### CUDDY& FEDER

445 Hamilton Avenue, 14th Floor White Plains, New York 10601 Tel 914.761.1300 Fax 914.761.5372 www.cuddyfeder.com

May 9, 2013

#### **BY EMAIL & FEDEX**

Robert Stein, Chairman and Members of the Connecticut Siting Council 10 Franklin Square New Britain, CT 06051 Email: siting.council@ct.gov

Re: Docket 429 New Cingular Wireless (AT&T) Application for Certificate of Environmental <u>Compatibility and Public Need in Willington, Connecticut</u>

Dear Chairman Stein and Members of the Siting Council:

On behalf of New Cingular Wireless ("AT&T") please accept for review and Council approval this Development and Management Plan ("D&M Plan") filing for the captioned Facility as approved in Docket 429.

#### Tower, Compound & Other Equipment

Enclosed are fifteen (15) sets of 11" x 17" signed and stamped drawings prepared by Clough Harbour and Associates ("CHA") dated April 22, 2013 ("D&M Plan") being filed in accordance with the Council's Decision and Order dated February 7, 2013. Two full-sized sets of the construction drawings will follow to the Council under separate cover. The D&M Plan incorporates a 160' monopole as provided for in the Siting Council's Order No. 1 in this Docket. AT&T will mount twelve (12) panel antennas on a low profile platform at a centerline height of 156' AGL. The D&M Plan also includes construction plans for the site clearing, drainage, and erosion and sedimentation control measures consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control as amended.

Attached to this letter please find a geotechnical study, structural design drawings for the tower and foundation, a drainage report ("Drainage Report") for the approved access drive (without Appendices) as well as a sample Erosion and Sedimentation Control Site Inspection Form to be used by AT&T's consultant APT in keeping with the public water supply protective measures developed for this site.<sup>1</sup> Finally, specifications for AT&T's antennas and backup emergency generator are also included.

Due to size considerations, four copies of the full structural and foundation calculations reports as well as the Drainage report *with* Appendices are being bulk filed with the Council. Should the Council or staff require additional copies please do not hesitate to contact me.

<sup>&</sup>lt;sup>1</sup> See Sheet CO5 of the D&M Plan, "Compound Plan & Site Notes".



May 9, 2013 Docket 429 AT&T Page 2

#### **Required Notifications**

In accordance with the provisions of RCSA Section 16-50j-77, AT&T hereby notifies the Council of its intention to begin site work after Council approval of the D&M Plan. Construction of the tower and other site improvements will commence upon issuance of a local building permit and after a pre-construction meeting.

The supervisor for all construction related matters on this project is Bryon Morawski of SAI. Mr. Morawski is located at 500 Enterprise Drive, Suite 3A, Rocky Hill, CT 06067 and can be reached by telephone at (860) 513-7223.

We respectfully request that this matter be included on the Council's next available agenda for review and approval.

Thank you for your consideration of the enclosed.

Very truly yours,

ML 1

Daniel M. Laub

Enclosures

cc: Robert and Marissa Golden, Intervenors Hon. Christina B. Mailhos, Willington First Selectman Lawrence C. Becker, Property Owner Michele Briggs, AT&T David Vivian, SAI Dean Gustafson, APT Paul Lusitani, CHA Christopher B. Fisher, Esq.



May 9, 2013 Docket 429 AT&T Page 3

#### CERTIFICATE OF SERVICE

I hereby certify that on this day, a copy of the foregoing was sent electronically and by overnight delivery to the Connecticut Siting Council with copy to:

Robert and Marissa Golden 52 Old South Willington Road Willington, CT 06279 marissakellner@aol.com

Lawrence C. Becker PO Box 535 Willington, CT 06279 beckerace@aol.com

Dated: May <u>9774</u>, 2013

M. ht

Daniel M. Laub

#### ATTACHMENT 1

#### DR. CLARENCE WELTI, P.E., P.C.

GEOTECHNICAL ENGINEERING

227 Williams Street · P.O. Box 397 Glastonbury, CT 06033-0397

(860) 633-4623 / FAX (860) 657-2514

May 7, 2013

Mr. David Vivian New Cingular Wireless PCS, LLC 500 Enterprise Drive, Suite 3A Rocky Hill, CT 06067

#### Re: Geotechnical Study for Proposed AT&T Tower Site No. SR1107 Tolland Turnpike, Willington, CT

Dear Mr. Vivian:

1.0 Herewith are the data from the test boring and probes taken at the above referenced site. One boring was drilled at the center of the proposed tower. Weathered rock was encountered at 3 feet and hard bedrock at 5 feet below the existing grade. The boring was augered to 5 feet and bedrock was the cored from 5 to 10 feet. Three probes were drilled to auger refusal at 2.5 to 5.5 feet below the existing grades. The boring and probe locations are shown on the attached plan. *The boring and probe were drilled by Clarence Welti Associates, Inc. and sampling was conducted by this firm solely to obtain indications of subsurface conditions as part of a geotechnical exploration program. No services were performed to evaluate subsurface environmental conditions.* 

2.0 The Subject Project will include the construction of a 160 foot monopole type tower.

3.0 The Soil/Rock Cross Section from the boring and probes was generally as follows:

Topsoil to about 6"

Fine to medium SAND, some Silt, little Gravel to the top of rock at 2.5 to 5.5 feet below the existing grades

Locally; Weathered Rock to 0 to 2 feet below the top of rock

Bedrock; Gneiss and Schist - The rock core taken from 5.0 to 10.0 feet had an RQD value of 40%. The bedrock has a dip of about  $60^{\circ}$  to the west.

3.1 The Ground Water Table was not encountered above the bedrock.

4.0 In general the criteria for tower support is that the foundation capacity would exceed the loads, which might collapse the tower. Movements from strains in the soils should be limited to differential settlement (or lateral movements of less than <sup>1</sup>/<sub>2</sub>'').

5.0 The foundation system for the proposed towers would be as follows:

### 1. A large mat, placed sufficiently deep to prevent overturning by gravity resistance of the pad. This may either require rock removal or construction above grade.

### 2. A mat with anchorage into the bedrock to provide the required resistance to overturning.

5.1.1 In alternate (1) the mat would provide the required weight for resistance to over turning. The mat could be placed on a prepared blasted rock surface, or on hard bedrock. The bottom of the mat should be at least 3.5 feet below finished grades for frost protection. The allowable loading directly on the hard bedrock would be 6 Tons/sf. If bedrock removal is required, the pad area could be over blasted by 1 to 2 feet and the area could be leveled with a minimum 8" layer of 3/8" crushed stone, after removal of any large and loose pieces of rock. The allowable loading on the crushed stone over a blasted rock surface or on weathered/fractured rock can be 3 Tons/sf.

5.1.2 Regarding alternate (2) the same criteria for loading will apply. The resistance to uplift and overturning would be provided by rock anchors tied into the foundation. The allowable bond between the cement grout and the bedrock would be 50 psi, starting from 4 feet into the bedrock. The minimum anchor depth shall be 15 feet. For global stability the volume of rock should be that in truncated cone, 5 feet in diameter at the base and extending to the surface at 30° from axis of tie down. The weight of the rock is 165 pcf. Where rock anchors are used the foundation should be directly on the clean bedrock surface.

Parameter	Value
Allowable Loading on Clean Sound Bedrock Surface	6 Tons/sf
Allowable Loading on Crushed Stone over Blasted Rock Surface	3 Tons/sf
Tie Downs	
Bond Rock to Cement Grout	50 psi
Pull Out Angle (from Vertical)	30°

5.2 Summary of design parameters:

5.3 It should be noted that the rock surface may be irregular. Concrete fill (a sub-footing) may be required, when the rock is exposed.

6.0 This report has been prepared for specific a application to the subject project in accordance with generally accepted soil and foundation engineering practices. No other warranty, express or implied, is made. In the event that any changes in the nature, design and location of structures are planned, the conclusions and recommendations contained in this report should not be considered valid unless the changes are reviewed and conclusions of this report modified or verified in writing.

The analyses and recommendations submitted in this report are based in part upon data obtained from referenced explorations. The extent of variations between explorations may not become evident until construction. If variations then appear evident, it will be necessary to re-evaluate the recommendations of this report.

Dr. Clarence Welti, P.E., P.C., should perform a general review of the final design and specifications in order that geotechnical design recommendations may be properly interpreted and implemented as they were intended.

If you have any questions please call me.

Very truly yours,

May Lille

Max Welti, P. E.



CLARENCE WELTI ASSOC., INC.				NC.	CLIENT				PROJECT NAME			
P.O. BOX 397								LOCATION				
GLASTONBURY, CONN 06033			SAI COMMUNICATION, INC.			IMUNICATION, INC.	TOLLAND TURNPIKE, WILLINGTON, CT					
		AUGER	CASING	SAMP	LER	CORE BAR. OFFSET		OFFSET	SURFACE ELEV. HOLE	NO. B-1		
ТҮРЕ		HSA		SS	;	NQ		LINE & STA.	GROUND WATER OBSERVATIONS	START	0/7/10	
SIZE I.I	).	3.75"		1.37	5"	2.0'	,	N. COORDINATE	AT NONE FT. AFTER O HOURS	DATE	2/7/13	
HAMM	ER WT.			1401	bs			F COORDINATE	AT FT. AFTER HOURS	FINISH	2/7/13	
HAMM	ER FALL			30	"					DATE		
DEPTH	NO	SAM	PLE		A			STRATUN	A DESCRIPTION + REMARKS		ELEV.	
0	1	16-10-5-5	0.00'	-2.00'			BR		SILT, LITTLE GRAVEL			
						-						
	2	16-60	2.00'-	-3.00'								
							WE	EATHERED ROCK		3.0	<u>&gt;</u>	
						-						
5 -							со	RED BEDROCK - GNEISS A	AND SCHIST	5.0	<u>&gt;</u>	
						-	RU	IN #1 5 0' - 10 0' BECO	VERED 59" BOD = 40%			
								11 / 10.0 10.0 NEOO				
						-						
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1.5												
15-												
20 -												
20 7												
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25 -												
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LEGE	LEGEND: COL. A:							DRILLER: BREWER INSPECTOR:				
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1 KOA OKTIONO USED. INKCL-V-10/0 LITILE-10-20/0 SUME-20-3370 AND-33-3070							SHEEL   OF   HOLE NO	J.	D-1			

CLARENCE WELTI ASSOC., INC.			CLIENT			PROJECT NAME AT&T SITE # SR1107								
GLASTONBURY, CONN 06033						LOCATION				0.7				
		AUGED	CASING	SAMPLE			OFFSET	ION, INC.	SURF	ACE ELEV.	URNPIKE,	WILLING		, СТ
TVDE		SOUD	CASINO	SAWIF LE		LE DAK.	I DIE 8 01	E A			HOLE	: NO.	PRC	DBES
SIZELL		4.0"					LINE & SI	TA.	GRC	UND WATER OBS	ERVATIONS	START DATE	2/7	//13
HAMM	FR WT	+.0					N. COORE	DINATE	AT N	ONE FT. AFTER	0 HOURS			
HAMM	ER FALL						E. COORD	DINATE	AT	FT. AFTER	HOURS	DATE	2/7	//13
DEDTU		SAM	PLE				1	STRATUN	1 DESCR	IPTION			ľ	
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						UTEEL		TIOLE IN	. r		С- 			

#### ATTACHMENT 2



Foundation Notes

1. This foundation has been designed for the following reactions.

Shear:	54.2 kips
Moment:	6728.7 ft-kips
Weight:	68.1 kips

2. Design based on geotechnical report dated 2/15/2013 by Clarence Welti Associates, Inc.; Project No. AT&T Site # SR1107.

3. A field inspection shall be performed in order to verify that the actual site soil parameters meet or exceed the assumed soil parameters and that the depth of standard foundations are adequate based on the frost penetration and groundwater depth. Local frost depth must be no deeper than the bottom of the base foundation.

4. Reinforcement shall be deformed and conform to the requirements of ASTM A615 Grade 60 unless otherwise noted. Splices in reinforcement shall not be allowed unless otherwise noted.

5. Welding is prohibited on reinforcing steel and anchorage.

6. Structural backfill placed below pad must be compacted in 8" loose lifts to a 97% of maximum dry density at optimum moisture content in accordance with ASTM D698. Backfill must be clean and free of organic and frozen soils and foreign materials.

7. Backfill above foundation should be compacted to 95% of maximum dry density at water content within 2 percent of optimum. Backfill must be clean and free of organic and frozen soils and foreign materials.

8. Foundation designs assume level ground at tower site.

9. Loose material shall be removed from bottom of excavation prior to concrete placement.

10. Concrete cover from exposed surface of concrete to surface of reinforcement shall not be less than 3".

11. Concrete and reinforcement installation must conform to ACI 318, "Building Code Requirements for Structual Concrete."

12. Concrete shall develop a minimum compressive strength of 4000 psi in 28 days.

13. Concrete shall be placed as soon as practical after excavating to avoid disturbance of bearing and side wall surfaces.

14. Concrete contractor shall be responsible for properly aligning anchor bolts and materials before and after placing concrete, regardless of whether an anchor bolt template is provided.

15. Positive drainage shall be maintained during construction and throughout the life of the facility to minimize the potential for surface water infiltration.

16. The sub-grade, if practical, should be proof-rolled with vibratory compaction prior to casting foundation or placing structural fill.

17. Overexcavation of unsuitable soils for compacted backfill placement below footings should extend laterally beyond all edges of the footings at least 12 inches per foot of overexcavation depth below footing base elevation.

18. It shall be the contractor's responsibility to locate and prevent damage to any existing underground utilities, foundations or other buried objects that might be damaged or interfered with during construction of the foundation.

19. It is permissible to utilize a cold joint during construction of a pier and pad type foundation. The cold joint must be located at the interface of the piers with the pad, and contractor shall use a bonding agent suitable for cold joints.

20. Foundation design assumes an ultimate bearing capacity value of 12,000 psf.

21. Weathered rock was encountered about 3 feet bgs and hard Gneiss/Schist bedrock was encountered about 5 feet bgs in the test boring. Difficult excavation should be anticipated and the contract prepared to remove such materials. Ripping, jack-hammering or other mechanical means will be required to advance excavation into bedrock. The depth to rock material will vary across the foundation of the foundation of the second seco

22. Design assumes entire footing is bearing on bedrock or properly placed concrete/stone structural fill.

23. In preparing the rock bearing surface for the footing; loose or soft material and debris should be removed, any cracks or seams in the rock should be filled with lean concrete or grout and the rock should be leveled. A level bearing surface may be established with lean concrete or 3/8" crushed stone.

24. Construction and installation methods shall be in accordance with the geotechnical report.

				COPYRIGHT NOTICE:	ORIG DATE: 4/26/2013	DWG
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ctor should be ion footprint.	BO STONAL	APR 29 2013
k surface	<u>TITLE:</u> SAI Communications NTP 55'' X 160'	
NO: 198289	Tolland Co., CT	211 W. Washington St., Suite 2000 South Bend, IN 46601-1705
T: 2 OF 2		Bus: (574)288-3632 Fax: (574)288-5860



iximum	Minimum
stance	Distance
о Тор	to Top
acking	Jacking
ut (in)	Nut (in)
3 1/16	8 3/8
3 7/8	7 3/16
11/16	6 7/8

#### Portholes

Elevation (ft)	Qty	Size (in)	Azimuth (deg)
152	3	6 x 12	60, 180, 300
152	3	8 x 16	60, 180, 300
142	3	6 x 12	60, 180, 300
132	3	6 x 12	60, 180, 300
122	3	6 x 12	60, 180, 300
7.5	1	9 x 24	0
7.5	1	10 x 30	90
7.5	1	9 x 24	180
7.5	1	9 x 24	270
3.5	1	9 x 24	0

#### Antenna Loading

	Heiat	nt Otv	Description
	160'	1	6' Lightning Rod
	155	12	SBNH-1D6565C
	155	4	Raycap DC6-48-60-18-8F
	155'	15	Radio Remote Unit (RRU)
	155'	1	Low Profile Platform
	150'	15	RRUS-11
	150'	1	Clamp Ring Assembly
	145'	12	SBNH-1D6565C
	145'	4	Raycap DC6-48-60-18-8F
	145'	15	Radio Remote Unit (RRU)
	145'	1	Low Profile Platform
	140'	15	RRUS-11
	140'	1	Clamp Ring Assembly
	135'	12	SBNH-1D6565C
	135'	4	Raycap DC6-48-60-18-8F
	135'	15	Radio Remote Unit (RRU)
	135'	1	Low Profile Platform
	130'	15	RRUS-11
	130'	1	Clamp Ring Assembly
	125'	12	SBNH-1D6565C
	125'	4	Raycap DC6-48-60-18-8F
125' 125'		15	Radio Remote Unit (RRU)
		1	Low Profile Platform
	120'	15	RRUS-11
	120'	1	Clamp Ring Assembly
REV	BY	DATE	DESCRIPTION
1	BRG	4/24/2013	Bovice tower leading per

#### Feedline Loading

Height	Qty.	Description	N
0' - 155'	8	1/2"	Note:
0' - 155'	36	LDF5-50A (7/8 FOAM)	footuror
0' - 145'	12	LDF7-50A (1-5/8 FOAM)	which c
0' - 135'	12	LDF7-50A (1-5/8 FOAM)	WHICH C
0' - 125'	12	LDF7-50A (1-5/8 FOAM)	



the 0 Degree Azimuth

REV	BY	DATE	DESCRIPTION	COPYRIGHT NOTICE: This drawing is the property of Nello Inc. It is not to be reproduced	ORIG. DATE:	4/24/2013	DWG NO:
1	BRG	4/24/2013	Revise tower loading per ECO3870	copied or traced in whole or in part without our written consent.	DWG. PROG:	v2.05	SHEET:





	PROVIDENTIAL CONNECTION	APR 29 2013
	TITLE: SAI Communications	
	NTP 55" X 160'	N E L L O
198288	Willington/SR1107	211 W. Washington St., Suite 2000
3 OF 4	Tolland Co., CT	South Bend, IN 46601-1705 Bus: (574)288-3632 Fax: (574)288-5860

#### **Tower Notes:**

1. Tower is designed per TIA-222-G, "Structural Standard for Antenna Supporting Structures and Antennas," for the following loading conditions:

100 mph 3-second gust basic wind speed with no ice

40 mph 3-second gust basic wind speed with 1-1/4 inch basic ice thickness

Structure Class: II

Exposure Category: C

Topographic Category: 1

- 2. Tower design loading is assumed to be based on site-specific data and must be verified by others prior to installation.
- 3. Tower design includes the antennas, dishes, and/or lines listed in the appurtenance loading tables on sheet 2.
- 4. Antenna mounting pipes may need to be field cut to match the lengths listed in the appurtenance loading tables on sheet 2.

5. Tower member design does not include stresses due to erection since erection equipment and procedures are unknown. Tower installation shall be performed by competent and qualified erectors in accordance with TIA-222-G and OSHA standards and all applicable building codes.

- 6. Field connections shall be bolted. No field welds shall be allowed unless otherwise noted.
- 7. Structural bolts shall conform to ASTM A325, except for 1/2 inch diameter and smaller bolts, which shall conform to ASTM A449 or SAE J429 Grade 5.
- 8. Structural steel and connection bolts shall be galvanized after fabrication in accordance with TIA-222-G.
- 9. All high strength bolts shall be tightened to a "snug tight" condition as defined in the November 13, 1985, AISC "Specification for Structural Joints Using ASTM A325 or A490 Bolts."
- 10. Tower shall be marked and lighted in conformance with local building codes, FAA regulations, and TIA-222-G.
- 11. Tower shall be grounded in conformance with local building codes and TIA-222-G.
- 12. Allowable tolerance on as-built tower steel height is plus 1% or minus 1/2%.
- 13. Maintenance and inspection shall be performed over the life of the structure in accordance with TIA-222-G.
- 14. Material specifications:

NTP 18-Sided Pole - ASTM A572 Grade 65

Pole Flange - ASTM A572 Grade 50

Pole Porthole Rim - ASTM A572 Grade 65

- 15. A jacking nut is placed near the top of each section which will have another section placed on top. The distance from this top jacking nut to the bottom of the next section must not exceed the value given in
- the column labeled "Maximum Distance to Top Jacking Nut." Jacking may be required to achieve the proper overlap.
- 16. The horizontal distance between the vertical centerlines at any two elevations shall not exceed 0.25 percent of the vertical distance between the two elevations. Measure early in the morning before the sunward side of the pole expands.
- 17. Sections must be erected with the 0 degree azimuth lined up to ensure proper fit.
- 18. Remove anchor bolt template before erecting pole. Non-shrink grout may be placed under base flange after leveling pole. Drain holes must be provided if grouting.

19. Concrete contractor shall be responsible for properly aligning anchor bolts and materials before and after placing concrete, regardless of whether an anchor bolt template is provided.

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REV	ы	DATE	DESCRIPTION	Nello Inc. It is not to be reproduced,			
1	BRG	4/24/2013	Revise tower loading per ECO3870	copied or traced in whole or in part without our written consent.	DWG. PROG:	v2.05	SHEET:



#### ATTACHMENT 3

### SR 1107 Access Road Drainage Report

### SAI Willington Tolland Turnpike Willington, CT 06279

CHA Project Number: 18301.1028.43000

**Prepared for:** SAI Communications 500 Enterprise Drive Rocky Hill, CT 06067

Prepared by:



April 2013

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#### **APPENDICES**

Appendix A –	-	NRCS Hydrologic Soil	Group	Map	&	Descriptions
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- Appendix B Composite Runoff Coefficient Calculations
- Appendix C Time of Concentration Calculations
- Appendix D CulvertMaster Output Data
- Appendix E Culvert Capacity Calculations
- Appendix F Manning's n Calculations
- Appendix G Swale Sizing Calculations
- Appendix H Shear Stress Calculations
- Appendix I Outlet Protection Calculations
- Appendix J Existing DA 2 Calculations

#### **FIGURES**

- Figure 1 USGS Map
- Figure 2 Aerial Map
- Figure 3 Drainage Areas
- Figure 4 Drainage Design
- Figure 5 Drainage Details
- Figure 6 Existing Drainage Area 2

#### 1.0 **INTRODUCTION**

The project site is located on Tolland Turnpike in the town of Willington, CT. The site is located on property owned by Lawrence Becker. The subject parcels are bounded by Tolland Turnpike to the North, residential parcels to the East and West, and a stone quarry and wooded areas to the South. Site access comes from an existing gravel access driveway on Tolland Turnpike.

The proposed work includes the installation of a fenced gravel compound for a telecommunications tower, construction of a gravel access drive to the tower site (910 linear feet), and installation of a stormwater collection system consisting of rock lined drainage swales, and storm drain culverts.

This report addresses the design of drainage swales, and storm drain culverts to protect the access road from washout, safely convey stormwater flows, and protect outfall locations from erosion. This report does not address the design of groundwater controls or slope stabilization, as site geotechnical information was not available at the time of this report.

Refer to the proposed D&M Drawings submission, dated 04-22-13, under a separate cover, for specific site details.

#### 2.0 HYDROLOGIC EVALUATION

#### **Existing Watershed Characteristics**

The Connecticut United States Geological Survey (USGS) Coventry Quandrangle Map indicates that the cellular tower and compound are located on a local high point, along an existing topographic ridge. Topography is varied and includes small topographic ridges, natural swales, flatlands, and wetlands in the surrounding area. Existing topography contributing to site drainage consists of elevations ranging from 777' above mean sea level (AMSL) just south of the proposed cell tower location to 695' AMSL at an existing depression adjacent to Tolland Turnpike on the east side of the existing access drive. Existing slopes vary from flat to very steep ranging (+/- 20%) (See Figure 1 – USGS Map).

Aerial photography and a site field visit indicate that the existing land use at the site consists primarily of forested area, with the exception of a few residential properties along Tolland Turnpike. There is also an existing stone quarry located to the south and west of the project site but it does not contribute to the site drainage areas (See Figure 2 – Aerial Map).

Project site soil characteristics were determined using the United States Department of Agriculture (USDA) Natural Resources Conservation Service (NRCS) Web Soil Survey. The site is comprised entirely of soils belonging to Hydrologic Soil Groups (HSG) B (See Appendix A). Below is a brief description of hydrologic soil group B:

 $Group \ B$  – Soils having a moderate infiltration rate when thoroughly wet. These consist chiefly of moderately deep or deep, moderately well drained or well drained soils that have moderately fine texture to moderately coarse texture. These soils have a moderate rate of water transmission.

A summary of the soil composition is shown in Table 1 below.

Unit Symbol – Unit Name	Hydrologic Soil Group	Percent of Drainage Areas
73C – Charlton-Chatfield complex, 3 to 15 percent slopes, very rocky	В	99.3
73E – Charlton-Chatfield complex, 15 to 45 percent slopes, very rocky	В	0.7

#### **Table 1 - Soil Analysis Summary**

#### **Design Methodology**

In order to design the proposed swales and culverts, peak flows (Q) for the 10- and 25-year design storms were calculated using the Rational Method (Q=CIA). Composite runoff coefficients (C) were developed from an analysis of existing land use and typical C-values provided in Tables 6-3 and 6-5 of the Connecticut Department of Transportation (ConnDOT) Drainage Manual, dated October 2000 (See Appendix B). Times of concentration ( $T_c$ ) were computed using standard NRCS TR-55 Methodology (See Appendix C). Rainfall intensities (I) were determined from Table B-2.1 of the ConnDOT Drainage Manual and the computed  $T_c$  values. A frequency factor ( $C_f$ ) was used to refine the calculated peak flow for the 25-year design storm as prescribed in Table 6-2 in Section 6.9.5 of the ConnDOT Drainage Manual.

#### Proposed Condition Hydrology

For the purposes of the proposed condition analysis, two (2) drainage areas (DA) and two (2) subdrainage areas (SDA) were developed to quantify the peak stormwater runoff rates to the proposed design points (DP). Drainage areas were determined through review of the existing topographic survey of the site (See D&M Drawing submission), the Connecticut USGS Coventry Quadrangle Map and a field visit to the site.

A summary of the results for the proposed condition hydrologic analysis is shown in Table 2 below (See Figure 4 site drainage areas).

Drainage Area/	Area	<b>Runoff</b>	Тс	Rainfall I (in	ntensity (I) /hr)	Peak Dis	charge (Q) cfs)
Design Point	(acres)	(C)	$(\min)^2$	10 year	25 year	10 year	25 year <sup>1</sup>
DA 1	1.70	0.23	10	4.8	5.5	1.9	2.4
DA 2	4.15	0.28	13	4.3	5.0	5.0	6.4
SDA 1.1	1.10	0.23	10	4.8	5.5	1.2	1.5
SDA 2.1	2.28	0.28	13	4.3	5.0	2.8	3.5

 Table 2 – Hydrologic Analysis Summary (Drainage Areas)

<sup>1</sup>Frequency Factor for 25-year recurrence interval is 1.1. (Table 6-2 of ConnDOT Drainage Manual)

<sup>2</sup>Per section 6.9.6 of the ConnDOT Drainage Manual, the minimum  $T_C$  used for design purposes shall be 10 minutes for grass areas.

#### 3.0 HYDRAULIC EVALUATION

#### 3.1 CULVERT

#### **Basis of Design**

In accordance with the design criteria and procedures set forth in Section 8.3 of the ConnDOT Drainage Manual, culverts shall be designed to:

- Allow for continuous flow and safe conveyance of the 25-year design storm peak flow.
- Have a HW/D ratio less than 1.5 (The hydraulic performance of a culvert is commonly expressed as a ratio of headwater depth (HW), which equals the depth of water measured from the invert of the culvert, to the culvert diameter (D) as HW/D).
- Have a minimum diameter of 18 inches.

#### **Design Methodology**

The proposed culverts were analyzed using Haestad Methods CulvertMaster Computer Software (Version 3.1). This program was utilized to compute the headwater elevation and discharge velocity of the culverts (evaluating both inlet and outlet control equations) (See Appendix D).

The pipe flow capacity was calculated using:

- Manning's Equation for velocity (V) using equation 7.6 of the ConnDOT Drainage Manual.
- The Continuity Equation for flow capacity (Q) using equation 7.5 of the ConnDOT Drainage Manual.

See Appendix E for culvert capacity calculations.

#### **Design Summary**

The access road design required one (1) culvert (at DP DA 1) for stormwater conveyance (See Figure 4 for location). The culvert at DP DA 1 will be an 18" diameter HDPE pipe culvert, 43feet in length, set at a slope of approximately 0.5 percent. (See Figure 5 for drainage details).

See Table 3 on the following page for a summary of the results of the culvert analysis

Culvert	Length (ft)	Slope (%)	Diameter (inches)	Manning's n <sup>1</sup> (unitless)	25-year Peak Design Flow (cfs)	Provided Flow Capacity <sup>2</sup> (cfs)	Computed HW (in)	HW/D Ratio (in/in)
DP DA 1	43	0.5	18	0.012	2.4	8.0	6.8	0.38

 Table 3 – Culvert Analysis

<sup>1</sup>Manning's n referenced from CulvertMaster.

<sup>2</sup>See Appendix E for culvert capacity calculations.

Based on the analysis, a 18" HDPE pipe culvert at DP DA 1will allow for continuous passage of the 25year frequency design storm, with a calculated HW/D ratio less than 1.5.

#### 3.2 SWALES

#### **Basis of Design**

In accordance with the design criteria and procedures set forth in Sections 7.3 and 7.6 of the ConnDOT Drainage Manual, roadway swales shall be designed:

- To safely convey the 10-year frequency design storm peak flow without causing erosive damage.
- With a lining that is sufficient to resist the shear forces created from the transportation of storm flows (The permissible or critical shear stress in a swale defines the force required to initiate movement of the channel bed or lining).

Additionally, in accordance with Chapter 5, Section 6, Permanent Lined Waterway, of the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control by The Connecticut Council on Soil and Water Conservation in Cooperation with the Connecticut Department of Environmental Protection (CTDEP), swales shall be designed with a minimum freeboard of 0.25 feet (3 inches) if no out-of-bank damage would be expected.

#### **Design Methodology**

Flow capacity of the swales was determined from the following:

- Velocity (V) Equation 7.6 of the ConnDOT Drainage Manual (Manning's Equation)
- Flow capacity (Q) Equation 7.5 of the ConnDOT Drainage Manual (The Continuity Equation).

See Appendix G for swale sizing calculations.

Swale lining was determined by the following:

- Average Shear Stress  $(\tau)$  Equation 7.11 of the ConnDOT Drainage Manual
- Maximum Shear Stress  $(\tau_d)$  Equation 7.12 of the ConnDOT Drainage Manual
- Lining Category (Material) and Type– Table 7-4 of the ConnDOT Drainage Manual

See Appendix H for shear stress calculations.

#### **Design Summary**

For ease of construction, one swale type (size) was designed which meets the dimensional requirements at all swale locations. (See Figure 4 for proposed swale locations and Figure 5 for drainage details). The swale selected is a 1-foot deep, 1-foot wide flat bottom trapezoidal swale with 2:1 side slopes.

See Table 4 on the following page for a summary of the results of the swale analysis.

Swale	Slope (ft/ft)	Manning's n <sup>1</sup> (unitless)	Velocity (ft/s)	10-yr Peak Design Flow (cfs)	Provided Flow Capacity (cfs)	Depth of Flow (in)	Provided Freeboard @ 10-year Peak Flow (in)
DA 1	0.11	0.064	3.0	1.9	8.2	4.6	7.4
SDA 1.1	0.20	0.078	2.9	1.2	9.1	3.4	8.6
SDA 1.2	0.07	0.059	3.0	2.8	7.1	5.8	6.2

 Table 4 – Swale Hydraulic Analysis

<sup>1</sup>Manning's n calculated using steep slope procedures in HEC-15, as prescribed in Section 7.6.9 of the ConnDOT Drainage Manual, as well as, the values listed in Table 7-4 of the ConnDOT Drainage Manual.

To determine the type of lining necessary to armor the swales and protect against erosive forces imparted by stormwater flows, shear stresses were calculated. Rock riprap lining was selected to armor the swales in order to withstand the calculated shear stresses. See Table 5 below for a summary of the results of the calculated shear stress and riprap sizing analysis.

	Calculated	Required Conn	DOT Riprap <sup>1</sup>	
Swale	Shear Stress (lb/ft <sup>2</sup> )	Permissible Shear Stress <sup>2</sup> (lb/ft <sup>2</sup> )	Classification	D <sub>50</sub> Size (inches)
DA 1	2.61	2.68	Intermediate	8
SDA 1.1	3.49	4.00	Intermediate	12
SDA 2.1	2.10	2.68	Intermediate	8

Table 5 – Shear Stress and Riprap Sizing Analysis

<sup>1</sup>Determined by selecting riprap with a higher permissible shear stress than the calculated shear stress <sup>2</sup>Permissible shear stress for lining materials is taken from Table 7-4 of the ConnDOT Drainage Manual

Based on the analyses, each of these swales will be capable of safely conveying the 10-year peak storm flows calculated for their respective Drainage Area, provide the required 3 inches of freeboard, and withstand calculated shear stresses.

#### 3.3 OUTLET PROTECTION

#### **Basis of Design**

In accordance with the design criteria and procedures set forth in Section 11.13.3 of the ConnDOT Drainage Manual, riprap outlet protection shall be designed to reduce the erosive potential at all discharge points.

#### Design Methodology

The type and dimensions of rip rap protection was determined by the guidelines established in Sections 11.13.2 and 11.13.5 of the ConnDOT Drainage Manual, and the following:

- Length (L<sub>a</sub>) Tables 11-12.1 and 11-13.1 of the ConnDOT Drainage Manual
- Width of apron at pipe outlet (W<sub>1</sub>) and width of apron at terminus (W<sub>2</sub>) Equation 11.33 of the ConnDOT Drainage Manual, as well as, Section 11.13.5 of the ConnDOT Drainage Manual.
- Riprap Specification Table 11.11 of the ConnDOT Drainage Manual

See Appendix I for outlet protection calculations.

#### **Design Summary**

Based on recommended design procedures in Section 11.13.2 of the ConnDOT Drainage Manual, a Type A riprap apron shall be used at all of the discharge points. The selected riprap apron shall have a length  $(L_a)$  of 12 feet, a width of apron at outlet  $(W_1)$  of 5 feet, and a width of apron at terminus  $(W_2)$  of 15 feet. Type A riprap aprons shall utilize modified riprap for erosion protection. (See Figure 5 for drainage details).

Table 6 on the following page summarizes the minimum outlet protection requirements.

Design		Diameter	Outlet	25-year Peak	Outlet		Calcul	ated Di	imensions <sup>6</sup>
Point	Structure	Structure or Span Vel (in) (ft	Velocity (ft/sec)	Discharge $(ft^3/sec)$	Туре	$L_a^{-1}$ (ft)	W <sub>1</sub> <sup>2</sup> (ft)	$W_2^3$ (ft)	Riprap Specification <sup>4</sup>
DA 1	Culvert	18	4.2	2.4	Type A	12	4.5	12.9	Modified
SDA 1.1	Swale <sup>5</sup>	12	3.1	1.5	Riprap	10	3	10	Modified
SDA 2.1	Swale <sup>5</sup>	12	3.2	3.5	Apron	10	3	10	Modified

 Table 6 – Outlet Protection Requirements

 ${}^{1}L_{a}$  values determined using Table 11-12.1 and 11-13.1 of the ConnDOT Drainage Manual.

 $^{2}W_{1}$  = width of apron at pipe outlet

 ${}^{3}W_{2}$  = width of apron at terminus

<sup>4</sup>Riprap specification selected from Table 11.11 of the ConnDOT Drainage Manual

<sup>5</sup>Diameter used for swales is the bottom channel width

<sup>6</sup>Dimensions represent minimum acceptable parameters based on calculations. Actual dimensions selected for use may differ

Based on analysis of proposed outfall locations, discharge velocities meet the ConnDOT requirements for use of riprap aprons (outlet velocities are less than 14 fps). A Type A riprap aprong with dimensions of 12' ( $L_a$ ) x 5' ( $W_1$ ) x 15' ( $W_2$ ) is sufficient to reduce the erosive potential at all discharge points.

#### 4.0 DRAINAGE AREA 2 DESIGN POINT

The design point for DA 2 is an existing topographic depression on the east side of the gravel access drive, adjacent to Tolland Turnpike. The gravel access drive (existing and proposed condition) forms a topographic ridge which isolates the depression and stops the flow of water to the east. To ensure the development of the access road does not create drainage issues at this design point, a pre-development versus post-development analysis was done for this design point (See Figure 3 for proposed DA 2 details; See Figure 6 for existing DA 2 details). Table 7 below shows the results of the pre- vs post- hydrologic analysis.

Drainage Area/	Area	Runoff Coefficient	Tc	Rainfall Intensity (I) (in/hr)		Peak Discharge (Q) (cfs)		
Design Point	(acres)	(C)	$(\min)^2$	10 year	25 year	10 year	25 year <sup>1</sup>	
DA 2 - Existing	3.09	0.25	12	4.5	5.1	3.5	4.4	
DA 2 - Proposed	4.15	0.28	13	4.3	5.0	5.0	6.4	

Table 7 – Pre-Development versus Post Development Hydrology for DA 2

<sup>1</sup>Frequency Factor for 25-year recurrence interval is 1.1. (Table 6-2 of ConnDOT Drainage Manual)

<sup>2</sup>Per section 6.9.6 of the ConnDOT Drainage Manual, the minimum  $T_C$  used for design purposes shall be 10 minutes for grass areas.

Table 8 shows that the 10- and 25-year design storm peak flows will increase about 25% for the proposed condition. However, there are mitigating factors which justify this increase as being insignificant. First, discussion with an adjacent property owner revealed that the existing topographic depressions on either side of the gravel access drive remain dry year-round. The property owner has never seen the depression at the DA 2 design point collect water and indicated that everything infiltrates. Second, groundwater infiltration has not been factored into the calculations for peak flows, which is a conservative design assumption at this site.

#### 5.0 **INSPECTION AND MAINTENANCE**

Inspection and maintenance of the stormwater collection system (riprap lined swales, storm drain culverts, and riprap aprons) is critical to maintaining proper function. Normally, a visual inspection of all components should be completed annually and after major storm events. Due to steep gradients which produce high shear stresses in the proposed swales, an increased inspection and maintenance schedule is required. A visual inspection of the swale riprap lining should be completed semi-annually and after major storm events.

The following maintenance tasks should be completed during the inspection process:

- Removal of any organic matter, trash/debris, or obstructions found in swales or riprap aprons
- Removal of any accumulated sediment found in culvert, swales or riprap aprons
- Removal of any potential obstructions at culvert inlet/outlet points
- Replacement of any riprap material that may have washed away during large storm events

Careful inspection and proper maintenance on a regular basis will enable the system to safely convey stormwater flows and reduce the risk of system backup or overflow during major storm events.

#### 6.0 CONCLUSION

All proposed drainage improvements (swales, culverts, outlet protection) have been designed in accordance with the engineering guidelines established in the ConnDOT Drainage Manual. Based on the analysis, the following design parameters are recommended:

- A culvert is required at DP DA 1 to convey flows underneath an existing gravel access drive. The culvert shall be an 18" diameter HDPE pipe culvert which is 43feet in length, and set at a slope of 0.5%. The culvert will be capable of safely conveying the 25-year design storm peak flow with an HW/D ratio less than 1.5.
- Swales shall be at minimum 1-foot wide flat bottom, 1-foot deep, riprap lined trapezoidal swales with 2:1 side slopes. The designed swales will meet the ConnDOT requirements for conveying the 10-year design storm peak flows while withstanding the calculated shear stresses. They will also meet the DEEP requirement of providing 0.25 feet of freeboard.
- Outlet protection for swales SDA 1.1, SDA 2.1 and Culvert 1 shall be Type A riprap aprons with the following minimum parameters:
  - o Length  $(L_a) 12$  feet
  - o Width of apron at pipe outlet  $(W_1) 5$  feet
  - $\circ \quad \text{Width of apron at terminus } (W_2) 15 \text{ feet}$
  - Utilize modified riprap for armoring.

This will meet the ConnDOT requirements for use of riprap aprons (discharge velocities < 14 fps) to provide erosion protection at outfall locations.

ATTACHMENT 4

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APT Example Erosion and Sedimentation Control Site Inspection Form

### **Project Name**

Site E&S Inspection Form Report No.

#### APT Project #:

Project Street Address Project Town, State

Date of Inspection:	Weather Conditions:
Time of Inspection:	Latest Precipitation Event:

Construction Activities Underway since last documented inspection:

Check if NOT Functioning Properly	Erosion Control Measure
	Street Sweeping/ Construction Access
	Stabilized Construction Entrance
	Temporary/Permanent Check Dams
	Temporary/Permanent Sediment Basins/Traps
	Drainage Swales and Diversion Channels
	Perimeter Controls (i.e. hay bales, straw wattles, silt fencing etc.)
	Catch Basin Protection
	Temporary/Permanent Slope Stabilization
	Dewatering Basins and Filter Devices
	Outlet Protection (i.e. plunge pool, splash pad, level spreader, etc.)
	Active Treatment Systems

\*In the event of a spill refer to the Spill Response Procedure and contact appropriate agencies. Refer to SWPPP for Spill Prevention Plan and Response Procedures.

Are sediment/pollution discharges from the site present?				
□ No □ Yes If yes, describe:				

Im	mediate Action Items:
1.	
2.	
3.	
4.	

Ad	ditional Action Items/Comments:
1.	
2.	
3.	
4	

Ite	Items/Comments Addressed From Previous Report(s):		
1.			
2.			
3.			
4.			

I certify under penalty of law that this document and all attachments were prepared under my direction or supervision in accordance with a system designed to assure that qualified personnel properly gathered and evaluated the information submitted. Based on my inquiry of the person or persons who manage the system, or those persons directly responsible for gathering the information, the information submitted is, to the best of my knowledge and belief, true, accurate, and complete. I am aware that there are significant penalties for submitting false information, including the possibility of fine and imprisonment for knowing violations.

Erosion Control Inspector: \_\_\_\_\_ Date: \_\_\_\_\_ Date: \_\_\_\_\_

Qualifications: \_\_\_\_\_

\*\*A copy of this report should be placed in the Monitoring Section of the Stormwater Pollution Prevention Plan, if applicable.

#### ATTACHMENT 5



SBNH-1D6565C

#### **Mechanical Specifications**

Color	Light gray			
Connector Interface	7-16 DIN Female			
Connector Location	Bottom			
Connector Quantity	4			
Radome Material	Fiberglass, UV resistant			
Wind Loading, maximum	879.0 N @ 150 km/h 197.6 lbf @ 150 km/h			
Wind Speed, maximum	241.0 km/h   149.8 mph			

#### Dimensions

Depth	181.0 mm   7.1 in
Length	2449.0 mm   96.4 in
Width	301.0 mm   11.9 in
Net Weight	27.6 kg   60.8 lb

#### Remote Electrical Tilt (RET) Information

Adjustment Time, full range, maximum	30 s
Annual Failure Rate, maximum	0.01%
Power Consumption, during motor movements, maximum	11.0 W
Power Consumption, idle state, maximum	2.0 W
Power Input	10-30 V
Protocol	3GPP/AISG 2.0 Multi-RET
RET Interface	RS-485 Male (input port, 1)   RS-485 Female (daisy chain port ,1)
RET System	Teletilt®

#### Regulatory Compliance/Certifications

Agency RoHS 2002/95/EC China RoHS SJ/T 11364-2006 **Classification** Compliant by Exemption Above Maximum Concentration Value (MCV)



#### INCLUDED PRODUCTS

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#### SBNH-1D6565C

DualPol® Dual Band Antenna, 698–896 MHz and 1710–2170 MHz, 65° horizontal beamwidth, RET compatible variable electrical tilt



- Two DualPol® antennas under one radome
- Interleaved dipole technology providing for attractive, low wind load mechanical package
- Each antenna is independently capable of field adjustable electrical tilt
- Internal next generation actuator eliminates field installation and defines new standards for reliability
- Fully compatible with Andrew Teletilt® remote control system

#### CHARACTERISTICS

#### **General Specifications**

Antenna Type	SmartBeam®
Brand	DualPol®   SmartBeam®   Teletilt®
Operating Frequency Band	1710 – 2170 MHz   698 – 896 MHz

#### **Electrical Specifications**

698-806	806-896	1710-1880	1850-1990	1920-2170
71	67	58	57	59
±3	±6	±3	±3	±3
13.6	14.3	15.9	15.9	15.9
15.7	16.4	18.0	18.0	18.0
8.6	7.8	5.5	5.1	4.8
0-11	0-11	0-7	0-7	0-7
15	15	16	16	16
25	28	34	31	31
21	22	30	27	26
24	21	17	17	17
11	8	9	8	9
30	30	30	30	30
35	35	35	35	35
1.5:1   14.0	1.5:1   14.0	1.5:1   14.0	1.5:1   14.0	1.5:1   14.0
-150	-150	-150	-150	-150
400	400	300	300	300
±45°	±45°	±45°	±45°	±45°
50	50	50	50	50
dc Ground	dc Ground	dc Ground	dc Ground	dc Ground
	<b>698-806</b> 71 ±3 13.6 15.7 8.6 0-11 15 25 21 24 11 30 35 1.5:1   14.0 -150 400 ±45° 50 dc Ground	698-806806-89671 $67$ $\pm 3$ $\pm 6$ 13.614.315.716.48.67.80-110-111515252821222421118303035351.5:1   14.0-150 $-150$ $400$ $\pm 45^{\circ}$ $\pm 45^{\circ}$ 5050dc Grounddc Ground	698-806806-8961710-1880716758 $\pm 3$ $\pm 6$ $\pm 3$ 13.614.315.915.716.418.08.67.85.50-110-110-715151625283421223024211711893030303535351.5:1   14.01.5:1   14.0-150-150-150400400300 $\pm 45^{\circ}$ $\pm 45^{\circ}$ $\pm 45^{\circ}$ 50505050dc Grounddc Grounddc Ground	698-806806-8961710-18801850-199071675857 $\pm 3$ $\pm 6$ $\pm 3$ $\pm 3$ 13.614.315.915.915.716.418.018.08.67.85.55.10-110-110-70-7151516162528343121223027242117171189830303030353535351.5:1   14.01.5:1   14.01.5:1   14.0-150-150-150-150400400300300 $\pm 45^\circ$ $\pm 45^\circ$ $\pm 45^\circ$ 50505050dc Grounddc Grounddc Ground

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SBNH-1D6565C





#### **DB**380

Pipe Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members



#### DB5083

Downtilt Mounting Kit for 2.4 - 4.5 in (60 - 115 mm) OD round members

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SBNH-1D6565C

#### Horizontal Pattern

#### Vertical Pattern







Freq: 850 MHz, Tilt: 0°



Freq: 725 MHz, Tilt: 0°









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SBNH-1D6565C





Freq: 1920 MHz, Tilt: 0\*





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#### ATTACHMENT 6





### **Industrial Diesel Generator Set**

**EPA Emissions Certification: Tier III** 

# **SD050**

CUSTOM MODEL

Standby Power Rating 50KW 60 Hz









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. **Controls** 

<u>Alternator</u>

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Generator Set

### **benefits**

PROTOTYPE & TORSIONALLY TESTED	►	PROVIDES A PROVEN UNIT
UL2200 TESTED	►	ENSURES A QUALITY PRODUCT
RHINOCOAT PAINT SYSTEM	►	IMPROVES RESISTANCE TO ELEMENTS
SOUND LEVEL 2 ENCLOSURE	•	71dbA @ 7 METERS (23FT)
EPA TIER CERTIFIED	►	ENVIRONMENTALLY FRIENDLY
INDUSTRIAL TESTED, GENERAC APPROVED	►	ENSURES INDUSTRIAL STANDARDS
POWER-MATCHED OUTPUT	►	ENGINEERED FOR PERFORMANCE
INDUSTRIAL GRADE	►	IMPROVES LONGEVITY AND RELIABILITY
tor		
TWO-THIRDS PITCH	►	ELIMINATES HARMFUL 3RD HARMONIC
LAYER WOUND ROTOR & STATOR	►	IMPROVES COOLING
CLASS H MATERIALS	►	HEAT TOLERANT DESIGN
DIGITAL 3-PHASE VOLTAGE CONTROL	•	FAST AND ACCURATE RESPONSE
<u>s</u>		
ENCAPSULATED BOARD W/ SEALED HARNESS	►	EASY, AFFORDABLE REPLACEMENT
4-20mA VOLTAGE-TO-CURRENT SENSORS	►	NOISE RESISTANT 24/7 MONITORING
SURFACE-MOUNT TECHNOLOGY	►	PROVIDES VIBRATION RESISTANCE
ADVANCED DIAGNOSTICS & COMMUNICATIONS	►	HARDENED RELIABILITY

### primary codes and standards





**€₽** 



1 of 5

### application and engineering data

#### 2 of 5

#### ENGINE SPECIFICATIONS

General		
Make	lveco	/ FPT
EPA Emissions Compliance	Tie	er III
EPA Emissions Reference	See Emission	ns Data Sheet
Cylinder #	2	4
Туре	Die	esel
Displacement - L (cu. in.)	4.5	(274)
Bore - mm (in.)	105	(4.1)
Stroke - mm (in.)	132	(5.2)
Compression Ratio	17.	.5:1
Intake Air Method	Turboo	harged
Cylinder Head Type	2 V	alve
Piston Type	Alum	iinum
Crankshaft Type	Forged Steel	
Engine Block Type	Cast Iron / Wet Sleeve	

Engine Governing	
Governor	Electronic Isochronous
Frequency Regulation (Steady State)	+/- 0.25%

#### Lubrication System

Oil Pump Type	Gear
Oil Filter Type	Full Flow
Crankcase Capacity - L (gal)(qts)	13.6 (3.6) (14.4)

#### Cooling System

Cooling System Type	Closed
Water Pump	Belt Driven Centrifugal
Fan Type	Pusher
Fan Blade Number	2538 (10)
Fan Diameter (in.)	26
Coolant Heater Wattage	1500
Coolant Heater Standard Voltage	120

#### Fuel System

Fuel Type	Ultra Low Sulfur Diesel Fuel
Fuel Specifications	ASTM
Fuel Filtering (microns)	5
Fuel Inject Pump Make	Standyne
Fuel Pump Type	Engine Driven Gear
Injector Type	Mechanical
Engine Type	Direct Injection
Fuel Supply Line - mm (in.)	1/4 inch Npt
Fuel Return Line - mm (in.)	1/4 inch Npt

#### Engine Electrical System

System Voltage	12VDC
Battery Charging Alternator	90 Amp
Battery Size (at 0 oC)	Optima Redtop
Battery Group	34
Battery Voltage	12VC
Ground Polarity	Negative

#### ALTERNATOR SPECIFICATIONS

Standard Model	390
Poles	4
Field Type	Revolving
Insulation Class - Rotor	Н
Insulation Class - Stator	н
Total Harmonic Distortion	< 3.5%
Telephone Interference Factor (TIF)	< 50
Standard Excitation	PMG
Bearings	Single Sealed Cartridge
Coupling	Direct, Flexible Disc
Load Capacity - Standby	100%
Load Capacity - Prime	100%
Prototype Short Circuit Test	Y

#### CODES AND STANDARDS COMPLIANCE (WHERE APPLICABLE)

NFPA 99 NFPA 110 ISO 8528-5 ISO 1708A.5 ISO 3046 BS5514 SAE J1349 DIN6271 IEEE C62.41 TESTING NEMA ICS 1

Rating Definitions:

Standby - Applicable for a varying emergency load for the duration of a utility power outage with no overload capability. (Max. load factor = 70%)

Prime – Applicable for supplying power to a varying load in lieu of utility for an unlimited amount of running time. (Max. load factor = 80%) A 10% overload capacity is available for 1 out of every 12 hours.

Voltage Regulator Type	Digital
Number of Sensed Phases	All
Regulation Accuracy (Steady State)	+/- 0.25%

### SD050

### operating data (60Hz)

#### POWER RATINGS (kW)

Single-Phase 120/240VAC @1.0pf
Three-Phase 120/208VAC @0.8pf
Three-Phase 120/240VAC @0.8pf
Three-Phase 277/480VAC @0.8pf
Three-Phase 346/600VAC @0.8pf

#### STARTING CAPABILITIES (sKVA)

	STANDBY					
50	Amps:	208				
-	Amps:	-				
-	Amps:	-				
-	Amps:	-				
-	Amps:	-				
NOTE: Generator output limited to 200A.						

NOTE. Generator of

							sKVA vs. V	oltage Dip				<u> </u>	
				48	OVAC			208/240VAC					
Alternator*	<u>kW</u>	10%	15%	20%	25%	30%	35%	10%	15%	20%	25%	30%	35%
Standard	50	-	-	· ·	-	-	-	26	39	52	65	77	90
Upsize 1		-	-	-	-	-	-	-	-	-	-	-	-
Upsize 2		-	-	-	-	-	-	-	-	-	-	-	-
	*All Generac temperature	industrial alterr rise. Upsize 2 p	nators utilize C rovides less th	lass H insulatio an or equal	n materials. Sta	ndard alternate	or provides less	than or equal to	o Class B temp	erature rise. U	psize 1 provide	s less than or e	qual to Cla
JEL													
					Fuel C	onsumptio	n Rates						
Fuel Pump Lift	- in (m)	_			<u>STA</u>	NDBY							
36(.9)				Perce	nt Load	gph	lph	_					
		-		2	5%	1.52	5.75						
				5	0%	2.33	8.82						
				7.	5%	3.08	11.65						
				10	0%	4.15	15.71						
OOLING													
Coolant System	Capacity	- Gal (L)	-							STA	NDBY	-	
4.5	(17.44)		Coolant Flow per Minute						gpm (lpm)	32.7(	123.8)		
				Heat reje	leat rejection to Coolant				BTU/min	123	8,000		
Maximum Radia	ator Backp	oressure	-	Inlet Air				cfm	(m3/min)	6,360	(180.0)		
1.5" H <sub>2</sub> (	O Column			Max. Operating Radiator Air Temp					F <sup>o</sup> (C <sup>o</sup> )	122	2(50)		
	Ma			Max. Ope	Max. Operating Ambient Temperature				F <sup>o</sup> (C <sup>o</sup> )	122	2(50)		
OMBUSTION AIR	REOUIR	EMENTS		P								4	
						STANDBY							
Intake Flow at Rat	ed Power		cfm	(m3/min)	247		(7.00)	1					
				( -, ,			()	1					
XHAUST													
Exhaust Outle	t Size (Ope	n Set)								STA	NDBY		
3	.0"			Exhaust F	low (Rate	d Output)		cfr	n (m3/hr)	534(	906.7)	Ĩ	
Maximum Backpre	ssure (Post	t-Silencer)		Maximun	n Backpres	sure		i	nHg (Kpa)	1.5	(5.1)	1	
1.5	" Hg			Exhaust T	emp (Rate	ed Output)			°F (°C)	9	30(498.8)	1	
								8	. ,			4	
										STA	NDRY		
				Rated En	pine Sneer	1		1	rnm	15	300	T	
				Horsepoy	ver at Rate	ed kW			hn		93	1	
				Тапарала	Lune Devet					Concult	Fastan	1	
				Tempera	lure Derai	ion				CONSUM	LFACLORV		

\* CA units include aftertreatment



### standard features and options

4 of 5

GENERATOR SET	
Genset Vibration Isolation	

Genset Vibration Isolation	Std
Factory Testing	Std
Extended warranty	Std
Padlockable Doors	Std
Steel Enclosure (Enclosed Models)	Std
Remote Emergency Shutdown	Opt

-	LHC ME

CONTROL SYSTEM

### ENGINE SYSTEM

**SD050** 

deneral	
Oil Drain Extension	Std
Air Cleaner	Std
Industrial Exhaust Silencer (Open Sets, ship loose)	Std
<ul> <li>Critical Exhaust Silencer (Enclosed Sets)</li> </ul>	Std
Stainless steel flexible exhaust connection	Std
Fuel System	
Primary Fuel Filter with Water Separator	Std
Flexible Fuel Lines	Std
UL142 Fuel Tank, 48 Hr Runtime	Std
2 Gal Overflow Containment with Alarm	Std

Cooling System	
<ul> <li>120VAC Coolant Heater (3-wire connection cord)</li> </ul>	Std
50%/50% Coolant	Std
Level 1 Guarding (Open Sets)	Std
Closed Coolant Recovery System	Std
UV/Ozone resistant hoses	Std
Factory-Installed Radiator	Std
Radiator Drain Extension	Std
Fan guard	Std
<ul> <li>Radiator duct adapter (Open Sets)</li> </ul>	Std

#### Engine Electrical System

Battery charging alternator	Std
Battery cables	Std
Battery tray	Std
75W 120VAC Battery heater	Std
Solenoid activated starter motor	Std
10A UL float/equalize battery charger	Std
Weather Resistant electrical connections	Std
Duplex GFCI Convenience Outlet	Std

#### ALTERNATOR SYSTEM

•	UL2200 GENprotect <sup>™</sup>	Std
0	100% Rated 200A Main Line Circuit Breaker	Std

-	Control Panel	<b>C</b> 1
ž	Digital H Control Pariel - Dual 4x20 Display	Sta
ž	7 Day Programmable Eversion (requires H Transfer Switch)	Stu
ž	Special Applications Programmable DLC	Stu
ž		Stu
ž		Stu Std
ž	All-Phase Sensing DVR	Std
ž	Full System Status	Std
ž	Litility Monitoring (Bog. H. Transfor Switch)	Ct d
ž		Stu
2	2-Wire Start Compatible	Std
2	Power Output (kW)	Std
2	Power Factor	Std
2	Reactive Power	Std
2	All phase AC Voltage	Std
2	All phase Currents	Std
2	Oil Pressure	Std
2	Coolant Temperature	Std
2	Coolant Level	Std
2	Low Fuel Pressure Indication	Std
2	Engine Speed	Std
2	Battery Voltage	Std
2	Frequency	Std
2	Date/Time Fault History (Event Log)	Std
	UL2200 GENprotect™	Std
õ	Low-Speed Exercise	Opt
2	Isochronous Governor Control	Std
2	-40deg C - 70deg C Operation	Std
	Weather Resistant Electrical Connections	Std
	Audible Alarms and Shutdowns	Std
2	Not in Auto (Flashing Light)	Std
	On/Off/Manual Switch	Std
	E-Stop (Red Mushroom-Type)	Std
õ	Remote E-Stop (Break Glass-Type, Surface Mount)	-
õ	Remote E-Stop (Red Mushroom-Type, Surface Mount)	-
õ	Remote E-Stop (Red Mushroom-Type, Flush Mount)	-
	NFPA 110 Level I and II (Programmable)	Std
	Remote Communication - RS232	Std

# Alarms (Programmable Tolerances, Pre-Alarms and Shutdowns) Low Fuel Std Oil Pressure (Pre-programmed Low Pressure Shutdown) Std Coolant Temperature (Pre-programmed High Temp Shutdov Std Coolant Level (Pre-programmed Low Level Shutdown) Std Engine Speed (Pre-programmed Overspeed Shutdown) Std

Voltage (Pre-programmed Overvoltage Shutdown)
 Battery Voltage
 Std

Other Options

- je



0



### dimensions, weights and sound levels









	OPEN SET							
		TANK	SIZE					
	RUNTIME	CAPACITY	TANK					
	HOURS	(GAL)	VOLUME	L	W	Н	WT	dBA*
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	84
0	-	-	-	-	-	-	-	04
	48	210	210	76	38	87	3400	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	

	LEVEL 2 S	OUND ENG	LOSURE					
		TANK	SIZE					
	RUNTIME	CAPACITY	TANK					
	HOURS	(GAL)	VOLUME	L	W	Н	WT	dBA*
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	71
0	-	-	-	-	-	-	-	/1
	48	210	210	94.8	38	99	3935	
0	-	-	-	-	-	-	-	
0	-	-	-	-	-	-	-	

\*Required gallons based on 100% of standby rating. Weights consider steel enclosure and are without fuel in tank. Sound levels measured at 23ft (7m) and does not account for ambient site conditions.

YOUR FACTORY RECOGNIZED GENERAC INDUSTRIAL DEALER			

Specification characteristics may change without notice. Dimensions and weights are for preliminary purposes only. Please consult a Generac Power Systems Industrial Dealer for detailed installation drawings.

**SD050** 

# NEW CINGULAR WIRELESS PCS, LLC WIRELESS COMMUNICATIONS FACILITY #SR1 WILLINGTON

### TOLLAND TURNPIKE WILLINGTON, CONNECTICUT



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5	0+27.01	
5	0+34.30	
7	1+16.05	
)	2+07.74	
2	3+48.38	
)	4+23.09	
)	8+29.95	
I	8+72.92	
I	9+12.17	
I	N/A	



TABLE				
	BEARING	DISTANCE		
	S16-40-49W	27.01		
TANGENCY #1	S12-30-17W	7.28		
2	S08-19-44W	81.75		
TANGENCY #2	S07-07-17E	90.58		
3	S22-34-19E	140.64		
TANGENCY #3	S43-58-34E	72.99		
ł	S65-22-49E	406.85		
TANGENCY #4	S77-41-25E	42.64		
	EAST	39.25		
	NORTH	40.00		
	EAST	45.00		
	SOUTH	80.00		
	WEST	45.00		
	NORTH	40.00		





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- 7. ALL EXISTING INACTIVE SEWER, WATER, GAS, ELECTRIC AND OTHER UTILITIES, WHICH 16. INTERFERE WITH THE EXECUTION OF THE WORK, SHALL BE REMOVED AND/OR CAPPED, PLUGGED OR OTHERWISE DISCONTINUED AT POINTS WHICH WILL NOT INTERFERE WITH THE EXECUTION OF THE WORK, SUBJECT TO THE APPROVAL OF ENGINEERING.
- 8. CONTRACTOR IS TO SUPPLY COMBINATION LOCKS PER OWNER SPECIFICATIONS
- CONTRACTOR SHALL MINIMIZE DISTURBANCE TO EXISTING SITE DURING CONSTRUCTION. 9 EROSION CONTROL MEASURES SHALL BE IN CONFORMANCE WITH STATE OF CONNECTICUT GUIDELINES FOR EROSION AND SEDIMENT CONTROL AND COORDINATED WITH THE TOWN/COUNTY CODE ENFORCEMENT OFFICE.
- NOT GREATER THAN 80,000 SQUARE FEET OF LAND SHALL BE EXPOSED AT ANY ONE TIME DURING DEVELOPMENT. WHEN LAND IS EXPOSED DURING DEVELOPMENT, THE EXPOSURE SHOULD BE KEPT TO THE SHORTEST PRACTICAL PERIOD OF TIME AND SHALL NOT EXCEED 90 DAYS. LAND SHOULD NOT BE LEFT EXPOSED DURING THE WINTER 17. ANY DISTURBED AREAS OUTSIDE LIMITS OF CONSTRUCTION SHALL BE TOPSOILED, SEEDED
- WITH RYE GRASS, AND MACHINE HAY MULCHED TO PREVENT EROSION. HAY OR STRAW MULCH SHALL BE APPLIED TO ALL FRESHLY SEEDED AREAS AT A RATE OF 2 TONS PER ACRES. BALES SHALL BE UNSPOILED, AIR-DRIED, AND FREE FROM WEED, SEEDS, AND ANY COARSE MATERIAL

#### PETROLEUM/HAZARDOUS MATERIALS STORAGE AND SPILL PREVENTION PLAN:

CERTAIN PRECAUTIONS ARE NECESSARY TO STORE PETROLEUM AND HAZARDOUS MATERIALS, REFUEL AND CONTAIN AND PROPERLY CLEAN UP ANY INADVERTENT FUEL OR PETROLEUM (I.E., OIL, HYDRAULIC FLUID, ETC.) SPILL DUE TO THE PROJECT'S LOCATION IN A PUBLIC WATER SUPPLY WATERSHED. A SPILL CONTAINMENT KIT CONSISTING OF A SUFFICIENT SUPPLY OF ABSORBENT PADS AND ABSORBENT MATERIAL WILL BE MAINTAINED BY THE SITE CONTRACTOR AT THE CONSTRUCTION SITE THROUGHOUT THE DURATION OF THE PROJECT. IN ADDITION. A WASTE DRUM WILL BE KEPT ON SITE TO CONTAIN ANY USED ABSORBENT PADS/MATERIAL FOR PROPER DISPOSAL OFF SITE

THE FOLLOWING RESTRICTIONS, PROTECTIVE MEASURES AND PROCEDURES WILL BE ADHERED TO BY THE CONTRACTOR.

- PETROLEUM AND HAZARDOUS MATERIALS STORAGE AND REFUELING SERVICING OF MACHINERY SHOULD BE COMPLETED OUTSIDE OF THE PUBLIC
- WATER SUPPLY WATERSHED. • REFUELING OF VEHICLES OR MACHINERY SHOULD TAKE PLACE ON AN
- PUBLIC WATER SUPPLY WATERSHED.
- WATER SUPPLY WATERSHED DURING WORKING HOURS SHOULD BE STORED ON AN IMPERVIOUS SURFACE UTILIZING SECONDARY CONTAINMENT.

#### IN THE EVENT OF SPILL:

INITIAL RESPONSE

- STOP OPERATIONS AND SHUT OFF EQUIPMENT.
- · REMOVE ANY SOURCES OF SPARK OR FLAME.
- · CONTAIN THE SOURCE OF THE SPILL.

- OF THE SPILL TO SENSITIVE NEARBY WATERWAYS OR WETLANDS. . ENSURE THAT FELLOW WORKERS ARE NOTIFIED OF THE SPILL.

CLEAN UP & CONTAINMENT

- OBTAIN SPILL RESPONSE MATERIALS FROM THE ON-SITE SPILL RESPONSE KIT.
   LIMIT THE SPREAD OF THE SPILL BY PLACING ABSORBENT MATERIALS AROUND THE PERIMETER OF THE SPILL.
- CONTACT WINDHAM WATER WORKS IMMEDIATELY AT (860) 465-3086, ALONG WITH OTHER APPROPRIATE LOCAL, STATE AND/OR FEDERAL AGENCIES, AS NECESSARY
- · CONTACT A DISPOSAL COMPANY TO PROPERLY DISPOSE OF CONTAMINATED MATERIALS.

FOLLOW-UF

· COMPLETE AN INCIDENT REPORT.

· SUBMIT A COMPLETED INCIDENT REPORT TO WINDHAM WATER WORKS.

THE WINDHAM WATER WORKS AND CONNECTICUT SITING COUNCIL WILL BE NOTICED AT LEAST 48 HOURS IN ADVANCE OF A PRE-CONSTRUCTION MEETING WITH AN INVITATION TO ATTEND. DURING THE PROJECT'S PRE-CONSTRUCTION MEETING, THE CONTRACTOR WILL BE MADE AWARE OF THE SPECIAL PROTECTIVE PRECAUTIONS THAT ARE REQUIRED DUE TO THE PROJECT'S LOCATION IN THE MANSFIELD HOLLOW RESERVOIR PUBLIC WATER SUPPLY WATERSHED.

#### EROSION AND SEDIMENTATION CONTROLS

THE PROPOSED AT&T CONSTRUCTION PROJECT WILL FOLLOW AN APPROVED SOIL EROSION AND SEDIMENTATION CONTROL PLAN DESIGNED IN ACCORDANCE WITH THE 2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL. THE INSTALLED EROSION DEVICES WILL BE INSPECTED ONCE EVERY SEVEN DAYS AND AFTER SIGNIFICANT RAINFALL EVENTS OF GREATER THAN ONE HALF INCH OVER A 24-HOUR PERIOD TO ENSURE THAT PROPER PRECAUTIONS ARE TAKEN TO AVOID THE RELEASE OF SEDIMENT INTO NEARBY RESOURCE AREAS. THESE INSPECTIONS WILL BE DOCUMENTED ON AN EROSION AND SEDIMENTATION CONTROL SITE INSPECTION FORM (PLEASE REFER TO ATTACHED FORM). IN ADDITION TO THE SITE CONTRACTOR BEING RESPONSIBLE FOR THE PROPER INSTALLATION AND DAILY INSPECTION OF EROSION AND SEDIMENTATION (E&S) CONTROLS, STAFF FROM APT WILL INDEPENDENTLY INSPECT E&S CONTROLS AND DOCUMENT THEIR CONDITION AND RECOMMEND ANY ACTIONS NECESSARY TO BRING THE CONTROLS BACK INTO COMPLIANCE. THIS EXS CONTROL INSPECTION PROCEDURE WILL HELP AVOID EROSION AND SEDIMENTATION PROBLEMS BY ENSURING THAT THE EROSION CONTROL DEVICES ARE MAINTAINED AND FUNCTIONING PROPERLY. COPIES OF THE COMPLETED FORMS WILL BE SUBMITTED TO THE WINDHAM WATER WORKS AND CONNECTICUT SITING COUNCIL THROUGHOUT THE DURATION OF THE CONSTRUCTION PROJECT. IN ADDITION, WINDHAM WATER WORKS PERSONNEL WILL BE ALLOWED ACCESS TO THE PROJECT FOR PERIOD INSPECTIONS.

EROSION AND SEDIMENTATION CONTROL ITEMS SUBJECT TO INSPECTION INCLUDE, BUT ARE NOT LIMITED TO THE FOLLOWING:

- CONSTRUCTION ENTRANCE PAD
- SEDIMENT TRAPS
- SEDIMENT/ DETENTION BASINS • TEMPORARY SOIL STOCKPILE AREAS
- SILT FENCING/HAY BALES
  - SEEDING & MULCHING
- DRAINAGE SWALES DRAINAGE SWALE CHECK DAMS
- OTHER SITE-SPECIFIC EROSION CONTROL DEVICES

IMPERVIOUS PAD WITH SECONDARY CONTAINMENT DESIGNED TO CONTAIN FUELS. • FUEL AND OTHER HAZARDOUS MATERIALS SHOULD NOT BE STORED WITHIN THE

• ANY FUEL OR HAZARDOUS MATERIALS THAT MUST BE KEPT WITHIN THE PUBLIC

OETERMINE THE APPROXIMATE VOLUME OF THE SPILL.
 IDENTIFY THE LOCATION OF NATURAL FLOW PATHS TO PREVENT THE RELEASE













2	SILT FENCE/HAY	BALE
C10	NO SCALE	

NOTE:

- 1. THE GOETEXTILE FABRIC SHALL MEET THE DESIGN CRITERIA FOR SILT FENCES.
- 2. THE FABRIC SHALL BE EMBEDDED A MINIMUM OF 12" INTO THE GROUND AND THE SOIL COMPACTED OVER THE EMBEDDED FABRIC.
- 3. WOVEN WIRE FENCES SHALL BE FASTENED SECURELY TO THE FENCE POSTS WITH WIRE TIES OR STAPLES.
- 4. FILTER CLOTH SHALL BE FASTENED SECURELY TO THE WOVEN WIRE FENCE WITH TIES SPACED EVERY 24 INCHES AT THE TOP, MID-SECTION, AND BOTTOM
- 5. WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN ONE ANOTHER, THEY SHALL BE OVERLAPPED BY 6 INCHES, FOLDED AND STAPLED.
- 6. FENCE POSTS SHALL BE A MINIMUM OF 36" LONG AND DRIVEN A MINIMUM OF 24" INTO THE GROUND. WOOD POSTS SHALL BE OF SOUND QUALITY HARDWOOD AND SHALL HAVE A MINIMUM CROSS SECTIONAL AREA OF 3.0 SQUARE INCHES.
- 7. MAINTENANCE SHALL BE PERFORMED AS NEEDED TO PREVENT BULGES IN THE SILT FENCE DUE TO DEPOSITION OF SEDIMENT.

1. STANDARD RIPRAP:

THE MATERIAL SHALL CONFORM, TO THE FOLLOWING REQUIREMENTS:

A. NOT MORE THAN 15% OF THE RIPRAP SHALL BE SCATTERED SPALLS AND STONES LESS THAN 6 INCHES (150 MILLIMETERS) IN SIZE.

B. NO STONE SHALL BE LARGER THAN 30 INCHES (760 MILLIMETERS) IN SIZE, AND AT LEAST 75% OF THE WEIGHT (MASS) SHALL BE STONES AT LEAST 15 INCHES (380 MILLIMETERS) IN SIZE.

STONE SIZE:	% OF THE WEIGHT (MASS)
18 INCHES (460 MILLIMETERS OR OVER)	0
10 INCHES TO 18 INCHES (255 MILLIMETERS TO 460 MILLIMETERS)	30-50
6 INCHES TO 10 INCHES (150 MILLIMETERS TO 255 MILLIMETERS)	30-50
4 INCHES TO 6 INCHES (100 MILLIMETERS TO 150 MILLIMETERS)	20-30
2 INCHES TO 4 INCHES (50 MILLIMETERS TO 100 MILLIMETERS)	10-20
LESS THAN 2 INCHES (LESS THAN 50 MILLIMETERS)	0-10



![](_page_61_Figure_0.jpeg)

#### GENERAL NOTES

- 1. ALL DIMENSIONS TO, OF, AND ON EXISTING BUILDINGS, DRAINAGE STRUCTURES, AND SITE IMPROVEMENTS SHALL BE VERIFIED IN FIELD BY CONTRACTOR WITH ALL DISCREPANCIES REPORTED TO THE ENGINEER.
- 2. DO NOT CHANGE SIZE NOR SPACING OF STRUCTURAL ELEMENTS.
- 3. DETAILS SHOWN ARE TYPICAL; SIMILAR DETAILS APPLY TO SIMILAR CONDITIONS UNLESS OTHERWISE NOTED.
- 4. THESE DRAWINGS DO NOT INCLUDE NECESSARY COMPONENTS FOR CONSTRUCTION SAFETY
- 5. BRACE STRUCTURES UNTIL ALL STRUCTURAL ELEMENTS NEEDED FOR STABILITY ARE INSTALLED. THESE ELEMENTS ARE AS FOLLOWS: LATERAL BRACING, ANCHOR BOLTS, ETC.
- 6. DETERMINE EXACT LOCATION OF EXISTING UTILITIES, GROUNDS DRAINS, DRAIN PIPES, VENTS, ETC. BEFORE COMMENCING WORK.
- 7. INCORRECTLY FABRICATED, DAMAGED, OR OTHERWISE MISFITTING OR NONCONFORMING MATERIALS OR CONDITIONS SHALL BE REPORTED TO THE OWNER PRIOR TO REMEDIAL OR CORRECTIVE ACTION. ANY SUCH ACTION SHALL REQUIRE APPROVAL.
- 8. EACH CONTRACTOR SHALL COOPERATE WITH THE OWNER'S REPRESENTATIVE, AND COORDINATE HIS WORK WITH THE WORK OF OTHERS.
- 9. CONTRACTOR TO FOLLOW ALL STATE, LOCAL AND NATIONAL CODES AS APPLICABLE.

#### DESIGN DATA

LIVE LOADS: PER INTERNATIONAL BUILDING CODE WIND LOADS: PER INTERNATIONAL BUILDING CODE & TIA/EIA-222-F ICE LOADS: 1/2" RADIAL ON ALL COMPONENTS & CABLE SNOW LOAD: PER INTERNATIONAL BUILDING CODE SEISMIC LOADS: PER INTERNATIONAL BUILDING CODE

#### ANTENNA SUPPORT BRACKET NOTES

- DESIGN RESPONSIBILITY OF ANTENNA MOUNTING BRACKETS AND POLES AND ALL COMPONENTS THERE OF AND ATTACHMENT THERE TO SHALL BE THE RESPONSIBILITY OF THE MANUFACTURER. MFR. SHALL PROVIDE TO THE ENGINEER FOR APPROVAL, DRAWINGS DETAILING ALL COMPONENTS OF THE ASSEMBLY, INCLUDING CONNECTIONS, DESIGN LOADS. AND ALL OTHER PERTINENT DATA. ALL SUBMISSIONS SHALL BEAR THE STAMP AND SIGNATURE OF A PROFESSIONAL ENGINEER REGISTERED IN THE STATE THE WORK IS BEING PERFORMED.
- 2. BRACKETS SHALL BE DESIGNED TO SUPPORT CURRENT AND FUTURE PANEL ANTENNAS AND COAXIAL CABLES AS SHOWN.

#### STRUCTURAL STEEL NOTES

- 1. STRUCTURAL STEEL SHALL CONFORM TO THE LATEST EDITION OF THE AISC "SPECIFICATION FOR THE DESIGN, FABRICATION AND ERECTION OF STRUCTURAL STEEL FOR BUILDINGS"
- 2. ALL INTERIOR STRUCTURAL STEEL USED SHALL BE, WHEN DELIVERED, FINISHED WITH ONE COAT FABRICATOR'S NON-LEAD, RED OXIDE PRIMER. PRIMING SHALL BE PERFORMED AFTER SHOP FABRICATION TO THE GREATEST EXTENT POSSIBLE. ALL DINGS, SCRAPES, MARS, AND WELDS IN THE PRIMED AREAS SHALL BE REPAIRED BY FIELD TOUCHUP PRIOR TO COMPLETION OF THE WORK.
- 3. ALL EXTERIOR STEEL WORK SHALL BE GALVANIZED IN ACCORDANCE WITH SPECIFICATION ASTM A123 UNLESS OTHERWISE NOTED. GALVANIZING SHALL BE PERFORMED AFTER SHOP FABRICATION TO THE GREATEST EXTENT POSSIBLE. ALL DINGS. SCRAPES, MARS, AND WELDS IN THE GALVANIZED AREAS SHALL BE REPAIRED BY FIELD TOUCHUP PRIOR TO COMPLETION OF THE WORK USING ZRC COLD GALVANIZING COMPOUND OR APPROVED EQUAL.
- 4. DO NOT PLACE HOLES THROUGH STRUCTURAL STEEL MEMBERS EXCEPT AS SHOWN AND DETAILED ON STRUCTURAL DRAWINGS.
- 5 CONNECTIONS
- A. ALL WELDING SHALL BE DONE BY A CERTIFIED WELDER USING E70XX ELECTRODES AND WELDING SHALL CONFORM TO AISC AND AWS D1.1. WHERE FILLET WELD SIZES ARE NOT SHOWN, PROVIDE THE MINIMUM SIZE PER TABLE J2.4 IN THE AISC "MANUAL OF STEEL CONSTRUCTION ", 9TH EDITION. AT THE COMPLETION OF WELDING. ALL DAMAGE TO GALVANIZED COATING SHALL BE REPAIRED.
- B. BOLTED CONNECTIONS SHALL USE BEARING TYPE GALVANIZED ASTM A325 BOLTS (3/4" DIA) AND SHALL HAVE MINIMUM OF TWO BOLTS UNLESS NOTED OTHERWISE.
- C. NON-STRUCTURAL CONNECTIONS FOR STEEL GRATING MAY USE 5/8" DIA. GALVANIZED ASTM A 307 BOLTS UNLESS NOTED OTHERWISE.
- D. CONNECTION DESIGN BY FABRICATOR WILL BE SUBJECT TO REVIEW AND APPROVAL BY ENGINEER.
- E. ALL BOLTED CONNECTIONS SHALL HAVE A FLAT WASHER & NUT TIGHTENED TO AISC "SNUGTIGHT" CRITERIA, UNLESS NOTED OTHERWISE.

#### STRUCTURAL STEEL NOTES (CONT.)

- 6. STRUCTURAL STEEL GRATING SHALL BE 1 1/2" X 3/16" GALVANIZED STEEL BAR GRATING (IKG BORDEN TYPE-WB OR EQUAL) ATTACHED @ 1'-6" o.c. WITH GRATING CLAMPS. UNLESS OTHERWISE NOTED.
- 7. NEW STRUCTURAL STEEL LOCATED WITHIN A BUILDING OR ENCLOSURE SHALL BE FIRERATED PER LOCAL CODE.
- 8. REINFORCING BARS: ASTM A625, GRADE 60 DEFORMED BARS.
- 9. WELDED WIRE MESH: TO ASTM A185. PROVIDE IN FLAT SHEETS ONLY. VERTICAL PLACEMENT TOLERANCE TO BE 3/8 INCH.
- 10. THE CONTRACTOR SHALL FABRICATE ALL REINFORCEMENT AND FURNISH ALL ACCESSORIES, BOLSTERS, CHAIRS, SPACER BARS AND SUPPORTS NECESSARY TO SECURE THE REINFORCEMENT UNLESS INDICATED OTHERWISE.
- 11. IN SLABS WHERE REINFORCING IS SHOWN IN ONE DIRECTION ONLY, PROVIDE INDICATED TEMPERATURE REINFORCEMENT AT 90 DEGREES TO PRINCIPAL REINFORCEMENT.
- 12. LAP SPLICES:

a) CONCRETE: PROVIDE CLASS B TENSION LAP SPLICES U.N.O.

b) WELDED WIRE MESH: MINIMUM LAP 8 INCHES, MEASURED BETWEEN OUTERMOST CROSS-WIRES OF EACH SHEET.

#### CONCRETE NOTES

- 1. DESIGN AND CONSTRUCTION OF ALL CONCRETE ELEMENTS SHALL CONFORM TO THE LATEST EDITIONS OF THE FOLLOWING APPLICABLE CODES: ACI 301 "SPECIFICATIONS FOR STRUCTURAL CONCRETE FOR BUILDINGS"; ACI 318, "BUILDING CODE REQUIREMENTS FOR REINFORCED CONCRETE"
- 2. MIX DESIGN SHALL BE APPROVED BY OWNER'S REPRESENTATIVE PRIOR TO PLACING CONCRETE. PREPARE AND SUBMIT MIX DESIGNS FOR EACH TYPE AND STRENGTH OF CONCRETE IN ACCORDANCE WITH ACI 211, "PROPORTIONING CONCRETE MIXTURES, AND ACL 301. "SPECIFICATIONS FOR STRUCTURAL CONCRETE"
- 3. CONCRETE (EXCEPT TREMIE MIX) SHALL BE NORMAL WEIGHT, 6% AIR ENTRAINED (±1.5%) WITH A MAXIMUM 4" SLUMP, AND HAVE A MINIMUM 28-DAY COMPRESSIVE STRENGTH OF 3000 PSI UNLESS OTHERWISE NOTED.
- 4. MAXIMUM AGGREGATE SIZE SHALL BE 3/4".
- 5. THE FOLLOWING MATERIALS SHALL BE USED:

PORTLAND CEMENT: **REINFORCEMENT:** NORMAL WEIGHT AGGREGATE: WATER ADMIXTURES

ASTM C 150. TYPE I ASTM A 615, GRADE 60 ASTM C 33 POTABLE NON-CHLORIDE CONTAINING

- 6. REINFORCING DETAILS SHALL BE IN ACCORDANCE WITH THE LATEST EDITION OF ACI 315.
- 7. REINFORCING STEEL SHALL CONFORM TO ASTM A 615, GRADE 60, DEFORMED UNLESS NOTED OTHERWISE. WELDED WIRE FABRIC SHALL CONFORM TO ASTM A 185 WELDED STEEL WIRE FABRIC UNLESS NOTED OTHERWISE. SPLICES SHALL BE CLASS "B" AND ALL HOOKS SHALL BE STANDARD, UNO.
- 8. THE FOLLOWING MINIMUM CONCRETE COVER SHALL BE PROVIDED FOR REINFORCING STEEL UNLESS SHOWN OTHERWISE ON DRAWINGS:

CONCRETE EXPOSED TO EARTH OR WEATHER: #6 AND LARGER .2 IN

#5 AND SMALLER & WWF .... ..1 1/2 IN

CONCRETE NOT EXPOSED TO EARTH OR WEATHER OR NOT CAST AGAINST THE GROUND

- SLAB AND WALL ... 3/4 IN BEAMS AND COLUMNS ...1 1/2 IN.
- 9. A CHAMFER 1" SHALL BE PROVIDED AT ALL EXPOSED EDGES OF CONCRETE, UNO, IN ACCORDANCE WITH ACI 301 SECTION 4.2.4.
- 10. INSTALLATION OF CONCRETE EXPANSION/WEDGE ANCHOR SHALL BE PER MANUFACTURES WRITTEN RECOMMENDED PROCEDURE. THE ANCHOR BOLT, DOWEL OR ROD SHALL CONFORM TO MANUFACTURER'S RECOMMENDATION FOR EMBEDMENT DEPTH OR AS SHOWN ON THE DRAWINGS, NO REBAR SHALL BE CUT WITHOUT PRIOR ENGINEERING APPROVAL WHEN DRILLING HOLES IN CONCRETE.
- 11. CURING COMPOUNDS SHALL CONFORM TO ASTM C-309.
- 12. ADMIXTURES SHALL CONFORM TO THE APPROPRIATE ASTM STANDARD AS REFERENCED IN ACI-301
- 13. DO NOT WELD OR TACKWELD REINFORCING STEEL
- 14 ALL DOWELS ANCHOR BOLTS EMBEDDED STEEL ELECTRICAL CONDULTS PIPE SLEEVES GROUNDS AND ALL OTHER EMBEDDED ITEMS AND FORMED DETAILS SHALL BE IN PLACE BEFORE START OF CONCRETE PLACEMENT.

#### CONCRETE NOTES (CONT.)

- 15. LOCATE ADDITIONAL CONSTRUCTION JOINTS REQUIRED TO FACILITATE CONSTRUCTION AS ACCEPTABLE TO ENGINEER. PLACE REINFORCEMENT CONTINUOUSLY THROUGH JOINT.
- 16. REINFORCEMENT SHALL BE COLD BENT WHENEVER BENDING IS REQUIRED.
- 17. PLACE CONCRETE IN A UNIFORM MANNER TO PREVENT THE FORMATION OF COLD JOINTS AND OTHER PLANES OF WEAKNESS. VIBRATE THE CONCRETE TO FULLY EMBED REINFORCING. DO NOT USE VIBRATORS TO TRANSPORT CONCRETE THROUGH CHUTES OR FORMWORK
- 18. DO NOT PLACE CONCRETE IN WATER, ICE, OR ON FROZEN GROUND.
- 19. DO NOT ALLOW CONCRETE SUBBASE TO FREEZE DURING CONCRETE CURING AND SETTING PERIOD, OR FOR A MINIMUM OF 14 DAYS AFTER PLACEMENT.
- 20. FOR COLD-WEATHER AND HOT-WEATHER CONCRETE PLACEMENT, CONFORM TO APPLICABLE ACI CODES AND RECOMMENDATIONS. IN EITHER CASE, MATERIALS CONTAINING CHLORIDE, CALCIUM, SALTS, ETC. SHALL NOT BE USED. PROTECT FRESH CONCRETE FROM WEATHER FOR 7 DAYS MINIMUM.
- 21. READY-MIX CONCRETE SUPPLIERS TO BE NRMCA-CERTIFIED.

22 NO ADDITIONAL WATER SHALL BE ADDED TO THE CONCRETE AT THE JOB SITE.

23. HOT WEATHER CONCRETE: COMPLY WITH ACI 305R.

24. NO PLASTIZISOR TO BE USED IN TREMIE MIX

#### EXCAVATIONS/FOUNDATION

- 1. FOUNDATION EXCAVATION SHALL BE HAND-TRIMMED TO REMOVE LOOSE MATERIALS.
- 2. DO NOT PLACE FOOTINGS IN WATER OR ON FROZEN GROUND.
- 3. SOIL BEARING SURFACES, PREVIOUSLY ACCEPTED BY GEOTECHNICAL ENGINEER. WHICH ARE ALLOWED TO BECOME SATURATED, FROZEN OR DISTURBED SHALL BE REWORKED TO SATISFACTION OF GEOTECHNICAL ENGINEER
- 4. DO NOT ALLOW GROUND BENEATH FOOTINGS TO FREEZE.
- 5. ALL STRUCTURAL BACKFILL AND SUBBASE UNDER SLABS SHALL BE SELECT STRUCTURAL FILL MEETING THE GRADATION AND SOUNDNESS REQUIREMENTS IN ACCORDANCE WITH THE FOLLOWING GRADATION:

SEIVE SIZE 4 INCH NO. 40 NO. 200

- B. MATERIALS SHALL BE SUBSTANTIALLY FREE OF SHALE OR OTHER SOFT, POOR DURABILITY PARTICLES. IF TESTING IS ELECTED BY OWNER, MATERIAL WITH A MAGNESIUM SUIFATE SOUNDNESS LOSS EXCEEDING 30% WILL BE REJECTED
- 6. COMPACT TO 95% STANDARD PROCTOR DENSITY PER ASTM D-698.
- 7. SUBGRADE BELOW SLAB-ON-GRADE SHALL BE REVIEWED AND ACCEPTED BY GEOTECHNICAL ENGINEER BEFORE CONCRETE SLAB PLACEMENT.
- 8. ALL LOOSE AND/OR ORGANIC MATERIAL SHALL BE REMOVED PRIOR TO PREPARATION OF THE AREA FOR PLACEMENT OF STRUCTURAL BACKFILL. OVERALL PLAN AREA OF WORK SHALL EXTEND 3'-O" MINIMUM BEYOND THE FINAL DIMENSIONS.
- 9. SCARIFY THE EXISTING SOILS TO A DEPTH OF 6" AND RE-COMPACT USING A PLATE TAMPER. ANY SOFT AREAS SHALL BE OVEREXCAVATED 12" AND BACKFILLED WITH MATERIALS AND COMPACTION REQUIREMENTS SHOWN ON THE DRAWINGS.
- 10. PLACEMENT AND COMPACTION OF STRUCTURAL BACKFILL AND SUBBASE SHALL BE DONE IN 8" LIFTS. EXCAVATE FOR THE FOOTING EDGE AS SHOWN ON THE DRAWINGS.
- 11. CONTRACTOR TO GRADE SITE LEVEL WITH EXISTING, TWO FEET BEYOND PROPOSED EQUIPMENT PAD FOOTPRINT, THEN TAPER TO EXISTING GRADE IF REQUIRED AT A MAXIMUM OF 3:1 SLOPE.

#### DESIGN NOTES

MATERIALS STRUCTURAL STEEL ANGLES AND PLATES RECTANGULAR STRUCTURAL TUBING STANDARD PIPE HIGH STRENGTH BOLTS ANCHOR BOLTS WELDING ELECTRODES

CONCRETE (28 DAYS):

FOOTINGS SLAB-ON-GRADE ALL OTHER CONCRETE REINFORCING STEEL WELDED WIRE EABRIC HEADED STUDS

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