

56 Prospect Street P.O. Box 270 Hartford, CT 06141-0270

Kathleen M. Shanley Manager – Transmission Siting Tel: 860-728-4527

September 5, 2019

Ms. Melanie Bachman, Executive Director Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

RE: Docket No. 461A: Greenwich Substation and Line Project, Indian Harbor Crossing Development and Management Plan Submission of the Final Pedestrian/Utility Bridge Design and Provision of Information Regarding the Bridge Design and 100-Year Flood

Dear Ms. Bachman:

Pursuant to the condition in the Connecticut Siting Council's (Council's) May 23, 2019 approval of the above-referenced Development and Management (D&M) Plan, the Connecticut Light and Power Company doing business as Eversource Energy (Eversource) submits the enclosed information regarding the following:

- 1. Final design details and drawings for the pedestrian/utility bridge over Indian Harbor¹ (Attachment A); and
- 2. Information from the Town of Greenwich's engineering consultant demonstrating that the bridge will not be affected by a 100-year flood. (Attachment B).

Attached to this original are two copies of this information. Should you have any questions, please do not hesitate to contact me at via e-mail at <u>kathleen.shanley@eversource.com</u> or telephone at (860) 728-4527.

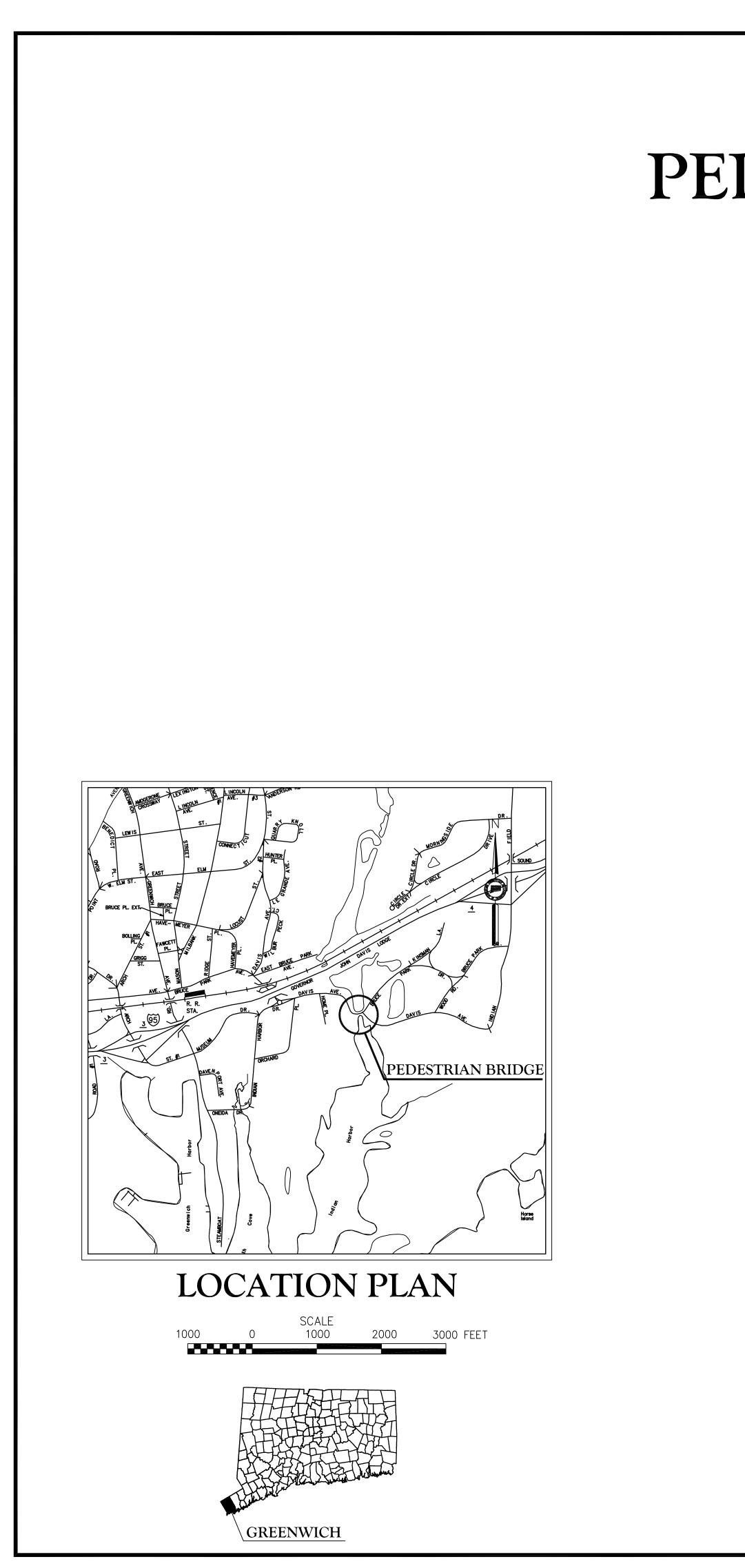
Sincerely,

Kathleen M. Shanley

¹ Note: The bridge will technically span Davis Mill Pond, which is the impounded area between the Interstate 95 and Davis Avenue bridges. Indian Harbor is to the south of the Davis Avenue bridge. However, for the purposes of the D&M Plan, the bridge is referred to generically as crossing "Indian Harbor".

ATTACHMENT A

FINAL DESIGN PEDESTRIAN/UTILITY BRIDGE OVER DAVIS MILL POND



PEDESTRIAN/UTILITY BRIDGE OVER DAVIS MILL POND

GREENWICH, CT

JULY 2019



LIST OF DRAWINGS

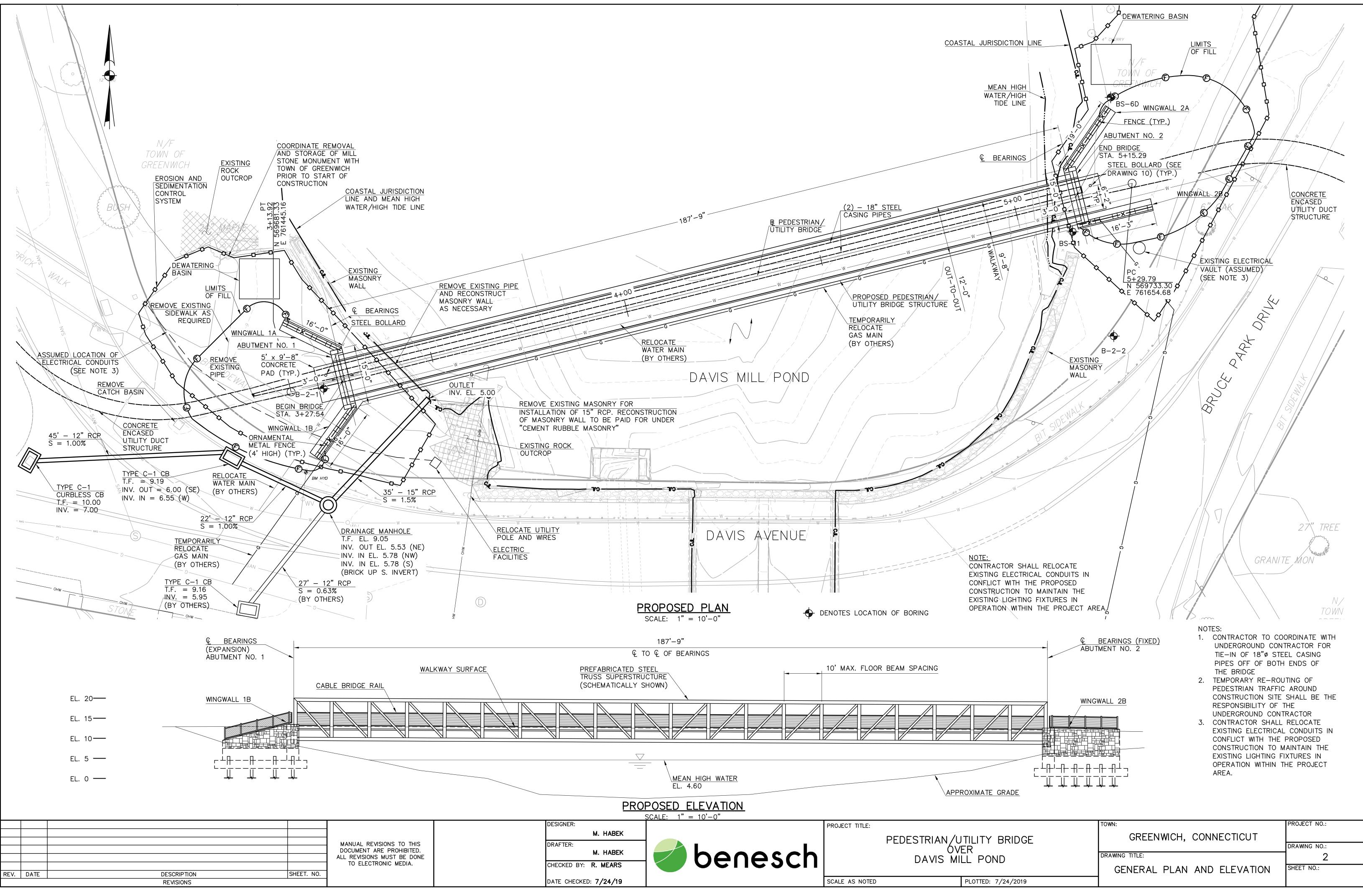
DRAWING TITLE	DRAWING NO.
TITLE SHEET	1
GENERAL PLAN AND ELEVATION	2
PROFILE	3
BRIDGE SECTION AND NOTES	4
BORING LOGS - 1	5
BORING LOGS - 2	6
PILE FOUNDATION PLAN AND DETAILS	7
ABUTMENT NO. 1 AND WINGWALLS 1A/1B	8
ABUTMENT NO. 2 AND WINGWALLS 2A/1B	9
DECK PLAN	10
RAILING DETAILS	11
UTILITY DETAILS	12

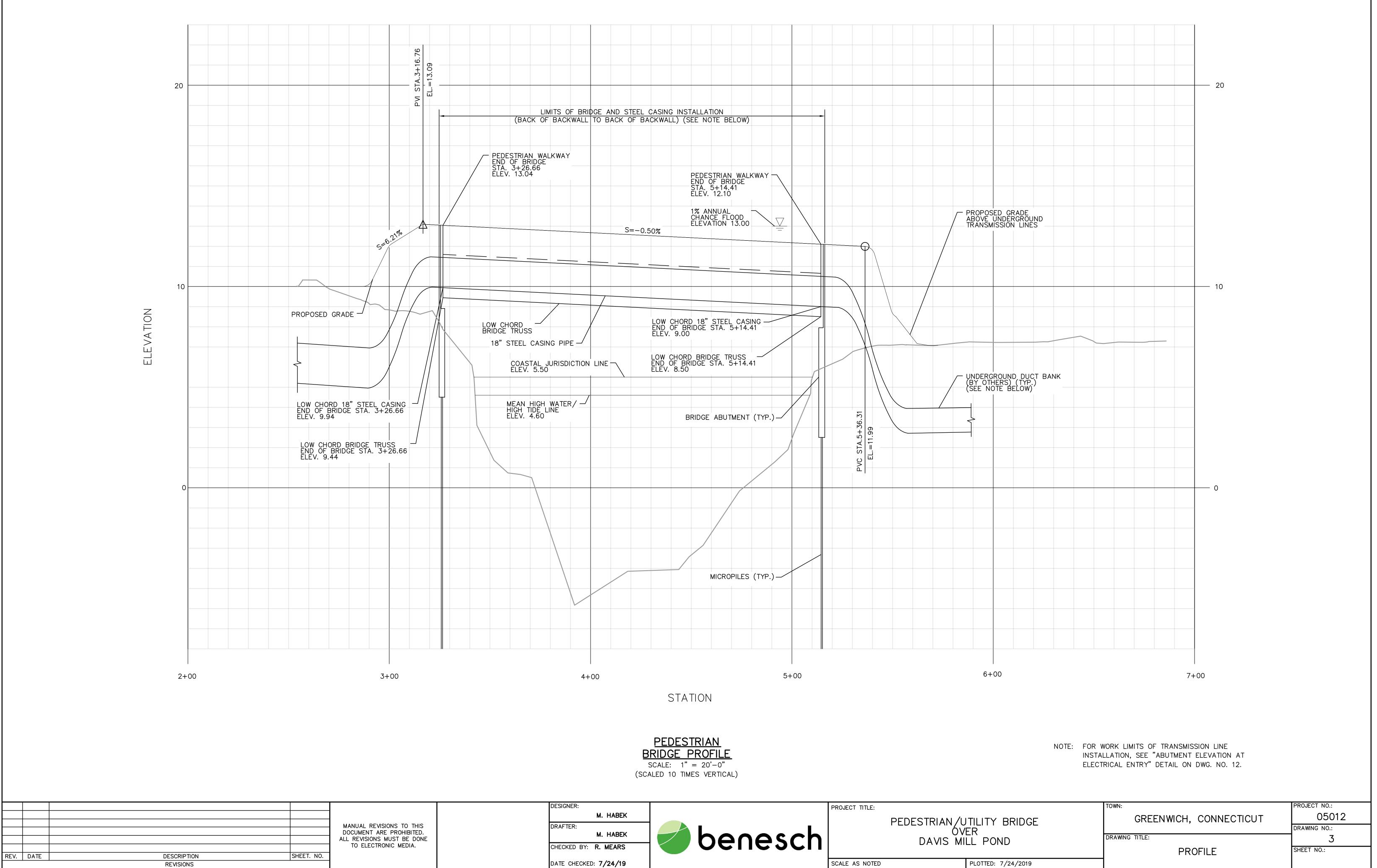


STEVEN J. DRECHSLER

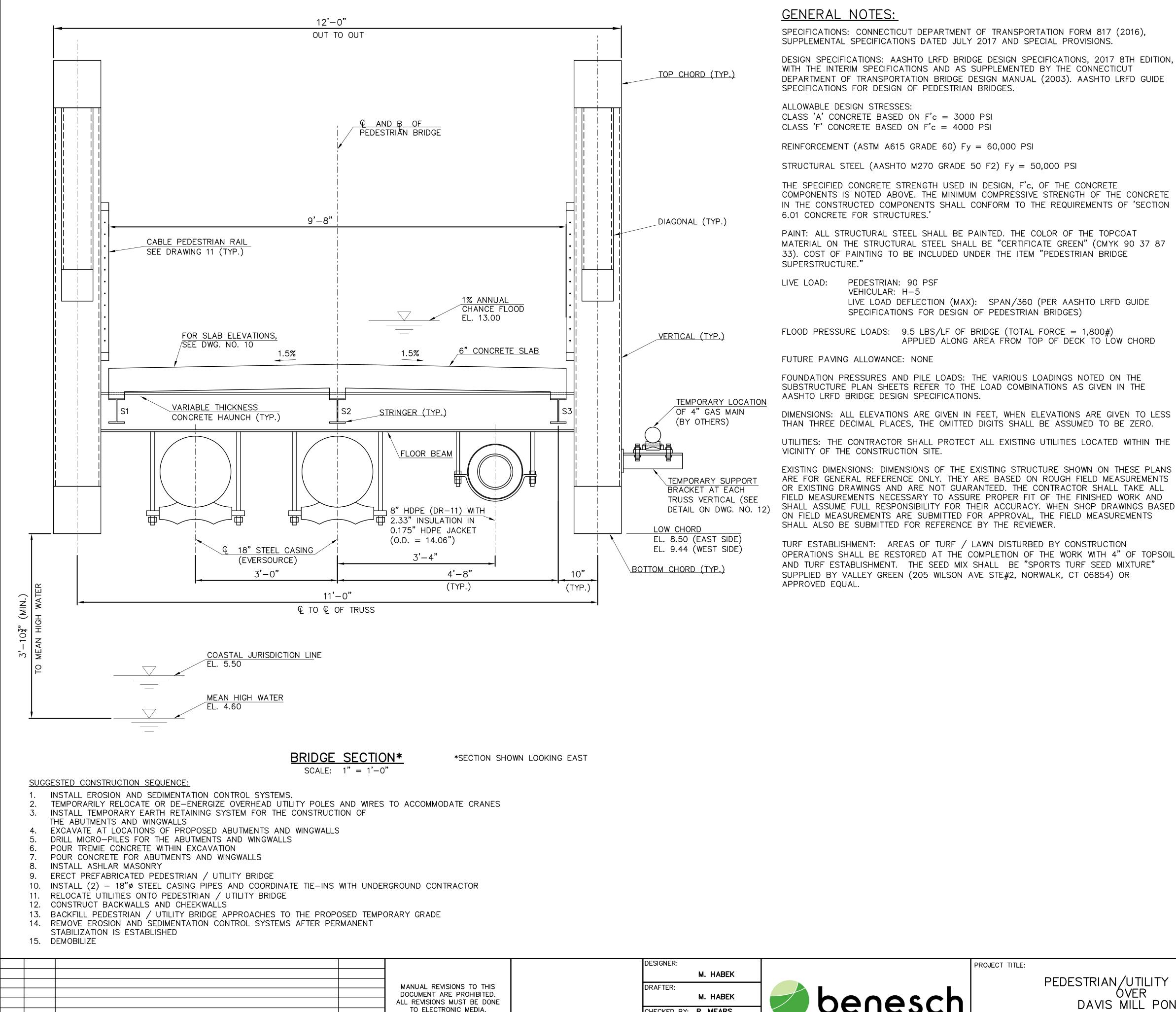
7/30/2019

DATE





M. HABEK		
DRAFTER:		
M. HABEK	benesch	
CHECKED BY: R. MEARS		
DATE CHECKED: 7/24/19		SCALE AS NOTED



DESCRIPTION REVISIONS

REV. DATE

TO ELECTRONIC MEDIA.

SHEET. NO.

DESIGNER:		PROJECT TITLE:		TOWN:	PROJECT NO.:
M. HABEK		PEDESTRIAN/U	TILITY BRIDGE	GREENWICH, CONNECTICUT	
DRAFTER:		OVI			DRAWING NO.:
M. HABEK	benesch	DAVIS MI		DRAWING TITLE:	4
CHECKED BY: R. MEARS				BRIDGE SECTION AND NOTES	SHEET NO.:
				DRIDGE SECTION AND NOTES	
DATE CHECKED: 7/24/19		SCALE AS NOTED	PLOTTED: 7/24/2019		

	<u>CONCRETE NOTES:</u>
6),	CLASS "A" CONCRETE: CLASS "A" CONCRETE SHALL BE USED FOR WINGWALLS, PILE CAPS, AND BACKWALLS
EDITION,	CLASS "F" CONCRETE: CLASS "F" CONCRETE SHALL BE USED FOR THE BRIDGE DECK AND CONCRETE PADS
GUIDE	UNDERWATER CONCRETE: UNDERWATER CONCRETE SHALL BE USED FOR TREMIES
	EXPOSED EDGES: EXPOSED EDGES OF CONCRETE SHALL BE BEVELED 1" \times 1" UNLESS DIMENSIONED OTHERWISE.
	CONCRETE COVER: ALL REINFORCEMENT SHALL HAVE TWO INCHES COVER UNLESS DIMENSIONED OTHERWISE.
	REINFORCEMENT: ALL REINFORCEMENT SHALL BE ASTM A615 GRADE 60.
ONCRETE	EPOXY COATED REINFORCING BARS: ALL REINFORCEMENT SHALL BE EPOXY COATED AND SHALL BE INCLUDED IN THE ITEM "DEFORMED STEEL BARS (EPOXY COATED)."
SECTION	CONSTRUCTION JOINTS: CONSTRUCTION JOINTS, OTHER THAN THOSE SHOWN ON THE PLANS, WILL NOT BE PERMITTED WITHOUT PRIOR APPROVAL OF THE ENGINEER.
37 87	CLOSED CELL ELASTOMER: THE COST OF FURNISHING AND INSTALLING CLOSED CELL ELASTOMER SHALL BE INCLUDED IN THE COST OF THE ITEM "CLASS 'F' CONCRETE."
	STRUCTURAL STEEL NOTES:
JIDE	 ALL STRUCTURAL STEEL (LOW ALLOY) SHALL CONFORM TO AASHTO M270, GRADE 50 F2, Fy = 50,000 PSI
HORD	 WELDING DETAILS, PROCEDURES, AND TESTING METHODS SHALL CONFORM TO ANSI AASHTO/AWS D1.5-(95)- BRIDGE WELDING CODE, UNLESS NOTED OTHERWISE ON THE PLANS.
IE HE TO LESS	3. ALL SHOP WELDS SHALL BE INSPECTED BY RADIOGRAPHIC OR ULTRASONIC TESTING AND FINISHED SMOOTH AND FLUSH WITH BASE METAL ON ALL SURFACES BY GRINDING IN THE DIRECTION OF THE APPLIED STRESS, LEAVING THE SURFACES FREE FROM DEPRESSIONS. CHIPPING MAY BE USED PROVIDED IT IS FOLLOWED BY GRINDING. THE GRINDING PROCESS SHALL NOT REDUCE THE THICKNESS OF THE BASE METAL BY MORE THAN 5% OF THE TOTAL THICKNESS.
ERO.	4. THE STRUCTURE SHALL NOT HAVE NEGATIVE CAMBER AFTER THE APPLICATION OF THE FULL DEAD LOADS, INCLUDING BUT NOT LIMITED TO: REINFORCED CONCRETE DECK, AND GALVANIZED STAY-IN-PLACE FORMS.
E PLANS REMENTS KE ALL K AND GS BASED	5. THE STRUCTURAL STEEL FABRICATORS SHALL AT A MINIMUM BE CERTIFIED AS AN INTERMEDIATE BRIDGE MANUFACTURER PER THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION (AISC). THE STRUCTURAL STEEL FABRICATOR SHALL ALSO HOLD A FRACTURE CRITICAL ENDORSEMENT THROUGH AISC.
INTS	6. THE COST OF FURNISHING AND INSTALLATION OF BEARINGS AT EACH ABUTMENT SHALL BE PAID FOR UNDER THE ITEM "PEDESTRIAN BRIDGE SUPERSTRUCTURE."
	7 NO ELELD WELDING TO ERACTURE CRITICAL MEMBERS SHALL RE ALLOWED

- 7. NO FIELD WELDING TO FRACTURE CRITICAL MEMBERS SHALL BE ALLOWED.
- 8. THE REINFORCED CONCRETE DECK SHALL BE COMPOSITE WITH THE SUPERSTRUCTURE BY USE OF SHEAR STUDS, PAID FOR UNDER "PEDESTRIAN BRIDGE SUPERSTRUCTURE."

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			ifety Han Ib.): 14					er Type: SS er O.D. (in.): 2.0		Date	Groundv Time			th (ft.) Depth	Stab. Time
Ham	mer Fal	II (in.):			n.): 3	& 4	Sample	er Length (in.): 24 arrel Size: NX					Note	91	
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5		SS-3	6-8	24	8	15 16 20 8	36	SS-3 : Dense, brown, fine t Gravel (Organic smell)	to coarse	SAND and	SILT, some			<u>6</u>	
-		SS-4	8-10	24	14	6 8 12 17	20	SS-4 : Medium dense, brov	wn, grey,	SILT, some	e Gravel, trace				ORGANIC SILT
10 _		SS-5	10- 10.7	8	6	15 50/2		SS-5 : Brown, fine to coars	e SAND,	little Grave	I, trace Silt			10	
-			10.7												GLACIAL TILL
- 15 _		SS-6	15-15	0	0	50/0"		SS-6 : No Penetration				3		14	
- - 20 _	2	SS-7 C-1	20-20 21-26	0	0	50/0"		SS-7 : No Penetration C-1 : Moderately hard, mod	derately t	o hiahly we	athered				
- 25 _	2.25 1.5 2.75 2.5				53			moderately fractured, fine t with medium spaced, low a REC=88%)	o mediur	n grained, g	rey GNEISS				BEDROCK
-	2.25 2.75 3	C-2	26-31	60	60			C-2 : Moderately hard, moderately fractured, fine t with medium spaced, low a REC=100%)	o mediur	n grained, g	rey GNEISS				
30	2.5		0												
MARKS	2.2 feel barrel fi 2.2 feel 2 - Incr	t to 10 rom 21 t eased	feet. 3-ir to 31 fe	nch ca eet. Co esista	asing ore ra nce fr	telescoped te in minu rom 2 to 6	d to 15 fe tes/foot. feet and	A) from ground surface to 2. eet and used to advance bord RQD=Rock Quality Designa 1 10 to 20 feet ollerbitting ahead	ehole to 2	21 feet. Roo	k coring perform	med	with N	X-sized	double-tube c
Strati	fication	lines r	epresent	t appr	oxima	ite bounda	ries betv	ween soil and bedrock types.	Actual to	ransitions m	nay be gradual.	_			ration No.: B-2-1

BORING B-2-1

				MANUAL REVISIONS TO THIS
				DOCUMENT ARE PROHIBITED.
				ALL REVISIONS MUST BE DONE
				TO ELECTRONIC MEDIA.
REV.	DATE	DESCRIPTION	SHEET. NO.	
		REVISIONS		

									TEST BORIN	IG LOG							
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Ham	mer Ty	pe: Sa	afety Har	nmer					er Type: SS	£13	Dete		ndwate			Chall T	1
Ham	mer Fal	II (in.)	lb.): 1 : 30 D.D./I.D		n.): 3	& 4	Sam	nple	er O.D. (in.): 2.0 er Length (in.): 24 arrel Size: NX		Date	Time		Vater I Note		Stab. T	Ime
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35 _																	
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50 55 60 Strati																	
Strati	fication	lines	epresen	t appr	oxima	te bound	aries	betv	ween soil and bedrock typ	oes. Actual ti	ransitions r	nay be gradu	ial.		Explo	oration N B-2-1	o.:

BORING B-2-1 (CONT.)



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Hamr Hamr	ner We ner Fa	eight (l II (in.):	lb.): 14	40			Sample	er O.D. (in.): 2.0 er Length (in.): 24 arrel Size: NX		Date	Time	N	Note	Depth 9 1	Stab. Time
epth (ft)	Casing Blows/ Core	No.	Depth	Samp Pen.	Rec.	Blows	SPT	Sample Descrip (Modified Bu			1	Remark	Field Test	₩ ee	STRATUM Description
(11)	Rate	SS-1	(ft.) 0-2	(in) 24	(in) 14	(per 6 in. 3 4) Value 11	SS-1 : Top 8": Topsoil		Tocedure		<u>2</u>	Data	-	TOPSOIL
-		33-1	0-2	24	14	7 14		Bottom 6": Brown, fine to co	arse SAN	ND, some G	ravel, little	1		0.75	
-		SS-2	2-3.3	15	9	30 47 100/3"		Silt SS-2 : Top 3": Brown, fine to Gravel Bottom 7": White, fine to co						3	FILL
5_		SS-3	5-6.5	18	13	34 37 63 50/0	R	(Decomposed Rock) SS-3 : Very dense, brown, f little fine to coarse Gravel (E			and SILT,			POSS	IBLE DECOMPOS ROCK
10 _	3	1202070/012	10-10	0	0	50/0"		SS-4 : No Penetration						11	
- - 15 _	2.75 2.75 5.5 6	C-1	11-16	60	60			C-1 : Moderately hard, sligh moderately fractured, fine to with moderately spaced, mo (RQD=60%, REC=100%)	medium	grained, gre	ey GNEISS	2			
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- - 25 _									g						
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KEMA			epresen			te bounda	ries betv	ween soil and bedrock types.	Actual tra	ansitions ma	v be gradual			Fxplo	ration No.:
			-p. 00011	- oppi	220110						, se gradadi.				B-2-2

BORING B-2-2

	TOWN:	PROJECT NO.:
TILITY BRIDGE	GREENWICH, CONNECTICUT	
FR		DRAWING NO.:
	DRAWING TITLE:	5
	BORING LOGS - 1	SHEET NO.:
PLOTTED: 7/24/2019		

TYPE HSA SS NQ LINE & STA. GROUND WATER OBSERVATIONS START 9/10 SIZE I.D. 3.75" 1.375" 2.0" N. COORDINATE at 1.5 FT. AFTER 0 HOURS TATE 9/10 HAMMER WT. 140 lbs E. COORDINATE AT FT. AFTER HOURS FINISH DATE 9/10	P.O. B	OX 397			, INC.	CLIE	NT		PROJECT NAME UNDERGROUND T LOCATION	RANSMISS	SION LINE	PRO
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SIZE LD 3.75" 1.375" 2.0" N. COORDINATE AT 15 PT ATER 0 HOURS INTER 971 HAMMER NT. 140 lbs E COORDINATE AT 15 PT ATER 0 HOURS PT ATER 10 HOURS PT ATER 1	TVDE		1011000000000000000000	CASING		15		ak.		HOLE N	0. B	S-6
HAMMER WT. 140 bs N. COMDINATE AT TOPSOL MAX MAX <th< td=""><td></td><td></td><td></td><td></td><td>-</td><td></td><td>0.0.00</td><td></td><td></td><td></td><td>START 9/ DATE 9/</td><td>/10/1</td></th<>					-		0.0.00				START 9/ DATE 9/	/10/1
Instruction Product SAMPLE A STRATUM DESCRIPTION 0 1 3-2-1-2 0.00°-2.00° Image: stratum description + REAARKS 0 1 3-2-1-2 0.00°-2.00° Image: stratum description - REAARKS 2 1-2-13-14 2.00°-4.00° Image: stratum description - REAARKS - 0.50 2 1-2-13-14 2.00°-4.00° Image: stratum description - 0.50 - 0.50 2 1-2-13-14 2.00°-4.00° Image: stratum description - 0.50 - 0.50 3 8-10-10-60 5.00°-7.00° Image: stratum description - 0.50 - 0.50 10 Image: stratum description - 0.50 - 0.50 - 0.50 - 0.50 10 Image: stratum description - 0.50 - 0.50 - 0.50 - 0.50 10 Image: stratum description - 0.50 - 0.50 - 0.50 - 0.50 - 0.50 10 Image: stratum description - 0.50 - 0.50 - 0.50 - 0.50 - 0.50 - 0.50 10 Image: stratum description - 0.50 - 0.50 - 0.50 <td></td> <td>WT.</td> <td>0.10</td> <td></td> <td>-</td> <td></td> <td>2.0</td> <td></td> <td>2007 2007 000000</td> <td></td> <td>FINISH</td> <td></td>		WT.	0.10		-		2.0		2007 2007 000000		FINISH	
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Image: Construction of the second	10					-	_	CORED BEDROCK - GNEISS			9.5	1
Image: Second						-		RUN #1 9.5' - 14.5' RECOVER	RED 60" RQD=36%			
15 1								RUN #2 14.5' - 19.5' RECOVE	RED 60" RQD=52%			
LEGEND: COL. A: SAMPLE TYPE: D-DRY A=AUGER C=CORE U=UNDISTURBED PISTON S=SPLIT SPON								RUN #3 19.,5' - 24.0' RECOVE	RED 52" RQD=22%			
LEGEND: COL. A: SAMPLE TYPE: D=DRY A=AUGER C=CORE U=UNDISTURBED PISTON S=SPLIT SPOON DIRILLER: J. BREWER INSPECTOR: DIRILLER: J. BREWER INSPECTOR: DIRILER: J. BREWER INSPECTOR: DIRILER: J. BREWER INSPECTOR: DIRILER: J. BREWER DIRILER: J. BREWER DIR	15			_		-	_					
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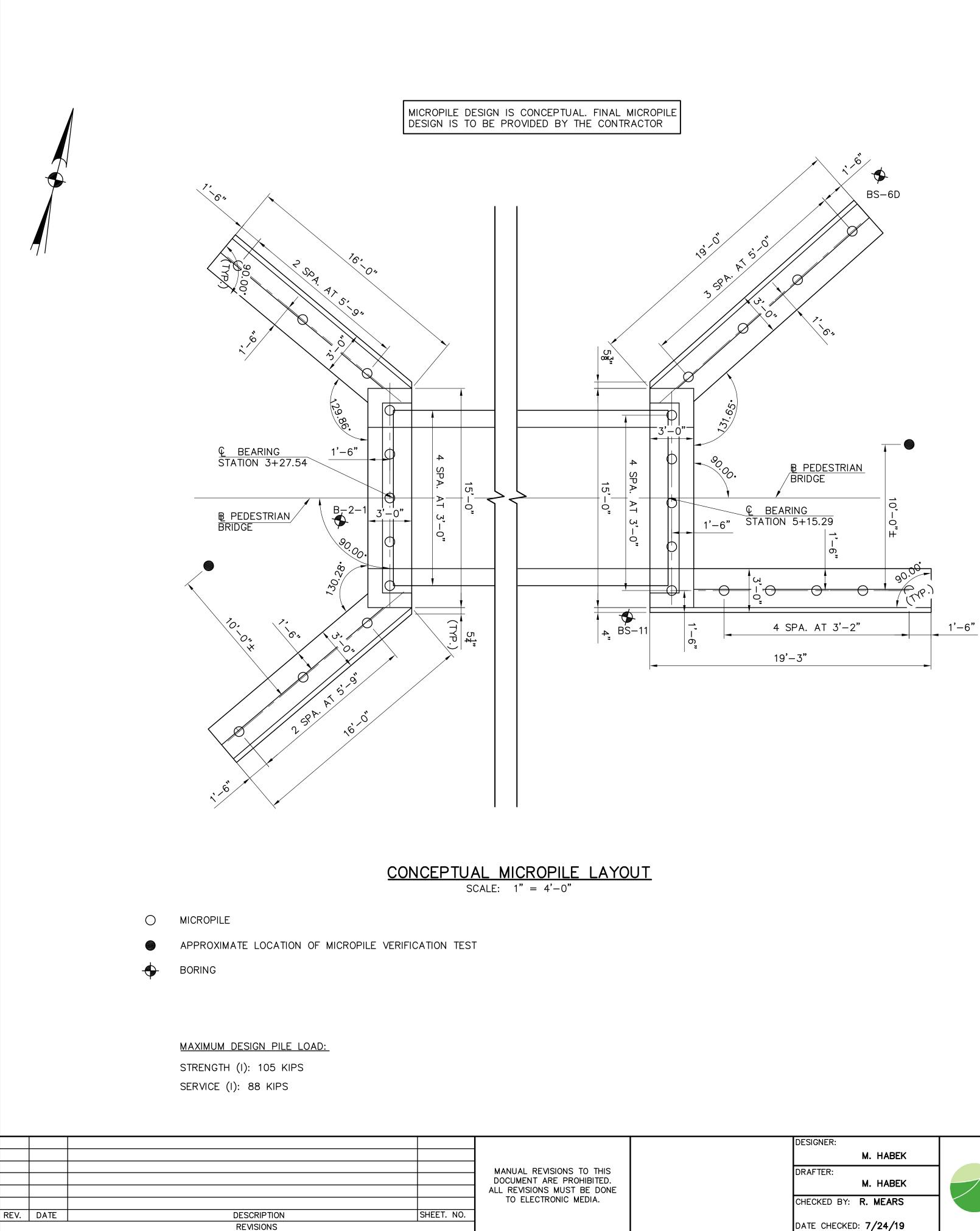
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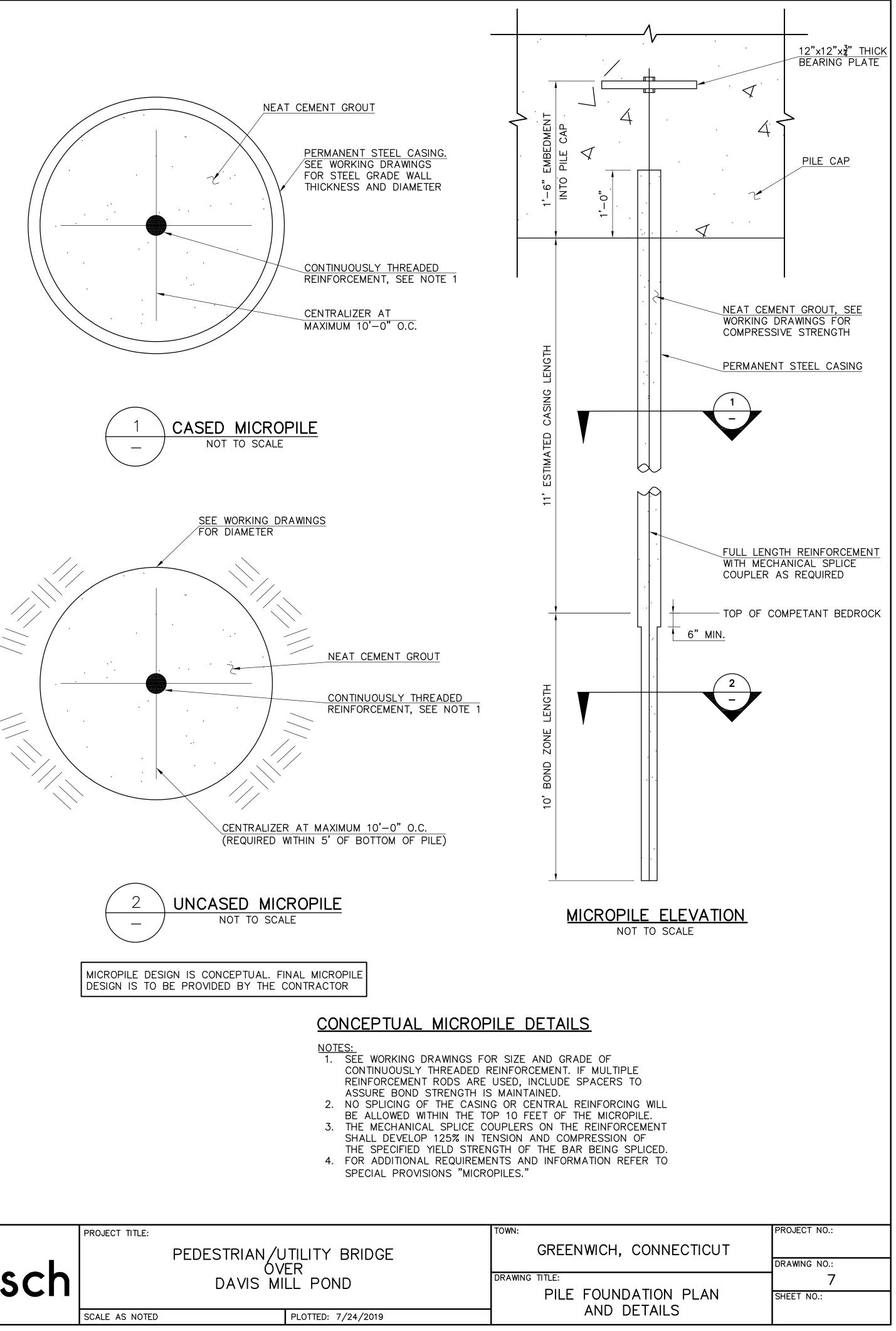
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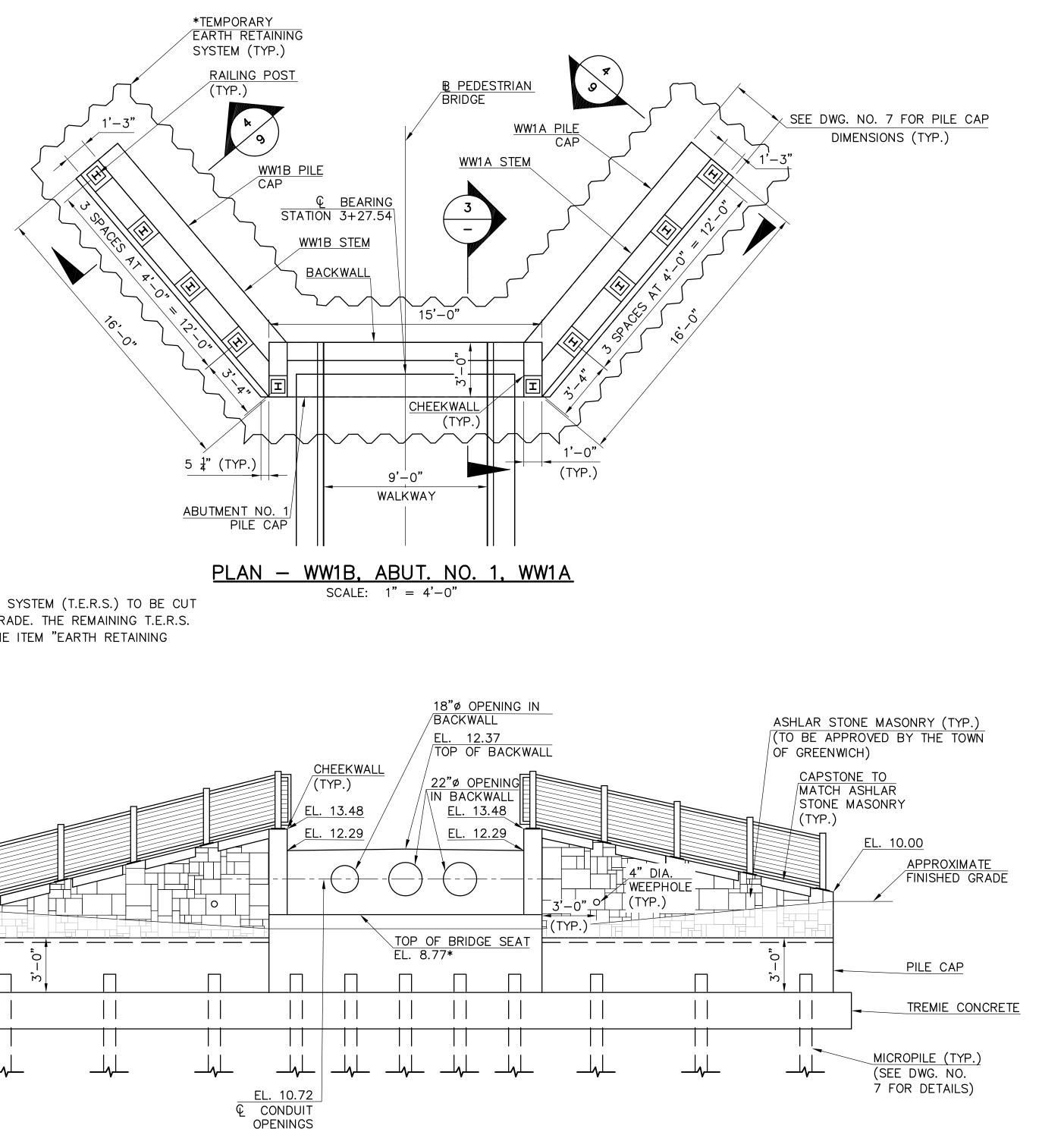


	TOWN:	PROJECT NO.:
UTILITY BRIDGE	GREENWICH, CONNECTICUT	
VER		DRAWING NO.:
ILL POND	DRAWING TITLE:	6
	BORING LOGS - 2	SHEET NO.:
PLOTTED: 7/24/2019		

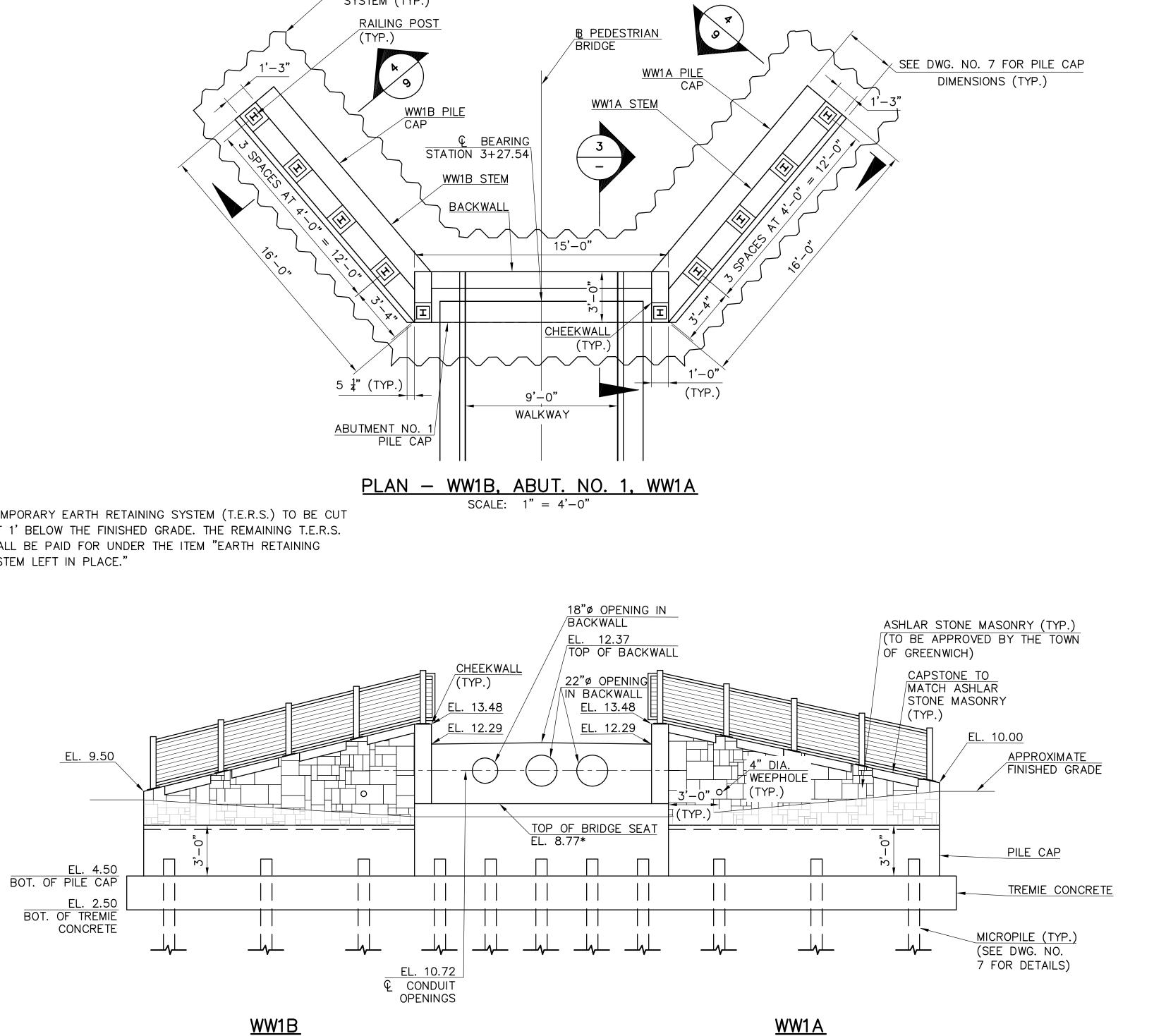




DESIGNER: M. HABEK DRAFTER: M. HABEK CHECKED BY: R. MEARS	benesch	PROJECT TITLE:	PEDESTRIAN/U OVI DAVIS MII	E
DATE CHECKED: 7/24/19		SCALE AS NOTED		F



*TEMPORARY EARTH RETAINING SYSTEM (T.E.R.S.) TO BE CUT OFF 1' BELOW THE FINISHED GRADE. THE REMAINING T.E.R.S. SHALL BE PAID FOR UNDER THE ITEM "EARTH RETAINING SYSTEM LEFT IN PLACE."

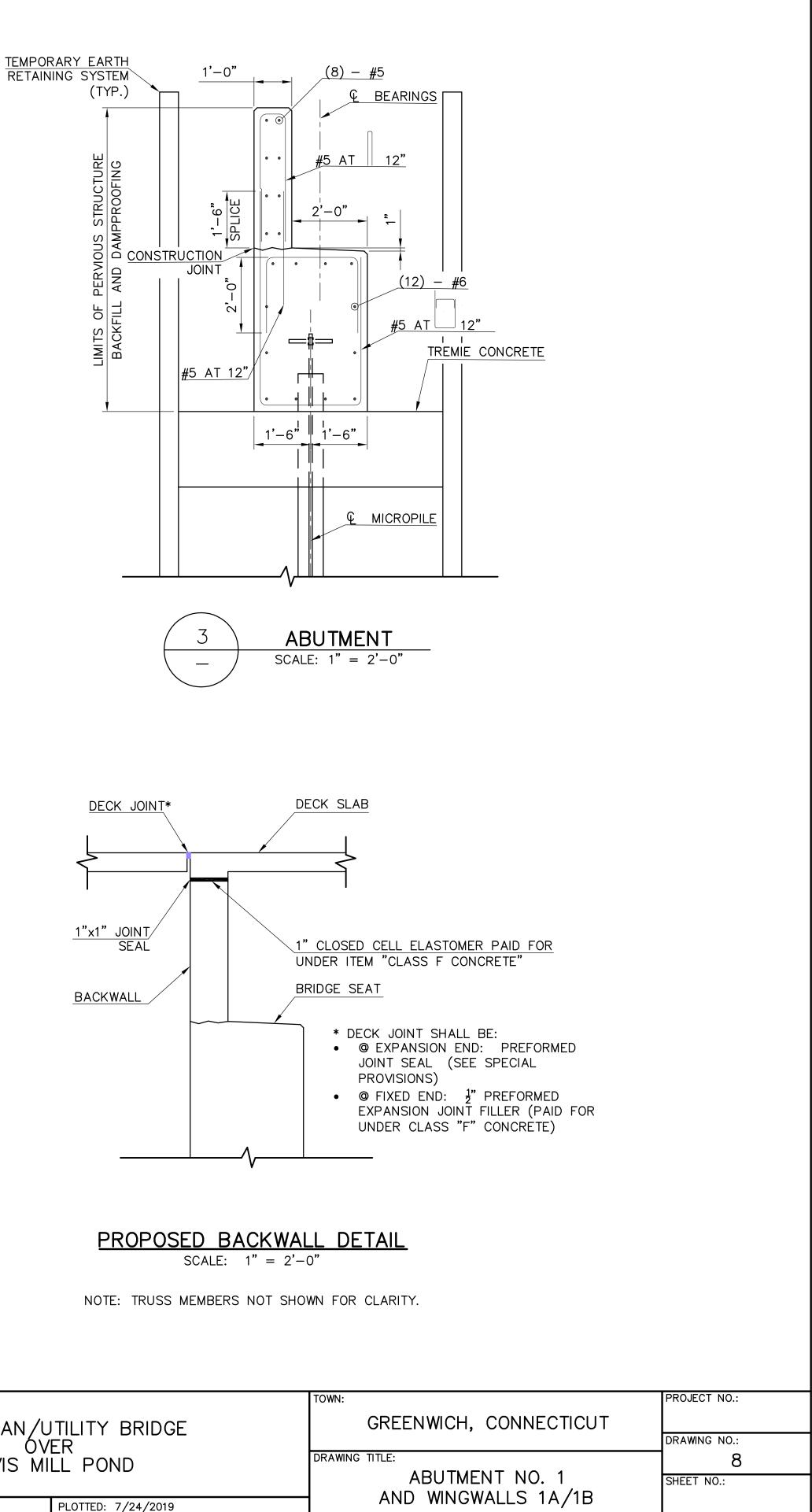


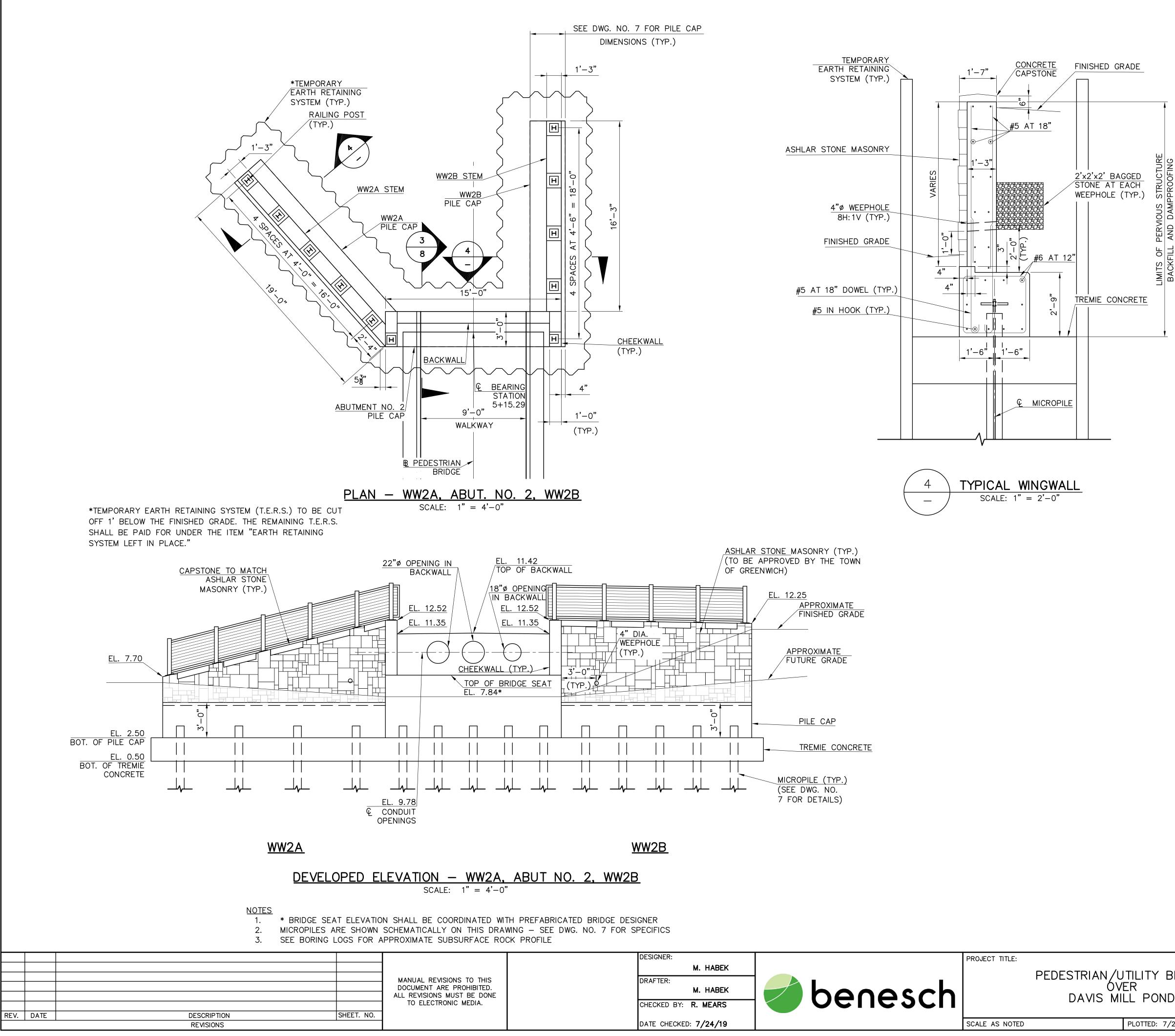
DEVELOPED ELEVATION - WW1B, ABUT NO. 1, WW1A SCALE: 1'' = 4' - 0''

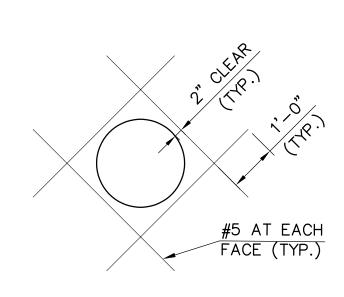
<u>NOTES</u> * BRIDGE SEAT ELEVATION SHALL BE COORDINATED WITH PREFABRICATED BRIDGE DESIGNER 1. MICROPILES ARE SHOWN SCHEMATICALLY ON THIS DRAWING - SEE DWG. NO. 7 FOR SPECIFICS 2. SEE BORING LOGS FOR APPROXIMATE SUBSURFACE ROCK PROFILE MANUAL REVISIONS TO THIS DOCUMENT ARE PROHIBITED. ALL REVISIONS MUST BE DONE TO ELECTRONIC MEDIA. SHEET. NO. REV. DATE DESCRIPTION REVISIONS

<u>WW1A</u>

DESIGNER: M. HABEK DRAFTER: M. HABEK CHECKED BY: R. MEARS	benesch	PROJECT TITLE: PEDESTRIAN/U OV DAVIS M	/ER
DATE CHECKED: 7/24/19		SCALE AS NOTED	PLC

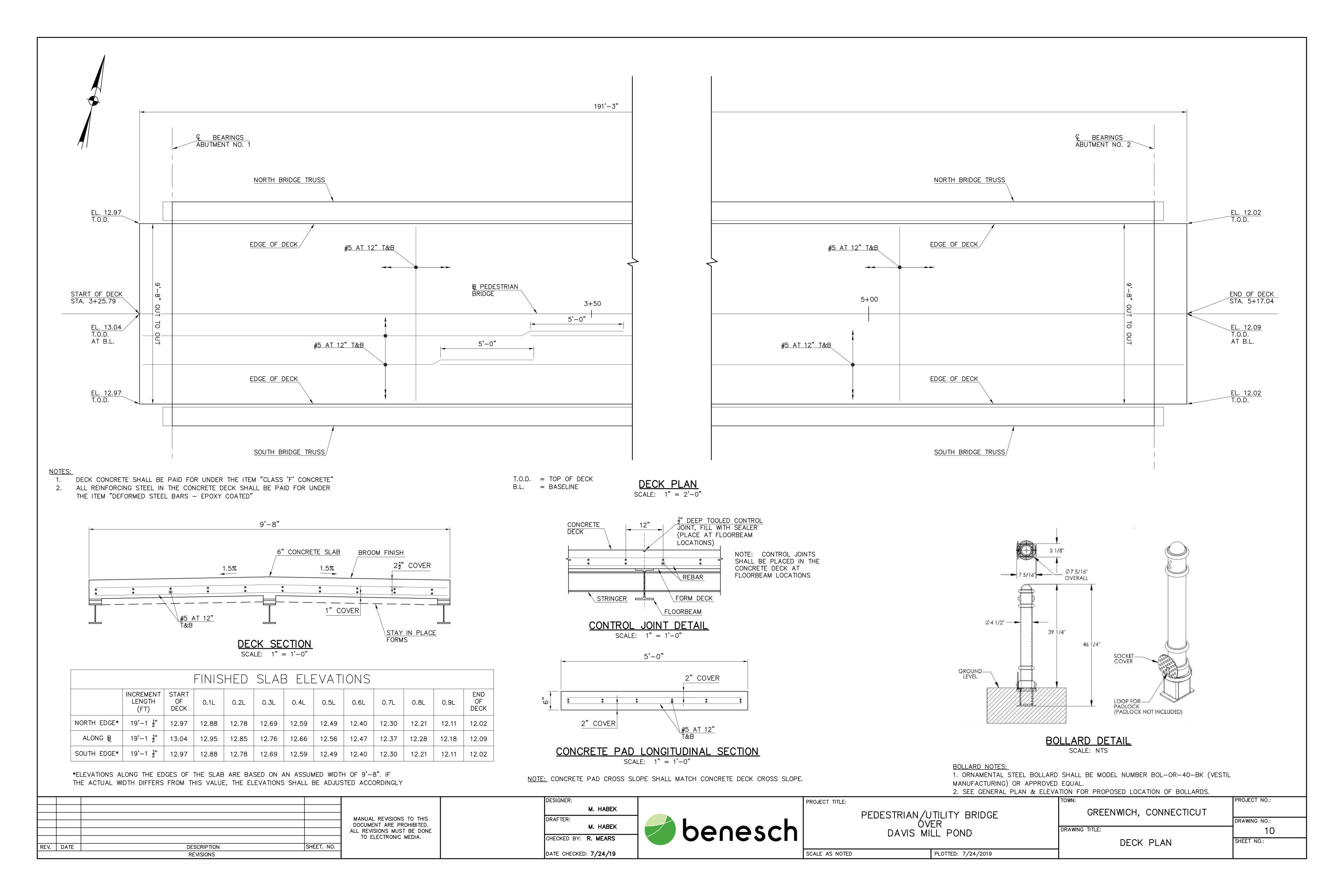


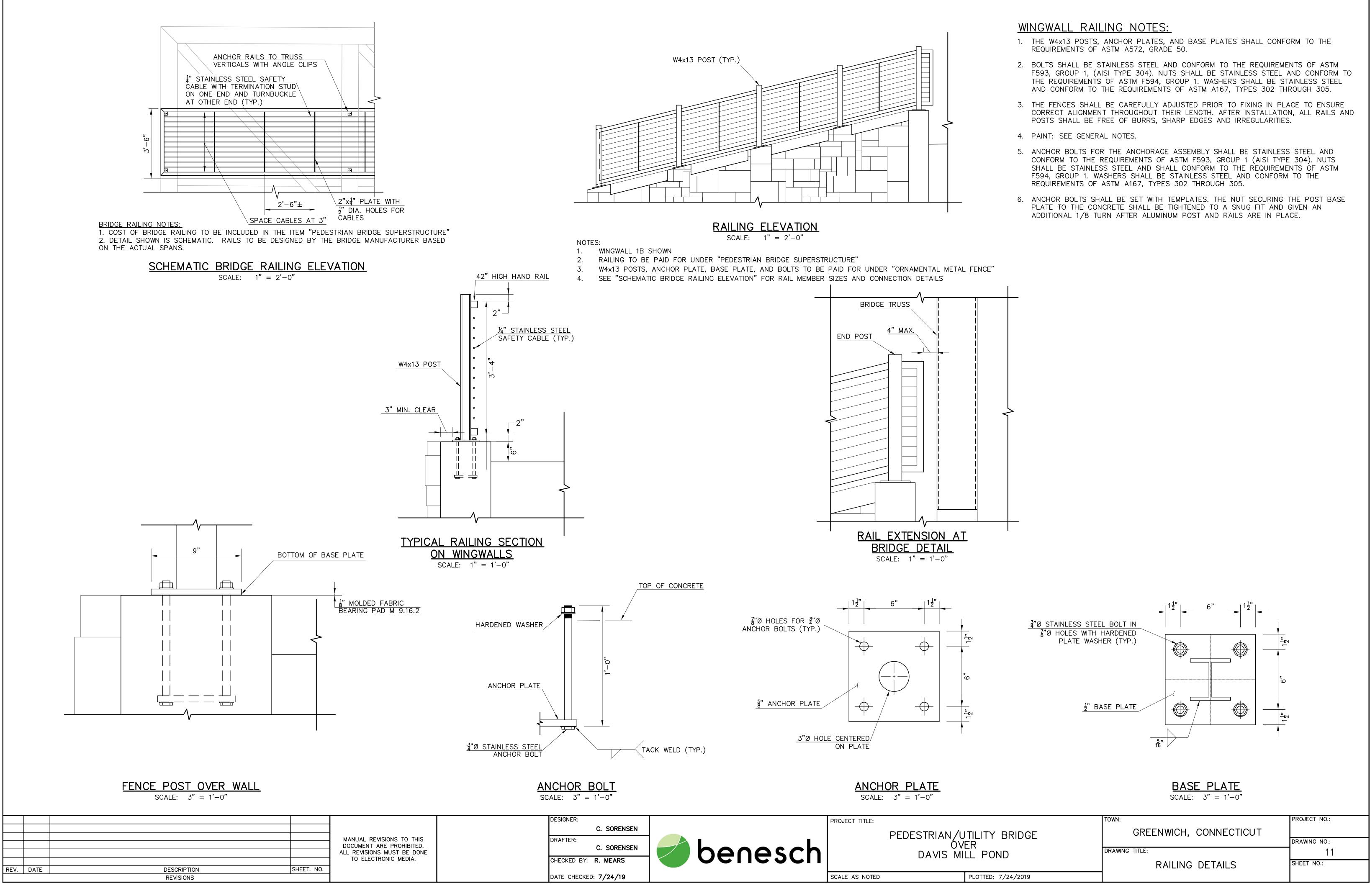


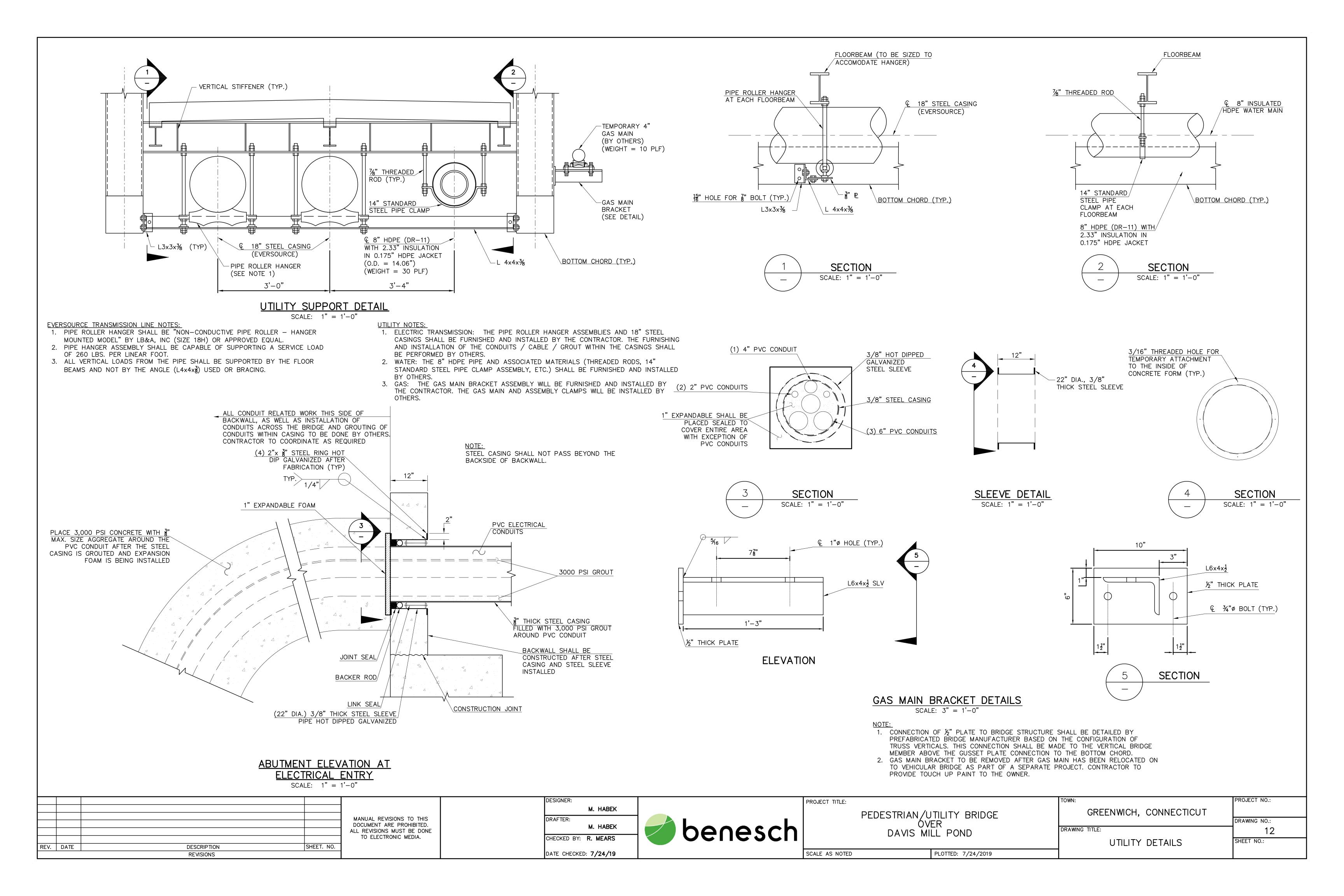


ADDITIONAL REINFORCEMENT AROUND PIPE OPENING SCALE: 1" = 2' - 0"

	TOWN:	PROJECT NO.:
JTILITY BRIDGE	GREENWICH, CONNECTICUT	
ÆR		DRAWING NO.:
	DRAWING TITLE:	9
	ABUTMENT NO. 2	SHEET NO.:
PLOTTED: 7/24/2019	AND WINGWALLS 2A/2B	







ATTACHMENT B

SUMMARY OF FLOOD IMPACT ANALYLSES: PEDESTRIAN/UTILITY BRIDGE OVER DAVIS MILL POND (Correspondence from Town of Greenwich's Engineering Consultant)



Alfred Benesch & Company 120 Hebron Avenue, Floor 2 Glastonbury, CT 06033 www.benesch.com P 860-633-8341 F 860-633-1068

September 4, 2019

Ms. Kathleen Shanley Eversource Energy Manager – Transmission Siting 59 Prospect Street Hartford, CT 06141

RE: Greenwich Substation and Line Project: Indian Harbor/Davis Mill Pond Crossing Analysis Regarding the Pedestrian/Utility Bridge and 100-Year Flood

Dear Ms. Shanley:

Alfred Benesch & Company, as the engineering consultant to the Town of Greenwich, hereby provides to Eversource Energy a Flood Impact Analysis Summary that details the analysis undertaken to demonstrate that the planned pedestrian/utility bridge over Davis Mill Pond will not be affected by a 100-year flood event as defined by the Federal Emergency Management Agency. The proposed pedestrian/utility bridge crosses over Davis Mill Pond which is just north of the Davis Avenue Vehicular bridge over Indian Harbor/Davis Mill Pond. This information is submitted to you in fulfillment of the request from the Connecticut Siting Council in its May 23, 2019 approval of the Development and Management Plan for the Indian Harbor Crossing

Sincerely,

Alfred Benesch & Company

Steven J. Drechsler, PE Senior Project Manager/ Public Infrastructure Group Manager

FLOOD IMPACT ANALYSIS SUMMARY PEDESTRIAN/UTILITY BRIDGE OVER DAVIS MILL POND TOWN OF GREENWICH

The pedestrian/utility bridge that will be constructed over the tidally-influenced Davis Mill Pond within Bruce Park in the Town of Greenwich, Fairfield County (referred to in the Greenwich Substation and Line Project [GSLP] as the Indian Harbor crossing) have incorporated design loads to withstand riverine and coastal flood events into the contract construction documents. The planned bridge will connect pedestrian paths within Bruce Park (the current sidewalk connecting the two parts of the Park extends adjacent to the Davis Avenue bridge) and, in addition to an approximately 9-foot-wide pedestrian walkway, will support Eversource Energy's two new 115-kilovolt (kV) transmission cables (being constructed as part of the GSLP) and an 8-inch diameter Aquarion Water Company water main.

As described below, the bridge design incorporates the consideration of the latest Federal Emergency Management Agency (FEMA) flood mapping and the results of hydraulic modeling studies, which were performed to assess the potential effects of flooding (including storm surge from Long Island Sound) and the critical surge velocity that the bridge would have to be constructed to withstand.

As illustrated on the attached Figure 1, the planned pedestrian/utility bridge will be located between two existing highway bridges: specifically, it will be situated 50 feet upstream of the Davis Avenue vehicular bridge and 700 feet downstream of the I-95 bridge. Davis Mill Pond is fed from the north by Greenwich Creek and is an impoundment of the creek; the pond is tidally influenced and is connected to Indian Harbor via a dam/weir structure at the Davis Avenue bridge. Thus, the pedestrian/utility bridge will be situated at the upper end of tidal influence from Long Island Sound; Indian Harbor, an embayment that connects directly to the Sound, is located south of the Davis Avenue bridge.

In 2013, FEMA issued revised base flood elevation maps for Fairfield County, including the Town of Greenwich. The 2013 FEMA mapping identifies the area of the proposed location of the pedestrian/utility bridge (as well as adjacent areas within Bruce Park) as entirely within Special Flood Hazard Area Zone AE. FEMA Zone AE denotes an area expected to be subject to inundation by the 1% annual chance flood (100-year flood event), or base flood. The FEMA-designated base flood elevation (BFE) for the pedestrian/utility bridge area is 13 feet NAVD88. (Refer to Figure 2, excerpt from the FEMA Flood Insurance Rate Map dated July 8, 2013 from the Fairfield County Flood Insurance Study.) The bridge will not be within either a floodway or a FEMA Zone VE – that is, a coastal flood zone with a velocity hazard (wave action).

FEMA's hydraulic modeling of flood elevations at Davis Mill Pond (i.e., the 13 feet NAVD88) reflects the consideration of influences from both tidal backwater from Long Island Sound and upstream flows from Greenwich Creek. The flood elevation is the result of a storm surge of Long Island Sound which will inundate Bruce Park. The Davis Avenue Bridge acts as a buffer to reduce the impacts of a storm surge from the Long Island Sound.

The pedestrian/utility bridge, which will be a single 187.75-foot steel truss span with a concrete walkway, will cross the limits of the Davis Mill Pond water surface at the Connecticut Coastal Jurisdiction Line (CJL) elevation of 5.5 feet. The tidal range is about 7.5 feet; the estimated mean high-water elevation at the planned bridge is 4.6 feet. The pedestrian walkway elevation will vary between elevation 13.04 feet at

the west abutment and 12.10 feet at the east abutment. The low chord¹ of the bridge will range from 9.44 feet at the west abutment and 8.5 feet at the east abutment. Both abutments will be above the mean high water and CJL.

Eversource's 115-kV electric transmission cables will be placed within two 18-inch diameter steel casing pipes that will be supported under the pedestrian walkway. The steel casing pipes, and their support hangers will not project below the low chord² of the bridge span. The bridge will project approximately 4.5 feet below the FEMA 1% annual chance flood elevation of 13. feet.

To determine the critical flow velocity that would impact the bridge structure, a hydraulic analysis was performed utilizing various tide and riverine conditions. The critical flow velocity calculated at the upstream face of the bridge was 1.22 feet per second. The resultant force on the bridge structure projecting below the flood water surface is 9.3 pounds per linear foot of bridge span. A resultant force on the 18-inch diameter steel pipes that will be below the flood elevation was calculated to be 4.5 pounds per linear foot of exposed pipe.

Taking into account the results of the hydraulic modeling, the utility supports for the electric transmission cable casings were specified to be capable of resisting the lateral load of 4.5 pounds per linear foot (as noted above) and the proposed bridge truss was specified to be capable of withstanding the calculated 9.3 pounds per linear foot (as also noted above).

The contract documents for the construction of the bridge contain a performance specification for the pedestrian/utility truss bridge and associated utility support systems. This specification calls for the submittal of design calculations incorporating all loads imposed onto the bridge and utility support structures, including those from the 100-year storm event. The calculations shall be performed by a structural engineer licensed in the State of Connecticut and shall be submitted for review and approval by Eversource prior to fabrication and installation.

In summary, the impacts of the 100-year flood event at the location of the proposed utility/pedestrian bridge and associated utility supports crossing have been analyzed and the results of this analysis have been incorporated into the contract documents for the construction of this bridge. In accordance with these requirements, the proposed bridge would not be adversely impacted by the 100-year storm event.

¹ Low chord" refers to the lowest structural element of the bridge; see the engineering drawings in Attachment A.

