

445 Hamilton Avenue, 14th Floor White Plains, New York 10601 Tel 914.761.1300 Fax 914.761.5372 www.cuddyfeder.com

December 18, 2015

BY EMAIL & FEDEX

Hon. Robert Stein, Chairman and Members of the Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re:

Development and Management Plan ("D&M Plan") Amendment

Connecticut Siting Council Docket No. 449

Telecommunications Facility at Redding Ridge Fire Department

186 Black Rock Turnpike, Redding, Connecticut

Dear Chairman Stein and Members of the Council:

On behalf of Message Center Management, Inc. ("MCM"), and in furtherance of the captioned Certificate, please accept for review and Siting Council ("Council") approval this amendment ("D&M Plan Amendment") to the Development Management Plan ("D&M Plan") approved by the Council on September 17, 2015 for the captioned Facility as approved in Docket No. 449.

Subsequent to the September 17, 2015 D&M Plan approval MCM consulted with a number of different construction firms as part of a bidding process. These consultations revealed a unanimous concern with the size of the equipment required for installation of the foundation and the nature of the confined space at the site. While construction is feasible, contractors felt this was not a prudent option and expressed concerns about completing the construction process.

Further consultation with contractors revealed however that a "pad and pier" foundation design would not require the same size equipment for foundation construction and would reduce greatly the potential for damage to existing structures or equipment on site. The difficult logistics of constructing the foundation proposed in the original D&M Plan demands a construction solution of less potential impact and that in turn requires removal of the existing tower prior to construction.

The final foundation will be 25' x 25' and is in keeping with the recommendations of the geotechnical engineering report included in the original August 19, 2015 D&M Plan filing. The tower location, compound size, equipment, and other features of the facility remain as approved in the original D&M Plan with the need for a larger foundation, construction sequencing and a temporary tower and being the only changes in this D&M Plan Amendment.

Accordingly, enclosed please find a D&M Plan Amendment for Council review and approval which includes a pad and pier design along and revised construction sequencing including removal of the of the existing tower installation of a temporary freestanding tower. The temporary tower will be approximately 60' AGL in height with antennas extending to 80' AGL and will be the same height as the existing tower. MCM estimates that the temporary tower will



be in place approximately 6-8 weeks and removed once construction of the new approved tower is complete.

The tower still incorporates a yield point to ensure the setback radius remains within the boundaries of the subject property and a revised structural analysis incorporating the new foundation design is included and is described in the November 13, 2015 letter from Valmont Structures included in this submission (four copies of the calculations are being bulk filed to minimize the size of this filing). The final site plans including specifications for the antennas, equipment compound, radio equipment, access utilities and emergency backup details of the associated compound and access drive remain unchanged. Of note, the D&M Plan also includes construction sequencing and site preparations, drainage, and erosion and sedimentation control measures consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control as amended.

In furtherance of this request, enclosed please find an original and fifteen (15) sets of 11" x 17" D&M Plan Amendment drawings prepared by All Points Technology Corporation ("APT") last revised December 10, 2015 being filed in accordance with the Council's Decision and Order dated November 3, 2014. Two full sized sets of the D&M Plan drawings are also enclosed.

Should you have any questions or require further information please do not hesitate to contact me. We thank you for your consideration of the enclosed.

Very truly yours,

Daniel M. Laub

Attachments & Enclosures

cc: Redding Fire District No. 1

Hon. Julia Pemberton, First Selectman, Town of Redding

Aimee Pardee, M.A., ZEO, Town of Redding

Maria Scotti, MCM

Virginia King, MCM

Christopher Gelinas, MCM

Scott Chasse, P.E., APT

Michael Libertine, APT

Dean Gustafson, APT

Michele Briggs, AT&T

Christopher B. Fisher, Esq.



CERTIFICATE OF SERVICE

I hereby certify that on this day, an original and 15 copies of the foregoing was sent electronically and by overnight delivery to the Connecticut Siting Council with copy to:

Intervenor:

Cellco Partnership d/b/a/ Verizon Wireless Kenneth C. Baldwin, Esq. Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103-3597 kbaldwin@rd.com

Facility Site Owner: Redding Ridge Fire District No. 1 Bennet Pardee, Fire Commissioner 186 Black Rock Turnpike, Redding, CT 06896

Dated: December 18, 2015

Daniel M. Laub, Esq.



November 13, 2015

Ref: Design and Failure Modes for a 150-ft AGL Tapered Monopole

Quality of Steel and Fabrication of a Monopole Structure

Valmont Project No. 239975

Site: Redding-Blackrock Tower, CT

Pole Designed with a maximum Theoretical Fall Radius of 21'.

In order to assure you of the high quality of all Valmont products, we would like to offer the following comments:

- Communications monopole structures designed by Valmont are sized in accordance with the latest governing revision of the ANSI/TIA 222 standard unless otherwise requested by our customer. This standard has been approved by ANSI/ASCE-7, which has dealt with the design of antenna support structures for over 40 years. The TIA standard, based on provisions of this nationally known specification, has a long history of reliability. At its core philosophy is its first and foremost priority to safeguard and maintain the health and welfare of the public.
- The TIA standard designates a minimum wind loading for each county in the United States.
 Valmont uses the wind loading listed in the TIA standard unless a greater value is specified by our customer. Structures are also designed for radial ice at a code specified reduced design wind loading. Code designated coefficients are used to ensure that the structure will survive the designed wind speed. The structure can usually survive even a greater wind load than the basic design wind speed because of these conservative coefficients.
- Design and loading assumptions that are used for the analyses of these structures are very conservative in nature when compared to other codes, which makes structural failure highly improbable.
- Failure of a steel monopole occurs when a point is reached where the induced stresses exceed the
 yield strength of the material. At this point, the deflections induced in the material are no longer
 temporary. Hence, a permanent deflection in the monopole would exist.
- The term failure above refers to local buckling at a designated point on the pole. Local buckling
 does not cause a free falling pole; rather it relieves the stresses from the pole at this location.
 Monopoles are flexible, forgiving structures, which are not generally susceptible to damage by
 impact loads such as wind gust or earthquake shocks.
- When local buckling occurs, a relatively small portion of the shaft distorts and "kinks" the steel. When the pole begins to bend the exposure area is reduced and therefore, the force due to wind is decreased as well. Even though buckling exists, the cross section of the pole is capable of carrying the entire vertical load. Therefore, wind induced loads could not conceivably bring this type of structure to the ground due to the excellent ductile properties, design criteria, and failure mode.
- Valmont's communication poles have proven to be very reliable products. Valmont has provided structures that have performed well during earthquakes in California, hurricanes in the South (including Hugo, Andrew, Opal and Katrina), and a number of tornadoes. In over 25 years of engineering and fabricating thousands of monopoles, to our knowledge Valmont has never experienced an in service failure of a communication pole due to weather induced overloading, even though, as in the cases of Hurricanes Hugo, Andrew and Katrina, the wind speeds exceeded the design wind speed. We use the latest standards, wind speed information, and sophisticated analytical tools to ensure that we maintain our unblemished record for quality.



Valmont Quality of Steel and Manufacturing:

- Monopoles are fabricated from ASTM A572 Grade 65 material with a controlled silicon content of 0.06% maximum to ensure a uniform galvanized coating. The base material is fabricated from Grade 50 material. All plate material meets a V-Notch toughness requirement of 15 ft-lbs. @ -20 degrees Fahrenheit. By meeting the strict toughness requirement, monopoles are best suited to resist the cyclic/fatigue type loading (i.e. wind induced loading) these structures exhibit.
- Valmont's anchor bolts are fabricated from A615 Grade 75 material. The bolts are 2 ¼ in diameter, made from #18J bar stock. Anchor bolts come complete with five (5) A194 Grade 2H hex nuts.
- For the past 40 years, our company has always guaranteed the quality of the steel used in building
 our structures. Material Certifications are available on all material at the time of fabrication.
 Fabrication of the monopole is performed in accordance with the provisions of the AISC Manual of
 Steel Construction and ASCE Design of steel Transmission Pole Structures. All welding and
 inspection is in accordance with the American Welding Society's Specification D1.1-latest revision.
 Testing and inspection reports are available upon request at the time of fabrication.

In addition, we have designed this monopole with a theoretical break point at approximately 131.5-ft elevation, by purposely over designing the pole sections below this point. In the unlikely event the pole were to fail at this point, the significant loading reduction caused by the removal of the tower wind area and weight above would greatly reduce any chance that the remaining tower would have any structural damage, thereby providing a theoretical failure zone of approximately 18.5-ft for the 150-ft AGL monopole.

I hope these comments address any issues that you might encounter relative to the anticipated performance of monopole structures and quality of steel fabrication. If you have additional questions or comments, I may be reached at 503-589-6626.

Sincerely,

Donatta

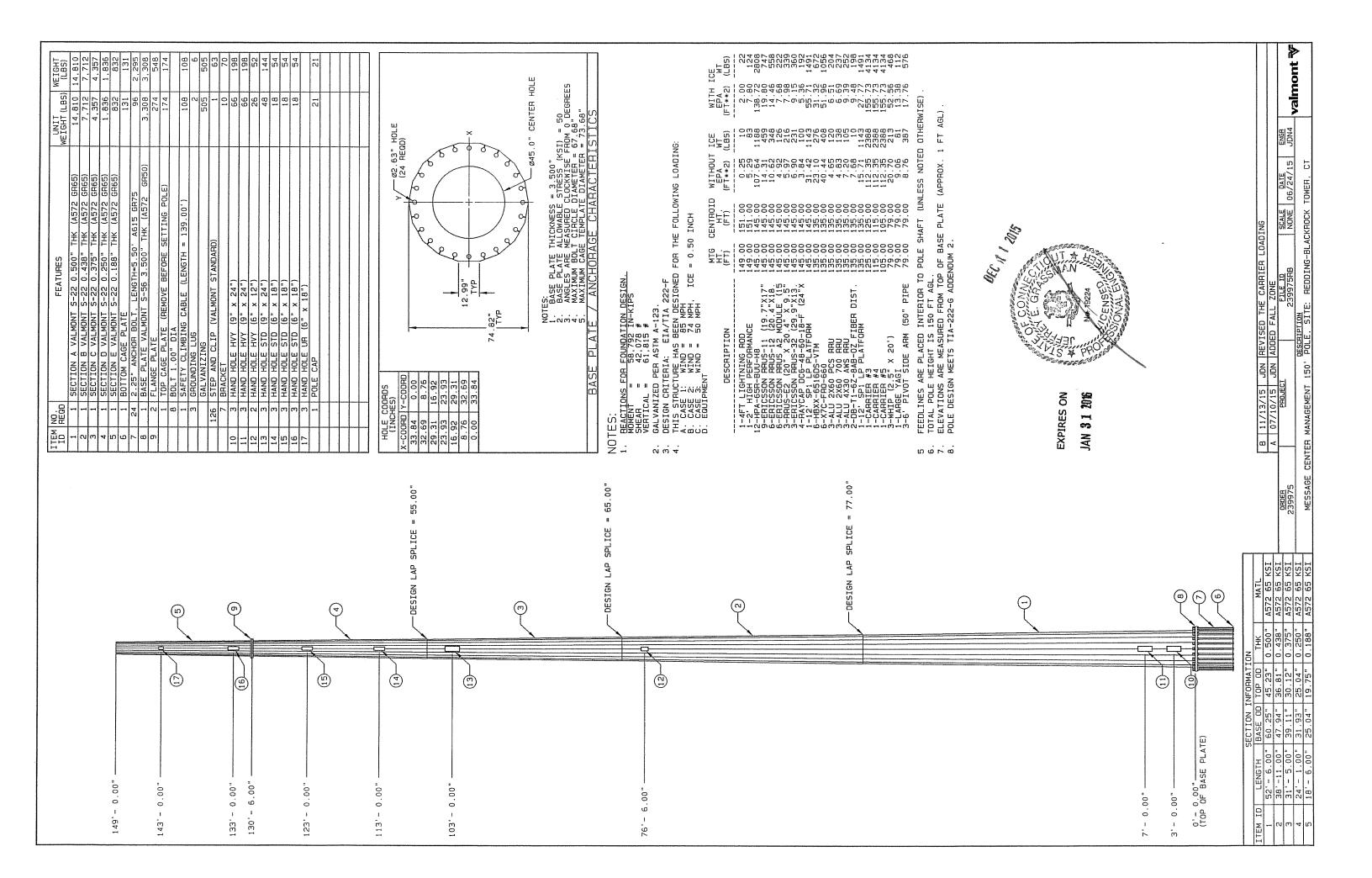
Jonathon Neumann Associate Engineer, EIT Valmont Microflect

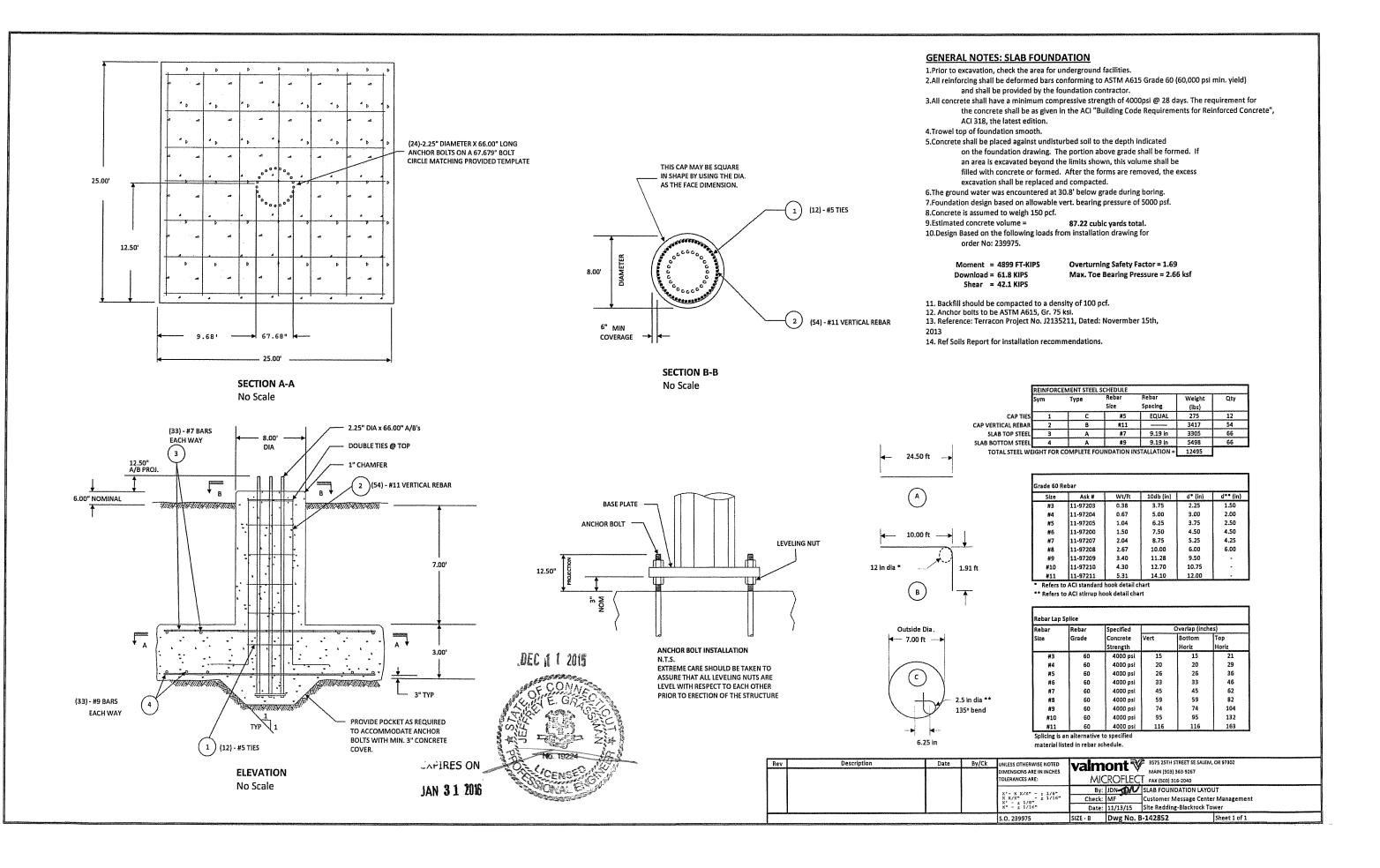
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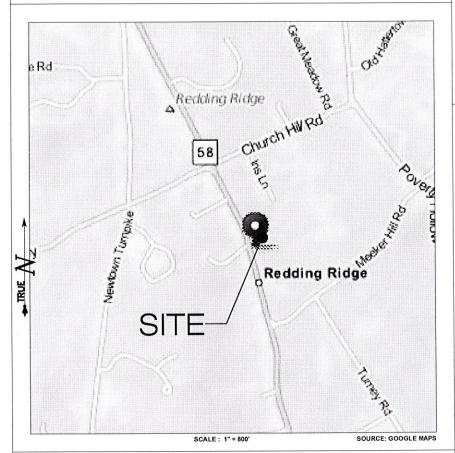
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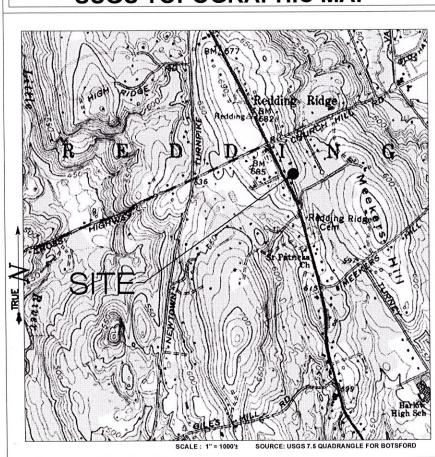




LOCATION MAP



USGS TOPOGRAPHIC MAP



SPRINGWICH CELLULAR LIMITED PARTNERSHIP





d/b/a at&t mobility

500 ENTERPRISE DRIVE ROCKY HILL, CT 06067



3 SADDLEBROOK DRIVE KILLINGWORTH, CT 06419 WWW.ALLPOINTSTECH.COM PHONE: (860)-663-1697 FAX: (860)-663-0935

CONTACT PERSONNEL

MESSAGE CENTER MANAGEMENT 40 WOODLAND STREET HARTFORD, CT 06105

> CO-APPLICANTS AT&T MOBILITY 500 ENTERPRISE DRIVE ROCKY HILL, CT 06067

> > LANDLORD

REDDING FIRE DISTRICT 1 PO BOX 45 REDDING, CT 06875

MCM PROJECT MANAGER:

VIRGINIA KING (860) 727-5790

MCM PROJECT ATTORNEY:

CUDDY & FEDER, LLP 445 HAMILTON AVE., 14TH FLOOR WHITE PLAINS, NY 10601 914-761-1300

POWER PROVIDER:

EVERSOURCE (203) 845-3487 RICHARD MATHIES - CASE #2299239

TELCO PROVIDER: FRONTIER: (800) 921-8102

CALL BEFORE YOU DIG: (800) 922-4455

GOVERNING CODEs: 2009 CONNECTICUT BUILDING CODE (2003 IBC BASIS) 2011 NATIONAL ELECTRIC CODE

SITE INFORMATION

REDDING RIDGE **186 BLACK ROCK TURNPIKE** REDDING, CT 06896

DEVELOPMENT & MANAGEMENT DOCUMENTS

REV.4:

REDDING RIDGE 186 BLACK ROCK TURNPIKE REDDING, CT 06896		SHEET NDEX
DESIGN TYPE:	APT FILING NUMBER: C	T-242-310
	APT DRAWING NUMBER	R: CT-505 T-1
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	CHECKED BY: SMC	DATE: 08/03/15
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EV.2: 12/02/15: TOWER REVISIONS: SMC	_ 5 40 8	/\A
FV.3: 12/10/15: TEMP TOWER REVS: SMC		

MESSAGE CENTER MANAGEMENT

40 WOODLAND STREET HARTFORD, CT 06105 OFFICE: (888) 973-7483

DEVELOPMENT & MANAGEMENT PLAN DRAWING INDEX

T-1 TITLE SHEET & INDEX

1 OF 1 EXISTING CONDITIONS SURVEY

MCM

R-1 ABUTTERS MAP

SP-1 SITE PLAN

SP-2 SEDIMENTATION & EROSION CONTROL PLAN

SP-3 DEMOLITION & ROOF LEADER PLAN

A-1 COMPOUND PLAN & TOWER ELEVATION

C-1 AT&T EQUIP. SHELTER PLAN & DETAILS

C-2 AT&T ANTENNA PLAN & DETAILS

C-3 VZW EQUIP. SHELTER PLAN & DETAILS

C-4 VZW ANTENNA PLAN & DETAILS

C-5 TOWN ANTENNA PLAN & DETAILS

S-1 COMPOUND DETAILS

S-2 COMPOUND DETAILS & ENVIRONMENTAL NOTES

M-1 MECHANICAL PLAN & DETAILS

E-1 ELECTRICAL PLAN & DETAILS

E-2 ELECTRICAL DETAILS

N-1 NOTES & SPECIFICATIONS

*SITE INFORMATION:

-SITE NAME:. -SITE ID NUMBER:. CT-505

-LATITUDE LONGITUDE -ELEVATION -

-FEMA/FIRM DESIGNATION -ACREAGE:

PANEL #09001C0265F - ZONE 'X'

41° 18' 35.77" N

73° 20' 51 35" W

636'± AMSL

REDDING RIDGE

186 BLACK ROCK TURNPIKE REDDING, CT 06896

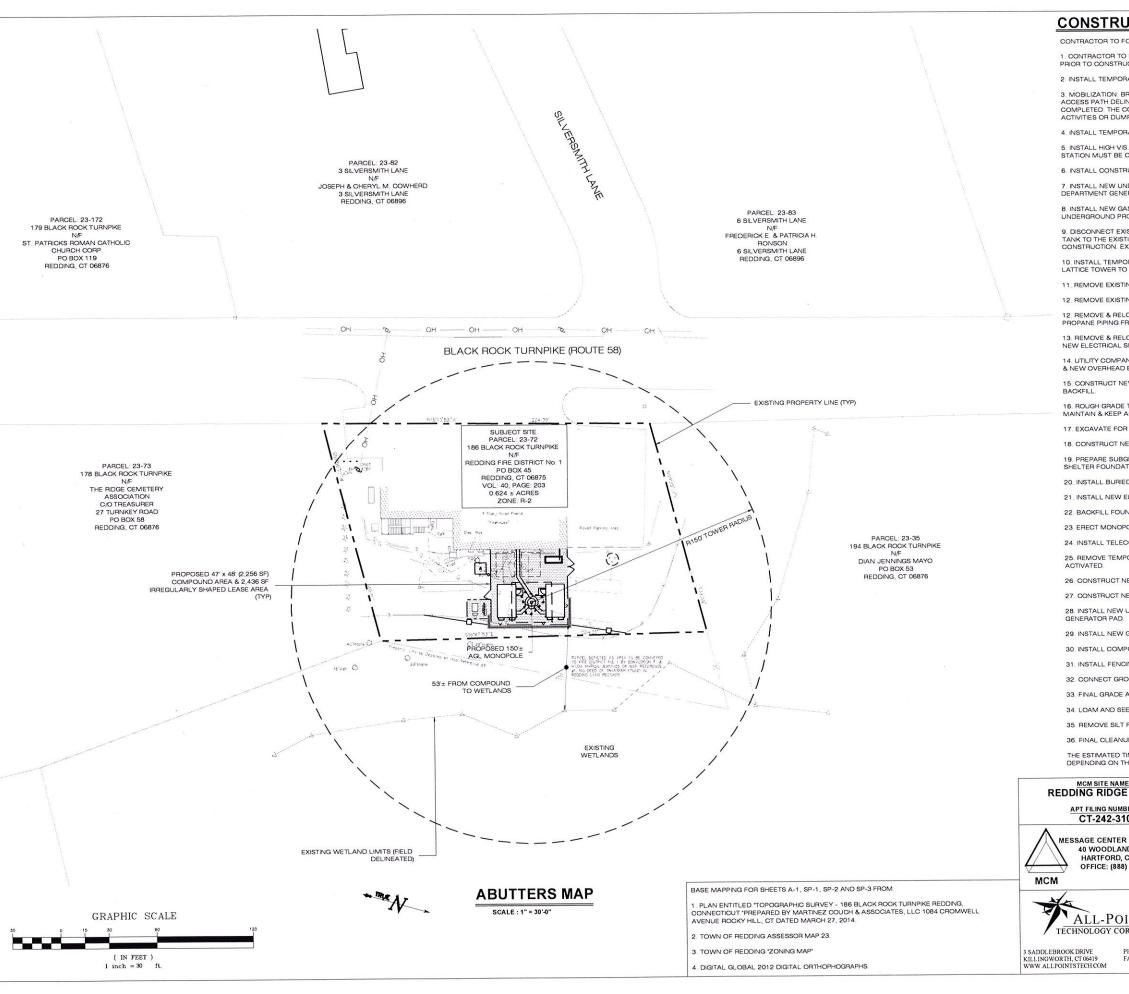
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TECHNOLOGY CORPORATION MEA.0: TO MY KNOWLEDGE AND BELLEY THIS MAP IS SUBSTANTALLY CORRECT AS NOTED HEREON GRAPHIC SCALE DATE: 03/27/14 CHECKED BA: YEM DEAWN BY: JBR SCALE: 17=20" MAN LAND APT DRAWING NUMBER: CT-505 APT FILING NUMBER: CT-242-310 DESIGN LABE: 186 BLACK ROCK TURNPIKE REDDING, CT 06896 CT-242-310 SURVEY KEDDING KIDGE **EXISTING CONDITIONS** REDDING RIDGE C1505 PERMITTING DOCUMENTS 0 | M Hydront

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THE RIDGE CEMETERY ASSOCIATION
178 BLACK ROCK TURNPIKE
VOL. 69 P. 68 NAME IN PAYENENT 3 Story Wood Frame PARCEL OWNER OF RECORD: REDDING FIRE DISTRICT NO. 1 IMC#H PARCEL ADDRESS: 188 BLACK ROCK TURNPIKE SAET ON BE ETEAVLIONS BYSED ON NVAD 1888 DVLDW NORTH CRIENTATION AND COORDINATES REfer to connecticut grid system had 83_{\odot} W. INCAE . 20¢∵2∂, MISSERGIN (PJ) D BLACK ROCK TURNPIKE 82 .TA SURVEY NOTES SILVERSMITH LANE ROPE & SER ROMBON ROMBON ROMBON JOSEPH & CHEŘYL M. COWHERD 3 SILVERSMITH LANE VOL. 365 P. 114 N/F
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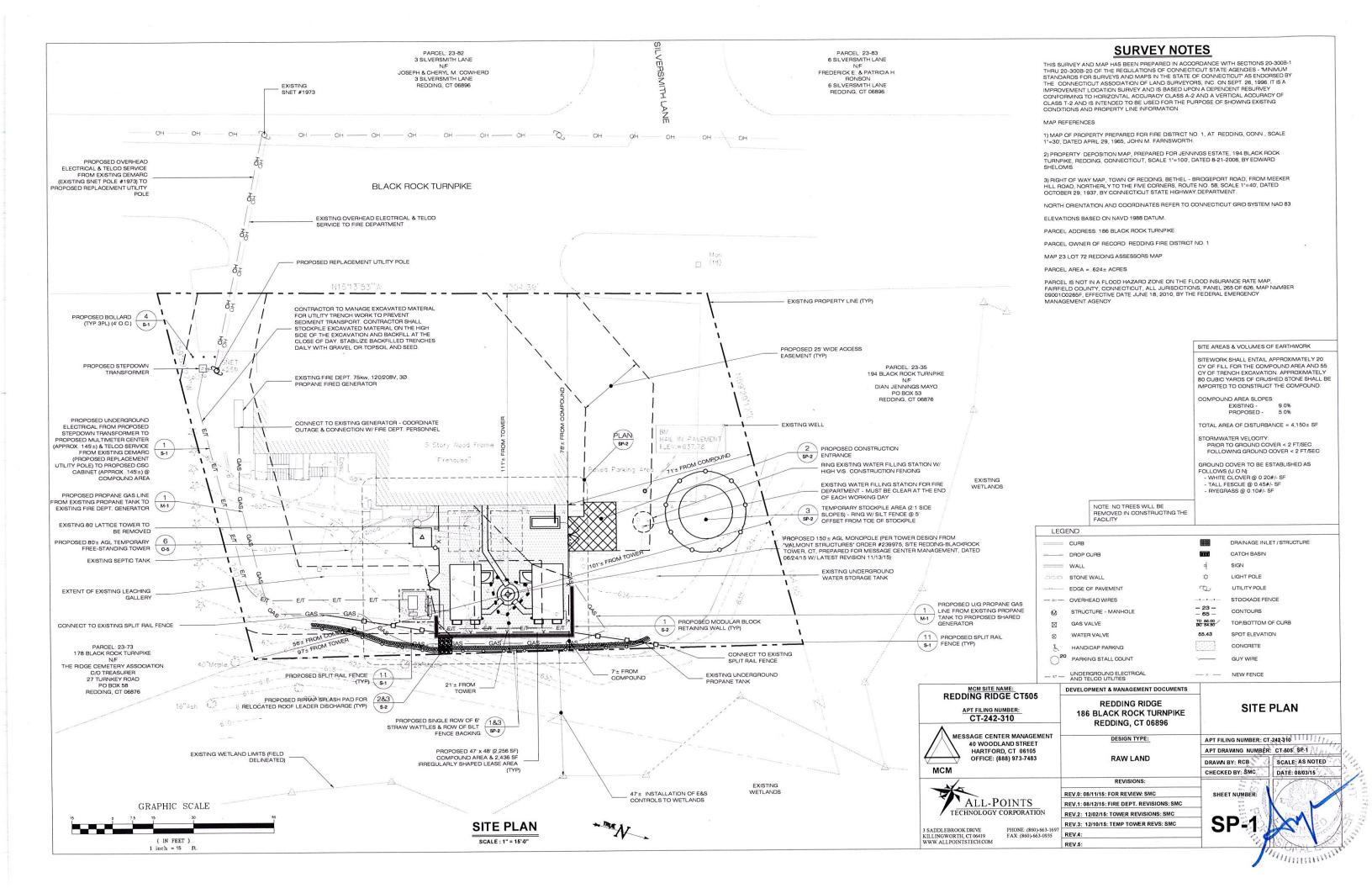


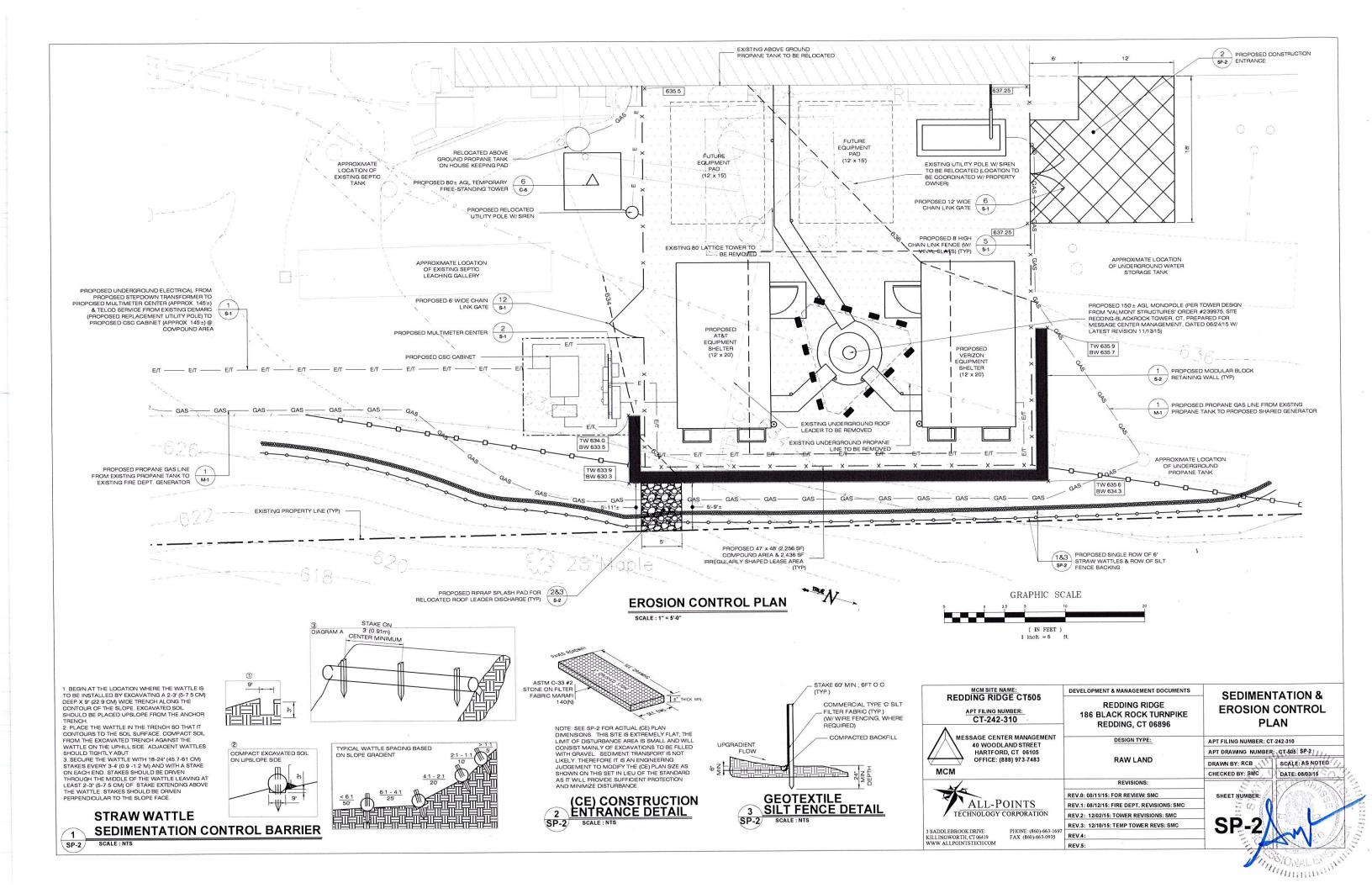
CONSTRUCTION SEQUENCING

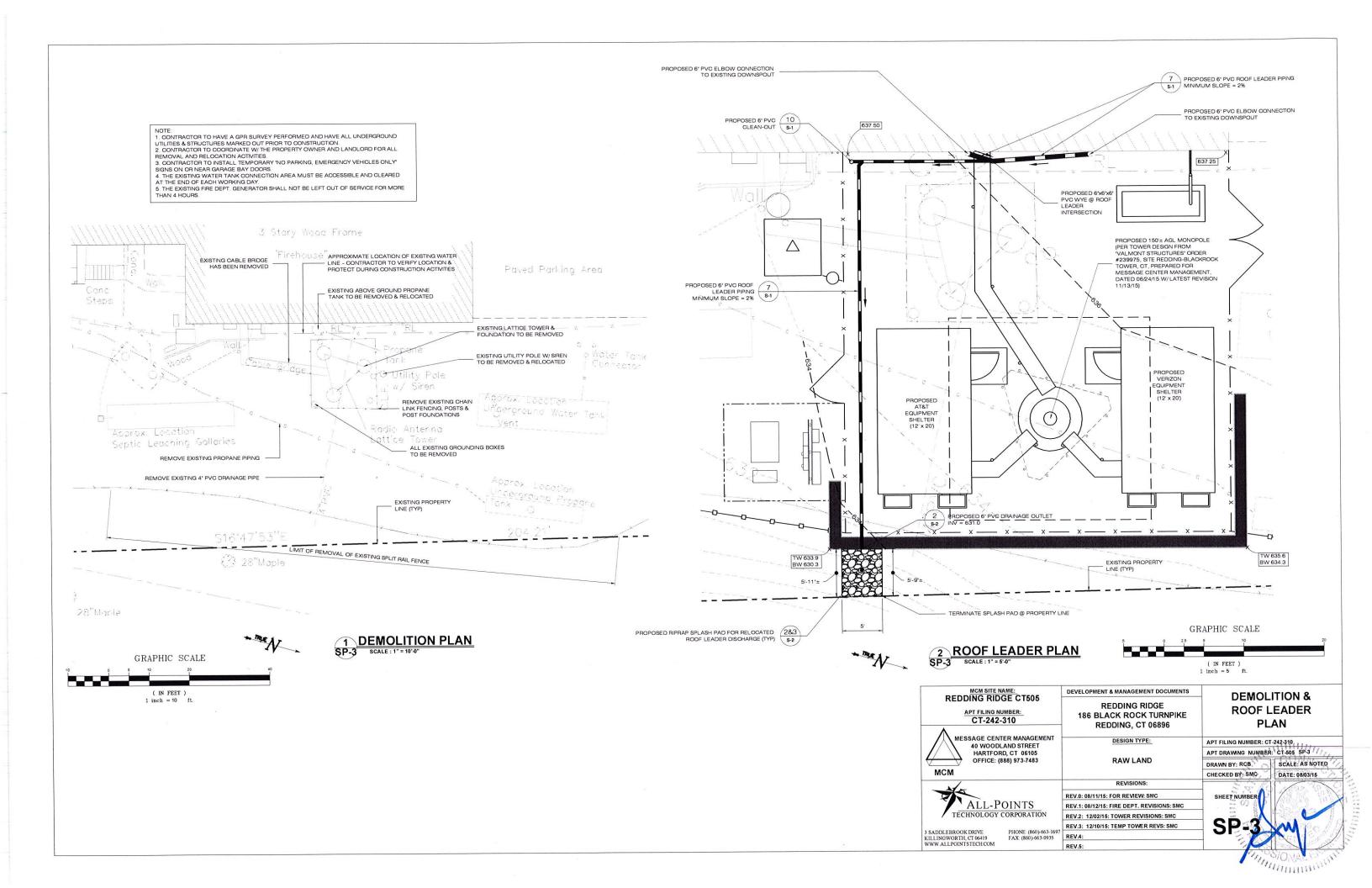
CONTRACTOR TO FOLLOW THE FOLLOWING CONSTRUCTION PHASING AS CLOSELY AS POSSIBLE

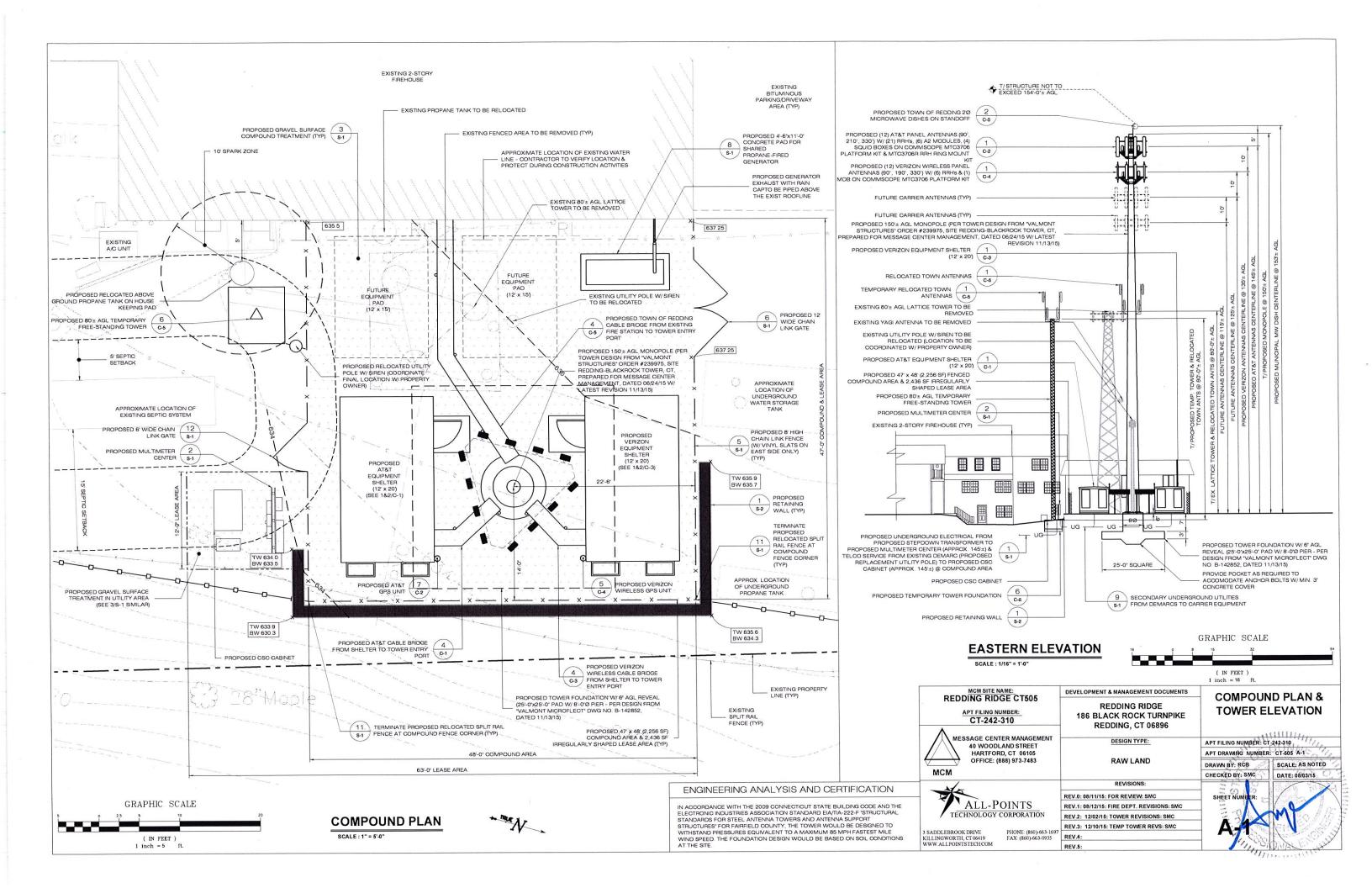
- 1. CONTRACTOR TO HAVE A GPR SURVEY PERFORMED AND HAVE ALL UNDERGROUND UTILITIES & STRUCTURES MARKED OUT
- 2 INSTALL TEMPORARY 'NO PARKING, EMERGENCY VEHICLES ONLY' SIGNS ON OR NEAR FIRE DEPT. GARAGE BAY DOORS.
- 3. MOBILIZATION, BRING MATERIAL AND EQUIPMENT TO SITE. ALL CONSTRUCTION TRAFFIC AND ACTIVITIES MUST RESIDE INSIDE ACCESS PATH DELINEATED, WITHIN STAGING AND STOCKPILE AREA, OR WITHIN AREA WHERE PROPOSED WORK IS BEING COMPLETED. THE CONTRACTOR IS TO PROTECT WETLANDS FROM DISTURBANCE AT ALL TIMES AND NO CONSTRUCTION ACTIVITIES OR DUMPING SHALL OCCUR IN THE WETLANDS.
- 4. INSTALL TEMPORARY EROSION AND SEDIMENTATION CONTROL BARRIERS
- 5. INSTALL HIGH VIS. CONSTRUCTION FENCING ALONG EXISTING UNDERGROUND STRUCTURES. EXISTING WATER FILLING STATION MUST BE CLEARED AND ACCESSIBLE AT THE END OF EACH WORKING DAY.
- 6. INSTALL CONSTRUCTION ENTRANCE
- 7. INSTALL NEW UNDERGROUND PROPANE GAS LINE FROM EXISTING UNDERGROUND PROPANE TANK TO EXISTING FIRE DEPARTMENT GENERATOR.
- 8. INSTALL NEW GAS SERVICE MANIFOLD AND CONNECT & ACTIVATE NEW UNDERGROUND PROPANE GAS LINE FROM EXISTING UNDERGROUND PROPANE TANK TO EXISTING FIRE DEPARTMENT GENERATOR.
- 9. DISCONNECT EXISTING UNDERGROUND PROPANE LINE AT BOTH ENDS THAT RUNS FROM EXISTING UNDERGROUND PROPANE TANK TO THE EXISTING FIRE DEPARTMENT GENERATOR AND REMOVE EXISTING PIPING WITHIN THE PROPOSED LIMITS OF CONSTRUCTION. EXISTING FIRE DEPT. GENERATOR SHALL NOT BE LEFT OUT OF SERVICE FOR MORE THAN 4 HOURS.
- 10. INSTALL TEMPORARY TELECOOMUNICATION TOWER ON SITE AND RELOCATE FIRE DEPARTMENT ANTENNAS FROM EXISTING LATTICE TOWER TO TEMPORARY TOWER AND RUN CABLES FROM RELOCATED ANTENNAS TO FIRE DEPARTMENT.
- 11. REMOVE EXISTING CHAIN LINK FENCE, FENCE POSTS & POST FOUNDATIONS.
- 12. REMOVE EXISTING LATTICE TOWER, ANTENNAS, CABLING, TOWER FOUNDATION & GROUNDING BOXES.
- 12. REMOVE & RELOCATE EXISTING ABOVE GROUND PROPANE TANK & ASSOCIATED PIPING INSTALL NEW ASSOCIATED PROPANE PIPING FROM NEW ABOVE GROUND TANK LOCATION TO EXISTING FIRE DEPARTMENT ENTRY PORT.
- 13. REMOVE & RELOCATE EXISTING UTILITY POLE, SIREN & ASSOCIATED ELECTRICAL SERVICE CONDUITS AND WIRING. INSTALL NEW ELECTRICAL SERVICE FROM NEW SIREN LOCATION TO NEW FIRE DEPARTMENT ENTRY PORT.
- 14. UTILITY COMPANY TO REMOVE EXISTING UTILITY POLE (SNET #4259) & INSTALL NEW REPLACEMENT UTILITY POLE, GUY WIRE & NEW OVERHEAD ELECTRIC AND TELCO SERVICE FROM EXISTING UTILITY POLE (SNET #1973) TO NEW REPLACEMENT POLE.
- 15 CONSTRUCT NEW ELECTRIC & TELCO UTILITY TRENCH & INSTALL CONDUITS TO NEW UTILITY AREA @ COMPOUND & BACKFILL.
- 16. ROUGH GRADE THE PORTION OF THE COMPOUND AREA IN THE AREA OF THE NEW TOWER AND SHELTERS (PROTECT, MAINTAIN & KEEP ACTIVE EXISTING LATTICE TOWER).
- 17. EXCAVATE FOR TOWER FOUNDATION AND EQUIPMENT SHELTER FOUNDATIONS
- 18. CONSTRUCT NEW ROOF LEADER DRAINAGE PIPING & SPLASH PAD.
- 19. PREPARE SUBGRADE AND INSTALL FORMS, STEEL REINFORCING, AND CONCRETE FOR TOWER FOUNDATION & EQUIPMENT SHELTER FOUNDATIONS.
- 20. INSTALL BURIED GROUND RINGS, GROUND RODS, GROUND LEADS, UTILITY CONDUITS, AND UTILITY EQUIPMENT.
- 21. INSTALL NEW ELECTRICAL & TELCO CONDUITS FROM NEW UTILITY AREA TO NEW EQUIPMENT SHELTERS.
- 22. BACKFILL FOUNDATION & EQUIPMENT SHELTER FOUNDATION
- 23. ERECT MONOPOLE.
- 24. INSTALL TELECOMMUNICATIONS EQUIPMENT ON TOWER AND IN COMPOUND.
- 25. REMOVE TEMPORARY TOWER ONCE FIRE DEPARTMENT ANTENNAS HAVE BEEN RELOCATED TO NEW TOWER AND
- 26. CONSTRUCT NEW RETAINING WALL.
- 27. CONSTRUCT NEW CONCRETE PAD FOR NEW SHARED GENERATOR.
- 28. INSTALL NEW UNDERGROUND PROPANE LINE FROM EXISTING UNDERGROUND PROPANE TANK TO NEW SHARED
- 29. INSTALL NEW GENERATOR & EXHAUST PIPING. CONNECT NEW PROPANE LINE.
- 30. INSTALL COMPOUND GRAVEL SURFACES.
- 31. INSTALL FENCING.
- 32. CONNECT GROUNDING LEADS AND LIGHTENING PROTECTION.
- 33. FINAL GRADE AROUND COMPOUND.
- 34. LOAM AND SEED DISTURBED AREAS OUTSIDE COMPOUND, AS REQUIRED.
- 35. REMOVE SILT FENCING AFTER SEEDED AREAS HAVE ESTABLISHED VEGETATION.
- 36. FINAL CLEANUP AND EQUIPMENT TESTING.
- THE ESTIMATED TIME FOR COMPLETION OF THE WORK IS APPROXIMATELY EIGHT (8) WEEKS. THE EXACT PROCESS MAY VARY DEPENDING ON THE CONTRACTORS. AND SUBCONTRACTORS AVAILABILITY TO COMPLETE WORK AND WEATHER DELAYS.

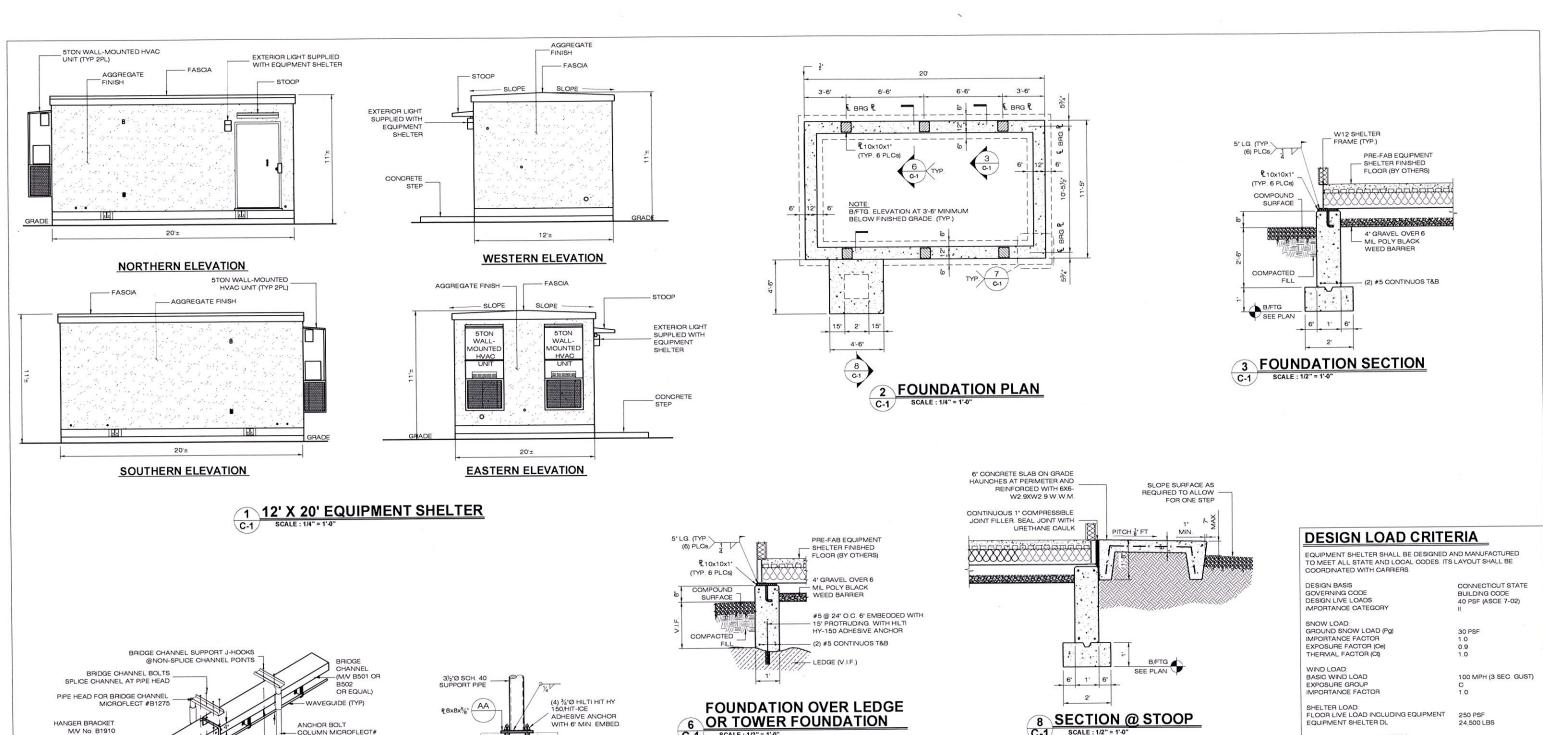
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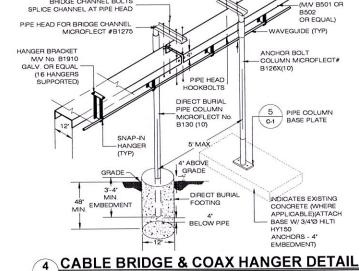


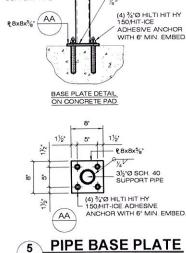












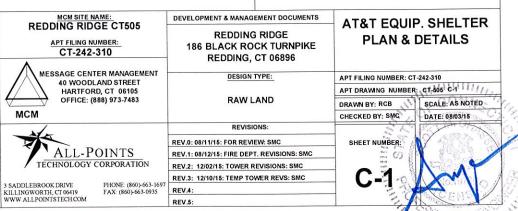


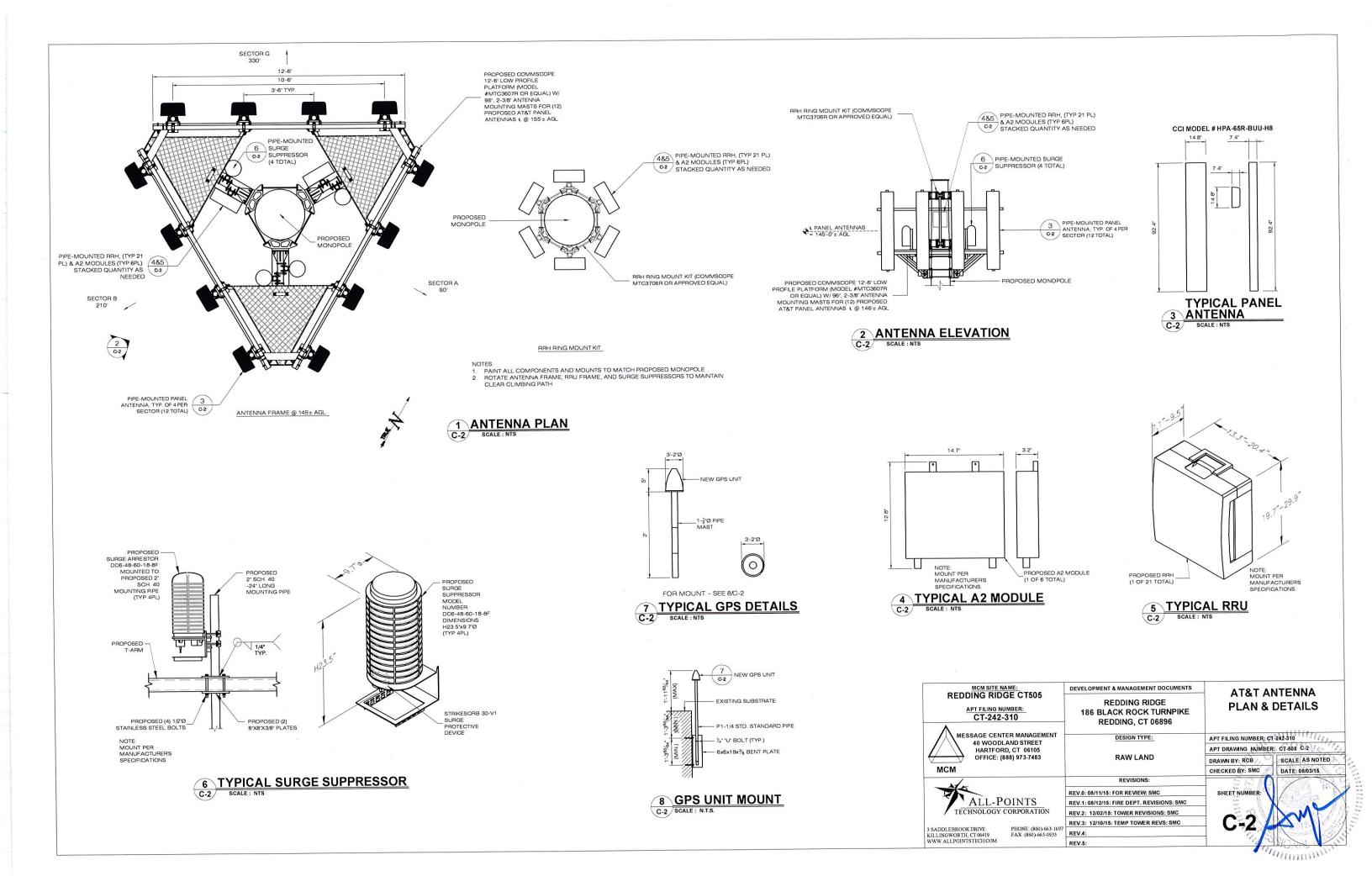


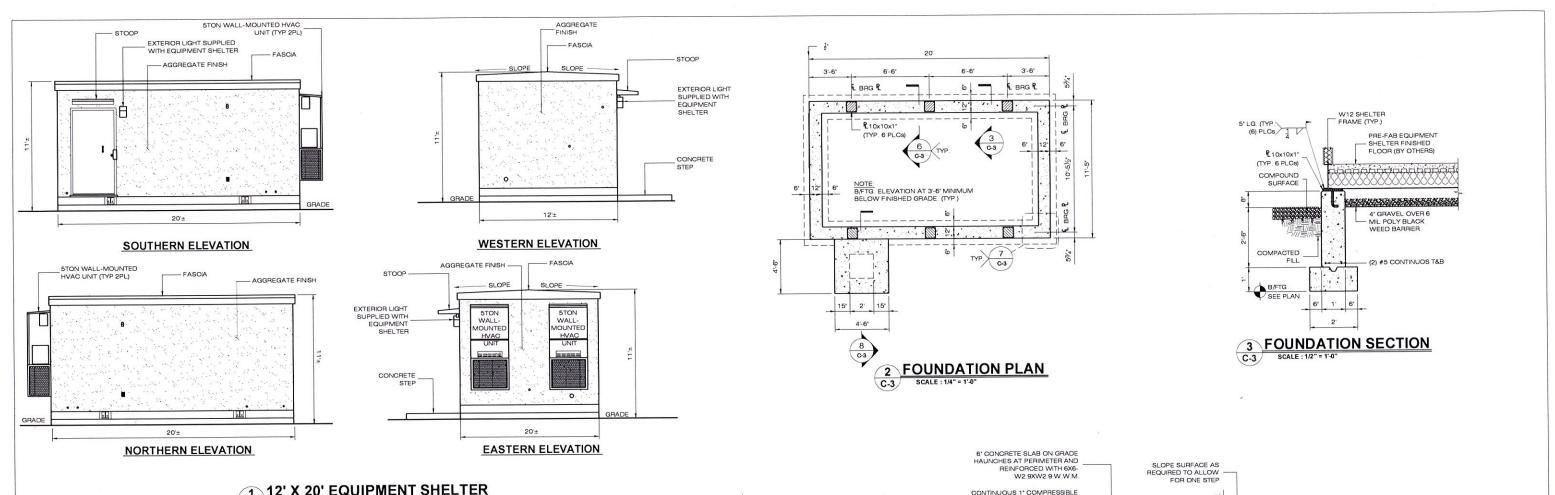
SITE CLASS D FOR UNKNOWN SOIL PROPERTIES

WILLIAM WALL

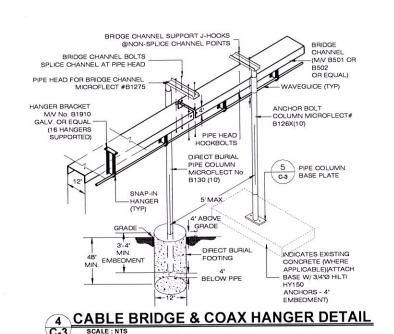
IMPORTANCE FACTOR

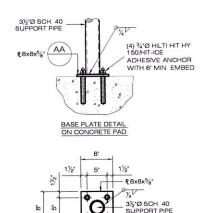










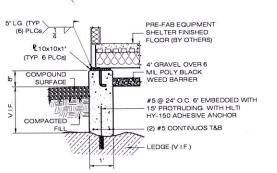




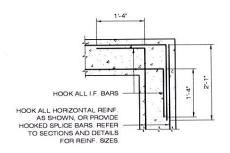
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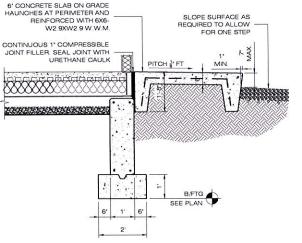
ANCHOR WITH 6' MIN. EMBED.



FOUNDATION OVER LEDGE OR TOWER FOUNDATION







SECTION @ STOOP

DESIGN LOAD CRITERIA

EQUIPMENT SHELTER SHALL BE DESIGNED AND MANUFACTURED TO MEET ALL STATE AND LOCAL CODES. ITS LAYOUT SHALL BE COORDINATED WITH CARRIERS

DESIGN BASIS GOVERNING CODE DESIGN LIVE LOADS CONNECTICUT STATE BUILDING CODE 40 PSF (ASCE 7-02) IMPORTANCE CATEGORY

SNOW LOAD: GROUND SNOW LOAD (Pg) IMPORTANCE FACTOR EXPOSURE FACTOR (Ce) THERMAL FACTOR (Ct)

WIND LOAD: BASIC WIND LOAD EXPOSURE GROUP IMPORTANCE FACTOR 100 MPH (3 SEC. GUST)

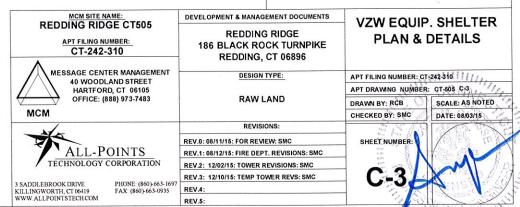
250 PSF

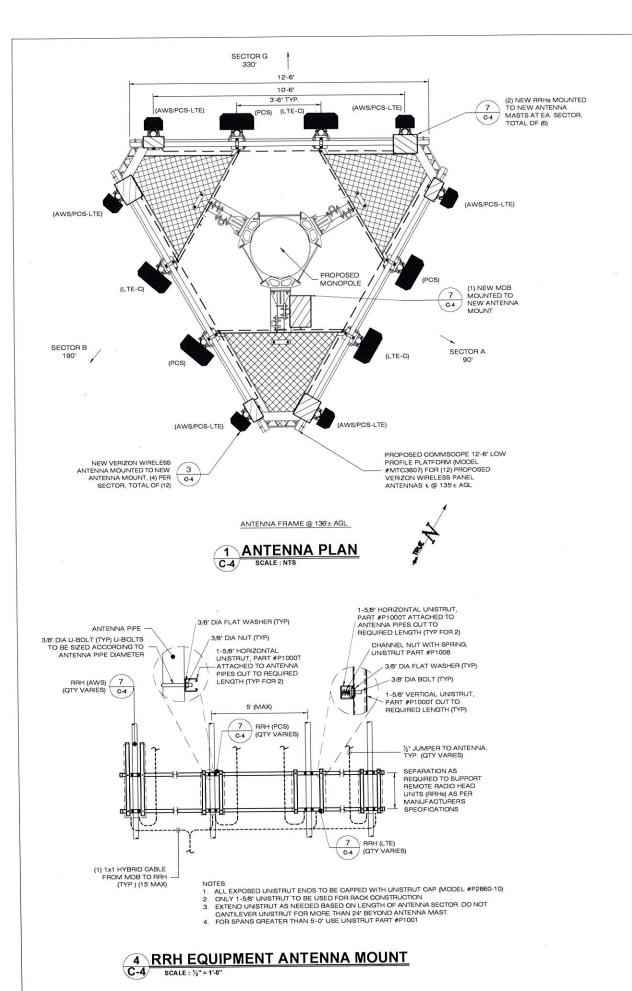
SHELTER LOAD. FLOOR LIVE LOAD INCLUDING EQUIPMENT EQUIPMENT SHELTER DL

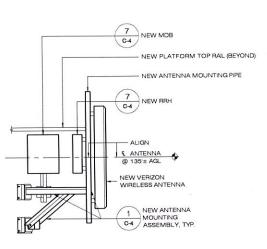
SEISMIC DESIGN PARAMETERS:

SEISMIC USE GROUP MCE SPECTRAL ACCELERATION SHORT (Sa) 0.288 0.066 D FOR UNKNOWN SOIL PROPERTIES MCE SPECTRAL ACCELERATION SHORT (SI) SITE CLASS

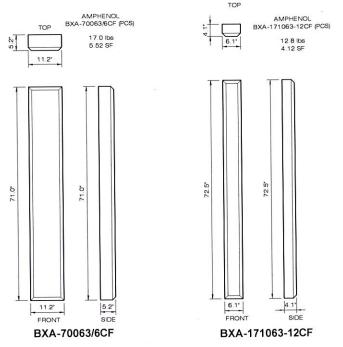
IMPORTANCE FACTOR



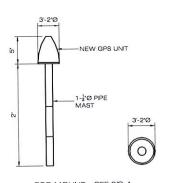




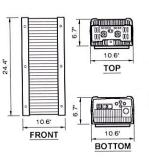
2 ANTENNA MOUNTING DETAIL C4 SCALE: NTS



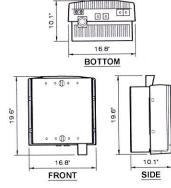




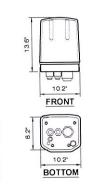
5 TYPICAL GPS DETAILS



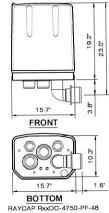
ALCATEL LUCENT FDD RRH 2x40W AWS REMOTE RADIO HEAD (RRH) WxDxH = 10.6'x6.7'x24.4' (43 Lbs)



ALCATEL LUCENT FDD RRH 2x40W 700 MHz REMOTE RADIO HEAD (RRH) WXDxH = 17"x10"x20" (51 Lbs)



RAYCAP RXXDC-4291-PF-48
OR RAYCAP RXXDC-1064-PF-48
SECTOR DISTRIBUTION BOX
(SDB) WXDXH =
10.15 x8.15 x13.58" (8.9 Lbs)



BOTTOM

RAYOAP RXXDC-4750-PF-48

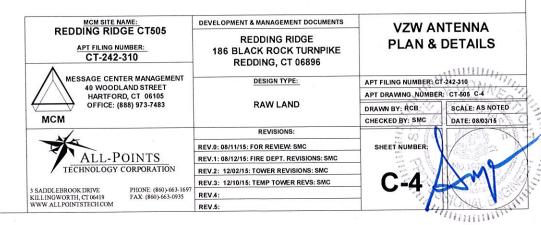
OR RAYCAP RXXDC-3315-PF-48

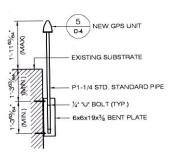
MAIN DISTRIBUTION BOX

(MDB) WXDXH =

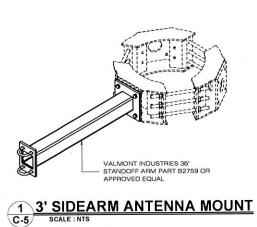
15.73'X10.25'X19.18' (21.4 Lbs)



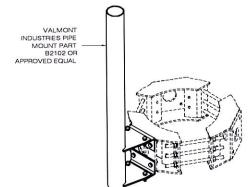




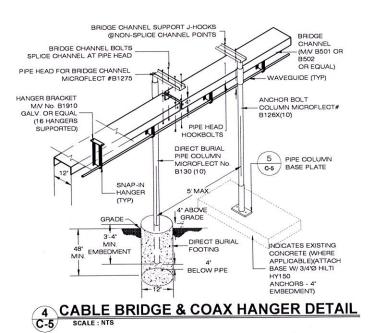
6 GPS UNIT MOUNT
C-4 SCALE: N.T.S.

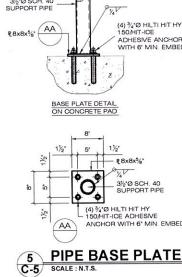


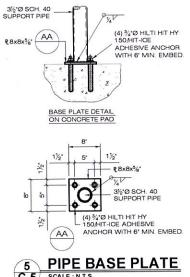












High Performance Series for RADIOWAVES THE LEADER IN MICROVAVE 4.4-5.0 GHz Frequencies ANTENNA INNOVATION

Key Features

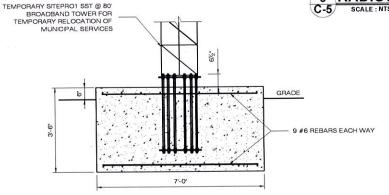
- High Performance antennas minimize interference as they have more stringent radiation side lobe and front-to-back
- Lightweight and rugged design
- Easily installed with our superior mounting system included with the antenna
- Some models are available with 7/16 DIN Connector. Please call the factory for availability
- Our industry leading 5-year warranty
- Radome is included
- Single (HP) and Dual (HPD) polarizatio are available



Model	Diameter	Frequency		Gain (di	31)	39B BM	X-Pol Rejection.	F/B Ratio	VSWR, Max	Antenna
Number	ft. (m)	GHz	Low	Med	High	degs	dB	dB	(R.L., ∉B)	Weight
HP2-4.7	2 (0.6)	4 4-5 0	25.8	26.4	29.6	7.1 deg	28 dB	48 dB	1.5.1 (14.0)	27 lbs (12 3 kg)
HP3-47	3 (0.9)	4.4-5.0	29 2	29.8	30 3	4.7 deg	30 dB	52 dB	1.5.1 (14.0)	50 lbs. (22.7 kg)
HP4-4.7	4 (1.2)	44-50	31.8	32.4	32 9	3 6 deg	30 dB	54 dB	1.5 1 (14.0)	85 lbs (38 3 kg)
HP6-4.7	6 (1.8)	44-50	34.8	354	35.3	2.6 deg	30 dB	57 dB	1.5.1 (14.0)	251 lbs. (113.0 kg)
HP8-4.7	8 (24)	4.4-5 D	48.2	38 8	39 3	1.8 deg	30 dB	81 dB	1.5.1 (14.0)	424 lbs (194 5 kg
HPD2-4.7	2 (0 6)	4.4-50	25.8	26.4	26.9	7.1 deg	28 dB	48 dB	151 (14.0)	27 lbs. (12.3 kg)
HPD3-4.7	3 (0 9)	4.4-5.0	25 8 29 2	29 8	30.3	4.7 deg	30 dB	52 dB	1.5 1 (14.0)	50 lbs (22.7 kg)
HPD4-47	4 (12)	4.4-5.0	31.8	32.4	32 B	3.6 deg.	30 dB	54 dB	1.5.1 (14.0)	85 lbs (38 3 kg)
HPD6-4.7	6 (18)	4.4-5.0	34.8	35 4	35.9	2 6 deg	30 dB	57 dB	151 (140)	251 lbs (113 0 kg
HPD8-4.7	8 (2.4)	4.4-5.0	38.2	38.8	39.3	1 B deg	30 dB	61 dB	1.5.1 (14.0)	424 lbs (194 5 kg

Radio Waves, Inc. • 495 R Billerica Avenue • N. Billerica, MA 01862 USA • Tel: (978) 459-8800 • Fax: (978) 459-3310 / 8810

3 RADIOWAVES HFD2-4.7 ANTENNA



NOTES: 1. THE DESIGN ASSUMES A SOFT/LOOSE SOIL EXHIBITING THE FOLLOWING PROPERTIES: ALLOWABLE BEARING PRESSURE OF 2000 PSF, A SOIL UNIT WEIGHT OF 100 PCF, COEFFICIENT OF BASE SLIDING FRICTION OF 0.20, AND NO GROUNDEATER ENCOUNTERED.

- 2. REINFORCING BAR TO CONFORM TO ASTM A615 GRADE 60 SPECIFICATIONS. A MINIMUM OF 3 INCHES OF CONCRETE SHALL COVER ALL REINFORCEMENT.
- 3. CONCRETE INSTALLATION TO CONFORM TO ACI-318 (2002) BUILDING REQUIREMENTS FOR 3. CONCRETE INSTALLATION TO CONFORM TO ACISTO (2002) OCIDING RECOMMENTATION TO CONFORETE OF REINFORCED CONCRETE TO BE PLACED AGAINST UNDISTURBED EARTH FREE OF WATER AND ALL FOREIGN OBJECTS AND MATERIALS. A MINIMUM OF 3 INCHES OF CONCRETE SHALL COVER ALL REINFORCEMENT. MINIMUM 28-DAY COMPRESSION STRENGTH OF CONCRETE SHALL BE 3000 PSI.
- 4. FOUNDATION MUST BEAR AT OR BELOW LOCAL FROST DEPTH FOR UNHEATED STRUCTURES.

6 TEMPORARY TOWER FOUNDATION C-5 SCALE : 1/2" = 1'-0"

DESIGN LOAD CRITERIA

EQUIPMENT SHELTER SHALL BE DESIGNED AND MANUFACTURED TO MEET ALL STATE AND LOCAL CODES. ITS LAYOUT SHALL BE COORDINATED WITH CARRIERS

DESIGN BASIS GOVERNING CODE DESIGN LIVE LOADS IMPORTANCE CATEGORY CONNECTICUT STATE BUILDING CODE 40 PSF (ASCE 7-02)

SNOW LOAD: GROUND SNOW LOAD (Pg)
IMPORTANCE FACTOR
EXPOSURE FACTOR (Ce) 30 PSF 1.0 0.9

THERMAL FACTOR (Ct) WIND LOAD

BASIC WIND LOAD EXPOSURE GROUP IMPORTANCE FACTOR 100 MPH (3 SEC. GUST) 1.0

SHELTER LOAD: FLOOR LIVE LOAD INCLUDING EQUIPMENT EQUIPMENT SHELTER DL 250 PSF 24,500 LBS

SEISMIC DESIGN PARAMETERS:
SEISMIC USE GROUP
MCE SPECTRAL ACCELERATION SHORT (Sa) 0.288

MCE SPECTRAL ACCELERATION SHORT (SI) SITE CLASS

IMPORTANCE FACTOR

0.066 D FOR UNKNOWN

DEVELOPMENT & MANAGEMENT DOCUMENTS **TOWN ANTENNA** REDDING RIDGE CT505 REDDING RIDGE **PLAN & DETAILS** 186 BLACK ROCK TURNPIKE CT-242-310 REDDING, CT 06896 MESSAGE CENTER MANAGEMENT DESIGN TYPE: 40 WOODLAND STREET

RAW LAND

OFFICE: (888) 973-7483 мсм

HARTFORD, CT 06105

ALL-POINTS TECHNOLOGY CORPORATION

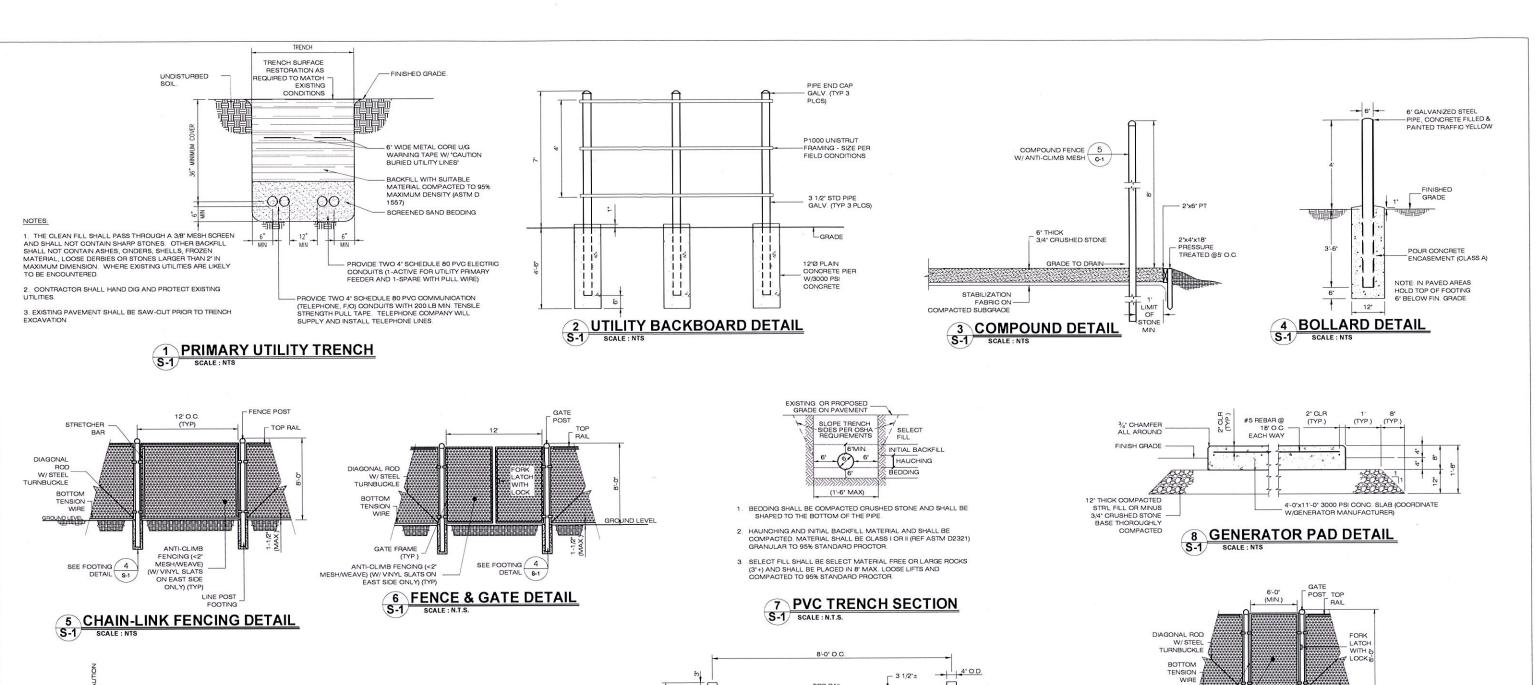
3 SADDLEBROOK DRIVE PHONE: (860)-663-1697 REV.4: KILLINGWORTH, CT 06419 WWW.ALLPOINTSTECH.COM FAX: (860)-663-0935

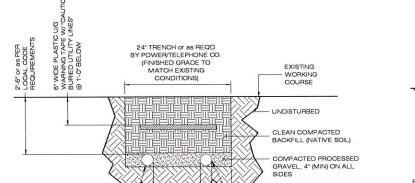
REV.5:

REV.0: 08/11/15: FOR REVIEW: SMC REV.1: 08/12/15: FIRE DEPT. REVISIONS: SMC REV.2: 12/02/15: TOWER REVISIONS: SMC REV.3: 12/10/15: TEMP TOWER REVS: SMC

APT FILING NUMBER: CT-242-310] APT DRAWING NUMBER: CT-505 C-5 DRAWN BY: RCB SCALE: AS NOTED

CHECKED BY: SMC DATE: 08/03/15 SHEET NUMBER





9 SECONDARY TRENCH DETAIL
SCALE: N.T.S.

(VEIRIFY

W/LOCAL

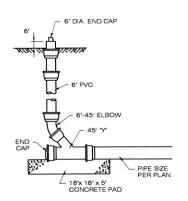
- ELECTRIC CONDUIT

(WHERE INDICATED)

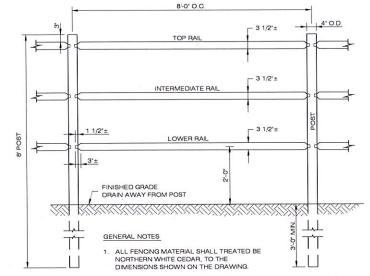
6° MIN (TYP)

4ºØ SCH 80 PVC COMMUNICATION

4"9 SCH. 90 PVC COMMUNICATION (TELEPHONE, F/O) CONDUIT WITH 200 LB MIN. TENSILE STRENGTH PULL TAPE (WHERE INDICATED). TELEPHONE COMPANY WILL SUPPLY AND INSTALL TELEPHONE LINES.

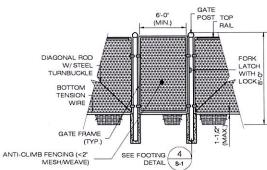


10 DRAINAGE CLEAN-OUT

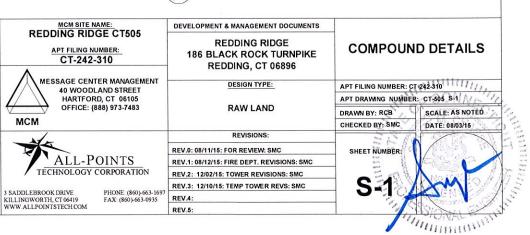


ALL POSTS SHALL BE INSTALLED PARALLEL AND PLUMB. ALL RAILS SHALL BE INSTALLED PARALLEL AND TRUE.

11 SPLIT RAIL FENCE S-1 SCALE : N.T.S.



12 MAN GATE DETAIL



ENVIRONMENTAL NOTES:

WETLAND AND PUBLIC WATER SUPPLY WATERSHED PROTECTION PROGRAM

Portions of the proposed MCM Redding Ridge Facility's compound are located in close proximity (±53 feet) to a wetland area. In addition, the MCM Redding Ridge Facility is located within the public water supply watershed of the Hemicok Reservoir and active source of public drinking water maintained by the Aquarion Water Company (PWSID #CT0501). As a result, the following protective measures shall be followed to help avoid degradation of the nearby wetland system or water quality that could affect his public water supply watershed. These protective measures satisfy recommendations from the Sinking Water Section (DWS) of the Department of Public Health as specified in a June 27, 2014 letter and Condition No. 3 of the Connectiout Siting Councits Decision and Order (Docket No. 449) dated October 30, 2014.

It is of the utmost importance that the Contractor complies with the requirement for the installation of protective measures and the education of its employees and subcontractors performing work on the project site. These measures will also provide protection to a nearby wetland system. This protection program shall be implemented regardless of time of get the construction activities occur. All-Points Technology Corporation, P.C. (PAPT) will serve as the Environmental Monitor for this project to ensure that wetland protection measures are implemented properly. The Contractor shall contact Dean Gustafson, Senior Environmental Scientist at APT and Aquarion Water Company personnel, at least 5 business days prior to the pre-construction meeting. Mr. Gustafson can be reached by phone at (860) 663-1697 ext. 201 or via email at dgustafson@allpointstech.com

The wetland and public water supply watershed protection program consists of several components: use of appropriate erosion control measures to control and contain erosion while avoiding/minimizing wildlife entanglement, periodic inspection and maintenance of isolation structures and erosion control measures; education of all contractors and sub-contractors prior to initiation of work on the site; protective measures; and, reporting.

- Erosion and Sedimentation Controls

 a. Plastic netting used in a variety of erosion control products (i.e., erosion control blankets, fiber rolls [watties], reinforced silt fence) has been found to entangle wildlife, including reptiles, amphibians, birds and small mammals. No permanent erosion control products or reinforced silt fence will be used on the MCM project. Temporary Erosion control products will use either erosion control blankets and liber rolls composed of processed fibers mechanically bound together to form a continuous matrix, (real tess) or netting composed of planar woven natural biodegradable fiber to avoid/minimize wildlife entanglement.

 Installation of erosion control measures (i.e., conventional silt fenoing, straw bales, straw wattles, compost filter socks, etc.) shall be performed by the Contractor prior to any earthwork. APT will inspect the work zone following erosion control barrier installation to ensure erosion controls are properly installed prior to the start of earthwork.

 c. All erosion controls materials and installation/maintenance methods shall follow the 2002 Connecticut Gudelines for Soil Erosion and Sediment Control (DEP Bulletin 34), as amended. The Contractor is responsible for daily
- Soil Frosion and Sediment Control (DEP Bulletin 34), as amended. The Contractor is responsible for daily
- Soil Erosion and Sediment Control (DEP Bulletin 34), as amended. The Contractor is responsible for daily inspections of erosion control measures for tears or breeches in the fabric/material and accumulation levels of sediment, particularly following storm events of 0.10 inch or greater. APT will provide periodic inspections of the erosion control measures throughout the duration of construction activities, generally on a biweekly frequency or more frequently if site conditions warrant. The extent of the erosion control barriers will be as shown on the site plans. The Contractor shall have additional erosion control materials stockpiled on site should field conditions warrant extending/reinforcing erosion control barriers as directed by APT or other responsible agencies. All sit fencing and other erosion control devices shall be removed within 30 days of completion of work and permanent stabilization of site soils so that repite and amphibian movement between uplands and wetlands is not restricted. If fiber rolls/wattles, straw bales, or other natural material erosion control products are used, such devices will not be left in place to biodegrade and shall be prompily removed after soils are states so as not to create a barrier to migrating wildlife. Seed from seeding of soils should not spread over fiber rolls/wattles as it makes them harder to remove once soils are stabilized by vegetation.

- tractor Education
 Prior to work on site, the Contractor shall attend an educational session at the pre-construction meeting with APT.
 This orientation and educational session will consist of an introductory meeting with APT to understand the
 environmentally sensitive nature of the development site and the need to follow Protective Measures as described in
 Section 3 below.

 The Contractor will be provided with cell phone and email contacts for Aquarion Water Company personnel to
 immediately report any releases of sediment or fuel or hazardous material releases.

- 3. Petroleum Materials Storage and Spill Prevention
 a. Certain precautions are necessary to store petroleum materials, refuel and contain and property clean up any inadvertent fuel or petroleum (i.e. oil, hydraulic fluid, etc.) spill due to the projects location in proximity to sensitive wetlands and within the Hermlock Reservoir public weter supply watershed.
 b. A spill containment kit consisting of a sufficient supply of absorbent pads and absorbent material will be maintained by the Contractor at the construction site throughout the duration of the project. In addition, a waste drum will be kept on site to contain any used absorbent pads/material for proper and timely disposal off site in accordance with able local, state and federal laws.
 - The following petroleum and hazardous materials storage and refueling restrictions and spill response procedures will be adhered to by the Contractor.

- Petroleum and Hazardous Materials Storage and Refueling

 1. Refueling of vehicles or machinery shall occur a minimum of 100 feet from wetlands or wateroourses and shall take place on an impervious pad with secondary containment designed to contain fuels.

 2. Any fuel or hazardous materials that must be kept on site shall be stored on an impervious surface utilizing secondary containment a minimum of 100 feet from wetlands or wateroourses.

Initial Spill Response Procedures

- Stop operations and shut off equipment. Remove any sources of spark or flame. Contain the source of the spill.

- Determine the approximate volume of the spill lidentify the location of natural flow paths to prevent the release of the spill to sensitive nearby waterways
- or wetlands.
 6. Ensure that fellow workers are notified of the spill
- Spill Clean Up & Containment I Clean Up & Containment
 Obtain spill response materials from the on-site spill response kit. Place absorbent materials directly on
 the release area.
 Limit the spread of the spill by placing absorbent materials around the perimeter of the spill.
 Isolate and eliminate the spill source.
 Contact Aquarion Water Company personnel and Connecticut Siting Council along with other
 appropriate local, state and/or federal agencies, as necessary.
 Contact a disposal company to properly dispose of contaminated materials.

Complete an incident report.

Submit a completed incident report to Aquarion Water Company and the Connecticut Siting Council

ide and Pesticide Restrictions

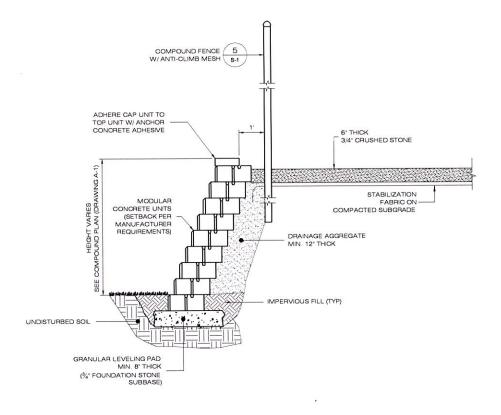
The use of herbicides and pesticides at the proposed wireless telecommunications facility is strictly prohibited.

orting

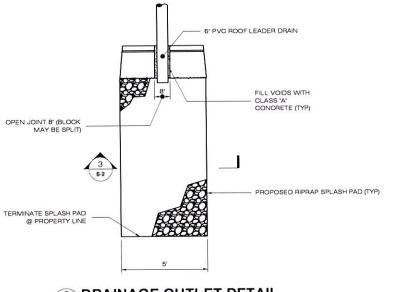
Monthly inspection reports (brief narrative and applicable photos) will be submitted to the Connecticut Siting Council

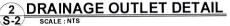
for compliance verification.

Any significant releases of sediment (e.g., impacting the nearby wellands) will be reported to the Connecticut Siting Council and Aquarion Water Company within 24 hours.



1 TYPICAL RETAINING WALL SECTION





GENERAL NOTES:

- STRIP ALL VEGETATION AND ORGANIC SOIL FROM THE WALL ALIGNMENT
- BENCH CUT ALL EXCAVATED SLOPES.
 DO NOT OVER EXCAVATE UNLESS DIRECTED BY SITE SOIL ENGINEER TO REMOVE UNSUITABLE
- 4. SITE SOIL ENGINEER SHALL VERIFY FOUNDATION SOILS AS BEING COMPETENT PER THE DESIGN
- SITE SUIL ENGINEER SMALL VEHIFY FOUNDATION SOILS AS BEING COMPETENT PER THE DESIGNATION AND PRANMETERS.
 LEVELING PAD SHALL CONSIST OF 3/4" FOUNDATION STONE, MINIMUM 8" THICK, OR 3,000 PSI
- 6. CONTRACTOR MAY OPT FOR A CONCRETE FOOTING. CONCRETE FOOTING SHALL BE
- UNREINFORCED, DEPTH OF CONCRETE TO BE A MINIMUM THICKNESS OF 6°.

 7. MINIMUM EMBEDMENT OF WALL BELOW FINISH GRADE SHALL BE 16° FOR WALL HEIGHTS FROM 4' AND UP TO 10, 8° FOR HEIGHTS BELOW 4' UNLESS SHOWN DIFFERENTLY.

 8. FOLLOW APPLICABLE PROVISIONS OF THE MANUFACTURERS INSTALLATION INSTRUCTIONS AND
- WRITTEN SPECIFICATIONS. 9. COMPACTION TESTS SHALL BE TAKEN AS THE WALL IS INSTALLED. THE MINIMUM NUMBER OF
- 9 COMPACTION 1531S PHALL BE PARENT AS THE WALL STONG ACLES TO MANUAL TESTS SHALL BE DETERMINED BY THE SITE SOILS ENGINEER, OR AS INDICATED IN THE SPECIFICATION.

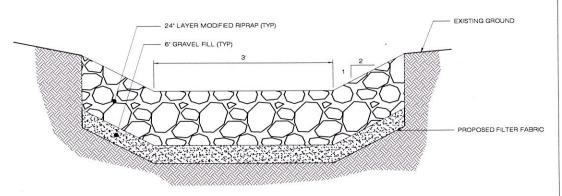
 10. COMPACTION SHALL BE 95% OF MAXIMUM DRY DENSITY PER ASTM D-1557.

 11. ESTABLISH TURF AS SOON AS THE WALL IS COMPLETED.
- 12. FINAL WALL ALIGNMENT SHALL BE LOCATED IN THE FIELD
- 13. REINFORCED BACK FILL REQUIREMENTS FOR THE SEGMENTAL CONCRETE RETAINING WALL SHALL CONFORM TO THE FOLLOWING SPECIFICATIONS:

SIEVE SIZE	PERCENT PASSIN
	REINFORCED BACK FIL
2 INCH	100
NO. 4	40-85
NO. 10	25-75
NO. 40	15-50
NO. 100	10-40
NO. 200	4-12

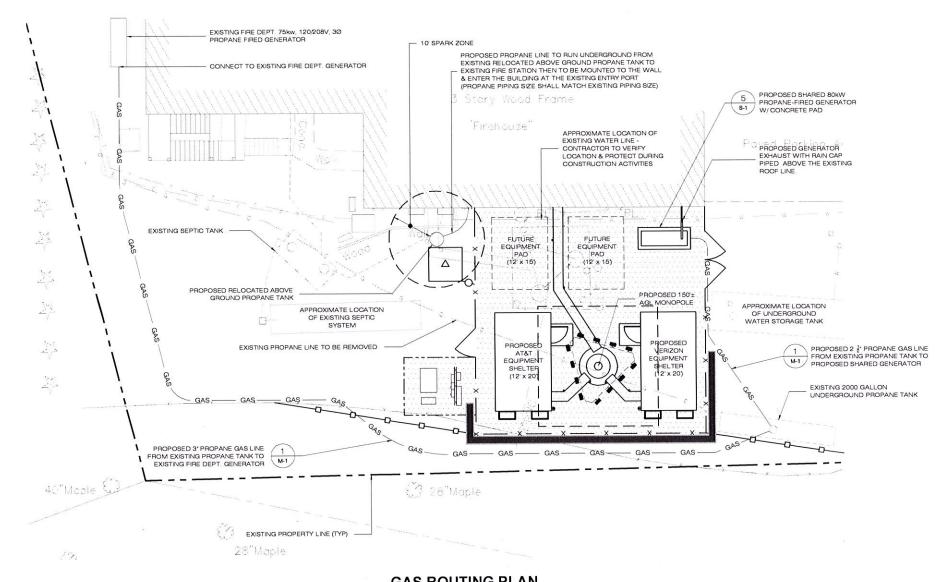
PLASTICITY INDEX (PI) LESS THAN OR EQUAL TO 10 AND A LIQUID LIMIT LESS THAN OR EQUAL TO 40. REINFORCED BACK FILL SHALL BE PLACED AND COMPACTED IN LIFTS NOT EXCEEDING 10 INCHES. REINFORCED BACK FILL SHALL BE COMPACTED TO 95 PERCENT OF THE MAXIMUM DENSITY AS DETERMINED BY ASTM-1557 THE MOISTURE CONTENT OF THE BACK FILL MATERIAL PRIOR TO AND DURING COMPACTION SHALL BE WITHIN 2 PERCENTAGE POINTS OF DRY OPTIMUM.

IF CONDITIONS ARE DIFFERENT THAN THOSE STATED IN THESE DRAWINGS AND SPECIFICATIONS, THE CONTRACTOR MUST CONTACT THE ENGINEER PRIOR TO PROCEEDING WITH THE CONSTRUCTION OF THE WALL

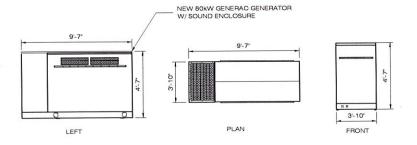


3 RIPRAP SPLASHPAD SECTION

MCM SITE NAME:	DEVELOPMENT & MANAGEMENT DOCUMENTS	COMPOUN	D DETAILS
REDDING RIDGE CT50 APT FILING NUMBER: CT-242-310	REDDING RIDGE 186 BLACK ROCK TURNPIKE REDDING, CT 06896	& ENVIRO	NMENTAL TES
MESSAGE CENTER MANAGE 40 WOODLAND STREE	DESIGN TIPE:	APT FILING NUMBER: C	T-242-310
HARTFORD, CT 06105		APT DRAWING NUMBE	R: CT-505 S-2
OFFICE: (888) 973-7483	RAW LAND	RAW LAND DRAWN BY: RCB SCALE	SCALE: AS NOTED
MCM		CHECKED BY: SMC	DATE: 08/03/15
.	REVISIONS:	1.4.5	3/02/03
	REV.0: 08/11/15: FOR REVIEW: SMC	SHEET NUMBER:	The state of
ALL-POINTS	REV.1: 08/12/15: FIRE DEPT. REVISIONS: SMC	Free E	
TECHNOLOGY CORPORAT	ION REV.2: 12/02/15: TOWER REVISIONS: SMC		-44
3 SADDLEBROOK DRIVE PHONE: (860) KILLINGWORTH, CT 06419 FAX: (860)-66	REV.3: 12/10/15: TEMP TOWER REVS: SMC	S = 2 2 1	X VI D
			JANO NO
WWW.ALLPOINTSTECH.COM	REV.5:	2.5	0 1002-

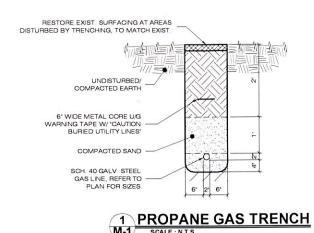


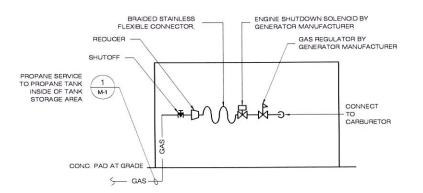
GAS ROUTING PLAN



FOR GENERATOR PAD, SEE 8/S-1

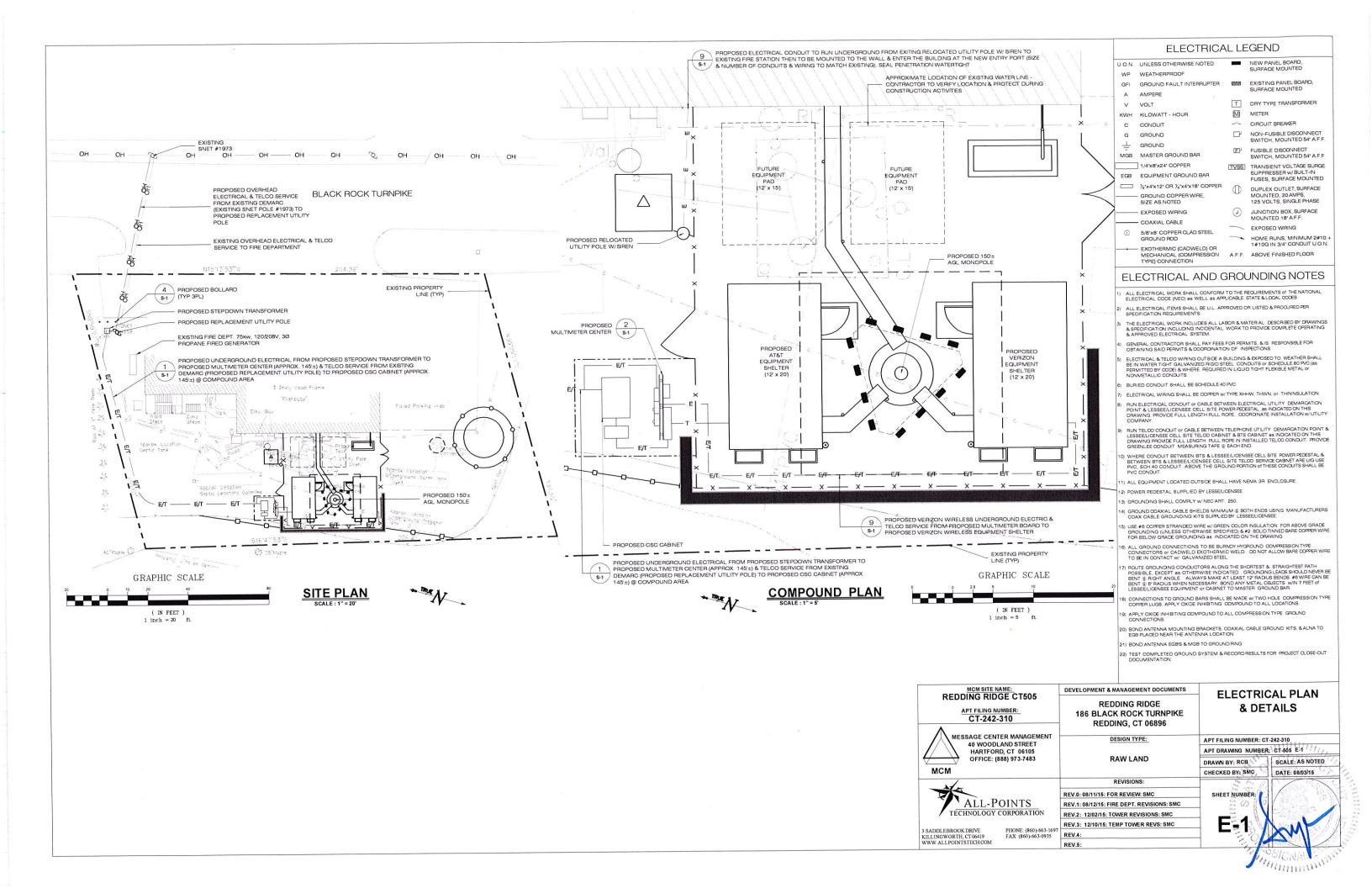
5 80KW PROPANE GENERATOR
M-1 SCALE: NTS

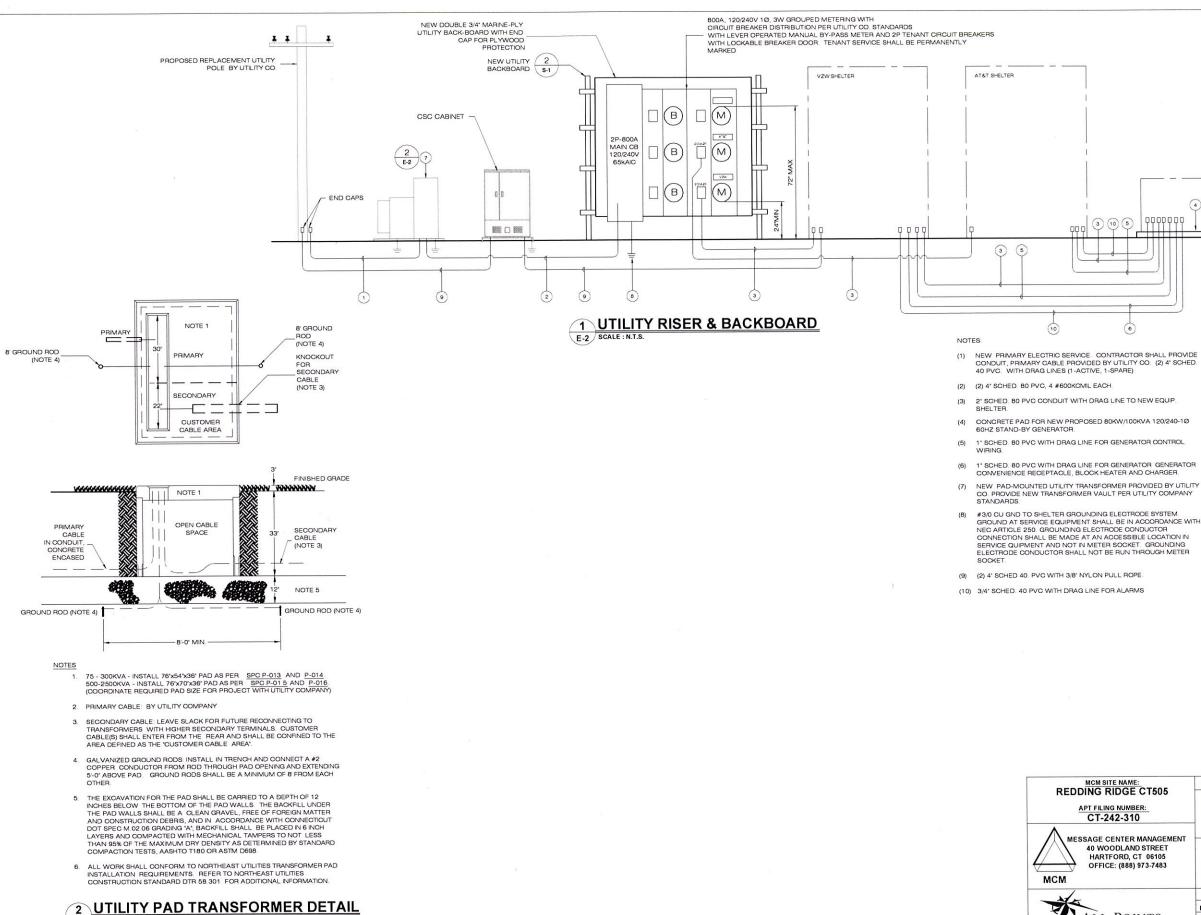




2 GENERATOR CONNECTION DETAIL
M-1 SCALE: NTS

MCM SITE NAME:	DEVELOPMENT & MANAGEMENT DOCUMENTS	MECHANICAL PLAN	
REDDING RIDGE CT505 APT FILING NUMBER: CT-242-310	REDDING RIDGE 186 BLACK ROCK TURNPIKE REDDING, CT 06896	& DETAILS	
MESSAGE CENTER MANAGEMENT 40 WOODLAND STREET	DESIGN TYPE:	APT FILING NUMBER: CT-242-310	
HARTFORD, CT 06105	RAW LAND DRAWN BY: RCB St	APT DRAWING NUMBER: CT-505 M-1	
OFFICE: (888) 973-7483		DRAWN BY: RCB SCALE: AS NOTED	
MCM		CHECKED BY: SMC DATE: 08/03/15	
M -	REVISIONS:		
	REV.0: 08/11/15: FOR REVIEW: SMC	SHEET NUMBER:	
ALL-POINTS	REV.1: 08/12/15: FIRE DEPT. REVISIONS: SMC		
TECHNOLOGY CORPORATION	REV.2: 12/02/15: TOWER REVISIONS: SMC		
3 SADDLEBROOK DRIVE PHONE: (860)-663-1697 KILLINGWORTH, CT 06419 FAX: (860)-663-0935	REV.3: 12/10/15: TEMP TOWER REVS: SMC	→ M-15/N →	
	REV.4:	9	
WW.ALLPOINTSTECH.COM	REV.5:	0000	

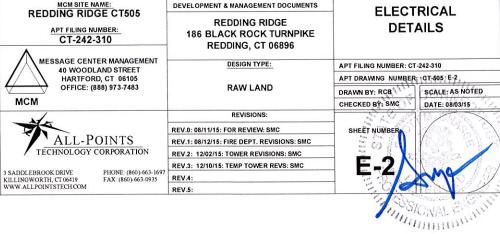




E-2 SCALE : N.T.S.

ELECTRICAL LEGEND U.O.N. UNLESS OTHERWISE NOTED WP WEATHERPROOF EXISTING PANEL BOARD, GFI GROUND FAULT INTERRUPTER SURFACE MOUNTED AMPERE DRY TYPE TRANSFORMER VOLT M METER KWH KILOWATT - HOUR CONDUIT ~ CIRCUIT BREAKER NON-FUSIBLE DISCONNECT SWITCH, MOUNTED 54' A.F.F. \Box GROUND GROUND FUSIBLE DISCONNECT MGB MASTER GROUND BAR SWITCH, MOUNTED 54" A.F.F TVSS TRANSIENT VOLTAGE SURGE SUPPRESSER W/BUILT-IN FUSES, SURFACE MOUNTED 1/4'x8'x24' COPPER EGB EQUIPMENT GROUND BAR ☐ 1/4"x4"x12" OR 1/4"x4"x18" COPPER DUPLEX OUTLET, SURFACE 125 VOLTS, SINGLE PHASE JUNCTION BOX, SURFACE MOUNTED 18' A.F.F. EXPOSED WIRING COAXIAL CABLE EXPOSED WIRING 5/8'x8' COPPER CLAD STEEL HOME RUNS, MINIMUM 2#10 + 1#10G IN 3/4" CONDUIT U.O.N. GROUND ROD EXOTHERMIC (CADWELD) OR MECHANICAL (COMPRESSION A.F.F. ABOVE FINISHED FLOOR TYPE) CONNECTION ELECTRICAL AND GROUNDING NOTES ALL ELECTRICAL WORK SHALL CONFORM TO THE REQUIREMENTS OF THE NATIONAL ELECTRICAL CODE (NEC) as WELL as APPLICABLE STATE & LOCAL CODES ALL ELECTRICAL ITEMS SHALL BE U.L. APPROVED OR LISTED & PROCURED PER SPECIFICATION REQUIREMENTS. THE ELECTRICAL WORK INCLUDES ALL LABOR & MATERIAL DESCRIBED BY DRAWINGS & SPECIFICATION INCLUDING INCIDENTAL WORK TO PROVIDE COMPLETE OPERATING & APPROVED ELECTRICAL SYSTEM. GENERAL CONTRACTOR SHALL PAY FEES FOR PERMITS, & IS RESPONSIBLE FOR OBTAINING SAID PERMITS & COORDINATION OF INSPECTIONS.

- ELECTRICAL & TELCO WIRING OUTSIDE A BULDING & EXPOSED TO WEATHER SHALL BE IN WATER TIGHT GALVANIZED RIGID STEEL CONDUITS OF SCHEDULE 80 PVC (as PERMITTED BY COOD) & WHERE REQUIRED IN LIQUID TIGHT FLEXIBLE METAL OF NORMETAL COORD ITS. NONMETALLIC CONDUITS. BURIED CONDUIT SHALL BE SCHEDULE 40 PVC.
- ELECTRICAL WIRING SHALL BE COPPER W/TYPE XHHW, THWN, or THININSULATION.
- RUN ELECTRICAL CONDUIT Or CABLE BETWEEN ELECTRICAL UTILITY DEMARCATION POINT & LESSEELICENSEE CELL SITE POWER PECESTAL as INDICATED ON THIS DRAWING. PROVIDE FULL LENGTH PULL ROPE. COORDINATE INSTALLATION W/UTILITY COMPANY.
- RUN TELCO CONDUIT OF CABLE BETWEEN TELEPHONE UTILITY DEMARCATION POINT & LESSEAUCENSEE CELL SITE TELCO CABINET & BTS CABINET as INDICATED ON THIS DRAWING PROVIDE FULL LENGTH PULL ROPE IN INSTALLED TELCO CONDUIT. PROVIDE GREENLEE CONDUIT MEASURING TAPE @ EACH END.
- WHERE CONDUIT RETWEEN BTS & LESSEE/LICENSEE CELL SITE POWER PEDESTAL & WHENE CURDON BE WEEN BY A LESSECHICLOSSE WILL SHE POWER FACE UNDER SHOULD SERVICE ORBINET ARE UNDER SHOULD SERVICE ORBINET ARE UNDER SHOULD SHOULD FOR SHALL BE PVC, SCH 40 CONDIT. ABOVE THE GROUND PORTION OF THESE CONDUITS SHALL BE PVC CONDUIT.
- 1) ALL EQUIPMENT LOCATED OUTSIDE SHALL HAVE NEWA 3R ENCLOSURE
- 12) POWER PEDESTAL SUPPLIED BY LESSE/LICENSEE.
- 13) GROUNDING SHALL COMPLY W/ NEC ART. 250
- 14) GROUND COAXIAL CABLE SHIELDS MINIMUM @ BOTH ENDS USING MANUFACTURERS COAX CABLE GROUNDING KITS SUPPLIED BY LESSEE/LICENSEE.
- I) USE #6 COPPER STRANDED WIRE W/ GREEN COLOR INSULATION FOR ABOVE GRADE GROUNDING (UNLESS OTHERWISE SPECIFIED) & ₱2 SOLID TINNED BARE COPPER WIRE FOR BELLOW GRADE GROUNDING as INJICATED ON THE DRAWING.
- 16) ALL GROUND CONNECTIONS TO BE BURNDY HYGROUND COMPRESSION TYPE CONNECTORS of CADWELD EXOTHERMIC WELD. DO NOT ALLOW BARE COPPER WIRE TO BE IN CONTACT W. GALVANIZED STEEL.
- 7) ROUTE GROUNDING CONDUCTORS ALONG THE SHORTEST & STRAIGHTEST PATH POSSIBLE, EXCEPT as OTHERWISE INDICATED. GROUNDING LEADS SHOULD NEVER BE BENT & RIGHT ANGLE. ALWAYS MAKE AT LEAT 12 RADIUS BENDS. #5 WIRE CAN BE BENT @ #6 RADIUS WHEN NECESSARY. BOND ANY METAL OBJECTS WIN 7 FEET of LESSEE/LICENSEE EQUIPMENT OF CABINET TO MASTER GROUND BAR.
- 8) CONNECTIONS TO GROUND BARS SHALL BE MADE W/TWO HOLE COMPRESSION TYPE COPPER LUGS. APPLY OXIDE INH BITING COMPOUND TO ALL LOCATIONS.
- 19) APPLY OXIDE INHIBITING COMPOUND TO ALL COMPRESSION TYPE GROUND CONNECTIONS.
- 20) BOND ANTENNA MOUNTING BRACKETS, COAXIAL CABLE GROUND KITS, & ALNA TO EGB PLACED NEAR THE ANTENNA LOCATION.
- 21) BOND ANTENNA EGBS & MGB TO GROUND RING
- 22) TEST COMPLETED GROUND SYSTEM & RECORD RESULTS FOR PROJECT CLOSE-OUT DOCUMENTATION.



GENERAL NOTES:

- ALL MATERIALS AND METHODS OF CONSTRUCTION SHALL COMPLY WITH THE STANDARDS AND SPECIFICATIONS OF THE TOWN OF REDDING, AND OTHER
- 2. THE CONTRACTOR SHALL BE RESPONSIBLE FOR SECURING ALL NECESSARY PERMITS BEFORE COMMENCING WORK. THE CONTRACTOR SHALL FOLLOW CONDITIONS OF ALL APPLICABLE PERMITS AND WORK IN ACCORD WITH OSHA REGULATIONS.
- 3. UTILITY INFORMATION SHOWN ON THE PLAN IS BASED ON VISIBLE FIELD EVIDENCE AND AVAILABLE RECORDS. THE CONTRACTOR SHALL FIELD VERIFY THE LOCATION OF ALL UTILITIES PRIOR TO COMMENCING WORK. THE CONTRACTOR IS ADVISED THAT THESE DRAWINGS MAY NOT ACCURATELY DEPICT AS-BUILT LOCATIONS AND OTHER UNKNOWN STRUCTURES. THE CONTRACTOR SHALL THEREFORE DETERMINE THE EXACT LOCATION OF EXISTING UNDERGROUND ELEMENTS AND EXCAVATE WITH CARE AFTER CALLING MARKOUT SERVICE AT 1-800-922-4455 (72) HOURS BEFORE DIGGING, DRILLING OR BLASTING. CARE SHALL BE TAKEN NOT TO DISTURB EXISTING UTILITIES AND SERVICE CONNECTIONS (OR PORTIONS THERE OF) TO REMAIN. CONTRACTOR IS RESPONSIBLE FOR REPAIRING OR REPLACING STRUCTURES OR UTILITIES DAMAGED BY HIS OPERATIONS.
- 4. THE CONTRACTOR IS RESPONSIBLE FOR THE INSTALLATION OF NEW SERVICE CONNECTIONS AND SHALL COORDINATE WORK WITH THE APPROPRIATE
- 5. ALL EXISTING ACTIVE SEWER, WATER, GAS, ELECTRIC, FIBER OPTIC, AND OTHER UTILITIES WHERE ENCOUNTERED IN THE WORK, SHALL BE PROTECTED AT ALL TIMES, AND WHERE REQUIRED FOR THE PROPER EXECUTION OF THE WORK, SHALL BE RELOCATED AS DIRECTED BY THE ENGINEER.
- 6. EXTREME CAUTION SHOULD BE USED BY THE CONTRACTOR WHEN EXCAVATING OR PIER DRILLING AROUND OR NEAR UTILITIES. CONTRACTOR SHALL PROVIDE SAFETY TRAINING FOR THE WORKING CREW. THIS WILL INCLUDE, BUT NOT BE LIMITED TO.

 A) FALL PROTECTION,
- B) CONFINED SPACE ENTRY
- C) ELECTRICAL SAFETY AND TRENCHING & EXCAVATION
- ELECTRIC SERVICE SHALL BE COORDINATED WITH EVERSOURCE.
- 8. ALL ELEVATIONS SHOWN ARE IN N.G.V. DATUM 1929.
- 9. ALL RUBBISH, STUMPS, DEBRIS, STICKS, STONES, AND OTHER REFUSE SHALL BE REMOVED FROM THE SITE AND DISPOSED OF LEGALLY.
- 10. CONTRACTOR SHALL PROTECT EXISTING PAVED AND GRAVEL SURFACES, CURBS, LANDSCAPE AND STRUCTURES AND RESTORE SITE TO PRECONSTRUCTION CONDITION WITH AS GOOD, OR BETTER, MATERIALS. NEW MATERIALS SHALL MATCH EXISTING THICKNESS AND TYPE.
- THE CONTRACTOR SHALL SHORE ALL TRENCH EXCAVATION GREATER THAN 5 FEET IN DEPTH OR LESS WHERE SOIL CONDITIONS ARE DEEMED UNSTABLE. ALL SHEETING AND/OR SHORING METHODS SHALL BE DESIGNED BY A PROFESSIONAL ENGINEER.
- THE CONTRACTOR IS RESPONSIBLE FOR MANAGING GROUNDWATER LEVELS IN THE VICINITY OF EXCAVATIONS TO PROTECT ADJACENT PROPERTIES AND THE COUNTINATION & RESPONDED FOR MANAGEMENT AND ACCORDANCE WITH LOCAL SEDIMENTATION & EROSION CONTROL GUIDELINES NEW WORK, GROUNDWATER SHALL BE DRAINED IN ACCORDANCE WITH LOCAL SEDIMENTATION & EROSION CONTROL GUIDELINES
- 13. THE CONTRACTOR IS REQUIRED TO REVIEW THE STATEMENT OF SPECIAL INSPECTION PRIOR TO THE START OF WORK. THE CONTRACTOR TO PROVIDE E-MAIL REQUEST TO THE PROJECT ENGINEER FOR INSPECTION 72 HOURS IN ADVANCE OF INSPECTION.

14. EXLAVATION
CONTRACTOR SHALL GRADE ONLY AREAS SHOWN TO BE MODIFIED HEREIN AND ONLY TO THE EXTENT REQUIRED TO SHED OVERLAND WATER FLOW AWAY FROM SITE. ALL SLOPES SHALL NOT BE STEEPER THAN 3.1 (HORIZ VERT).

BEDROCK SUBGRADE SHOULD NOT BE STEEPER THAN 4H.1V. HIGH SPOTS IN BEDROCK SUBGRADES MAY NEED TO BE REMOVED AND LOW SPOTS MAY BE FILLED WITH LEAN CONCRETE OR MINUS 1/2 CRUSHED STONE TO PROVIDE A LEVEL SURFACE. BEDROCK SUBGRADES DO NOT REQUIRE PROOFROLLING.

SEDIMENTATION AND EROSION CONTROLS SHOWN AND SPECIFIED SHALL BE ESTABLISHED BEFORE STRIPPING EXISTING VEGETATION.

ORGANIC MATERIAL AND DEBRIS SHALL BE STRIPPED AND STOCKPILED BEFORE ADDING FILL MATERIAL

NO FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN GROUND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED IN ANY FILL OR

ALL FILL SHALL BE PLACED IN EIGHT INCH LIFTS AND COMPACTED IN PLACE. STRUCTURAL FILL SHALL BE COMPACTED TO 95% MAXIMUM MODIFIED PROCTOR DRY DENSITY TESTED IN ACCORDANCE WITH ASTM D1557, METHOD C.

EXCAVATIONS FOR FOOTINGS SHALL BE CUT LEVEL TO THE REQUIRED DEPTH AND TO UNDISTURBED SOIL. REPORT UNSUITABLE SOIL CONDITIONS TO THE

STRUCTURAL FILL SHALL BE TESTED FOR MOISTURE CONTENT AND COMPACTION DURING PLACEMENT. SHOULD THE RESULTS OF THE IN-PLACE DENSITY TESTS INDICATE THE SPECIFIED MOISTURE OR COMPACTION LIMITS HAVE NOT BEEN MET, THE AREA REPRESENTED BY THE TEST SHOULD BE REWORKED AND RETESTED, AS REQUIRED, UNTIL THE SPECIFIED MOISTURE AND COMPACTION REQUIREMENTS ARE ACHIEVED.

MINUS \$\frac{1}{4}\]INCH CRUSHED STONE PLACED ON THE EXISTING FILL, THE SURFACE OF WHICH SHOULD BE THOROUGHLY COMPACTED AND CLEAR OF ORGANIC MATTER. EQUIPMENT CABINETS MAY BE SUPPORTED ON SLABS-ON-GRADE UNDERLAIN BY AT LEAST A 12-INCH THICKNESS OF COMPACTED STRUCTURAL FILL OR

THE AREA UNDERLYING THE SLABS SHOULD BE ROUGH GRADED AND THEN THOROUGHLY PROOFROLLED WITH A VIBRATORY ROLLER OR HEAVY PLATE COMPACTOR PRIOR TO FINAL GRADING AND PLACEMENT OF STRUCTURAL FILL OR MINUS 2"-INCH CRUSHED STONE.

A SOIL UNIT WEIGHT OF 100 LBS PER CUBIC FOOT (PCF) SHOULD BE USED FOR ENGINEERED FILL OVERLYING THE FOOTINGS.

TRENCH EXCAVATIONS SHALL BE BACKFILLED AT THE END OF EACH DAY

SURPLUS MATERIAL SHALL BE REMOVED FROM THE SITE.

TOWER FOUNDATION EXCAVATION, BACKFILL AND COMPACTION SHALL BE IN ACCORD WITH TOWER MANUFACTURERS DESIGNS AND SPECIFICATIONS

CONTRACTOR TO VERIFY THAT FOOTING ELEVATIONS AND PIER ELEVATION PROVIDED HEREIN ARE CONSISTENT WITH THE TOWER DESIGN REQUIREMENTS.

14. MATERIALS
NATIVE GRAVEL MATERIAL MAY BE USED FOR TRENCH BACKFILL WHERE SELECT MATERIAL IS NOT SPECIFIED. GRAVEL
MATERIAL FOR CONDUIT TRENCH BACKFILL SHALL NOT CONTAIN ROCK GREATER THAN 2 INCHES IN DIAMETER.

BANK OR CRUSHED GRAVEL SHALL CONSIST OF TOUGH, DURABLE PARTICLES OF CRUSHED OR UNCRUSHED GRAVEL FREE OF SOFT, THIN, ELONGATED OR LAMINATED PIECES AND MEET THE GRADATION.

FILL SHOULD MEET THE FOLLOWING MATERIAL PROPERTY REQUIREMENTS:

FILL TYPE (1)	USCS CLASSIFICATION	ACCEPTABLE LOCATION FOR PLACEMENT
STRUCTURAL FILL	GW (2)	ALL LOCATIONS AND ELEVATIONS. THE EXISTING FILL MAY BE SELECTIVELY RE-USED AS STRUCTURAL FILL PROVIDED IT IS FREE OF ORGANIC AND CLOSELY MEETS THE GRADATION REQUIREMENTS IN NOTE 2, BELOW.
COMMON FILL	VARIES (3)	COMMON FILL MAY BE USED FOR GENERAL SITE GRADING TO WITHIN 12 INCHES OF FINISHED GRADE. COMMON FILL SHOULD NOT BE USED UNDER SETTLEMENT SENSITIVE STRUCTURES. THE EXISTING FILL MAY BE RE-USED AS COMMON FILL, PROVIDED IT IS FREE OF ORGANICS AND CAN BE ADEQUATELY COMPACTED.

1. COMPACTED FILL SHOULD CONSIST OF APPROVED MATERIALS THAT ARE FREE OF ORGANIC MATERIAL SHOULD NOT BE USED. FILL SHOULD NOT BE PLACED ON A FROZEN SUBGRADE

2. IMPORTED STRUCTURAL FILL SHOULD MEET THE FOLLOWING GRADATION: PERCENT PASSING BY WEIGHT

SIEVE SIZE	STRUCTURAL FILL
6'	100
3'	70-100
2"	(100)*
3"	45-95
NO. 4	30-90
NO. 10	25-80
NO. 40	10-50
NO. 200	0-12

* MAXIMUM 2-INCH PARTICLE SIZE WITHIN 12 INCHES OF THE UNDERSIDE OF CONCRETE ELEMENTS

3. COMMON FILL SHOULD HAVE A MAXIMUM PARTICLE SIZE OF 6 INCHES AND NO MORE THAN 25 PERCENT BY WEIGHT PASSING THE US NO 200 SIEVE

SEDIMENTATION/EROSION

THE CONTRACTOR SHALL MINIMIZE DISTURBANCE TO THE EXISTING SITE DURING CONSTRUCTION. EROSION CONTROL MEASURES SHALL BE IN CONFORMANCE WITH THE 2002 CONNECTICUT GUIDLINES FOR SOIL EROSION AND SEDIMENT CONTROL.

CONTRACTOR SHALL PERFORM CONSTRUCTION SEQUENCING SUCH THAT EARTH MATERIALS ARE EXPOSED FOR A MINIMUM OF TIME BEFORE THEY ARE COVERD, SEEDED, OR OTHERWISE STABLIZED TO PREVENT EROSION THE FOLLOWING GENAL CONDITIONS SHALL BE OBSERVED.

A. LIMITS OF CLEARING AND GRUBBING SHALL BE CLEARLY MARKED BEFORE

B. EXISTING VEGETATION TO REMAIN SHALL BE PROTECTED AND REMAIN

C. CLEARING AND GRADING SHALL BE SCHEDULED SO AS TO MINIMIZE THE SIZE OF EXPOSED AREAS AND THE LENGTH OF TIME THAT AREAS ARE EXPOSED.

D. TOPSOIL SHALL BE SPREAD TO FINISH GRADES AND SEEDED AS SOON AS FINISHED GRADES ARE ESTABLISHED. STRAW MULCH, JUTE NETTING OR MATS SHALL BE USED WHERE THE NEW SEED IS PLACED.

THE LENGTH AND STEEPNESS OF CLEARED SLOPES SHALL BE MINIMIZED TO REDUCE RUNOFF VELOCITIES

- F. RUNOFF SHALL BE DIVERTED AWAY FROM CLEARED SLOPES.
- G ALL SEDIMENT SHALL BE TRAPPED ON THE SITE.
- SEDIMENTATION AND EROSION CONTROL (SEC) MEASURES SHOWN SHALL BE INSTALLED PRIOR TO LAND CLEARING, EXCAVATION OR GRADING OPERATIONS.
 REQUIREMENTS SPECIFIED SHALL BE MET PRIOR TO COMMENCING EARTHWORK CONTRACTOR.
- IT IS THE CONTRACTOR'S RESPONSIBILITY TO MAINTAIN SEC MEASURES HROUGHOUT DURATION OF PROJECT UNTIL DISTURBED LAND IS THOROUGHLY
- 5. FAILURE OF THE SEC SYSTEMS SHALL BE CORRECTED IMMEDIATELY AND SUPPLEMENTED WITH ADDITIONAL MEASURES AS NEEDED
- VEGETATIVE SEEDING: UON, AREA TO BE SEEDED SHALL BE LOOSE AND FRIABLE 6. VEGETATIVE SEEDING UON, AREA TO BE SEEDED SHALL BE LOOSE AND FIRMS. TO A DEPTH OF 3'. TOPSOIL SHALL BE LOOSENED BY RAKING OR DISKING BEFORE SEEDING. APPLY 50 Lbs. OF DOLOMITIC LIMESTONE AND 25 Lbs. OF 10-10-10 FERTILIZER IPPR 1000 SF. HARROW LIME AND FERTILIZER INTO LOOSE SOIL. APPLY COMMON BERMUDA AND RYE GRASS AT 50 Lbs/ACRE. USE CYCLONE SEED DRILL CULTIPACKER SEEDER OR HYDROSEDED REGED & FERTILIZER BLURRY) FOR STEEP SLOPES. IRRIGATE UNTIL VEGETATION IS COMPLETELY ESTABLISHED.
- PRIOR TO STARTING ANY OTHER WORK ON THE SITE, THE CONTRACTOR SHALL NOTIFY APPROPRIATE AGENCIES AND SHALL INSTALL EROSINO CONTROL MEASURES AS SHOWN ON THE PLANS AND AS IDENTIFIED IN FEDERAL, STATE, AND LOCAL OVAL DOCUMENTS PERTAINING TO THIS PROJECT
- 8. INSPECT AND MAINTAIN EROSION CONTROL MEASURES, AND REMOVE SEDIMENT THEREFROM ON A WEEKLY BASIS AND WITHIN TWELVE HOURS AFTER EACH STORM EVENT AND DISPOSE OF SEDIMENTS IN AN UPLAND AREA SUCH THAT THEY DO NOT ENCUMBER OTHER DRAINAGE STRUCTURES AND PROTECTED AREAS
- 9. CONTRACTOR SHALL BE FULLY RESPONSIBLE TO CONTROL CONSTRUCTION SUCH THAT SEDIMENTATION SHALL NOT AFFECT REGULATORY PROTECTED AREAS, WHETHER SUCH SEDIMENTATION IS CAUSED BY WATER, WIND, OR DIRECT DEPOS IT
- 10. UPON COMPLETION OF CONSTRUCTION AND ESTABLISHMENT OF PERMANENT GROUND COVER, CONTRACTOR SHALL REMOVE AND DISPOSE OF EROSION CONTROL MEASURES AND CLEAN SEDIMENT AND DEBRIS FROM ENTIRE DRAINAGE SYSTEMS
- 11. APPROPRIATE MEANS SHALL BE USED TO CONTROL DUST DURING CONSTRUCTION.
- 12 A STABILIZED CONSTRUCTION ENTRANCE SHALL BE MAINTAINED TO PREVENT SO AND LOOSE DEBRIS FORM BEING TRACKED ONTO LOCAL ROADS. THE CONSTRUCTION ENTRANCE SHALL BE MAINTAINED UNTIL THE SITE IS PERMANENTLY STABILIZED.
- 13. CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION, EROSION CONTROL MEASURES SHALL BE IN CONFORMACE WITH THE STATE OF CONNECTICUT GUIDELINES FOR EROSION AND SEDIMENT CONTROL, AS
- 14. TEMPORARY SILT FENCE EROSION CONTROL BARRIER SHALL BE MAINTAINED THROUGHOUT SITE CONSTRUCTION. STOCKPILE ON SITE 100 FT. OF SILT FENCE FOR EMERGENCY USE. TEMPORARY EROSION BARRIERS SHALL REMAIN IN PLACE UNTIL PERMANENT VEGETATIVE GROUND COVER IS ESTABLISHED.
- 15. ALL DISTURBED AREAS OUTSIDE THE LIMITS OF THE EQUIPMENT LEASE AREA SHALL BE PERMANENTLY ESTABLISHED WITH A VEGETATIVE GROUND COVER.
- 16. STILLING BASIN SHALL BE UTILIZED FOR ANY DE-WATERING DISCHARGE WHICH MAY OCCUR DURING CONSTRUCTION OPERATIONS
- 17. PROPOSED CONSTRUCTION IMPACTS AND PERMANENT IMPROVEMENTS SHALL NOT 17. PROPOSED ONS INSURANCE WATER RUNOFF PATTERNS, VOLUME OR PEAK FLOW RATES THE FLAT GRADE OF THE EQUIPMENT COMPOUND AND STONE SURFACE WILL PROMOTE STORM WATER INFLITATION.
- 18. CONTRACTOR SHALL INSTALL ALL EROSION AND SEDIMENTATION CONTROL MEASURES PRIOR TO ANY GRADING ACTIVITIES IN LOCATIONS SHOWN ON THESE DRAWINGS.
- 19. SILT FENCES SHALL BE INSPECTED IMMEDIATELY AFTER EACH RAINFALL AND AT LEAST DAILY DURING PROLONGED RAINFALL. ANY REPAIRS THAT ARE REQUIRED SHALL BE MADE IMMEDIATELY.
- 20. IF THE FABRIC ON A SILT FENCE SHOULD DECOMPOSE OR BECOME INEFFECTIVE DURING THE EXPECTED LIFE OF THE FENCE, THE FABRIC SHALL BE REPLACED PROMPTLY.
- 21. SEDIMENT DEPOSITS SHOULD BE INSPECTED AFTER EVERY STORM EVENT. THE DEPOSITS SHOULD BE REMOVED WHEN THEY REACH APPROXIMATELY ONE-HALF THE HEIGHT OF THE
- 22. SEDIMENT DEPOSITS THAT ARE REMOVED OR LEFT IN PLACE AFTER THE FABRIC HAS BEEN REMOVED SHALL BE GRADED TO CONFORM WITH THE EXISTING TOPOGRAPHY AND VEGETATION
- 23. NO GREATER THAN 80,000 SQUARE FEET OF LAND SHALL BE EXPOSED AT ANY ONE TIME DURING DEVELOPMENT. WHEN LAND IS EXPOSED DURING DEVELOPMENT, THE EXPOSURE SHOULD BE KEPT TO THE SHORTEST PRACTICAL PERIOD OF TIME AND SHALL NOT EXCEED 10 DAYS. LAND SHOULD NOT BE LEFT EXPOSED DURING THE WINTER MONTHS.
- 24. ANY DISTURBED AREAS WHICH ARE TO BE LEFT TEMPORARILY, AND WHICH WILL BE REGRADED LATER DURING CONSTRUCTION SHALL BE MACHINE HAY MULCHED AND SEEDED WITH RYE GRASS TO PREVENT EROSION. HAY OR STRAW MULCH SHALL BE APPLIED TO ALL FRESHLY SEEDED AREAS AT A RATE OF 2 TONS PER ACRES. BALES SHALL BE UNSPOILED. AIR-DRIED, AND FREE FROM WEED, SEEDS, AND ANY COARSE MATERIAL

STRUCTURAL NOTES & SPECS

CONTRACTORS SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE FIELD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. THE ENGINEER SHALL BE NOTIFIED OF ANY CONDITIONS WHICH PRECLUDE COMPLETION OF THE WORK IN ACCORDANCE WITH THE CONTRACT DOCUMENTS.

- DESIGN AND CONSTRUCTION OF STRUCTURAL STEEL SHALL CONFORM TO LATEST EDITION OF THE AMERICAN INSTITUTE OF STEEL CONSTRUCTION "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS"
- STRUCTURAL AND MISCELLANEOUS STEEL SHALL CONFORM TO ASTM A992 (FY-50 KSI), UNLESS OTHERWISE NOTED.
- STEEL PIPE SHALL CONFORM TO ASTM A500, GRADE B, STEEL PIPE DIAMETERS NOTED ON THE DRAWINGS ARE NOMINAL
- STRUCTURAL CONNECTION BOLTS SHALL CONFORM TO ASTM A325. ALL BOLTS SHALL BE 3/4" DIAMETER MINIMUM AND SHALL HAVE MINIMUM OF TWO BOLTS, UNLESS NOTED OTHERWISE ON THE DRAWINGS. LOCK WASHER ARE NOT PERMITTED FOR A325 STEEL ASSEMBLIES.
- NON-STRUCTURAL CONNECTIONS FOR STEEL GRATING MAY USE 5/8" DIAMETER GALVANIZED ASTM A 307 BOLTS UNLESS OTHERWISE NOTED.
- ALL STEEL MATERIAL EXPOSED TO WEATHER SHALL BE GALVANIZED AFTER FABRICATION IN ACCORDANCE WITH ASTM A123 "ZINC (HOT-DIPPED GALVANIZED) COATINGS" ON IRON AND STEEL PRODUCTS.
- ALL BOLTS ANCHORS AND MISCELLANEOUS HARDWARE EXPOSED TO WEATHER SHALL BE GALVANIZED IN ACCORDANCE WITH ASTM A153 "ZINC COATING (HOT-DIP) ON IRON AND STEEL HARDWARE.
- DAMAGED GALVANIZED SURFACES SHALL BE REPAIRED BY UP ALL DAMAGED GALVANIZED STEEL WITH COLD ZINC, "GALVANOX", "DRY GALV", "ZINC IT", OR APPROVED EQUIVALENT, IN ACCORDANCE WITH MANUFACTURERS GUIDELINES, TOUCH UP DAMAGED NON GALVANIZED STEEL WITH SAME PAINT APPLIED IN SHOP OR FIELD.
- CONTRACTOR SHALL COMPLY WITH AWS CODE FOR PROCEDURES APPEARANCE AND QUALITY OF WELDS, AND WELDING PROCESSES SHALL BE QUALIFIED IN ACCORDANCE WITH AWS 'STANDARD QUALIFICATION PROCEDURES. ALL WELDING SHALL BE DONE USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND D1 1 WHERE FILLET WELD SIZES ARE NOT SHOWN. PROVIDE THE MINIMUM SIZE PER TABLE JZ. 4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION" 9TH EDITION. AT THE COMPLETION OF WELDING, ALL DAMAGE TO GALVANIZED COATING SHALL BE REPAIRED. SEE NOTE 9.
- THE ENGINEER SHALL BE NOTIFIED OF ANY INCORRECTLY FABRICATED, DAMAGED OR OTHERWISE MISFITTING OR NON CONFORMING MATERIALS OR CONDITIONS TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE ENGINEER REVIEW.

SITE NOTES

1. ALL DIMENSIONS, ELEVATIONS AND EXISTING CONDITIONS SHOWN ON THE DRAWINGS SHALL BE VERIFIED BY THE CONTRACTOR AND THE TESTING AGENCY PRIOR TO BEGINNING ANY MATERIAL ORDERING, FABRICATION OR CONSTRUCTION WORK ON THIS PROJECT. ANY DISCREPANCIES SHALL BE IMMEDIATELY BROUGHT TO THE THE CONTRACTOR OF THE OWNER AND THE OWNERS ENGINEER. THE DISCREPANCIES MUST BE RESOLVED BEFORE THE CONTRACTOR IS TO PROCEED WITH THE WORK. THE CONTRACT DOCUMENTS DO NOT INDICATE THE METHOD OF CONSTRUCTION. THE CONTRACTOR SHALL SUPERVISE AND DIRECT THE WORK AND SHALL BE SOLLETY RESPONSIBLE FOR ALL CONSTRUCTION MEANS, METHODS, TECHNIQUES, SEQUENCES AND PROCEDURES. OBSERVATION VISITS TO THE SITE BY THE OWNER AND/OR THE ENGINEER SHALL NOT INCLUDE INSPECTION OF THE PROTECTIVE MEASURES OR THE CONSTRUCTION PROCEDURES. CONSTRUCTION PROCEDURES.

2. DAMAGE BY THE CONTRACTOR TO UTILITIES OR PROPERTY OF OTHERS, INCLUDING EXISTING PAVEMENT AND 2. DAMAGE BY THE CONTRACTOR TO UTILES ON PAPERT FOR THEM, INC.
OTHER SURFACES DISTURBED BY THE CONTRACTOR DURING CONSTRUCTION SHALL BE REPAIRED TO
PRE-CONSTRUCTION CONDITIONS BY THE CONTRACTOR AT NO ADDITIONAL COST TO THE CLIENT. FOR GRASSED
AREAS, SEED AND MULCH SHALL BE ACCEPTABLE.

3. THE CONTRACTOR SHALL REWORK (DRY, SCARIFY, ETC.) ALL MATERIAL NOT SUITABLE FOR SUBGRADE IN ITS PRESENT STATE. IF THE MATERIAL, AFTER REWORKING, REMAINS UNSUITABLE THEN THE CONTRACTOR SHALL UNDERCUT THIS MATERIAL AND REPLACED WITH APPROVED MATERIAL AT HIS EXPENSE. ALL SUBGRADES SHALL BE PROOF ROLLED WITH A FULLY LOADED TANDEM AXLE DUMP TRUCK PRIOR TO PAVING. ANY SOFT MATERIAL SHALL BE REWORKED AND SEEN ACCE. REWORKED AND REPLACED.

4. THE CONTRACTOR IS REQUIRED TO MAINTAIN ALL DITCHES, PIPES, AND OTHER DRAINAGE STRUCTURES FREE FROM 4. THE CONTRACTION IS REQUIRED TO MAINTAIN ALL DIT ONES, PIFES, AND OTHER PROVINCES THE PROPERTY OF ANY DAMAGES OBSTRUCTION UNTIL WORK IS ACCEPTABLE BY THE OWNER THE CONTRACTOR IS RESPONSIBLE FOR ANY DAMAGES CAUSED BY FAILURE TO MAINTAIN DRAINAGE STRUCTURES IN OPERABLE CONDITION.

5. ALL DIMENSIONS SHALL BE VERIFIED WITH THE PLANS (LATEST REVISION) PRIOR TO COMMENCING CONSTRUCTION.
NOTIFY THE OWNER IMMEDIATELY IF DISCREPANCIES ARE DISCOVERED. THE CONTRACTOR SHALL HAVE A SET OF
APPROVED PLANS AVAILABLE AT THE SITE AT ALL TIMES WHEN WORK IS BEING PERFORMED. A DESIGNATED RESPONSIBLE EMPLOYEE SHALL BE AVAILABLE FOR CONTACT BY GOVERNING AGENCY INSPECTORS

6. CONTRACTOR SHALL SECURE ALL NECESSARY PERMITS FOR THIS PROJECT FROM ALL APPLICABLE GOVERNMENTAL AGENCIES (NOT SUPPLIED BY OWNER).

ANY PERMITS WHICH MUST BE OBTAINED SHALL BE THE CONTRACTORS RESPONSIBILTY. THE CONTRACTOR SHALL BE RESPONSIBLE FOR ABIDING BY ALL CONDITIONS AND REQUIREMENTS OF THE PERMITS (NOT SUPPLIED BY OW

8. ALL WORK SHALL BE IN ACCORDANCE WITH LOCAL CODES AND THE LATEST APPLICABLE CODES AND STANDARDS.

9. THE CONTRACTOR SHALL NOTIFY THE APPLICABLE JURISDICTIONAL (STATE, COUNTY, OR CITY) ENGINEER 24 HOURS PRIOR TO BEGINNING OF CONSTRUCTION

10. CONTRACTOR RESPONSIBLE FOR CLOSING AND FILING ALL PERMITS ASSOCIATED WITH THE SITE

11. THE SITE SHALL BE GRADED TO CAUSE SURFACE WATER TO FLOW AWAY FROM THE EQUIPMENT AND TOWER

12. ALL EXISTING AREAS DISTURBED BY CONSTRUCTION ACTIVITIES SHALL BE RESTORED TO MATCH

13. THE CONTRACTOR SHALL CONTACT 'CALL BEFORE YOU DIG' AT LEAST 48 HOURS PRIOR TO CONSTRUCTION **ACTIVITIES COMMENCING**

CONCRETE NOTES

ALL CONCRETE CONSTRUCTION SHALL BE DONE IN ACCORD WITH AMERICAN CONCRETE INSTITUTE (ACI) CODES 301 & 318, LATEST REVISION.

2. TOWER FOUNDATION WORK SHALL BE IN ACCORDANCE WITH TOWER MANUFACTURERS DESIGNS AND

3. ALL CONCRETE USED SHALL BE 4000 PSI (28 DAY COMP STRENGTH). THE CONCRETE MIX SHALL BE BASED ON USING THE FOLLOWING MATERIALS AND PARAMETERS:

PORTLAND CEMENT: ASTM C150, T1 AGGREGATE: ASTM C33, 1 INCH MAX POTABLE ADMIXTURE: NON-CHLORIDE

4 INCH SLUMP UNLESS NOTED OTHERWISE

*ALL CONCRETE EXPOSED TO FREEZING WEATHER SHALL CONTAIN ENTRAINED AIR PER ACI 211 TABLE 4:2:1 OF ACI

4. ALL REINFORCING STEEL SHALL BE ASTM A615, GR 60 (DEFORMED) UNLESS NOTED OTHERWISE. WELDED WRE FABRIC SHALL CONFORM TO ASTM A185 WELDED STEEL WIRE FABRIC UNLESS NOTED OTHERWISE. SPLICES SHALL BE CLASS B' AND ALL HOOKS SHALL BE ACI STANDARD UND. REINFORCING BARS SHALL BE COLD BENT WHERE REQUIRED AND TIED (NOT WELDED).

5. THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON DRAWNIGS:
CONCRETE CAST AGAINST EARTH = 3 IN.
CONCRETE EXPOSED TO EARTH OR WEATHER.

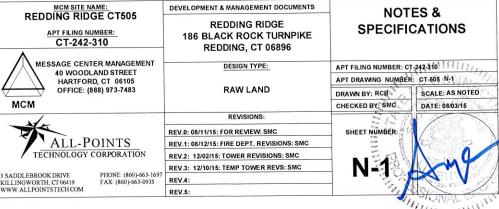
#6 AND LARGER = 2 IN. #5 AND DANSER = 2 IIV.
#5 AND SWALLER = 1 1/2 IN.
CONCRETE NOT EXPOSED TO EARTH OR WEATHER OR NOT
CAST AGAINST THE GROUND. SLAB AND WALL = 3/4 IN BEAMS AND COLUMNS = 1 1/2 IN

6. A 3/4 IN. CHAMFER SHALL BE PROVIDED AT ALL EXPOSED EDGES OR CONCRETE, UNO, IN ACCORDANCE WITH ACI

7. CONCRETE SHALL BE PLACED IN A UNIFORM MANNER AND CONSOLIDATED IN PLACE.

8. CONCRETE FOOTINGS SHALL BE CAST AGAINST LEVEL, COMPACTED, NON-FROZEN BASE SOIL FREE OF STANDING

9. APPLY A QUALITY CONCRETE SEALER SUCH AS THEROSEAL TO EXPOSED CONCRETE IN ACCORDANCE WITH MANUFACTURERS APPLICATIONS DIRECTIONS.



CERTIFICATE OF SERVICE

I hereby certify that on December 18, 2015, an original and 15 copies of the D&M Amendment submission was sent by overnight delivery to the Connecticut Siting Council with copies sent to the below intervenor and property owner. Electronic submission was made on December 21, 2015.

Intervenor:

Cellco Partnership d/b/a/ Verizon Wireless Kenneth C. Baldwin, Esq. Robinson & Cole LLP 280 Trumbull Street Hartford, CT 06103-3597 kbaldwin@rd.com

Facility Site Owner: Redding Ridge Fire District No. 1 Bennet Pardee, Fire Commissioner 186 Black Rock Turnpike, Redding, CT 06896

Dated: December 21, 2015

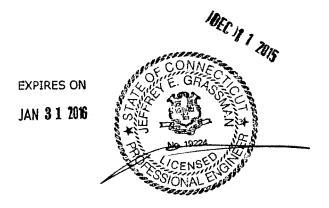
Daniel M. Laub, Esq.



STRUCTURES

VALMONT MICROFLECT
3575 25th St. SE
Salem, OR 97302
PHONE: 1-800-547-2151
ENGINEER: Jonathon Neumann
Reviewed by:

COMMUNICATION POLE DESIGN CALCULATIONS



Message Center Management VALMONT ORDER# 239975

SITE NAME: Redding-Blackrock Tower, CT

POLE HEIGHT: 149FT (150 FT AGL)



STRUCTURES

11/13/15

ENGINEERING DATA

for

Message Center Management Redding-Blackrock Tower, CT VALMONT QUOTATION 239975

1)	STRUCTURE DESIGN CONFORMS TO EIA/TIA-222-F INCLUDING:
•	85.0 MPH FASTEST MILE BASIC WIND SPEED WITH NO ICE
	73.6 MPH FASTEST MILE BASIC WIND SPEED WITH ICE
	DESIGN ICE THICKNESS = 0.50 INCHES
	50.0 MPH FASTEST MILE BASIC WIND SPEED WITH NO ICE FOR TWIST AND SWAY
2)	FEEDLINES ARE ASSUMED TO BE PLACED INTERIOR TO THE POLE.
3)	ALL MICROWAVE ASSUMED TO BE 6 GHz UNLESS OTHERWISE NOTED.
4)	TOTAL POLE HEIGHT IS 150 FT AGL.
5)	ELEVATIONS ARE MEASURED FROM TOP OF BASE PLATE (APPROX. 1 FT AGL).
6)	POLE DESIGN MEETS TIA-222-G ADDENDUM 2.
7)	LOADING AS FOLLOWS:
	149.0' POLE
	1 - 4ft lightning rod @ 149.0
	1 - 2' HIGH PERFORMANCE (5.5 GHz) @ 149.0
	12 - HPA-65R-BUU-H8 @ 145.0
	9 - Ericsson RRUS-11 (19.7"x17"x7.2") @ 145.0
	6 - Ericsson RRUS-12 (20.4"x18.6"x7.4") @ 145.0
	6 - Ericsson RRUS A2 Module (15"x12.8" x3.4") @ 145.0
	3 - RRUS-E2 (20" X 20.4" X 9.5") @ 145.0
	3 - Ericsson RRUS-32 (29.9"x13.3"x9.5") @ 145.0
	4 - Raycap DC6-48-60-18-F (24"x11") @ 145.0
	1 - 12' SP1 LP Platform @ 145.0
	6 - HBXX-6516DS-VTM @ 135.0
	6 - X7C-FRO-660 @ 135.0
	3 - ALU 2X60 PCS RRU @ 135.0
	3 - ALU 2X60 700 RRU @ 135.0
	3 - ALU 4X30 AWS RRU @ 135.0
	2 - DB-T1-6Z-8AB-OZ FIBER DIST. BOX @ 135.0
	1 - 12' SP1 LP Platform @ 135.0
	1 - CARRIER #3 @ 125.0
	1 - CARRIER #4 @ 115.0
	1 - CARRIER #5 @ 105.0
	3 - WHIP (2.5" X 20') @ 79.0
	1 - LARGE YAGI @ 79.0
	3 - 6' Pivot Side Arm @ 79.0

STRUCTURE	ANCHORAGE	INFORMATION
OTTOOTOTIC	711101101010	1111 OT 1110 TITOTT

POLE HEIGHT(FT):	149	NUMBER OF A.B.'s:	24
BOLT CIRCLE(IN):	67.68	DIA. OF A.B.'s(IN):	2.25
BASE VERTIC	61.82	LENGTH OF A.B.'s(IN):	66.00
BASE SHEAR(K):	42.08	PROJECTION LENGTH(IN):	12.50
BASE MOMENT(FT-K):	4899	TEMPLATE OD(IN):	71.18







STRUCTURES

BY	DATE	SINOCIONES
CHKD. BY	DATE	SHEET NO

11/13/15 **ENGINEERING DATA**

for

Message Center Management Redding-Blackrock Tower, CT **VALMONT QUOTATION 239975**

EIA/TIA-222-F

BASIC WIND:

85.0 MPH

WIND & ICE:

MPH AND 0.5 IN. ICE 73.6

TWIST & SWAY: 50.0

			DATA W.C). ICE	DATA W/ ICE			
QTY	DESCRIPTION	HEIGHT	EPA	WT	EPA	WT		
1	4ft lightning rod	@ 149.0 '	0.25	10	2.00	22		
1	2' HIGH PERFORMANCE	@ 149.0 '	5.29	83	7.80	124		
12	HPA-65R-BUU-H8	@ 145.0 '	107.64	1188	138.72	2808		
9	Ericsson RRUS-11 (19.7"x17"x7.2")	@ 145.0 '	14.31	459	19.80	747		
6	Ericsson RRUS-12 (20.4"x18.6"x7.4")	@ 145.0 '	10.62	348	14.46	558		
	Ericsson RRUS A2 Module (15"x12.8" x3.4")	@ 145.0 '	4.92	126	7.68	222		
3	RRUS-E2 (20" X 20.4" X 9.5")	@ 145.0 '	5.97	216	7.98	339		
3	Ericsson RRUS-32 (29.9"x13.3"x9.5")	@ 145.0 '	6.90	231	9.15	360		
4	Raycap DC6-48-60-18-F (24"x11")	@ 145.0 '	3.84	100	5.36	192		
1	12' SP1 LP Platform	@ 145.0 '	31.42	1143	55.71	1491		
6	HBXX-6516DS-VTM	@ 135.0'	23.10	276	31.32	672		
6	X7C-FRO-660	@ 135.0 '	40.44	408	51.96	1056		
3	ALU 2X60 PCS RRU	@ 135.0 '	4.65	120	6.51	204		
3	ALU 2X60 700 RRU	@ 135.0 '	4.83	138	6.69	237		
3	ALU 4X30 AWS RRU	@ 135.0 '	7.20	105	9.39	252		
2	DB-T1-6Z-8AB-OZ FIBER DIST. BOX	@ 135.0 '	7.68	10	9.48	198		
1	12' SP1 LP Platform	@ 135.0 '	15.71	1143	27.77	1491		
1	CARRIER#3	@ 125.0'	112.35	2388	155.73	4134		
1	CARRIER #4	@ 115.0 '	112.35	2388	155.73	4134		
1	CARRIER #5	@ 105.0 '	112.35	2388	155.73	4134		
3	WHIP (2.5" X 20')	@ 79.0'	20.70	213	52.56	468		
	LARGE YAGI	@ 79.0'	9.06	81	13.38	112		
-	6' Pivot Side Arm (50" pipe)	@ 79.0'	8.76	387	17.76	576		
	, ,,,	=						





DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR: BY VALMONT INDUSTRIES

*

SUMMARY

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Design Code: BIA-222-F	1 1 1 1 1 1 1 1	!	DESIGN SUMMARY		; ; ; ; ; ; ; ;	
Height Above Base Plate (ft) 149.00		Ground Line Diameter (in)	л) 60.250	Pole Shaft Weight (lbs)	29547	
	Top Diameter (in)	ter (in)	19.752			
	Pole Tape	Pole Taper (in/ft)	0.28606	Shape: 18 Sides		
Connections Between Sections	/First/	/Second/	/Third/	/Fourth/		
Height Above Ground (ft) Type Overlap Length (in) Maximum Axial Force (lbs)	52.50 Slip Joint 77 38986	85.00 Slip Joint 65 28805	111.00 Slip Joint 55 19840	130.50 Flange Joint 0 10471		
Section Characteristics	/First/	/Second/	/Third/	/Fourth/ /Fifth/	/1	
Base Diameter (in) Top Diameter (in) Thickness (in) Length (ft) Weight (lbs)	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	47.942 36.810 0.43750 38.917 7712	39.109 30.122 0.37500 31.417 4357	31.933 25 25.044 19 0.25000 0.1. 24.083 18	25.044 19.752 0.18750 18.500 832	
	A	ANALYSIS SUMMAKI	Governing	Governing Governing	ing Governing	Pole

	pole Top	ICE + WIND 149.00 9 369 106 0.17 51.99 99.90
	Governing Level Sec.5	ICE + WIND 130.50 2212 16636 10471 25.08 51.99 2.07
	Governing Level Sec.4	ICE + WIND 111.00 7445 28895 19840 42.05 51.99 1.24
	Governing Level Sec.3	ICE + WIND 85.00 17961 35637 28805 44.97 51.99 1.16
	Governing Level Sec.2	ICE + WIND 52.50 32989 39797 38986 46.84 51.99 1.11
	Governing Level Sec.1	ICE + WIND 29.00 44366 40765 48129 43.45 51.99 1.20 3.04
•	Pt. of Fixity	ICE + WIND 0.00 58792 42145 58459 42.68 51.99 1.22 0.00
		Governing Load Case Height (ft) Resultant Moment (in-kips) Shear Force (lbs) Axial Force (lbs) Combined Stress (ksi) Allowable Stress (ksi) Allowable Combined Stress Total Deflection (in)

Note: Diameters are outside, measured across the flats Forces and moments are reported in the local element coordinate system

DATE 11/13/2015	בות דידיייי									
ACKROCK TOWER, CT		(lbs) 29547		70			/Fifth/	25.044 19.752 0.18750 18.500	/Fifth/	24.990 19.752 0.18750 18.313
MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT	ED	Pole Shaft Weight (lbs)		Shape: 18 Sides		130.50 Flange Joint 2.000 0.250	/Fourth/	31.933 25.044 0.25000 24.083	/Fourth/	31.933 25.098 0.25000 23.896
	ONS AS DETAIL	60.250 Pol	19.752	0.28606 Sha	/Third/ /Fourth/	0	/Third/	39.109 30.122 0.37500 31.417	/Third/	39.109 30.122 0.37500 31.417
	CTION DIMENSI	eter (in)		~		52.50 85.00 111.00 Slip Joint Slip Joint	/Second/	47.942 36.810 0.43750 38.917	/Second/	47.942 36.810 0.43750 38.917
	- SUMMARY OF SECTION DIMENSIONS AS DETAILED	다 유 다	Pole Taper (in/ft)	/First/ /Second/	/First/		60.250 45.232 0.50000 52.500	/First/	60.250 45.232 0.50000 52.500	
BY VALMONT INDUSTRIES FOR:		Height Above Base Plate (ft) 149.00			Connections Between Sections /F	Height Above Ground (ft) Type Flange Thickness (in) Weld Root Gap (in)	Theoretical Design Section Dimension	Base Diameter (in) Top Diameter (in) Thickness (in) Length (ft)	As Detailed Section Characteristic	Base Diameter (in) Top Diameter (in) Thickness (in) Length (ft)
BY	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	Height A			Connecti	Не ТУ F1	Theoreti	Ba To Th	As Detai	Ba To Th

Note: Diameter are outside, measured across the flats

DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR: BY VALMONT INDUSTRIES

Notes 42600 42078 14753 Resultant (X & Y) (1bs) Shear In In X-Direction Y-Direction 32634 32234 11301 Shear (1bs) 27383 27047 9483 *** POLE SHAFT POINT OF FIXITY REACTIONS *** Shear (1bs) 44070 58507 43565 Vertical Force (lbs) 000 Torsional (in-kips) Moments 57227 58792 19834 Moments Resultant (X & Y) (in-kips) -36785 -37791 -12749 Moments About Y-Axis (in-kips) 43839 45037 15194 Moments About X-Axis (in-kips) ICE + WIND T+S Identifier Loading Case WIND

Note: Positive vertical force is downward. Reactions are considered in the global coordinate system.

R, CT DATE 11/13/2015 Fuse 1.13.0.0		Orientation of System	* * (Transverse)	: *	* (Vertical)	* +Z-Axis
E: REDDING-BLACKROCK TOWE		Orientat	*	*	(Longitudinal) *	+Y-Axis *
LE, SIT						
MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT		85.00 mph Ice Thickness 0.00	50.0 Degrees Clockwise From +X Axis	.69	Orientations are Measured Clockwise From +X Axis	Positive Y Axis is 90 Degrees Clockwise From +X Axis Foundation Rotation of 0.00 Degrees Elevation of structure base above surrounding terrain = 1.00 ft
FOR:	7 1 1	w	50.0	actor 1.	asured (s 90 Deg of 0.00 ure base
BY VALMONT INDUSTRIES	Design Code BIA-222-F Loading Case WIMD	Ve	Wind Orientation is	Exposure C, Gust Factor 1.69	Orientations are Me.	Positive Y Axis is 90 Deg Foundation Rotation of 0.00 Elevation of structure base

•	1-4ft lightni	1-2' HIGH PER	12-HPA-65R-BUU	9-Ericsson RR	6-Ericsson RR	6-Ericsson RR	3-RRUS-E2 (20	3-Ericsson RR	4-Raycap DC6-	1-12' SP1 LP	6-HBXX-6516DS	6-X7C-FRO-660	3-ALU 2X60 PC	3-ALU 2X60 70	3-ALU 4X30 AW	2-DB-T1-6Z-8A	1-12; SP1 LP	1-CARRIER #3
EPA (£t^2)	0.25	5.29	107.64	14.31	10.62	4.92	5.97	6.90	3.84	31.42	23.10	40.44	4.65	4.83	7.20	7.68	15.71	112.35
Force-Z (lbs)	10	83	1188	459	348	126	216	231	100	1143	276	408	120	138	105	10	1143	2388
Force-Y (lbs)	σı	196	3942	524	389	180	219	253	141	1151	829	1451	167	173	258	276	564	3945
Force-X (lbs)	8	164	3308	440	326	151	183	212	118	996	969	1218	140	145	217	231	473	3310
Orientation in XY Plane (Degrees)	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00
Load Eccentricity (ft)	0.00	0.00	0.00	00.00	00.00	00.00	00.00	0.00	00.00	0.00	0.00	00.00	00.00	00.00	00.00	00.00	00.00	00.0
Load Height (ft)	151.00	151.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	135.00	135.00	135.00	135.00	135.00	135.00	135.00	125.00
Mounting Height (ft)	149.00	149.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	135.00	135.00	135.00	135.00	135.00	135.00	135.00	125.00
Load Number	Н	73	м	4	ហ	9	7	ω	σ	10	11	12	13	14	15	16	17	18

DATE 11/13/2015	0.0.ET:T asn.		System 1-CARRIER #3 1-CARRIER #3 1-CARRIER #3	1-CARRIER #4	1-CARRIER #5	3-WHIP (2.5"	1-LARGE YAGI	3-6' Pivot Si
CK TOWER, CT		9 · · · · · · · · · · · · · · · · · · ·	Orientation of System $1-C^{\gamma}$ EPA $1-C^{\gamma}$ $(\pm t^{-2})$ $1-C^{\gamma}$	112.35	112.35	20.70	9.06	8.76
EDDING-BLACKRO		Ċ	Force-Z (lbs)	2388	2388	213	81	387
MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER,		Force-Y (1bs)	3853	3755	638	279	270	
	INPUT LOADS ***		Force-X (lbs)	3233	3151	536	234	227
	* *		Orientation in XY Plane (Degrees)	50.00	50.00	50.00	50.00	50.00
FOR:		WIND - Continued	Load Eccentricity (ft)	00.00	00.00	00.00	00.00	00.00
USTRIES		WIND -	Load Height (ft)	115.00	105.00	79.00	79.00	79.00
BY VALMONT INDUSTRIES		Loading Case	Mounting Height (ft)	115.00	105.00	79.00	79.00	79.00
BY		Lo	Load Number	19	20	21	22	23

DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT

FOR:

BY VALMONT INDUSTRIES

*** INPUT LOADS ***

Basic Wind Velocity is 73.61 mph Ice Thickness 0.50 Wind Orientation is 50.0 Degrees Clockwise From +X Axis Structure Weight Overload Factor is 1.000 Gust Factor 1.69 EIA-222-F ICE + WIND Exposure C, Loading Case Design Code

Orientation of System

12-HPA-65R-BUU 6-X7C-FRO-660 9-Ericsson RR RR 3-RRUS-E2 (20 6-HBXX-6516DS 3-ALU 2X60 70 3-ALU 4X30 AW 2-DB-T1-6Z-8A 1-2' HIGH PER 6-Ericsson RR 3-Ericsson RR 1-4ft lightni 4-Raycap DC6-1-12' SP1 LP 1-12' SP1 LP 1-CARRIER #3 (Transverse) 6-Ericsson 3-ALU 2X60 +***** +X-Axis (Vertical) +Z-Axis 9.48 2.00 7.68 7.98 9.15 5.36 55.71 51.96 6.51 9.39 155.73 7.80 19.80 31.32 69.9 27.77 138.72 14.46 EPA (ft^2) (Longitudinal) +Y-Axis 339 672 1056 4134 22 2808 747 558 222 360 192 1491 204 237 252 198 1491 124 Force-Z (lbs) 255 4101 3810 1530 1398 175 180 253 747 217 544 397 211 251 147 843 Force-Y (1bs) Foundation Rotation of 0.00 Degrees Elevation of structure base above surrounding terrain = 1.00 ft 1173 212 1284 707 147 627 47 182 3197 456 333 177 184 211 124 151 Force-X (lbs) Positive Y Axis is 90 Degrees Clockwise From +X Axis Axis 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 50.00 Orientation in XY Plane 50.00 50.00 50.00 50.00 50.00 50.00 50.00 (Degrees) Orientations are Measured Clockwise From +X 0.00 0.00 0.00 00.0 00.0 00.0 00.0 00.0 0.00 0.00 0.00 0.00 0.00 00.0 00.0 00.0 00.0 00.0 Eccentricity Load (ft) 145.00 145.00 145.00 151.00 151.00 145.00 145.00 145.00 145.00 145.00 135.00 135.00 135.00 135.00 135.00 135.00 135.00 125.00 Height Load (ft) Mounting Height 135.00 135.00 135.00 135.00 125.00 145.00 145.00 135.00 135.00 135.00 149.00 145.00 145.00 145.00 145.00 149.00 145.00 145,00 (ft) Number Load

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MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR: BY VALMONT INDUSTRIES

DATE 11/13/2015 Fuse 1.13.0.0 1-CARRIER #3 1-CARRIER #3 1-CARRIER #3 3-6' Pivot Si 1-CARRIER #4 1-CARRIER #5 3-WHIP (2.5" 1-LARGE YAGI Orientation of System 17.76 13.38 155.73 155.73 52.56 EPA (ft^2) 112 576 4134 4134 468 Force-Z (1bs) 4005 1216 309 3903 411 Force-Y (1bs) *** INPUT LOADS *** 3361 3275 1020 260 345 Force-X (1bs) Orientation in XY Plane (Degrees) 50.00 50.00 50.00 50.00 50.00 ICE + WIND - Continued Load Eccentricity (ft) 00.00 00.00 00.0 00.00 0.00 105.00 79.00 79.00 79.00 115.00 Load Height (ft) Mounting Height (ft) Loading Case 79.00 79.00 79.00 115.00 105.00 Load Number 13 20 21 22 23

MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR:

BY VALMONT INDUSTRIES

DATE 11/13/2015 Fuse 1.13.0.0 Orientation of System
+****** +X-Axis
* * (Transverse) * (Vertical)
* +Z-Axis (Longitudinal) * +Y-Axis * *** INPUT LOADS *** Basic Wind Velocity is 50.00 mph Ice Thickness 0.00 Wind Orientation is 50.0 Degrees Clockwise From +X Axis Structure Weight Overload Factor is 1.000 Exposure C, Gust Factor 1.69 Orientations are Measured Clockwise From +X Axis Positive Y Axis is 90 Degrees Clockwise From +X Axis Foundation Rotation of 0.00 Degrees Elevation of structure base above surrounding terrain = 1.00 ft EIA-222-F T+S Design Code Loading Case

	1-4ft lightni	1-2' HIGH PER	12-HPA-65R-BUU	9-Ericsson RR	6-Ericsson RR	6-Ericsson RR	3-RRUS-E2 (20	3-Ericsson RR	4-Raycap DC6-	1-12' SP1 LP	6-HBXX-6516DS	6-X7C-FRO-660	3-ALU 2X60 PC	3-ALU 2X60 70	3-ALU 4X30 AW	2-DB-T1-6Z-8A	1-12' SP1 LP	1-CARRIER #3
EPA (ft^2)	0.25	5.29	107.64	14.31	10.62	4.92	5.97	6.90	3.84	31.42	23.10	40.44	4.65	4.83	7.20	7.68	15.71	112.35
Force-Z (1bs)	10	83	1188	459	348	126	216	231	100	1143	276	408	120	138	105	10	1143	2388
Force-Y (lbs)	m	68	1364	181	135	62	16	87	49	398	287	502	58	09	89	95	195	1365
Force-X (1bs)	m	57	1145	152	113	52	63	73	41	334	241	421	48	50	75	80	164	1145
Orientation in XY Plane (Degrees)	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	20.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00	50.00
Load Eccentricity (ft)	00.00	00.00	0.00	00.00	00.00	00.00	00.0	00.0	00.00	00.00	00.00	00.0	00.00	00.0	00.00	00.0	00.0	0.00
Load Height (ft)	151.00	151.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	135.00	135.00	135.00	135.00	135.00	135.00	135.00	125.00
Mounting Height (ft)	149.00	149.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	145.00	135.00	135.00	135.00	135.00	135.00	135.00	135.00	125.00
Load	н	7	м	4	Ŋ	9	7	æ	σ,	10	11	12	13	14	15	16	17	18

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MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR: BY VALMONT INDUSTRIES

DATE 11/13/2015 Fuse 1.13.0.0 Orientation of System 1-CARRIER #3
EPA 1-CARRIER #3
(ft^2) 1-CARRIER #3 1-LARGE YAGI 1-CARRIER #4 1-CARRIER #5 3-WHIP (2.5" 9.06 112.35 112.35 20.70 2388 2388 213 81 Force-Z (1bs) 1333 1299 221 97 9 Force-Y (1bs) *** INPUT LOADS *** 1119 1090 185 78 81 Force-X (1bs) Orientation in XY Plane (Degrees) 50.00 50.00 50.00 50.00 50.00 Load Eccentricity (ft) 00.0 00.0 0.00 0.00 0.00 T+S - Continued 105.00 79.00 79.00 Load Height (ft) 115.00 79.00 Mounting Height (ft) Loading Case 105.00 79.00 79.00 79.00 115.00 Load Number 19 20 21 22 23

3-6' Pivot Si

8.76

387

DATE 11/13/2015 Fuse 1.13.0.0

*** Properties ***

Area (in^2)	11.64	12.49 13.35 14.03	19.67	20.92	23.19 23.19 23.42 24.10	35.41	36.09	37.79 39.49 41.19 42.90	50.51	5 5 7 5 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8 8	70.99
Moments of Inertia (in^4)	563 668	696 848 984 1020	1154	1837 1837 1898 1898	2502 2502 2576 2808	3957	4190 4504 4682	4811 5491 6232 7037 7729	8439 8640 956	10854 10854 12042 13349 14749 16238	17940
w/t Across Flats	16.81	18.16 19.50 20.58 20.85	21.79	17.01	19.03 19.23 19.83	12.40	13.02	13.34 14.69 15.36 15.90	13.07	11 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	14.19
D/t Across Flats	105.34	112.97 120.60 126.70 128.23	133.57	106.47	117.91 119.06 122.49	80.33	83.82 84.90	85.67 89.48 93.29 97.11	84.14 84.79 87.68	88.06 91.33 94.60 97.87 101.14 104.41	90.46
Wall Thickness (in)	0.1875	0.1875 0.1875 0.1875 0.1875	0.1875	0.2500	0.2500	0.3750	0.3750	0.3750 0.3750 0.3750 0.3750	0.4375	0.4375 0.4375 0.4375 0.4375 0.4375 0.4375	0.5000
Diameter Across Flats (in)	19.752	21.182 22.613 23.757 24.043	25.044 25.044 25.473	26.617 26.904 28.334	29.478 29.764 30.622	30.122	31.433	33.555 34.985 36.416 37.560	36.810 37.096 38.359	38.526 39.957 41.387 42.817 44.247 45.678	45.232
Distance From Base (ft)	149.00	144.00 139.00 135.00 134.00	130.50	125.00 124.00 119.00	115.00 114.00 111.00	111.00	105.00	99.00 94.00 89.00	85.00 84.00 79.58	79.00 74.00 69.00 64.00 59.00 52.00	52.50
Connection Locations	Top of Sect 5 EPA 3	EPA 11	Top of Sect 4	EPA 18	EPA 19	Top of Sect 3	Base of Sect 4 EPA 20		Top of Sect 2 Base of Sect 3	EPA 21	Top of Sect 1

DATE
ដ
TOWER,
: REDDING-BLACKROCK TO
SITE:
POLE,
150'
MANAGEMENT
CENTER
MESSAGE
R:

DATE 11/13/2015 Fuse 1.13.0.0 FOR:

		Area	(in^2)	73.90	77.12	79.39	81.65	83.92	86.19	88.46	90.73	93.00	94.82
	- S.	Inertia	(in	20240									
* * *	w/t	Across	Flats	15.05	15.55	16.05	16.56	17.06	17.57	18.07	18.58	19.08	19.48
Properties	D/t	Across	Flats	95.33	98.19	101.05	103.91	106.77	109.63	112.49	115.35	118.21	120.50
* * *	Wall	Thickness	(nr)	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000
	Δ .			47.663									
	Distance From	Base	(IE)	44.00	39.00	34.00	29.00	24.00	19.00	14.00	9.00	4.00	00.0
		Connection	Base of Sect 2	4 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3 3									Pt of Fixity

DATE 11/13/2015 Fuse 1.13.0.0

FOR: BY VALMONT INDUSTRIES

Forces and Moments for Pole in the Local Element Coordinate System

Axial (1bs)	65	227	3096	3138	3377	3562	5275	5344	5516	5541	5669	5947	7865	7987	8438	8747	10745	10878	11120	28111	71637	91221	12398	14426	14636	15436	16271	17124	17716	17794	18196	19727	19831	20511	21581	22684	23822	24992	26143	26465
Resultant Shear (lbs)	276	494	9716	9772	10057	10304	15351	15406	15633	15625	15717	15996	21338	21391	21725	22029	27225	27281	27516	19776	07870	27866	27985	33044	33092	33456	33825	34207	34575	34535	34597	35013	35068	36606	36988	37372	37756	38140	38557	38702
Shear Y-Dir. (lbs)	212	378	7443	7486	7704	7893	11759	11802	11976	11969	12040	12254	16346	16386	16643	16875	20856	20898	21079	21059	21181	21346	21437	25313	25350	25629	25912	26204	26486	26455	650	26822	26864	28042	28335	28629	28923	29217	29536	29648
Shear X-Dir. (lbs)	177	317	6245	6281	6465	6623	9867	9903	10049	10043	10103	10282	13716	13750	13965	14160	17500	17536	17687	17671	17773	17912	17988	21240	21271	21505	21743	21988	22224	22199	22238	22506	22541	23530	23776	24022	24269	24516	24784	24877
Torsion (in-kips)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	. 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
Resultant Mx & My (in-kips)	7	25	25	142	737	1226	1226	1410	2062	2062	2344	3105	3105	3362	4656	2106	5706	6034	7020	7020	7682	8543	9017	9017	9414	11413	13433	15477	17127	17127	17542	19388	19633	19633	21844	24078	26334	28614	30917	31612
My (in-kips)	4	-16	-16	-91	-474	-788	-788	-907	-1325	-1325	-1507	-1996	9661-	-2161	-2993	-3668	~3668	-3878	-4512	-4512	-4938	-5491	-5796	-5796	-6051	-7336	-8635	-9948	-11009	-11009	-11276	-12462	-12620	-12620	-14041	-15477	-16927	-18393	-19873	-20320
e WIND Mx (in-kips)	ις	19	19	109	565	939	93	1080	58	1580	1796	2379	2379	2575	3567	4371	4371	4622	5378	5378	88	ഗ	o,	6908	C4	87	02		37	312	343	14852	504	504	673	844	Ę,	9	23684	24217
Loading Case WIND Dist. From Base M (ft) (in-k	149.00	145.00	145.00	144.00	139.00	135.00	135.00	134.00	130.50	130.50	σ	S	S	124.00	o,	S	LO	₩.		i	φ.	ů.	'n.	105.00	₹.	φ.	٠			rυ.	₹.	79.58	o,	σ.	₹.	ė,	4.	e,	4	ς.

DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER. FOR:

Ω	E4																				
ដ :				17	î	7000	1000	28244	9689	21201	7 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	T 74 / T 6	3202	14706	16243	7817	20426	9 6	C/01	2744	44022
TOWER				AXi	(1bs)	•	•	. 4				'1 '	•••	(*)	117	(P)	, (*	, ,	4 '	4	4,
			Resultant	Shear	(lbs)	כשטמר	7000	38954	39205	29329	70000	***************************************	4005I	40399	40753	41113	41480	1 1 6	CC01#	42244	42649
SITE: KED			Shear	Y-Dir.	(lbs)	01986	9 6	73847	30033	30128	30408	9 6	7890£	30947	31218	31494	31.775	22062	7000	32361	32671
ישחסא .חבד זאי	E		Shear	X-Dir.	(1bs)	24846	1 0	25039	25201	25280	25515	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	##/C7	25968	26195	26427	26663	25902	1 1	Z/154	27415
מואמטאאיייי אפוואם	in the Local Element Coordinate System			Torsion	(in-kips)	0	, ,	>	0	0	c	, ,) (D	0	0	0	c	• 0	>	0
	cal Element C		Resultant	Mx & My	(in-kips)	31612	AACEE	# 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	34612	35595	37969	40365	7 7	T9/75	45219	47679	20160	52664	001111	OCTOO	57227
	Pole in the Lo			ΜV	(in-kips)	-20320	-21369	0 0	-22248	-22880	-24406	-25946	00776	66417-	-29066	-30647	-32242	-33852	35475	7	-36/85
	for	WIND .		MX .	(sdix-ui)	24217	25466	1 1 1	CTC 07	27267	29086	30921	27772	7777	34640	36524	38425	40343	4227B	0 0 0	45639
	Forces and Moments	Loading Case WIND	Dist. From	Base	(11)	52.50	49.00	90	0 .	44.00	39.00	34.00	29.00		00.47	19.00	14.00	9.00	4.00		

FOR: BY VALMONT INDUSTRIES

BY \	BY VALMONT INDUSTRIES	NDUSTRIES	FOR:	MES	SAGE CENT	MESSAGE CENTER MANAGEMENT 150'	ENT 150' P	POLE, SITE:		REDDING-BLACKROCK TOWER,	OWER, CT	
Deflections	and	Stresses f	for Pole									Fuse 1.13.0.0
Loading C	Case WIND					Ŭ * *	*** Deflections	and	Stresses ***			
Distance From Base (ft)	Defl. X-Dir (in)	Defl. Y-Dir (in)	Defl. Resultant X & Y (in)	Defl. Z-Dir (in)	Rotation (deg.)	Applied Bending Stress (ksi)	Applied Axial Stress (ksi)	Applied Torsion Stress (ksi)	Applied Shear Stress (ksi)	Applied Combined Stress (ksi)	Allowable Stress (ksi)	Allowable Divided by Combined
149.00	60.9	72.5	94.7	и, С	70 7	0.12	0	c	2	ć		ć
145.00	57.7	68.7	89.7) m	96.10	0.40	10.0	•	0.00	7.7	שני. בים מים	05.00
145.00	57.7	68.7	89.7	9.6	5.96	0.40	0.25	00.00	0 H	2.76	7 L L	טט. עט אמ מר
144.00	56.9	67.8	88.5	а .2	5.96	2.20	0.25	0.00	1.57	2.76	51.99	18.87
139.00	52.9	63.0	82.3	2.9	5.89	9.98	0.25	00.0	1.51	10.24	51.99	5.08
135.00	4.5.7	59.3	77.4	2.6	^	15.02	0.25	00.00	1.48	15.28	51.99	3.40
134 00	7.0	υ п υ α	77.4	10.10	5.79	15.02	0.38	0.00	2.20	15.40	51.99	3.38
130.50	46.3	55.2	72.0	4 7. 10 4.	5.76 5.63	16.87 22.72	0.38	0.00	2.18	17.25	51.99	3.01
								1)	•	7
130.50	46.3	55.2	72.0	•	φ.	17.17	0.28	00.00	1.60	17.45	51.99	2.98
124.00	n c	m	70.2	.3	5.58	18.85	0.28		1.58	19.14	51.99	2.72
125.00	2.24	50.3	. n	0.0	7. 64.	22.84	0.28	0.00	1.54	23.13	51.99	2.25
124.00	1 -		0.79 0.10		υ п 4. и 2. о	42.84	0.38		2.05	23.22	51.99	2.24
119.00	37.9	, m	0.69		5.16	30.18	0.38		2.U3	24.98	אניבת מטיבת	2.12
115.00	LO.	H	54.8	Н 5.	4.95	34.13	0.38		. E	34.53	• -) L
115.00	Ŋ	ä	54.8	1.5	4.95	34.13	0.46		2.36	34.59	51.99	1.50
114.00	4	41.2	53.7	1.5	4.89	35.39			2.34	35.85	51.99	1.45
	C/I	œ	50.7	1.4	4.72	38.87	0.46	00.0	ų.	39.33	i.	1.32
	3	æ	50.7	1.4	4.72	7.1	0.32	0.00	1.56	27.45	51.99	
	Н	~	48.8	1.3	4.64	σ,	w	•	1.54	28.90		1.80
	σ, ι	S)	46.3	1.2	4.52	30.27	'n	•	1.52	30.60	51.99	
105.00	30 0	ಳ	44.0	4,	4.46	31.13	ų.	٠	1.50	31.46	51.99	1.65
	ο α	t r	44.9	-i -	4.46	31.13	0.39	٠	1.77	31.52	≓,	1.65
	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	30.3) L.	T 6	4.41	34.32	0.39	00.0	1.76	32.30	51.99	1.61
94.00	N	~	35.3	8.0	3.92	38.29	0.0		יין ר צע	20.00	ביברת	n <
9	0	4	31.3	0.7	3.66		4		1.60	41.06		10.1 10.1
ιú ·	œ	ન	28.3	9.0	3.45	0	4.	00.0	ru.	42.66	51.99	1.22
r)	Φ)	\vdash	28.3	9.0	3.45	37.93	0.35	00.00	1.37	38.28	51.99	1.36
₩.	7	Н	27.6	0.5	3.40	38.24	0.36	00.0	1.37	38.60	٥.	1.35
σ.	S	α	24.6	0.5	3.19	9.4	ų.	00.0	1.34	39.85	ď	1.30
σ	n r	co c	24.2	4.0	3.16	39.63	w.	00.00	1.33	40.00	ri	1.30
ν.	n r	ď	24.2	0.4	3.16	6	ų.	۰.	1.39	40.02	O.	1.30
69.00	13.5	1.6.1	21.0	4.0	2.92	40.94	0.39	0.00	H .	41.33	51.99	1.26
3 44	4 0	7 -	1 t		7 . O .	42.UI	4, 4	00.00	27 F	42.41	o, c	1.23
ı on	. m	10	1 1	. 0	2.22	44.04.09.09.09.09.09.09.09.09.09.09.09.09.09.	4.0	20.0	7 · · ·	43.43	T (T	1.70 8. r
₹#	6.9	8.2	10.7	0.1	1.99		0.42	0.00	1.23	44.57	1 -1	1.17

BY VALMONT INDUSTRIES FOR:

MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT

Deflections and Stresses for Pole

*** Deflections and Stresses ***

DATE 11/13/2015 Fuse 1.13.0.0

Loading Case WIND

Allowable Divided by Combined	1.16		1.6.	/ V . F	9 C	0 7 · F	7.73	1.25	1.25	1.24	1.25	100	1 .	1.45	1.25	1.26
Allowable Di Stress C (ksi)	51.99		U 0	U. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1. 1.	7. 1. 1	11.00	E	51.99	51.99	51.99	51.99	00	100	44.1C	51.99	51.99
Applied Combined Stress (ksi)	44.72	0.7	40.04	14.00 10.11	72.12	71.5	7	41.6y	41.76	41.78	41.76	41 70	27 - 77	70.14	41.51	41.41
Applied Shear Stress (ksi)	1.23	0) a	1.00	יים ד		1 1	TO.1	0.99	0.98	0.96	0.94	. 0		0.91	0.90
Applied Torsion Stress (ksi)	0.00	0		00.0	00.0	000		00.0	0.00	0.00	00.0	00.00	000		00.00	00.00
Applied Axial Stress (ksi)	0.42	0.37	0.39	0.40	0.41	0.41		7.00	0.43	0.43	0.44	0.45	0.45	, ,	0.46	0.46
Applied Bending Stress (ksi)	44.30	40.47	40.70	40.87	40.96	41.15	70 17	70:1:	41.33	41.34	41.32	41.26	41.17	. L	41.05	40.95
Rotation (deg.)	1.92	1.92	1.78	1.66	1.58	1.38	ני		DO - 0	0.81	0.63	0.46	0.29		0.13	00.00
Defl. Z-Dir (in)	0.1	0.1	0.1	0.1	0.1	0.0	C			0.0	0.0	0.0	0.0	c		0.0
Defl. Resultant X & Y (in)	10.1	10.1	8.7	7.7	7.0	5.4	4.1			0.7	1.2	0.7	0.3	c	1 1	0.0
Defl. Y-Dir (in)	7.7	7.7	6.7	5.9	5.4	4.2	3.1	, C) L	. i	0.4	0.51	0.2	c		0.0
Defl. X-Dir (in)	6.5	6.5	5.6	4.9	4.5	Э.S	5.6	1.9		n (р ·	4.	0.5	0.0))
Distance From Base (ft)	52.50	52.50	49.00	46.08	44.00	39.00	34.00	29.00	24 00	7 6	19.00	14.00	9.00	4.00		

	1 124					vo	œ.	et '	an '	n r	n -	, ~	•		_						~	_																						
TO STROP				Axial		106	318	5984	6038	6348	0360	10247	10471		10500	10655	10995	14611	14756	15301 17705	15580	19385	19840		19908	20431	21099	21305	25044	25283	26196	24.1.4 28103	28805	00000	29339	31066	31184	32286	33490	34732	36011	37327	38622	38986
SITE: REDDING-BLACKBOCK TOWER			Resultant	Shear (1bs)	•	369	550	80 F C	1010 t	10987	16413	16449	16636	,	16619	16683	16914	72630	T0977	16627 16166	1 # T C Z	28460	28895		28848	28963	29128	29226	34617	34620	00040	35.00	35637	איני	35586	35904	35948	æ	38696	38932	39166	39398	39681	39797
			Shear	Y-Dir. (1bs)	1	283	422	0000	0000	8417	12573	12601	12744		12/31	12/80	17231	17267	17536	17777	01970	21987	22135	:	22099	22187	22314	22389	26518	76520	00000	27070	27299	27247	27260	27504	27538	29461	29643	29824	30003	30180	30397	30486
TENT 150' POLE	cem		Shear	X-Dir. (1bs)	1	737	5354	6784	1269	7062	10550	10573	10694	0	10002	10877	14545	14560	14714	14875	18435	18450	18574	t t	18543	18617	18723	18785	10000	22433	22555	22715	22907	22863	22874	23079	23107	24721	24873	25025	25175	25324	25506	25581
MESSAGE CENTER MANAGEMENT 150' POLE,	oordinate System			Torsion (in-kips)	c	o c		0	0	0	0	0	0	c	o c	o c	0	. 0	0	0	0	0	0	c	> 0	o c	> 0	> C	,	o 0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
MESSAGE	Œ		Resultant	Mx & My (in-kips)	σ) E	31	157	798	1320	1320	1517	2212	2272	2512	3318	3318	3590	4958	6909	6909	6408	7445	7000	9 6 6	0000	ט היינט ט היינט	9 22 60	9952	12039	14141	16258	17961	17961	18389	20285	20536	20536	22855	25189	27536	29898	32273	32989
ES FOR:	Pole in the Local		ž	My (in-kips)	9	-20	-20	-101	-513	-849	-849	- 975	-1422	-1422	-1615	-2133	-2133	-2308	-3187	-3897	-3897	-4119	-4785	-4785	-5231	- 587	-6129	-6129	-6397	-7739	0606-	-10450	-11545	-11545	-11820	-13039	-13201	-13201	-14691	-16191	00//T-	17677	-20/45 	007171
BY VALMONT INDUSTRIES	and Moments for Po	ICE + WIND	Z	(in-kips)	7	24	24	121	611	1011	1011	9	1 1 1 1	1695	1924	2542	2542	2750	3798	4645	4645	4909	5703	5703	6235	6925	30	7305	7623	9223	0	5	43/59	13759	14086	15539	15732	15/32	2 0	``	41044	5 5	1 1	
MIAV VALM	Forces and M	Loading Case	Dist. From	(ft)	149.00	145.00	145.00	144.00	139.00	135.00	135.00	134.00	9	130.50	129.00	125.00	125.00	124.00	119.00	115.00	115.00	114.00		111.00	109.00	106.42	105.00	105.00	104.00	99.00	94.00	89.00	00.60	85.00	. ı	ņ			. c	, 0		9 0	, r)

DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR:

Force

	Axial (1bs)	39063	40961	4275	43058	44842	46465	48129	49832	51576	53359	55182	57034	1 6
	Resultant Shear Ab (lbs) (1	39721	39924	40093	40140	40357	40565	40765	40969	41176	41387	41602	41836) I
	Shear Y-Dir. (lbs)	30428	30583	30713	30749	30915	31075	31228	31384	31543	31704	31869	32048	1 0 0 0 0
me	Shear X-Dir. (1bs)	25532	25662	25771	25802	25941	26075	26203	26334	26468	26603	26741	26891	19076
oordinate syst	Torsion (in-kips)	0	0	0	0	0	0	0	0	0	0	0	0	c
rore in the bocal Element Coordinate System	Resultant Mx & My (in-kips)	32989	34663	36065	37069	39489	41921	44366	46823	49292	51774	54269	56776	58792
סדב דוו רווב דס	My (in-kips)	-21205	-22281	-23182	-23828	-25383	-26947	-28518	-30097	-31684	-33280	-34883	-36495	-37791
707	: ICE + WIND MX (in-kips)	25271	26554	27627	28397	30250	32114	33986	35868	37760	39661	41572	43493	45037
	Loading Case ICE + WIND Dist. From Mx Base Mx (ft) (in-kips)	52.50	49.00	46.08	44.00	39.00	34.00	29.00	24.00	19.00	14.00	00.6	4.00	0.00

BY VALMONT INDUSTRIES FOR

Deflections and Stresses for Pole

Loading Case ICE + WIND

*** Deflections and Stresses ***

99.90 99.90 17.28 16.98 4.61 3.12 3.08 2.75 2.75 2.74 2.51 2.08 2.00 1.96 1.96 1.41 1.41 1.40 1.35 1.69 1.69 1.59 1.55 1.51 1.27 1.27 1.20 Allowable Allowable Allowable Divided by Stress Combined 1.28 1.28 1.28 1.24 1.20 1.20 1.17 1.11 51.99 0.17 0.52 3.01 3.06 11.28 16.65 16.90 25.08 18.95 20.73 24.94 25.11 26.54 32.82 36.94 37.10 38.42 42.05 29.33 30.84 32.60 33.49 33.59 34.41 38.02 40.96 44.97 40.35 40.66 41.90 42.04 42.06 43.45 43.45 44.56 46.16 Applied Combined Stress (ksi) 0.06 0.09 1.71 1.70 1.62 1.57 2.35 2.35 2.35 1.70 1.68 1.68 2.17 2.17 2.07 2.07 2.49 2.45 Applied Shear Stress (ksi) 1.64 1.61 1.58 1.58 1.84 1.77 1.77 1.71 Torsion Stress (ksi) Applied Applied Axial Stress (ksi) 0.01 0.03 0.49 0.48 0.47 0.72 0.72 0.53 0.53 0.53 0.70 0.70 0.69 0.68 0.83 0.56 0.57 0.57 0.57 0.67 0.66 0.66 0.57 0.58 0.59 0.59 0.61 0.61 0.61 0.61 0.16 0.49 0.49 0.49 10.80 16.18 16.18 16.18 16.18 18.41 20.20 24.41 24.41 25.84 32.13 36.27 36.27 41.22 28.77 30.27 32.03 32.92 32.92 33.74 33.74 40.30 44.32 339.78 41.31 41.45 41.45 441.45 442.84 443.95 44.84 45.55 Applied Bending Stress (ksi) Defl.
Z-Dir Rotation
(in) (deg.) 6.26 6.26 6.26 6.25 6.18 6.07 6.07 5.90 5.90 5.84 5.68 5.68 5.64 5.17 5.117 4.93 (deg.) Resultant X & Y (in) 98.8 93.5 93.5 92.2 85.7 86.6 779.3 75.0 68.3 68.3 68.3 67.1 61.4 61.4 56.9 55.9 29.4 255.5 255.5 255.1 221.7 118.7 113.4 Defl. 75.7 71.7 71.7 70.7 65.7 61.7 61.7 40.4 38.3 38.8 35.8 35.0 35.0 4.1 24.9 22.5 Defl. Y-Dir (in) 63.5 60.1 60.1 559.3 551.8 51.8 48.2 Defl. X-Dir (in) 18.9 116.1 116.1 116.1 116.1 110.2 110.2 1.0 1.0 1.0 149.00 145.00 145.00 139.00 135.00 135.00 135.00 130.50 129.00 125.00 125.00 124.00 119.00 115.00 1115.00 1111.00 109.00 106.42 105.00 105.00 104.00 99.00 94.00 85.00 85.00 84.00 79.58 79.00 74.00 69.00 64.00 59.00 Distance Base (ft)

ដ MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER,

DATE 11/13/2015 Fuse 1.13.0.0 11.20 Allowable Divided by Stress Combined 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 Applied Combined 443.01 443.01 443.16 443.24 443.38 443.45 443.45 443.40 443.31 443.03 442.68 46.84 Stress (ksi) Applied Shear Stress (ksi) *** Deflections and Stresses *** Applied Torsion Stress (ksi) 0.55 0.56 0.58 0.59 0.59 0.59 0.60 0.60 0.61 0.61 0.61 Applied Axial Stress (ksi) 42.23 42.44 42.58 42.66 42.80 42.86 42.86 42.86 42.86 42.86 42.86 42.87 42.81 42.71 42.71 42.71 42.58 46.23 Applied Bending Stress (ksi) Defl. Z-Dir Rotation 1.99 1.84 1.72 1.63 1.03 1.03 1.03 1.03 1.03 0.65 0.30 0.30 (deg.) (in) Resultant X & Y (in) FOR: Deflections and Stresses for Pole Defl. BY VALMONT INDUSTRIES 8.0 Defl. Y-Dir (in) Loading Case ICE + WIND 6.7 Defl. X-Dir (in) 552.50 449.00 446.08 339.00 334.00 229.00 24.00 119.00 9.00 9.00 9.00 Distance From Base (ft)

DATE 11/13/2015 Fuse 1.13.0.0

Forces and Moments for Pole in the Local Element Coordinate System

FOR:

	06	253	09	32	r.	401	542	593	ξ.	89	73	13	33	12	0,1	6	00	9,	919	9:	d	52	4.	6	7.	2	9	8	ᅼ	0	13	2	9	7	7	Ħ	4	런	4	مر
Axial (1bs)	0.	22	3950	3992	421	44(654	625	6765	6768	6873	7151	9483	9561	9940	10249	12590	12676	1291	12926	13341	13885	14064	16409	16547	17222	1792	1865	19251	19260	1955	21062	2116	2184	22782	23751	24754	2575	2685	27176
Resultant Shear (1bs)	96	172	3378	3397	3496	3582	5335	5354	5433	5429	5461	5558	7413	7430	7544	7649	9452	9470	9552	9542	9536	9670	9711	11466	11481	11604	11730	11860	11987	11972	11992	12136	12155	12687	12817	94	308	13212	13355	13406
Shear Y-Dir. (lbs)	74	132	2588	2603	2678	2744	4087	4102	4162	4159	4183	4258	5679	5695	5779	5860	7241	7255	7317	7309	7351	7407	7439	8783	8795	8889	8982	8	9183	9171	9187	9297	9311	9718	9819	9919	10020	10121	10231	10269
Shear X-Dir. (lbs)	62	110	2171	2184	2247	2302	3430	3442	3492	3490	3510	3573	4765	4776	4849	4917	9209	6087	6140	6133	6168	6216	6242	7370	7380	7459	7540	7623	7705	7696	7709	7801	7813	8155	8239	8323	8408	8492	8585	8617
Torsion (in-kips)	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	O	0	0	0	0	0	0	0	0	0	0	0
Resultant Mx & My (in-kips)	64	σ	6	49	256	426	426	490	717	717	815	1079	1079	1168	1618	1983	1983	60	2439	2439	2668	2967	3132	3132	3270	3963	4664	5372	5945	5945	6088	6728	6813	6813	7579	8353	9135	9925	10723	10964
My (in-kips)	T-	9-	9-	-32	-165	-274	-274	-315	-461	-461	-524	-694	-694	-751	-1040	-1274	-1274	-1347	-1568	-1568	-1715	-1907	-2013	-2013	-2102	-2547	-2998	-3453	-3821	-3821	-3914	-4325	-4379	-4379	-4872	-5369	-5872	-6380	-6892	-7047
e T+S Mx (in-kips)	13	7	7	38	196	326	326	376	549	549	624	827	827	895	1239	1519	1519	1606	1868	1868	2044	2273	2399	2399	2505	3036	3573	디	4554	4554	4664	5154	5219	5219	5806	63399	6998	60	8214	8399
Loading Case T+S Dist. From Base (ft) (in-	149.00	145.00	145.00	144.00	139.00	135.00	135.00	134.00	130.50	130.50	129.00	125.00	125.00	124.00	119.00	115.00	115.00	114.00	i	111.00	109.00	106.42	105.00	105.00	104.00	99.00	94.00	89.00	85.00	85.00	84.00	79.58	79.00	79.00	74.00	69.00	64.00	29.00	54.00	52.50

DA	Fu													
TOWER, CT		Axial (1bs)	27185	30198	30737	32046	33393	34779	36203	37665	39166	40705	42281	43559
ING-BLACKROCK		Resultant Shear (1bs)	13388	13578	13621	13747	13870	13990	14112	14237	14364	14494	14629	14770
, SITE: REDD)		Shear Y-Dir. (lbs)	10256	10402	10434	10531	10625	10717	10811	10906	11004	11103	11207	11314
ENT 150' POLE	E	Shear X-Dir. (lbs)	8606	8728	8755	8836	8915	8993	9071	9152	9233	9316	9403	9494
MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER,	in the Local Element Coordinate System	Torsion (in-kips)	00	. 0	0	0	0	0	0	0	0	0	0	0
MESSAGE	ocal Element C	Resultant Mx & My (in-kips)	10964	12003	12343	13165	13995	14832	15676	16528	17387	18254	19129	19834
S FOR:	Pole in the Lo	My (in-kips)	-7047	-7715	-7934	-8462	9668-	-9534	-10076	-10624	-11176	-11733	-12296	-12749
BY VALMONT INDUSTRIES	oments for Po	T+S MX (in-kips)	8399	9195	9455	10085	10721	11362	12009	12661	13319	13983	14654	15194
BY VALM	Forces and Moments for	Loading Case T+S Dist. From Base [ft] (in-1	52.50	46.08	44.00	39.00	34.00	29.00	24.00	19.00	14.00	9.00	4.00	0.00

BY VALMONT INDUSTRIES FO

Deflections and Stresses for Pole

5.31 4.65 4.65 4.62 3.77 3.57 3.44 99.90 99.90 51.64 47.69 13.73 9.39 9.14 8.21 6.22 Allowable Divided by Stress Combined 51.99 51.99 51.99 51.99 51.99 51.99 51.99 Stress (ksi) 551.99 551.99 551.99 551.99 551.99 551.99 551.99 551.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 51.99 0.05 0.16 1.01 1.01 3.79 5.54 6.33 8.33 6.31 6.39 8.28 8.28 8.39 112.30 112.30 112.40 9.79 10.29 10.89 111.25 111.52 112.73 12.73 13.73 14.55 13.55 13.66 14.15 14.15 14.62 14.99 15.30 15.30 Applied Combined Stress 0.02 0.03 0.55 0.55 0.53 0.51 0.76 0.76 0.55 0.55 0.53 0.71 0.68 0.66 0.82 0.82 0.54 0.53 0.53 0.53 0.62 0.61 0.54 0.54 Applied Shear Stress (ksi) *** Deflections and Stresses *** Applied Torsion Stress (ksi) 00.38 00.38 00.44 00.44.0 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.42 00.44 00.4 0.01 0.02 0.32 0.32 0.31 0.47 0.46 0.37 0.337 0.388 0.388 0.388 0.444 0.444 0.444 0.444 0.444 Applied Axial Stress (ksi) 13.16 13.27 13.70 13.75 13.75 14.21 14.88 14.88 15.12 0.04 0.14 0.14 0.76 3.47 5.22 5.22 5.87 7.90 5.97 6.55 7.94 7.94 10.49 11.86 11.86 11.86 11.30 9.42 9.92 10.51 10.81 10.81 11.08 12.30 13.29 14.11 Applied Bending Stress (ksi) 1.64 1.53 1.53 1.53 1.53 1.53 1.53 1.27 1.20 1.18 1.11 1.11 1.10 1.01 0.93 0.85 2.07 2.07 2.07 2.07 2.05 2.01 2.01 2.00 1.95 1.95 1.94 1.88 1.88 1.87 1.72 1.72 1.72 1.72 Rotation Z-Dir (in) Defl. Defl.
Resultant
X & Y
(in) 332.9 31.1 30.7 28.0 26.9 26.9 25.9 25.9 25.9 225.0 224.4 222.8 222.8 222.8 4.20.1 190.0 1190.0 17.6 16.9 16.9 116.9 115.6 115.6 112.3 10.9 9.8 8 6 N 4 4 W W W W V 255.2 23.9 23.9 23.9 221.9 20.6 20.6 19.3 19.3 19.1 17.4 17.4 17.4 17.1 15.7 14.6 14.6 13.5 113.5 1123.0 1112.3 111.9 10.7 10.7 10.5 7 Defl. Y-Dir (in) 21.1 20.0 20.0 20.0 119.7 118.4 117.3 117.3 116.1 115.7 114.6 114.6 113.2 112.2 112.2 112.3 111.3 110.9 110.9 110.0 10.0 10.0 7.9 7.9 Defl. X-Dir (in) Loading Case T+S 1111.00 109.00 106.42 105.00 105.00 99.00 94.00 89.00 85.00 149.00 145.00 145.00 139.00 139.00 135.00 135.00 130.50 129.00 125.00 125.00 1124.00 1115.00 115.00 1115.00 85.00 84.00 79.58 79.00 74.00 69.00 64.00 54.00 Distance From Base (ft)

FOR: BY VALMONT INDUSTRIES

			!					THE STATE OF THE PARTY OF THE PROPERTY OF THE	Part Coard	THEORY	Owak, CI	Fuse 1.13.0.0
ctio	Deflections and Stresses for Pol	tresses	for Pole									
ing Ca	Loading Case T+S					A * *	eflections	*** Deflections and Stresses ***	* * *			
Distance From Base (ft)	Defl. X-Dir (in)	Defl. Y-Dir (in)	Defl. Resultant X & Y (in)	Defl. Z-Dir (in)	Rotation (deg.)	Applied Bending Stress (ksi)	Applied Axial Stress (ksi)	Applied Torsion Stress (ksi)	Applied Shear Stress (ksi)	Applied Combined Stress (ksi)	Allowable Stress (ksi)	Allowable Allowable Divided by Stress Combined (ksi)
52.50	2.3	2.7	3.5	0.0	0.67	15.36	0.43	00.00	0.42	15.79	51.99	3.29
52.50	2.3	2.7		0.0	0.67	14.03	0.38	00.00	0.38	14.42	51.99	3.61
49.00	1.9	2.3	3.0	0.0	0.62	14.12	0.40	00.0	0.37	14.51	51.99	3.58
46.08	1.7	2.0		0.0	0.58	14.17	0.41	0.00	0.37	14.58	51.99	3.57
44.00	1.6	1.9		0.0	0.55	14.21	0.41	00.00	0.37	14.62	51.99	3.56
39.00	1.2	1.4		0.0	0.48	14.27	0.42	00.0	0.36	14.68	51.99	3.54
1.00	٥.	1.1		0.0	0.41	14.31	0.42	00.0	0.35	14.73	51.99	3.53
9.00	0.7	0.8		0.0	0.35	14.33	0.43	0.00	0.34	14.75	51.99	3.52
1.00	0.4	0.5		0.0	0.28	14.33	0.43	00.0	0.34	14.76	51.99	3.52
19.00	0.3	0.3		0.0	0.22	14.32	0.44	00.00	0.33	14.76	51.99	3.52
14.00	0.1	0.2		0.0	0.16	14.30	0.44	00.0	0.33	14.74	51.99	3.53
9.00	0.1	0.1		0.0	0.10	14.27	0.45	00.00	0.32	14.72	51.99	3.53
4.00	0.0	0.0		0.0	0.04	14.23	0.45	00.0	0.32	14.68	51.99	3.54
00.	0.0	0.0		0.0	00.0	14.19	0.46	00.0	0.31	14.65	51.99	3.55

MINIMUM DEFLECTION RATIO // DEFLECTION LIMIT / DEFLECTION // IS

FLANGE ANALYSIS Version IMPAX-16.11.2015

FLANGE FOR THE D - E JOINT : CONTROLLING LOAD CASE ICE + WIND

Input Data)) 1 1 1 1)) 	1	Results			1
Applied Reactions					Bolts			
Resultant Moment		Ð	2,212	in-kips	Maximum Bolt Axial Force=	ial Force=	39,707	lbs
Torsion		tŧ	0	in-kips	Maximum Bolt Shear	ear =	2,080	lbs
Resultant Shear		II	16,636	lbs	Allowable Axial Stress	Stress =	85	ksi
Axial		li	-10,471	lbs	Combined Safety Factor	Factor =	1.04	
Bolts					Flange			
Number of Bolts		Ð	80		Weight	11	274	lbs
Bolt Diameter		11	1.00	in	Controlling Stress	655	Shear	
Bolt Material		II	A325		Minimum Safety Factor	Factor =	3.57	
Bolt Circle		u	28.81	in	Bending Safety Factor	Factor =	6.71	
					Shear Safety Factor Bearing Safety Factor	ctor =	3.57	
Flange					7			
Outside Diameter		11	31.31	in				
Thickness		H	2.000	ri				
Yield Strength		H	20	ksi				
Tensile Strength		H	65	ksi				
Valmont Material S	Spec.	II	3-56					
Tube								
No. of sides		Ħ	18					
Design Diameter		8	25.044	in				
Sect.	Dia	11	25.098	in				
Detailed "E" Sect.	Dia	n	24.990	in				
Thickness		11	0.2500	in				
Yield		н	65	ksi				
			* * *	*** BOLT COORDINATES ***	4TES ***			
BOLT NO. X-COORD	ORD C	¥-0	Y-COORD	4	BOLT NO.	X-COORD	Y-COORD	
, t 14.	14.40	- ,	0.00	k 4	71	70.TR	10.18	
· o	2	4	4.4C	•				

DATE 11/13/2015 Fuse 1.13.0.0 MESSAGE CENTER MANAGEMENT 150' POLE, SITE: REDDING-BLACKROCK TOWER, CT FOR: BY VALMONT INDUSTRIES

*** ANCHOR BOLT CHARACTERISTICS GOVERNED BY LOADING CASE ICE ***

THREAD SIZE	4.5-UNC-2A	CONFIGURATION OF BOTTOM END OF ANCHOR BOLT THREADED WITH HEAVY HEX HEAD NUT		TENSION-LB MAX FORCE-LB 35034 39910 99937 104817 137413 142289			SIDE LENGTH (IN.)	13.00	TOTAL MOMENT ALONG FAIL LINE (INLB.)	3084508			**************************************
GALVANIZED LENGTH (IN.)	66.00	вотто тнкварвр		Y-COORD MAX TEN 8,758 35 23.928 99 32.687 137		* *	RAW MATERIAL WEIGHT (LB.)	5466	EFFECTIVE LENGTH (IN.)	60.77	MAX. VERTICAL SHEAR STRESS (PSI)	7418	
PROJECTION LENGTH (IN.)	12.50	SAFETY FACTOR 1.32		O. X-COORD 32.687 23.928 8.758	73.68 IN.	ING CASE ICE	ACTUAL WEIGHT (LB.)	3308	TOTAL LENGTH OF FAIL MODE LINE (IN.)	74.69	MAX. SHE)T ***********
SHIPPED HT AS .)	2641 BOLTS, TEMPLATES	WABLE STRESS RESS AREA SI) (SQ. IN.) 59985 3.250	COORDINATES AND FORCES ***	MAX FORCE-LB * BOLT NO. 2438 * 2 74828 * 4 127825 * 6	TEMPLATE DIAMETER =	*** BASE PLATE CHARACTERISTICS GOVERNED BY LOADING CASE ICE	THICKNESS (IN.)	3.5000	CRITICAL TOT FAILURE MODE FF	rt	ALLOWABLE STRESS (PSI)	50010	SYSTEM ************************************
LENGTH WEIGHT (IN.) (LB.)	66 20	MAXIMUM ALLOWABLE STRESS STRESS (PSI) (PSI) 45308 59985	*** BOLT COOR	TENSION-LB - 2438 69952 122950 142346	IN.	E PLATE CHARACTERI	OVERALL WIDTH (IN.)	74.82	POLE DIAM. (MAJOR DIAM.) (IN.)	60.25	STRESS STRESS (PSI) (24861	GLOBAL COORDINATE S WIND ICE 43839 45037 - 36785 - 37791 42600 42078 44070 58507
DIAMETER (IN.)	2.250	MAXIMUM BOLT FORCE (LB.) 147222		X-COORD Y-COORD MAX 33.840 0.00 29.306 16.920 16.920 29.306 0.00 33.840	BOLT CIRCLE = 67.68	*** BAS	OVERALL LENGTH (IN.)	73.68			STEEL BE SPECIF. OTHER	A572	BASE IN THE ICATION IN-KIP) IN-KIP)
NUMBER OF BOLTS	24	STEEL SPECIF. A615		BOLT MO. 3	MAX. BOLI		DRAWING NUMBER	SD18-98	TOP WIDTH (IN.)	13.00	SI SI VALMONT	856	** LOADS AT POLE LOADING CASE IDENTIF MOMENT ABT. X-AXIS (MOMENT ABT. Y-AXIS (SHEAR FORCE (LB.) VERTICAL FORCE (LB.)