

10 Industrial Ave, Suite 3 Mahwah, NJ 07430 Phone: (845)499-4712 Jennifer Notaro Real Estate Consultant

July 29, 2014

#### **Hand Delivered**

Ms. Melanie A. Bachman Acting Executive Director Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

CC to Property Owner Monte, LLC 40 Woodland Street, Hartford, CT 06105

RE: Sprint Spectrum L.P. notice of intent to modify an existing telecommunications facility located at 81 Montevideo Road, Avon, CT 06001. Known to Sprint Spectrum L.P. as site CT03XC053.

#### Dear Ms. Bachman:

In order to accommodate technological changes, implement Code Division Multiple Access ("CDMA") and/or Long Term Evolution ("LTE") capabilities, and enhance system performance in the state of Connecticut, Sprint Spectrum L.P. plans to modify the equipment configurations at many of its existing cell sites. Please accept this letter and attachments as notification, pursuant to R.C.S.A. Section 16-50j-73, of construction which constitutes an exempt modification pursuant to R.C.S.A. Section 16-50j-72(b)(2). In compliance with R.C.S.A. Section 16-50j-73, a copy of this letter and its attachments is being sent to the chief elected official of the municipality in which affected cell site is located.

CDMA employs Spread-Spectrum technology and special coding scheme to allow multiple users to be multiplexed over the same physical channel.

LTE is a new high-performance air interface for cellular mobile communications. It is designed to increase the capacity and speed of mobile telephone networks.

Attached is a summary of the planned modifications, including power density calculations reflecting the change in Sprint's operations at the site. Also included is documentation of the structural sufficiency of the tower to accommodate the revised antenna configuration.

The changes to the facility do not constitute modification as defined Connecticut General Statues ("C.G.S.") Section 16-50i(d) because the general physical characteristics of the facility will not be significantly changed or altered. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for the R.C.S.A. Section 16-50i-72(b)(2).

- 1. The height of the overall structure will not be affected.
- 2. The proposed changes will not extend the site boundaries. There will be no effect on the site compound.
- 3. The proposed changes will not increase the noise level at the existing facility by 6 decibels or more.
- 4. Radio Frequency power density may increase due to the use of one or more CDMA transmissions. Moreover, LTE will utilize additional radio frequencies newly licensed by the FCC for cellular mobile communications. However, the changes will not increase the calculated "worst case" power density for the combined operations at the site to a level at or above the applicable standard for uncontrolled environments as calculated for a mixed frequency site.

For the foregoing reasons Sprint Spectrum L.P. respectfully submits that the proposed changes at the referenced site constitute exempt modifications under R.C.S.A. Section 16-50j-72(b)(2).

Please feel free to call me at (845)-499-4712 or email <a href="Months of English Notaro@Transcendwireless.com">Months of English Notaro@Transcendwireless.com</a> with questions concerning this matter. Thank you for your consideration.

Sincerely,

Jennifer Notaro Real Estate Consultant



## RADIO FREQUENCY FCC REGULATORY COMPLIANCE MAXIMUM PERMISSIBLE EXPOSURE (MPE) ASSESSMENT

**Sprint Existing Facility** 

Site ID: CT03XC053

**Avon Mountain** 

81 Montevideo Road Avon, CT 06001

July 27, 2014

EBI Project Number: 62144004

21 B Street Burlington, MA 01803 Tel: (781) 273.2500 Fax: (781) 273.3311



July 27, 2014

Sprint Attn: RF Engineering Manager 1 International Boulevard, Suite 800 Mahwah, NJ 07495

Re: Radio Frequency Maximum Permissible Exposure (MPE) Assessment for Site: CT03XC053 - Avon Mountain

Site Total: 3.02% - MPE% in full compliance

EBI Consulting was directed to analyze the proposed upgrades to the existing Sprint facility located at 81 Montevideo Road, Avon, CT, for the purpose of determining whether the radio frequency (RF) exposure levels from the proposed Sprint equipment upgrades on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu$ W/cm2). The number of  $\mu$ W/cm2 calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu$ W/cm<sup>2</sup>). The general population exposure limit for the cellular band (850 MHz Band) is approximately 567  $\mu$ W/cm<sup>2</sup>, and the general population exposure limit for the 1900 MHz and 2500 MHz bands is 1000  $\mu$ W/cm<sup>2</sup>. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.



Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

#### **CALCULATIONS**

Calculations were done for the proposed upgrades to the existing Sprint Wireless antenna facility located at 81 Montevideo Road, Avon, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. All calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all emissions were calculated using the following assumptions:

- 1) 3 channels in the 1900 MHz Band were considered for each sector of the proposed installation.
- 2) 1 channel in the 800 MHz Band was considered for each sector of the proposed installation
- 3) 2 channels in the 2500 MHz Band were considered for each sector of the proposed installation.
- 4) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 5) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.



- 6) The antennas used in this modeling are the RFS APXVSPP18-C-A20 and the RFS APXVTM14-C-I20. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APXVSPP18-C-A20 has a 15.9 dBd gain value at its main lobe at 1900 MHz and 13.4 dBd at its main lobe for 850 MHz. The RFS APXVTM14-C-I20 has a 15.9 dBd gain value at its main lobe at 2500 MHz. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 7) The antenna mounting height centerline for the proposed antennas is **147 feet** above ground level (AGL).
- 8) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculation were done with respect to uncontrolled / general public threshold limits

					_											
	Site ID		C053 - Avon Mo													
	Site Addresss	81 Montevi	deo Road, Avor	n, CT, 06001												
	Site Type	Se	elf Support Tow	er												
	Sector 1															
						Power										
						Out Per			Antenna Gain							Power
Antenna						Channel	Number of	Composite	(10 db	Antenna	analysis		Cable Loss	Additional		Density
Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	reduction)	Height (ft)	height	Cable Size	(dB)	Loss (dB)	ERP	Percentage
1a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	147	141	1/2 "	0.5	0	208.04	0.38%
1a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	147	141	1/2 "	0.5	0	39.00	0.12%
1B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	147	141	1/2 "	0.5	0	138.69	0.44%
												Sector to	otal Power D	Density Value:	0.94%	
							Sector 2									
						Power										
						Out Per			Antenna Gain							Power
Antenna						Channel	Number of	Composite	(10 db	Antenna	analysis		Cable Loss	Additional		Density
Number	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	reduction)	Height (ft)	height	Cable Size	(dB)	Loss (dB)	ERP	Percentage
2a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	147	141	1/2 "	0.5	0	208.04	0.38%
2a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	147	141	1/2 "	0.5	0	39.00	0.12%
2B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	147	141	1/2 "	0.5	0	138.69	0.44%
												Sector to	otal Power D	Density Value:	0.94%	
							Sector 3									
						Dower										
						Power Out Per			Antenna Gain							Power
Antenna							Number of	Composite	(10 db	Antenna	analysis		Cable Loss	Additional		Density
	Antenna Make	Antenna Model	Radio Type	Frequency Band	Technology	(Watts)	Channels	Power	,	Height (ft)	height	Cable Size	(dB)	Loss (dB)	ERP	Percentage
3a	RFS	APXVSPP18-C-A20	RRH	1900 MHz	CDMA / LTE	20	3	60	5.9	147	141	1/2 "	0.5	0	208.04	0.38%
3a	RFS	APXVSPP18-C-A20	RRH	850 MHz	CDMA / LTE	20	1	20	3.4	147	141	1/2 "	0.5	0	39.00	0.12%
3B	RFS	APXVTMM14-C-120	RRH	2500 MHz	CDMA / LTE	20	2	40	5.9	147	141	1/2 "	0.5	0	138.69	0.44%
30	1113	7.1.7.4	Mari	2300 141112	CONTA / ETC				3.3	177	171			Density Value:	0.94%	0.4470
												Jector tt	Juli Fowel L	chaity value.	0.5470	

Site Composite MPE %					
Carrier	MPE %				
Sprint	2.83%				
T-Mobile	0.19%				
Total Site MPE %	3.02%				



#### **Summary**

All calculations performed for this analysis yielded results that were well within the allowable limits for general public Maximum Permissible Exposure (MPE) to radio frequency energy.

The anticipated Maximum Composite contributions from the Sprint facility are 2.83% (0.94% from sector 1, 0.94% from sector 2 and 0.94% from sector 3) of the allowable FCC established general public limit considering all three sectors simultaneously sampled at the ground level.

The anticipated composite MPE value for this site assuming all carriers present is **3.02**% of the allowable FCC established general public limit sampled at 6 feet above ground level. This total composite site value is based upon MPE values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.

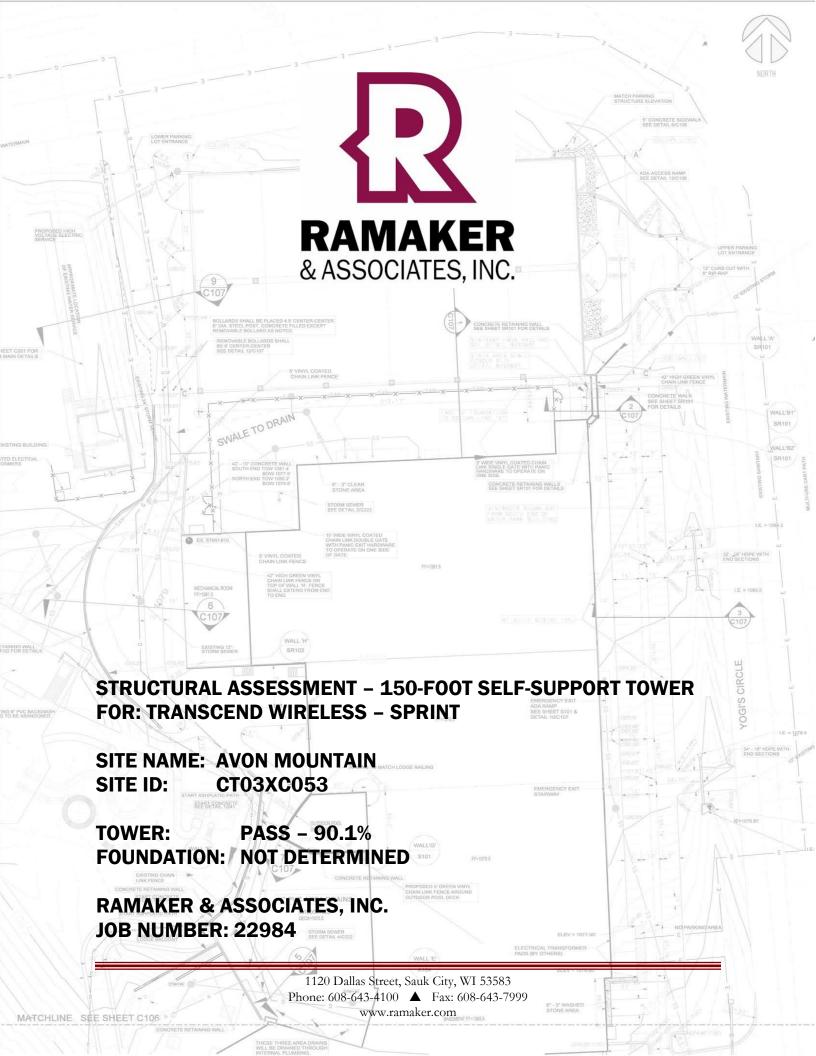
Scott Heffernan

RF Engineering Director

**EBI Consulting** 

21 B Street

Burlington, MA 01803



#### STRUCTURAL ASSESSMENT

SITE: Avon Mountain (CT03XC053)

81 Montevideo Road

Avon, Hartford County, Connecticut 06001

**PREPARED FOR:** Transcend Wireless

**CONTACT PERSON:** Mike Kithcart

**Transcend Wireless** 

48 Spruce Street, Oakland, NJ 07436

**PREPARED BY:** Ramaker & Associates, Inc.

1120 Dallas Street

Sauk City, Wisconsin 53583 Telephone: (608) 643-4100 Facsimile: (608) 643-7999

RAMAKER JOB NUMBER: 22984

**DATE OF REPORT ISSUANCE:** July 14, 2014

Jonathan Styx

**Engineering Technician** 

07/14/14

Date

James R. Skowronski, P.E.

Supervising Engineer

Date

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- B. TOWER CALCULATIONS
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## SECTION 1 EXECUTIVE SUMMARY

This report summarizes the structural analysis conducted by Ramaker & Associates, Inc. (RAMAKER) for Transcend Wireless on behalf of Sprint, who intends to install additional equipment on an existing tower.

The Sprint proposed loading includes installing three (3) RFS APXV9TM14-ALU-120 panel antennas and three (3) Alcatel-Lucent TD-RRH 8x20 units on the two (2) existing steel mounting frames and one (1) proposed steel mounting frame at a centerline elevation of 147-feet AGL. The proposed antennas shall be fed with one (1) new 1-1/4-inch hybrid coax.

Results of our tower analysis show that the tower will be stressed to a maximum of 90.1 percent of capacity under proposed loading conditions. Information regarding the existing soils or the existing tower foundation was not available for analysis. Therefore, no conclusions could be made regarding the adequacy of the existing foundations.

Results of our mount assessment show that by engineering calculation and inspection, the antenna and RRH mounting structure is capable of supporting the existing and proposed Sprint 2.5 equipment deployment without causing an overstress condition in the antenna and RRH mounting structure, provided the proposed structural modifications are completed prior to installation of new equipment per construction drawings by Ramaker & Associates.

In summary, the tower will pass the TIA/EIA-222-F code requirements under proposed loading conditions. However, the adequacy of the existing foundations could not be verified. The mounting structure will pass the TIA-222 code requirements under proposed loading conditions.

## SECTION 2 INTRODUCTION

#### 2.1 PROJECT INFORMATION

This report summarizes the structural analysis conducted by Ramaker & Associates, Inc. (RAMAKER) for Transcend Wireless on behalf of Sprint, who intends to install additional equipment on an existing tower.

#### 2.2 PURPOSE OF REPORT

The analysis activities of this report were conducted for the purposes of creating and analyzing a model of the subject structure under the required loading conditions. Base reactions from the resulting model were also determined for tower foundation and support development. Recommendations regarding the analysis results, loading configuration, and structural modifications are also provided.

#### 2.3 SCOPE OF SERVICES

RAMAKER developed a finite element model (FEM) of the tower, using tnxTower, for member force, joint deflection, and structure reaction determinations. Subsequently, this report was drafted to provide our engineering recommendations. All information contained herein is valid only for the described structure configuration and loading conditions. RAMAKER reserves the right to modify our recommendations should alterations to the tower loading occur.

## SECTION 3 MODEL DEVELOPMENT

#### 3.1 INTRODUCTION

RAMAKER developed a FEM of the tower superstructure. Required static loads consisting of the antenna configuration, wind forces, ice loads, and linear appurtenances (including cable loads) were then applied to the FEM. As a result, all member forces, allowable capacities, and base reactions were computed. Additionally, potentially overstressed members were identified.

#### 3.2 EXISTING STRUCTURE INFORMATION

Existing structure information was gathered from:

• Previous structural analysis by RAMAKER, project number 22984, dated October 10, 2013.

#### 3.3 TOWER LOADING

RAMAKER understands that the tower loading to be used for this analysis will consist of the existing and proposed antenna, mount, and cable configurations as shown in the following chart:

Elevation	Appurtenance	Mount	Coax	Owner	Status
149	Lightning Rod	Tower Leg		Tower	Existing
149	8' Whip Antenna	Tower Leg	(1) 7/8	Tower	Existing
	(3) RFS APXVSPP18-C				
	(3) ALU 1900 MHz 4x40W RRH	Proposed Sector	(6) 1-5/8		Existing
147	(3) ALU 800 MHz 2x50 RRH	Frame (Alpha) Sector Frame (Beta)	(1) 1-1/4	Sprint	
	(3) RFS APXV9TM14-ALU-120	Stand-off (Gamma)	Hybrid		Duamanad
	(3) ALU TD-RRH 8x20 RRH				Proposed
136	(3) RFS APXV18-206516S-C	Sector Frame	(6) 1-5/8	T-Mobile	Existing
121	14' Whip Antenna	Standoff	(1) 7/8	Unknown	Existing
117	21' Whip Antenna	Standoff	(1) 1-1/4	Unknown	Existing
108	10' Dipole Antenna	Standoff	(1) 7/8	Unknown	Existing
105	8' Whip Antenna	Standoff	(1) 1-1/4	Unknown	Existing
102	6'-4" Antenna	Tower Leg	(1) 1/2	Unknown	Existing
98	12' Whip Antenna	Standoff	(1) 7/8	Unknown	Existing
84	3'-6" Microwave Dish	Standoff	(1) 1/4	Unknown	Existing
78	4'-0" Microwave Dish	Standoff	(1) 1/4	Unknown	Existing
74	GPS Antenna	Tower Leg	(1) 1/2	Unknown	Existing
72	4'-0" Microwave Dish	Standoff	(1) 1/4	Unknown	Existing
67	GPS Antenna	Tower Leg	(1) 1/4	Unknown	Existing
12	GPS Antenna	Tower Leg	(2) 1/2	Unknown	Existing

#### 3.4 WIND AND ICE LOAD

Wind forces used in model development are in compliance with the TIA/EIA-222-F Standard. These guidelines call for an analysis to be performed which assumes a basic wind speed of 80 miles-perhour (mph) without ice in Hartford County. The tower is also designed for a 70 mph basic wind speed with 1.25-inch of radial ice.

## SECTION 4 ANALYSIS RESULTS

#### 4.1 ANALYSIS RESULTS

The tower superstructure was analyzed with the combined existing and proposed antenna loading with and without radial ice. The computed maximum tower member stress capacities are as follows:

Component Type	Percent Capacity
Leg	90.1
Diagonal	49.0
Horizontal	37.3
Bolt	58.9
RATING =	90.1

#### 4.2 BASE REACTIONS

The computed maximum reactions under the corresponding maximum moment are as follows:

Load Type	Original Design	Proposed Model
Total Axial (k)		75.0
Total Shear (k)		31.8
Total Moment (k-ft)		2597.3
Leg Uplift (k)		183.5
Leg Compression (k)		239.2
Leg Shear (k)		21.5

Information regarding the existing soils or the existing tower foundation was not available for analysis. Therefore, no conclusions could be made regarding the adequacy of the existing foundations.

#### **AVON MOUNTAIN (CT03XC053)**

#### 4.3 MOUNT ASSESSMENT

Results of our mount assessment show that by engineering calculation and inspection, the antenna and RRH mounting structure is capable of supporting the existing and proposed Sprint 2.5 equipment deployment without causing an overstress condition in the antenna and RRH mounting structure, provided the proposed structural modifications are completed prior to installation of new equipment per construction drawings by Ramaker & Associates.

This assessment is inclusive of the entire antenna mounting structure, including tower platforms, arms, and all other aspects of the mounting structure that will support the Sprint 2.5 equipment deployment. This assessment assumes that the mounting structure(s) has been installed correctly, is free from deterioration, and is maintained properly.

## SECTION 5 LIMITATIONS

The recommendations contained within this report were developed using general project information provided by the owner, tower manufacturer, general field observations, reference information and laboratory testing data, as applicable. All recommendations pertain only to the proposed tower construction, location, and loading as described in this report. RAMAKER assumes no responsibility for failures caused by factors beyond our control. These include but are not limited to the following:

- 1. Missing, corroding, and/or deteriorating members
- 2. Improper manufacturing and/or construction
- 3. Improper maintenance

RAMAKER assumes no responsibility for modifications completed prior to or hereafter in which RAMAKER was not directly involved. These modifications include but are not limited to the following:

- 1. Replacing or strengthening bracing members
- 2. Reinforcing or extending vertical members
- 3. Installing or removing antenna mounting gates or side arms
- 4. Changing loading configurations

Furthermore, RAMAKER hereby states that this document represents the entire report and that it assumes no liability for any factual changes that may occur after the date of this report. All representations, recommendations and conclusions are based on the information contained and set forth herein. If you are aware of any information contrary to that contained herein, or if you are aware of any defects arising from the original design, material, fabrication and erection deficiencies, you should disregard this report and immediately contact RAMAKER. RAMAKER isn't liable for any representation, recommendation or conclusion not expressly stated herein.

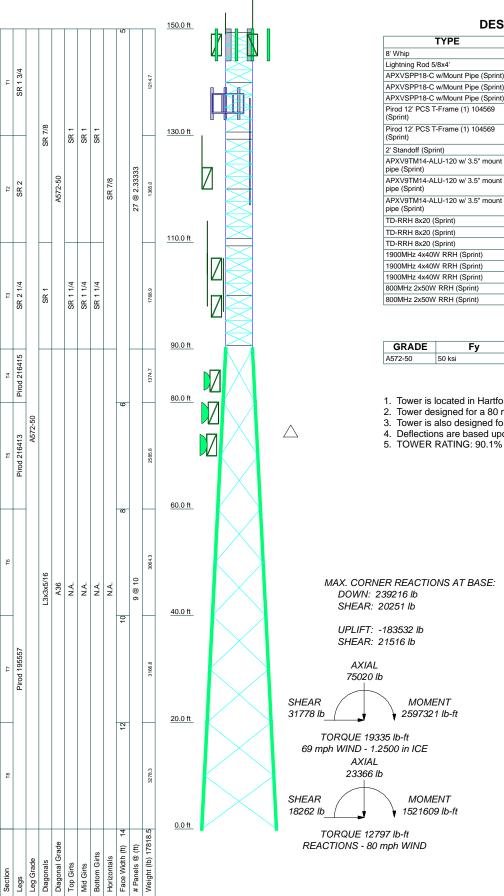
The tower owner is responsible for verifying that the existing loading on the tower is consistent with the loading applied to the tower within this report.

## SECTION 6 REFERENCES

- 1. 2003 International Building Code.
- 2. Telecommunications Industries Association, <u>Structural Standards for Steel Antenna Towers and Antenna Supporting Structures</u>, TIA Standard TIA/EIA-222-F 1996, Washington, D.C.

## APPENDIX A

**TOWER FIGURES** 



DESIGNED APPURTENANCE LOADING	ì
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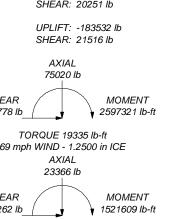
TYPE	ELEVATION	TYPE	ELEVATION	
8' Whip	149	800MHz 2x50W RRH (Sprint)	145	
Lightning Rod 5/8x4'	149	Andrew 12'-6" Universal Sector Frame	136	
APXVSPP18-C w/Mount Pipe (Sprint)	147	(T-Mobile)		
APXVSPP18-C w/Mount Pipe (Sprint)	147	(3) APXV18-206516S-C	136	
APXVSPP18-C w/Mount Pipe (Sprint)	147	15' Omni	121	
Pirod 12' PCS T-Frame (1) 104569	147	6' Standoff	121	
(Sprint)		20' Omni	117	
Pirod 12' PCS T-Frame (1) 104569	147	6' Standoff	117	
(Sprint)		10' Dipole	108	
2' Standoff (Sprint)	147	6' Standoff	108	
APXV9TM14-ALU-120 w/ 3.5" mount	147	8' Whip	105	
pipe (Sprint)	1.47	4' Standoff	105	
APXV9TM14-ALU-120 w/ 3.5" mount pipe (Sprint)	147	8' Omni	102	
APXV9TM14-ALU-120 w/ 3.5" mount	147	6' Standoff	98	
pipe (Sprint)	141	12' Omni	98	
TD-RRH 8x20 (Sprint)	147	3' Standoff	84	
TD-RRH 8x20 (Sprint)	147	3'-6" Dish (84)	84	
TD-RRH 8x20 (Sprint)	147	3' Standoff	78	
1900MHz 4x40W RRH (Sprint)	145	4' Dish	78	
1900MHz 4x40W RRH (Sprint)	145	GPS	74	
1900MHz 4x40W RRH (Sprint)	145	3' Standoff	72	
800MHz 2x50W RRH (Sprint)	145	4' Dish	72	
800MHz 2x50W RRH (Sprint)	145	GPS	67	
(	-	GPS	12	

#### **MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-50	50 ksi	65 ksi	A36	36 ksi	58 ksi

#### **TOWER DESIGN NOTES**

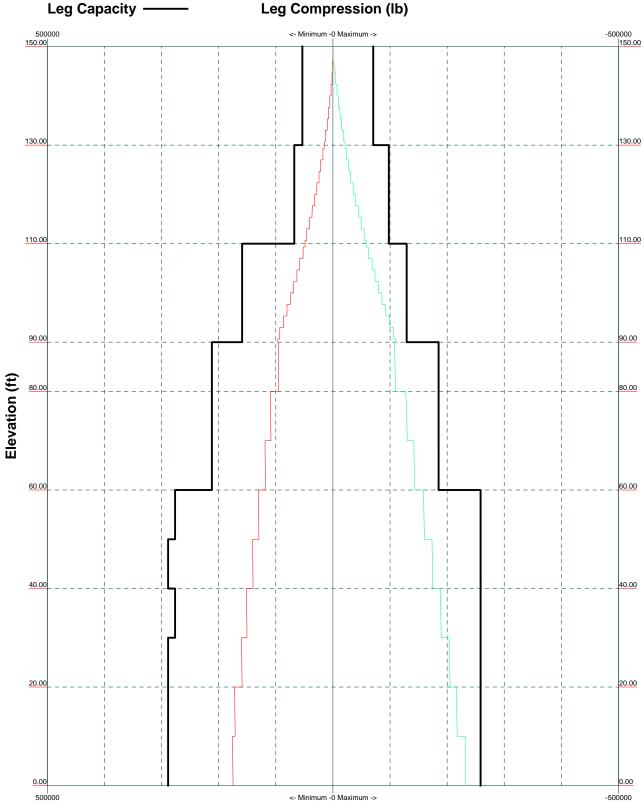
- 1. Tower is located in Hartford County, Connecticut.
- 2. Tower designed for a 80 mph basic wind in accordance with the TIA/EIA-222-F Standard.
- 3. Tower is also designed for a 69 mph basic wind with 1.25 in ice.
- 4. Deflections are based upon a 60 mph wind.



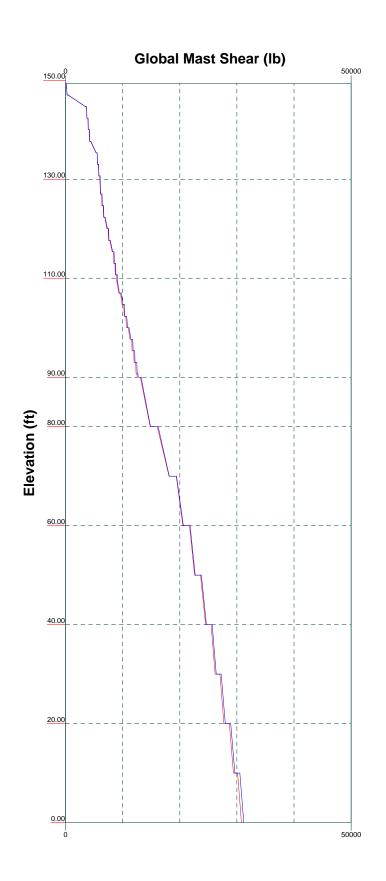
Ramaker & Associates 1120 Dallas St. Sauk City, WI 53583 Phone: (608) 643-4100 FAX: (608) 643-7999

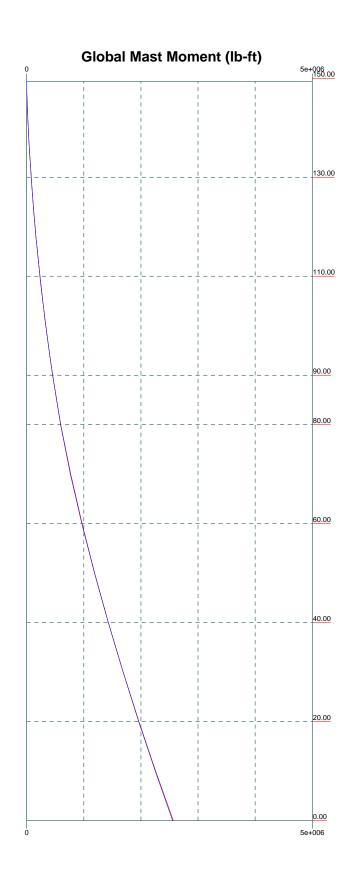
Avon Mountain (CT03XC053) Project: **22984** Client: Sprint Drawn by: JDS App'd: Code: TIA/EIA-222-F Date: 07/03/14 Scale: NTS Path: | Dwg No. E-1

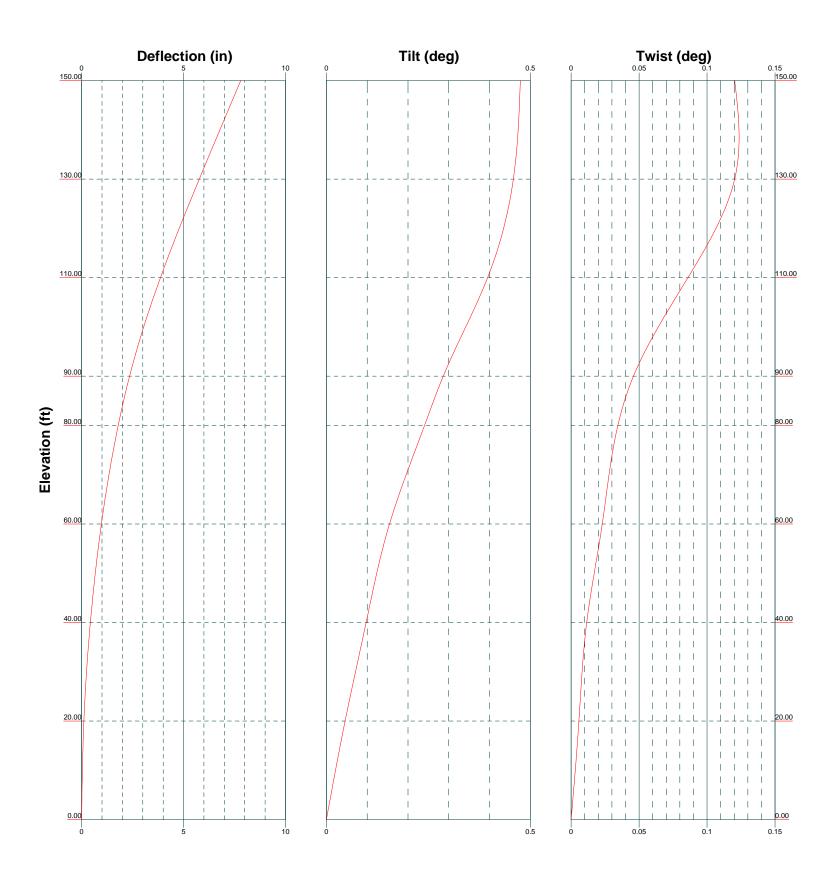
TIA/EIA-222-F - 80 mph/69 mph 1.2500 in Ice Leg Compression (lb)













#### Feed Line Plan

App Out Face

Truss-Leg

App In Face

Flat

Round

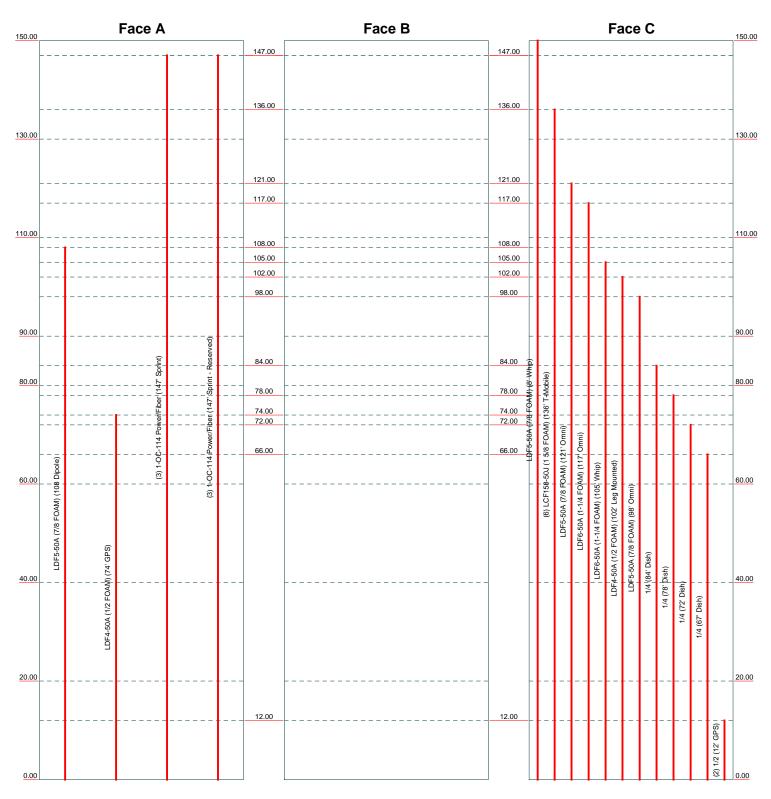
(3) 1-OC-114 Rower/Eiher (1477 Sprint - Reserved) GPS)
LDF5-50A (7/8 FOAM) (108 Dipole)

Ramaker & Associates
1120 Dallas St.
Sauk City, WI 53583
Phone: (608) 643-4100
FAX: (608) 643-7999

Ramaker & Associates

1120 Dallas St.
Sprint
Drawn by: JDS | App'd: Code: TIA/EIA-222-F | Date: 07/03/14 | Scale: NTS |
Path: (122900122984)Structural/Risal22984 Rev2.eri | Dwg No. E-7

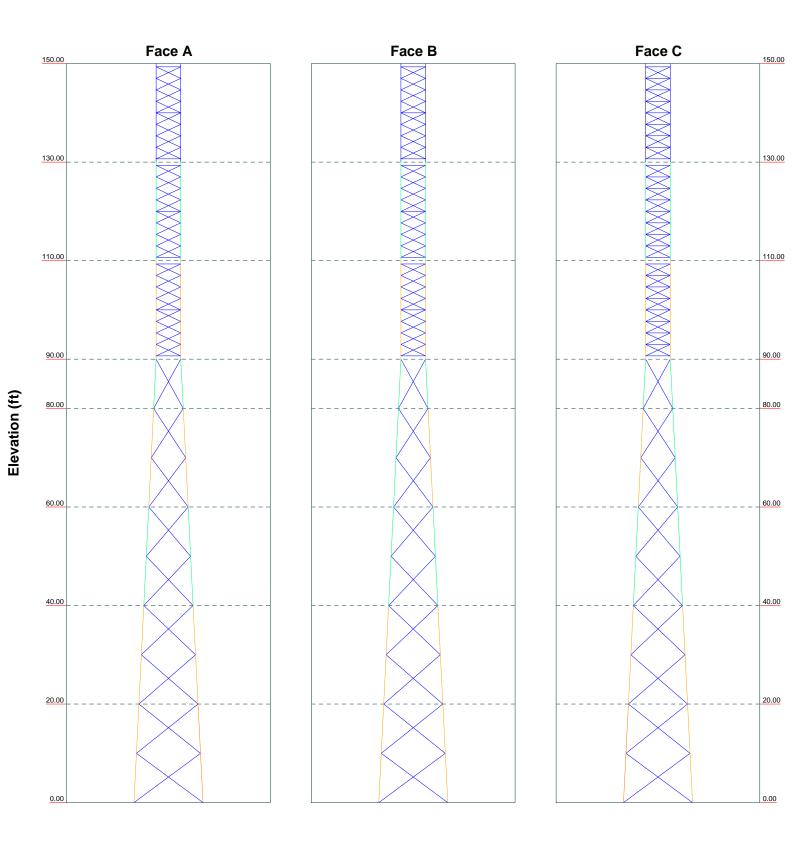




13	Ramaker & Associates	<sup>Job:</sup> Avon Mounta	ain (CT03X	C053)
177	1120 Dallas St.	Project: <b>22984</b>		
RAMAKER LASSOCIATES, INC.	Sauk City, WI 53583	<sup>Client:</sup> Sprint	Drawn by: JDS	App'd:
	Phone: (608) 643-4100	Code: TIA/EIA-222-F	Date: 07/03/14	Scale: NTS
	FAX: (608) 643-7999	Path: I:\22900\22984\Structural\	Risa\22984 Rev2.eri	Dwg No. E-7

#### Stress Distribution Chart 0' - 150'







# APPENDIX B TOWER CALCULATIONS

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tnxTower		Avon Mountain (CT03XC053)	1 of 26
Daniel and C. Annanier	Project		Date
Ramaker & Associates 1120 Dallas St.		22984	09:40:47 07/03/14
Sauk City, WI 53583	Client		Designed by
Phone: (608) 643-4100 FAX: (608) 643-7999		Sprint	JDS

#### **Tower Input Data**

The main tower is a 3x free standing tower with an overall height of 150.00 ft above the ground line.

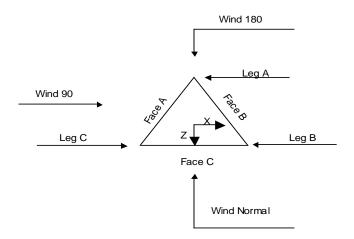
The base of the tower is set at an elevation of 0.00 ft above the ground line.

The face width of the tower is 5.00 ft at the top and 14.00 ft at the base.

This tower is designed using the TIA/EIA-222-F standard.

The following design criteria apply:

- Tower is located in Hartford County, Connecticut.
- Basic wind speed of 80 mph.
- Nominal ice thickness of 1.2500 in.
- Ice density of 56 pcf.
- A wind speed of 69 mph is used in combination with ice.
- Temperature drop of 50 °F.
- Deflections calculated using a wind speed of 60 mph.
- A non-linear (P-delta) analysis was used.
- Pressures are calculated at each section.
- Stress ratio used in tower member design is 1.333.
- Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.



Triangular Tower

### **Tower Section Geometry**

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Tower	Tower	Assembly	Description	Section	Number	Section
Section	Elevation	Database		Width	of	Length
					Sections	
	ft			ft		ft
T1	150.00-130.00			5.00	1	20.00
T2	130.00-110.00			5.00	1	20.00
T3	110.00-90.00			5.00	1	20.00
T4	90.00-80.00			5.00	1	10.00
T5	80.00-60.00			6.00	1	20.00
T6	60.00-40.00			8.00	1	20.00
T7	40.00-20.00			10.00	1	20.00
Т8	20.00-0.00			12.00	1	20.00

Tower Section	Geometry	(cont'd)
---------------	----------	----------

Tower	Tower	Diagonal	Bracing	Has	Has	Top Girt	Bottom Giri
Section	Elevation	Spacing	Type	K Brace	Horizontals	Offset	Offset
				End			
	ft	ft		Panels		in	in
T1	150.00-130.00	2.33	X Brace	No	Steps	8.0000	8.0000
T2	130.00-110.00	2.33	X Brace	No	Steps	8.0000	8.0000
T3	110.00-90.00	2.33	X Brace	No	Steps	8.0000	8.0000
T4	90.00-80.00	10.00	X Brace	No	No	0.0000	0.0000
T5	80.00-60.00	10.00	X Brace	No	No	0.0000	0.0000
T6	60.00-40.00	10.00	X Brace	No	No	0.0000	0.0000
T7	40.00-20.00	10.00	X Brace	No	No	0.0000	0.0000
T8	20.00-0.00	10.00	X Brace	No	No	0.0000	0.0000

## Tower Section Geometry (cont'd)

Tower	Leg	Leg	Leg	Diagonal	Diagonal	Diagonal
Elevation ft	Туре	Size	Grade	Type	Size	Grade
T1 150.00-130.00	Solid Round	1 3/4	A572-50	Solid Round	7/8	A572-50
			(50 ksi)			(50 ksi)
T2 130.00-110.00	Solid Round	2	A572-50	Solid Round	7/8	A572-50
			(50 ksi)			(50 ksi)
T3 110.00-90.00	Solid Round	2 1/4	A572-50	Solid Round	1	A572-50
			(50 ksi)			(50 ksi)
T4 90.00-80.00	Truss Leg	Pirod 216415	A572-50	Equal Angle	L3x3x5/16	A36
	-		(50 ksi)			(36 ksi)
T5 80.00-60.00	Truss Leg	Pirod 216413	A572-50	Equal Angle	L3x3x5/16	A36
	-		(50 ksi)			(36 ksi)
T6 60.00-40.00	Truss Leg	Pirod 195557	A572-50	Equal Angle	L3x3x5/16	A36
	-		(50 ksi)			(36 ksi)
T7 40.00-20.00	Truss Leg	Pirod 195557	A572-50	Equal Angle	L3x3x5/16	A36
	•		(50 ksi)	-		(36 ksi)
T8 20.00-0.00	Truss Leg	Pirod 195557	A572-50	Equal Angle	L3x3x5/16	A36
	-		(50 ksi)	-		(36 ksi)

## **Tower Section Geometry** (cont'd)

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Tower Elevation ft	Top Girt Type	Top Girt Size	Top Girt Grade	Bottom Girt Type	Bottom Girt Size	Bottom Girt Grade
T1 150.00-130.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T2 130.00-110.00	Solid Round	1	A572-50 (50 ksi)	Solid Round	1	A572-50 (50 ksi)
T3 110.00-90.00	Solid Round	1 1/4	A572-50 (50 ksi)	Solid Round	1 1/4	A572-50 (50 ksi)

		To	wer Section	n Geomet	r <b>y</b> (cont'd)		
Tower	No.	Mid Girt	Mid Girt	Mid Girt	Horizontal	Horizontal	Horizontal
Elevation	of Mid	Type	Size	Grade	Type	Size	Grade
ft	Girts						
T1 150.00-130.00	1	Solid Round	1	A572-50	Solid Round	7/8	A572-50
				(50 ksi)			(50 ksi)
T2 130.00-110.00	1	Solid Round	1	A572-50	Solid Round	7/8	A572-50
				(50 ksi)			(50 ksi)
T3 110.00-90.00	1	Solid Round	1 1/4	A572-50	Solid Round	7/8	A572-50
				(50 ksi)			(50 ksi)

Tower Section Geometry (cont'd)												
Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor $A_f$	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals				
ft	ft <sup>2</sup>	in					in	in				
T1 150.00-130.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T2 130.00-110.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T3 110.00-90.00	0.00	0.0000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T4 90.00-80.00	0.33	0.5000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T5 80.00-60.00	0.77	0.5000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T6 60.00-40.00	0.77	0.5000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T7 40.00-20.00	0.77	0.5000	A36 (36 ksi)	1	1	1	36.0000	36.0000				
T8 20.00-0.00	0.77	0.5000	A36 (36 ksi)	1	1	1	36.0000	36.0000				

## **Tower Section Geometry** (cont'd)

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Tower Elevation	Calc K Single	Calc K Solid	Legs	X Brace Diags	K Brace Diags	Single Diags	Girts	Horiz.	Sec. Horiz.	Inner Brace
	Angles	Rounds		X	X	X	X	X	X	X
ft				Y	Y	Y	Y	Y	Y	Y
T1	Yes	Yes	1	1	1	1	1	1	1	1
150.00-130.00				1	1	1	1	1	1	1
T2	Yes	Yes	1	1	1	1	1	1	1	1
130.00-110.00				1	1	1	1	1	1	1
T3	Yes	Yes	1	1	1	1	1	1	1	1
110.00-90.00				1	1	1	1	1	1	1
T4 90.00-80.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T5 80.00-60.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T6 60.00-40.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T7 40.00-20.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1
T8 20.00-0.00	Yes	Yes	1	1	1	1	1	1	1	1
				1	1	1	1	1	1	1

Note: K factors are applied to member segment lengths. K-braces without inner supporting members will have the K factor in the out-of-plane direction applied to the overall length.

### **Tower Section Geometry** (cont'd)

	Truss-Leg K Factors										
	Tru	ss-Legs Used As Leg Men	ibers	Truss-Legs Used As Inner Members							
Tower	Leg	X	Z	Leg	X	Z					
Elevation	Panels	Brace	Brace	Panels	Brace	Brace					
ft		Diagonals	Diagonals		Diagonals	Diagonals					
T4 90.00-80.00	1	0.5	0.85	1	0.5	0.85					
T5 80.00-60.00	1	0.5	0.85	1	0.5	0.85					
T6 60.00-40.00	1	0.5	0.85	1	0.5	0.85					
T7 40.00-20.00	1	0.5	0.85	1	0.5	0.85					
T8 20.00-0.00	1	0.5	0.85	1	0.5	0.85					

### **Tower Section Geometry** (cont'd)

	Dimensi													
Tower	Leg		Diago	nal	Top G	Top Girt		Bottom Girt		Mid Girt		rizontal	Short Hor	rizontal
Elevation														
ft														
	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	U
	Deduct		Deduct		Deduct		Deduct		Deduct		Deduct		Deduct	
	in		in		in		in		in		in		in	
T1	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
150.00-130.00														
T2	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
130.00-110.00														
T3	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
110.00-90.00														
T4 90.00-80.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T5 80.00-60.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T6 60.00-40.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75
T7 40.00-20.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

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Tower Elevation	Leg		Diago	nal	Top G	irt	Bottom	Girt	Mid C	irt	Long Hor	izontal	Short Hor	izontal
Elevation ft														
,	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	U	Net Width	$\overline{U}$
	Deduct		Deduct		Deduct		Deduct		Deduct		Deduct		Deduct	
	in		in		in		in		in		in		in	
T8 20.00-0.00	0.0000	1	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75	0.0000	0.75

## **Tower Section Geometry** (cont'd)

Tower	Leg	Leg		Diagor	ıal	Top G	irt	Bottom	Girt	Mid G	irt	Long Hori	zontal	Short Hort	izontal
Elevation	Connection														
ft	Type														
		Bolt Size	No.	Bolt Size	No.	Bolt Size	No.	Bolt Size	No.						
		in		in		in		in		in		in		in	
T1	Sleeve DS	0.6250	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
150.00-130.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T2	Sleeve DS	0.7500	5	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
130.00-110.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T3	Flange	1.0000	6	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
110.00-90.00		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T4 90.00-80.00	Flange	1.0000	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T5 80.00-60.00	Flange	1.0000	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	_	A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T6 60.00-40.00	Flange	1.0000	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
	_	A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T7 40.00-20.00	Flange	1.0000	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A325N		A325N		A325N		A325N		A325N		A325N		A325N	
T8 20.00-0.00	Flange	1.0000	6	1.2500	1	0.6250	0	0.6250	0	0.6250	0	0.6250	0	0.6250	0
		A687		A325N		A325N		A325N		A325N		A325N		A325N	

## Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Face or	Allow Shield	Component Type	Placement	Face Offset	Lateral Offset	#	# Per	Clear Spacing	Width or I Diameter	Perimeter	Weight
	Leg			ft	in	(Frac FW)		Row	in	in	in	plf
LDF5-50A (7/8 FOAM) (8' Whip) ************************************	С	Yes	Ar (CfAe)	150.00 - 0.00	-16.0000	0.4	1	1	1.0900	1.0900		0.33
LCF158-50J (1 5/8 FOAM) (136' T-Mobile) ************************************	С	Yes	Ar (CfAe)	136.00 - 0.00	-8.0000	0.4	6	3	2.0100	2.0100		0.92
LDF5-50A (7/8 FOAM) (121' Omni)	C	No	Ar (CfAe)	121.00 - 0.00	-20.0000	0.4	1	1	1.0900	1.0900		0.33
LDF6-50A (1-1/4 FOAM) (117' Omni)	С	No	Ar (CfAe)	117.00 - 0.00	-20.0000	0.4	1	1	1.5500	1.5500		0.66
LDF5-50A (7/8 FOAM) (108 Dipole)	A	Yes	Ar (CfAe)	108.00 - 0.00	-18.0000	0.4	1	1	1.0900	1.0900		0.33
LDF6-50A (1-1/4 FOAM) (105' Whip)	C	Yes	Ar (CfAe)	105.00 - 0.00	-16.0000	0.42	1	1	1.5500	1.5500		0.66
LDF4-50A (1/2 FOAM) (102' Leg Mounted)	C	Yes	Ar (CfAe)	102.00 - 0.00	-21.0000	0.4	1	1	0.6300	0.6300		0.15
LDF5-50A (7/8 FOAM)	C	Yes	Ar (CfAe)	98.00 - 0.00	-21.0000	0.4	1	1	1.0900	1.0900		0.33

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Description		Allow Shield	Component Type	Placement	Face Offset	Lateral Offset	#	# Per	Clear Spacing	Width or 1 Diameter	Perimeter	Weight
	Leg			ft	in	(Frac FW)		Row	in	in	in	plf
(98' Omni) ************												
1/4 (84' Dish)	С	Yes	Ar (CfAe)	84.00 - 0.00	-18.0000	0.42	1	1	0.2900	0.2900		0.07
1/4 (78' Dish)	C	Yes	Ar (CfAe)	78.00 - 0.00	-18.0000	0.4	1	1	0.2900	0.2900		0.07
LDF4-50A (1/2 FOAM) (74' GPS)	A	Yes	Ar (CfAe)	74.00 - 0.00	-18.0000	0.42	1	1	0.6300	0.6300		0.15
1/4 (72' Dish)	C	Yes	Ar (CfAe)	72.00 - 0.00	-19.0000	0.42	1	1	0.2900	0.2900		0.07
1/4 (67' Dish)	C	Yes	Ar (CfAe)	66.00 - 0.00	-19.0000	0.4	1	1	0.2900	0.2900		0.07
1/2 (12' GPS) ************************************	C *	Yes	Ar (CfAe)	12.00 - 0.00	0.0000	-0.45	2	2	0.5800	0.5800		0.25
1-OC-114 Power/Fiber (147' Sprint)	A	Yes	Ar (CfAe)	147.00 - 0.00	-10.0000	0.4	3	3	1.5400	1.5400		1.00
1-OC-114 Power/Fiber (147' Sprint - Reserved)	A	Yes	Ar (CfAe)	147.00 - 0.00	-7.0000	0.4	3	3	1.5400	1.5400		1.00

Feed Line/Linear Appurtenances Section Areas											
	T.	r		4			TT7 * 1 .				
Tower	Tower	Face	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight				
Section	Elevation				In Face	Out Face					
	C.		c.2	c2	c.2	c.2	11				

Tower	Tower	гасе	$A_R$	$A_F$	$C_A A_A$	$C_{A}A_{A}$	weigni
Section	Elevation		2	2	In Face	Out Face	
	ft		$ft^2$	$ft^2$	$ft^2$	ft <sup>2</sup>	lb
T1	150.00-130.00	A	13.090	0.000	0.000	0.000	102.00
		В	0.000	0.000	0.000	0.000	0.00
		C	4.832	0.000	0.000	0.000	39.72
T2	130.00-110.00	A	15.400	0.000	0.000	0.000	120.00
		В	0.000	0.000	0.000	0.000	0.00
		C	13.770	0.000	0.000	0.000	125.25
T3	110.00-90.00	A	17.035	0.000	0.000	0.000	125.94
		В	0.000	0.000	0.000	0.000	0.00
		C	19.561	0.000	0.000	0.000	151.14
T4	90.00-80.00	A	8.608	0.000	0.000	0.000	63.30
		В	0.000	0.000	0.000	0.000	0.00
		C	10.955	0.000	0.000	0.000	80.08
T5	80.00-60.00	A	17.952	0.000	0.000	0.000	128.70
		В	0.000	0.000	0.000	0.000	0.00
		C	23.070	0.000	0.000	0.000	163.52
T6	60.00-40.00	A	18.267	0.000	0.000	0.000	129.60
		В	0.000	0.000	0.000	0.000	0.00
		C	23.650	0.000	0.000	0.000	165.20
T7	40.00-20.00	A	18.267	0.000	0.000	0.000	129.60
		В	0.000	0.000	0.000	0.000	0.00
		C	23.650	0.000	0.000	0.000	165.20
T8	20.00-0.00	A	18.267	0.000	0.000	0.000	129.60
		В	0.000	0.000	0.000	0.000	0.00
		C	24.810	0.000	0.000	0.000	171.20

## Feed Line/Linear Appurtenances Section Areas - With Ice

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Tower	Tower	Face	Ice Thickness	$A_R$	$A_F$	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	in			In Face	Out Face	_
	ft	Leg		$ft^2$	$ft^2$	$ft^2$	ft <sup>2</sup>	lb
T1	150.00-130.00	A	1.250	11.447	17.453	0.000	0.000	526.66
		В		0.000	0.000	0.000	0.000	0.00
		C		8.238	4.020	0.000	0.000	306.37
T2	130.00-110.00	A	1.250	13.467	20.533	0.000	0.000	619.60
		В		0.000	0.000	0.000	0.000	0.00
		C		19.153	13.400	0.000	0.000	916.56
T3	110.00-90.00	A	1.250	18.852	20.533	0.000	0.000	689.87
		В		0.000	0.000	0.000	0.000	0.00
		C		36.819	13.400	0.000	0.000	1157.38
T4	90.00-80.00	A	1.250	9.725	10.267	0.000	0.000	348.84
		В		0.000	0.000	0.000	0.000	0.00
		C		23.022	6.700	0.000	0.000	636.22
T5	80.00-60.00	A	1.250	23.102	20.533	0.000	0.000	739.97
		В		0.000	0.000	0.000	0.000	0.00
		C		57.203	13.400	0.000	0.000	1388.70
T6	60.00-40.00	Α	1.250	24.667	20.533	0.000	0.000	758.10
		В		0.000	0.000	0.000	0.000	0.00
		C		62.783	13.400	0.000	0.000	1446.82
T7	40.00-20.00	A	1.250	24.667	20.533	0.000	0.000	758.10
		В		0.000	0.000	0.000	0.000	0.00
		C		62.783	13.400	0.000	0.000	1446.82
T8	20.00-0.00	A	1.250	24.667	20.533	0.000	0.000	758.10
		В		0.000	0.000	0.000	0.000	0.00
		C		65.863	14.560	0.000	0.000	1501.80

	Feed Line Shielding								
Section	Elevation	Face	$A_R$	$A_R$	$A_F$	$A_F$			
	ft		ft²	Ice ft²	ft²	Ice ft²			
T1	150.00-130.00	A	1.006	8.440	0.000	0.000			
	120100 120100	В	0.000	0.000	0.000	0.000			
		C	0.477	4.614	0.000	0.000			
T2	130.00-110.00	A	1.184	9.930	0.000	0.000			
		В	0.000	0.000	0.000	0.000			
		C	1.172	10.126	0.000	0.000			
Т3	110.00-90.00	A	1.519	11.987	0.000	0.000			
		В	0.000	0.000	0.000	0.000			
		C	1.684	14.572	0.000	0.000			
T4	90.00-80.00	A	0.000	1.727	0.892	2.072			
		В	0.000	0.000	0.000	0.000			
		C	0.000	2.017	0.907	2.421			
T5	80.00-60.00	A	0.000	3.181	1.571	3.818			
		В	0.000	0.000	0.000	0.000			
		C	0.000	4.219	1.633	5.063			
T6	60.00-40.00	A	0.000	2.820	1.368	3.384			
		В	0.000	0.000	0.000	0.000			
		C	0.000	3.959	1.441	4.751			
T7	40.00-20.00	A	0.000	2.548	1.236	3.057			
		В	0.000	0.000	0.000	0.000			
		C	0.000	3.577	1.302	4.292			
T8	20.00-0.00	A	0.000	2.378	1.153	2.853			
		В	0.000	0.000	0.000	0.000			
		C	0.000	3.561	1.288	4.273			

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1120 Dallas St.

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	Feed Line Center of Pressure										
Section	Elevation	$CP_X$	CP <sub>Z</sub>	CP <sub>X</sub> Ice	CP <sub>Z</sub> Ice						
	ft	in	in	in	in						
T1	150.00-130.00	-0.7485	-4.6273	-0.5128	-1.2426						
T2	130.00-110.00	-3.2417	-3.7103	-1.6520	-1.2037						
T3	110.00-90.00	-4.0732	-3.6219	-2.8018	-1.5771						
T4	90.00-80.00	-3.1133	-2.1945	-2.9070	-1.1507						
T5	80.00-60.00	-4.2418	-2.4421	-4.6206	-1.1632						
Т6	60.00-40.00	-5.5452	-2.6419	-6.4444	-0.9278						
T7	40.00-20.00	-6.8279	-2.8621	-7.9444	-0.6581						
Т8	20.00-0.00	-7.5270	-2.7521	-9.1645	-0.3117						

			Discrete Tower Loads						
Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			ft ft ft ft	۰	ft		ft <sup>2</sup>	$ft^2$	lb
8' Whip	В	From Leg	0.00 0.00 4.00	0.0000	149.00	No Ice 1/2" Ice 1" Ice 2" Ice	1.36 2.26 3.20 4.57	1.36 2.26 3.20 4.57	43.65 56.01 74.83 131.26
Lightning Rod 5/8x4'	С	From Leg	0.00 0.00 2.00	0.0000	149.00	No Ice 1/2" Ice 1" Ice 2" Ice	0.25 0.66 0.97 1.49	0.25 0.66 0.97 1.49	31.00 33.82 39.29 58.83
********						Z icc	1.47	1.49	30.03
Andrew 12'-6" Universal Sector Frame (T-Mobile)	A	From Face	1.00 0.00 0.00	0.0000	136.00	No Ice 1/2" Ice 1" Ice 2" Ice	10.80 15.10 19.40 28.00	10.80 15.10 19.40 28.00	525.00 675.00 825.00 1125.00
(3) APXV18-206516S-C	A	From Face	1.50 0.00 0.00	0.0000	136.00	No Ice 1/2" Ice 1" Ice 2" Ice	5.93 6.39 6.85 7.81	4.61 4.99 5.43 6.36	18.70 58.72 103.97 210.96
*********						2 100	7.61	0.30	210.90
15' Omni	С	From Leg	4.00 0.00 4.00	0.0000	121.00	No Ice 1/2" Ice 1" Ice 2" Ice	3.75 5.28 6.83 9.97	3.75 5.28 6.83 9.97	40.00 67.80 105.17 209.24
6' Standoff	С	From Leg	2.00 0.00 0.00	0.0000	121.00	No Ice 1/2" Ice 1" Ice 2" Ice	4.97 6.12 7.27 9.57	4.97 6.12 7.27 9.57	70.00 130.00 190.00 310.00
20' Omni	A	From Leg	4.00 0.00 10.00	0.0000	117.00	No Ice 1/2" Ice 1" Ice 2" Ice	5.00 7.03 9.07 13.22	5.00 7.03 9.07 13.22	55.00 91.96 141.55 279.21
6' Standoff	A	From Leg	2.00 0.00 0.00	0.0000	117.00	No Ice 1/2" Ice 1" Ice	4.97 6.12 7.27	4.97 6.12 7.27	70.00 130.00 190.00

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	$C_AA_A$ Side	Weigh
			Vert ft ft ft	0	ft		ft²	ft <sup>2</sup>	lb
			,			2" Ice	9.57	9.57	310.00
10' Dipole	A	From Leg	4.00	0.0000	108.00	No Ice	3.00	3.00	30.00
			0.00			1/2" Ice	4.00	4.00	55.00
			4.00			1" Ice	5.00	5.00	85.00
						2" Ice	6.25	6.25	100.00
6' Standoff	A	From Leg	2.00	0.0000	108.00	No Ice	4.97	4.97	70.00
			0.00			1/2" Ice	6.12	6.12	130.0
			0.00			1" Ice	7.27	7.27	190.0
01.2241 ;	C	г т	4.00	0.0000	105.00	2" Ice	9.57	9.57	310.0
8' Whip	C	From Leg	4.00	0.0000	105.00	No Ice	1.36	1.36	43.65
			0.00			1/2" Ice	2.26	2.26	56.01
			4.00			1" Ice 2" Ice	3.20	3.20	74.83
4' Standoff	C	Enom Loo	2.00	0.0000	105.00	No Ice	4.57 2.72	4.57 2.72	131.2 50.00
4 Standoll	С	From Leg	0.00	0.0000	105.00	1/2" Ice	4.91	4.91	89.00
			0.00			1/2 Ice 1" Ice	7.10	7.10	128.0
			0.00			2" Ice	11.48	11.48	206.0
8' Omni	C	From Leg	0.50	0.0000	102.00	No Ice	2.20	2.20	30.00
o Ollin	C	110III Leg	0.00	0.0000	102.00	1/2" Ice	3.03	3.03	46.24
			0.00			1" Ice	3.57	3.57	67.80
			0.00			2" Ice	4.56	4.56	127.4
12' Omni	C	From Leg	4.00	0.0000	98.00	No Ice	3.00	3.00	35.00
12 0	Ü	Trom Leg	0.00	0.0000	70.00	1/2" Ice	4.23	4.23	57.30
			5.00			1" Ice	5.47	5.47	87.34
						2" Ice	7.69	7.69	171.2
6' Standoff	C	From Leg	2.00	0.0000	98.00	No Ice	4.97	4.97	70.00
		C	0.00			1/2" Ice	6.12	6.12	130.0
			0.00			1" Ice	7.27	7.27	190.0
						2" Ice	9.57	9.57	310.0
******									
3' Standoff	C	From Leg	2.00	0.0000	84.00	No Ice	2.00	2.00	38.00
			0.00			1/2" Ice	3.70	3.70	67.00
			0.00			1" Ice	5.40	5.40	96.00
	_					2" Ice	8.80	8.80	154.0
3' Standoff	C	From Leg	2.00	0.0000	78.00	No Ice	2.00	2.00	38.00
			0.00			1/2" Ice	3.70	3.70	67.00
			0.00			1" Ice	5.40	5.40	96.00
******						2" Ice	8.80	8.80	154.0
GPS	A	From Leg	0.50	0.0000	74.00	No Ice	1.00	1.00	10.00
OI 5	А	110III Leg	0.00	0.0000	74.00	1/2" Ice	1.50	1.50	15.00
			0.00			1" Ice	2.00	2.00	20.00
			0.00			2" Ice	3.00	3.00	30.00
******						_ 100	2.20	2.00	20.00
3' Standoff	C	From Leg	2.00	0.0000	72.00	No Ice	2.00	2.00	38.00
		Č	0.00			1/2" Ice	3.70	3.70	67.00
			0.00			1" Ice	5.40	5.40	96.00
						2" Ice	8.80	8.80	154.0
******									
GPS	C	From Leg	0.50	0.0000	67.00	No Ice	1.00	1.00	10.00
			0.00			1/2" Ice	1.50	1.50	15.00
			0.00			1" Ice	2.00	2.00	20.00
						2" Ice	3.00	3.00	30.00
******		_							
GPS	В	From Leg	0.50	0.0000	12.00	No Ice	1.00	1.00	10.00
			0.00			1/2" Ice	1.50	1.50	15.00
			0.00			1" Ice	2.00	2.00	20.00

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	C <sub>A</sub> A <sub>A</sub> Side	Weight
			Vert ft ft ft	0	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
********						2" Ice	3.00	3.00	30.00
APXVSPP18-C w/Mount Pipe	A	From Leg	0.00	0.0000	147.00	No Ice	8.26	6.71	78.90
(Sprint)		Č	2.00			1/2" Ice	8.81	7.66	144.31
			0.00			1" Ice	9.36	8.49	217.47
						2" Ice	10.50	10.20	390.34
APXVSPP18-C w/Mount Pipe	В	From Leg	0.00	0.0000	147.00	No Ice	8.26	6.71	78.90
(Sprint)			-6.00			1/2" Ice	8.81	7.66	144.31
<b>,</b>			0.00			1" Ice	9.36	8.49	217.47
						2" Ice	10.50	10.20	390.34
APXVSPP18-C w/Mount Pipe	В	From Leg	0.00	0.0000	147.00	No Ice	8.26	6.71	78.90
(Sprint)		C	6.00			1/2" Ice	8.81	7.66	144.31
(-r -/			0.00			1" Ice	9.36	8.49	217.47
						2" Ice	10.50	10.20	390.34
1900MHz 4x40W RRH	A	From Leg	0.00	0.0000	145.00	No Ice	2.71	2.61	60.00
(Sprint)			1.00			1/2" Ice	2.95	2.84	83.12
(-r -/			0.00			1" Ice	3.20	3.09	109.48
						2" Ice	3.72	3.61	172.67
1900MHz 4x40W RRH	В	From Leg	0.00	0.0000	145.00	No Ice	2.71	2.61	60.00
(Sprint)	2	110m Leg	1.00	0.0000	1.0.00	1/2" Ice	2.95	2.84	83.12
(5)11111)			0.00			1" Ice	3.20	3.09	109.48
			0.00			2" Ice	3.72	3.61	172.67
1900MHz 4x40W RRH	C	From Leg	0.00	0.0000	145.00	No Ice	2.71	2.61	60.00
(Sprint)	C	Trom Leg	1.00	0.0000	143.00	1/2" Ice	2.95	2.84	83.12
(Sprint)			0.00			1" Ice	3.20	3.09	109.48
			0.00			2" Ice	3.72	3.61	172.67
800MHz 2x50W RRH	A	From Leg	0.00	0.0000	145.00	No Ice	2.40	2.25	64.00
(Sprint)	А	110m Leg	-1.00	0.0000	143.00	1/2" Ice	2.61	2.46	86.12
(Sprint)			0.00			1" Ice	2.83	2.68	111.30
			0.00			2" Ice	3.30	3.13	171.62
800MHz 2x50W RRH	В	From Leg	0.00	0.0000	145.00	No Ice	2.40	2.25	64.00
(Sprint)	ь	110iii Leg	-1.00	0.0000	143.00	1/2" Ice	2.40	2.46	86.12
(Spriit)			0.00			1" Ice	2.83	2.40	111.30
			0.00			2" Ice	3.30	3.13	171.62
800MHz 2x50W RRH	C	From Leg	0.00	0.0000	145.00	No Ice	2.40	2.25	64.00
(Sprint)	C	110iii Leg	-1.00	0.0000	143.00	1/2" Ice	2.40	2.46	86.12
(Spriit)			0.00			1" Ice	2.83	2.40	111.30
			0.00			2" Ice	3.30	3.13	171.62
Pirod 12' PCS T-Frame (1)	A	From Leg	0.00	0.0000	147.00	No Ice	9.80	9.80	260.00
104569	Α	110III Leg	0.00	0.0000	147.00	1/2" Ice	14.80	14.80	360.00
(Sprint)			0.00			1" Ice	19.80	19.80	460.00
(Sprint)			0.00			2" Ice	29.80	29.80	660.00
Pirod 12' PCS T-Frame (1)	В	From Leg	0.00	0.0000	147.00	No Ice	9.80	9.80	260.00
104569	ь	rioin Leg	0.00	0.0000	147.00	1/2" Ice	14.80	14.80	360.00
(Sprint)			0.00			1" Ice	19.80	19.80	460.00
(Spriit)			0.00			2" Ice	29.80	29.80	
2! Standoff	C	Enom Loo	2.00	0.0000	147.00				660.00
2' Standoff (Sprint)	C	From Leg	2.00 0.00	0.0000	147.00	No Ice 1/2" Ice	1.80 3.30	1.80 3.30	33.00 59.00
(Spinit)			0.00			1/2 Ice 1" Ice	4.80	4.80	85.00
			0.00			2" Ice	4.80 7.80		
APXV9TM14-ALU-120 w/ 3.5"	٨	From Leg	0.00	0.0000	147.00	No Ice		7.80 6.75	137.00
	A	rioiii Leg		0.0000	147.00	No Ice 1/2" Ice	8.20	6.75 7.59	128.00
mount pipe			-2.00				8.85	7.59 8.45	201.91
(Sprint)			0.00			1" Ice 2" Ice	9.51 10.87		285.73
DVMOTM14 AT IT 120/ 2 5"	D	From I as	0.00	0.0000	147.00		10.87	10.26	471.85
APXV9TM14-ALU-120 w/ 3.5"	В	From Leg	0.00	0.0000	147.00	No Ice 1/2" Ice	8.20	6.75	128.00
mount pipe (Sprint)			0.00 0.00			1/2" Ice 1" Ice	8.85 9.51	7.59 8.45	201.91 285.73
			O OO			I ICE	9 7 1	x 45	/X3 /3

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Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		C <sub>A</sub> A <sub>A</sub> Front	$C_AA_A$ Side	Weight
			Vert ft ft ft	0	ft		ft <sup>2</sup>	ft <sup>2</sup>	lb
						2" Ice	10.87	10.26	471.85
APXV9TM14-ALU-120 w/ 3.5"	C	From Leg	2.00	0.0000	147.00	No Ice	8.20	6.75	128.00
mount pipe			0.00			1/2" Ice	8.85	7.59	201.91
(Sprint)			0.00			1" Ice	9.51	8.45	285.73
-						2" Ice	10.87	10.26	471.85
TD-RRH 8x20	Α	From Leg	1.00	0.0000	147.00	No Ice	4.32	1.41	66.13
(Sprint)		•	-0.50			1/2" Ice	4.60	1.61	90.06
			1.00			1" Ice	4.89	1.83	117.33
						2" Ice	5.50	2.28	182.69
TD-RRH 8x20	В	From Leg	1.00	0.0000	147.00	No Ice	4.32	1.41	66.13
(Sprint)			-0.50			1/2" Ice	4.60	1.61	90.06
<b>\ 1</b>			1.00			1" Ice	4.89	1.83	117.33
						2" Ice	5.50	2.28	182.69
TD-RRH 8x20	C	From Leg	1.00	0.0000	147.00	No Ice	4.32	1.41	66.13
(Sprint)			-0.50		,	1/2" Ice	4.60	1.61	90.06
V-1			1.00			1" Ice	4.89	1.83	117.33
			1.00			2" Ice	5.50	2.28	182.69

					Dishe	S					
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weigh
				ft	0	0	ft	ft		$ft^2$	lb
3'-6" Dish	С	Paraboloid w/o	From	3.00	0.0000		84.00	3.50	No Ice	12.57	150.00
(84)		Radome	Leg	0.00					1/2" Ice	13.10	217.2
			•	0.00					1" Ice	13.62	284.49
									2" Ice	14.68	418.9
4' Dish	C	Paraboloid w/o	From	3.00	0.0000		78.00	4.00	No Ice	12.57	150.0
		Radome	Leg	0.00					1/2" Ice	13.10	217.2
			•	0.00					1" Ice	13.62	284.4
									2" Ice	14.68	418.9
4' Dish	C	Paraboloid w/o	From	3.00	0.0000		72.00	4.00	No Ice	12.57	150.0
		Radome	Leg	0.00					1/2" Ice	13.10	217.2
			Ü	0.00					1" Ice	13.62	284.4
									2" Ice	14.68	418.9

	Truss-Leg Properties						
Section Designation	Area	Area Ice	Self Weight	Ice Weight	Equiv. Diameter	Equiv. Diameter Ice	Leg Area
	$in^2$	$in^2$	lb	lb	in	in	$in^2$
Pirod 216415	1080.4244	2978.7225	625.26	936.87	7.5029	20.6856	5.3014
Pirod 216413	2292.1448	5870.4117	549.31	1861.38	7.9588	20.3834	5.3014
Pirod 195557	2421.2300	5942.4117	678.42	1891.12	8.4070	20.6334	7.2158
Pirod 195557	2421.2300	5942.4117	678.42	1891.12	8.4070	20.6334	7.2158

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Section	Area	Area	Self Weight	Ice Weight	Equiv. Diameter	Equiv. Diameter	Leg
Designation		Ice	Weight	Weight	Diameier	Ice	Area
	in <sup>2</sup>	in <sup>2</sup>	lb	lb	in	in	in <sup>2</sup>
Pirod 195557	2421.2300	5942.4117	678.42	1891.12	8.4070	20.6334	7.2158

# **Force Totals**

Load	Vertical	Sum of	Sum of	Sum of Overturning	Sum of Overturning	Sum of Torques
Case	Forces	Forces	Forces	Moments, $M_x$	Moments, $M_z$	
		X	Z	lb-ft	lb-ft	
	lb	lb	lb	,	,	lb-ft
Leg Weight	10650.41					,
Bracing Weight	6959.05					
Total Member Self-Weight	17609.45			-912.97	8459.82	
Gusset Weight	209.05					
Total Weight	23366.04			-912.97	8459.82	
Wind 0 deg - No Ice		1083.13	-18109.75	-1503764.58	-70714.10	-10221.34
Wind 30 deg - No Ice		9578.34	-15188.65	-1272864.77	-787566.77	-9740.20
Wind 60 deg - No Ice		15659.63	-8963.78	-749619.12	-1306970.05	-8473.47
Wind 90 deg - No Ice		18058.90	-633.80	-44999.93	-1507232.50	-5030.12
Wind 120 deg - No Ice		16358.98	8116.86	681946.21	-1351267.58	1531.15
Wind 150 deg - No Ice		8653.26	14874.94	1251947.44	-724691.49	7839.29
Wind 180 deg - No Ice		-63.63	17247.53	1452760.06	8023.37	12029.68
Wind 210 deg - No Ice		-8784.08	15166.03	1269272.87	742464.66	12739.11
Wind 240 deg - No Ice		-15704.37	8989.61	740735.09	1311664.70	8690.19
Wind 270 deg - No Ice		-17642.18	-42.74	-9655.43	1491611.89	2031.21
Wind 300 deg - No Ice		-15102.53	-8568.66	-728127.46	1285792.13	-3556.21
Wind 330 deg - No Ice		-8671.42	-14864.46	-1252954.45	743029.55	-7839.29
Member Ice	34526.12	0071:12	1 100 1.10	1232/31.13	7 13023.33	7037.27
Gusset Ice	140.69					
Total Weight Ice	75020.02			-4323.40	40143.52	
Wind 0 deg - Ice	73020.02	916.24	-31684.90	-2535514.69	-28220.55	-17607.51
Wind 30 deg - Ice		16138.09	-26772.72	-2145744.90	-1248835.16	-15669.45
Wind 60 deg - Ice		27073.27	-15578.05	-1248854.84	-2128011.35	-11130.81
Wind 90 deg - Ice		31333.95	-543.99	-43619.34	-2469751.27	-3707.08
Wind 120 deg - Ice		27989.33	15048.96	1202067.22	-2198677.65	6251.76
Wind 150 deg - Ice		15338.94	26493.92	2118509.99	-1191944.86	14554.80
Wind 180 deg - Ice		-71.63	30559.98	2443702.58	42553.59	18974.93
Wind 210 deg - Ice		-15480.08	26753.99	2135635.07	1277739.67	18153.92
Wind 240 deg - Ice		-27465.92	15804.75	1255572.10	2234909.72	11355.75
Wind 240 deg - Ice Wind 270 deg - Ice		-30988.72	-16.49	-8794.52	2523080.03	1222.60
Wind 300 deg - Ice		-26592.82	-15217.96	-1226249.20	2173964.42	-7844.12
Wind 300 deg - Ice Wind 330 deg - Ice		-15353.99	-26485.23	-2126478.34	1273407.00	-14554.80
Total Weight	23366.04	-13333.99	-20463.23	-2120478.34 -912.97	8459.82	-14334.60
Wind 0 deg - Service	23300.04	609.26	-10186.74	-844664.44	-39210.77	-5749.50
Wind 30 deg - Service		5387.81	-8543.62	-714783.29	-39210.77 -442440.40	-5478.86
Wind 60 deg - Service		8808.54	-5042.12		-734604.74	
<u> </u>		10158.13	-356.51	-420457.62 -24109.32	-734604.74 -847252.37	-4766.33 -2829.44
Wind 90 deg - Service						
Wind 120 deg - Service		9201.93	4565.73 8367.16	384797.88	-759522.10 -407073.05	861.27 4409.60
Wind 180 deg - Service		4867.46	8367.16	705423.57		
Wind 180 deg - Service		-35.79	9701.74	818380.67	5079.06	6766.70
Wind 210 deg - Service		-4941.05	8530.89	715169.13	418202.29	7165.75
Wind 240 deg - Service		-8833.71	5056.66	417866.62	738377.31	4888.23
Wind 270 deg - Service		-9923.73	-24.04	-4228.04	839597.60	1142.56
Wind 300 deg - Service		-8495.17	-4819.87	-408368.56	723823.99	-2000.37
Wind 330 deg - Service		-4877.67	-8361.26	-703583.74	418520.04	-4409.60

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# **Load Combinations**

Comb.		Description
No.		•
1	Dead Only	
2	Dead+Wind 0 deg - No Ice	
3	Dead+Wind 30 deg - No Ice	
4	Dead+Wind 60 deg - No Ice	
5	Dead+Wind 90 deg - No Ice	
6	Dead+Wind 120 deg - No Ice	
7	Dead+Wind 150 deg - No Ice	
8	Dead+Wind 180 deg - No Ice	
9	Dead+Wind 210 deg - No Ice	
10	Dead+Wind 240 deg - No Ice	
11	Dead+Wind 270 deg - No Ice	
12	Dead+Wind 300 deg - No Ice	
13	Dead+Wind 330 deg - No Ice	
14	Dead+Ice+Temp	
15	Dead+Wind 0 deg+Ice+Temp	
16	Dead+Wind 30 deg+Ice+Temp	
17	Dead+Wind 60 deg+Ice+Temp	
18	Dead+Wind 90 deg+Ice+Temp	
19	Dead+Wind 120 deg+Ice+Temp	
20	Dead+Wind 150 deg+Ice+Temp	
21	Dead+Wind 180 deg+Ice+Temp	
22	Dead+Wind 210 deg+Ice+Temp	
23	Dead+Wind 240 deg+Ice+Temp	
24	Dead+Wind 270 deg+Ice+Temp	
25	Dead+Wind 300 deg+Ice+Temp	
26	Dead+Wind 330 deg+Ice+Temp	
27	Dead+Wind 0 deg - Service	
28	Dead+Wind 30 deg - Service	
29	Dead+Wind 60 deg - Service	
30	Dead+Wind 90 deg - Service	
31	Dead+Wind 120 deg - Service	
32	Dead+Wind 150 deg - Service	
33	Dead+Wind 180 deg - Service	
34	Dead+Wind 210 deg - Service	
35	Dead+Wind 240 deg - Service	
36	Dead+Wind 270 deg - Service	
37	Dead+Wind 300 deg - Service	
38	Dead+Wind 330 deg - Service	

# **Maximum Member Forces**

Section	Elevation	Component	Condition	Gov.	Force	Major Axis	Minor Axis
No.	ft	Type		Load		Moment	Moment
	·	**		Comb.	lb	lb-ft	lb-ft
T1	150 - 130	Leg	Max Tension	25	15309.10	-931.53	-608.42
			Max. Compression	15	-21203.28	-8.39	302.20
			Max. Mx	24	-3574.68	-1093.41	-1.34
			Max. My	15	-21188.10	26.89	-1134.18
			Max. Vy	24	-2035.99	261.95	4.34
			Max. Vx	15	-2157.26	-8.39	302.20
		Diagonal	Max Tension	22	2933.04	0.00	0.00
		_	Max. Compression	16	-2924.51	0.00	0.00
			Max. Mx	23	433.98	-6.14	-0.37
			Max. My	17	-2503.18	-4.56	-0.99
			Max. Vy	24	-8.86	-6.10	-0.36
			Max. Vx	17	-0.36	0.00	0.00

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Section Elevation No. ft		Elevation Component ft Type		Gov. Load	Force	Major Axis Moment	Minor Axis Moment
	•	71		Comb.	lb	lb-ft	lb-ft
		Horizontal	Max Tension	15	336.46	0.00	0.00
			Max. Compression	21	-281.30	0.00	0.00
			Max. Mx	15	336.46	16.54	0.00
			Max. My	23	185.62	0.00	-0.00
			Max. Vy	15	-13.23	0.00	0.00
			Max. Vx	23	0.00	0.00	0.00
		Top Girt	Max Tension	25	225.21	0.00	0.00
			Max. Compression	23	-279.45	0.00	0.00
			Max. Mx	14	-26.75	19.09	0.00
			Max. My	22	-29.68	0.00	0.00
			Max. Vy	14	15.27	0.00	0.00
			Max. Vx	22	0.00	0.00	0.00
		Bottom Girt	Max Tension	25	1421.95	0.00	0.00
			Max. Compression	19	-1461.19	0.00	0.00
			Max. Mx	14	32.01	19.09	0.00
			Max. My	22	146.18	0.00	0.00
			Max. Vy	14	15.27	0.00	0.00
		M. I.C.	Max. Vx	22	0.00	0.00	0.00
		Mid Girt	Max Tension	17	216.71	0.00	0.00
			Max. Compression	19	-180.08	0.00	0.00
			Max. Mx	14	17.73	19.09	0.00
			Max. My	22	8.33	0.00	0.00
			Max. Vy	14 22	15.27 0.00	0.00	0.00
T2	120 110	Las	Max. Vx Max Tension	25	48846.44	0.00 335.60	0.00 229.79
12	130 - 110	Leg	Max. Compression	25 15	-58075.87	-38.00	457.90
			Max. Mx	24	-5917.64	-1663.31	17.03
			Max. My	15	-58060.64	172.66	-1754.72
			Max. Vy	24	-3087.35	392.87	4.02
			Max. Vx	15	-3321.66	-38.00	457.90
		Diagonal	Max Tension	22	4764.05	0.00	0.00
		Diagonar	Max. Compression	16	-4696.65	0.00	0.00
			Max. Mx	24	2826.21	-6.88	-0.39
			Max. My	22	-4633.96	-3.40	2.17
			Max. Vy	24	-9.14	-6.88	-0.39
			Max. Vx	22	-0.80	-3.40	2.17
		Horizontal	Max Tension	21	877.31	0.00	0.00
			Max. Compression	15	-727.35	0.00	0.00
			Max. Mx	15	102.28	16.54	0.00
			Max. My	23	491.03	0.00	-0.00
			Max. Vy	15	-13.23	0.00	0.00
			Max. Vx	23	0.00	0.00	0.00
		Top Girt	Max Tension	19	1623.37	0.00	0.00
			Max. Compression	25	-1539.09	0.00	0.00
			Max. Mx	14	-4.14	19.09	0.00
			Max. My	22	-96.15	0.00	0.00
			Max. Vy	14	15.27	0.00	0.00
		D 61	Max. Vx	22	0.00	0.00	0.00
		Bottom Girt	Max Tension	25	2074.27	0.00	0.00
			Max. Compression	19	-2210.41	0.00	0.00
			Max. Mx	14	42.04	19.09	0.00
			Max. My	22	349.66	0.00	0.00
			Max. Vy	14	15.27	0.00	0.00
		Mid Cint	Max. Vx	22	0.00	0.00	0.00
		Mid Girt	Max Tension	21	508.99	0.00	0.00
			Max. Compression	15 14	-334.91 37.00	0.00 19.09	0.00 0.00
			Max. Mx Max. My	14 22	57.16	0.00	0.00
			Max. Vy	14	15.27	0.00	0.00
							0.00
			Max. Vx	22	0.00	0.00	0.00

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Section No.	Elevation ft	*		Gov. Load	Force lb	Major Axis Moment	Minor Ax Moment
				Comb.		lb-ft	lb-ft
			Max. Compression	23	-110147.83	2339.12	-1757.11
			Max. Mx	19	-107084.57	-2543.44	-1455.97
			Max. My	15	-109857.05	-363.11	2912.37
			Max. Vy	19	4521.48	-2543.44	-1455.97
			Max. Vx	15	-5132.45	-363.11	2912.37
		Diagonal	Max Tension	16	5722.00	0.00	0.00
			Max. Compression	22	-5829.32	0.00	0.00
			Max. Mx	15	4893.66	-10.22	-0.00
			Max. My	17	-4890.73	-4.98	-3.72
			Max. Vy	15	11.39	-10.22	-0.00
			Max. Vx	17	-1.36	0.00	0.00
		Horizontal	Max Tension	21	1412.79	0.00	0.00
			Max. Compression	15	-1207.73	0.00	0.00
			Max. Mx	15	-735.85	16.54	0.00
			Max. My	23	785.03	0.00	-0.00
			Max. Vy	15	-13.23	0.00	0.00
			Max. Vx	23	0.00	0.00	0.00
		Top Girt	Max Tension	19	2269.61	0.00	0.00
		Top Gift	Max. Compression	25	-2050.80	0.00	0.00
			-				
			Max. Mx	14	7.65	24.98	0.00
			Max. My	22	-275.30	0.00	0.00
			Max. Vy	14	-19.98	0.00	0.00
			Max. Vx	22	-0.00	0.00	0.00
		Bottom Girt	Max Tension	21	2296.17	0.00	0.00
			Max. Compression	15	-2131.83	0.00	0.00
			Max. Mx	14	113.98	24.98	0.00
			Max. My	22	62.30	0.00	0.00
			Max. Vy	14	-19.98	0.00	0.00
			Max. Vx	22	-0.00	0.00	0.00
		Mid Girt	Max Tension	21	1169.99	0.00	0.00
		iviid Oilt	Max. Compression	15	-937.66	0.00	0.00
			Max. Mx	19	-359.08	24.98	0.00
			Max. My	22	130.97	0.00	0.00
			Max. Vy	19	-19.98	0.00	0.00
			Max. Vx	22	-0.00	0.00	0.00
Т4	00 00	Las					
T4	90 - 80	Leg	Max Tension	25	95713.56	-2678.66	17.29
			Max. Compression	23	-109581.97	4874.28	194.33
			Max. Mx	25	95358.45	-5605.52	192.47
			Max. My	26	-9633.57	-316.80	9496.09
			Max. Vy	17	657.20	-5562.77	162.86
			Max. Vx	26	-1099.85	-316.80	9496.09
		Diagonal	Max Tension	23	6528.01	0.00	0.00
			Max. Compression	26	-7564.84	0.00	0.00
			Max. Mx	25	3999.02	217.35	-28.37
			Max. My	22	-4689.47	-136.38	-78.70
			Max. Vy	25	56.70	217.35	-28.37
			Max. Vx	22	16.19	0.00	0.00
T5	80 - 60	Leg	Max Tension	25	118991.60	-5624.24	164.27
10	00 00	Leg	Max. Compression	23	-143216.53	4886.40	48.39
			Max. Mx	23	-130313.92	5804.44	-7.69
			Max. My	26	-130313.92	-317.06	9496.08
			Max. Vy	17	-448.22	-5562.77	162.84
						-3362.77 -317.06	
		D: 1	Max. Vx	26	902.18		9496.08
		Diagonal	Max Tension	15	6667.55	0.00	0.00
			Max. Compression	15	-6939.37	0.00	0.00
			Max. Mx	23	5877.04	246.26	5.48
			Max. My	21	1807.83	195.89	-32.69
			Max. Vy	23	-66.49	246.26	5.48
			Max. Vx	21	7.12	0.00	0.00
m c	60 - 40	Leg	Max Tension	25	140749.32	-5041.44	65.43
T6	00 - 40	LCS	Max Telision	23	140/47.32	-3041.44	05.45

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Section	Elevation	Component	Condition	Gov.	Force	Major Axis	Minor Axis
No.	ft	Type		Load		Moment	Moment
		• •		Comb.	lb	lb-ft	lb-ft
			Max. Mx	23	-160158.16	5514.66	33.39
			Max. My	24	-13596.13	-127.33	-5265.80
			Max. Vy	19	240.38	5388.67	-78.48
			Max. Vx	26	246.69	-44.80	5215.60
		Diagonal	Max Tension	22	6239.64	0.00	0.00
			Max. Compression	22	-6518.34	0.00	0.00
			Max. Mx	23	3408.63	175.95	-16.39
			Max. My	22	1088.90	133.80	-22.72
			Max. Vy	23	-58.10	168.53	-12.27
			Max. Vx	22	5.02	0.00	0.00
T7	40 - 20	Leg	Max Tension	25	159992.05	-3467.24	67.20
			Max. Compression	23	-205081.07	2735.60	23.17
			Max. Mx	25	159022.01	-7456.31	44.20
			Max. My	24	-20457.41	1155.59	-5150.15
			Max. Vy	17	558.69	-7407.31	37.37
			Max. Vx	26	364.30	1209.25	5087.01
		Diagonal	Max Tension	16	6802.00	0.00	0.00
			Max. Compression	16	-6752.86	0.00	0.00
			Max. Mx	23	3283.56	174.33	-13.93
			Max. My	21	-5827.71	18.20	-20.15
			Max. Vy	23	-62.56	169.04	-14.04
			Max. Vx	21	4.37	0.00	0.00
T8	20 - 0	Leg	Max Tension	25	175796.89	-1168.93	103.39
			Max. Compression	23	-232924.13	-0.00	1.18
			Max. Mx	23	-217637.07	7610.81	89.69
			Max. My	24	-25946.50	3157.33	-8723.31
			Max. Vy	19	837.51	7536.52	-216.59
			Max. Vx	26	993.53	3199.19	8596.75
		Diagonal	Max Tension	21	9066.58	0.00	0.00
		-	Max. Compression	16	-7428.00	0.00	0.00
			Max. Mx	25	1794.88	192.42	14.31
			Max. My	21	-7066.53	67.46	-30.09
			Max. Vy	25	69.52	192.42	14.31
			Max. Vx	21	5.51	0.00	0.00

Maximum Reactions								
	G 11:1		17	T 1 7	T 1.7			
Location	Condition	Gov. Load	Vertical lb	Horizontal, X lb	Horizontal, Z lb			

Location	Conailion	Gov.	verucai	norizoniai, x	norizoniai, Z
		Load	lb	lb	lb
		Comb.			
Leg C	Max. Vert	23	239215.78	17270.69	-10575.32
	Max. H <sub>x</sub>	23	239215.78	17270.69	-10575.32
	Max. H <sub>z</sub>	17	-181118.16	-18624.00	11248.11
	Min. Vert	17	-181118.16	-18624.00	11248.11
	Min. H <sub>x</sub>	17	-181118.16	-18624.00	11248.11
	Min. Hz	23	239215.78	17270.69	-10575.32
Leg B	Max. Vert	19	234345.01	-17607.66	-9822.12
	Max. H <sub>x</sub>	25	-183531.59	18780.94	10498.65
	Max. H <sub>z</sub>	25	-183531.59	18780.94	10498.65
	Min. Vert	25	-183531.59	18780.94	10498.65
	Min. H <sub>x</sub>	19	234345.01	-17607.66	-9822.12
	Min. H <sub>z</sub>	19	234345.01	-17607.66	-9822.12
Leg A	Max. Vert	15	236811.71	-821.17	20182.10
	Max. H <sub>x</sub>	21	-179246.44	727.31	-21366.10
	Max. H <sub>z</sub>	15	236811.71	-821.17	20182.10
	Min. Vert	21	-179246.44	727.31	-21366.10
	Min. H <sub>x</sub>	15	236811.71	-821.17	20182.10

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Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal, X lb	Horizontal, Z lb
	Min. H <sub>z</sub>	21	-179246.44	727.31	-21366.10

# **Tower Mast Reaction Summary**

Load	Vertical	$Shear_x$	$Shear_z$	Overturning	Overturning	Torque
Combination				Moment, $M_x$	Moment, $M_z$	
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Dead Only	23366.04	0.00	0.00	-655.32	8483.71	0.05
Dead+Wind 0 deg - No Ice	23366.04	1083.13	-18109.75	-1511353.63	-70849.14	-10283.84
Dead+Wind 30 deg - No Ice	23366.04	9578.34	-15188.65	-1279314.46	-791542.70	-9795.75
Dead+Wind 60 deg - No Ice	23366.04	15659.63	-8963.78	-753285.10	-1313759.74	-8512.77
Dead+Wind 90 deg - No Ice	23366.04	18058.90	-633.80	-44882.02	-1515100.09	-5044.42
Dead+Wind 120 deg - No Ice	23366.04	16358.98	8116.86	685925.46	-1358233.93	1551.60
Dead+Wind 150 deg - No Ice	23366.04	8653.26	14874.94	1258880.62	-728520.39	7887.60
Dead+Wind 180 deg - No Ice	23366.04	-63.63	17247.53	1460724.82	8082.62	12090.47
Dead+Wind 210 deg - No Ice	23366.04	-8784.08	15166.03	1276197.97	746408.92	12796.54
Dead+Wind 240 deg - No Ice	23366.04	-15704.37	8989.61	744824.29	1318540.43	8730.11
Dead+Wind 270 deg - No Ice	23366.04	-17642.18	-42.74	-9478.57	1499491.25	2042.84
Dead+Wind 300 deg - No Ice	23366.04	-15102.53	-8568.66	-731749.59	1292633.38	-3578.34
Dead+Wind 330 deg - No Ice	23366.04	-8671.42	-14864.46	-1259343.93	747034.57	-7889.01
Dead+Ice+Temp	75020.02	0.00	0.00	-3749.92	40701.42	0.48
Dead+Wind 0 deg+Ice+Temp	75020.02	916.24	-31684.85	-2567999.55	-28097.76	-17980.33
Dead+Wind 30 deg+Ice+Temp	75020.02	16138.08	-26772.71	-2173238.01	-1264834.14	-15994.74
Dead+Wind 60 deg+Ice+Temp	75020.02	27073.25	-15578.04	-1264573.19	-2155646.00	-11370.33
Dead+Wind 90 deg+Ice+Temp	75020.02	31333.89	-544.03	-43438.99	-2501888.62	-3799.67
Dead+Wind 120 deg+Ice+Temp	75020.02	27989.28	15048.94	1218674.04	-2227134.89	6370.32
Dead+Wind 150 deg+Ice+Temp	75020.02	15338.91	26493.90	2147043.25	-1207431.65	14853.63
Dead+Wind 180 deg+Ice+Temp	75020.02	-71.62	30559.97	2476437.41	43259.32	19334.86
Dead+Wind 210 deg+Ice+Temp	75020.02	-15480.07	26753.98	2164216.61	1294609.62	18480.35
Dead+Wind 240 deg+Ice+Temp	75020.02	-27465.88	15804.73	1272545.73	2264222.87	11602.64
Dead+Wind 270 deg+Ice+Temp	75020.02	-30988.66	-16.53	-8341.14	2556222.73	1312.32
Dead+Wind 300 deg+Ice+Temp	75020.02	-26592.80	-15217.95	-1241732.63	2202621.01	-7966.71
Dead+Wind 330 deg+Ice+Temp	75020.02	-15353.99	-26485.19	-2153750.24	1290341.48	-14856.84
Dead+Wind 0 deg - Service	23366.04	609.26	-10186.74	-850438.73	-36132.55	-5785.06
Dead+Wind 30 deg - Service	23366.04	5387.81	-8543.62	-719909.72	-441526.42	-5512.94
Dead+Wind 60 deg - Service	23366.04	8808.54	-5042.12	-424009.80	-735275.14	-4788.57
Dead+Wind 90 deg - Service	23366.04	10158.13	-356.51	-25527.62	-848528.93	-2834.76
Dead+Wind 120 deg - Service	23366.04	9201.93	4565.73	385552.06	-760292.09	873.00
Dead+Wind 150 deg - Service	23366.04	4867.46	8367.16	707842.20	-406076.68	4435.29
Dead+Wind 180 deg - Service	23366.04	-35.79	9701.74	821381.46	8265.16	6800.81
Dead+Wind 210 deg - Service	23366.04	-4941.05	8530.89	717589.24	423581.91	7200.51
Dead+Wind 240 deg - Service	23366.04	-8833.71	5056.66	418689.67	745416.87	4910.93
Dead+Wind 270 deg - Service	23366.04	-9923.73	-24.04	-5616.37	847206.55	1147.65
Dead+Wind 300 deg - Service	23366.04	-8495.17	-4819.87	-411905.00	730843.96	-2012.56
Dead+Wind 330 deg - Service	23366.04	-4877.67	-8361.26	-708684.23	423936.28	-4435.94

# **Solution Summary**

	S	um of Applied Forces			Sum of Reactions		
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	lb	lb	lb	lb	lb	lb	
1	0.00	-23366.04	0.00	-0.00	23366.04	-0.00	0.000%
2	1083.13	-23366.04	-18109.75	-1083.13	23366.04	18109.75	0.000%
3	9578.34	-23366.04	-15188.65	-9578.34	23366.04	15188.65	0.000%

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	Sı	ım of Applied Forces			Sum of Reactions	•	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	lb	lb	lb	lb	lb	lb	
4	15659.63	-23366.04	-8963.78	-15659.63	23366.04	8963.78	0.000%
5	18058.90	-23366.04	-633.80	-18058.90	23366.04	633.80	0.000%
6	16358.98	-23366.04	8116.86	-16358.98	23366.04	-8116.86	0.000%
7	8653.26	-23366.04	14874.94	-8653.26	23366.04	-14874.94	0.000%
8	-63.63	-23366.04	17247.53	63.63	23366.04	-17247.53	0.000%
9	-8784.08	-23366.04	15166.03	8784.08	23366.04	-15166.03	0.000%
10	-15704.37	-23366.04	8989.61	15704.37	23366.04	-8989.61	0.000%
11	-17642.18	-23366.04	-42.74	17642.18	23366.04	42.74	0.000%
12	-15102.53	-23366.04	-8568.66	15102.53	23366.04	8568.66	0.000%
13	-8671.42	-23366.04	-14864.46	8671.42	23366.04	14864.46	0.000%
14	0.00	-75020.02	0.00	-0.00	75020.02	-0.00	0.000%
15	916.24	-75020.02	-31684.90	-916.24	75020.02	31684.85	0.000%
16	16138.09	-75020.02	-26772.72	-16138.08	75020.02	26772.71	0.000%
17	27073.27	-75020.02	-15578.05	-27073.25	75020.02	15578.04	0.000%
18	31333.95	-75020.02	-543.99	-31333.89	75020.02	544.03	0.000%
19	27989.33	-75020.02	15048.96	-27989.28	75020.02	-15048.94	0.000%
20	15338.94	-75020.02	26493.92	-15338.91	75020.02	-26493.90	0.000%
21	-71.63	-75020.02	30559.98	71.62	75020.02	-30559.97	0.000%
22	-15480.08	-75020.02	26753.99	15480.07	75020.02	-26753.98	0.000%
23	-27465.92	-75020.02	15804.75	27465.88	75020.02	-15804.73	0.000%
24	-30988.72	-75020.02	-16.49	30988.66	75020.02	16.53	0.000%
25	-26592.82	-75020.02	-15217.96	26592.80	75020.02	15217.95	0.000%
26	-15353.99	-75020.02	-26485.23	15353.99	75020.02	26485.19	0.000%
27	609.26	-23366.04	-10186.74	-609.26	23366.04	10186.74	0.000%
28	5387.81	-23366.04	-8543.62	-5387.81	23366.04	8543.62	0.000%
29	8808.54	-23366.04	-5042.12	-8808.54	23366.04	5042.12	0.000%
30	10158.13	-23366.04	-356.51	-10158.13	23366.04	356.51	0.000%
31	9201.93	-23366.04	4565.73	-9201.93	23366.04	-4565.73	0.000%
32	4867.46	-23366.04	8367.16	-4867.46	23366.04	-8367.16	0.000%
33	-35.79	-23366.04	9701.74	35.79	23366.04	-9701.74	0.000%
34	-4941.05	-23366.04	8530.89	4941.05	23366.04	-8530.89	0.000%
35	-8833.71	-23366.04	5056.66	8833.71	23366.04	-5056.66	0.000%
36	-9923.73	-23366.04	-24.04	9923.73	23366.04	24.04	0.000%
37	-8495.17	-23366.04	-4819.87	8495.17	23366.04	4819.87	0.000%
38	-4877.67	-23366.04	-8361.26	4877.67	23366.04	8361.26	0.000%

# Non-Linear Convergence Results

Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.0000001	0.00000001
2	Yes	4	0.0000001	0.00000001
3	Yes	4	0.0000001	0.00000001
4	Yes	4	0.0000001	0.00000001
5	Yes	4	0.0000001	0.00000001
6	Yes	4	0.0000001	0.00000001
7	Yes	4	0.0000001	0.00000001
8	Yes	4	0.0000001	0.00000001
9	Yes	4	0.0000001	0.00000001
10	Yes	4	0.0000001	0.00000001
11	Yes	4	0.0000001	0.00000001
12	Yes	4	0.0000001	0.00000001
13	Yes	4	0.0000001	0.00000001
14	Yes	4	0.0000001	0.00000001
15	Yes	4	0.0000001	0.00001065
16	Yes	4	0.0000001	0.00001166

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17     Yes     4     0.00000001     0.00000       18     Yes     4     0.00000001     0.00000       19     Yes     4     0.00000001     0.00000       20     Yes     4     0.00000001     0.00001       21     Yes     4     0.00000001     0.00001       22     Yes     4     0.00000001     0.00001       23     Yes     4     0.00000001     0.00001       24     Yes     4     0.00000001     0.00001       25     Yes     4     0.00000001     0.00001       26     Yes     4     0.00000001     0.00001       27     Yes     4     0.00000001     0.00000       27     Yes     4     0.00000001     0.00000	
19     Yes     4     0.00000001     0.00000       20     Yes     4     0.00000001     0.00000       21     Yes     4     0.00000001     0.00000       22     Yes     4     0.00000001     0.00000       23     Yes     4     0.00000001     0.00001       24     Yes     4     0.00000001     0.00001       25     Yes     4     0.00000001     0.00001       26     Yes     4     0.00000001     0.00001	295
20     Yes     4     0.00000001     0.00000       21     Yes     4     0.00000001     0.00000       22     Yes     4     0.00000001     0.00000       23     Yes     4     0.00000001     0.00000       24     Yes     4     0.00000001     0.00001       25     Yes     4     0.00000001     0.00001       26     Yes     4     0.00000001     0.00001	199
21     Yes     4     0.00000001     0.00000       22     Yes     4     0.00000001     0.00000       23     Yes     4     0.00000001     0.00000       24     Yes     4     0.00000001     0.00000       25     Yes     4     0.00000001     0.00000       26     Yes     4     0.00000001     0.00000	996
22     Yes     4     0.0000001     0.00000       23     Yes     4     0.00000001     0.00000       24     Yes     4     0.00000001     0.00000       25     Yes     4     0.00000001     0.00000       26     Yes     4     0.00000001     0.00000	201
23     Yes     4     0.00000001     0.00001       24     Yes     4     0.00000001     0.00001       25     Yes     4     0.00000001     0.00001       26     Yes     4     0.00000001     0.00001       26     Yes     4     0.00000001     0.00001	287
24     Yes     4     0.0000001     0.0000       25     Yes     4     0.0000001     0.0000       26     Yes     4     0.0000001     0.0000       27     0.0000001     0.00000       28     4     0.00000001     0.00000	163
25         Yes         4         0.0000001         0.0000           26         Yes         4         0.0000001         0.0000	078
26 Yes 4 0.00000001 0.00001	175
	223
27 Yes 4 0.0000001 0.0000	192
	001
28 Yes 4 0.00000001 0.00000	001
29 Yes 4 0.00000001 0.00000	001
30 Yes 4 0.00000001 0.00000	001
31 Yes 4 0.00000001 0.00000	001
32 Yes 4 0.00000001 0.00000	001
33 Yes 4 0.00000001 0.00000	001
34 Yes 4 0.00000001 0.00000	001
35 Yes 4 0.00000001 0.00000	001
36 Yes 4 0.00000001 0.00000	001
37 Yes 4 0.00000001 0.00000	001
38 Yes 4 0.0000001 0.00000	001

Maximum Tower Deflections - Service Wind					
Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	0	٥
T1	150 - 130	7.804	37	0.4758	0.1217
T2	130 - 110	5.771	37	0.4586	0.1176
T3	110 - 90	3.867	36	0.3944	0.0867
T4	90 - 80	2.352	35	0.2863	0.0485
T5	80 - 60	1.796	35	0.2391	0.0365

0.971

0.430

0.111

# **Critical Deflections and Radius of Curvature - Service Wind**

35

35

31

0.1547

0.0994

0.0481

0.0203

0.0109

0.0047

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of Curvature
		Load				ft
ft		Comb.	in	0	0	
149.00	8' Whip	37	7.702	0.4754	0.1218	252282
147.00	APXVSPP18-C w/Mount Pipe	37	7.497	0.4746	0.1220	252282
145.00	1900MHz 4x40W RRH	37	7.293	0.4736	0.1222	252282
136.00	Andrew 12'-6" Universal Sector Frame	37	6.376	0.4670	0.1211	90101
121.00	15' Omni	36	4.885	0.4370	0.1067	20980
117.00	20' Omni	36	4.504	0.4237	0.1001	16153
108.00	10' Dipole	36	3.694	0.3846	0.0826	11045
105.00	8' Whip	36	3.442	0.3690	0.0765	10330
102.00	8' Omni	36	3.200	0.3526	0.0703	9728
98.00	12' Omni	36	2.895	0.3300	0.0623	9027
84.00	3'-6" Dish	35	2.004	0.2574	0.0408	10038
78.00	4' Dish	35	1.698	0.2300	0.0346	12518
74.00	GPS	35	1.513	0.2119	0.0308	13371
72.00	4' Dish	35	1.426	0.2030	0.0291	13783

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Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of Curvature
		Load				ft
ft		Comb.	in	٥	0	
67.00	GPS	35	1.223	0.1815	0.0251	14937
12.00	GPS	31	0.049	0.0285	0.0027	30152

# **Maximum Tower Deflections - Design Wind**

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	in	Comb.	۰	0
T1	150 - 130	21.634	23	1.2627	0.2704
T2	130 - 110	16.253	23	1.2247	0.2643
T3	110 - 90	11.124	23	1.0751	0.2013
T4	90 - 80	6.923	23	0.8080	0.1155
T5	80 - 60	5.333	23	0.6859	0.0892
T6	60 - 40	2.921	23	0.4564	0.0517
T7	40 - 20	1.306	23	0.2974	0.0286
T8	20 - 0	0.338	23	0.1454	0.0125

# **Critical Deflections and Radius of Curvature - Design Wind**

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of Curvature
		Load				ft
ft		Comb.	in	0	0	
149.00	8' Whip	23	21.364	1.2619	0.2707	128867
147.00	APXVSPP18-C w/Mount Pipe	23	20.823	1.2601	0.2714	128867
145.00	1900MHz 4x40W RRH	23	20.283	1.2581	0.2719	128867
136.00	Andrew 12'-6" Universal Sector Frame	23	17.859	1.2435	0.2708	46024
121.00	15' Omni	23	13.878	1.1756	0.2428	9209
117.00	20' Omni	23	12.851	1.1446	0.2293	6990
108.00	10' Dipole	23	10.651	1.0515	0.1925	4659
105.00	8' Whip	23	9.960	1.0135	0.1789	4294
102.00	8' Omni	23	9.295	0.9732	0.1652	3989
98.00	12' Omni	23	8.450	0.9176	0.1472	3644
84.00	3'-6" Dish	23	5.931	0.7336	0.0984	3912
78.00	4' Dish	23	5.050	0.6617	0.0848	4796
74.00	GPS	23	4.513	0.6133	0.0765	5063
72.00	4' Dish	23	4.258	0.5892	0.0725	5179
67.00	GPS	23	3.663	0.5307	0.0631	5492
12.00	GPS	23	0.152	0.0862	0.0073	9993

# **Bolt Design Data**

Section No.	Elevation ft	Component Type	Bolt Grade	Bolt Size	Number Of Bolts	Maximum Load per Bolt lb	Allowable Load lb	Ratio Load Allowable	Allowable Ratio	Criteria
T1	150	Leg	A325N	0.6250	5	3061.82	12885.40	0.238	1.333	Bolt DS
T2	130	Leg	A325N	0.7500	5	9769.29	18555.00	0.527	1.333	Bolt DS

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Section No.	Elevation	Component Type	Bolt Grade	Bolt Size	Number Of	Maximum Load per	Allowable Load	Ratio Load	Allowable Ratio	Criteria
	ft			in	Bolts	BoÎt lb	lb	Allowable		
Т3	110	Leg	A325N	1.0000	6	16097.70	34517.60	0.466	1.333	Bolt Tension
T4	90	Leg	A325N	1.0000	6	15952.30	34556.90	0.462	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6528.01	11554.70	0.565	1.333	Member Block Shear
T5	80	Leg	A325N	1.0000	6	19831.90	34557.40	0.574	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6667.55	11554.70	0.577	1.333	Member Block Shear
T6	60	Leg	A325N	1.0000	6	23458.20	34557.40	0.679	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6239.64	11554.70	0.540	1.333	Member Block Shear
T7	40	Leg	A325N	1.0000	6	26665.30	34557.00	0.772	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	6802.00	11554.70	0.589	1.333	Member Block Shear
T8	20	Leg	A687	1.0000	6	29299.50	38877.20	0.754	1.333	Bolt Tension
		Diagonal	A325N	1.2500	1	9066.58	11554.70	0.785	1.333	Member Block Shear

# Compression Checks

		Leg I	Design	Data (	Comp	ressio	n)			
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. P <sub>a</sub>	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1 3/4	20.00	2.33	64.0 K=1.00	22.023	2.4053	-21203.30	52971.60	0.400
T2	130 - 110	2	20.00	2.33	56.0 K=1.00	23.389	3.1416	-58075.90	73477.20	0.790
Т3	110 - 90	2 1/4	20.00	2.33	49.8 K=1.00	24.385	3.9761	-110148.00	96957.60	1.136
T4	90 - 80	Pirod 216415	10.02	10.02	37.5 K=1.00	26.178	5.3014	-109582.00	138780.00	0.790
T5	80 - 60	Pirod 216413	20.03	10.02	37.5 K=1.00	26.178	5.3014	-143217.00	138780.00	1.032
Т6	60 - 40	Pirod 195557	20.03	10.02	32.1 K=1.00	26.884	7.2158	-174993.00	193990.00	0.902
T7	40 - 20	Pirod 195557	20.03	10.02	32.1 K=1.00	26.884	7.2158	-205081.00	193990.00	1.057
Т8	20 - 0	Pirod 195557	20.03	10.02	32.1 K=1.00	26.884	7.2158	-232924.00	193990.00	1.201

# Truss-Leg Diagonal Data

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Section No.	Elevation	Diagonal Size	$L_d$	Kl/r	$F_a$	A	Actual V	Allow. $V_a$	Stress Ratio
	ft		ft		ksi	$in^2$	lb	lb	
T4	90 - 80	0.5	1.46	119.3	10.377	0.1963	1103.12	2292.15	0.481
T5	80 - 60	0.5	1.46	119.3	10.377	0.1963	910.97	2292.15	0.397
T6	60 - 40	0.5	1.45	118.3	10.520	0.1963	273.84	2323.87	0.118
T7	40 - 20	0.5	1.45	118.3	10.520	0.1963	579.71	2323.87	0.249
Т8	20 - 0	0.5	1.45	118.3	10.520	0.1963	1058.24	2323.87	0.455

		Diagon	al Desig	ın Da	ta (Cor	npress	sion)			
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	7/8	5.52	2.68	110.2 K=0.75	12.298	0.6013	-2924.51	7394.87	0.395
T2	130 - 110	7/8	5.52	2.67	109.7 K=0.75	12.404	0.6013	-4696.65	7458.76	0.630
Т3	110 - 90	1	5.52	2.66	95.6 K=0.75	15.710	0.7854	-5829.32	12338.40	0.472
T4	90 - 80	L3x3x5/16	11.42	4.99	106.3 K=1.04	12.166	1.7800	-7564.84	21655.10	0.349
T5	80 - 60	L3x3x5/16	12.50	5.64	116.1 K=1.01	10.829	1.7800	-6939.37	19274.90	0.360
Т6	60 - 40	L3x3x5/16	13.80	6.34	129.1 K=1.00	8.958	1.7800	-6494.39	15944.60	0.407
T7	40 - 20	L3x3x5/16	14.50	6.74	137.2 K=1.00	7.928	1.7800	-6752.86	14112.20	0.479
Т8	20 - 0	L3x3x5/16	16.01	7.51	152.9 K=1.00	6.387	1.7800	-7428.00	11368.50	0.653

	Horizontal Design Data (Compression)										
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. $P_a$	Ratio P	
	ft		ft	ft		ksi	$in^2$	lb	$l\ddot{b}$	$P_a$	
T1	150 - 130	7/8	5.00	4.85	186.4 K=0.70	4.298	0.6013	-281.30	2584.43	0.109	
T2	130 - 110	7/8	5.00	4.83	185.6 K=0.70	4.335	0.6013	-727.35	2606.76	0.279	
Т3	110 - 90	7/8	5.00	4.81	184.8 K=0.70	4.373	0.6013	-1207.73	2629.38	0.459	

# **Top Girt Design Data (Compression)**

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Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	$Allow.$ $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	163.1 K=0.70	5.614	0.7854	-279.45	4408.93	0.063
T2	130 - 110	1	5.00	4.83	162.4 K=0.70	5.662	0.7854	-1539.09	4447.02	0.346
Т3	110 - 90	1 1/4	5.00	4.81	129.4 K=0.70	8.924	1.2272	-2050.80	10951.20	0.187

		Bottom	Girt Des	ign D	ata (Co	ompre	ssion)			
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	$Allow.$ $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	163.1 K=0.70	5.614	0.7854	-1461.19	4408.93	0.331
T2	130 - 110	1	5.00	4.83	162.4 K=0.70	5.662	0.7854	-2210.41	4447.02	0.497
Т3	110 - 90	1 1/4	5.00	4.81	129.4 K=0.70	8.924	1.2272	-2131.83	10951.20	0.195

	Mid Girt Design Data (Compression)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. P <sub>a</sub>	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	163.1 K=0.70	5.614	0.7854	-180.08	4408.93	0.041
T2	130 - 110	1	5.00	4.83	162.4 K=0.70	5.662	0.7854	-334.91	4447.02	0.075
Т3	110 - 90	1 1/4	5.00	4.81	129.4 K=0.70	8.924	1.2272	-937.66	10951.20	0.086

# Tension Checks

		Le	g Desig	ın Dat	a (Ter	nsion)				
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. P <sub>a</sub>	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	$lb^{"}$	$P_a$
T1	150 - 130	1 3/4	20.00	2.33	64.0	32.500	1.2339	15309.10	40100.60	0.382
T2	130 - 110	2	20.00	2.33	56.0	32.500	1.5625	48846.40	50780.20	0.962
T3	110 - 90	2 1/4	20.00	2.33	49.8	30.000	3.9761	96586.10	119282.00	0.810

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Section	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual	Allow.	Ratio
No.								P	$P_a$	P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
										~
T4	90 - 80	Pirod 216415	10.02	10.02	37.5	30.000	5.3014	95713.60	159043.00	0.602
										~
T5	80 - 60	Pirod 216413	20.03	10.02	37.5	30.000	5.3014	118992.00	159043.00	0.748
										1
T6	60 - 40	Pirod 195557	20.03	10.02	32.1	30.000	7.2158	140749.00	216475.00	0.650
										~
T7	40 - 20	Pirod 195557	20.03	10.02	32.1	30.000	7.2158	159992.00	216475.00	0.739
										1
T8	20 - 0	Pirod 195557	20.03	10.02	32.1	30.000	7.2158	175797.00	216475.00	0.812
										1

	Truss-Leg Diagonal Data								
Section No.	Elevation	Diagonal Size	$L_d$	Kl/r	$F_a$	A	Actual V	$Allow.$ $V_a$	Stress Ratio
	ft		ft		ksi	$in^2$	lb	lb	
T4	90 - 80	0.5	1.46	119.3	10.377	0.1963	1103.12	2292.15	0.481
T5	80 - 60	0.5	1.46	119.3	10.377	0.1963	910.97	2292.15	0.397
T6	60 - 40	0.5	1.45	118.3	10.520	0.1963	273.84	2323.87	0.118
T7	40 - 20	0.5	1.45	118.3	10.520	0.1963	579.71	2323.87	0.249
Т8	20 - 0	0.5	1.45	118.3	10.520	0.1963	1058.24	2323.87	0.455

	Diagonal Design Data (Tension)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	$Allow.$ $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	7/8	5.52	2.68	146.9	30.000	0.6013	2933.04	18039.60	0.163
T2	130 - 110	7/8	5.52	2.67	146.3	30.000	0.6013	4764.05	18039.60	0.264
Т3	110 - 90	1	5.52	2.66	127.5	30.000	0.7854	5722.00	23561.90	0.243
T4	90 - 80	L3x3x5/16	11.42	4.99	67.6	29.000	1.0127	6528.01	29369.30	0.222
T5	80 - 60	L3x3x5/16	11.93	5.39	72.8	29.000	1.0127	6667.55	29369.30	0.227
Т6	60 - 40	L3x3x5/16	13.13	6.03	81.0	29.000	1.0127	6239.64	29369.30	0.212
T7	40 - 20	L3x3x5/16	15.24	7.09	94.9	29.000	1.0127	6802.00	29369.30	0.232
Т8	20 - 0	L3x3x5/16	16.80	7.89	105.3	29.000	1.0127	9066.58	29369.30	0.309

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	Horizontal Design Data (Tension)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	7/8	5.00	4.85	266.3	30.000	0.6013	336.46	18039.60	0.019
T2	130 - 110	7/8	5.00	4.83	265.1	30.000	0.6013	877.31	18039.60	0.049
Т3	110 - 90	7/8	5.00	4.81	264.0	30.000	0.6013	1412.79	18039.60	0.078

	Top Girt Design Data (Tension)									
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	233.0	30.000	0.7854	225.21	23561.90	0.010
T2	130 - 110	1	5.00	4.83	232.0	30.000	0.7854	1623.37	23561.90	0.069
Т3	110 - 90	1 1/4	5.00	4.81	184.8	30.000	1.2272	2269.61	36815.50	0.062

	Bottom Girt Design Data (Tension)									
Section Elevation Size $L$ $L_u$ $Kl/r$ $F_a$ $A$ Actual Allow. Ratio $No$ . $P$ $P_a$ $P$										
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	233.0	30.000	0.7854	1421.95	23561.90	0.060
T2	130 - 110	1	5.00	4.83	232.0	30.000	0.7854	2074.27	23561.90	0.088
Т3	110 - 90	1 1/4	5.00	4.81	184.8	30.000	1.2272	2296.17	36815.50	0.062

Mid Girt Design Data (Tension)										
Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	Allow. P <sub>a</sub>	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
T1	150 - 130	1	5.00	4.85	233.0	30.000	0.7854	216.71	23561.90	0.009
T2	130 - 110	1	5.00	4.83	232.0	30.000	0.7854	508.99	23561.90	0.022

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Section No.	Elevation	Size	L	$L_u$	Kl/r	$F_a$	A	Actual P	$Allow.$ $P_a$	Ratio P
	ft		ft	ft		ksi	$in^2$	lb	lb	$P_a$
Т3	110 - 90	1 1/4	5.00	4.81	184.8	30.000	1.2272	1169.99	36815.50	0.032

# **Section Capacity Table**

Section	Elevation	Component	Size	Critical	P	$SF*P_{allow}$	% Capacity	Pass
No.	ft	Type		Element	lb	lb		Fail
T1	150 - 130	Leg	1 3/4	3	-21203.30	70611.14	30.0	Pass
		Diagonal	7/8	17	-2924.51	9857.36	29.7	Pass
		Horizontal	7/8	60	-281.30	3445.04	8.2	Pass
		Top Girt	1	5	-279.45	5877.10	4.8	Pass
		Bottom Girt	1	9	-1461.19	5877.10	24.9	Pass
		Mid Girt	1	12	-180.08	5877.10	3.1	Pass
T2	130 - 110	Leg	2	68	48846.40	67690.00	72.2	Pass
		Diagonal	7/8	83	-4696.65	9942.53	47.2	Pass
		Horizontal	7/8	126	-727.35	3474.81	20.9	Pass
		Top Girt	1	72	-1539.09	5927.88	26.0	Pass
		Bottom Girt	1	75	-2210.41	5927.88	37.3	Pass
		Mid Girt	1	76	-334.91	5927.88	5.6	Pass
T3	110 - 90	Leg	2 1/4	133	-110148.00	129244.48	85.2	Pass
		Diagonal	1	150	-5829.32	16447.09	35.4	Pass
		Horizontal	7/8	192	-1207.73	3504.96	34.5	Pass
		Top Girt	1 1/4	138	-2050.80	14597.95	14.0	Pass
		Bottom Girt	1 1/4	139	-2131.83	14597.95	14.6	Pass
		Mid Girt	1 1/4	142	-937.66	14597.95	6.4	Pass
T4	90 - 80	Leg	Pirod 216415	199	-109582.00	184993.73	59.2	Pass
		Diagonal	L3x3x5/16	206	-7564.84	28866.25	26.2	Pass
T5	80 - 60	Leg	Pirod 216413	208	-143217.00	184993.73	77.4	Pass
		Diagonal	L3x3x5/16	215	-6939.37	25693.44	27.0	Pass
T6	60 - 40	Leg	Pirod 195557	223	-174993.00	258588.66	67.7	Pass
		Diagonal	L3x3x5/16	231	-6494.39	21254.15	30.6	Pass
T7	40 - 20	Leg	Pirod 195557	238	-205081.00	258588.66	79.3	Pass
		Diagonal	L3x3x5/16	251	-6752.86	18811.56	35.9	Pass
T8	20 - 0	Leg	Pirod 195557	253	-232924.00	258588.66	90.1	Pass
		Diagonal	L3x3x5/16	266	-7428.00	15154.21	49.0	Pass
		_					Summary	
						Leg (T8)	90.1	Pass
						Diagonal (T8)	49.0	Pass
						Horizontal	34.5	Pass
						(T3)	2.50	-
						Top Girt (T2)	26.0	Pass
						Bottom Girt (T2)	37.3	Pass
						Mid Girt (T3)		Pass
						Bolt Checks	58.9	Pass
						RATING =	90.1	Pass

# APPENDIX C MOUNT CALCULATIONS



# WINDSPEED BY LOCATION

# **Search Results**

**Latitude:** 41.8031 **Longitude:** -72.8013

ASCE 7-10 Wind Speeds (3-sec peak gust MPH\*):

Risk Category I: 110 Risk Category II: 120 Risk Category III-IV: 130

MRI\*\* 10 Year: 76 MRI\*\* 25 Year: 86 MRI\*\* 50 Year: 92 MRI\*\* 100 Year: 98

**ASCE 7-05**: 98 **ASCE 7-93**: 79

\*MPH(Miles per hour)

\*\*MRI Mean Recurrence Interval (years)

Users should consult with local building officials
to determine if there are community-specific wind speed
requirements that govern.



### WIND SPEED WEB SITE DISCLAIMER:

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1120 Dallas Street Sauk City, WI 53583

Office: (608) 643-4100

Job: 22984

Project: Avon Mountain (CT03XC053-A)

By: JMO

7/14/2014 Date:

### **Topographic Effects TIA-222**

2.6.6.2 Topographic Categories

The topographic category for a structure shall be assessed as being one of the following:

- 1. Category 1: No abrupt changes in general topography, e.g. flat or rolling terrain, no wind speed-up consideration shall be required.
- 2. Category 2: Structures located at or near the crest of an escarpment. Wind speed-up shall be considered to occur in all directions. Structures located vertically on the lower half of an escarpment or horizontally beyond 8 times the height of the escarpment from its crest, shall be permitted to be considered as Topographic Category 1.
- 3. Category 3: Structures located in the upper half of a hill. Wind speed-up shall be considered to occur in all directions. Structures located vertically on the lower half of a hill shall be permitted to be considered as Topographic Category 1.
- 4. Category 4: Structures located in the upper half of a ridge. Wind speed-up shall be considered to occur in all directions. Structures located vertically on the lower half of a ridge shall be permitted to be considered as Topographic Category 1.

**Topographic Category** 4 H = 575 ft height of hill **Exposure Category** В z = 147 ft height of antennas above ground level Ke = 0.90 Kt = 0.72 f = 1.50 Kh = 1.47 2.08 Kzt =



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### Wind Load on Antennas TIA-222

### 2.6.9.6 Velocity Pressure

 $q_z = 0.00256 K_z K_{zt} K_d V^2 I$ 

Occupancy: II Classification of Structures (Table 2-1)

Exposure: B Exposure Category

V: 98 mph Basic Wind Speed (Annex B)

z: 147 ft Height above ground level to the center of the antenna

I: 1.00 Importance Factor (Table 2-3)

K<sub>z</sub>: 1.10 Velocity Pressure Coefficient (2.6.5.2)

K<sub>zt</sub>: 2.08 Topographic Factor (2.6.6.4)

K<sub>d</sub>: 0.95 Wind Direction Probability Factor (Table 2-2)

 $q_z = 53.6 \text{ psf}$ 

G<sub>h</sub>: 1.00 Appurtenances and their Connections

### **Mount & Antenna Wind Loads**

Appurtenance	Height	Depth	h/D	Shape	$C_a$	$A_f$	$F = q_z G_h C_a A_a$	
Pipe2STD x 10.5 ft	126.0 in	2.4 in	52.9	Round	1.200	2.08 sf	133.9 lb	 12.8 plf
Pipe1-1/2STD x 7 ft	84.0 in	1.9 in	44.2	Round	1.200	1.11 sf	71.3 lb	10.2 plf
Pipe2STD x 3 ft	36.0 in	2.4 in	15.1	Round	0.981	0.60 sf	31.3 lb	10.4 plf
Pipe1/2STD x 2.5 ft	30.0 in	0.8 in	35.7	Round	1.200	0.18 sf	11.3 lb	4.5 plf
APXV9TM14-ALU-120	56.3 in	6.3 in	8.9	Flat	1.465	2.46 sf	193.3 lb	
TD-RRH8x20	26.1 in	6.7 in	3.9	Flat	1.262	1.21 sf	82.1 lb	
APXVSPP18-C-A20	72.0 in	7.0 in	10.3	Flat	1.509	3.50 sf	283.5 lb	



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By: JMO

Date:

7/14/2014

### Wind Load on Antennas TIA-222

### 2.6.9.6 Velocity Pressure

 $q_z = 0.00256 K_z K_{zt} K_d V^2 I$ 

Occupancy: II Classification of Structures (Table 2-1)

Exposure: B Exposure Category

V: 98 mph Basic Wind Speed (Annex B)

z: 147 ft Height above ground level to the center of the antenna

I: 1.00 Importance Factor (Table 2-3)

K<sub>z</sub>: 1.10 Velocity Pressure Coefficient (2.6.5.2)

K<sub>zt</sub>: 2.08 Topographic Factor (2.6.6.4)

K<sub>d</sub>: 0.95 Wind Direction Probability Factor (Table 2-2)

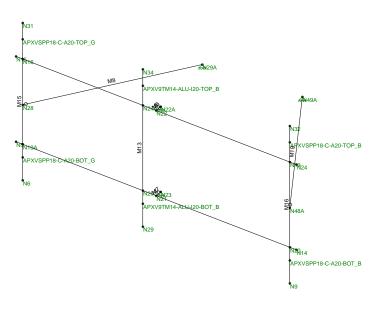
 $q_z = 53.6$  psf

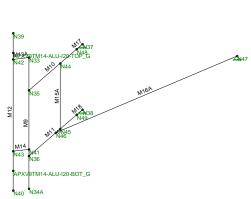
G<sub>h</sub>: 1.00 Appurtenances and their Connections

### **Mount & Antenna Wind Loads**

Appurtenance	Height	Width	h/D	Shape	$C_a$	$A_f$	$F = q_z G_h C_a A_a$	
Pipe2STD x 10.5 ft	126.0 in	2.4 in	52.9	Round	1.200	2.08 sf	133.9 lb	12.8 plf
Pipe1-1/2STD x 7 ft	84.0 in	1.9 in	44.2	Round	1.200	1.11 sf	71.3 lb	10.2 plf
Pipe2STD x 3 ft	36.0 in	2.4 in	15.1	Round	0.981	0.60 sf	31.3 lb	10.4 plf
Pipe1/2STD x 2.5 ft	30.0 in	0.8 in	35.7	Round	1.200	0.18 sf	11.3 lb	4.5 plf
APXV9TM14-ALU-120	56.3 in	12.6 in	4.5	Flat	1.287	4.93 sf	339.9 lb	
TD-RRH8x20	26.1 in	18.6 in	1.4	Flat	1.200	3.37 sf	216.8 lb	
APXVSPP18-C-A20	72.0 in	11.9 in	6.1	Flat	1.358	5.95 sf	432.8 lb	



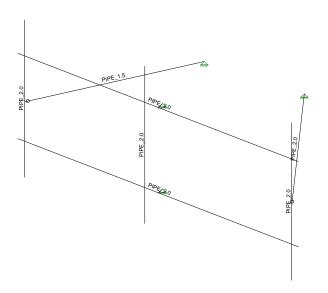


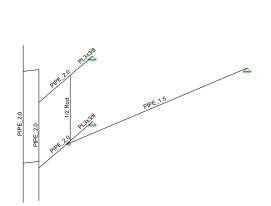


Envelope Only Solution

Ramaker & Associates		SK - 1
JMO	Avon Mountain (CT03XC053-A)	July 14, 2014 at 11:28 AM
22984		22984 Mount.r3d







Envelope Only Solution

Ramaker & Associates		SK - 2
JMO	Avon Mountain (CT03XC053-A)	July 14, 2014 at 11:29 AM
22984		22984 Mount.r3d

: Ramaker & Associates: JMO: 22984

Model Name : Avon Mountain (CT03XC053-A)

July 14, 2014

Checked By:\_\_

### **Hot Rolled Steel Properties**

	Label	E [ksi]	G [ksi]	Nu	Therm (\1E	.Density[k/ft	Yield[ksi]	Ry	Fu[ksi]	Rt
1	A36 Gr.36	29000	11154	.3	.65	.49	36	1.5	58	1.2
2	A572 Gr.50	29000	11154	.3	.65	.49	50	1.1	65	1.1
3	A992	29000	11154	.3	.65	.49	50	1.1	65	1.1
4	A500 Gr.42	29000	11154	.3	.65	.49	42	1.4	58	1.3
5	A500 Gr.46	29000	11154	.3	.65	.49	46	1.4	58	1.3
6	A53 Gr. B	29000	11154	.3	.65	.49	35	1.5	60	1.2

### Hot Rolled Steel Section Sets

	Label	Shape	Type	Design List	Material	Design R	A [in2]	lyy [in4]	Izz [in4]	J [in4]
1	pipe 2.0	PIPE 2.0	Beam	Pipe	A53 Gr. B	Typical	1.02	.627	.627	1.25
2	pipe 1.5	PIPE 1.5	Beam	Pipe	A53 Gr. B	Typical	.749	.293	.293	.586
3	solid rod	1/2 Rod	Beam	BÁR	A36 Gr.36	Typical	.196	.003	.003	.006
4	plate	PL3x3/8	Beam	RECT	A36 Gr.36	Typical	1.125	.013	.844	.049

### Member Primary Data

	Label	I Joint	J Joint	K Joint	Rotate(deg)	Section/Shape	Type	Design List	Material	Design Rules
1	M2	N5	N14		, 3,	pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
2	M5	N15	N24		180	pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
3	M13	N34	N29			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
4	M15	N31	N6			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
5	M16	N32	N9			pipe 2.0	Beam	Pipe .	A53 Gr. B	Typical
6	M6	N22	N22A			RIGID	None	None	RIGID	Typical
7	M7	N21	N23			RIGID	None	None	RIGID	Typical
8	M8	N28	N29A			pipe 1.5	Beam	Pipe	A53 Gr. B	Typical
9	M9	N33	N34A			pipe 2.0	Beam	Pipe .	A53 Gr. B	Typical
10	M10	N35	N48			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
11	M11	N36	N49			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
12	M12	N39	N40			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical
13	M13A	N42	N33			RIGID	None	None	RIGID	Typical
14	M14	N43	N41			RIGID	None	None	RIGID	Typical
15	M15A	N44	N45			solid rod	Beam	BAR	A36 Gr.36	Typical
16	M16A	N46	N47			pipe 1.5	Beam	Pipe	A53 Gr. B	Typical
17	M17	N48	N37		90	plate	Beam	RECT	A36 Gr.36	Typical
18	M18	N49	N38		90	plate	Beam	RECT	A36 Gr.36	Typical
19	M19	N48A	N49A			pipe 2.0	Beam	Pipe	A53 Gr. B	Typical

### Joint Coordinates and Temperatures

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap
1	N5	3.455	4.67	08	0	· ·
2	N6	3.705	3.295	08	0	
3	N9	13.705	3.295	08	0	
4	N14	13.955	4.67	08	0	
5	N15	3.455	7.92	08	0	
6	N16	3.705	7.92	08	0	
7	N19	13.705	7.92	08	0	
8	N22	8.705	7.92	08	0	
9	N24	13.955	7.92	08	0	
10	APXV9TM14-ALU-I20-BOT_B	8.205	4.17	08	0	
11	APXVSPP18-C-A20-BOT_B	13.705	4.17	08	0	
12	APXV9TM14-ALU-I20-TOP_B	8.205	8.67	08	0	
13	APXVSPP18-C-A20-TOP_B	13.705	8.67	08	0	



: Ramaker & Associates : JMO : 22984

Model Name : Avon Mountain (CT03XC053-A) July 14, 2014

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### Joint Coordinates and Temperatures (Continued)

	Label	X [ft]	Y [ft]	Z [ft]	Temp [F]	Detach From Diap
14	N31	3.705	9.295	08	0	
15	N32	13.705	9.295	08	0	
16	N34	8.205	9.295	08	0	
17	N29	8.205	3.295	08	0	
18	N19A	3.705	4.67	08	0	
19	N20	13.705	4.67	08	0	
20	N21	8.705	4.67	08	0	
21	N22A	8.705	7.92	33	0	
22	N23	8.705	4.67	33	0	
23	N24A	8.205	7.92	08	0	
24	N25	8.205	4.67	08	0	
25	APXVSPP18-C-A20-BOT_G	3.705	4.17	08	0	
26	APXVSPP18-C-A20-TOP_G	3.705	8.67	08	0	
27	N28	3.705	6.17	08	0	
28	N29A	7.146459	6.17	-4.994912	0	
29	APXV9TM14-ALU-I20-BOT_G	17.851447	4.92	0.273553	0	
30	APXV9TM14-ALU-I20-TOP_G	17.851447	9.42	0.273553	0	
31	N33	18.205	9.17	08	0	
32	N34A	18.205	4.17	08	0	
33	N35	18.205	7.92	08	0	
34	N36	18.205	5.42	08	0	
35	N37	18.205	7.92	-3.08	0	
36	N38	18.205	5.42	-3.08	0	
37	N39	17.851447	10.17	0.273553	0	
38	N40	17.851447	4.17	0.273553	0	
39	N41	18.205	5.67	08	0	
40	N42	17.851447	9.17	0.273553	0	
41	N43	17.851447	5.67	0.273553	0	
42	N44	18.205	7.92	-1.83	0	
43	N45	18.205	5.42	-1.83	0	
44	N46	18.205	5.42	-1.58	0	
45	N47	20.599141	5.42	-8.157848	0	
46	N48	18.205	7.92	-2.75	0	
47	N49	18.205	5.42	-2.75	0	
48	N48A	13.705	6.17	08	0	
49	N49A	10.705	6.17	-5.276153	0	

### **Joint Boundary Conditions**

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]	Footing
1	APXV9TM14-ALU							
2	APXV9TM14-ALU							
3	N31							
4	N16							
5	N6							
6	N34							
7	N22							
8	N24							
9	N14							
10	N15							
11	N5							
12	N19							
13	N9							
14	N32							
15	APXVSPP18-C-A2							
16	APXVSPP18-C-A2							



Model Name

: Ramaker & Associates : JMO

: 22984 : Avon Mountain (CT03XC053-A) July 14, 2014

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### Joint Boundary Conditions (Continued)

	Joint Label	X [k/in]	Y [k/in]	Z [k/in]	X Rot.[k-ft/rad]	Y Rot.[k-ft/rad]	Z Rot.[k-ft/rad]	Footing
17	N29					-		
18	N19A							
19	N20							
20	N21							
21	N22A	Reaction	Reaction	Reaction				
22	N23	Reaction	Reaction	Reaction				
23	N24A							
24	N25							
25	APXVSPP18-C-A2							
26	APXVSPP18-C-A2							
27	N28							
28	N29A	Reaction	Reaction	Reaction				
29	APXV9TM14-ALU							
30	APXV9TM14-ALU							
31	N33							
32	N34A							
33	N35							
34	N36							
35	N37	Reaction	Reaction	Reaction				
36	N38	Reaction	Reaction	Reaction				
37	N39							
38	N40							
39	N41							
40	N42							
41	N43							
42	N44							
43	N45							
44	N46							
45	N47	Reaction	Reaction	Reaction				
46	N48A							
47	N49A	Reaction	Reaction	Reaction				

### Joint Loads and Enforced Displacements (BLC 1 : DL)

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*
1	APXV9TM14-ALU-I20-TOP B	L	Υ	-27.5
2	APXV9TM14-ALU-I20-BOT B	L	Υ	-27.5
3	APXVSPP18-C-A20-TOP B	L	Υ	-28.5
4	APXVSPP18-C-A20-BOT B	L	Υ	-28.5
5	APXVSPP18-C-A20-BOT G	L	Υ	-28.5
6	APXVSPP18-C-A20-TOP G	L	Υ	-28.5
7	APXV9TM14-ALU-I20-BOT G	L	Y	-27.5
8	APXV9TM14-ALU-I20-TOP G	L	Υ	-27.5

### Joint Loads and Enforced Displacements (BLC 2 : WLz)

	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*
1	APXV9TM14-ALU-I20-TOP B	L	Z	-170
2	APXV9TM14-ALU-I20-BOT B	L	Z	-170
3	APXVSPP18-C-A20-TOP B	L	Z	-216.4
4	APXVSPP18-C-A20-BOT B	L	Z	-216.4
5	APXVSPP18-C-A20-BOT G	L	Z	-216.4
6	APXVSPP18-C-A20-TOP G	L	Z	-216.4
7	APXV9TM14-ALU-I20-BOT G	L	Z	-96.7
8	APXV9TM14-ALU-I20-TOP G	L	Z	-96.7



Company : Ramak Designer : JMO Job Number : 22984

: Ramaker & Associates : JMO

Model Name : Avon Mountain (CT03XC053-A)

July 14, 2014

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### Joint Loads and Enforced Displacements (BLC 3 : WLx)

_	Joint Label	L,D,M	Direction	Magnitude[(lb,lb-ft), (in,rad), (lb*
1	APXV9TM14-ALU-I20-TOP B	L	X	-96.7
2	APXV9TM14-ALU-I20-BOT B	L	X	-96.7
3	APXVSPP18-C-A20-TOP B	L	X	-141.7
4	APXVSPP18-C-A20-BOT B	L	X	-141.7
5	APXVSPP18-C-A20-BOT G	L	X	-141.7
6	APXVSPP18-C-A20-TOP G	L	X	-141.7
7	APXV9TM14-ALU-I20-BOT G	L	X	-170
8	APXV9TM14-ALU-I20-TOP G	L	X	-170

### Member Distributed Loads (BLC 2 : WLz)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M2	Ζ	-12.8	-12.8	0	0
2	M5	Z	-12.8	-12.8	0	0
3	M8	PZ	-10.2	-10.2	0	0
4	M16A	PZ	-10.2	-10.2	0	0
5	M9	Ζ	-12.8	-12.8	0	0
6	M12	Ζ	-12.8	-12.8	0	0
7	M19	PZ	-12.8	-12.8	0	0

### Member Distributed Loads (BLC 3 : WLx)

	Member Label	Direction	Start Magnitude[lb/ft,F]	End Magnitude[lb/ft,F]	Start Location[ft,%]	End Location[ft,%]
1	M13	X	-12.8	-12.8	0	0
2	M15	X	-12.8	-12.8	0	0
3	M16	X	-12.8	-12.8	0	0
4	M8	PX	-10.2	-10.2	0	0
5	M16A	PX	-10.2	-10.2	0	0
6	M10	X	-10.4	-10.4	0	0
7	M11	X	-10.4	-10.4	0	0
8	M15A	X	-4.5	-4.5	0	0
9	M19	PX	-12.8	-12.8	0	0

### Member Area Loads

Joint A	Joint B	Joint C	Joint D	Direction	Distribution	Magnitude[psf]
		No D	ata to Print			

### **Basic Load Cases**

		BLC Description	Category	X Gravity	Y Gravity	Z Gravity	Joint	Point	Distributed	Area(Me	Surface(P
-	1	DL	DĽ		-1		8			,	,
2	2	WLz	WLZ				8		7		
- (	3	WLx	WLX				8		9		
4	4	LL1	LL					2			
	5	LL2	None					1			

### **Load Combinations**

	Description	Sol	<b>PDelta</b>	SR	.BLC	Fact	BLC	Fact.	BLC	Fact.	BLC	Fact								
1	1.4DL	Yes	Υ		DL	1.4														
2	1.2DL+1.6WLz	Yes	Υ		DL	1.2	WLZ	1.6												
3	1.2DL-1.6WLz	Yes	Υ		DL	1.2	WLZ	-1.6												
4	1.2DL+1.6WLx	Yes	Υ		DL	1.2	W	1.6												
5	1.2DL-1.6WLx	Yes	Υ		DL	1.2	W	-1.6												



Model Name

: Ramaker & Associates : JMO : 22984

: Avon Mountain (CT03XC053-A)

July 14, 2014

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### **Load Combinations (Continued)**

	Description	SolI	PDelta	SRBLC	Fact.	.BLC	Fact.	BLC	Fact.	.BLC	Fact	BLC	Fact	BLC	Fact	BLC	Fact	BLC	Fact
6	1.2DL+1.6(0.75WLz+0.75WLx)	Yes	Υ	DL	1.2	WLZ	1.2	W	1.2										
7	1.2DL+1.6(0.75WLz-0.75WLx)	Yes	Υ	DL	1.2	WLZ	1.2	W	-1.2										
8	1.2DL-1.6(0.75WLz-0.75WLx)	Yes	Υ	DL	1.2	WLZ	-1.2	W	1.2										
9	1.2DL-1.6(0.75WLz+0.75WLx)	Yes	Υ	DL	1.2	WLZ	-1.2	W	-1.2										
10	1.2DL+1.5LLend	Yes	Υ	DL	1.2	LL	1.5												
11	1.2DL+1.5LLmid	Yes	Υ	DL	1.2	5	1.5												
12	1.2DL+1.5LL+10%1.6WLz	Yes	Υ	DL	1.2	LL	1.5	WLZ	.16										
13	1.2DL+1.5LL-10%1.6WLz	Yes	Υ	DL	1.2	LL	1.5	WLZ	16										
14	1.2DL+1.5LL+10%1.6WLx	Yes	Υ	DL	1.2	LL	1.5	W	.16										
15	1.2DL+1.5LL-10%1.6WLx	Yes	Υ	DL	1.2	LL	1.5	W	16										
16	1.2DL+1.5LL+10%1.6(0.75WLz+	Yes	Υ	DL	1.2	LL	1.5	WLZ	.12	W	.12								
17	1.2DL+1.5LL+10%1.6(0.75WLz	Yes	Υ	DL	1.2	LL		WLZ											
18	1.2DL+1.5LL-10%1.6(0.75WLz-0.	.Yes	Υ	DL	1.2	LL	1.5	WLZ	12	W	.12								
19	1.2DL+1.5LL-10%1.6(0.75WLz+	Yes	Υ	DL	1.2	LL	1.5	WLZ	12	W	12								
20	1.2DL+1.5LL+10%1.6WLz	Yes	Υ	DL	1.2	5	1.5	WLZ	.16										
21	1.2DL+1.5LL-10%1.6WLz	Yes	Υ	DL	1.2	5		WLZ											
22	1.2DL+1.5LL+10%1.6WLx	Yes	Υ	DL	1.2	5		W											
23	1.2DL+1.5LL-10%1.6WLx	Yes	Υ	DL	1.2	5		W											
24	1.2DL+1.5LL+10%1.6(0.75WLz+	Yes	Υ	DL	1.2	5		WLZ			.12								
25	1.2DL+1.5LL+10%1.6(0.75WLz		Υ	DL	1.2	5	1.5	WLZ	.12	W	12								
26	1.2DL+1.5LL-10%1.6(0.75WLz-0.		Υ	DL	1.2	5		WLZ											
27	1.2DL+1.5LL-10%1.6(0.75WLz+	Yes	Υ	DL	1.2	5	1.5	WLZ	12	W	12								
28	DL		Υ	DL	1														
29	WLz		Υ	WLZ	1														
30	WLx		Υ	W	1														

### Envelope Joint Reactions

	Joint		X [lb]	LC	Y [lb]	LC	Z [lb]	LC	MX [lb-ft]	LC	MY [lb-ft]	LC	MZ [lb-ft]	LC
1	N22A	max	913.667	4	738.791	2	541.46	2	Ô	1	0	1	Ò	1
2		min	-895.955	5	-350.815	3	-599.769	3	0	1	0	1	0	1
3	N23	max	819.894	4	735.173	3	339.154	2	0	1	0	1	0	1
4		min	-837.713	5	-349.36	2	-277.56	3	0	1	0	1	0	1
5	N29A	max	559.167	3	10.704	1	825.714	2	0	1	0	1	0	1
6		min	-559.259	2	8.079	2	-827.703	3	0	1	0	1	0	1
7	N37	max	445.878	4	275.774	18	182.042	2	0	1	0	1	0	1
8		min	-424.663	5	66.653	7	-653.996	13	0	1	0	1	0	1
9	N38	max	1081.621	5	254.544	15	3929.272	4	0	1	0	1	0	1
10		min	-1111.101	4	62.047	8	-3587.655	5	0	1	0	1	0	1
11	N47	max	1423.454	4	13.962	4	3747.477	5	0	1	0	1	0	1
12		min	-1415.189	5	7.459	5	-3756.572	4	0	1	0	1	0	1
13	N49A	max	427.248	2	14.577	1	770.317	2	0	1	0	1	0	1
14		min	-427.53	3	11.066	2	-771.613	3	0	1	0	1	0	1
15	Totals:	max	2529.82	4	1319.077	16	3050.438	2						
16		min	-2529.82	5	569.075	5	-3050.438	3						

### Envelope AISC 13th(360-05): LRFD Steel Code Checks

	Member	Shape	Code Ch	. Loc[ft]	LC	Shear	Loc[ft]	Dir	LC	phi*Pncphi*Pnt [.	phi*Mn	phi*Mn	Cb Eqn
1	M2	PIPE 2.0	.365	10.172	13	.152	5.25		3	8922.084 32130	1871.625	1871.625	1.8 H1-1b
2	M5	PIPE 2.0	.349	10.172	16	.149	5.25		2	8922.084 32130	1871.625	1871.625	1.8 H1-1b
3	M13	PIPE 2.0	.205	1.375	3	.057	1.375		19	20866.7 32130	1871.625	1871.625	1H1-1b
4	M15	PIPE 2.0	.444	3.125	2	.090	3.125		3	20866.7 32130	1871.625	1871.625	1H1-1b
5	M16	PIPE 2.0	.401	3.125	2	.087	3.125		3	20866.7 32130	1871.625	1871.625	1H1-1b
6	M8	PIPE 1.5	.083	3	6	.005	6		9	11973.623593.5	1105.125	1105.125	1H1-1b
7	M9	PIPE 2.0	.721	3.75	4	.833	3.542		4	29810.2 32130	1871.625	1871.625	1 H3-6



Company Designer Job Number Model Name

: Ramaker & Associates : JMO : 22984

: Avon Mountain (CT03XC053-A)

July 14, 2014

Checked By:\_

### Envelope AISC 13th(360-05): LRFD Steel Code Checks (Continued)

	Member	Shape	Code Ch	. Loc[ft]	LC	Shear	Loc[ft]	Dir	LC	phi*Pncphi*Pnt [phi*Mn phi*Mn Cb Eqn
8	M10	PIPE 2.0	.636	0	4	.064	1.724		4	29497.8 32130   1871.625   1871.625   1H1-1b
9	M11	PIPE 2.0	.946	1.502	4	.134	1.502		5	29497.8 32130   1871.625   1871.625   1H1-1b
10	M12	PIPE 2.0	.241	4.5	4	.266	1		4	20866.7 32130  1871.625  1871.625  1 H3-6
11	M15A	1/2 Rod	.755	0	4	.314	0		4	1822.745 6361.74 53.015 53.015 2H1-1b
12	M16A	PIPE 1.5	.498	3.573	5	.007	7		5	9372.519 23593.5 1105.125 1105.125 1H1-1a
13	M17	PL3x3/8	.321	0	14	.030	0	У	4	33970.5 36450 284.766 2278.125 1H1-1b
14	M18	PL3x3/8	.339	0	14	.076	0	У	4	33970.5 36450 284.766 2278.125 1H1-1b
15	M19	PIPE_2.0	.055	3	7	.005	0	_	5	20866.7 32130   1871.625   1871.625   1 H1-1b



2.5 EQUIPMENT DEPLOYMENT PROJECT:

SITE NAME: AVON MOUNTAIN

SITE CASCADE: CTO3XCO53-A

SITE ADDRESS: 81 MONTEVIDEO ROAD AVON, CT 06001

SITE TYPE: 150'-0" SELF SUPPORT TOWER

SHT NO:

SP-2

SP-3

A-2

A-3

A-4

A-5

A-6

A-7

A-8

E-1

F-2

E-3

## **48 SPRUCE STREET** OAKLAND, NJ 07346

REV:

Α

Α

ENGINEER:

JRS

JRS

JRS

JRS

IRS

SHEET INDEX

SHEET TITLE:

BUILDING ELEVATION # ANTENNA DETAILS

TITLE SHEET

SPRINT SPECIFICATIONS

SPRINT SPECIFICATIONS

SPRINT SPECIFICATIONS

FIBER PLUMBING DIAGRAM

ANTENNA # HYBRID CABLE DETAILS

EQUIPMENT UTILITY & GROUNDING PLAN

DC POWER DETAILS & PANEL SCHEDULES

CABLE COLOR CODING

EQUIPMENT DETAILS

GROUNDING DETAILS

EQUIPMENT PLAN

RF DATA SHEET

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RAMAKER

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Transcend Wir**el**ess

hereby certify that this plan, specification, or report was prepare by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of <u>Connecticut</u>.



FINAL DATE 07/14/2014

> AVON MOUNTAIN CTO3XCO53-A

81 MONTEVIDEO ROAD AVON. CT 06001 HARTFORD COUNTY

TITLE SHEET

SCALE: NONE

22984

### SITE INFORMATION

### PROPERTY OWNER:

MONTE LLC PO BOX 320623 HARTFORD, CT 06132-0623

### SITE ADDRESS:

81 MONTEVIDEO ROAD AVON, CT 0600 I

### GEOGRAPHIC COORDINATES:

LATITUDE: 41° 48' 11.0298" N (41.80306388) LONGITUDE: 72° 48' 4.6398" W (-72.80128888)

### ZONING JURISDICTION:

TOWN OF AVON

# ZONING DISTRICT:

RESIDENTIAL

### POWER COMPANY:

NORTHEAST UTILITIES PH.: (800) 286-2000

### AAV PROVIDER:

PH.: (210) 821-4105

### SPRINT CONSTRUCTION MANAGER:

NAME: MIKE DELIA PHONE: (781) 316-6348 E-MAIL: michael.delia@Sprint.com

### EQUIPMENT SUPPLIER:

ALCATEL-LUCENT 600-700 MOUNTAIN AVENUE PH.: (908) 508-8080

### PLANS PREPARED BY:

RAMAKER \$ ASSOCIATES, INC CONTACT: KEITH BOHNSACK, PROJECT MANAGER PH.: (608) 643-4100 EMAIL: kbohnsack@ramaker.com



LOCATION MAP

### PROJECT DESCRIPTION

- INSTALL NEW 2.5 EQUIPMENT IN EXISTING BTS CABINET \*(1) RECTIFIER SHELF AND (3) RECTIFIERS
  \*(1) BASE BAND UNIT
- INSTALL NEW BATTERY STRING(S) IN EXISTING BATTERY CABINET
- INSTALL (3) PANEL ANTENNAS
- INSTALL (3) RRH'S ON TOWER
- INSTALL (I) HYBRID CABLE AND (2) SECTOR JUMPERS
- INSTALL (27) ANTENNA / RRH JUMPERS

# APPLICABLE CODES

- \* ALL WORK SHALL BE PERFORMED AND MATERIALS INSTALLED IN ACCORDANCE WITH THE FOLLOWING CODES AS ADOPTED BY THE LOCAL GOVERNING AUTHORITIES. NOTHING IN THESE PLANS IS TO BE CONSTRUED TO PERMIT WORK NOT CONFORMING TO THESE CODES.
- I. INTERNATIONAL BUILDING CODE
- 2. ANSI/TIA-222 STRUCTURAL STANDARD FOR ANTENNA STRUCTURES
- 3. NEPA 780 LIGHTNING PROTECTION CODE
- 4. NATIONAL ELECTRIC CODE



### SECTION OI 100 - SCOPE OF WORK

THESE STANDARD CONSTRUCTION SPECIFICATIONS IN CONJUNCTION WITH THE CONSTRUCTION DRAWINGS AND ASSOCIATED OUTLINE SPECIFICATIONS AND THE SITE SPECIFIC WORK ORDER, DESCRIBE THE WORK TO BE PERFORMED BY THIS CONSTRUCTION CONTRACTOR (SUPPLIER).

- A. THE REQUIREMENTS OF EACH SECTION OF THIS SPECIFICATION APPLY TO ALL SECTIONS, INDIVIDUALLY
- B. RELATED DOCUMENTS: THE CONTRACTOR SHALL COMPLY WITH THE MOST CURRENT VERSION OF THE FOLLOWING SUPPLEMENTAL REQUIREMENTS FOR INSTALLATION AND TESTING
- I . EN-2012-001: (FIBER OPTIC, DC CABLE, AND DC CIRCUIT BREAKER TAGGING STANDARDS) 2.TS-0200 (TRANSMISSION ANTENNA LINE ACCEPTANCE STANDARDS)
- 3.EL-0568: (FIBER TESTING POLICY)
- 4.NP-3 | 2-20 |: (EXTERIOR GROUNDING SYSTEM TESTING)
- 5.NP-760-500: ETHERNET, MICROWAVE, TESTING AND ACCEPTANCE

SHOULD CONFLICTS OCCUR BETWEEN THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AND THE CONSTRUCTION DRAWINGS, INFORMATION ON THE CONSTRUCTION DRAWINGS SHALL TAKE PRECEDENCE. NOTIFY SPRINT CONSTRUCTION MANAGER IF THIS OCCURS.

NATIONALLY RECOGNIZED CODES AND STANDARDS:
THE WORK SHALL COMPLY WITH APPLICABLE NATIONAL AND LOCAL CODES AND STANDARDS, LATEST

- EDITION, AND PORTIONS THEREOF, INCLUDED BUT NOT LIMITED TO THE FOLLOWING:
- A. GR-63-CORE NEBS REQUIREMENTS: PHYSICAL PROTECTION
  B. GR-78-CORE GENERIC REQUIREMENTS FOR THE PHYSICAL DESIGN AND MANUFACTURE OF TELECOMMUNICATIONS EQUIPMENT.
- C. GR-1089 CORE, ELECTROMAGNETIC COMPATIBILITY AND ELECTRICAL SAFETY -GENERIC CRITERIA FOR
- NETWORK TELECOMMUNICATIONS EQUIPMENT.
  D. NATIONAL FIRE PROTECTION ASSOCIATION CODES AND STANDARDS (NFPA) INCLUDING NFPA 70
- (NATIONAL ELECTRICAL CODE "NEC") AND NFPA IOI (LIFE SAFETY CODE). E. AMERICAN SOCIETY FOR TESTING OF MATERIALS (ASTM)
- F. INSTITUTE OF ELECTRONIC AND ELECTRICAL ENGINEERS (IEEE)
  G. AMERICAN CONCRETE INSTITUTE (ACI)

- AMERICAN WIRE PRODUCERS ASSOCIATION (AWPA)
- CONCRETE REINFORCING STEEL INSTITUTE (CRSI) AMERICAN ASSOCIATION OF STATE HIGHWAY AND TRANSPORTATION OFFICIALS (AASHTO)
- K. PORTLAND CEMENT ASSOCIATION (PCA)
- NATIONAL CONCRETE MASONRY ASSOCIATION (NCMA)
- M. BRICK INDUSTRY ASSOCIATION (BIA)
- I. AMERICAN WELDING SOCIETY (AWS)
- O. NATIONAL ROOFING CONTRACTORS ASSOCIATION (NRCA)
- SHEET METAL AND AIR CONDITIONING CONTRACTORS' NATIONAL ASSOCIATION (SMACNA)
- Q DOOR AND HARDWARE INSTITUTE (DHI)
- R. OCCUPATIONAL SAFETY AND HEALTH ACT (OSHA)
- S. APPLICABLE BUILDING CODES INCLUDING UNIFORM BUILDING CODE, SOUTHERN BUILDING CODE, BOCA, AND THE INTERNATIONAL BUILDING CODE.

- DEFINITIONS:

  A. WORK: THE SUM OF TASKS AND RESPONSIBILITIES IDENTIFIED IN THE CONTRACT DOCUMENTS.

  B. COMPANY: "SPRINT"; SPRINT NEXTEL CORPORATION AND ITS OPERATING ENTITIES.
- C. ENGINEER: SYNONYMOUS WITH ARCHITECT & ENGINEER AND "A&E". THE DESIGN PROFESSIONAL HAVING PROFESSIONAL RESPONSIBILITY FOR DESIGN OF THE PROJECT.
- D. CONTRACTOR: CONSTRUCTION CONTRACTOR, SUPPLIER, CONSTRUCTION VENDOR; INDIVIDUAL OR ENTITY WHO AFTER EXECUTION OF A CONTRACT IS BOUND TO ACCOMPLISH THE WORK.
- . THIRD PARTY VENDOR OR AGENCY: A VENDOR OR AGENCY ENGAGED SEPARATELY BY THE COMPANY, A&E, OR CONTRACTOR TO PROVIDE MATERIALS OR TO ACCOMPLISH SPECIFIC TASKS RELATED TO BUT NOT INCLUDED IN THE WORK
- F. CONSTRUCTION MANAGER ALL PROJECTS RELATED COMMUNICATION TO FLOW THROUGH SPRINT REPRESENTATIVE IN CHARGE OF PROJECT.

CONTRACTOR SHALL BE RESPONSIBLE FOR FAMILIARIZING HIMSELF WITH ALL CONTRACT DOCUMENTS. FIELD CONDITIONS AND DIMENSIONS PRIOR TO PROCEEDING WITH CONSTRUCTION. ANY DISCREPANCIES SHALL BE BROUGHT TO THE ATTENTION OF THE SPRINT CONSTRUCTION MANAGER PRIOR TO THE COMMENCEMENT OF WORK. NO COMPENSATION WILL BE AWARDED BASED ON CLAIM OF LACK OF KNOWLEDGE OR FIELD CONDITIONS.

COMMUNICATION BETWEEN SPRINT AND THE CONTRACTOR SHALL FLOW THROUGH THE SINGLE SPRINT CONSTRUCTION MANAGER APPOINTED TO MANAGE THE PROJECT FOR SPRINT.

THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE RESPONSIBLE FOR CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES, AND PROCEDURES IN ACCORDANCE WITH THE CONTRACT DOCUMENTS. THE CONTRACTOR SHALL EMPLOY A COMPETENT SUPERINTENDENT WHO SHALL BE IN ATTENDANCE AT THE SITE AT ALL TIMES DURING PERFORMANCE OF THE WORK

THE CONSTRUCTION CONTRACTOR SHALL MAINTAIN A FULL SET OF THE CONSTRUCTION DRAWINGS FOR WIRELESS SITES AND THE STANDARD CONSTRUCTION SPECIFICATIONS FOR WIRELESS SITES AT THE JOBSITE FROM MOBILIZATION THROUGH CONSTRUCTION COMPLETION.

- THE JOBSITE DRAWINGS SHALL BE CLEARLY MARKED DAILY IN RED PENCIL WITH ANY CHANGES IN CONSTRUCTION OVER WHAT IS DEPICTED IN THE DOCUMENTS. AT CONSTRUCTION COMPLETION, THIS JOBSITE MARKUP SET SHALL BE DELIVERED TO THE COMPANY OR COMPANY'S DESIGNATED REPRESENTATIVE TO BE FORWARDED TO THE COMPANY'S A\$E VENDOR FOR PRODUCTION OF "AS-BUILT" DRAWINGS
- B. DIMENSIONS SHOWN ARE TO FINISH SURFACES UNLESS NOTED OTHERWISE. SPACING BETWEEN EQUIPMENT IS THE REQUIRED CLEARANCE. SHOULD THERE BE ANY QUESTIONS REGARDING THE CONTRACT DOCUMENTS, EXISTING CONDITIONS AND/OR DESIGN INTENT, THE CONTRACTOR SHALL BE RESPONSIBLE FOR OBTAINING A CLARIFICATION FROM THE SPRINT CONSTRUCTION MANAGER PRIOR TO PROCEEDING WITH THE WORK

THE CONTRACTOR SHALL CONFINE ALL CONSTRUCTION AND RELATED OPERATIONS INCLUDING STAGING AND STORAGE OF MATERIALS AND EQUIPMENT, PARKING, TEMPORARY FACILITIES, AND WASTE STORAGE TO THE LEASE PARCEL UNLESS OTHERWISE PERMITTED BY THE CONTRACT DOCUMENTS.

WHERE NECESSARY TO CUT EXISTING PIPES, ELECTRICAL WIRES, CONDUITS, CABLES, ETC., OF UTILITY SERVICES, OR OF FIRE PROTECTION OR COMMUNICATIONS SYSTEMS, THEY SHALL BE CUT AND CAPPED AT SUITABLE PLACES OR WHERE SHOWN. ALL SUCH ACTIONS SHALL BE COORDINATED WITH THE UTILITY

WHEN REQUIRED THAT A PERMIT OR CONNECTION FEE BE PAID TO A PUBLIC LITILITY PROVIDER FOR NEW SERVICE TO THE CONSTRUCTION PROJECT, PAYMENT OF SUCH FEE SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR.

CONTRACTOR:
CONTRACTOR SHALL TAKE ALL MEASURES AND PROVIDE ALL MATERIAL NECESSARY FOR PROTECTING EXISTING EQUIPMENT AND PROPERTY.

JSE OF ELECTRONIC PROJECT MANAGEMENT SYSTEMS: CONTRACTOR WILL UTILIZE ITS BEST EFFORTS TO WORK WITH SPRINT ELECTRONIC PROJECT MANAGEMENT SYSTEMS, CONTRACTOR UNDERSTANDS THAT SUFFICIENT INTERNET ACCESS, EQUIVALENT TO "BROADBAND" OR BETTER, IS REQUIRED TO TIMELY AND EFFECTIVELY UTILIZE SPRINT DATA AND DOCUMENT MANAGEMENT YSTEMS AND AGREES TO MAINTAIN APPROPRIATE CONNECTIONS FOR CONTRACTOR'S STAFF AND OFFICES THAT ARE COMPATIBLE WITH SPRINT DATA AND DOCUMENT MANAGEMENT SYSTEMS

### TEMPORARY UTILITIES AND FACILITIES

THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL TEMPORARY UTILITIES AND FACILITIES NECESSARY EXCEPT AS OTHERWISE INDICATED IN THE CONSTRUCTION DOCUMENTS, TEMPORARY UTILITIES AND FACILITIES INCLUDE POTABLE WATER, HEAT, HVAC, ELECTRICITY, SANITARY FACILITIES, WASTE DISPOSAL FACILITIES, AND TELEPHONE/COMMUNICATION SERVICES. PROVIDE TEMPORARY UTILITIES AND FACILITIES IN ACCORDANCE WITH OSHA AND THE AUTHORITY HAVING JURISDICTION. CONTRACTOR MAY UTILIZE THE COMPANY ELECTRICAL SERVICE IN THE COMPLETION OF THE WORK WHEN IT BECOMES AVAILABLE. USE OF THE LESSOR'S OR SITE OWNER'S UTILITIES OR FACILITIES IS EXPRESSLY FORBIDDEN EXCEPT AS OTHERWISE ALLOWED IN THE CONTRACT DOCUMENTS.

THE CONTRACTOR SHALL PROVIDE ACCESS TO THE JOB SITE FOR AUTHORIZED COMPANY PERSONNEL AND AUTHORIZED REPRESENTATIVES OF THE ARCHITECT/ENGINEER DURING ALL PHASES OF THE WORK.

VERIFY DIMENSIONS INDICATED ON DRAWINGS WITH FIELD DIMENSIONS BEFORE FABRICATION OR ORDERING OF MATERIALS. DO NOT SCALE DRAWINGS.

NOTIFY THE SPRINT CONSTRUCTION MANAGER OF EXISTING CONDITIONS DIFFERING FROM THOSE INDICATED ON THE DRAWINGS. DO NOT REMOVE OR ALTER STRUCTURAL COMPONENTS WITHOUT PRIOR WRITTEN APPROVAL FROM THE ARCHITECT AND ENGINEER.

### SECTION O I 200 - COMPANY FURNISHED MATERIAL AND EQUIPMENT

FURNISHED MATERIALS: COMPANY FURNISHED MATERIALS AND EQUIPMENT TO BE INSTALLED BY THE CONTRACTOR (OFIC) IS IDENTIFIED ON THE RF DATA SHEET IN THE CONSTRUCTION DOCUMENTS.

RECEIPT OF MATERIAL AND EQUIPMENT:

A. THE CONTRACTOR IS RESPONSIBLE FOR SPRINT PROVIDED MATERIAL AND EQUIPMENT AND UPON RECEIPT

- L. ACCEPT DELIVERIES AS SHIPPED AND TAKE RECEIPT.
- 2. VERIFY COMPLETENESS AND CONDITION OF ALL DELIVERIES
- 3. TAKE RESPONSIBILITY FOR EQUIPMENT AND PROVIDE INSURANCE PROTECTION AS REQUIRED IN AGREEMENT
- B.RECORD ANY DEFECTS OR DAMAGES AND WITHIN TWENTY-FOUR HOURS AFTER RECEIPT, REPORT TO SPRINT OR ITS DESIGNATED PROJECT REPRESENTATIVE OF SUCH.
- C PROVIDE SECURE AND NECESSARY WEATHER PROTECTED WAREHOUSING
- D.COORDINATE SAFE AND SECURE TRANSPORTATION OF MATERIAL AND EQUIPMENT, DELIVERING AND OFF-LOADING FROM CONTRACTOR'S WAREHOUSE TO SITE.

A.COMPLETE SHIPPING AND RECEIPT DOCUMENTATION IN ACCORDANCE WITH COMPANY PRACTICE. B.IF APPLICABLE, COMPLETE LOST/STOLEN/DAMAGED DOCUMENTATION REPORT AS NECESSARY IN ACCORDANCE WITH COMPANY PRACTICE, AND AS DIRECTED BY COMPANY.

### SECTION 01 300 - CELL SITE CONSTRUCTION

A NO WORK SHALL COMMENCE PRIOR TO COMPANYS ISSUANCE OF THE WORK ORDER.
B.UPON RECEIVING NOTICE TO PROCEED, CONTRACTOR SHALL FULLY PERFORM ALL WORK NECESSARY TO PROVIDE SPRINT WITH AN OPERATIONAL WIRELESS FACILITY.

- GENERAL REQUIREMENTS FOR CONSTRUCTION:

  A.CONTRACTOR SHALL KEEP THE SITE FREE FROM ACCUMULATING WASTE MATERIAL, DEBRIS, AND TRASH. AT THE COMPLETION OF THE WORK, CONTRACTOR SHALL REMOVE FROM THE SITE ALL REMAINING RUBBISH, IMPLEMENTS, TEMPORARY FACILITIES, AND SURPLUS MATERIALS.
- B.EQUIPMENT ROOMS SHALL AT ALL TIMES BE MAINTAINED "BROOM CLEAN" AND CLEAR OF DEBRIS. C.CONTRACTOR SHALL TAKE ALL REASONABLE PRECAUTIONS TO DISCOVER AND LOCATE ANY HAZARDOUS
- I IN THE EVENT CONTRACTOR ENCOUNTERS ANY HAZARDOUS CONDITION WHICH HAS NOT BEEN ABATED OR OTHERWISE MITIGATED, CONTRACTOR AND ALL OTHER PERSONS SHALL IMMEDIATELY STOP WORK IN THE AFFECTED AREA AND NOTIFY COMPANY IN WRITING. THE WORK IN THE AFFECTED AREA SHALL NOT BE RESUMED EXCEPT BY WRITTEN NOTIFICATION BY COMPANY.

  2. CONTRACTOR AGREES TO USE CARE WHILE ON THE SITE AND SHALL NOT TAKE ANY ACTION THAT WILL
- OR MAY RESULT IN OR CAUSE THE HAZARDOUS CONDITION TO BE FURTHER RELEASED IN THE ENVIRONMENT OR TO FURTHER EXPOSE INDIVIDUALS TO THE HAZARD D.CONTRACTOR'S ACTIVITIES SHALL BE RESTRICTED TO THE PROJECT LIMITS. SHOULD AREAS OUTSIDE THE
- PROJECT LIMITS BE AFFECTED BY CONTRACTOR'S ACTIVITIES, CONTRACTOR SHALL IMMEDIATELY RETURN THEM TO ORIGINAL CONDITION

- A THE ACTIVITIES DESCRIBED IN THIS PARAGRAPH REPRESENT MINIMUM ACTIONS AND PROCESSES REQUIRED TO SUCCESSFULLY COMPLETE THE WORK. CONTRACTOR SHALL TAKE ALL ACTIONS AS NECESSARY TO SUCCESSFULLY COMPLETE THE CONSTRUCTION OF A FULLY FUNCTIONING WIRELESS FACILITY AT THE SITE IN ACCORDANCE WITH COMPANY PROCESSES.
- B. SUBMIT SPECIFIC DOCUMENTATION AS INDICATED HEREIN, AND OBTAIN REQUIRED APPROVALS WHILE THE WORK IS BEING PERFORMED. C.MANAGE AND CONDUCT ALL FIELD CONSTRUCTION SERVICE RELATED ACTIVITIES
- D.PROVIDE CONSTRUCTION ACTIVITIES TO THE EXTENT REQUIRED BY THE CONTRACT DOCUMENTS,
- INCLUDING BUT NOT LIMITED TO THE FOLLOWING:

  I. PERFORM ANY REQUIRED SITE ENVIRONMENTAL MITIGATION.
- 2. PREPARE GROUND SITES; PROVIDE DE-GRUBBING; AND ROUGH AND FINAL GRADING, AND COMPOUND SURFACE TREATMENTS. 3.MANAGE AND CONDUCT ALL ACTIVITIES FOR INSTALLATION OF UTILITIES INCLUDING ELECTRICAL AND BACKHAUL (FIBER, COPPER, OR MICROWAVE).
- 4.INSTALL UNDERGROUND FACILITIES INCLUDING UNDERGROUND POWER AND COMMUNICATIONS CONDUITS. AND UNDERGROUND GROUNDING SYSTEM.
- 5.INSTALL ABOVE GROUND GROUNDING SYSTEMS, CONDUIT AND BOXES 6.PROVIDE NEW HVAC INSTALLATIONS AND MODIFICATIONS.
- 7.INSTALL "H-FRAMES", CABINETS AND PADS AND PLATFORMS AS INDICATED. 8, INSTALL ROADS, ACCESS WAYS, CURBS AND DRAINS AS INDICATED.
- 9.ACCOMPLISH REQUIRED MODIFICATION OF EXISTING FACILITIES.

- LO PROVIDE ANTENNA SUPPORT STRUCTURE FOUNDATIONS
- PROVIDE SLABS AND EQUIPMENT PLATFORMS.
- INSTALL COMPOUND FENCING, SIGHT SHIELDING, LANDSCAPING AND ACCESS BARRIERS. PERFORM INSPECTION AND MATERIAL TESTING AS REQUIRED HEREINAFTER.
- CONDUCT SITE RESISTANCE TO EARTH TESTING AS REQUIRED HEREINAFTER INSTALL FIXED GENERATOR SETS AND OTHER STANDBY POWER SOLUTIONS.
- INSTALL TOWERS, ANTENNA SUPPORT STRUCTURES AND PLATFORMS ON EXISTING TOWERS AS REQUIRED.
- INSTALL CELL SITE RADIOS, MICROWAVE, GPS, COAXIAL MAINLINE, ANTENNAS, CROSS BAND COUPLERS, TOWER TOP AMPLIFIERS, LOW NOISE AMPLIFIERS AND RELATED EQUIPMENT.
- CONDUCT ALL REQUIRED TESTS AND INSPECTIONS
- PERFORM, DOCUMENT, AND CLOSE OUT ALL JURISDICTIONAL PERMITTING REQUIREMENTS AND ANY CONSTRUCTION CONTROL DOCUMENTS THAT MAY BE REQUIRED BY GOVERNMENT AGENCIES AND LANDLORDS.
- 20. PERFORM ALL ADDITIONAL WORK AS IDENTIFIED IN SCOPE OF SERVICES ATTACHED TO THE SUPPLIER AGREEMENT FOR THIS PROJECT. THIS WORK MAY INCLUDE COMMISSIONING INTEGRATION, SPECIAL WAREHOUSING, REVERSE LOGISTICS ACTIVITIES, ETC. PERFORM COMMISSIONING AND INTEGRATION ACTIVITIES PER APPLICABLE MOPS

- DELIVERABLES:
  A. THE CONTRACTOR SHALL PROVIDE ALL REQUIRED TEST REPORTS AND DOCUMENTATION INCLUDED BUT
- PRODUCT SPECIFICATIONS FOR MATERIALS OR SPECIAL CONSTRUCTION IF REQUESTED BY SPRINT
- 2. ACTUALIZE ALL CONSTRUCTION RELATED MILESTONES IN SITERRA AND COMPLETE ALL ON-LINE FORMS AND COMPLETE DOCUMENT UP-LOADS. UPLOAD ALL REQUIRED CLOSEOUT DOCUMENTS AND FINAL
- 3. SCANABLE BARCODE PHOTOGRAPHS OF TOWER TOP AND INACCESSIBLE SERIALIZED EQUIPMENT LEFT ON SITE INSIDE BASE OF MAIN RF CABINET IN A PROTECTIVE POUCH.
- 4 ALL REQUIRED TEST REPORTS
- 5. REQUIRED CLOSEOUT DOCUMENTATION INCLUDING BUT NOT LIMITED TO:
- a. ALL JURISDICTIONAL PERMITTING AND OCCUPANCY INFORMATION b. PDF SCAN OF REDLINES PRODUCED IN THE FIELD
- c. ELECTRONIC AS-BUILT DRAWINGS IN AUTOCAD AND PDF FORMATS
- d.LIEN WAIVERS
- E. FINAL PAYMENT APPLICATION f. REQUIRED FINAL CONSTRUCTION PHOTOS
- CONSTRUCTION AND COMMISSIONING CHECKLIST COMPLETE WITH NO DEFICIENT ITEMS h. LISTS OF SUBCONTRACTORS
- B.PROVIDE ADDITIONAL DOCUMENTATION INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING. DOCUMENTATION SHALL BE FORWARDED IN ORIGINAL FORMAT AND/OR UPLOADED INTO SMS.
  - ALL CORRESPONDENCE AND PRELIMINARY CONSTRUCTION REPORTS.
- 2. PROJECT PROGRESS REPORTS
- 3. PRE-CONSTRUCTION MEETING NOTES

# SECTION O I 400 - TESTS, INSPECTIONS, SUBMITTALS, AND PROJECT

A. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ALL CONSTRUCTION TESTS, INSPECTIONS AND PROJECT

- B. CONTRACTOR SHALL ACCOMPLISH TESTING INCLUDING BUT NOT LIMITED TO THE FOLLOWING 1. COAX SWEEPS AND FIBER TESTS PER TS-0200 (CURRENT VERSION) ANTENNA LINE ACCEPTANCE
- STANDARDS 2. POST CONSTRUCTION HEIGHT VERIFICATION, AZIMUTH AND DOWNTILT USING ELECTRONIC
- COMMERCIAL MADE-FOR-THE-PURPOSE ANTENNA ALIGNMENT TOOL. 3. CONCRETE BREAK TESTS
- SITE RESISTANCE TO EARTH TEST
   STRUCTURAL BACKFILL COMPACTION TESTS
- 6. CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN SITE INSPECTION ACTIVITIES AND/OR AS A RESULT OF TESTING.
- 7. ADDITIONAL TESTING AS REQUIRED ELSEWHERE IN THIS SPECIFICATION.

- A. THE WORK IN ALL ASPECTS SHALL COMPLY WITH THE CONSTRUCTION DRAWINGS AND THESE
- B.UPLOAD THE FOLLOWING TO SITERRA AS APPLICABLE INCLUDING BUT NOT LIMITED TO THE FOLLOWING
- CONCRETE MIX-DESIGNS FOR TOWER FOUNDATIONS, ANCHORS PIERS, AND CONCRETE PAVING.
   CONCRETE BREAK TESTS AS SPECIFIED HEREIN.
- CHEMICAL GROUNDING SYSTEM 4 REINFORCEMENT CERTIFICATIONS
- STRUCTURAL BACKFILL TEST RESULTS 6. SWEEP AND FIBER TESTS
- ANTENNA AZIMUTH AND DOWN-TILT VERIFICATION

COST REDUCTION PROPOSED FOR USE OF ALTERNATE PRODUCT.

8 POST CONSTRUCTION HEIGHT VERIFICATION ADDITIONAL SUBMITTALS MAY BE REQUIRED FOR SPECIAL CONSTRUCTION OR MINOR MATERIALS C.ALTERNATES: AT THE COMPANY'S REQUEST, ANY ALTERNATIVES TO THE MATERIALS OR METHODS SPECIFIED SHALL BE SUBMITTED TO SPRINT'S CONSTRUCTION MANAGER FOR APPROVAL PRIOR TO BEING SHIPPED TO SITE. SPRINT WILL REVIEW AND APPROVE ONLY THOSE REQUESTS MADE IN WRITING. NO VERBAL APPROVALS WILL BE CONSIDERED. SUBMITTAL FOR APPROVAL SHALL INCLUDE A STATEMENT OF

- A.EMPLOY AN AGENCY OF ENGINEERS AND SCIENTISTS WHO IS REGULARLY ENGAGED IN FIELD AND LABORATORY TESTING AND ANALYSIS. AGENCY SHALL HAVE BEEN IN BUSINESS A MINIMUM OF FIVE YEARS, AND BE LICENSED AS PROFESSIONAL ENGINEERS IN THE STATE WHERE THE PROJECT IS LOCATED.
- AGENCY IS SUBJECT TO APPROVAL BY COMPANY.

  I. AGENCY MUST HAVE A THOROUGH UNDERSTANDING OF LOCAL AVAILABLE MATERIALS, INCLUDING THE SOIL, ROCK, AND GROUNDWATER CONDITIONS.

  2. AGENCY IS TO BE FAMILIAR WITH THE APPLICABLE REQUIREMENTS FOR THE TESTS TO BE DONE,
- EQUIPMENT TO BE USED, AND ASSOCIATED HEALTH AND SAFETY ISSUES.

  3. EXPERIENCE IN SOILS, CONCRETE, MASONRY, AGGREGATE, AND ASPHALT TESTING USING ASTM,
- AASJTO, AND OTHER METHODS IS NEEDED.
  B.REQUIRED THIRD PARTY TESTS:
  - SITE RESISTANCE TO EARTH TEST PER NP-3 | 2-20 |
- 2. CONCRETE CYLINDER BREAK TESTS FOR TOWER PIER AND ANCHORS PER NATIONALLY RECOGNIZED
- 3. STRUCTURAL SOILS COMPACTION TESTS PER NATIONALLY RECOGNIZED STANDARDS REBAR PLACEMENT VERIFICATION WITH REPORT TESTING TENSION STUDY FOR ROCK ANCHORS
- ALL THIRD PARTY TESTS AS REQUIRED BY LOCAL JURISDICTION C.REQUIRED TESTS BY CONTRACTOR
  - COAX SWEEP TESTS PER SPRINT STANDARD TS-0200
  - 2 FIBER TESTS PER SPRINT STANDARD FL-0568 . MICROWAVE LINK TESTS PER NP-760-500
- 4. ANTENNA AZIMUTHS AND DOWN TILT USING ELECTRONIC ALIGNMENT TOOL PER ANTENNA INSTALLATION SPECIFICATION HEREIN



6580 SPRINT PARKWAY OVERLAND PARK, KANSAS 66251



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**48 SPRUCE STREET** OAKLAND, NJ 07346

hereby certify that this plan, specification, or report was pi y me or under my direct supervision and that I am a duly Licensec rofessional Engineer under the laws of the State of Connecticut



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MARK	DATE	DESCRIPTION	_

AVON MOUNTAIN CTO3XCO53-A

DATE 07/14/2014

8 I MONTEVIDEO ROAD AVON. CT 06001 HARTFORD COUNTY

FINAL

SPRINT SPECIFICATIONS

SCALE: NONE

22984

- POST CONSTRUCTION HEIGHT VERIFICATION AS REQUIRED HEREWITH IN THE TOWER INSTALLATION SPECIFICATIONS
- ASPHALT ROADWAY COMPACTED THICKNESS, SURFACE SMOOTHNESS, AND COMPACTED DENSITY TESTING AS SPECIFIED HEREWITH IN THE ASPHALT PAVING SPECIFICATIONS
- FIELD QUALITY CONTROL TESTING AS SPECIFIED HEREWITH IN THE CONCRETE PAVING SPECIFICATIONS
- TESTING REQUIRED HEREWITH UNDER SPECIFICATIONS FOR AGGREGATE BASE FOR ROADWAYS
- 9. ALL OTHER TESTS REQUIRED BY LOCAL JURISDICTION
  D.INSPECTIONS BY COMPANY: THE CONTRACTOR SHALL BE RESPONSIBLE FOR ANY AND ALL CORRECTIONS TO ANY WORK IDENTIFIED AS UNACCEPTABLE IN INSPECTION ACTIVITIES, FINAL ACCEPTANCE / PUNCH WALK REVIEW, AND/OR AS A RESULT OF TESTING
- E. SPRINT RESERVES THE RIGHT TO INSPECT THE CONSTRUCTION SITE AT ANY TIME VIA SITE WAIKS AND/OR PHOTO REVIEWS. CONTRACTOR SHALL GIVE SPRINT 24 HOURS NOTICE PRIOR TO THE COMMENCEMENT OF THE FOLLOWING CONSTRUCTION ACTIVITIES AND PHOTOGRAPHS OF THE IN-PROGRESS WORK, I. GROUNDING SYSTEM AND BURIED UTILITIES INSTALLATION PRIOR TO EARTH CONCEALMENT
  - DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A¢E OR SPRINT REPRESENTATIVE
  - FORMING FOR CONCRETE AND REBAR PLACEMENT PRIOR TO POUR DOCUMENTED WITH DIGITAL PHOTOGRAPHS BY CONTRACTOR, APPROVED BY A\$E OR SPRINT REPRESENTATIVE.
  - COMPACTION OF BACKFILL MATERIALS AGGREGATE BASE FOR ROADS, PADS, AND ANCHORS ASPHALT PAVING, AND SHAFT BACKFILL FOR CONCRETE AND WOOD POLES, BY INDEPENDENT THIRD PARTY AGENCY.
  - PRE AND POST CONSTRUCTION ROOFTOP AND STRUCTURAL INSPECTIONS ON EXISTING FACILITIES. PRIOR TO CONSTRUCTION ACTIVITIES AND AFTER CONSTRUCTION IS COMPLETE, PROVIDE PHOTOGRAPHIC DOCUMENTATION OF ROOF, FLASHINGS, AND PARAPETS, BOTH BEFORE AND AFTER CONSTRUCTION IS COMPLETE
- TOWER ERECTION SECTION STACKING AND PLATFORM ATTACHMENT DOCUMENTED BY DIGITAL PHOTOGRAPHS BY THIRD PARTY AGENCY.
- TOWER TOP AND INACCESSIBLE EQUIPMENT (RRUS, ANTENNAS, AND CABLING): PROVIDE PHOTOS OF THE BACKS OF ALL ANTENNAS, RRUS, COMBINERS, FILTERS, FIBER AND DC CABLING, CABLE COLOR CODING. EQUIPMENT GROUNDING AND CONNECTOR WATER PROOFING INCLUDING NAME PLATE AND SERIAL NUMBER FOR ALL SERIALIZED EQUIPMENT.

A.FINAL ACCEPTANCE PUNCH WALK AND INSPECTION: AS IDENTIFIED IN THE SCOPE OF SERVICES, SPRINT WILL CONDUCT A FINAL PUNCH WALK OR FINAL DESK TOP PHOTO REVIEW (SITE MODIFICATIONS). PUNCI WALKS MUST BE SCHEDULED IN ADVANCE AS REQUIRED. AT THE PUNCH WALK / REVIEW. SPRINT MAY IDENTIFY CRITICAL DEFICIENCIES WHICH MUST BE CORRECTED PRIOR TO PUTTING SITE ON AIR. MINOR DEFICIENCIES MUST BE CORRECTED WITHIN 30 DAYS EXCEPT AS OTHERWISE REQUIRED. VERIFICATIONS OF CORRECTIONS MAY BE MADE BY COMPANY DURING A REPEAT SITE WALK OR DESK TOP PHOTO REVIEW AT COMPANYS SOLE DISCRETION.

B.CLOSEOUT DOCUMENTATION: ALL CLOSEOUT DOCUMENTATION AND PHOTOGRAPHS SHALL BE UPLOADED

PRIOR TO FINAL ACCEPTANCE. SPRINT WILL REVIEW CLOSEOUT DOCUMENTATION FOR PRESENCE AND CONTENT. CLOSEOUT DOCUMENTATION SHALL INCLUDE BUT IS NOT LIMITED TO THE FOLLOWING AS APPLICABLE:

- COAX SWEEP TESTS:
- FIBER TESTS:
  JURISDICTION FINAL INSPECTION DOCUMENTATION
- REINFORCEMENT CERTIFICATION (MILL CERTIFICATION)
  CONCRETE MIX DESIGN AND PRODUCT DATA (TOWER FOUNDATION)
- LIEN WAIVERS AND RELEASES.
  POST -CONSTRUCTION HEIGHT VERIFICATION
- JURISDICTION CERTIFICATE OF OCCUPANCY
  ELECTRONIC ANTENNA AZIMUTH AND DOWN TILT VERIFICATION
- STRUCTURAL BACKFILL TEST RESULTS (IF APPLICABLE)
- CELL SITE UTILITY SETUP
- AS-BUILT REDLINE CONSTRUCTION DRAWINGS (PDF SCAN OF FIELD MARKS) 13. AS-BUILT CONSTRUCTION DRAWINGS IN DWG AND PDF FORMATS
- LIST OF SUB CONTRACTORS
- 15. APPROVED PERMITTING DOCUMENTS 16. FINAL SITE PHOTOS UP-LOADED TO SITERRA. INCLUDE THE FOLLOWING AS APPLICABLE: a. TOWER, ANTENNAS, RRUS, AND MAINLINE: INSPECTION AND PHOTOGRAPHS OF SECTION
  - STACKING; INSPECTION AND PHOTOGRAPHS OF PLATFORM COMPONENT ATTACHMENT POINTS; PHOTOGRAPHS OF TOWER TOP GROUNDING: PHOTOS OF TOWER COAX/CABLE LINE COLOR CODING AT THE TOP AND AT GROUND LEVEL; INSPECTION AND PHOTOGRAPHS OF OPERATIONAL OF TOWER LIGHTING, AND PLACEMENT OF FAA REGISTRATION SIGN; PHOTOGRAPHS SHOWING ADDITIONAL GROUNDING POINTS FOR TOWERS GREATER THAN 200 FEET.; PHOTOS OF ANTENNA GROUND BAR, EQUIPMENT GROUND BAR, AND MASTER GROUND BAR, PHOTOS OF GPS ANTENNA(S); PHOTOS OF EACH SECTOR OF ANTENNAS; ONE PHOTOGRAPH LOOKING AT THE SECTOR AND ONE FROM BEHIND SHOWING THE PROJECTED COVERAGE AREA; PHOTOS OF COAX WEATHERPROOFING - TOP AND BOTTOM; PHOTOS OF COAX GROUNDING--TOP AND BOTTOM; PHOTOS OF ANTENNA AND MAST GROUNDING; PHOTOS OF COAX CABLE ENTRY INTO SHELTER; PHOTOS OF PLATFORM MECHANICAL CONNECTIONS TO TOWER/MONOPOLE.
  - b. ROOF TOPS: PRE-CONSTRUCTION AND POST-CONSTRUCTION VISUAL INSPECTION AND PHOTOGRAPHS OF THE ROOF AND INTERIOR TO DETERMINE AND DOCUMENT CONDITIONS; ROOF TOP CONSTRUCTION INSPECTIONS AS REQUIRED BY THE JURISDICTION; PHOTOGRAPHS OF CABLE TRAY AND/OR ICE BRIDGE; PHOTOGRAPHS OF DOGHOUSE/CABLE EXIT FROM ROOF;
  - c. SITE LAYOUT PHOTOGRAPHS OF THE OVERALL COMPOUND, INCLUDING EQUIPMENT PLATFORM FROM ALL FOUR CORNERS.
  - ALFINISHED UTILITIES: CLOSE-UP PHOTOGRAPHS OF THE PPC BREAKER PANEL; CLOSE-UP PHOTOGRAPH OF THE INSIDE OF THE TELCO PANEL AND NIU; CLOSE-UP PHOTOGRAPH OF THE POWER METER AND DISCONNECT; PHOTOS OF POWER AND TELCO ENTRANCE TO COMPANY ENCLOSURE; PHOTOGRAPHS AT METER BOX AND/OR FACILITY DISTRIBUTION PANEL.

A.PROVIDE PROJECT CLOSEOUT GENERAL ARRANGEMENT PHOTOS OF ALL NEW WORK. THE FOLLOWING LIST REPRESENTS MINIMUM REQUIREMENTS AND MINIMUM QUANTITY. ADDITIONAL PHOTOS MAY BE REQUIRED TO ADEQUATELY DOCUMENT THE WORK.

- ASR AND RF MPE SIGNAGE (IF NOT IN PLACE, SUPPLIER NOTIFIES EMS FIELD REPRESENTATIVE)
- BACK OF ANTENNAS AND RRUS (I EACH SECTOR)
  BACK OF ANTENNAS AND RRUS (I EACH SECTOR) CLOSE UP SHOWING WEATHERPROOFING AND GROUNDING (AS REQUIRED). CLOSE-UP OF BACK SIDE OF EACH PERMANENT RRU SHOWING SERIAL NUMBER/BAR CODE
- VIEW (I EACH SECTOR) ALONG THE AZIMUTH AND TILT OF THE ANTENNAS
- TOP OF TOWER FROM GROUND, I EACH SECTOR
  MAINLINE HYBRID CABLE ROUTE DOWN TOWER SHOWING FASTENERS AND SUPPORT
- MAINLINE/HYBRID CABLE ROUTE ALONG ICE BRIDGE OR IN CABLE TRAY SHOWING FASTENERS AND
- GROUND MOUNTED RRU RACKS (FRONT AND BACK)
- FRONT, SIDE AND BACK ELEVATIONS OF ALL GROUND CABINETS
- LO VIEW OF COMPOUND FROM A DISTANCE
- 11. VIEW OF EACH GROUND CABINET (POWER, RF, FIBER SPOOL, PPC POWER, PPC TELCO WITH DOOR
- 12. BACKHAUL FIBER MEET-ME-POINT AND CONDUIT ROUTE (MICROWAVE INSTALLATION IF NOT FIBER)
- 13. AAV NETWORK INTERFACE DEVICE OR MICROWAVE RADIO INSTALLATION

CONTRACTOR IS RESPONSIBLE FOR ALL CORRECTIONS TO DEFICIENCIES IDENTIFIED THROUGH TESTING, REVIEW OF SUBMITTALS, INSPECTIONS AND CLOSEOUT REVIEWS.

### SECTION O I 500 - PROJECT REPORTING

A CONTRACTOR SHALL REPORT TO SPRINT AT MINIMUM ON A WEEKLY BASIS VIA SITERRA BY LIPDATING ALL APPLICABLE POST END KEEPING MILESTONES WITH ACTUAL AND FORECASTED COMPLETION DATES, B. ADDITIONAL REQUIREMENTS FOR REPORTING MAY BE IDENTIFIED ELSEWHERE OR REQUIRED BY THE SCOPE

OF SERVICES OR SPRINTS LOCAL MARKET CONSTRUCTION MANAGER. THIS INFORMATION WILL PROVIDE A BASIS FOR PROGRESS MONITORING AND PAYMENT.

SPRINT MAY HOLD PERIODIC PROJECT CONFERENCE CALLS. CONTRACTOR WILL BE REQUIRED TO COMMUNICATE SITE STATUS, MILESTONE COMPLETIONS AND UPCOMING MILESTONE PROJECTIONS, AND ANSWER ANY OTHER SITE STATUS QUESTIONS AS NECESSARY.

FINAL PROJECT ACCEPTANCE: PRIOR TO SPRINTS FINAL PROJECT ACCEPTANCE. ALL REQUIRED MILESTONE ACTUALS MUST BE UPDATED IN SITERRA AND ALL REQUIRED REPORTING TASKS MUST BE COMPLETE.

### SECTION I I 700 - ANTENNA ASSEMBLY, REMOTE RADIO UNITS AND CABLE INSTALLATION

THIS SECTION SPECIFIES INSTALLATION OF ANTENNAS, RRU'S, AND CABLE EQUIPMENT, INSTALLATION, AND TESTING OF COAXIAL FIBER CABLE.

THE NUMBER AND TYPE OF ANTENNAS AND RRU'S TO BE INSTALLED IS DETAILED ON THE CONSTRUCTION DRAWINGS.

HYBRID CABLE WILL BE DC/FIBER AND FURNISHED FOR INSTALLATION AT EACH SITE. CABLE SHALL BE INSTALLED PER THE CONSTRUCTION DRAWINGS AND THE APPLICABLE MANUFACTURER'S REQUIREMENTS

JUMPERS AND CONNECTORS: FURNISH AND INSTALL 1/2" COAX JUMPER CABLES BETWEEN THE RRUS AND ANTENNAS, JUMPERS SHALL BE TYPE LDF 4, FLC 12-50, CR 540, OR FXL 540. SUPER-FLEX CABLES ARE NOT ACCEPTABLE. JUMPERS BETWEEN THE RRU'S AND ANTENNAS OR TOWER TOP AMPLIFIERS SHALL CONSIST OF 1/2 INCH FOAM DIELECTRIC, OUTDOOR RATED COAXIAL CABLE, MIN. LENGTH FOR JUMPER SHALL BE 10"-0".

### REMOTE ELECTRICAL TILT (RET) CABLES:

INSTALL SPLITTERS, COMBINERS, FILTERS PER RF DATA SHEET, FURNISHED BY SPRINT.

THE CONTRACTOR SHALL ASSEMBLE ALL ANTENNAS ONSITE IN ACCORDANCE WITH THE INSTRUCTIONS SUPPLIED BY THE MANUFACTURER. ANTENNA HEIGHT, AZIMUTH, AND FEED ORIENTATION INFORMATION SHALL BE A DESIGNATED ON THE CONSTRUCTION DRAWINGS.

- A. THE CONTRACTOR SHALL POSITION THE ANTENNA ON TOWER PIPE MOUNTS SO THAT THE BOTTOM STRUT IS LEVEL. THE PIPE MOUNTS SHALL BE PLUMB TO WITHIN I DEGREE.
- B.ANTENNA MOUNTING REQUIREMENTS: PROVIDE ANTENNA MOUNTING HARDWARE AS INDICATED ON THE

### HYBRID CABLE INSTALLATION:

- A. THE CONTRACTOR SHALL ROUTE, TEST, AND INSTALL ALL CABLES AS INDICATED ON THE CONSTRUCTION DRAWINGS AND IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS
- B THE INSTALLED RADIUS OF THE CABLES SHALL NOT BE LESS THAN THE MANUFACTURER'S SPECIFICATIONS

C.EXTREME CARE SHALL BE TAKEN TO AVOID DAMAGE TO THE CABLES DURING HANDLING AND INSTALLATION.

- I. FASTENING MAIN HYBRID CABLES: ALL CABLES SHALL BE INSTALLED INSIDE MONOPOLE WITH CABLE SUPPORT GRIPS AS REQUIRED BY THE MANUFACTURER.
- 2. FASTENING INDIVIDUAL FIBER AND DC CABLES ABOVE BREAKOUT ENCLOSURE (MEDUSA), WITHIN THE MMBS CABINET AND ANY INTERMEDIATE DISTRIBUTION BOXES:
  - a. FIBER: SUPPORT FIBER BUNDLES USING 1/2" VELCRO STRAPS OF THE REQUIRED LENGTH AT 18" O.C. STRAPS SHALL BE UV, OIL AND WATER RESISTANT AND SUITABLE FOR INDUSTRIAL INSTALLATIONS AS MANUFACTURED BY TEXTOL OR APPROVED EQUAL.
  - b. DC: SUPPORT DC BUNDLES WITH ZIP TIES OF THE ADEQUATE LENGTH. ZIP TIES TO BE UV STABILIZED, BLACK NYLON, WITH TENSILE STRENGTH AT 12,000 PSI AS MANUFACTURED BY NELCO PRODUCTS OR EQUAL.
- 3. FASTENING JUMPERS: SECURE JUMPERS TO THE SIDE ARMS OR HEAD FRAMES USING STAINLESS STEEL TIE WRAPS OR STAINLESS STEEL BUTTERFLY CLIPS.
- 4. CABLE INSTALLATION
  - a. INSPECT CABLE PRIOR TO USE FOR SHIPPING DAMAGE, NOTIFY THE CONSTRUCTION
  - b. CABLE ROUTING: CABLE INSTALLATION SHALL BE PLANNED TO ENSURE THAT THE LINES MILL BE PROPERLY ROUTED IN THE CABLE ENVELOP AS INDICATED ON THE DRAWINGS. AVOID TWISTING AND CROSSOVERS.
  - c. HOIST CABLE USING PROPER HOISTING GRIPS. DO NOT EXCEED MANUFACTURER'S RECOMMENDED MAXIMUM BEND RADIUS
- 5. GROUNDING OF TRANSMISSION LINES: ALL TRANSMISSION LINES SHALL BE GROUNDED AS INDICATED ON DRAWINGS
- 6. HYBRID CABLE COLOR CODING: ALL COLOR CODING SHALL BE AS REQUIRED IN TS 0200 (CURRENT 7. HYBRID CABLE LABELING: INDIVIDUAL HYBRID AND DC BUNDLES SHALL BE LABELED ALPHA-NUMERICALLY ACCORDING TO SPRINT CELL SITE ENGINEERING NOTICE - EN 2012-001, REV I

### WEATHERPROOFING EXTERIOR CONNECTORS AND HYBRID CABLE GROUND KITS:

A. ALL FIBER ¢ COAX CONNECTORS AND GROUND KITS SHALL BE WEATHERPROOFED

- B. WEATHERPROOFED USING ONE OF THE FOLLOWING METHODS. ALL INSTALLATIONS MUST BE DONE IN ACCORDANCE WITH THE MANUFACTURER'S RECOMMENDATIONS AND INDUSTRY BEST PRACTICES.
- COLD SHRINK: ENCOMPASS CONNECTOR IN COLD SHRINK TUBING AND PROVIDE A DOUBLE WRAP OF " ELECTRICAL TAPE EXTENDING 2" BEYOND TUBING. PROVIDE 3M COLD SHRINK CXS SERIES OR
- 2 SELF-AMALGAMATING TAPE: CLEAN SURFACES, APPLY A DOUBLE WRAP OF SELF-AMALGAMATING TAPE 2" BEYOND CONNECTOR. APPLY A SECOND WRAP OF SELF-AMALGAMATING TAPE IN OPPOSITE DIRECTION. APPLY DOUBLE WRAP OF 2" WIDE ELECTRICAL TAPE EXTENDING 2" BEYOND THE
- 3. 3M SLIM LOCK CLOSURE 716: SUBSTITUTIONS WILL NOT BE ALLOWED.
- 4. OPEN FLAME ON JOB SITE IS NOT ACCEPTABLE

# SECTION 1 1 800 - INSTALLATION OF MULTIMODAL BASE STATIONS (MMBS)

### SUMMARY

- A. THIS SECTION SPECIFIES MMBS CABINETS, POWER CABINETS, AND INTERNAL EQUIPMENT INCLUDING BY NOT LIMITED TO RECTIFIERS, POWER DISTRIBUTION UNITS, BASE BAND UNITS, SURGE ARRESTORS, BATTERIES, AND SIMILAR EQUIPMENT FURNISHED BY THE COMPANY FOR INSTALLATION BY THE CONTRACTOR (OFCI)
- B. CONTRACTOR SHALL PROVIDE AND INSTALL ALL MISCELLANEOUS MATERIALS AND PROVIDE ALL LABOR REQUIRED FOR INSTALLATION EQUIPMENT IN EXISTING CABINET OR NEW CABINET AS SHOWN ON DRAWINGS AND AS REQUIRED BY THE APPLICABLE INSTALLATION MOPS.

C.COMPLY WITH MANUFACTURER'S INSTALLATION AND START-UP REQUIREMENTS.

### DC CIRCUIT BREAKER LABELING

A.NEW DC CIRCUIT IS REQUIRED IN MMBS CABINET SHALL BE CLEARLY IDENTIFIED AS TO RRU BEING SERVICED.

### SECTION 26 100 - BASIC ELECTRICAL REQUIREMENTS

THIS SECTION SPECIFIES BASIC ELECTRICAL REQUIREMENTS FOR SYSTEMS AND COMPONENTS

### QUALITY ASSURANCE:

- A.ALL EQUIPMENT FURNISHED UNDER DIVISION 26 SHALL CARRY UL LABELS AND LISTINGS WHERE SUCH LABELS AND LISTINGS ARE AVAILABLE IN THE INDUSTRY.
- B.MANUFACTURERS OF EQUIPMENT SHALL HAVE A MINIMUM OF THREE YEARS EXPERIENCE WITH THEIR EQUIPMENT INSTALLED AND OPERATING IN THE FIELD IN A USE SIMILAR TO THE PROPOSED USE FOR THIS
- C.MATERIALS AND EQUIPMENT: ALL MATERIALS AND EQUIPMENT SPECIFIED IN DIVISION 26 OF THE SAME TYPE SHALL BE OF THE SAME MANUFACTURER AND SHALL BE NEW, OF THE BEST QUALITY AND DESIGN, AND FREE FROM DEFECTS.

### SUPPORTING DEVICES

- A.MANUFACTURED STRUCTURAL SUPPORT MATERIALS: SUBJECT TO COMPLIANCE WITH REQUIREMENTS, PROVIDE PRODUCTS BY THE FOLLOWING:
- I. ALLIED TUBE AND CONDUIT
- 2. B-LINE SYSTEM.
- 3. UNISTRUT DIVERSIFIED PRODUCTS.
- 4. THOMAS & BETTS

B.FASTENERS: TYPES, MATERIALS, AND CONSTRUCTION FEATURES AS FOLLOWS

- I. EXPANSION ANCHORS: CARBON STEEL WEDGE OR SLEEVE TYPE.
- 2. POWER-DRIVEN THREADED STUDS: HEAT-TREATED STEEL, DESIGNED SPECIFICALLY FOR THE INTENDED
- 3. FASTEN BY MEANS OF WOOD SCREWS ON WOOD
- 4. TOGGLE BOLTS ON HOLLOW MASONRY UNITS.
- 5. CONCRETE INSERTS OR EXPANSION BOLTS ON CONCRETE OR SOLID MASONRY.
- 6. MACHINE SCREWS, WELDED THREADED STUDS, OR SPRING-TENSION CLAMPS ON STEEL
- 7. EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE SHALL NOT BE PERMITTED
- 8. DO NOT WELD CONDUIT, PIPE STRAPS, OR ITEMS OTHER THAN THREADED STUDS TO STEEL
- 9. IN PARTITIONS OF LIGHT STEEL CONSTRUCTION, USE SHEET METAL SCREWS.



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hereby certify that this plan, specification, or re y me or under my direct supervision and that I am a duly Licensec rofessional Engineer under the laws of the State of Connecticut



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DATE 07/14/2014

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SPRINT SPECIFICATIONS

SCALE: NONE

22984

### SUPPORTING DEVICES:

- A. INSTALL SUPPORTING DEVICES TO FASTEN ELECTRICAL COMPONENTS SECURELY AND PERMANENTLY IN
- B. COORDINATE WITH THE BUILDING STRUCTURAL SYSTEM AND WITH OTHER TRADES.
- C. UNLESS OTHERWISE INDICATED ON THE DRAWINGS, FASTEN ELECTRICAL ITEMS AND THEIR SUPPORTING HARDWARE SECURELY TO THE STRUCTURE IN ACCORDANCE WITH THE FOLLOWING
- I. ENSURE THAT THE LOAD APPLIED BY ANY FASTENER DOES NOT EXCEED 25 PERCENT OF
- 2. USE VIBRATION AND SHOCK-RESISTANT FASTENERS FOR ATTACHMENTS TO CONCRETE

### ELECTRICAL IDENTIFICATION:

- A. UPDATE AND PROVIDE TYPED CIRCUIT BREAKER SCHEDULES IN THE MOUNTING BRACKET, INSIDE DOORS
- BRANCH CIRCUITS FEEDING AVIATION OBSTRUCTION LIGHTING EQUIPMENT SHALL BE CLEARLY IDENTIFIED AS SUCH AT THE BRANCH CIRCUIT PANELBOARD.

### SECTION 26 200 - ELECTRICAL MATERIALS AND EQUIPMENT

- A. RIGID GALVANIZED STEEL (RGS) CONDUIT SHALL BE USED FOR EXTERIOR LOCATIONS ABOVE GROUND AND IN UNFINISHED INTERIOR LOCATIONS AND FOR UNDERGROUND RUNS. RIGID CONDUIT AND FITTINGS SHALL BE STEEL, COATED WITH ZINC EXTERIOR AND INTERIOR BY THE HOT DIP GALVANIZING PROCESS, CONDUIT SHALL BE PRODUCED TO ANSI SPECIFICATIONS CO. I, FEDERAL SPECIFICATION WW-C-58 I AND SHALL BE LISTED WITH THE UNDERWRITERS' LABORATORIES, FITTINGS SHALL BE THREADED - SET SCREW OR COMPRESSION FITTINGS WILL NOT BE ACCEPTABLE. RGS CONDUITS SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND.
- B. UNDERGROUND CONDUIT IN CONCRETE SHALL BE POLYVINY CHLORIDE (PVC) SUITABLE FOR DIRECT BURIAL AS APPLICABLE. JOINTS SHALL BE BELLED, AND FLUSH SOLVENT WELDED IN ACCORDANCE WITH MANUFACTURER'S INSTRUCTIONS. CONDUIT SHALL BE CARLON ELECTRICAL PRODUCTS OR APPROVED
- C. TRANSITIONS BETWEEN PVC AND RIGID (RGS) SHALL BE MADE WITH PVC COATED METALLIC LONG SWEEP
- D FMT OR RIGID GALVANIZED STEEL CONDUIT MAY BE LISED IN FINISHED SPACES CONCEALED IN WALLS AND CEILINGS. EMT SHALL BE MILD STEEL, ELECTRICALLY WELDED, ELECTRO-GALVANIZED OR HOT-DIPPED GALVANIZED AND PRODUCED TO ANSI SPÉCIFICATION C80.3, FEDERAL SPÉCIFICATION WW-C-563, AND SHALL BE UL LISTED. EMT SHALL BE MANUFACTURED BY ALLIED, REPUBLIC OR WHEATLAND, OR APPROVED EQUAL. FITTINGS SHALL BE METALLIC COMPRESSION. SET SCREW CONNECTIONS SHALL NOT
- LIQUID TIGHT FLEXIBLE METALLIC CONDUIT SHALL BE USED FOR FINAL CONNECTION TO EQUIPMENT. FITTINGS SHALL BE METALLIC GLAND TYPE COMPRESSION FITTINGS, MAINTAINING THE INTEGRITY OF CONDUIT SYSTEM. SET SCREW CONNECTIONS SHALL NOT BE ACCEPTABLE. MAXIMUM LENGTH OF FLEXIBLE CONDUIT SHALL NOT EXCED G-FEET. LFMC SHALL BE PROTECTED AND EXPORTED AS REQUIRED BY NEC. MANUFACTURERS OF FLEXIBLE CONDUITS SHALL BE CAROL, ANACONDA METAL HOSE OR UNIVERSAL METAL HOSE, OR APPROVED EQUAL.
- F. MINIMUM SIZE CONDUIT SHALL BE 3/4 INCH (2 I MM).

### HUBS AND BOXES:

- AT ENTRANCES TO CABINETS OR OTHER EQUIPMENT NOT HAVING INTEGRAL THREADED HUBS PROVIDE METALLIC THREADED HUBS OF THE SIZE AND CONFIGURATION REQUIRED. HUB SHALL INCLUDE LOCKNUT AND NEOPRENE O-RING SEAL. PROVIDE IMPACT RESISTANT 105 DEGREE C PLASTIC BUSHINGS TO PROTECT CABLE INSULATION.
- B. CABLE TERMINATION FITTINGS FOR CONDUIT
- CABLE TERMINATORS FOR RGS CONDUITS SHALL BE TYPE CRC BY O-Z/GEDNEY OR EQUAL BY
- CABLE TERMINATORS FOR LFMC SHALL BE ETCO CL2075; OR MADE FOR THE PURPOSE PRODUCTS BY ROXTEC
- C. EXTERIOR PULL BOXES AND PULL BOXES IN INTERIOR INDUSTRIAL AREAS SHALL BE PLATED CAST ALLOY HEAVY DUTY, WEATHERPROOF, DUST PROOF, WITH GASKET, PLATED IRON ALLOY COVER AND STAINLESS STEEL COVER SCREWS, CROUSE-HINDS WAB SERIES OR EQUAL.
- CONDUIT OUTLET BODIES SHALL BE PLATED CAST ALLOY WITH SIMILAR GASKET COVERS. OUTLET BODIES SHALL BE OF THE CONFIGURATION AND SIZE SUITABLE FOR THE APPLICATION. PROVIDE CROUSE-HINDS FORM 8 OR EQUAL
- E. MANUFACTURER FOR BOXES AND COVERS SHALL BE HOFFMAN, SQUARE "D", CROUSE-HINDS, COOPER, ADALET, APPLETON, O-Z GEDNEY, RACO, OR APPROVED EQUAL.

### SUPPLEMENTAL GROUNDING SYSTEM:

- A. FURNISH AND INSTALL A SUPPLEMENTAL GROUNDING SYSTEM TO THE EXTENT INDICATED ON THE DRAWINGS, SUPPORT SYSTEM WITH NON-MAGNETIC STAINLESS STEEL CLIPS WITH RUBBER GROMMETS. GROUNDING CONNECTORS SHALL BE TINNED COPPER WIRE, SIZES AS INDICATED ON THE DRAWINGS. PROVIDE STRANDED OR SOLID BARE OR INSULATED CONDUCTORS EXCEPT AS OTHERWISE NOTED.
- B. SUPPLEMENTAL GROUNDING SYSTEM: ALL CONNECTIONS TO BE MADE WITH CAD WELDS. EXCEPT AT EQUIPMENT USE LUGS OR OTHER AVAILABLE GROUNDING MEANS AS REQUIRED BY MANUFACTURER; AT GROUND BARS USE TWO HOLE SPADES WITH NO-OX.
- C. STOLEN GROUND-BARS: IN THE EVENT OF STOLEN GROUND BARS, CONTACT SPRINT CM FOR REPLACEMENT INSTRUCTION USING THREADED ROD KITS.

### EXISTING STRUCTURE:

A. EXISTING EXPOSED WIRING AND ALL EXPOSED OUTLETS, RECEPTACLES, SWITCHES, DEVICES, BOXES, AND OTHER EQUIPMENT THAT ARE NOT TO BE UTILIZED IN THE COMPLETED PROJECT SHALL BE REMOVED OR DE-ENERGIZED AND CAPPED IN THE WALL, CEILING, OR FLOOR SO THAT THEY ARE CONCEALED AND SAFE. WALL, CEILING, OR FLOOR SHALL BE PATCHED TO MATCH THE ADJACENT CONSTRUCTION

### CONDUIT AND CONDUCTOR INSTALLATION:

A.CONDUITS SHALL BE FASTENED SECURELY IN PLACE WITH APPROVED NON-PERFORATED STRAPS AND HANGERS, EXPLOSIVE DEVICES FOR ATTACHING HANGERS TO STRUCTURE WILL NOT BE PERMITTED.
CLOSELY FOLLOW THE LINES OF THE STRUCTURE, MAINTAIN CLOSE PROXIMITY TO THE STRUCTURE AND KEEP CONDUITS IN TIGHT ENVELOPES. CHANGES IN DIRECTION TO ROUTE AROUND OBSTACLES SHALL BE MADE WITH CONDUIT OUTLET BODIES. CONDUIT SHALL BE INSTALLED IN A NEAT AND WORKMANLIKE MANNER, PARALLEL AND PERPENDICULAR TO STRUCTURE WALL AND CEILING LINES. ALL CONDUIT SHALL BE FISHED TO CLEAR OBSTRUCTIONS. ENDS OF CONDUITS SHALL BE TEMPORARILY CAPPED TO PREVENT CONCRETE, PLASTER OR DIRT FROM ENTERING. CONDUITS SHALL BE RIGIDLY CLAMPED TO BOXES BY GALVANIZED MALLEABLE IRON BUSHING ON INSIDE AND GALVANIZED MALLEABLE IRON LOCKNUT ON

B.CONDUCTORS SHALL BE PULLED IN ACCORDANCE WITH ACCEPTED GOOD PRACTICE.



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DATE 07/14/2014 FINAL

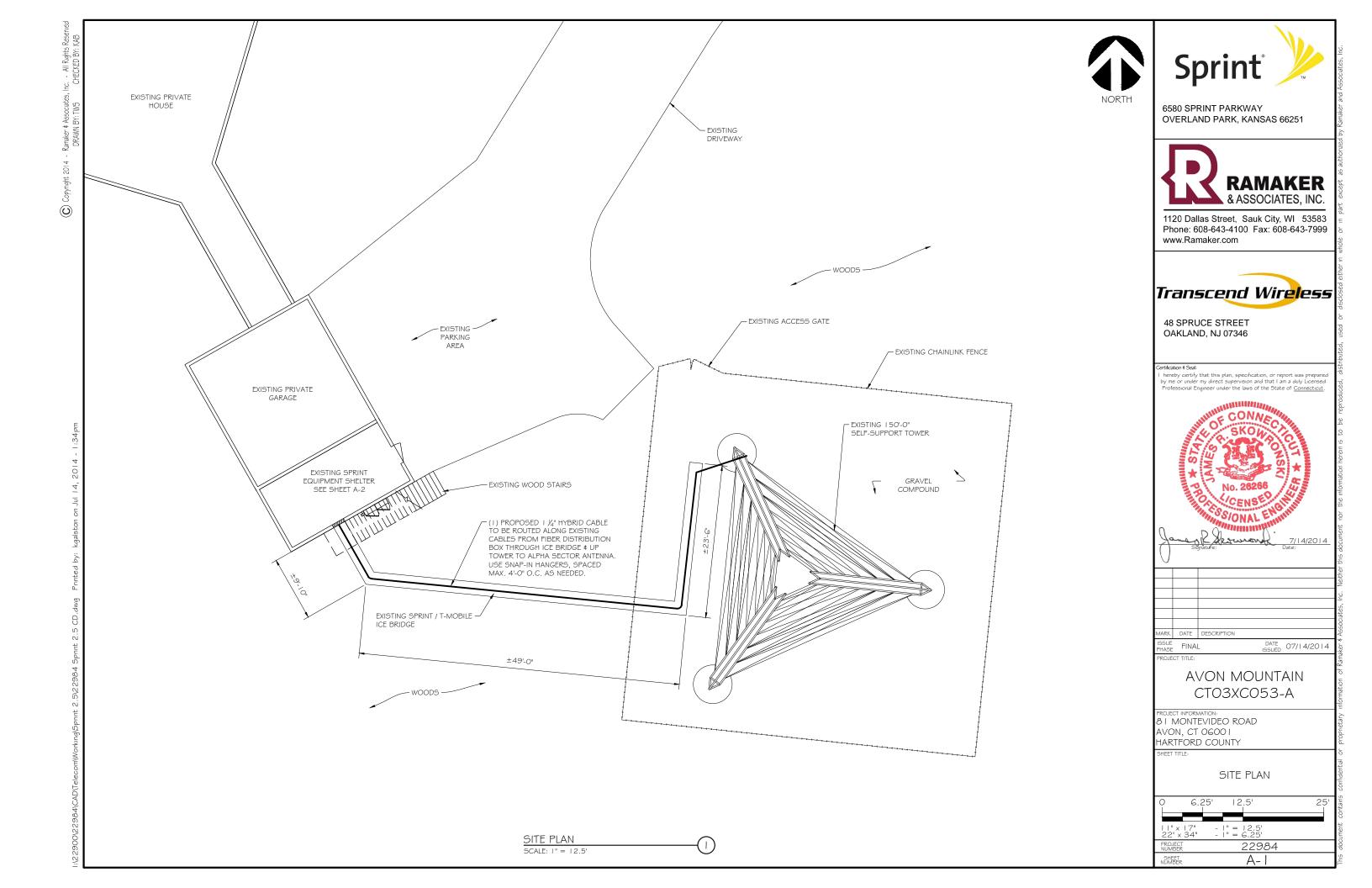
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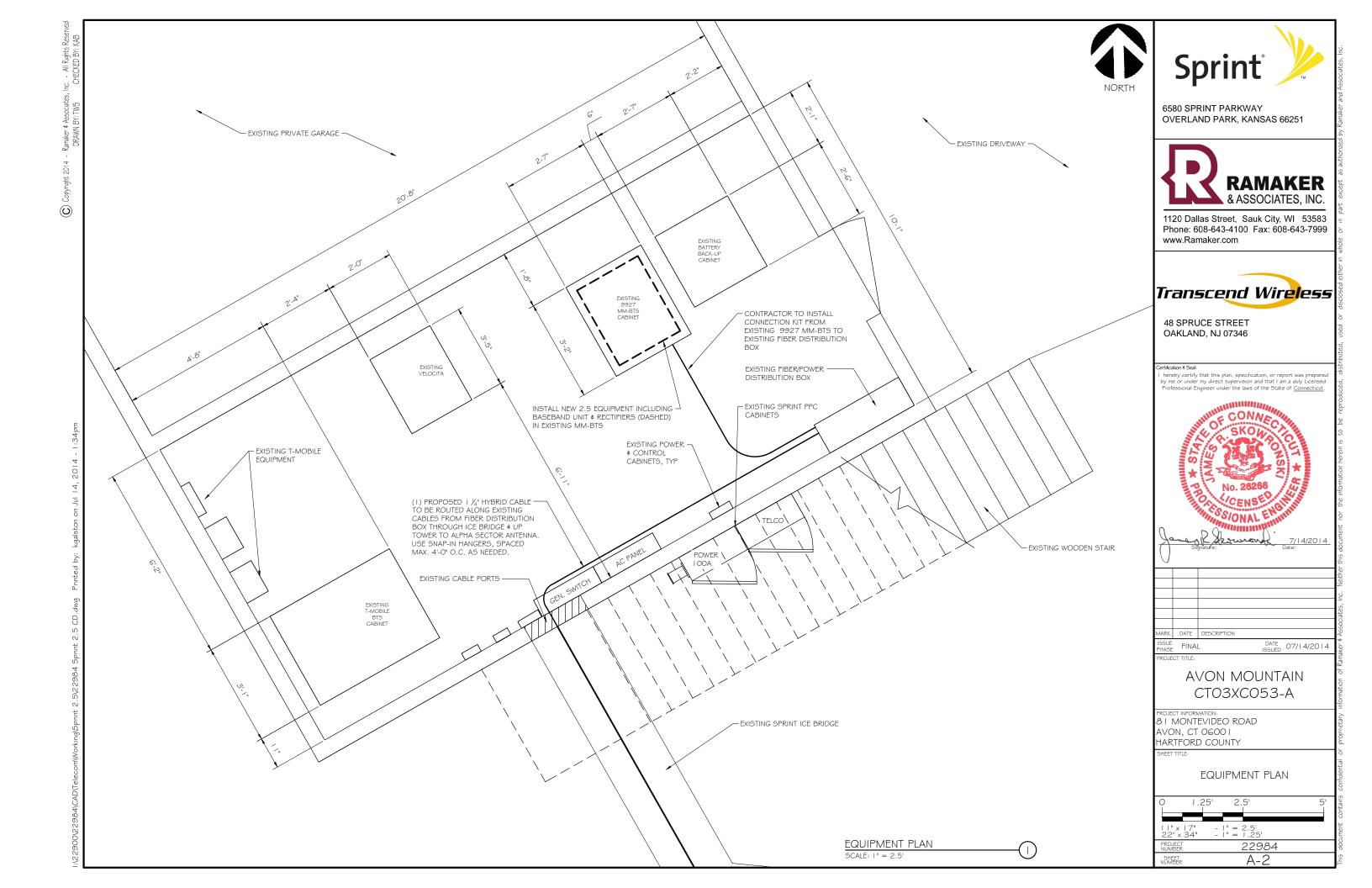
81 MONTEVIDEO ROAD AVON, CT 06001 HARTFORD COUNTY

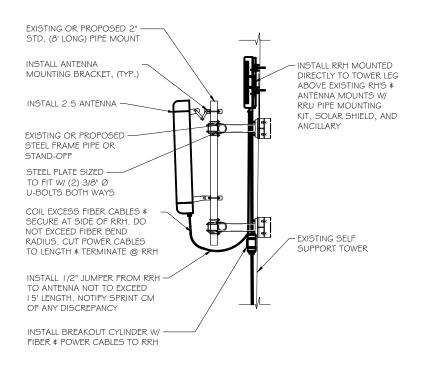
SPRINT SPECIFICATIONS

SCALE: NONE

22984 SP-3 SHEET







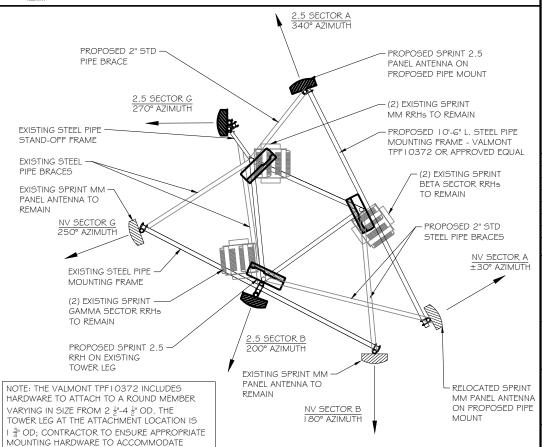
ANTENNA & RRH MOUNTING DETAILS

EXISTING SPRINT MM — NV SECTOR A ±30° AZIMUTH PANEL ANTENNA TO BE RELOCATED (2) EXISTING SPRINT EXISTING STEEL PIPE MM RRHs TO REMAIN STAND-OFF FRAME EXISTING STEEL PIPE BRACES EXISTING SPRINT MM -PANEL ANTENNA TO REMAIN NV SECTOR G 250° AZIMUTH EXISTING STEEL PIPE MOUNTING FRAME (2) EXISTING SPRINT (2) EXISTING SPRINT GAMMA SECTOR RRHs BETA SECTOR RRHs TO REMAIN TO REMAIN EXISTING VACANT PIPE MOUNT EXISTING SPRINT MM -PANEL ANTENNA TO NV SECTOR B 180° AZIMUTH



TOWER LEG IS ORDERED/INSTALLED.

PROPOSED ANTENNA ARRAY





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I hereby certify that this plan, specification, or report was prepared by me or under my direct supervision and that I am a duly Licensed Professional Engineer under the laws of the State of <u>Connecticut</u>.



MARK DATE DESCRIPTION

ISSUE FINAL DATE O7/14/2014

CT TITLE:

# AVON MOUNTAIN CT03XC053-A

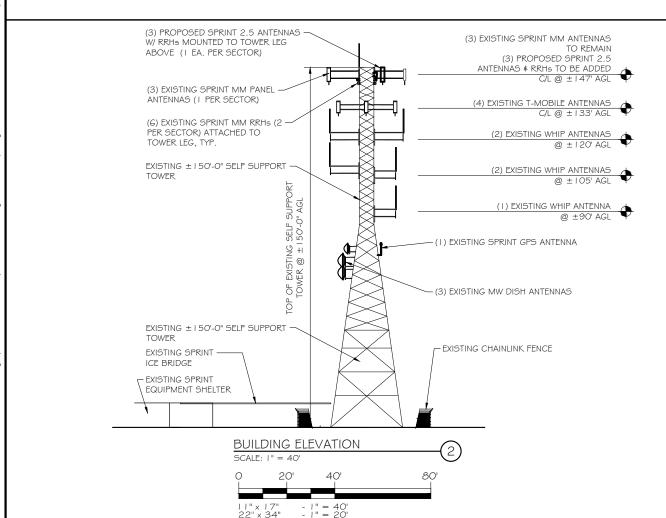
8 I MONTEVIDEO ROAD AVON, CT 0600 I HARTFORD COUNTY

HEET TITLE:

BUILDING ELEVATIONS \$
ANTENNA DETAILS

SCALE: AS NOTED

PROJECT 22984
SHEET A-3





### **RFDS Sheet**

### **General Site Information**

Site ID	CT03XC053
Market	Northern Connecticut
Region	Northeast
MLA	N/A
Structure Type	lattice
BTS Type	

Equipment Vendor	Alcatel-Lucent
Lattitude	41.80278
Longitude	-72.80111
LL SITE ID	N/A

Solution ID

Siterra SR Equipment type Alcatel-Lucent **Equipment Vendor** 

Incremental Power Draw needed by added Equipment N/A

### **Base Equipment**

BBU Kit	
BBU Kit Qty	

A	ALU BBU Kit	-
	1	

None

N/A

N/A N/A

Top Hat	
Top Hat Qty	
Top Hat Dimenstions	
Top Hat Weight (lbs)	

None
N/A
N/A
N/A

**Growth Cabinet** 

**Growth Cabinet Qty** 

Growth	Cabinet Dimensions
Growth	Cabinet Weight

### RF Path Information

RRH
RRH Qty
RRH Dimensions
RRH Weight. lbs.
RRH Mount Weight. Lbs.
Power and Fiber Cable
Cable Qty
Weight per foot. Lbs.
Diameter. Inches.
March at the

Length Ft. Coax Jumper Coax Jumper Qty Coax Jumper Length. Feet. Coax Jumper Weight Coax Jumper Diameter. Inches

AISG Cable Qty AISG Diameter. Inches. AISG Cable length. Feet.

AISG Cable

Weight of entire AISG cable. Lbs.

8

1.3

calculated as antenna height plus 20%)

### Antenna Sector Information

Antenna make/model
Antenna qty
Antenna Dimensions. Inches
Antenna Weight. Lbs
Antenna Mounting Kit Weight. Lbs.
CL Height
Antenna Azimuth
Antenna Mechanical Downtilt
Antenna etilt

Sector 1	Sector 2	Sector 3
RFS APXV9TM14-ALU-I20	RFS APXV9TM14-ALU-I20	RFS APXV9TM14-ALU-I20
1	1	1
56.3"x12.6"x6.3"	56.3"x12.6"x6.3"	56.3"x12.6"x6.3"
55.12	55.12	55.12
11.5	11.5	11.5
147	147	147
340	200	270
0	0	0
-2	-2	-2

\*REDS SHEET WAS GENERATED BY RAMAKER & ASSOCIATES FROM PLAN OF RECORD (POR) PROVIDED BY SPRINT. CONTRACTOR SHALL VERIFY AND OBTAIN FINAL RFDS FROM SPRINT CONSTRUCTION MANAGER PRIOR TO CONSTRUCTION.

# Sprint

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PROJECT INFORMATION: 8 I MONTEVIDEO ROAD AVON, CT 06001 HARTFORD COUNTY

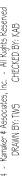
RF DATA SHEET

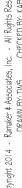
SCALE: AS NOTED

22984 A-4 SHEET

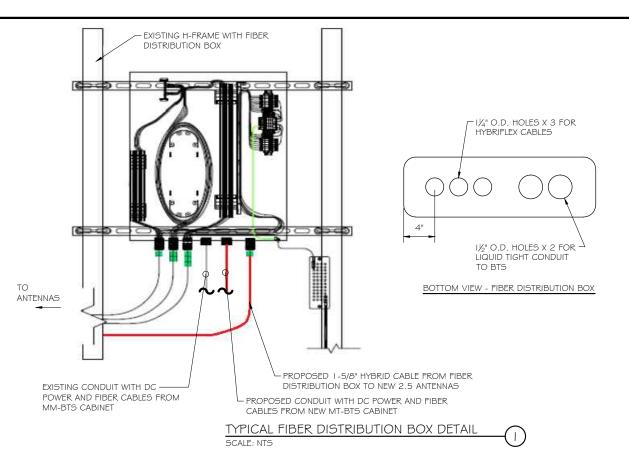
NOTES: I. GENERAL CONTRACTOR TO FIELD VERIFY AZIMUTH AND

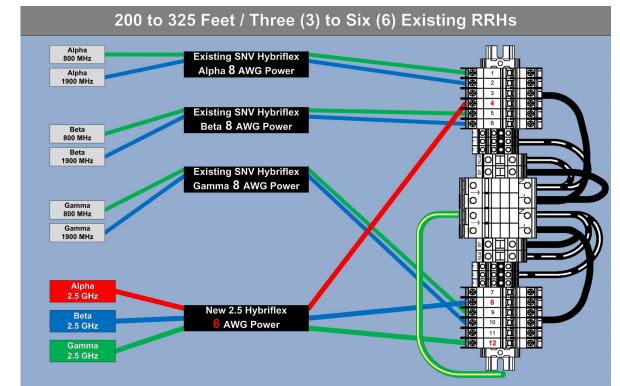
- C/L HEIGHT AND MECHANICAL DOWNTILT. IF DIFFERENT THAN CALLED OUT BELOW, HALT ANTENNA WORK FOR ONE HOUR, CALL SPRINT RF ENGINEER (OR MANAGER IF RF ENGINEER DOES NOT ANSWER, BUT STILL LEAVE A MESSAGE TO RF ENGINEER) USING CONTACT INFORMATION ABOVE FOR FURTHER INSTRUCTIONS. IF SPRINT DOES NOT RESPOND WITHIN ONE HOUR, PLACE 2.5GHZ ANTENNA AT SAME C/L HEIGHT AS PLACE 2.56H2 ANI ENNA A1 5AME (J. HEIGH1 A5 1.96H2 ANTENNA AND EMAIL CORRECT C/L HEIGHT AND AZIMUTH TO SPRINT RF ENGINEER. UPDATE AS-BUILD DRAWING WITH CORRECT C/L HEIGHT. ALSO EMAIL CORRECT 1.96H2 AND 800MHZ ANTENNA C/L HEIGHT, AZIMUTH AND MECHANICAL DOWNTILT TO RF ENCINEER. ENGINEER.
- AISG TESTS TO VERIPY OPERATION IS TO BE
  PERFORMED AFTER FINAL INSTALLATION OF ANTENNAS
  AND AISG CABLES HAVE BEEN CONNECTED. VERIPY OPERATION OF ALL EXISTING SPRINT AISG EQUIPMENT INCLUDING 800MHZ, I.9GHZ AND 2.5GHZ. TEST TO INCLUDE COMPLETE DOWNTILT, AZIMUTH (IF APPLICABLE) AND BEAMWIDTH SWINGS (IF APPLICABLE). DOCUMENT AISG TEST RESULTS IN COAX SWEEP TEST SPREADSHEET.
- 3. GENERAL CONTRACTOR MUST ENSURE THAT NO OBJECT 19 LOCATED WITHIN 45 DEGREES OF LEFT AND RIGHT OF FRONT OF ANTENNA OR 7 DEGREES UP AND DOWN FROM CENTER OF ANTENNA. IF THIS IS NOT POSSIBLE, CONTACT RF ENGINEER FOR FURTHER INSTRUCTION. IN ADDITION, 2.5GHZ ANTENNA IS NOT TO BE PLACED IN FRONT OF ANY OTHER ANTENNA
  USING THE SAME 45 DEGREE RULE. THIS INCLUDES SPRINT AND NON-SPRINT ANTENNAS.
- 4. 2.5GHZ ANTENNA MUST BE AT LEAST 6" FROM 1.9GHZ ANTENNA, 30" FROM 800MHZ ANTENNA AND 30" FROM DUAL BAND I .9GHZ AND 800MHZ ANTENNA.
- 5. GENERAL CONTRACT IS REQUIRED TO USE A DIGITAL ALIGNMENT TOOL TO SET AZIMUTH, ROLL AND DOWNTILT. AZIMUTH ACCURACY IS TO BE WITHIN I DEGREE. DOWNTILT AND ROLL (LEFT TO RIGHT TILT) IS TO BE WITHIN O. I DEGREES. IF FOR SOME REASON THIS ACCURACY CANNOT BE ACHIEVED. UPDATE AS-BUILT DRAWINGS AND EMAIL SPRINT RF ENGINEER
  WITH AS-BUILT SETTINGS. USE 3Z RF ALIGNMENT TOOL OR EQUIVALENT TOOL.



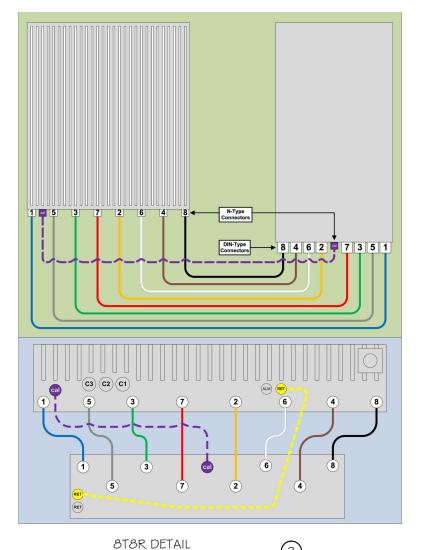




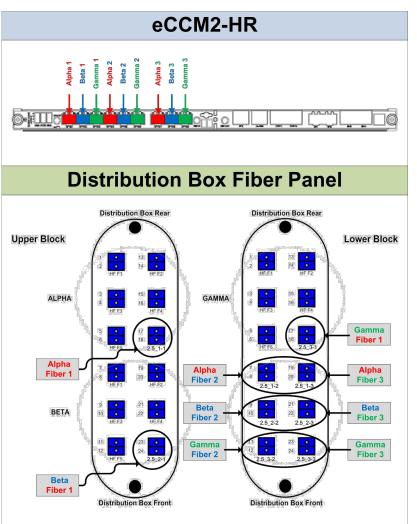


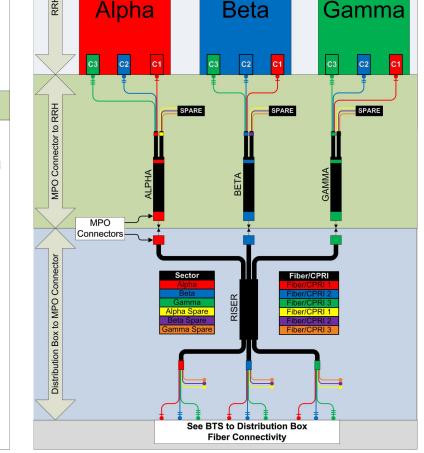


RRH TO DISTRIBUTION BOX POWER CONNECTIVITY DETAIL SCALE: NTS



(3)





RRH TO DISTRIBUTION BOX FIBER CONNECTIVITY DETAIL

Sprint

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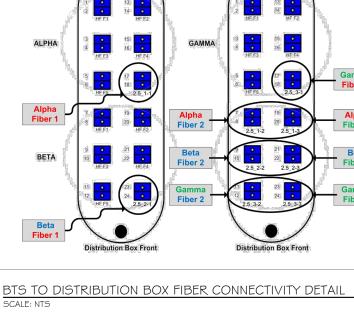
### AVON MOUNTAIN CTO3XCO53-A

PROJECT INFORMATION: 8 I MONTEVIDEO ROAD AVON. CT 06001 HARTFORD COUNTY

FIBER PLUMBING DIAGRAM

SCALE: AS NOTED

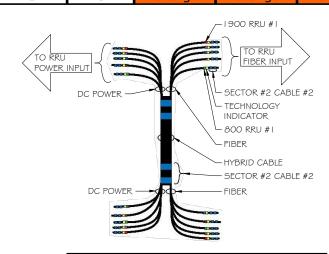
22984 SHEET A-5

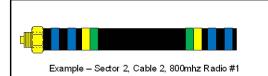


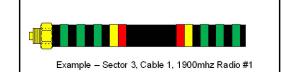
2.5			
<b>FREQUENCY</b>	INDICAT	ΓOR	ID
2500 -1	YEL	WHT	GRN
2500 -2	YEL	WHT	RED
2500 -3	YEL	WHT	BRN
2500 -4	YEL	WHT	BLU
2500 -5	YEL	WHT	SLT
2500 -6	YEL	WHT	ORG
2500 -7	YEL	WHT	WHT
2500 -8	YEL	WHT	PPL

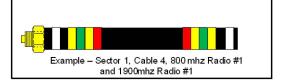
NV FREQUENCY	INDICATOR	ID
800-1	YEL	GRN
1900-1	YEL	RED
1900-2	YEL	BRN
1900-3	YEL	BLU
1900-4	YEL	SLT
800-1	YEL	ORG
RESERVED	YEL	WHT
RESERVED	YEL	PPL

			Second	
Sector	Cable	First Ring	Ring	Third Ring
1 Alpha	1	Green	No Tape	No Tape
1	2		No Tape	No Tape
1	3	Brown	No Tape	No Tape
1	4	White	No Tape	No Tape
1	5	Red	No Tape	No Tape
1	6	Grey	No Tape	No Tape
1	7	Purple	No Tape	No Tape
1	8	Orange	No Tape	No Tape
2 Beta	1	Green	Green	No Tape
2	2			No Tape
2	3	Brown	Brown	No Tape
2	4	White	White	No Tape
2	5	Red	Red	No Tape
2	6	Grey	Grey	No Tape
2	7	Purple	Purple	No Tape
2	8	Orange	Orange	No Tape
3 Gamma	1	Green	Green	Green
3	2			Blue
3	3	Brown	Brown	Brown
3	4	White	White	White
3	5	Red	Red	Red
3	6	Grey	Grey	Grey
3	7	Purple	Purple	Purple
3	8	Orange	Orange	Orange









COLOR CODING CHARTS SCALE: NTS



# CABLE MARKING NOTES

- I. ALL CABLES SHALL BE MARKED WITH 2" WIDE, UV STABILIZED, UL APPROVED TAPE.
- THE FIRST RING SHALL BE CLOSEST TO THE END OF THE CABLE AND SPACED APPROXIMATELY 2" FROM THE END CONNECTOR, WEATHERPROOFING, OR BREAKOUT UNIT. THERE SHALL BE 1" SPACE BETWEEN EACH RING.
- 3. A 2" GAP SHALL SEPARATE THE CABLE COLOR CODE FROM THE FREQUENCY COLOR CODE. THE 2"
  COLOR RINGS FOR THE FREQUENCY CODE SHALL BE PLACED NEXT TO EACH OTHER WITH NO SPACES.
- 4. THE 2" COLORED TAPE(S) SHALL BE WRAPPED A MINIMUM OF 3 TIMES AROUND THE INDIVIDUAL CABLES, AND THE TAPE SHALL BE KEPT IN THE SAME LOCATION AS MUCH AS POSSIBLE.
- 5. SITES WITH MORE THAN FOUR (4) SECTORS WILL REQUIRE ADDITIONAL RINGS FOR EACH SECTOR, FOLLOWING THE PATTERN. HIGH CAPACITY SITES WILL USE THE SECOND CABLE IDENTIFIED BY BLUE BANDS OF TAPE
- 6. HYBRID FIBER CABLE SHALL BE SECTOR IDENTIFIED INSIDE THE CABINET ON PREQUENCY BUNDLES, ON THE SEALTITE, ON THE MAIN LINE UPON EXIT OF SEALTITE, AND BEFORE AND AFTER THE BREAKOUT UNIT (MEDUSA), AS WELL AS BEFORE AND AFTER ANY ENTRANCE OR EXIT.
- 7. HFC "MAIN TRUNK" WILL NOT BE MARKED WITH THE FREQUENCY CODES, AS IT CONTAINS ALL FREQUENCIES.
- 8. INDIVIDUAL POWER PAIRS AND FIBER BUNDLES SHALL BE LABELED WITH BOTH THE CABLE AND



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### AVON MOUNTAIN CTO3XCO53-A

PROJECT INFORMATION: 8 I MONTEVIDEO ROAD AVON, CT 06001 HARTFORD COUNTY

CABLE COLOR CODING

SCALE: AS NOTED

22984 SHEET A-6

FIBER ONLY

# HYBRID CABLE DC CONDUCTOR SIZE GUIDELINE

CABLE	LENGTH	DC CONDUCTOR	CABLE DIAMETER
Fiber Only	Varies	Use NV Hybriflex	5/8"
Hybriflex	<200'	8 AWG	1-1/4"
Hybriflex	225-300'	6 AWG	1-1/4"
Hybriflex	325-375'	4 AWG	1-1/4"

### RFS HYBRIFLEX RISER CABLE SCHEDULE

	_ <del></del>	
FIBER ONLY (EXISTING DC POWER)	Hybrid cable MN:HB058-M12-050F	
,	12x multi-mode fiber pairs, Top:Outdoor protected connectors, Bottom:LC	50 ft
	Connectors, 5/8 cable, 50 ft	
	MN:HB058-M12-075F	75 ft
	MN:HB058-M12-100F	100 ft
	MN:HB058-M12-125F	125 ft
	MN:HB058-M12-150F	150 ft
	MN:HB058-M12-175F	175 ft
	MN:HB058-M12-200F	200 ft

8 AWG Power	Hybrid cable	
	MN:HB114-08U3M12-050F	50 ft
	3x 8 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 50 ft	30 11
	MN:HB114-08U3M12-075F	75 ft
	MN:HB114-08U3M12-100F	100 ft
	MN:HB114-08U3M12-125F	125 ft
	MN:HB114-08U3M12-150F	150 ft
	MN:HB114-08U3M12-175F	175 ft
	MN:HB114-08U3M12-200F	200 ft
6 AWC Power	Hybrid cable	

	MN:HB114-13U3M12-225F  3x 6 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 225 ft	225 ft
	MN:HB114-13U3M12-250F	250 ft
	MN:HB114-13U3M12-275F	275 ft
	MN:HB114-13U3M12-300F	300 ft
4 AWG Power	Hybrid cable	
4 AVVG Power	Hybrid cable	
	MN:HB114-21U3M12-325F	325 ft
	3x 4 AWG power pairs, 12x multi-mode fiber pairs, Outdoor rated connectors & LC connectors. 1 1/4 cable, 325 ft	
	MN:HB114-21U3M12-350F	350 ft
	MN:HB114-21113M12-375E	375 ft

### RFS HYBRIFLEX JUMPER CABLE SCHEDULE

Hybrid Jumper cable MN:HBF012-M3-5F1

	5 ft, 3x multi-mode fiber pairs, Outdoor & LC connectors, 1/2 cable	
	MN:HBF012-M3-10F1	10 ft
	MN:HBF012-M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE:	
	JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15	,
	NOTIFY SPRINT CM OF ANY DISCREPANCY	
8 AWG POWER	Hybrid Jumper cable	
	MN:HBF058-08U1M3-5F1	5 ft
	5 ft, 1x 8 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 5/8 cable	511
	MN:HBF058-08U1M3-10F1	10 ft
	MN:HBF058-08U1M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE:	
	JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15	,
	NOTIFY SPRINT CM OF ANY DISCREPANCY	
6 AWG POWER	Hybrid lumper cable	-

	NOTIFY SPRINT CM OF ANY DISCREPANCY	
6 AWG POWER	Hybrid Jumper cable MN:HBF058-13U1M3-5F1 5 ft, 1 x 6 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 5/8 cable	5 ft
	MN:HBF058-13U1M3-10F1	10 ft
	MN:HBF058-13U1M3-15F1	15 ft
	SPECIAL INSTALLATION NOTE:  JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED  NOTIFY SPRINT CM OF ANY DISCREPANCY	15'
4 AWG POWER	Hybrid Jumper cable MN:HBF078-21U1M3-5F1 5 ft, 1x 4 AWG power pair, 3x multi-mode fiber pairs, Outdoor & LC connectors, 7/8 cable	5 ft
	MN:HBF078-21U1M3-10F1	10 ft

JUMPERS FROM 2.5 RRH TO 2.5 ANTENNA SHALL NOT EXCEED 15'

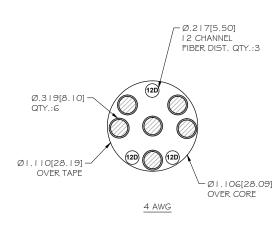
SPECIAL INSTALLATION NOTE

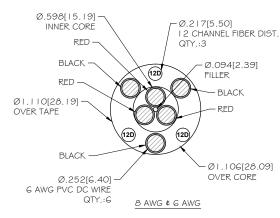
NOTIFY SPRINT CM OF ANY DISCREPANCY

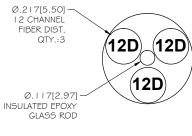
\*NOTE: SPRINT CM TO CONFIRM HYBRID/FIBER RISER CABLE \$ HYBRID/FIBER

JUMPER CABLE MODEL NUMBERS BEFORE PREPARING BOM.









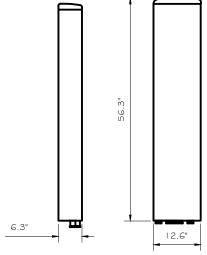
FIBER ONLY

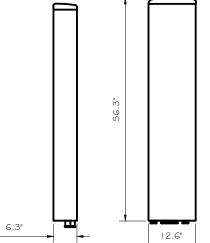
### RFS: APXV9TM14-ALU-120

56.3" x 12.6" x 6.3" DIMENSIONS, HxWxD:

55.12 lbs. WEIGHT, WITHOUT PRE-MOUNTED BRACKETS:

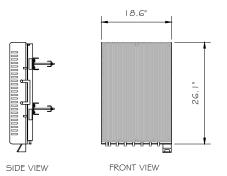
(9) MINI-DIN FEMALE/BOTTOM CONNECTOR:

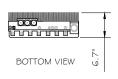




2.5 ANTENNA DETAIL

SCALE: NTS





ALCATEL-LUCENT: TD-RRH8x20

 $HxWxD = 26.1" \times 18.6" \times 6.7"$ 

WEIGHT = 70 lbs.

2.5 RRH DETAIL SCALE: NTS



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MARK	DATE	DESCRIPTION

HASE FINAL

DATE 07/14/2014

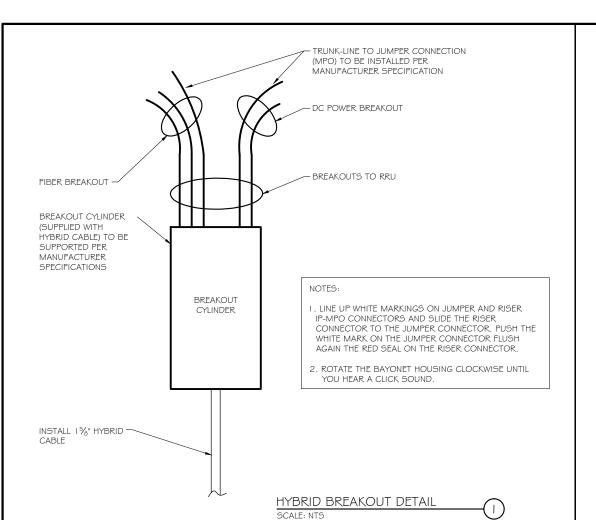
### AVON MOUNTAIN CTO3XCO53-A

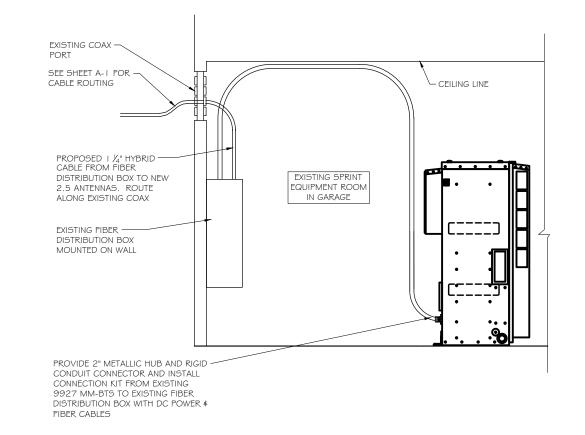
PROJECT INFORMATION: 8 I MONTEVIDEO ROAD AVON, CT 06001 HARTFORD COUNTY

ANTENNA \$ HYBRID CABLE DETAILS

SCALE: AS NOTED

22984 SHEET A-7



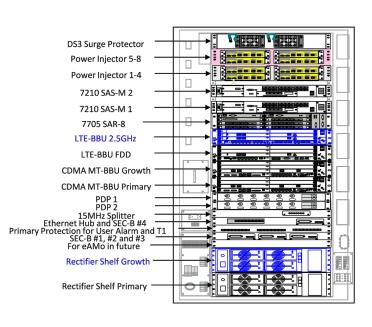


CABLE ROUTE FROM CABINET SCALE: NTS

PROPOSED BATTERY STRING(S) TO BE INSTALLED IN EXISTING BATTERY CABINET



NSTALL NEW 2.5 EQUIPMENT, INCLUDING BASE BAND UNIT, CELL SITE ROUTER, RECTIFIERS, AND SURGE ARRESTORS AS NEEDED IN EXISTING MM-BTS CABINET



EXISTING MMBS CABINET SCALE: NTS

Sprint

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### AVON MOUNTAIN CTO3XCO53-A

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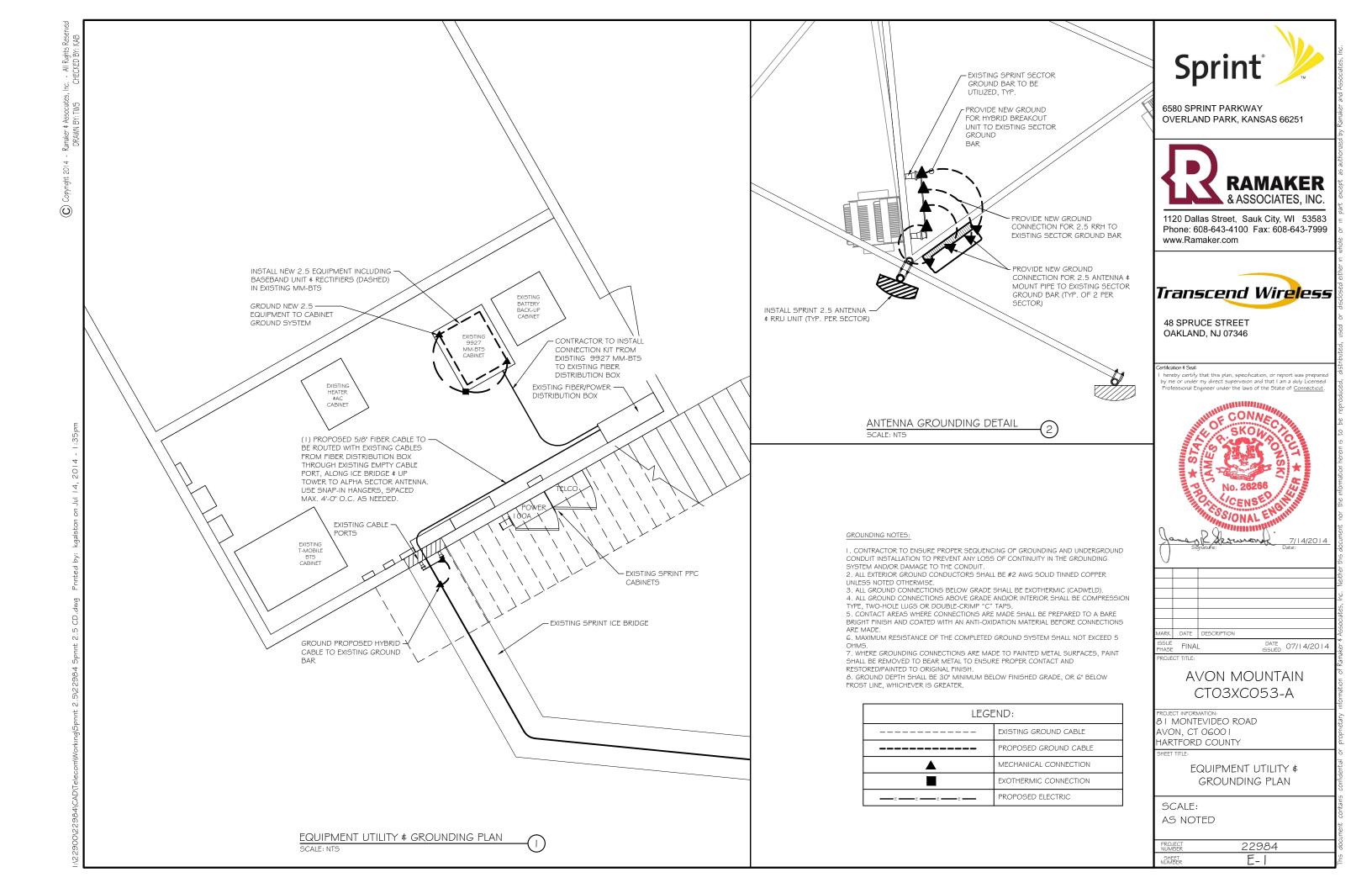
EQUIPMENT DETAILS

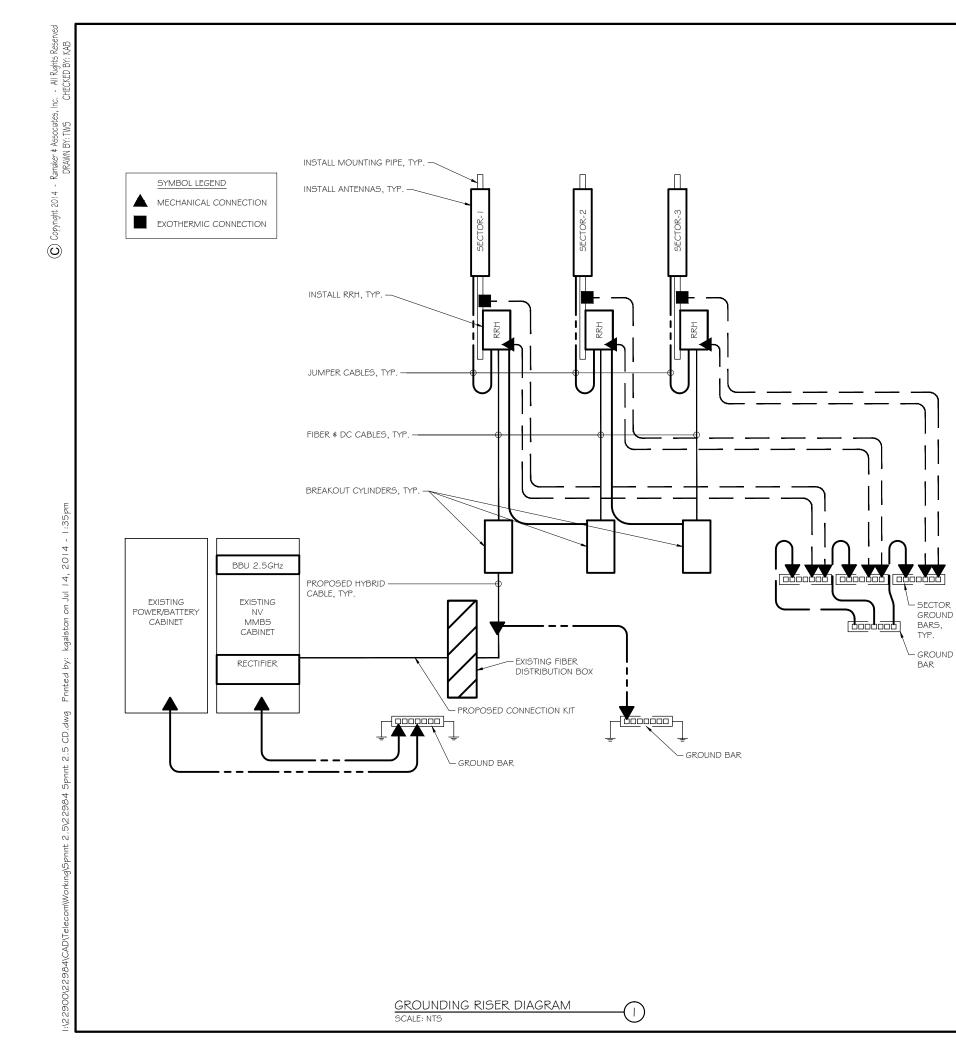
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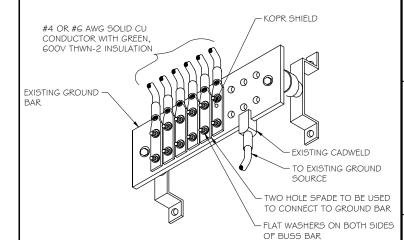
22984 SHEET A-8



EXISTING BBU CABINET SCALE: NTS



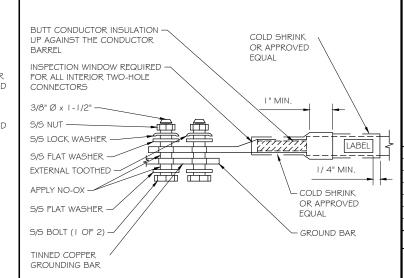




NOTES:
I. APPLY NO-OX TO LUG AND GROUND BAR CONTACT SURFACE. DO NOT COAT INLINE LUG.

2. IF STOLEN GROUND BARS ARE ENCOUNTERED, CONTACT SPRINT CM FOR REPLACEMENT THREADED

GROUNDING CONDUCTOR INSTALLATION





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PROJECT INFORMATION: 8 I MONTEVIDEO ROAD AVON, CT 06001 HARTFORD COUNTY

GROUNDING DETAILS

SCALE: AS NOTED

22984 E-2 SHEET

TWO-HOLE LUG SCALE: NTS

