI€€ÁÕ¦ÈÓÁÜ^&c	V^] a8æ	FÈ€G	ĒĞ	ĒĠ	FĚGÍ
- 1	Tæã ÁÚã ^	ÚŒÚÒ′IÈE	Ó^æŧ	Úā ^	OÉ €€ÁÕ¦ÈÓÁÜ^&c	V^1 a8aa	GÈÎ	ÎÈG	ÎÈG	FH∄

7c'X': cfa YX'GhYY'GYWJcb'GYhg

	Šæaà^∣	Ù@ 4^	V^]^	Ö^∙ãt}ÆŠãc	Tæe^∖ãæ⇔	Ö^• ã } ÁÜ ^•	OEÁŽAjGá	Q^ÆŽjlá	Q:Æãjlá	RÁŽájIá
F	WÞÒÙVÜW	FĚÔÙFĚ¢€ÎH	Ó^æ	ÔÙ	OÉÏ €ÁÕ¦ÈHH	V^]	ÈΘÍΗ	ÈÏÎ	ÈF	ÈE€ÉHÏI

5`ia]bia GYWi]cb GYhg

	Šæà^	Ù@ ≱ ^	V^]^	Ö^∙ã*}ÁŠã∙c	Tæe^∖ãæ⇔	Ö^• ã} Áܡ ^•	OEÆÃ)Gá	Q^ÃŽajlá	Q:Æãjlá	RÁŽájIá
F	OBŠFOE	OEOEÔÙFIÝFHÈÌ	Ó^æ{	OEOEÁÔ@æ}}^	H€€HËPFI	V^]	FF∄	ПЩ	I€F	FÈŪ

<chFc``YX'GhYY'DfcdYfl]Yg

	Šæ••}^	ÒÃŽ•ãã	ÕÆX•ãã	þř	V@N{ AQAFÒÈ	àD`^}•ãĉŽiĐodÌ	ÈŸã∧∣åŽ∙ãã	Ü^	Ø Ž•ãa	Üc
F	ŒIJĠ	GJ€€€	FFFÍ I	ÈH	ĒÍ	ÈJ	Í€	FÈ	ÎÍ	FÈ
G	OEHÎ ÁÕ¦ÈHÎ	GJ€€€	FFFÍ I	È	ĒÍ	ÈJ	Ĥ	FĚ	ĺĺ	FÈG
Н	OÉÏGÁÕ¦Ě€	GJ€€€	FFFÍ I	ÈH	Ēί	ÈΙ	Í€	FÈ	ÎÍ	FÈ
	OÉ €€ÁÕ¦ÈÓÁÜÞÖ	GJ€€€	FFFÍ I	ÈH	ÊÍ	ĚĞ	IG	FÈ	ĺ	FÈH

K V[, ^\AO)* \$,^^\\$, * AU[| `ca, } • ÊSŠÔ

R″|^ÂIÊÆŒŒ gk fáút Ô@&\^åÆÓ^K ′′′′

<chFc``YX`GhYY`DfcdYfh]Yg`fl7cbh]bi YXL</pre>

	Šæà^∣	ÒÃŽ•ãã	ÕÆX•ãã	Þř	V@\{ AQZFOB	HÖÒ^}•ãcîŽiÐodH	ÈŸãN¦åŽ∙ãã	Ü^	Ø Ž•ãã	Üc
ĺ	OÉ €€ÁÕ¦ÈÓÁÜ^&c	GJ€€€	FFFÍ I	È	Ēĺ	ĚĞ	ΙÎ	FÈ	ĺĺ	FÈH
Î	OÉ HÁÕ¦ ÈÓ	GJ€€€	FFFÍ I	È	Ēĺ	ÈΙ	HÍ	FÊ	΀	FÈG
ï	OEF€ÌÍ	GJ€€€	FFFÍ I	È	Ēĺ	ÈJ	Í€	FÈ	ÎÍ	FÈH

7c'X': cfa YX'GhYY'DfcdYfl]Yg

	Šæà^	ÒÁŽ•ãã	ÕÆX•ãã	Þř	V@\{ ÁQZFÒÍÁROD	OÖ^} •ãcÎŽÐcâHá	ŸãN∣åŽi∙ãã	Ø Ž•ãã
F	OÉÏ€ÆÕ¦ÈH	GJÍ €€	FFHI Î	ÈH	Ēί	ÈΙ	HH	ÍG
G	OÉÉÄÖFÁŐ¦ÉÍ	GJÍ €€	FFHI Î	È	Èí	ÈΙ	ĺĺ	Ï€

5`ia]bia DfcdYfh]Yg

	Šæà^	ÒÆX•ãã	ÕÆŽ•ãã	ÞŤ	V@∧¦{ ÁQÈÈ	ŽÖ^}•ãc°ŽÀ	È√æà ^ÁÓÈ	\c	ØčŽ.•ãã	ØĉŽ•ãa	Ø&îŽi∙ãã	Ø• ઁŽ•ãã	Ôс
F	H€€HËPFI			ÈH	FÈH	ÈΪΗ	Væà ^ÁÓ⊞E	F	FJ	FÎ	FH	FG	FLF
G	Î €Î FË∕Î	F€F€€	HÏÌÏĚ	ÈH	FÈH		Væà ^ÁÓ⊞	F	HÌ	HÍ	HÍ	G	FLF
Н	΀ÎHË∕Í	F€F€€	HÏÌÏĚ	ÈH	FÈH	ÈΪΗ	Væà ^ÁÓ⊞È	F	œ	FÎ	FÎ	FH	FLF
- 1	΀ÎHË∕Î	F€F€€	HÏÌÏĚ	ÈH	FÈH	ÈΪΗ	Væà ^ÁÓ⊞	F	H€	GÍ	ď	FJ	FLF
ĺ	Í€ÍGËPHI	F€G€€		ÈH	FÈH	ÈΪΗ	Væà ^ÁÓ⊞E	F	Н	Ĝ	G	G€	FLF
Î	Î €Î FË∕Î ÁY	F€F€€	HÏÌÏĚ	ÈH	FÈH	ÈΪΗ	Væà ^ÁÓ⊞È	F	G	FÍ	FÍ	FÍ	FLF

A Ya VYf Df]a Ufmi8 UHU

	¥			a b				ä. ~. ~.		# . # . #".v . <u>***</u>
	Šæà^	OÁR[ãjc	RÁR[ã]c	SAR(a)c	Ü[ææ^Çå∰Ù^			Ö^∙ãt}Æšãc	1 æ€^¦ææ¢	Ö^• ã} Áܡ ∰
F	TF	ÞJ	ÞŒŒ			ØØ	Ó^æ{	Úą ^	OÉ €€ÁÕ¦ÈÈ	
G	TG	ÞŒ	ÞŒHÓ			ØØ	Ó^æ{	Ú ą ^	OÉ €€ÁÕ¦ÈÈ	ÈV^]ã&æ ;
H	ΤH	ÞF€	ÞŒŒ			ØØ	Ó^æ	Úą ^	ŒÍ €€ÁÕ¦ÈÈÈ	
1	TI	ÞŒŒ	ÞĠÓ			ØØ	Ó^æ{	Úą ^	ŒÍ €€ÁÕ¦ÈÈ	
ĺ	TÚIŒ	ÞŒ	ÞG			TÁjāj^	Ó^æ{	Úā ^	ŒÍ€€ÁÕ¦ÈÈ	ÈV^1
Î	T ÚHŒ	ÞGH	ÞĜ			TÁÂ^	Ó^æ	Úẩ ^	ŒÉ€ÃÕ¦Œ	È V^]
Ϊ	T ÚFŒ	ÞŒ	ÞĞ			TÁÂ^	Ó^æ	Úẩ ^	CÉ €€ÁÕ¦ÈÈ	È V^]
ì	TF€	ÞG Œ	ÞŒŒ			ÜÕÖÜ	Ó^æ	Þ[}^	ÜÕÖÖ	ÖÜF
J	TFF	ÞGHŒ	ÞŒ			ÜÕÖÖ	Ó^æ	Þ[}^	ÜÕÖÖ	ÖÜF
F€	T F€Œ	ÞĜŒ	ÞĠÓ			ÜÕÖÜ	Ó^æ	Þ[}^	ÜÕÖÖ	ÖÜF
FF	T FFŒ	ÞÍGŒ	ÞŒHÓ			ÜÕÖÜ	Ó^æ	þ[}^	ÜÕÖÖ	ÖÜF
FG	T FG	ÞĠ	ÞFÎ			ÜÕÖÜ	Ó^æ{	þ[}^	ÜÕÖÖ	ÖÜF
FH	T FH	ÞĞ	ÞFÍ			ÜÕÖÖ	Ó^æ{	Þ[}^	ÜÕÖÖ	ÖÜF
FI	T FI	ÞHG	ÞŒ			ÜÕÖÜ	Ó^æ	þ[}^	ÜÕÖÖ	ÖÜF
FÍ	T FÍ	ÞÆ	ÞFJ			ÜÕÖÖ	Ó^æ	þ[}^	ÜÕÖÖ	ÖÜF
FÎ	T FÎ	ÞÆ	ÞFÌ			ÜÕÖÜ	Ó^æ	Þ[}^	ÜÕÖÖ	ÖÜF
FΪ	T FÏ	ÞGJ	ÞFÏ			ÜÕÖÜ	Ó^æ{	Þ[}^	ÜÕÖÖ	ÖÜF
FÌ	T FÌ	ÞĠÓ	ÞFI		Ú	ŰÓÚÓ, Œ E	Ó^æ	Úẩ ^	CÉ HÁÕI ÈÓ	V^]
FJ	T FJ	ÞŒHÓ	ÞFH		Ú	ŰÓÚÓ, CB∰E	Ó^æ	Úẩ ^	CÉ HÁÕI ÈÓ	V^1 a8æ
G€	T ÚŒŒ	ÞH	ÞĤ			TÁA^	Ó^æ	Úā^	OÉ €€ÁÕ¦ÈÈ	È V^1
GF	T GF	ÞÀ	ÞН			ÜÕÖÜ	Ó^æ	þ[}^	ÜÕÖÖ	ÖÜF
Œ	TŒ	ÞHÏ	ÞН			ÜÕÖÖ	Ó^æ	Þ[}^	ÜÕÖÖ	ÖÜF

K V[¸^¦ÁÔ}*ã¸^^¦ã¸*ÁÛ[|ˇơã;}•ÉÆŠŠÔ K K V/ÒÙÁÚ!!! ÞÞ&ÆÐ FÉÁ!! Í JÏ

K VÒÙÁÚ¦[b% aÁÞ [BÁUÍJÏ K ÔVGGEÏ FBÉBEÜÓCE T V´ŠU V´Š[æå•ÁJ} | ^´Ù^& q¦ÁCE Õ R' |^Â\ÊŒŒ GK FÁÚT Ô@&\^åÁÓ^K ′ ′ ′ ′

A Ya VYf'5 Xj UbWYX'8 UHJ

	Šæà^	QÂÜ^ ^æ•^	RÁÜ^ ^æe^	OÁJ~•^cŽajá	RÁU~•^cŽajá	VÐÔÁU} ^	Ú@• & æ	OBjæ∳•ãiAEE	Qa&cã;^	Ù^ã{ã&ÁÖ^•ã}ÁE
F	TF						Ϋ́Λ∙			Þ[}^
G	TG						Ϋ́Λ∙			þ[}^
Н	TH						Ϋ́Λ∙			þ[}^
1	TI						Ϋ́Λ∙			þ[}^
ĺĺ	T ÚI Œ						Ϋ́Λ∙			Þ[}^
Î	T ÚHŒ						ΫΛ∙			þ[}^
Ï	T ÚFŒ						Ϋ́Λ∙			Þ[}^
Ì	TF€						Ϋ́Λ∙			Þ[}^
J	T FF						Ϋ́Λ∙			Þ[}^
F€	T F€Œ						Ϋ́Λ∙			Þ[}^
FF	T FFŒ						ΫΛ∙			Þ[}^
FG	T FG						Ÿ∧•			Þ[}^
FH	T FH						Ÿ∧•			Þ[}^
FI	T FI						Ÿ∧•			Þ[}^
FÍ	T FÍ						Ϋ́Λ∙			Þ[}^
FÎ	T FÎ						Ϋ́Λ∙			Þ[}^
FΪ	T FÏ						Ÿ∧•			Þ[}^
FÌ	T FÌ						Ÿ∧ •			Þ[}^
FJ	T FJ						Ϋ́Λ∙			Þ[}^
G€	T ÚŒE						Ϋ́Λ∙			þ[}^
GF	TGF						Ϋ́Λ∙			Þ[}^
Œ	TŒ						Ϋ́Λ∙			Þ[}^

<chFc``YX'GhYY`8 Yg][b'DUfUa YhYfg</pre>

	Šæà^	Ù@ ∂ }^	Š^}* c@Žcá	Šà^^Žoá	Šà∷Žeá	Š&[{]Áq[]Žæá	iŠ&[{]Áa[cŽeá	iŠË(¦~`Œ	Ē S^^	S::	Ôà	Ø″}&ca[i}
F	TF	ØØ	GËÍ			Šà^^			ŒÈ	ŒÈ		Šæe^læ¢
G	TG	ØØ	ĺ			Šà^^			F	F		Šæe^\a\
Н	TH	ØØ	GËÍ			Šà^^			ŒÈ	ŒÈ		Šæe^læ¢
1	TI	ØØ	ĺ			Šà^^			F	F		Šæe^\a\
ĺ	TÚIŒ	TÁjāj^	ĺĚ			Šà^^						Šæe^læ
Î	T ÚHŒ	TÁjāj^	ĺĚ			Šà^^						Šæe^\a\
Ϊ	T ÚFŒ	TÁjā^	ĺĚ			Šà^^						Šæe^\a
Ì	ΤFÌ	ÚŒÔ Œ				Šà^^			ŒÈ	ŒÈ		Šæe^\a\
J	T FJ	ÚŒÒ′ŒĒ				Šà^^			ŒÈ	ŒÈ		Šæe^\a
F€	T ÚŒE	TÁjāj^	ĺĚ			Šà^^						Šæe^læ

7c`X': cfa YX'GhYY'8 Yg][b'DUfUa YhYfg

Šæà^|Ù@a}^Š^}*ddÈŠà^^ŽoáŠà::ŽoáŠà::ŽoáŠ&[{]ÁddÈŠ&[{]ÝdÈŠČ[¦ˇ¸^ÈÈS^^ S::Ô{EÈHÔ{EÈCÔàÜ æŽoá^Án,EÈEÁ,EÈ Þ[ÁÖæsæÁn[ÁÜ|ð]ơÁEÈ

5`ia]bia8Yg][b'DUfUaYhYfg



>c]bh@UXg'UbX'9bZcfVWX'8]gd`UWYa Ybhg'

R[ãjoÁŠæàn^	ŠÉÖÉT	Öã^&cã}}	Tæ*}ãã å^ŽQà ÉE ĒdDÁQ3 Éæ åDÁQà E• âGÈÈ
	Þ[ÁÖæææÁtjÁÚ¦ð]d	AEE .	

A Ya VYf 'Dc]bh'@cUXg 'f6 @7 '%. '5 bhYbbU'8 Ł

	T^{ à^ ÁŠæà^	Öã^&cã}	Tæ*}ãc°å^ŽjàÈĒeá	Š[&æqā[}ŽadÉĀá
F	T ÚFŒ	Ÿ	Η̈́Ι	Ě
G	T ÚFŒ	Ϋ	ĤΊ	ÍÉÍ
Н	T ÚHŒ	Ϋ	ËÎÈ	Ě
	T ÚHŒ	Ϋ	ËÎÎ	Н
ĺ	T ÚI Œ	Ϋ	ËÍĚ	È
Î	T ÚI Œ	Ϋ	ËÍĚ	Н
Ϊ	T ÚGŒ	Ϋ	Ё́G	É
ì	T ÚGŒ	Ϋ	Ё́G	Н
J	T ÚHŒ	Ϋ	ËFF	HĚ
F€	T ÚFŒ	Ϋ	Ё€	GËÍ
FF	T ÚI Œ	Ϋ	Η̈́Î	GËÍ

A Ya VYf 'Dc]bh'@:UXg'f6 @ '&'. '5 bhYbbU'8]Ł

	T^{ à^¦ASaaà^	Öã^&cã}	Tæ*}ãã å^ŽàÉĒēá ËHG€ĒÐĴJ	Š[&aea[]}ŽebĒĀá
F	T ÚFŒ	Ϋ	ËHG€ÈÌĴ	Ě
G	T ÚFŒ	Ϋ	EHŒÐI J	ÍÉÍ
Н	T ÚHŒ	Ϋ	ËFIÍÈEJÌ	Œ
	T ÚHŒ	Ϋ	ËFIÍ È€JÌ	Н
ĺ	T ÚI Œ	Ϋ	ËHËGF	Œ
Î	T ÚI Œ	Ϋ	ËFHLĚGF	Н
Ϊ	T ÚGŒ	Ϋ	ËG ÈÎ J	Œ
ì	T ÚGŒ	Ϋ	ËFG ÈFÎ J	Н
J	T ÚHŒ	Ϋ	ËGIÈJÍ F	HĚ
F€	T ÚFŒ	Ϋ	ËFF€ÐÌÌ	OEÏÍ
FF	T ÚI Œ	Ϋ	ËJÈĞ	G ∄ Í

A Ya VYf Dc]bh@cUXg f6 @7 " . 5 bhYbbU'K : fcblŁ

	T^{ à^¦ÆŠæà^	Öã^&cã}	Tæ*}ããå^ŽàÉcEcá EGGINEE€Î	Š[&aca[a]}ŽedĒĀá
F	T ÚFŒ	Z	ËGJÈ€Î	Ě
G	T ÚFŒ	Z	ÉGGJÉ€Ű	ÍÉÍ
Н	T ÚHŒ	Z	ËHË()	È
1	T ÚHŒ	Z	ËΗΪĺÌ	Н
ĺ	T ÚI Œ	Z	ËÌÈ€Î	È
Î	T ÚI Œ	Z	ËÎÌÈJ€Î	Н
Ï	T ÚGŒ	Z	ËÍÈÍF	È
Ì	T ÚGŒ	Z	ËÍÈÍF	Н
J	T ÚHŒ	Z	ËË	HĚ
F€	T ÚFŒ	Z	ËHÎ ÈHÎ	GËÍ
FF	T ÚI Œ	Z	ËFËHÏ	GËÍ

A Ya VYf 'Dc]bhi@cUXg'f6 @r'('.'5 bhYbbU'K]': fcbhŁ

		T^{ à^¦ÁŠæà^	Öã^&cã}}	Tæ*}ããå^ŽàÉsÉeá	Š[&anea[]}ŽedĒĀá
F	•	T ÚFŒ	Z	ËÍÈÎÏ	Ě
G	3	T ÚFŒ	Z	ËÍÈĤÏ	ÍÐ

K V[` ^ \AO} * \$\frac{a}{a} * AU[| ` ca{} } • ÊAŠŠÔ

R″|^ÂIÊÆŒŒ gk fáút Ô@\&\\^åÁÓ^K ′′′′

A Ya VYf Dc]bh@cUXg f6 @ (. 5 bhYbbU'K]: fcbhLf7 cbhJbi YXL

	T^{ à^¦ÁŠæà^	Öã^&cã}}	Tæ*}ããå^ŽàÉsÉeá	Š[&andal}ŽadŽá
Н	T ÚHŒ	Z	ËGÎÈJÏ	Ä
I	T ÚHŒ	Z	EGÎ ÈJÏ	H
ĺ	T ÚI Œ	Z	ËĞİ ÈĞİ G	É
Î	T ÚI Œ	Z	ËGÍ ÈGÌ G	H
Ï	T ÚGŒ	Z	ËGHÎ HF	É
Ì	T ÚGŒ	Z	ËGHËHF	H
J	T ÚHŒ	Z	Ë ÈS€Í	HĚ
F€	T ÚFŒ	Z	ËÎ ÈÍ G	GËÍ
FF	T ÚI Œ	Z	ËFÏËÌÌÍ	GËÍ

A Ya VYf 'Dc]bh'@cUXg'f6 @7') . '5 bhYbbU'K 'G]XYŁ

	T^{ à^¦ÆSeeà^	Öã^&cã}	Tæt}ãcå^ŽjàÉcËeá JŒHÍÏ	Š[&æqā[}ŽedÉĀá
F	T ÚFŒ	Ý	JŒĨÍÏ	Ě
G	T ÚFŒ	Ý	JŒĬÍÏ	ÍÉÍ
Н	T ÚHŒ	Ý	ÍHÈÏI	È
- 1	T ÚHŒ	Ý	ÍĦÏÏI	Н
ĺ	T ÚI Œ	Ý	ΙÌĖ̈́ÎÌ	É
Î	T ÚI Œ	Ý	lì Ħî Ì	Н
Ϊ	T ÚGŒ	Ý	GÌ ÈJÍ Ï	È
Ì	T ÚGŒ	Ý	ĠÈÍÏ	Н
J	T ÚHŒ	Ý	HĚG	HĚ
F€	T ÚFŒ	Ý	GÎÈH€Î	GËÍ
FF	T ÚI Œ	Ý	FÌĚÎ	GËÍ

A Ya VYf 'Dc]bh@cUXg 'f6 @ * . 5 bhYbbU'K] G]XYŁ

	T^{ à^!ASaaà^	Öã^&cã}	T æ* } ãc å^ ŽàÈ Ёeá HI Ě FH	Š[&æqā[}ŽædÉĀá
F	T ÚFŒ	Ý		Ě
G	T ÚFŒ	Ý	HIËFH	ÍĖ
Н	T ÚHŒ	Ý	G∈EĬÌI	ÈĠ
- 1	T ÚHŒ	Ý	G€ĬÌI	Н
ĺ	T ÚI Œ	Ý	FÌ ÈÌ J	Œ
Î	T ÚI Œ	Ý	FÌ ÈÌ J	Н
Ϊ	T ÚGŒ	Ý	FFÈJGH	Œ
ì	T ÚGŒ	Ý	FFÈJGH	Н
J	T ÚHŒ	Ý	HĚHÍÌ	HĚ
F€	T ÚFŒ	Ý	FŒHÍ	OËÍ
FF	T ÚI Œ	Ý	JËHF	GËÍ

A Ya VYf 'Dc]bh'@cUXg'f6 @ '+ . 'GYfj]WY @a %L

	T^{ à^¦ÁŠæà^	Öã^&cã[}	Tæ*}ããå^ŽàÉãËeá	Š[∧ā[}ŽadÉĀá
F	TF	Ÿ	Ű€	€

A Ya VYf 'Dc]bh'@cUXg'f6 @7', . 'GYfj]WY @a &L

	T^{à^¦ÁŠæà^	Öã^&cã[}	Tæ*}ããå^ŽàÉsÉeá	Š[&aea[]}ŽebĒĀá
F	T FJ	Ϋ	Ű€	à F€€



A Ya VYf 8]ghf]Vi hYX @ UXg f6 @ '% . Ghf i Wh fY 8]Ł

	T^{à^¦ÆŠæà^	Öã ^8cã }		ÈÒ}åÁTæ≛}ãčå^Ž[à—ĐαÊ2NÈ	Èùca⇔oÁš[&ænā[}ŽedÉÃá	Ò}åÆŠ[&ææã[}ŽoÉÃá
F	TF	Ÿ	ËFÍÈFJG	ËÍÈJG	€	à F€€
G	TG	Ϋ	ËFÍÈFJG	ËFÍÈFJG	€	à F€€
Н	TH	Ÿ	ËFÍÈFJG	ËÍÈJG	€	à F€€
1	ΤI	Ϋ	ËFÍÈFJG	ËFÍÈFJG	€	à F€€
ĺ	t úi Œ	Ϋ	ËFÍÈFJG	ËFÍÈFJG	€	à F€€
Î	T ÚHŒ	Ϋ	ËFÍÈFJG	ËFÍÈFJG	€	à F€€
Ï	T ÚFŒ	Ϋ	ËÍÈJG	ËÍÈJG	€	à F€€
Ì	T FÌ	Ϋ	ËFÍÈFJG	ËÍÈJG	€	à F€€
J	TFJ	Ϋ	ËFÍÈFJG	ËFÍÈFJG	€	à F€€
F€	T ÚŒE	Ϋ	ËFÍÈJG	ËFÍÈFJG	€	à F€€

A Ya VYf 8]ghf]Vi hYX @ UXg f6 @ '%. Ghf i Wh fY K : fcbhL

	T^{à^¦ÆŠæà^	Öã ^8cã }	ÙœadoÁTæt}ããå^ŽjàÐdilli	ÈÒ}åÁTæ≛}ãc`å^Ž(àÐe££20È2)È	ÈÙcæloÁš[&ænā[}ŽedÉĀá	Ò}åÆĞ[&ææã[}ŽodÉÃá
F	TF	ÚZ	ÉÈÏI	ÉÈÏI	€	à F€€
G	TG	ÚZ	ÉÈÏI	ĔĖÏI	€	à F€€
Н	TH	ÚZ	ĔĖÏI	ĔĖÏI	€	à F€€
1	TI	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
ĺ	T ÚI Œ	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
Î	T ÚHŒ	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
Ϊ	T ÚFŒ	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
Ì	T FÌ	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
J	T FJ	ÚZ	ĔÈÏI	ĔÈÏI	€	à F€€
F€	T ÚGŒ	ÚZ	ĔĖÏI	ËËÏI	€	à F€€

A Ya VYf 8]glf]Vi hYX @ UXg f6 @ '%. Glf i Wi fY K]: fcblL

	T^{ à^¦ÁŠæà^	Öã^&cã}	ÙœacÁTæt}ããå^ŽjàÐa££	ÈÒ}åÁTæ≛}ãc`å^Ž(àÐe££20È2)È	ÈÙceboÁŠ[&ænā[}ŽeÉĀá	Ò}åÆŠ[&ææã[}ŽoÉÃá
F	TF	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
G	TG	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
Н	TH	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
1	ΤI	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
ĺ	t úi Œ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
Î	T ÚHŒ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
Ϊ	T ÚFŒ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
ì	T FÌ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
J	T FJ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€
F€	T ÚŒ	ÚZ	ËÈÎÌ	ËÈÎÌ	€	à F€€

A Ya VYf'8]glfjVi hYX'@: UXg'f6 @7'%'. 'Glfi Wf fY'K'G]XYŁ

	T^{à^¦ÆŠæà^	Öã^&cã}}		ÈÒ}åÁTæ≛}ãcčå^ŽjàÐc£20È	ÈÙcækoÁŠ[&ænā[}ŽedÉÃá	Ò}åÆq[&ææq[]}ŽodÉĀá
F	TF	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
G	TG	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
Н	TH	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
1	TI	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
ĺ	T ÚI Œ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
Î	T ÚHŒ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
Ï	T ÚFŒ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
Ì	T FÌ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
J	T FJ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€
F€	T ÚŒ	ÚÝ	ÍÈÏI	ÍÈÏI	€	à F€€

R″|^ÂIÊÆŒŒ gk fáút Ô@&\^åÆÓ^K ′′′′

A Ya VYf 8]glf]Vi hYX @ UXg f6 @ '% . Glf i Wf fY K] G]XYŁ

	T^{à^¦ÆŠæà^	Öã^&cã}	ÙcæboÁTæ*}ãc°å^ŽjàÐoÊE	ÈÒ}åÁTæ*;ãc*å^ŽjàÐc£2ÒÈ	ÈÙcækoÁŠ[&ænā[}ŽedÉÃá	Ò}åÆq̃&ænaã[}ŽodÃá
F	TF	ÚÝ	l È Î Ì	ΙÈÎÌ	€	à F€€
G	TG	ÚÝ	ΙĖÎÌ	ΙÈÎÌ	€	à F€€
Н	TH	ÚÝ	ΙĖÎÌ	ΙÈÎÌ	€	à F€€
1	TI	ÚÝ	ΙÈÎÌ	ΙÈÎÌ	€	à F€€
ĺ	T ÚI Œ	ÚÝ	ΙĖÎÌ	ΙÈÎÌ	€	à F€€
Î	T ÚHŒ	ÚÝ	ΙĖÎÌ	ΙÈÎÌ	€	à F€€
Ϊ	T ÚFŒ	ÚÝ	ΙĖÎÌ	ΙÈÎÌ	€	à F€€
Ì	T FÌ	ÚÝ	lÈîì	ΙÈÎÌ	€	à F€€
J	T FJ	ÚÝ	ΙÈÎÌ	ΙÈÎÌ	€	à F€€
F€	T ÚŒE	ÚÝ	lÈîì	ΙÈÎÌ	€	à F€€

A Ya VYf'5fYU@cUXg'

R[ã] cÁCE	RĮ ã đÓ	R[ãjơÔ	RĮ ã cÁÖ	Öã^&cã}}	Öãrdiãa čo[a]}	Tæ*}ãc°å^Žo∙-á
		Þ[ÁÖæc				

>c]bh6ci bXUfm7cbX]h]cbg

<i>-</i>	~		~	~	, , v	v	/·· \v ··
	R[ãjoÁŠæà∧	ÝÁŽ Đặá	ŸÁŽĐĄjá	ZÁŽ Đặá	ÝÁÜ[dŽ ËdĐæåá	ŸÁÜ[dĚŽĒdĐæåá	ZÁÜ[dĚŽË+dĐæåá
F	Þĺ						
G	ÞÍ						
Н	ÞJ						
I	ÞF€						
İ	ÞFH						
Ĩ	ÞFJ						
Ï	ÞFÍ						
Ì	ÞFÎ						
J	ÞFÏ						
F€	ÞFÌ						
FF	ÞFJ						
FG	ÞŒ						
FH	ÞŒ						
FI	ÞŒ						
FÍ	ÞŒH						
FÎ	ÞG						
FΪ	ÞĞ						
FÌ	ÞĜ						
FJ	ÞÆŒ						
G€	ÞŒŒ						
Œ	ÞGHŒ	Ü^æ&æi }	Ü^æ&aãi}	Ü^æ & æ [}			
Œ	ÞG Œ	Ü^æ s æ i }	Ü^æ&ai }	Ü^æ&æi }			
GH	ÞŒHÓ						
GI	ÞG Ó						
GÍ	ÞĠŒ	Ü^æ s æ[}	Ü^æ \$ æ [}	Ü^æ&æa }			
GÎ	ÞĠŒ	Ü^æ s æ[}	Ü^æ&æi }	Ü^æ&æ{i}}			
G G G	ÞĞ						
GÌ	ÞĠ						
GJ	ÞGJ						
H€	ÞH€						
HF	ÞHF						
HG	ÞHG						

R' |^ Â\ÊŒŒ GK FÁÚT Ô@&\^åÁÓ^K ′′′′

>c]bh6ci bXUfm7cbX]h]cbg'f7cbh]bi YXŁ

	R[ā]oÁŠæà^	ÝÃŽÐajá	ŸÃŽÐājá	ZÁŽHā)á	ÝÁÜ[dĚŽËdĐæåá	ŸÁÜ[dÈŽËdĐæåá	ZÁÜ[dĚŽË-6Dænaaá
HH	ÞН						
Н	ÞH						
HÍ	ÞH						
HÎ	ÞĤ						
ΗÏ	ÞHÏ						
HÌ	ÞĤ						

9bj YcdY'>c]bhFYUM¶cbg

	R[ã]c		ÝÆjaá	ŠÔ	ŸÁÇàá	ŠÔ	Z <i>Ä</i> Žjàá	ŠÔ	ΤÝÆČËcá	ŠÔ	ΤΫΑΚΈσά	ŠÔ	TZÁŽË-cá	ŠÔ
F	ÞGHŒ	1 000	FÎI€ÈEJ	G	ÎIHÈJJ	Î	GÍÍÈG€G	ĺ	€	F	€	F	€	F
G			ËF΀ÏÈHH	F	FFÎ ÊÎ I	F€	GÌÈFÌ	I	€	F	€	F	€	F
Н	ÞG Œ	{ æ¢	FÏJŒHU	G	ÌF€LĚHJ	J	HÍ FÈÌÌ	F	€	F	€	F	€	F
		{ a	ËÌHÌËÏ	F	FFHÈ€JI	F€		O	€	F	€	F	€	F
ĺ	ÞĠŒ	{ æ¢	FÎÏÌÈIJ	F	F€FHĚFH	Î	ÎFIÈĞF	Ŧ	€	F	€	F	€	F
Î		{ a	ËFÍIÏÈÌG	G	ÎIËÌ	F	ËÎJÈIÌ	റ	€	F	€	F	€	F
Ϊ	ÞĠŒ	{ æ¢	FÏÎÏÈ€Î	F	F€FJÈĞİ	ĺ	ÌJHÈÏG	H	€	F	€	F	€	F
Ì		{ a I	ŒììıĚîì	G	Î⊕ÈHH	G	Ë⊞ÎH	G	€	F	€	F	€	F
J	V[œ ; K	{ æ¢	JÌHÈJÍ	ı	HGH€ÈLJÎ	Ï	FJF€Ë⊺G	F						
F€		{ a	ËÌHÈJÍ	Н	ÌÌJĚGJ	F	ËFJF€ËIG	G						

9bj Y`cdY'A Ya VYf 'GYWgcb': cfWYg

	T^{ à^¦	Ù^&		OT¢ão⇔Žàá	ŠÔ	^ÁÙ@^æbŽaaá	ŠÔ	:ÁÙ@^æţŽàá	ŠÔ	V[¦˘˘^Ž̇̀Ëcá	ŠÔ	^ËÆT[{ ^} B	ËŠÔ	:ËÁT[{ ^}È	EŠÔ
F	TF	F	{ æ¢	€	F	€	F	€	F	€	F	€	F	€	F
G			{ a	€	F	ËÍ€	J	€	F	€	F	€	F	€	F
Н		G	{ æ¢	€	F	ËHÈ€Ì	Н	ÍÐÌFG	G	€	F	È€€G	G	ĚFÏ	J
			{ a	€	F	ËÍHÈÈÌ	J	Ë₿FG	F	€	F	ËE€G	F	È€F	Н
ĺ		Н	{ æ¢	€	F	ÉÈÍJ	Н	FFÈ G	G	€	F	È€È	G	FÈ€HÍ	J
Î			{ a	€	F	ËÍÎÈÍJ	J	ËFÈG	F	€	F	ËE€Ì	F	È€	Н
Ϊ		1	{ æ¢	ÍHOÈHU	J	ÊHÈHÏ	F	HJĖTÏ	G	ËŒFI	F€	ÈÍÎ	G	ÈÏI	J
Ì			{ a	ËFÈÌÏ	1	ËHÎHÈ€ÌG	Î	ËHUËII	ĺ	ŒήΙ	J	⊞EÍ I	F	⊞€ÍJ	ΙÏ
J		ĺĺ	{ æ¢	ÍHGÈHU	J	ÊÎŒFÏ	F	ΙÍΉ́Ι	G	ËŒFI	F€	ÈÈÌÍ	G	ÈÍÍ	J
F€			{ a	ËFFÈÌÏ	1	ËHÏÎĒĒ€Î	Î	ËFIHÈ€J	ĺ	⊞fí∣	J	⊞GÌ	F	ÈEGG	F€
FF	TG	F	{ æ¢	FÎÏIĒĦ	G	HH ĚÍÎ	J	FĠ ĐJÍ	<u>ì</u>	ÈEÏÏ	<u>Î</u>	ÈÄI	F	ÈÍÍ	J
FG			{ a	Ė (Ï I ÈÈ) H	F	ÏÈĤ	F€	ËFÈÎ	F	Ë€F	J	⊞HGÍ	G	ÈEGG	F€
FH		G	{ æ¢	FÎÎÎÐÌH	G	G -È FG	J	FIÌĚFÍ	G	È€€G		ĖÌΗ	F	È≘IÎ	J
FI			{ a	ĔĺĴJÈÏĺ	F	ËJÈÌ	F€	ËFIGÈ€JI	F	Œ€FÍ	Ϊ	iii⊤ï ì	G	ËÉÈF	ΙÏ
FÍ		Н	{ æ¢	FÎÎÎÐÌH	G	FÏ∄€I	J	FÍJÈĠI	G	È€€G		È€GÏ	ĺ	È∃H	F€
FÎ			{ a	ĔÍĴJĚÏÍ	F	ËJÉËJ	F€	ËFÍGÐFÌ	F	Œ€FÍ	Ï	ËE€G	F	Ë€FF	G
FΪ		1	{ æ¢	FÎÎÎÐÌH	G	FŒŒI	J	FÎJÊŒ	G	È€€G		ÈG	G	ÈÎÍ	F€
FÌ			{ a	ĔÍĴJĚÏÍ	F	ËFFIÈGIG	Ï	ËÎHÊÎÏ	F	Œ€FÍ	Ï	ËG	F	ËŒF	G
FJ		ĺĺ	{ æ¢	FÎ΀ÈÏH	G	GIÈÐHÎ	F	FI€ÈGÍ	G	⊞⊞i	G	ÈFÌ	G	ĒĠ	Î
G€			{ a	ĖĺÏIĖFÍ	F	Ë∉FĒHÎ	Î	ËGGÎËÎÏ	F	EF) Í	Ï	⊞ÏG	F	ÈÉÎJ	F
GF	TH	F	{ æ¢	€	F	€	F	€	F	€	F	€	F	€	F
GG			{ a	€	F	€	F	€	F	€	F	€	F	€	F
GH		G	{ æ¢	€	F	ËHÈÈÌ	G	ÍÐFG	G	€	F	È€G	G	È€Í	Î
G			{ a	€	F	ËHĚG	<u>ì</u>	Ë₿FG	F	€	F	ËŒ€G	F	È€F	1
GÍ		Н	{ æ¢	€	F	ÉÈÍJ	G	FFÈ G	G	€	F	È€È	G	ÈEFJ	Ì
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ĞÏ		1	{ æ¢	FÍHĚÍÌ	Н	Η̈́Η̈́Η	G	HH€ÈFÍ	G	ŒFÎ	Н	ÈÌÍ	G	È€	



9bj Ycd Y'A Ya VYf GYVVjcb: cfVVg fl cbhjbi YXL

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GÌ	T^{ à^¦	Ù^& │	{ a	É HGÈ HJ	<u>ŠÔ</u> J	AJ@ æ4aa Ê I GÈ€GÌ	J	:ÁÙ@^æ\Žàá ĒGÎ ĒĒ Ì	F	VII A EKA	ì	EALL (^) E	F		#E3U
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IG			{ a	€ OTÍÈÎ L	F	<u>⊞</u> FÎ	Н	E COOTE CE	<u> </u>	€	F	€ E	F	€	F
IH		G	{ æ¢	GFÍ È Î J	+	ÌJĒÌH		FGGÈ€F	<u>F</u>	€	F	ÈHG	F	<u>É</u> JÎ	Н
			{ a	Î∰ÎÍJ	<u> </u>	ËJËÎÌ	Н	Ë COÈ FJ	G	€ È	F	#HG	G	ËŒJÎ	-
lĺ		Н	{ æ¢	Ï JĒ H	<u> </u>	GOĐĐ F	Η.	FĞ ÐÏ H	<u> </u>	ÈÉÎ G	J	ÈHF	G -	<u>È</u> J	J
l Î			{ a	E FOE I	J	<u>EÉ HOJĒ HU</u>	J	ĦÎĦJÏ	F	EEGG	G	∰íJ	J	⊞E F	
ΙΪ			{ æ¢	GÚÉGIF	<u> </u>	Ėĺĺ		FGHÈ€HÍ	<u> </u>	ÈÉÎ G	J	ÈĠ	<u> </u>	ËÌG	J
1Ì		,	{ }	ËÍFËFG	<u> </u>	<u>E</u> HOÊHU	J	ËÈÏF	Ģ	⊞EGG	G	<u> </u>	J	ÈEHG	H
IJ			{ æ¢	€	F	€	H	ÈF	<u> </u>	€	F	€	F	€	F
Í€	1'11 10F	_	{ }	€	F	Ë€FÎ	Ĵ	ËE€I	<u>J</u>	€	F	€	F	€	F
ÍF	T ÚHŒ	F	{ æ¢	€	F	ÈÉF		<u>ÈÉ</u> F	F	€	F	€	F	€	F
ÍG			{ a	€	F	⊞⊕F	Н	∰ï ï		€	F	€	F	€	F
ÍΗ		G	{ æ¢	GÍ FÈ Î Î	<u> </u>	JÏ∄JH		FGJË G	F	€	F	ÈIF	F	È€Í	H
ÍI			{ a	ÌÍÈÏJ	J	ËÏĒJH	Н	Ë GJË (I	G	€	F	⊞FIF	G	⊞€Í	
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EXHIBIT 9



RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CTI1284A

Avon_I 81 Montevideo Road Avon, Connecticut 06001

July 9, 2020

EBI Project Number: 6220002987

Site Comp	liance Summary
Compliance Status:	COMPLIANT
Site total MPE% of FCC general population allowable limit:	13.69%



July 9, 2020

T-Mobile Attn: Jason Overbey, RF Manager 35 Griffin Road South Bloomfield, Connecticut 06002

Emissions Analysis for Site: CT11284A - Avon_I

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **81 Montevideo Road** in **Avon, Connecticut** for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter (μ W/cm²). The number of μ W/cm² calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits; therefore, it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general population may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general population would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter (μ W/cm²). The general population exposure limits for the 600 MHz and 700 MHz frequency bands are approximately 400 μ W/cm² and 467 μ W/cm², respectively. The general population exposure limit for the 1900 MHz (PCS), 2100 MHz (AWS) and 11 GHz frequency bands is 1000 μ W/cm². Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at 81 Montevideo Road in Avon, Connecticut using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was focused at the base of the tower. For this report, the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 LTE channels (600 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) I NR channel (600 MHz Band) was considered for each sector of the proposed installation. This Channel has a transmit power of 80 Watts.
- 3) 2 LTE channels (700 MHz Band) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 4 GSM channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 5) 4 LTE channels (PCS Band 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.



- 6) 2 UMTS channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 7) 2 LTE channels (AWS Band 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
- 8) 2 LTE channels (BRS Band 2500 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 9) 2 NR channels (BRS Band 2500 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 40 Watts per Channel.
- 10) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 11) For the following calculations, the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 12) The antennas used in this modeling are the for the RFS APXVAARR24_43-U-NA20 for the 600 MHz / 600 MHz / 700 MHz / 1900 MHz channel(s), the Ericsson AIR 6449 for the 2500 MHz / 2500 MHz channel(s), the Ericsson AIR 32 for the 1900 MHz / 2100 MHz channel(s), the Ericsson AIR 21 for the 1900 MHz / 2100 MHz channel(s) in Sector C.This is based on feedback from the carrier with regard to anticipated antenna selection. All Antenna gain values and associated transmit power levels are shown in the Site Inventory and Power Data table below. The maximum gain of the antenna per the antenna manufacturer's supplied specifications, minus 10 dB for directional panel antennas and 20 dB for highly focused parabolic microwave dishes, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 13) The antenna mounting height centerline of the proposed antennas is feet above ground level (AGL).



- 14) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 15) All calculations were done with respect to uncontrolled / general population threshold limits.



T-Mobile Site Inventory and Power Data

Sector:	С
Antenna #:	I
Make / Model:	RFS APXVAARR24_43-U- NA20
Frequency Bands:	600 MHz / 600 MHz / 700 MHz / 1900 MHz
Gain:	12.95 dBd / 12.95 dBd / 13.35 dBd / 15.65 dBd
Height (AGL):	feet
Channel Count:	7
Total TX Power (W):	320 Watts
ERP (W):	8,466.41
Antenna CI MPE %:	2.74%
Antenna #:	2
Make / Model:	Ericsson AIR 6449
Frequency Bands:	2500 MHz / 2500 MHz
Gain:	22.05 dBd / 22.05 dBd
Height (AGL):	I36 feet
Channel Count:	4
Total TX Power (W):	160 Watts
ERP (W):	25,651.93
Antenna C2 MPE %:	4.99%
Antenna #:	3
Make / Model:	Ericsson AIR 32
Frequency Bands:	1900 MHz / 2100 MHz
Gain:	15.35 dBd / 15.85 dBd
Height (AGL):	136 feet
Channel Count:	4
Total TX Power (W):	240 Watts
ERP (W):	8,728.31
Antenna C3 MPE %:	1.70%
Antenna #:	4
Make / Model:	Ericsson AIR 21
Frequency Bands:	1900 MHz / 2100 MHz
Gain:	15.35 dBd / 15.35 dBd
Height (AGL):	I36 feet
Channel Count:	8
Total TX Power (W):	240 Watts
ERP (W):	8,226.43
Antenna C4 MPE %:	1.60%

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Site Composite MPE %									
Carrier	MPE %								
T-Mobile (Max at Sector C):	11.02%								
Sprint	2.67%								
Site Total MPE %:	13.69%								

T-Mobile MPE % F	er Sector
T-Mobile Sector C Total:	11.02%
Site Total MPE % :	13.69%

T-Mobile Maximum MPE Power Values (Sector C)								
T-Mobile Frequency Band / Technology (Sector C)	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density (µW/cm²)	Frequency (MHz)	Allowable MPE (μW/cm²)	Calculated % MPE	
T-Mobile 600 MHz LTE	2	591.73	136.0	2.30	600 MHz LTE	400	0.58%	
T-Mobile 600 MHz NR	I	1577.94	136.0	3.07	600 MHz NR	400	0.77%	
T-Mobile 700 MHz LTE	2	648.82	136.0	2.52	700 MHz LTE	467	0.54%	
T-Mobile 1900 MHz LTE	2	2203.69	136.0	8.57	1900 MHz LTE	1000	0.86%	
T-Mobile 2500 MHz LTE	2	6412.98	136.0	24.93	2500 MHz LTE	1000	2.49%	
T-Mobile 2500 MHz NR	2	6412.98	136.0	24.93	2500 MHz NR	1000	2.49%	
T-Mobile 1900 MHz LTE	2	2056.61	136.0	8.00	1900 MHz LTE	1000	0.80%	
T-Mobile 2100 MHz LTE	2	2307.55	136.0	8.97	2100 MHz LTE	1000	0.90%	
T-Mobile 1900 MHz GSM	4	1028.30	136.0	8.00	1900 MHz GSM	1000	0.80%	
T-Mobile 2100 MHz UMTS	4	1028.30	136.0	8.00	2100 MHz UMTS	1000	0.80%	
						Total:	11.02%	

[•] NOTE: Totals may vary by approximately 0.01% due to summation of remainders in calculations.



Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general population exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general population exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)		
Sector C:	11.02%		
T-Mobile Maximum MPE % (Sector C):	11.02%		
Site Total:	13.69%		
Site Compliance Status:	COMPLIANT		

The anticipated composite MPE value for this site assuming all carriers present is **13.69**% of the allowable FCC established general population limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.