April 7, 2015

Melanie A. Bachman
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

## RE: T-Mobile-Exempt Modification - Crown Site BU: 842856 <br> T-Mobile Site ID: CT11501E <br> Located at: 122 Jonathan Trumbull Highway (Route 6), Andover, CT 06232

Dear Ms. Bachman:
This letter and exhibits are submitted on behalf of T-Mobile. T-Mobile is making modifications to certain existing sites in its Connecticut system in order to implement their 700 MHz technology. Please accept this letter and exhibits as notification, pursuant to § 16-50j73 of the Regulations of Connecticut State Agencies ("R.C.S.A."), of construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In compliance with R.C.S.A. § $16-50 j-73$, a copy of this letter is being sent to The Honorable Robert Burbank, First Selectman for the Town of Andover, and ASC Real Estate, Inc., Property Owner.

T-Mobile plans to modify the existing wireless communications facility owned by Crown Castle and located at $\mathbf{1 2 2}$ Jonathan Trumbull Highway (Route 6), Andover, CT 06232. Attached are a compound plan and elevation depicting the planned changes (Exhibit-1), and documentation of the structural sufficiency of the structure to accommodate the revised antenna configuration (Exhibit-2). Also included is a power density table report reflecting the modification to T-Mobile's operations at the site (Exhibit-3).

The changes to the facility do not constitute a modification as defined in Connecticut General Statutes ("C.G.S.") § 16-50i(d) because the general physical characteristics of the facility will not be significantly changed. Rather, the planned changes to the facility fall squarely within those activities explicitly provided for in the R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing tower. T-Mobile's replacement antennas will be located at the same elevation on the existing tower.
2. There will be no proposed modifications to the ground and no extension of boundaries.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more.
4. The operation of the replacement antennas will not increase radio frequency (RF) emissions at the facility to a level at or above the Federal Communications Commission (FCC) adopted safety standard. A cumulative General Power Density table report for T-Mobile's modified facility is included as Exhibit-3.
5. A Structural Modification Report confirming that the tower and foundation can support T-Mobile's proposed modifications is included as Exhibit-2.

For the foregoing reasons, T-Mobile respectfully submits the proposed modifications to the above-reference telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Sincerely,

Jerry Feathers
Real Estate Specialist

## Enclosure

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes
Tab 2: Exhibit-2: Structural Modification Report
Tab 3: Exhibit-3: General Power Density Table Report (RF Emissions Analysis Report)

cc: The Honorable Robert Burbank, First Selectman<br>Andover Town Office<br>17 School Road<br>Andover, CT 06232

ASC Real Estate Inc.
P.O. Box 122

Andover, CT 06232

## T-MOBILE NORTHEAST LLC

T-MOBILE SITE \#: CT11501E CROWN CASTLE BU \#: 842856 SITE NAME: ANDOVER NORTH 122 JONATHAN TRUMBULL HIGHWAY (ROUTE 6) ANDOVER, CT 06232 TOLLAND COUNTY

CT11501E ANDOVER NORTH


EENERAL MOTES





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PARSIPPANY, NJ 07054

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ER: 50066258

| Job NUMER: | 50071485 |
| :--- | :--- | :--- |

22 JONATHAN TRUMBUL
HIGHWAY (ROUTE 6)
ANDOVER, CT 06232
TOLLAND COUNTY
SHEET TILE
general notes
Sheer number
$G-1$












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TYPICAL ANTENNA GROUNDING DETAIL
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SCHEMATIC GROUNDING DIAGRAM


22 JONATHAN TRUMBU HIGHWAY (ROUTE 6) ANDOVER, CT 06232 TOLLAND COUNTY SHEET TILE

GROUNDING NOTES \& DETAILS
$\qquad$

Date: March 13, 2015
GPD Engineering and Architecture Professional Corporation
Marianne Dunst
Crown Castle
3530 Toringdon Way Suite 300
Charlotte, NC 28277
(704) 405-6580

Subject:
Carrier Designation:
GPD
520 South Main Street, Suite 2531
Akron, OH 44311
(614) 859-1607
dpalkovic@gpdgroup.com

Structural Analysis Report

## T-Mobile Co-Locate Carrier Site Name:

 Carrier Site Number: CT11501ECrown Castle BU Number: Crown Castle Site Name: Crown Castle JDE Job Number: Crown Castle Work Order Number: Crown Castle Application Number:

GPD Group Project Number:
842856
325627
1022391
282530 Rev. 1

CT501/ATT Andover - Prime

ANDOVER NORTH
2015777.842856.01

122 Jonathan Trumbull Hwy (Rte 6), Andover, CT 06232, Tolland County Latitude $41^{\circ} 45^{\prime} 0.46^{\prime \prime}$, Longitude $-72^{\circ} 24^{\prime} 9.63^{\prime \prime}$
149 Foot - Modified EEI Monopole Tower

Dear Marianne Dunst,
GPD is pleased to submit this "Structural Analysis Report" to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural 'Statement of Work' and the terms of Crown Castle Purchase Order Number 764705, in accordance with application 282530, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

```
LC5: Existing + Proposed Equipment
Note: See Table I and Table II for the proposed and existing/reserved loading, respectively.
```


## Sufficient Capacity

The analysis has been performed in accordance with the TIA/EIA-222-F standard and the 2005 CT State Building Code based upon a wind speed of 85 mph fastest mile.

We at GPD appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects please give us a call.

Structural analysis prepared by: Elizabeth Boaz, El
Respectfully submitted by:

John N. Kabak, P.E.
Connecticut \#: PEN. 0028336


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## 1) INTRODUCTION

The existing tower consists of four major sections connected by slip joints. It has an 18 -sided cross section and is evenly tapered from $47.5^{\prime \prime}$ (flat-flat) at the base to $21.5^{\prime \prime}$ (flat-flat) at the top. It is galvanized and doesn't have aviation lighting.

This tower is a 149 ft Monopole tower designed by EEI in November of 2003. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-F.

The modifications designed by GPD (Project \#: 2009260.48, dated 01/29/2009), consisting of adding base plate stiffeners, have been considered in this analysis.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA/EIA-222-F Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a fastest mile wind speed of 85 mph with no ice, 38 mph with 1.25 inch ice thickness (in accordance with ASCE-7 ice conditions) and 50 mph under service loads.

Table 1 - Proposed Antenna and Cable Information

| Mounting <br> Level (ft) | Center <br> Line <br> Elevation <br> (ft) | Number <br> of <br> Antennas | Antenna <br> Manufacturer | Antenna Model | Number <br> of Feed <br> Lines | Feed <br> Line <br> Size (in) | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 140.0 | 140.0 | 3 | Andrew | MC-HPM1250-B Mount |  |  |  |
|  |  | 3 | Commscope | ATBT-BOTTOM-24V |  |  |  |

Table 2 - Existing and Reserved Antenna and Cable Information

| Mounting Level (ft) | Center Line Elevation $(\mathrm{ft})$ | Number of Antennas | Antenna Manufacturer | Antenna Model | Number of Feed Lines |  | Note |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 149.0 | 151.0 | 3 | Ericsson | RRUS-11 | $\begin{aligned} & 6 \\ & 2 \\ & 1 \end{aligned}$ | $\begin{gathered} 1-1 / 4 \\ 7 / 8 \\ 1 / 2 \end{gathered}$ |  |
|  |  | 3 | KMW <br> Communications | AM-X-CD-16-65-00T-RET |  |  |  |
|  |  | 3 | Powerwave <br> Technologies | 7770.00 |  |  |  |
|  |  | 6 | Powerwave Technologies | LGP17201 |  |  |  |
|  |  | 6 | Powerwave Technologies | LGP21901 |  |  |  |
|  |  | 1 | Raycap | DC6-48-60-18-8F |  |  |  |
|  | 149.0 | 1 |  | T-Arm Mount [TA 702-3] |  |  |  |
| 140.0 | 140.0 | 1 |  | Side Arm Mount [SO 1023] |  |  | 1 |
|  |  | 3 | RFS Celwave | APX16PV-16PVL | 12 | 1-5/8 | 2 |
|  |  | 6 | RFS Celwave | ATMAA1412D-1A20 |  |  |  |
| 130.0 | 130.0 | 1 |  | Pipe Mount [PM 602-3] | 6 | 1-5/8 | 3 |
|  |  | 3 | Kathrein | 742213 |  |  |  |

Notes:

1) Existing equipment to be removed; not considered in this analysis.
2) Existing equipment to be relocated to the proposed mount and reused. Coax to remain.
3) Abandoned equipment.
tnxTower Report - version 6.1.4.1

## 3) ANALYSIS PROCEDURE

Table 3 - Documents Provided

| Document | Remarks | Reference | Source |
| :---: | :---: | :---: | :---: |
| Tower Drawings | EEI Project \#: 12026, dated <br> $11 / 29 / 2003$ | 4713188 | CCISITES |
| Foundation Drawings | EEI Project \#: 12026, dated <br> 12/02/2003 | 4529267 | CCISITES |
| Geotechnical Report | VN Engineers Project \#: 23-120G, <br> dated 10/17/2003 | 4713186 | CCISITES |
| Modification Drawings | GPD Job \#: 2009260.48, dated <br> $01 / 29 / 2009$ | 4713190 | CCISITES |
| Post Modification Inspection | GPD Job \#: 2009513.00, dated <br> $03 / 18 / 2009$ | 4713189 | CCISITES |

## 3.1) Analysis Method

tnxTower (version 6.1.4.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

## 3.2) Assumptions

1) Tower and structures were built in accordance with the manufacturer's specifications.
2) The tower and structures have been maintained in accordance with the manufacturer's specification.
3) When applicable, transmission cables are considered as structural components for calculating wind loads as allowed by TIA/EIA-222-F.

This analysis may be affected if any assumptions are not valid or have been made in error. GPD Group should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

Table 5 - Section Capacity (Summary)

| Section No. | Elevation (ft) | Component Type | Size | Critical Element | P (K) | $\underset{(\mathrm{K})}{\mathrm{SF}^{\star} \mathrm{P}_{\text {_ }} \text { allow }}$ |  | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 149-123.612 | Pole | TP26.2021×21.5×0.1875 | 1 | -2.99 | 783.22 | 31.2 | Pass |
| L2 | $\begin{gathered} 123.612- \\ 79.128 \end{gathered}$ | Pole | TP33.9598×25.1277×0.1875 | 2 | -6.66 | 943.73 | 87.4 | Pass |
| L3 | $\begin{gathered} 79.128- \\ 43.243 \end{gathered}$ | Pole | TP40.1211x32.7164×0.25 | 3 | -11.28 | 1578.47 | 80.2 | Pass |
| L4 | 43.243-0 | Pole | TP47.5x38.6156x0.3125 | 4 | -20.15 | 2426.74 | 76.0 | Pass |
|  |  |  |  |  |  | Summary | ELC: | LC5 |
|  |  |  |  |  |  | Pole (L2) | 87.4 | Pass |
|  |  |  |  |  |  | Rating = | 87.4 | Pass |

Table 6 - Tower Component Stresses vs. Capacity - LC5

| Notes | Component | Elevation (ft) | \% Capacity | Pass / Fail |
| :---: | :---: | :---: | :---: | :---: |
| 1 | Anchor Rods | 0 | 64.1 | Pass |
| 1 | Base Plate | 0 | 82.4 | Pass |
| 1 | Base Foundation | 0 | 29.7 | Pass |
| 1 | Base Foundation <br> Soil Interaction | 0 | 61.5 | Pass |


| Structure Rating (max from all components) $=$ | $87.4 \%$ |
| :--- | :--- |

Notes:

1) See additional documentation in "Appendix C - Additional Calculations" for calculations supporting the \% capacity consumed.

## 4.1) Recommendations

The existing tower and its foundation are sufficient for the proposed loading and do not require modifications.

## 5) DISCLAIMER OF WARRANTIES

GPD GROUP has not performed a site visit to the tower to verify the member sizes or antenna/coax loading. If the existing conditions are not as represented on the tower elevation contained in this report, we should be contacted immediately to evaluate the significance of the discrepancy. This is not a condition assessment of the tower or foundation. This report does not replace a full tower inspection. The tower and foundations are assumed to have been properly fabricated, erected, maintained, in good condition, twist free, and plumb.

The engineering services rendered by GPD GROUP in connection with this Structural Analysis are limited to a computer analysis of the tower structure and theoretical capacity of its main structural members. No allowance was made for any damaged, bent, missing, loose, or rusted members (above and below ground). No allowance was made for loose bolts or cracked welds.

This analysis is limited to the designated maximum wind and seismic conditions per the governing tower standards and code. Wind forces resulting in tower vibrations near the structure's resonant frequencies were not considered in this analysis and are outside the scope of this analysis. Lateral loading from any dynamic response was not evaluated under a time-domain based fatigue analysis.

GPD GROUP does not analyze the fabrication of the structure (including welding). It is not possible to have all the very detailed information needed to perform a thorough analysis of every structural sub-component and connection of an existing tower. GPD GROUP provides a limited scope of service in that we cannot verify the adequacy of every weld, plate connection detail, etc. The purpose of this report is to assess the capability of adding appurtenances usually accompanied by transmission lines to the structure.

It is the owner's responsibility to determine the amount of ice accumulation in excess of the code specified amount, if any, that should be considered in the structural analysis.

The attached sketches are a schematic representation of the analyzed tower. If any material is fabricated from these sketches, the contractor shall be responsible for field verifying the existing conditions, proper fit, and clearance in the field. Any mentions of structural modifications are reasonable estimates and should not be used as a precise construction document. Precise modification drawings are obtainable from GPD GROUP, but are beyond the scope of this report.

Miscellaneous items such as antenna mounts, etc., have not been designed or detailed as a part of our work. We recommend that material of adequate size and strength be purchased from a reputable tower manufacturer.

Towers are designed to carry gravity, wind, and ice loads. All members, legs, diagonals, struts, and redundant members provide structural stability to the tower with little redundancy. Absence or removal of a member can trigger catastrophic failure unless a substitute is provided before any removal. Legs carry axial loads and derive their strength from shorter unbraced lengths by the presence of redundant members and their connection to the diagonals with bolts or welds. If the bolts or welds are removed without providing any substitute to the frame, the leg is subjected to a higher unbraced length that immediately reduces its load carrying capacity. If a diagonal is also removed in addition to the connection, the unbraced length of the leg is greatly increased, jeopardizing its load carrying capacity. Failure of one leg can result in a tower collapse because there is no redundancy. Redundant members and diagonals are critical to the stability of the tower.

GPD GROUP makes no warranties, expressed and/or implied, in connection with this report and disclaims any liability arising from material, fabrication, and erection of this tower. GPD GROUP will not be responsible whatsoever for, or on account of, consequential or incidental damages sustained by any person, firm, or organization as a result of any data or conclusions contained in this report. The maximum liability of GPD GROUP pursuant to this report will be limited to the total fee received for preparation of this report.

## APPENDIX A

TNXTOWER OUTPUT



TORQUE 1 kip-ft 38 mph WIND - 1.2500 in ICE AXIAL


TORQUE 4 kip-ft REACTIONS - 85 mph WIND


GPD Group
520 South Main Street, Suite 2531
Akron, OH 44311
Phone: (330) 572-2100
FAX: (330) 572-2101
${ }^{\text {Iob: }}$ ANDOVER NORTH / BU\#: 842856
Project: 2015777.842856.01
Client: Crown Castle USA, Inc. Drawn by: EBoaz App'd:

Feed Line Distribution Chart
0' - 149'
Flat $\qquad$ App In Face $\qquad$
$\qquad$ Truss Leg


| tnxTower | Job ANDOVER NORTH / BU\#: 842856 |  | $\begin{aligned} & \text { Page } \\ & \\ & \hline \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2015777.842856 .01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:26:19 03/13/15 } \end{array}$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |

## Tower Input Data

There is a pole section.
This tower is designed using the TIA/EIA-222-F standard.
The following design criteria apply:
Tower is located in Tolland County, Connecticut.
Basic wind speed of 85 mph .
Nominal ice thickness of 1.2500 in.
Ice thickness is considered to increase with height.
Ice density of 56 pcf .
A wind speed of 38 mph is used in combination with ice.
Temperature drop of $50^{\circ} \mathrm{F}$.
Deflections calculated using a wind speed of 50 mph .
A non-linear (P-delta) analysis was used.
Pressures are calculated at each section.
Stress ratio used in pole design is 1.333 .
Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

|  | Consider Moments - Legs |
| :--- | :--- |
|  | Consider Moments - Horizontals |
|  | Consider Moments - Diagonals |
|  | Use Moment Magnification |
| $\sqrt{ }$ | Use Code Stress Ratios |
| $\sqrt{ }$ Use Code Safety Factors - Guys |  |
| $\sqrt{ }$ Escalate Ice |  |
|  | Always Use Max Kz |
|  | Use Special Wind Profile |
|  | Include Bolts In Member Capacity |
| Leg Bolts Are At Top Of Section |  |
| Secondary Horizontal Braces Leg |  |
|  | Use Diamond Inner Bracing (4 Sided) |
|  | Add IBC $.6 \mathrm{D}+$ W Combination |

Distribute Leg Loads As Uniform Assume Legs Pinned
$\sqrt{ }$ Assume Rigid Index Plate
$\sqrt{ }$ Use Clear Spans For Wind Area
$\sqrt{ }$ Use Clear Spans For KL/r Retension Guys To Initial Tension
$\sqrt{ }$ Bypass Mast Stability Checks
$\sqrt{ }$ Use Azimuth Dish Coefficients
$\sqrt{ }$ Project Wind Area of Appurt. Autocalc Torque Arm Areas SR Members Have Cut Ends
$\sqrt{ }$ Sort Capacity Reports By Component Triangulate Diamond Inner Bracing Use TIA-222-G Tension Splice Capacity Exemption

Treat Feedline Bundles As Cylinder Use ASCE 10 X-Brace Ly Rules
Calculate Redundant Bracing Forces Ignore Redundant Members in FEA
SR Leg Bolts Resist Compression
All Leg Panels Have Same Allowable
Offset Girt At Foundation
$\checkmark$ Consider Feedline Torque
Include Angle Block Shear Check Poles
$\sqrt{ }$ Include Shear-Torsion Interaction
Always Use Sub-Critical Flow Use Top Mounted Sockets

## Tapered Pole Section Geometry

| Section | Elevation <br> ft | Section <br> Length <br> ft | Splice Length ft | Number <br> of Sides | Top Diameter in | Bottom Diameter in | Wall <br> Thickness in | Bend Radius in | Pole Grade |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 149.00-123.61 | 25.39 | 3.78 | 18 | 21.5000 | 26.2021 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L2 | 123.61-79.13 | 48.26 | 4.75 | 18 | 25.1277 | 33.9598 | 0.1875 | 0.7500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L3 | 79.13-43.24 | 40.63 | 5.52 | 18 | 32.7164 | 40.1211 | 0.2500 | 1.0000 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |
| L4 | 43.24-0.00 | 48.76 |  | 18 | 38.6156 | 47.5000 | 0.3125 | 1.2500 | $\begin{gathered} \text { A572-65 } \\ (65 \mathrm{ksi}) \end{gathered}$ |


| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | ANDOVER NORTH / BU\#: 842856 |  | $\text { Page } 2 \text { of } 8$ |
| :---: | :---: | :---: | :---: |
|  | Project | 2015777.842856.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:26:19 03/13/15 } \end{array}$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |

## Tapered Pole Properties

| Section | Tip Dia. in | $\begin{gathered} \text { Area } \\ i n^{2} \end{gathered}$ | $\begin{gathered} I \\ \mathrm{in}^{4} \end{gathered}$ | $\begin{gathered} r \\ i n \end{gathered}$ | $\begin{aligned} & C \\ & \text { in } \end{aligned}$ | $\begin{gathered} \mathrm{I} / C \\ i n^{3} \end{gathered}$ | $\begin{gathered} J \\ i n^{4} \end{gathered}$ | $\begin{gathered} I t / Q \\ i n^{2} \end{gathered}$ | $\begin{aligned} & w \\ & \text { in } \end{aligned}$ | $w / t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 21.8317 | 12.6836 | 727.8616 | 7.5659 | 10.9220 | 66.6418 | 1456.6810 | 6.3430 | 3.4540 | 18.421 |
|  | 26.6063 | 15.4819 | 1323.7230 | 9.2352 | 13.3107 | 99.4483 | 2649.1877 | 7.7424 | 4.2816 | 22.835 |
| L2 | 26.2171 | 14.8426 | 1166.4013 | 8.8538 | 12.7649 | 91.3757 | 2334.3374 | 7.4227 | 4.0925 | 21.827 |
|  | 34.4837 | 20.0987 | 2896.1934 | 11.9892 | 17.2516 | 167.8799 | 5796.1977 | 10.0513 | 5.6469 | 30.117 |
| L3 | 34.0992 | 25.7621 | 3430.7380 | 11.5256 | 16.6199 | 206.4230 | 6865.9902 | 12.8835 | 5.3181 | 21.272 |
|  | 40.7400 | 31.6377 | 6354.1730 | 14.1542 | 20.3815 | 311.7615 | 12716.7070 | 15.8219 | 6.6213 | 26.485 |
| L4 | 40.2321 | 37.9919 | 7042.0272 | 13.5976 | 19.6167 | 358.9804 | 14093.3205 | 18.9996 | 6.2464 | 19.988 |
|  | 48.2328 | 46.8041 | 13166.6503 | 16.7516 | 24.1300 | 545.6548 | 26350.6256 | 23.4065 | 7.8100 | 24.992 |

## Feed Line/Linear Appurtenances - Entered As Area

\begin{tabular}{|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Allow \\
Shield
\end{tabular} \& Component Type \& \begin{tabular}{l}
Placement \\
ft
\end{tabular} \& Total Number \& \& \(C_{A} A_{A}\)

$f t^{2} / f t$ \& | Weight |
| :--- |
| plf | <br>

\hline \multirow[t]{5}{*}{Climbing Pegs} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{149.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.01 \& 0.31 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.12 \& 0.71 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.22 \& 1.71 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.41 \& 5.56 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.82 \& 20.59 <br>
\hline \multirow[t]{5}{*}{Safety Line (3/8")} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{CaAa (Out Of Face)} \& \multirow[t]{5}{*}{149.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.04 \& 0.22 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.14 \& 0.75 <br>
\hline \& \& \& \& \& \& $1{ }^{\prime \prime}$ Ice \& 0.24 \& 1.28 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.44 \& 2.34 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.84 \& 4.46 <br>
\hline \multirow[t]{5}{*}{LDF4-50A (1/2 FOAM)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{149.00-8.00} \& \multirow[t]{5}{*}{1} \& No Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 0.00 \& 0.15 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.00 \& 0.15 <br>
\hline \multirow[t]{5}{*}{LDF5-50A (7/8 FOAM)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{149.00-8.00} \& \multirow[t]{5}{*}{2} \& No Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 0.00 \& 0.33 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 0.00 \& 0.33 <br>
\hline \multirow[t]{5}{*}{LDF6-50A (1-1/4 FOAM)} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{149.00-8.00} \& \multirow[t]{5}{*}{6} \& No Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.66 <br>
\hline \& \& \& \& \& \& 1" Ice \& 0.00 \& 0.66 <br>

\hline \& \& \& \& \& \& $$
2^{\prime \prime} \text { Ice }
$$ \& 0.00 \& 0.66 <br>

\hline \& \& \& \& \& \& 4 " Ice \& 0.00 \& 0.66 <br>
\hline \multirow[t]{5}{*}{AVA7-50(1-5/8)} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{140.00-8.00} \& \multirow[t]{5}{*}{3} \& No Ice \& 0.00 \& 0.70 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.70 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 0.00 \& 0.70 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.00 \& 0.70 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.00 \& 0.70 <br>
\hline \multirow[t]{5}{*}{LDF7-50A (1-5/8 FOAM)} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{140.00-8.00} \& \multirow[t]{5}{*}{9} \& No Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 0.00 \& 0.82 <br>
\hline \multirow[t]{5}{*}{LDF7-50A (1-5/8 FOAM)} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{No} \& \multirow[t]{5}{*}{Inside Pole} \& \multirow[t]{5}{*}{130.00-8.00} \& \multirow[t]{5}{*}{6} \& No Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& $1^{\prime \prime}$ Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.00 \& 0.82 <br>
\hline \& \& \& \& \& \& 4" Ice \& 0.00 \& 0.82 <br>
\hline
\end{tabular}

| tnxTower <br> GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | ANDOVER NORTH / BU\#: 842856 |  | Page 3 of 8 |
| :---: | :---: | :---: | :---: |
|  | Project | 2015777.842856 .01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:26:19 03/13/15 } \end{array}$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |

## Discrete Tower Loads

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& Face or Leg \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& Azimuth Adjustment \& Placement

$f t$ \& \& | $C_{A} A_{A}$ |
| :--- |
| Front |
| $f t^{2}$ | \& | $C_{A} A_{A}$ |
| :--- |
| Side |
| $f t^{2}$ | \& Weight

K <br>
\hline \multirow[t]{5}{*}{T-Arm Mount [TA 702-3]} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{None} \& \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 5.64 \& 5.64 \& 0.34 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 6.55 \& 6.55 \& 0.43 <br>
\hline \& \& \& \& \& \& 1 " Ice \& 7.46 \& 7.46 \& 0.52 <br>
\hline \& \& \& \& \& \& 2" Ice \& 9.28 \& 9.28 \& 0.70 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 12.92 \& 12.92 \& 1.06 <br>
\hline \multirow[t]{5}{*}{7770.00 w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 6.22 \& 4.35 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.77 \& 5.20 \& 0.11 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.30 \& 5.92 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& 8.38 \& 7.41 \& 0.29 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.69 \& 10.76 \& 0.68 <br>
\hline \multirow[t]{5}{*}{7770.00 w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 6.22 \& 4.35 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.77 \& 5.20 \& 0.11 <br>
\hline \& \& \& 2.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.30 \& 5.92 \& 0.16 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 8.38 \& 7.41 \& 0.29 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 10.69 \& 10.76 \& 0.68 <br>
\hline \multirow[t]{5}{*}{7770.00 w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 6.22 \& 4.35 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 6.77 \& 5.20 \& 0.11 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 7.30 \& 5.92 \& 0.16 <br>
\hline \& \& \& \& \& \& 2" Ice \& 8.38 \& 7.41 \& 0.29 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.69 \& 10.76 \& 0.68 <br>
\hline \multirow[t]{5}{*}{AM-X-CD-16-65-00T-RET w/ Mount Pipe} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 8.50 \& 6.30 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 9.15 \& 7.48 \& 0.14 <br>
\hline \& \& \& 2.00 \& \& \& 1 " Ice \& 9.77 \& 8.37 \& 0.21 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 11.03 \& 10.18 \& 0.38 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 13.68 \& 14.02 \& 0.87 <br>
\hline \multirow[t]{5}{*}{AM-X-CD-16-65-00T-RET w/ Mount Pipe} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 8.50 \& 6.30 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 9.15 \& 7.48 \& 0.14 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.77 \& 8.37 \& 0.21 <br>
\hline \& \& \& \& \& \& 2 " Ice \& 11.03 \& 10.18 \& 0.38 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 13.68 \& 14.02 \& 0.87 <br>
\hline \multirow[t]{5}{*}{AM-X-CD-16-65-00T-RET w/ Mount Pipe} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 8.50 \& 6.30 \& 0.07 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 9.15 \& 7.48 \& 0.14 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 9.77 \& 8.37 \& 0.21 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 11.03 \& 10.18 \& 0.38 <br>
\hline \& \& \& \& \& \& 4 " Ice \& 13.68 \& 14.02 \& 0.87 <br>
\hline \multirow[t]{5}{*}{(2) LGP17201} \& \multirow[t]{5}{*}{A} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 1.95 \& 0.52 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.13 \& 0.64 \& 0.04 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.33 \& 0.77 \& 0.06 <br>
\hline \& \& \& \& \& \& $2^{\prime \prime}$ Ice \& 2.75 \& 1.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.69 \& 1.73 \& 0.19 <br>
\hline \multirow[t]{5}{*}{(2) LGP17201} \& \multirow[t]{5}{*}{B} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 1.95 \& 0.52 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.13 \& 0.64 \& 0.04 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.33 \& 0.77 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.75 \& 1.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.69 \& 1.73 \& 0.19 <br>
\hline \multirow[t]{5}{*}{(2) LGP17201} \& \multirow[t]{5}{*}{C} \& \multirow[t]{5}{*}{From Leg} \& 3.00 \& \multirow[t]{5}{*}{0.0000} \& \multirow[t]{5}{*}{149.00} \& No Ice \& 1.95 \& 0.52 \& 0.03 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 2.13 \& 0.64 \& 0.04 <br>
\hline \& \& \& 2.00 \& \& \& $1^{\prime \prime}$ Ice \& 2.33 \& 0.77 \& 0.06 <br>
\hline \& \& \& \& \& \& 2" Ice \& 2.75 \& 1.06 \& 0.09 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.69 \& 1.73 \& 0.19 <br>
\hline \multirow[t]{4}{*}{(2) LGP21901} \& \multirow[t]{4}{*}{A} \& \multirow[t]{4}{*}{From Leg} \& 3.00 \& \multirow[t]{4}{*}{0.0000} \& \multirow[t]{4}{*}{149.00} \& No Ice \& 0.27 \& 0.18 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.34 \& 0.25 \& 0.01 <br>
\hline \& \& \& 2.00 \& \& \& 1 " Ice \& 0.43 \& 0.32 \& 0.01 <br>
\hline \& \& \& \& \& \& 2" Ice \& 0.62 \& 0.49 \& 0.02 <br>
\hline
\end{tabular}

| tnxTower | ANDOVER NORTH / BU\#: 842856 |  | Page 4 of 8 |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Suite 2531 | Project | 2015777.842856.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:26:19 03/13/15 } \end{array}$ |
| Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Client | Crown Castle USA, Inc. | Designed by EBoaz |

\begin{tabular}{|c|c|c|c|c|c|c|c|c|c|}
\hline Description \& \[
\begin{gathered}
\text { Face } \\
\text { or } \\
\text { Leg }
\end{gathered}
\] \& \begin{tabular}{l}
Offset \\
Type
\end{tabular} \& \begin{tabular}{l}
Offsets: \\
Horz \\
Lateral \\
Vert \\
\(f t\) \\
\(f t\) \\
ft
\end{tabular} \& \begin{tabular}{l}
Azimuth Adjustment \\
0
\end{tabular} \& Placement

$f t$ \& \& $C_{A} A_{A}$
Front

$f t^{2}$ \& $C_{A} A_{A}$
Side

$f t^{2}$ \& Weight <br>
\hline \multirow{6}{*}{(2) LGP21901} \& \multirow{5}{*}{B} \& \multirow{4}{*}{From Leg} \& \& \multirow{4}{*}{0.0000} \& \multirow{4}{*}{149.00} \& 4" Ice \& 1.10 \& 0.94 \& 0.07 <br>
\hline \& \& \& 3.00 \& \& \& No Ice \& 0.27 \& 0.18 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.34 \& 0.25 \& 0.01 <br>
\hline \& \& \& 2.00 \& \& \& 1 " Ice \& 0.43 \& 0.32 \& 0.01 <br>
\hline \& \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 2" Ice \& 0.62 \& 0.49 \& 0.02 <br>
\hline \& \multirow{4}{*}{C} \& \& \& \& \& 4" Ice \& 1.10 \& 0.94 \& 0.07 <br>
\hline \multirow[t]{5}{*}{(2) LGP21901} \& \& \& 3.00 \& \& \& No Ice \& 0.27 \& 0.18 \& 0.01 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 0.34 \& 0.25 \& 0.01 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 0.43 \& 0.32 \& 0.01 <br>
\hline \& \multirow{5}{*}{A} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 2" Ice \& 0.62 \& 0.49 \& 0.02 <br>
\hline \& \& \& \& \& \& 4" Ice \& 1.10 \& 0.94 \& 0.07 <br>
\hline \multirow[t]{5}{*}{RRUS-11} \& \& \& 3.00 \& \& \& No Ice \& 3.25 \& 1.37 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.49 \& 1.55 \& 0.07 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 3.74 \& 1.74 \& 0.09 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 2" Ice \& 4.27 \& 2.14 \& 0.15 <br>
\hline \& \& \& \& \& \& 4" Ice \& 5.43 \& 3.04 \& 0.31 <br>
\hline \multirow[t]{5}{*}{RRUS-11} \& \& \& 3.00 \& \& \& No Ice \& 3.25 \& 1.37 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.49 \& 1.55 \& 0.07 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 3.74 \& 1.74 \& 0.09 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 2" Ice \& 4.27 \& 2.14 \& 0.15 <br>
\hline \& \& \& \& \& \& 4" Ice \& 5.43 \& 3.04 \& 0.31 <br>
\hline \multirow[t]{5}{*}{RRUS-11} \& \& \& 3.00 \& \& \& No Ice \& 3.25 \& 1.37 \& 0.05 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 3.49 \& 1.55 \& 0.07 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 3.74 \& 1.74 \& 0.09 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{149.00} \& 2" Ice \& 4.27 \& 2.14 \& 0.15 <br>
\hline \& \& \& \& \& \& 4" Ice \& 5.43 \& 3.04 \& 0.31 <br>
\hline \multirow[t]{5}{*}{DC6-48-60-18-8F Surge Suppression Unit} \& \& \& 3.00 \& \& \& No Ice \& 1.47 \& 1.47 \& 0.02 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 1.67 \& 1.67 \& 0.04 <br>
\hline \& \& \& 2.00 \& \& \& 1" Ice \& 1.88 \& 1.88 \& 0.06 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{6}{*}{None} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{140.00} \& 2" Ice \& 2.33 \& 2.33 \& 0.11 <br>
\hline \& \& \& \& \& \& 4" Ice \& 3.38 \& 3.38 \& 0.24 <br>
\hline \multirow[t]{5}{*}{Commscope MC-HPM1250-B} \& \& \& \& \& \& No Ice \& 3.80 \& 3.80 \& 0.53 <br>
\hline \& \& \& \& \& \& 1/2" Ice \& 4.50 \& 4.50 \& 0.69 <br>
\hline \& \& \& \& \& \& 1" Ice \& 5.20 \& 5.20 \& 0.85 <br>
\hline \& \multirow{5}{*}{A} \& \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{140.00} \& 2" Ice \& 6.60 \& 6.60 \& 1.18 <br>
\hline \& \& \multirow{4}{*}{From Leg} \& \& \& \& 4" Ice \& 9.40 \& 9.40 \& 1.82 <br>
\hline \multirow[t]{5}{*}{APX16PV-16PVL w/ Mount Pipe} \& \& \& 2.00 \& \& \& No Ice \& 6.79 \& 3.05 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.23 \& 3.65 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 7.68 \& 4.27 \& 0.16 <br>
\hline \& \multirow{5}{*}{B} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{140.00} \& 2" Ice \& 8.60 \& 5.55 \& 0.28 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.54 \& 8.43 \& 0.63 <br>
\hline \multirow[t]{5}{*}{APX16PV-16PVL w/ Mount Pipe} \& \& \& 2.00 \& \& \& No Ice \& 6.79 \& 3.05 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.23 \& 3.65 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& 1" Ice \& 7.68 \& 4.27 \& 0.16 <br>
\hline \& \multirow{5}{*}{C} \& \multirow{5}{*}{From Leg} \& \& \multirow{5}{*}{0.0000} \& \multirow{5}{*}{140.00} \& 2" Ice \& 8.60 \& 5.55 \& 0.28 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.54 \& 8.43 \& 0.63 <br>
\hline \multirow[t]{5}{*}{APX16PV-16PVL w/ Mount Pipe} \& \& \& 2.00 \& \& \& No Ice \& 6.79 \& 3.05 \& 0.06 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 7.23 \& 3.65 \& 0.11 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 7.68 \& 4.27 \& 0.16 <br>
\hline \& \multirow{6}{*}{A} \& \multirow{7}{*}{From Leg} \& \& \multirow{7}{*}{0.0000} \& \multirow{7}{*}{140.00} \& 2" Ice \& 8.60 \& 5.55 \& 0.28 <br>
\hline \& \& \& \& \& \& 4" Ice \& 10.54 \& 8.43 \& 0.63 <br>
\hline \multirow[t]{5}{*}{LNX-6515DS-VTM w/ Mount Pipe} \& \& \& 2.00 \& \& \& No Ice \& 11.64 \& 9.79 \& 0.08 <br>
\hline \& \& \& 0.00 \& \& \& 1/2" Ice \& 12.34 \& 11.30 \& 0.17 <br>
\hline \& \& \& 0.00 \& \& \& $1{ }^{\prime \prime}$ Ice \& 13.04 \& 12.80 \& 0.27 <br>
\hline \& \& \& \& \& \& 2" Ice \& 14.48 \& 15.12 \& 0.50 <br>
\hline \& \& \& \& \& \& 4" Ice \& 17.71 \& 19.94 \& 1.14 <br>
\hline LNX-6515DS-VTM w/ Mount Pipe \& A \& From Leg \& 2.00 \& 0.0000 \& 140.00 \& No Ice \& 11.64 \& 9.79 \& 0.08 <br>
\hline
\end{tabular}

| tnxTower | ANDOVER NORTH / BU\#: 842856 |  | Page 5 |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2015777.842856.01 | $\begin{array}{\|l\|} \hline \text { Date } \\ \text { 14:26:19 03/13/15 } \end{array}$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |


| Description | $\begin{gathered} \text { Face } \\ \text { or } \\ \text { Leg } \end{gathered}$ | Offset <br> Type | Offsets: <br> Horz <br> Lateral <br> Vert <br> $f t$ <br> $f t$ <br> $f t$ | Azimuth Adjustment | Placement $f t$ |  | $C_{A} A_{A}$ <br> Front <br> $f t^{2}$ | $C_{A} A_{A}$ <br> Side <br> $f t^{2}$ | Weight <br> K |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LNX-6515DS-VTM w/ Mount Pipe |  |  | 0.00 |  |  | 1/2" Ice | 12.34 | 11.30 | 0.17 |
|  |  |  | 0.00 |  |  | 1 " Ice | 13.04 | 12.80 | 0.27 |
|  |  |  |  |  |  | 2" Ice | 14.48 | 15.12 | 0.50 |
|  |  |  |  |  |  | 4" Ice | 17.71 | 19.94 | 1.14 |
|  | A | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 11.64 | 9.79 | 0.08 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 12.34 | 11.30 | 0.17 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 13.04 | 12.80 | 0.27 |
|  |  |  |  |  |  | 2 " Ice | 14.48 | 15.12 | 0.50 |
|  |  |  |  |  |  | 4" Ice | 17.71 | 19.94 | 1.14 |
| (2) ATMAA1412D-1A20 | A | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 1.17 | 0.47 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 1.31 | 0.57 | 0.02 |
|  |  |  | 0.00 |  |  | $1{ }^{\prime \prime}$ Ice | 1.47 | 0.69 | 0.03 |
|  |  |  |  |  |  | 2 l Ice | 1.81 | 0.95 | 0.06 |
|  |  |  |  |  |  | 4 " Ice | 2.58 | 1.57 | 0.14 |
| (2) ATMAA1412D-1A20 | B | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 1.17 | 0.47 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 1.31 | 0.57 | 0.02 |
|  |  |  | 0.00 |  |  | 1 " Ice | 1.47 | 0.69 | 0.03 |
|  |  |  |  |  |  | 2 " Ice | 1.81 | 0.95 | 0.06 |
|  |  |  |  |  |  | 4" Ice | 2.58 | 1.57 | 0.14 |
| (2) ATMAA1412D-1A20 | C | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 1.17 | 0.47 | 0.01 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 1.31 | 0.57 | 0.02 |
|  |  |  | 0.00 |  |  | 1 " Ice | 1.47 | 0.69 | 0.03 |
|  |  |  |  |  |  | 2" Ice | 1.81 | 0.95 | 0.06 |
|  |  |  |  |  |  | 4" Ice | 2.58 | 1.57 | 0.14 |
| ATBT-BOTTOM-24V | A | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 0.12 | 0.08 | 0.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.17 | 0.12 | 0.00 |
|  |  |  | 0.00 |  |  | 1 " Ice | 0.23 | 0.17 | 0.01 |
|  |  |  |  |  |  | 2 " Ice | 0.38 | 0.30 | 0.01 |
|  |  |  |  |  |  | 4 " Ice | 0.77 | 0.67 | 0.04 |
| ATBT-BOTTOM-24V | B | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 0.12 | 0.08 | 0.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.17 | 0.12 | 0.00 |
|  |  |  |  |  |  | 1" Ice | 0.23 | 0.17 | 0.01 |
|  |  |  |  |  |  | 2 " Ice | 0.38 | 0.30 | 0.01 |
|  |  |  |  |  |  | 4 " Ice | 0.77 | 0.67 | 0.04 |
| ATBT-BOTTOM-24V | C | From Leg | 2.00 | 0.0000 | 140.00 | No Ice | 0.12 | 0.08 | 0.00 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 0.17 | 0.12 | 0.00 |
|  |  |  | 0.00 |  |  | 1" Ice | 0.23 | 0.17 | 0.01 |
|  |  |  |  |  |  | 2 " Ice | 0.38 | 0.30 | 0.01 |
|  |  |  |  |  |  | 4 " Ice | 0.77 | 0.67 | 0.04 |
| Pipe Mount [PM 602-3] | C | None |  | 0.0000 | 130.00 | No Ice | 7.68 | 7.68 | 0.28 |
|  |  |  |  |  |  | 1/2" Ice | 9.50 | 9.50 | 0.35 |
|  |  |  |  |  |  | $1^{\prime \prime}$ Ice | 11.32 | 11.32 | 0.43 |
|  |  |  |  |  |  | 2 " Ice | 14.96 | 14.96 | 0.58 |
|  |  |  |  |  |  | 4" Ice | 22.24 | 22.24 | 0.87 |
| 742213 | A | From Leg | 1.00 | 0.0000 | 130.00 | No Ice | 5.14 | 2.87 | 0.02 |
|  |  |  | $0.00$ |  |  | 1/2" Ice | 5.61 | 3.48 | 0.05 |
|  |  |  | 0.00 |  |  | 1" Ice | 6.09 | 3.95 | 0.08 |
|  |  |  |  |  |  | 2 " Ice | 7.07 | 4.89 | 0.16 |
|  |  |  |  |  |  | 4 " Ice | 9.13 | 6.88 | 0.39 |
| 742213 | B | From Leg | 1.00 | 0.0000 | 130.00 | No Ice | 5.14 | 2.87 | 0.02 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.61 | 3.48 | 0.05 |
|  |  |  | 0.00 |  |  | 1" Ice | 6.09 | 3.95 | 0.08 |
|  |  |  |  |  |  | 2 " Ice | 7.07 | 4.89 | 0.16 |
|  |  |  |  |  |  | 4 " Ice | 9.13 | 6.88 | 0.39 |
| 742213 | C | From Leg | 1.00 | 0.0000 | 130.00 | No Ice | 5.14 | 2.87 | 0.02 |
|  |  |  | 0.00 |  |  | 1/2" Ice | 5.61 | 3.48 | 0.05 |
|  |  |  | 0.00 |  |  | $1{ }^{1 \prime}$ Ice | 6.09 | 3.95 | 0.08 |


\left.| tnxTMOWer | Job | Page |
| :---: | :--- | :--- | :--- |
|  |  |  |$\right)$



## Critical Deflections and Radius of Curvature - Service Wind

| Elevation ft | Appurtenance | Gov. Load Comb. | Deflection in | Tilt | Twist 。 | Radius of Curvature $f t$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 149.00 | T-Arm Mount [TA 702-3] | 27 | 33.592 | 2.0139 | 0.0239 | 20904 |
| 140.00 | Commscope MC-HPM1250-B | 27 | 29.803 | 1.9822 | 0.0215 | 11613 |
| 130.00 | Pipe Mount [PM 602-3] | 27 | 25.695 | 1.9234 | 0.0188 | 5520 |


| Maximum Tower Deflections - Design Wind |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Horz. | Gov. | Tilt | Twist |
| No. |  | Deflection | Load |  |  |
|  | ft | in | Comb. | - | - |
| L1 | 149-123.612 | 96.575 | 2 | 5.7862 | 0.0685 |
| L2 | 127.388-79.128 | 70.926 | 2 | 5.4648 | 0.0517 |
| L3 | 83.873-43.243 | 29.355 | 2 | 3.4127 | 0.0177 |
| L4 | 48.76-0 | 9.718 | 2 | 1.8317 | 0.0070 |

Critical Deflections and Radius of Curvature - Design Wind

| Elevation | Appurtenance | Gov. <br> Load | Deflection | Tilt | Twist | Radius of Curvature |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $f t$ |  | Comb. | in |  |  |  |
| 149.00 |  | 2 | 96.575 | 5.7862 | 0 |  |
| 140.00 | T-Arm Mount [TA 702-3] | 2 | 85.705 | 5.6967 | 0.0685 |  |
| 130.00 | Commscope MC-HPM1250-B | 2 | 73.916 | 5.5294 | 0.0617 |  |


| tnxTower | Job ANDOVER NORTH / BU\#: 842856 |  | $\text { Page } 7 \text { of } 8$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2015777.842856 .01 | $\begin{aligned} & \text { Date } \\ & \text { 14:26:19 03/13/15 } \end{aligned}$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |

## Compression Checks

## Pole Design Data

| Section No. | Elevation | Size | $L$ | $L_{u}$ | Kl/r | $F_{a}$ | A | Actual $P$ | Allow. $P_{a}$ | Ratio $P$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | $f t$ |  | $f t$ | $f t$ |  | ksi | $i n^{2}$ | K | K | $P_{a}$ |
| L1 | 149-123.612 (1) | TP26.2021x21.5x0.1875 | 25.39 | 0.00 | 0.0 | 39.000 | 15.0657 | -2.99 | 587.56 | 0.005 |
| L2 | 123.612-79.128 (2) | TP33.9598x25.1277x0.1875 | 48.26 | 0.00 | 0.0 | 36.155 | 19.5819 | -6.66 | 707.98 | 0.009 |
| L3 | 79.128-43.243 (3) | TP40.1211x32.7164x0.25 | 40.63 | 0.00 | 0.0 | 38.397 | 30.8399 | -11.28 | 1184.15 | 0.010 |
| L4 | 43.243-0 (4) | TP47.5x38.6156x0.3125 | 48.76 | 0.00 | 0.0 | 38.896 | 46.8041 | -20.15 | 1820.51 | 0.011 |

## Pole Bending Design Data

| Section No. | Elevation <br> ft | Size | Actual $M_{x}$ <br> kip-ft | Actual $f_{b x}$ ksi | Allow. $F_{b x}$ ksi | $\begin{gathered} \hline \text { Ratio } \\ f_{b x} \\ \hline F_{b x} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Actual } \\ M_{y} \\ \text { kip-ft } \\ \hline \end{gathered}$ | Actual $f_{b y}$ ksi | Allow. $F_{b y}$ ksi | $\begin{gathered} \begin{array}{c} \text { Ratio } \\ f_{b y} \end{array} \\ \hline F_{b y} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 149-123.612 (1) | TP26.2021x21.5x0.1875 | 125.38 | 15.980 | 39.000 | 0.410 | 0.00 | 0.000 | 39.000 | 0.000 |
| L2 | 123.612-79.128 (2) | TP33.9598x25.1277x0.1875 | 554.60 | 41.768 | 36.155 | 1.155 | 0.00 | 0.000 | 36.155 | 0.000 |
| L3 | 79.128-43.243 (3) | TP40.1211x32.7164x0.25 | 1003.86 | 40.671 | 38.397 | 1.059 | 0.00 | 0.000 | 38.397 | 0.000 |
| L4 | 43.243-0 (4) | TP47.5x38.6156x0.3125 | 1771.83 | 38.966 | 38.896 | 1.002 | 0.00 | 0.000 | 38.896 | 0.000 |

## Pole Shear Design Data

| Section No. | Elevation $f t$ | Size | Actual $V$ $K$ | $\begin{gathered} \text { Actual } \\ f_{v} \\ k s i \end{gathered}$ | Allow. $F_{v}$ ksi | $\begin{gathered} \hline \text { Ratio } \\ f_{v} \\ \hline F_{v} \\ \hline \end{gathered}$ | $\begin{gathered} \text { Actual } \\ T \\ \text { kip-ft } \end{gathered}$ | $\begin{gathered} \text { Actual } \\ f_{v t} \\ k s i \end{gathered}$ | Allow. $F_{v t}$ ksi | $\begin{gathered} \hline \text { Ratio } \\ f_{v t} \\ \hline F_{v t} \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 149-123.612 (1) | TP26.2021×21.5x0.1875 | 8.28 | 0.550 | 26.000 | 0.042 | 0.24 | 0.015 | 26.000 | 0.001 |
| L2 | 123.612-79.128 (2) | TP33.9598x25.1277x0.1875 | 11.46 | 0.585 | 26.000 | 0.045 | 0.24 | 0.009 | 26.000 | 0.000 |
| L3 | 79.128-43.243 (3) | TP40.1211x32.7164x0.25 | 14.08 | 0.457 | 26.000 | 0.035 | 0.24 | 0.005 | 26.000 | 0.000 |
| L4 | 43.243-0 (4) | TP47.5x38.6156x0.3125 | 17.40 | 0.372 | 26.000 | 0.029 | 0.24 | 0.003 | 26.000 | 0.000 |

## Pole Interaction Design Data

| Section No. | Elevation <br> ft | $\begin{gathered} \hline \text { Ratio } \\ P \\ \hline P_{a} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ f_{b x} \\ \hline F_{b x} \\ \hline \end{gathered}$ | $\begin{gathered} \begin{array}{c} \text { Ratio } \\ f_{b y} \end{array} \\ \hline F_{b y} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \text { Ratio } \\ f_{v} \\ \hline F_{v} \\ \hline \end{gathered}$ | $\begin{gathered} \hline \begin{array}{c} \text { Ratio } \\ f_{v t} \end{array} \\ \hline F_{v t} \\ \hline \end{gathered}$ | Comb. Stress Ratio | Allow. Stress Ratio | Criteria |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| L1 | 149-123.612 (1) | 0.005 | 0.410 | 0.000 | 0.042 | 0.001 | 0.415 | 1.333 | H1-3+VT |
| L2 | 123.612-79.128 (2) | 0.009 | 1.155 | 0.000 | 0.045 | 0.000 | 1.165 | 1.333 | $\mathrm{H} 1-3+\mathrm{VT}$ |
| L3 | 79.128-43.243 (3) | 0.010 | 1.059 | 0.000 | 0.035 | 0.000 | 1.069 | 1.333 | $\mathrm{H} 1-3+\mathrm{VT}$ |
| L4 | 43.243-0 (4) | 0.011 | 1.002 | 0.000 | 0.029 | 0.000 | 1.013 | 1.333 | H1-3+VT |


| tnxTower | ANDOVER NORTH / BU\#: 842856 |  | $\begin{aligned} & \text { Page } 8 \text { of } 8 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| GPD Group <br> 520 South Main Street, Suite 2531 <br> Akron, OH 44311 <br> Phone: (330) 572-2100 <br> FAX: (330) 572-2101 | Project | 2015777.842856.01 | Date $14: 26: 19 \text { 03/13/15 }$ |
|  | Client | Crown Castle USA, Inc. | Designed by EBoaz |


| Section Capacity Table |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Section | Elevation | Component | Size | Critical | $P$ | $S F^{*} P_{\text {allow }}$ | \% Capacity | Pass |
| No. | $f t$ | Type |  | Element | K | K |  | Fail |
| L1 | 149-123.612 | Pole | TP26.2021×21.5x0.1875 | 1 | -2.99 | 783.22 | 31.2 | Pass |
| L2 | 123.612-79.128 | Pole | TP33.9598x25.1277x0.1875 | 2 | -6.66 | 943.73 | 87.4 | Pass |
| L3 | 79.128-43.243 | Pole | TP40.1211x32.7164x0.25 | 3 | -11.28 | 1578.47 | 80.2 | Pass |
| L4 | 43.243-0 | Pole | TP47.5x38.6156x0.3125 | 4 | -20.15 | 2426.74 | 76.0 | Pass |
|  |  |  |  |  |  | Summary | ELC: | LC5 |
|  |  |  |  |  |  | Pole (L2) | 87.4 | Pass |
|  |  |  |  |  |  | Rating $=$ | 87.4 | Pass |

## APPENDIX B

## BASE LEVEL DRAWING

8

business unit: 842856 TOWER ID: C_BASELEVEL

CROWN REGION ADDRESS
usA

3 ํ

CHECKED BY
DRAWING DATE: $11 / 08 / 14$
SITE NUMBE
SITE NAME:
SITE NAME
andover nort
${ }^{84856}$
STTE ADDRESS ${ }^{122 \text { JoNatrian rrembuli hg tway (Route b) }}$ ANDOVER, CTOE323
TOLLAND COUNTY
USA
SHEET TITLE
BASE LEVEL
BASE Le

## APPENDIX C

## ADDITIONAL CALCULATIONS

Stiffened or Unstiffened, Ungrouted, Circular Base Plate - Any Rod Material TIA Rev F

Site Data
BU\#: 842856
Site Name: ANDOVER NORTH
App \#: 282530 Rev. 1
Pole Manufacturer: ${ }^{\text {Other }}$

| Anchor Rod Data |  |  |
| ---: | :---: | :--- |
| Qty: | 12 |  |
| Diam: | 2.25 | in |
| Rod Material: | A615-J |  |
| Strength (Fu) | $: 100$ | ksi |
| Yield (Fy): | 75 | ksi |
| Bolt Circle: | 56 | in |


| Plate Data |  |  |
| ---: | :---: | :---: |
| Diam: | 62 | in |
| Thick: | 1.5 | in |
| Grade: | 60 | ksi |
| Single-Rod B-eff: | 12.56 | in |


| Stiffener Data (Welding at both sides) |  |  |
| :---: | :---: | :---: |
| Config: | 1 | * |
| Weld Type: | Both | $\begin{aligned} & \text { in ** } \\ & \text { degrees } \end{aligned}$ |
| Groove Depth: | 0.5625 |  |
| Groove Angle: | 45 |  |
| Fillet H. Weld: | 0.375 | in |
| Fillet V. Weld: | 0.1875 | in |
| Width: | 7 | in |
| Height: | 26 | in |
| Thick: | 1.5 | in |
| Notch: | 0.75 | in |
| Grade: | 50 | ksi |
| Weld str.: | 70 | ksi |


| Reactions |  |  |
| ---: | :---: | :--- |
| Moment: | 1772 | ft-kips |
| Axial | 20 | kips |
| Shear: | 17 | kips |

If No stiffeners, Criteria: $\quad$ AISC ASD <-Only Applcable to Unstiffened Cases

| Anchor Rod Results |  | Stiffened |
| :--- | :---: | :---: |
| Maximum Rod Tension: | 124.9 Kips | Service, ASD |
| Allowable Tension: | 195.0 Kips | Fty ${ }^{*}$ ASIF |
| Anchor Rod Stress Ratio: | $64.1 \%$ Pass |  |

Base Plate Results
Base Plate Stress:
Allowable Plate Stress:

Flexural Check
49.4 ksi
60.0 ksi
$82.4 \%$ Pass

| Stiffened |
| :---: |
| Service, ASD |
| $0.75^{*}$ Fy*ASIF |
| Y.L. Length: |
| N/A, Roark |

## Stiffener Results

| Horizontal Weld : | $55.1 \%$ Pass |
| :--- | ---: |
| Vertical Weld: | $57.6 \%$ Pass |
| Plate Flex+Shear, fb/Fb+(fv/Fv) ${ }^{\wedge} 2:$ | $3.8 \%$ Pass |
| Plate Tension+Shear, $\mathrm{ft} / \mathrm{Ft}+(\mathrm{fv} / \mathrm{Fv})^{\wedge} 2:$ | $27.2 \%$ Pass |
| Plate Comp. (AISC Bracket): | $26.7 \%$ Pass |

Pole Results
Pole Punching Shear Check: 7.9\% Pass

| Pole Data |  |  |
| ---: | :---: | :--- |
| Diam: | 47.5 | in |
| Thick: | 0.3125 | in |
| Grade | 65 | ksi |
| \# of Sides: | 18 | "0" IF Round |
| Fu | 80 | ksi |
|  | 0 | "0" if None |


| Stress Increase Factor |  |  |
| :---: | :---: | :---: |
| ASIF: 1.333 |  |  |



[^0]Mat Foundation Analysis
ANDOVER NORTH / BU\#: 842856
2015777.842856.01

| Bearing Summary |  |  | Load Case |
| :---: | :---: | :---: | :---: |
| Qxmax | 2.17 | ksf | 0.9D+1.6W |
| Qymax | 2.17 | ksf | 0.9D+1.6W |
| Qmax @ 45 | 2.41 | ksf | 0.9D+1.6W |
| $\mathrm{Q}_{\text {(all) Gross }}$ | 9.00 | ksf |  |
| Controlling Capacity | 26.8\% | Pass |  |


| Tower Reactions |  |
| :---: | :---: |
| Moment, M | $1772 \mathrm{k}-\mathrm{ft}$ |
| Axial, P | 20 k |
| Shear, V | 17 k |


| Pad \& Pier Geometry |  |  |
| :---: | :---: | :---: |
| Pier Width, $\varnothing$ | 6.5 | ft |
| Pad Length, L | 20.5 | ft |
| Pad Width, W | 20.5 | ft |
| Pad Thickness, t | 3 | ft |
| Depth, D | 6.5 | ft |
| Height Above Grade, HG | 1 | ft |


| Pad \& Pier Reinforcing |  |  |
| :---: | :---: | :--- |
| Rebar Fy | 60 | ksi |
| Concrete Fc' | 4 | ksi |
| Clear Cover | 3 | in |
| Reinforced Top \& Bottom? | Yes |  |
| Pad Reinforcing Size | $\# 8$ |  |
| Pad Quantity Per Layer | 21 |  |
| Pier Rebar Size | $\# 8$ |  |
| Pier Quantity of Rebar | 40 |  |


| Soil Properties |  |
| :---: | :---: |
| Soil Type | Granular |
| Soil Unit Weight | 115 pcf |
| Angle of Friction, $\varnothing$ | $30^{\circ}$ |
| Bearing Type | Gross |
| Ultimate Bearing | 12 ksf |
| Water Table Depth | 10 ft |
| Frost Depth | 3 ft |


| Overturning Summary (Required FS=1.0) |  | Load Case |  |
| :---: | :---: | :---: | :---: |
| FS(ot)x | 1.63 | $\geq 1.0$ | $0.9 \mathrm{D}+1.6 \mathrm{~W}$ |
| FS(ot)y | 1.63 | $\geq 1.0$ | $0.9 \mathrm{D}+1.6 \mathrm{~W}$ |
| Controlling Capacity | $\mathbf{6 1 . 5 \%}$ | Pass |  |



GPD Mat Foundation Analysis - V1.02

## Base Foundation Reinforcement Check ANDOVER NORTH / BU\#: 842856

Code
TIA-222-G
2015777.842856.01

| Tower Reactions |  |
| :---: | :---: |
| Moment | $1772 \mathrm{k}-\mathrm{ft}$ |
| Axial | 20 k |
| Shear | 17 k |


| Pad \& Pier Geometry |  |
| :---: | ---: |
| Height | 6.5 ft |
| Height above Grade | 1 ft |
| Pad Length, L | 20.5 ft |
| Pad Width, W | 20.5 ft |
| Pad Thickness | 3 ft |
| Pier Shape | Square |
| Square Pier Width | 6.5 ft |


| Pad \& Pier Reinforcing |  |
| :---: | :---: |
| Reinforcing Known | Yes |
| $\mathrm{f}_{\mathrm{c}}{ }^{\prime}$ | 4 ksi |
| Clear Cover | 3 in |
| Rebar Fy | 60 ksi |
| Reinforced Top \& Bottom? | Yes |
| Pad Rebar Size | $\# 8$ |
| Pad Rebar Quantity | 21 |
| Pier Rebar Size | $\# 8$ |
| Pier Rebar Quantity | 40 |


| Unit Weights |  |
| :---: | :---: |
| Concrete Unit Weight | 150 pcf |
| Soil Unit Weight | 115 pcf |


| Orthogonal Bearing |  |
| :---: | :---: |
| $\mathrm{Q}_{\max }$ | 2.89 ksf |
| $\mathrm{Q}_{\min }$ | 0.00 ksf |
| Bearing Length | 13.38 ft |


| Pad Moment Capacity |  |  |
| :---: | :---: | :--- |
| $\mathrm{M}_{\mathrm{u}}=$ | $33.39 \mathrm{k}-\mathrm{ft}$ |  |
| $\phi \mathrm{M}_{\mathrm{n}}=$ | $112.55 \mathrm{k}-\mathrm{ft}$ |  |
| Moment Capacity | $29.7 \%$ | OK |
| One-Way (Wide-Beam) Shear |  |  |
| $\mathrm{V}_{\mathrm{u}}=$ | 125.07 kips |  |
| $\phi \mathrm{V}_{\mathrm{n}}=$ | 735.13 kips |  |
| Shear Capacity | $17.0 \%$ | OK |
| $T$ wo-Way (Punching) Shear |  |  |
| $\mathrm{V}_{\mathrm{u}}=$ | 254.20 kips |  |
| $\phi \mathrm{V}_{\mathrm{n}}=$ | 2617.80 kips |  |
| Shear Capacity | $9.7 \%$ | OK |
| Pier Compression |  |  |
| $\mathrm{P}_{\mathrm{u}}=$ | 20.00 kips |  |
| $\phi \mathrm{P}_{\mathrm{n}}=$ | 11686.56 kips |  |
| 0.2\% | OK |  |

Base Foundation Reinforcement - V1.09

| Overall Capacities |  |  |
| :---: | :---: | :---: |
| Reinforcement Capacity | $29.7 \%$ | OK |
| As Min Met? | Yes |  |
| Controlling Capacity | $\mathbf{2 9 . 7 \%}$ | OK |


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# RADIO FREQUENCY EMISSIONS ANALYSIS REPORT EVALUATION OF HUMAN EXPOSURE POTENTIAL TO NON-IONIZING EMISSIONS 

T-Mobile Existing Facility

Site ID: CT11501E

CT501/ ATT Andover- Prime 122 Route 6
Andover, CT
March 24, 2015
EBI Project Number: 6215001738

| Site Compliance Summary |  |
| :---: | :---: |
| Compliance Status: | COMPLIANT |
| Site total MPE\% of <br> FCC general public <br> allowable limit: | $\mathbf{2 5 . 7 7} \%$ |

March 24, 2015

T-Mobile USA
Attn: Jason Overbey, RF Manager
35 Griffin Road South
Bloomfield, CT 06002

## Emissions Analysis for Site: CT11501E - CT501/ ATT Andover- Prime

EBI Consulting was directed to analyze the proposed T-Mobile facility located at 122 Route 6, Andover, CT, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (\% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm} 2$ ). The number of $\mu \mathrm{W} / \mathrm{cm}^{2}$ calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) - (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu \mathrm{W} / \mathrm{cm}^{2}$ ). The general population exposure limit for the 700 MHz Band is $467 \mu \mathrm{~W} / \mathrm{cm}^{2}$, and the general population exposure limit for the PCS and AWS bands is $1000 \mu \mathrm{~W} / \mathrm{cm}^{2}$. Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## CALCULATIONS

Calculations were done for the proposed T-Mobile Wireless antenna facility located at $\mathbf{1 2 2}$ Route $\mathbf{6}$, Andover, CT, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was focused at the base of the tower. For this report the sample point is the top of a 6 foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

1) 2 GSM channels (PCS Band - 1900 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel
2) 2 UMTS channels (AWS Band - 2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
3) 2 LTE channels (AWS Band - 2100 MHz ) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel.
4) 1 LTE channel ( 700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.
5) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
environmental | engineering | due diligence
6) For the following calculations the sample point was the top of a six foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
7) The antennas used in this modeling are the RFS APX16PV-16PVL-C for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the Commscope LNX-6515DS-VTM for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The RFS APX16PV-16PVL-C has a maximum gain of $\mathbf{1 6 . 3} \mathbf{d B d}$ at its main lobe. The Commscope LNX-6515DS-VTM has a maximum gain of $\mathbf{1 4 . 6} \mathbf{~ d B d}$ at its main lobe. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB , was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
8) The antenna mounting height centerline of the proposed antennas is $\mathbf{1 4 0}$ feet above ground level (AGL)
9) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.

All calculations were done with respect to uncontrolled / general public threshold limits.

## T-Mobile Site Inventory and Power Data

| Sector: | A | Sector: | B | Sector: | C |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Antenna \#: | 1 | Antenna \#: | 1 | Antenna \#: | 1 |
| Make / Model: | $\begin{gathered} \text { RFS APX16PV- } \\ \text { 16PVL-C } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { RFS APX16PV- } \\ \text { 16PVL-C } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { RFS APX16PV- } \\ \text { 16PVL-C } \end{gathered}$ |
| Gain: | 16.3 dBd | Gain: | 16.3 dBd | Gain: | 16.3 dBd |
| Height (AGL): | 140 | Height (AGL): | 140 | Height (AGL): | 140 |
| Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ | Frequency Bands | $\begin{aligned} & 1900 \mathrm{MHz}(\mathrm{PCS}) / \\ & 2100 \mathrm{MHz} \text { (AWS) } \end{aligned}$ |
| Channel Count | 6 | Channel Count | 6 | \# PCS Channels: | 6 |
| Total TX Power: | 240 | Total TX Power: | 240 | \# AWS Channels: | 240 |
| ERP (W): | 10,237.91 | ERP (W): | 10,237.91 | ERP (W): | 10,237.91 |
| Antenna A1 MPE\% | 2.05 | Antenna B1 MPE\% | 2.05 | Antenna C1 MPE\% | 2.05 |
| Antenna \#: | 2 | Antenna \#: | 2 | Antenna \#: | 2 |
| Make / Model: | $\begin{aligned} & \text { Commscope LNX- } \\ & \text { 6515DS-VTM } \end{aligned}$ | Make / Model: | $\begin{gathered} \text { Commscope LNX- } \\ \text { 6515DS-VTM } \end{gathered}$ | Make / Model: | $\begin{gathered} \text { Commscope LNX- } \\ \text { 6515DS-VTM } \end{gathered}$ |
| Gain: | 14.6 dBd | Gain: | 14.6 dBd | Gain: | 14.6 dBd |
| Height (AGL): | 140 | Height (AGL): | 140 | Height (AGL): | 140 |
| Frequency Bands | 700 MHz | Frequency Bands | 700 MHz | Frequency Bands | 700 MHz |
| Channel Count | 1 | Channel Count | 1 | Channel Count | 1 |
| Total TX Power: | 30 | Total TX Power: | 30 | Total TX Power: | 30 |
| ERP (W): | 865.21 | ERP (W): | 865.21 | ERP (W): | 865.21 |
| Antenna A2 MPE\% | 0.37 | Antenna B2 MPE\% | 0.37 | Antenna C2 MPE\% | 0.37 |
|  | Site Composite MPE \% |  |  | T-Mobile Sector 1 Total: T-Mobile Sector 2 Total: | l: 2.42 \% |
|  | Carrier | MPE\% |  |  | l: 2.42 \% |
|  | T-Mobile | 7.26 |  | T-Mobile Sector 3 Total: | l $\quad 2.42$ \% |
|  | AT\&T | 14.48 \% |  | Site Total: | l: 25.77 \% |


| Site Composite MPE \% |  |
| :---: | :---: |
| Carrier | MPE \% |
| T-Mobile | 7.26 |
| AT\&T | $14.48 \%$ |
| MetroPCS | $4.03 \%$ |
| Site Total MPE \%: | $25.77 \%$ |

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## Summary

All calculations performed for this analysis yielded results that were within the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

| T-Mobile Sector | Power Density Value (\%) |
| ---: | :--- |
| Sector 1: | $2.42 \%$ |
| Sector 2: | $2.42 \%$ |
| Sector 3: | $2.42 \%$ |
| T-Mobile Total: | $7.26 \%$ |
|  |  |
| Site Total: | $25.77 \%$ |
|  |  |
| Site Compliance Status: | COMPLIANT |

The anticipated composite MPE value for this site assuming all carriers present is $\mathbf{2 5 . 7 7 \%}$ of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a $5 \%$ contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable $100 \%$ threshold standard per the federal government.


## Scott Heffernan

RF Engineering Director

## EBI Consulting

21 B Street
Burlington, MA 01803


[^0]:    * 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt
    ** Note: for complete joint penetration groove welds the groove depth must be exactly $1 / 2$ the stiffener thickness for calculation purposes

