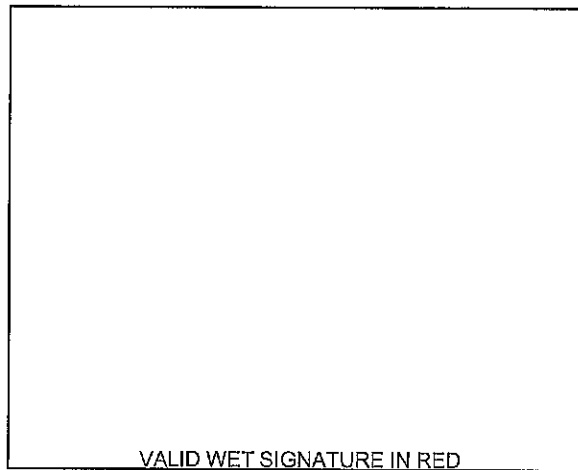


STRUCTURAL CALCULATIONS
for
WATERTOWN
at
655 BASSETT ROAD
WATERTOWN, CT 06795
for
LARSON CAMOUFLAGE (611200)



BY: **ROGER T. ALWORTH, S.E.**
PRINCIPAL

PROJECT #: **U1223-226-121**

DATE: **July 24, 2012**

NOTE: The calculations presented in this package are intended for a single use at the location indicated above, for the client listed above. These calculations shall not be reproduced, reused, "card filed", sold to a third party, or altered in any way without the written authorization of Vector Structural Engineers, PC.



JOB NO.: U1223-226-121
DATE: 07/24/12

DESIGNED: LCC
CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Design Criteria:

Code: Structural design is based on the California Building Code, 2010 Edition (2009 IBC)

Wind: Basic wind speed = 100 mph (3-second gust) per the TIA-222-G standard

Wind importance factor, $I = 1$

Structure class: II

Wind exposure: C

Topographic category: 1

Crest height: 0 ft

Ice: 1" radial ice @ 40 mph basic wind speed (3-second gust) per the TIA-222-G standard

Seismic: Seismic loads are based on the California Building Code, 2010 Edition (2009 IBC) and the TIA-222-G standard

Seismic importance factor, $I = 1$

Structure Class: II

Mapped spectral response accelerations: $S_S = 0.250442g$ $S_1 = 0.064682g$

Site class: D

Spectral response coefficients: $S_{DS} = 0.267g$ $S_{D1} = 0.103g$

Seismic design category: D

Basic seismic-force-resisting-system: Telecommunication Tower: Steel Pole

Seismic base shear, $V = 2.7 k$

Seismic response coefficient, $C_s = 0.09$

Response modification factor, $R = 1.5$

Analysis procedure: Equivalent lateral force

General Notes:

- 1 The contractor shall verify dimensions, conditions and elevations before starting work. The engineer shall be notified immediately if any discrepancies are found.
- 2 The typical notes and details shall apply in all cases unless specifically detailed elsewhere. Where no detail is shown, the construction shall be as shown for other similar work and as required by the building code.
- 3 These calculations are limited to the structural members shown in these calculations only. The connection of the members shown in these calculations to the existing structure shall be by others.
- 4 The contractor shall be responsible for compliance with local construction safety orders. Approval of shop drawings by the architect or structural engineer shall not be construed as accepting this responsibility.
- 5 All structural framing members shall be adequately shored and braced during erection and until full lateral and vertical support is provided by adjoining members.



JOB NO.: U1223-226-121
DATE: 07/24/12

DESIGNED: LCC
CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Structural Steel:

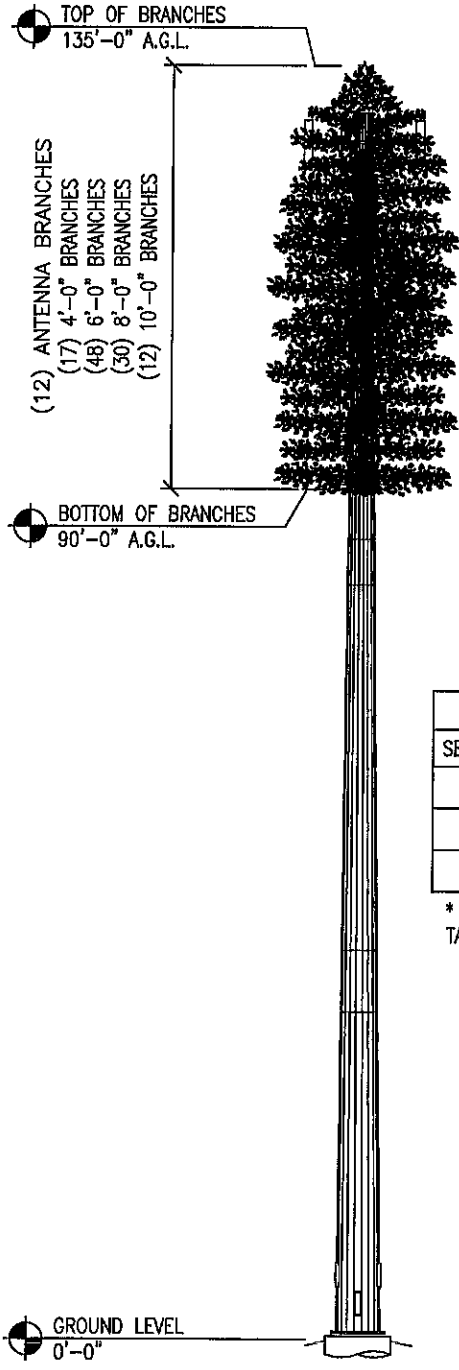
- 1 All structural steel code checks based on the AISC-LRFD, 3rd Edition per the TIA-222-G standard
- 2 All 18-sided, tapered shaft steel to be per ASTM A572 GR. 65, U.N.O.
- 3 The design length of slip splices is equal to 1.67 times the inside width of the base of the upper section. Slip splice length tolerance is equal to $\pm 10\%$ of the design slip splice length.
- 4 All other structural steel shapes & plates shall be per ASTM A36, U.N.O.
- 5 All anchor bolts shall be per ASTM A615 GR. 75, U.N.O.
- 6 All bolts for steel-to-steel connections shall be per ASTM A325N, U.N.O.
- 7 All bolted connections shall be tightened to "snug tight" condition as defined by AISC
- 8 All welding shall be performed by certified welders in accordance with the latest edition of the American Welding Society (AWS) D1.1
- 9 All steel surfaces shall be galvanized in accordance with the ASTM A123 and ASTM A153 standards, U.N.O.

Foundation / Concrete:

- 1 All concrete mixing, placement, forming, and reinforcing installation shall be performed in accordance with the requirements of "Building Code Requirements for Reinforced Concrete", ACI 318-08. Foundation installation shall be in accordance with the requirements of "Standard Specifications for the Construction of Drilled Piers", ACI 336, latest edition
- 2 All concrete shall have a minimum compressive strength of 4000 psi at 28 days.
- 3 Cement for all concrete shall be Type I or II with a minimum of 6% entrained air. Maximum aggregate size shall be $\frac{3}{4}$ ".
- 4 Reinforcing steel shall be per ASTM A615 Gr. 60, U.N.O.
- 5 Foundation design is based upon the project soils report prepared by:

Geotech: Berkshire Geo-Technologies
Date: 16-Jul-12

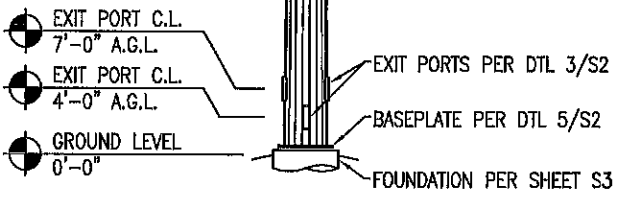
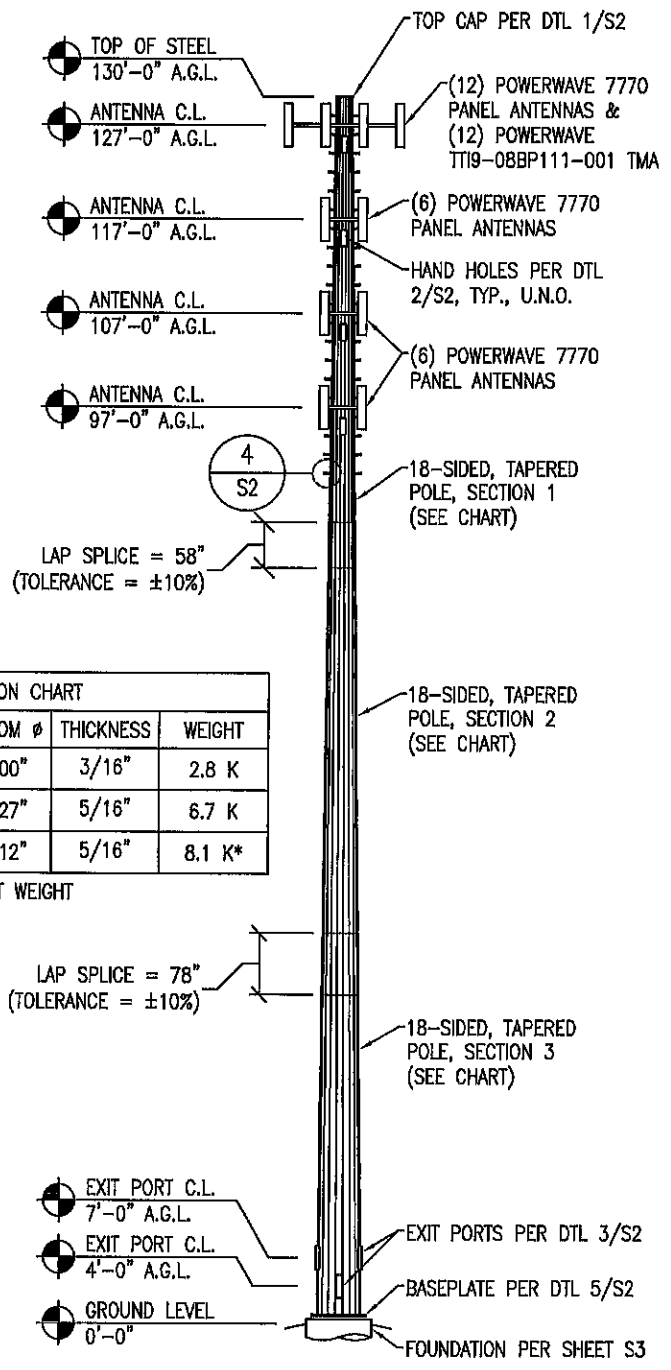
- 6 Approximate concrete volume for mat foundation = 55.4 cubic yards



BRANCHES ARE FOR ILLUSTRATIVE PURPOSES ONLY AND ARE NOT SHOWN TO SCALE.

MONOPOLE SECTION CHART					
SECTION	LENGTH	TOP ϕ	BOTTOM ϕ	THICKNESS	WEIGHT
1	50'-0"	21.00"	35.00"	3/16"	2.8 K
2	50'-0"	33.27"	47.27"	5/16"	6.7 K
3	40'-4"	44.83"	56.12"	5/16"	8.1 K*

* INCLUDES BASEPLATE & EXIT PORT WEIGHT
TAPER = 0.28 IN/FT





JOB NO.: U1223-226-121
 DATE: 07/24/12

DESIGNED: LCC
 CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Monopine Branch Layout

Eff. Area Factor:	0.84
Top Crown Radius:	5 ft
C _A Factor:	0.6
Bott. Branch Elev. (ft):	90.0 ft
Top Branch Elev. (ft):	130.0 ft

Branch Layout Along Pole:

Branch Length (ft)	Qty	Elevation		Branch Wt. (lbs)	Total Wt. (lbs)	Wind Area		
		Start (ft)	Stop (ft)			Gross (ft ²)	Eff. (ft ²)	C _{AAE} (ft ²)
4	26	121.0	130.0	26.0	676	88.4	74.2	44.5
6	24	112.3	121.0	40.0	960	115.5	97.0	58.2
6	24	104.5	112.8	40.0	960	116.3	97.7	58.6
8	15	99.3	104.5	50.0	750	93.7	78.7	47.2
8	15	94.1	99.3	60.0	750	94.0	78.9	47.4
10	12	90.0	94.1	66.0	792	91.9	77.2	46.3
Total (lbs):					4888			

Top Crown:

Branch Length (ft)	Qty	Total Wt.	Total Wt.
4	3	78	118
6	1	40	
Gross Area (ft²):		39.3	
Eff. Area (ft²):		33.0	
C_{AAE} (ft²):		19.8	

Random Branch Distribution:

Total C_{AAE} (ft²):	302.2
C_{AAE} per ft (ft²/ft):	7.56
Wt. per ft (lbs/ft):	122.2

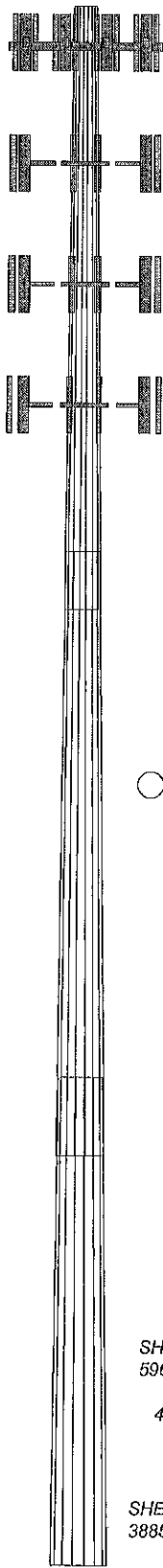
130.0 ft

Section	1	2	3
Length (ft)	50.00	50.00	40.33
Number of Sides	18	18	18
Thickness (in)	0.1875	0.3125	0.3125
Socket Length (ft)	4.83	6.50	44.8276
Top Dia (in)	21.0000	33.2726	56.1200
Bot Dia (in)	36.0000	47.2726	66.2719
Grade		A572-65	
Weight (lb)	2816.1	6743.6	6627.9
			16387.6

80.0 ft

34.8 ft

1.0 ft



DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Top Hat with (3) 4 ft, and (1) 6 ft branches	132.5	(2) Powerwave 7770.00 w/ Mount Pipe	117
(4) Powerwave 7770.00 w/ Mount Pipe	127	(24) 6 ft branches	116.9
(4) Powerwave 7770.00 w/ Mount Pipe	127	(24) 6 ft branches	108.6
12'-0" T-Arm	127	4'-0" T-Arm	107
12'-0" T-Arm	127	4'-0" T-Arm	107
12'-0" T-Arm	127	4'-0" T-Arm	107
(4) Powerwave TT19-08BP111-001 TMA	127	(2) Powerwave 7770.00 w/ Mount Pipe	107
(4) Powerwave TT19-08BP111-001 TMA	127	(2) Powerwave 7770.00 w/ Mount Pipe	107
(4) Powerwave TT19-08BP111-001 TMA	127	(15) 8 ft branches	101.9
(4) Powerwave 7770.00 w/ Mount Pipe	127	4'-0" T-Arm	97
(4) Powerwave 7770.00 w/ Mount Pipe	127	4'-0" T-Arm	97
(26) 4 ft branches	126.5	(2) Powerwave 7770.00 w/ Mount Pipe	97
(2) Powerwave 7770.00 w/ Mount Pipe	117	(2) Powerwave 7770.00 w/ Mount Pipe	97
4'-0" T-Arm	117	(2) Powerwave 7770.00 w/ Mount Pipe	97
4'-0" T-Arm	117	4'-0" T-Arm	97
4'-0" T-Arm	117	4'-0" T-Arm	97
(2) Powerwave 7770.00 w/ Mount Pipe	117	(13) 8 ft branches	96.7
		(12) 10 ft branches	92.1

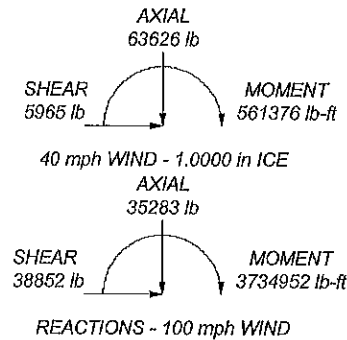
MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

TOWER DESIGN NOTES

1. Tower is located in Litchfield County, Connecticut.
2. Tower designed for Exposure C to the TIA-222-G Standard.
3. Tower designed for a 100 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.00 ft
8. TOWER RATING: 99.4%

ALL REACTIONS ARE FACTORED



<p>Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176</p>	Job:		
	Project:		
	Client:	Drawn by: Lindsey Cahoon	App'd:
	Code: TIA-222-G	Date: 07/24/12	Scale: NTS
	Path:	Dwg No. E-1	

maxTower		Job	Page
Vector Structural Engineers 9128 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 Fax: 801-990-1176		Project	1 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	

Tower Input Data

There is a pole section.
 This tower is designed using the TIA-222-G standard.
 The following design criteria apply:
 Tower is located in Litchfield County, Connecticut.
 Basic wind speed of 100 mph.
 Structure Class II.
 Exposure Category C.
 Topographic Category I.
 Crest Height 0.00 ft.
 Nominal ice thickness of 1.0000 in.
 Ice thickness is considered to increase with height.
 Ice density of 56 pcf.
 A wind speed of 40 mph. is used in combination with ice.
 Temperature drop of 50 °F.
 Deflections calculated using a wind speed of 60 mph.
 A non-linear (P-delta) analysis was used.
 Pressures are calculated at each section.
 Stress ratio used in pole design is 1.
 Local bending stresses due to climbing loads, feedline supports, and appearance mounts are not considered.

Options

- Consider Moments - Legs
- Consider Moments - Horizontals
- Use Moment Magnification
- Use Code Stress Ratios
- Use Code Safety Factors - Gyps
- Escape Ice
- Always Use Max Kz
- Use Wind Profile
- Use Safety Factor In
- Leg Bolts Are At Top Of Section
- Secondary Horizontal Brace Leg
- Use Diamond Inner Bracing (4 Sides)
- Add IBC 6D-W Combination
- Distribute Leg Loads As Uniform
- Assume Legs Pinned
- Use ASCE 10 X-Brac Ly Rules
- Calculate Redundant Bracing Forces
- Ignore Redundant Members In FEA
- SR Leg Bolts Resist Compression
- All Leg Panels Have Same Allowable
- Other Girt At Foundation
- Consider Feedline Torque
- Include Angle Block Shear Check
- Include Shear Tension Interaction
- Ways Use 8D-4 Critical Flow
- Use Top Mounted Sockets

Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
L1	130.00-80.00	50.00	4.85	18	21.0000	35.0000	0.1875	0.7500	A572-65 (65 lbs)
L2	80.00-34.83	50.00	6.50	18	33.2726	47.2736	0.3125	1.2500	A572-65 (65 lbs)
L3	34.83-1.00	40.33		18	44.8276	56.1200	0.3125	1.2500	A572-65

maxTower		Job	Page
Vector Structural Engineers 9128 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 Fax: 801-990-1176		Project	2 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
L1	130.00-80.00	50.00	4.85	18	21.0000	35.0000	0.1875	0.7500	A572-65 (65 lbs)
L2	80.00-34.83	50.00	6.50	18	33.2726	47.2736	0.3125	1.2500	A572-65 (65 lbs)
L3	34.83-1.00	40.33		18	44.8276	56.1200	0.3125	1.2500	A572-65 (65 lbs)

Tapered Pole Properties

Section	Tip Dia.	Area	I	f	C	Z/C	J	I/Q	w	w/I
L1	21.3240	12.3860	677.8263	7.3884	10.6680	65.5383	1556.5444	6.1942	3.3660	17.952
L2	35.5399	20.7178	3172.1322	12.3384	17.7800	178.4101	6348.4384	10.5609	5.8300	31.093
L3	48.0019	46.5785	12977.2130	16.6708	24.0145	540.3912	25971.5018	23.2957	7.7700	24.864
	47.3672	44.1534	11053.9235	15.8029	21.7724	485.4084	23122.3920	22.0809	7.3397	23.487
	56.9857	55.5541	21780.7133	19.8117	28.5069	763.9954	45590.0862	27.6823	9.3271	29.847

Tower Elevation	Gusset Area	Gusset Thickness	Adjust. Factor	Weight	Double Angle Spacing	Double Angle Spacing	Double Angle Spacing
L1	130.00-80.00	in	1	1	in	in	in
L2	80.00-34.83	in	1	1	in	in	in
L3	34.83-1.00	in	1	1	in	in	in

Monopole Base Plate Data

Base Plate Data	Base Plate Data
Base plate is square	Base plate is square
Base plate is grouted	Base plate is grouted
Anchor bolt grade	A615-75
Number of bolts	27500 m
Embedment length	72.0000 in
Grout space	6 in
Base plate grade	3.0000 in
Base plate thickness	4.572-50
Bolt circle diameter	2.5000 in
Outer diameter	65.5000 in
Inner diameter	60.0000 in
Base plate type	Plain Plate

Feed Line/Linear Appurtenances - Entered As Area

Description	Face Allow	Component Type	Placement	Total Number	C _{4,4}	W/B	Height
AV47-50 (L-58 LOW DENSIT. FOAM)	C No	Inside Pole	127.00 - 1.00	24	No Ice	0.00	0.72
					12" Ice	0.00	0.72
					1" Ice	0.00	0.72

tnxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	3 of 24
Client		Data	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Description	Face Allow or Shield	Component Type	Placement	Total Number	C.A.A.	Weight
					f^2/f	pl
AVA7-50 (1-5/8 LOW DENSIL FOAM)	C	No	Inside Pole	12	0.00	0.72
AVA7-50 (1-5/8 LOW DENSIL FOAM)	C	No	Inside Pole	12	0.00	0.72
AVA7-50 (1-5/8 LOW DENSIL FOAM)	C	No	Inside Pole	12	0.00	0.72
AVA7-50 (1-5/8 LOW DENSIL FOAM)	C	No	Inside Pole	12	0.00	0.72

Feed Line/Linear Appurtenances Section Areas

Tower Section	Elevation	Face	A _k	A _r	A _r	C.A.A.	C.A.A.	Weight
	f		f^2	f^2	f^2	In Face	Out Face	lb
L1	130.00-80.00	A	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	1512.00
L2	80.00-54.83	A	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	1951.34
L3	34.83-1.00	A	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	1463.46

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Elevation	Face or Leg	Ice Thickness	A _k	A _r	A _r	C.A.A.	C.A.A.	Weight
	f		t	f^2	f^2	f^2	In Face	Out Face	lb
L1	130.00-80.00	A	2.342	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.000	1512.00
L2	80.00-54.83	A	2.111	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.000	1951.34
L3	34.83-1.00	A	1.881	0.000	0.000	0.000	0.000	0.000	0.00
		B	0.000	0.000	0.000	0.000	0.000	0.000	0.00
		C	0.000	0.000	0.000	0.000	0.000	0.000	1463.46

Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K _c No. Ice	K _c Ice

User Defined Loads

Description	Elevation	Offset From Convoid	Weight	F _x	F _y	Wind Force	C.A.C.
	f	f	lb	lb	lb	lb	f^2
(12) 10 ft branches	92.10	0.00	792.00	0.00	0.00	0.00	1540.69
			871.20	0.00	0.00	0.00	271.53
			792.00	0.00	0.00	0.00	496.27
(15) 8 ft branches	96.70	0.00	750.00	0.00	0.00	0.00	1593.56
			825.00	0.00	0.00	0.00	280.25
			750.00	0.00	0.00	0.00	513.39
(15) 8 ft branches	101.50	0.00	750.00	0.00	0.00	0.00	1684.43
			825.00	0.00	0.00	0.00	282.27
			750.00	0.00	0.00	0.00	516.80
(24) 6 ft branches	108.60	0.00	750.00	0.00	0.00	0.00	208.83
			825.00	0.00	0.00	0.00	381.60
			750.00	0.00	0.00	0.00	58.60
(24) 6 ft branches	116.90	0.00	750.00	0.00	0.00	0.00	208.83
			825.00	0.00	0.00	0.00	381.60
			750.00	0.00	0.00	0.00	58.60
(26) 4 ft branches	125.50	0.00	676.00	0.00	0.00	0.00	158.07
			743.60	0.00	0.00	0.00	278.45
			676.00	0.00	0.00	0.00	44.50
Top Hat with (3) 4 ft, and (1) 6 ft branches	132.50	0.00	676.00	0.00	0.00	0.00	158.07
			743.60	0.00	0.00	0.00	278.45
			676.00	0.00	0.00	0.00	44.50
			118.00	0.00	0.00	0.00	711.30
			129.80	0.00	0.00	0.00	125.30
			118.00	0.00	0.00	0.00	229.11

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offset Horiz	Offset Lateral	Asymeth Adjustment	Placement	C.A.A. Front	C.A.A. Side	Weight
			f	f	f	f	f^2	f^2	lb
(4) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
(4) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
(4) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
12'-0" T-Arm	A	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
12'-0" T-Arm	B	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
12'-0" T-Arm	C	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
(4) Powerwave TT19-08B7111-001 TMA	A	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48
(4) Powerwave TT19-08B7111-001 TMA	B	From Face	3.00	0.00	0.0000	127.00	6.25	4.38	60.90
			3.00	0.00	0.0000	127.00	6.80	5.23	107.22
			3.00	0.00	0.0000	127.00	7.33	5.95	165.48

maxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	5 of 24
Client		Date	09:00:11 07/24/12
		Designed by	Lindsey Cahoon

maxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	6 of 24
Client		Date	09:00:11 07/24/12
		Designed by	Lindsey Cahoon

Description	Face or Leg	Offset	Offset	Astmsh	Placement	C.A.A. Front	C.A.A. Side	Weight	Placement	
									From Face	To Face
(1) Powerwave 1119-885T111-001 TMA	C	From Face	3.00	0.0000	127.00	0.64	0.52	16.00	f	l_b
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	117.00	0.88	0.62	21.80	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	117.00	6.25	5.38	29.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	117.00	7.33	5.85	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	117.00	6.25	4.38	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	117.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	117.00	7.33	5.85	107.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	117.00	6.25	4.38	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	117.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	117.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	107.00	6.80	5.23	107.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	107.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	107.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	107.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	107.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	107.00	7.33	5.85	107.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	97.00	6.25	4.38	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	97.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	97.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	97.00	7.33	5.85	107.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	97.00	6.25	4.38	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	97.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	97.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	97.00	7.33	5.85	107.22	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	97.00	6.25	4.38	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	A	From Face	3.00	0.0000	97.00	7.33	5.85	163.48	f	
(2) Powerwave 7770.00 w/ Mount Pipe	B	From Face	3.00	0.0000	97.00	6.80	5.23	60.90	f	
(2) Powerwave 7770.00 w/ Mount Pipe	C	From Face	3.00	0.0000	97.00	7.33	5.85	107.22	f	

Tower Pressures - No Ice

$G_H = L100$

Section Elevation	z	K_z	q_t	A_g	F	A_r	A_k	A_{kg}	Leg %	$C_A A_s$ In	$C_A A_s$ Out	$C_A A_s$ Face
L1 130.00-80.00	103.23	1.274	31	118.466	A	0.000	118.466	100.00	100.00	0.000	0.000	0.000
L2 80.00-34.83	56.73	1.123	27	156.516	A	0.000	156.516	100.00	100.00	0.000	0.000	0.000
L3 34.83-1.00	17.89	0.881	22	147.094	A	0.000	147.094	100.00	100.00	0.000	0.000	0.000

Tower Pressure - With Ice

$G_H = L100$

Section Elevation	z	K_z	q_t	t_z	in	if	A_r	A_s	Leg %	$C_A A_s$ In	$C_A A_s$ Out	$C_A A_s$ Face
L1 130.00-80.00	103.23	1.274	31	2.2416	5	137.146	0.000	137.146	100.00	0.000	0.000	0.000
L2 80.00-34.83	56.73	1.123	27	2.1113	4	173.391	0.000	173.391	100.00	0.000	0.000	0.000
L3 34.83-1.00	17.89	0.881	22	1.8812	4	158.999	0.000	158.999	100.00	0.000	0.000	0.000

Tower Pressure - Service

$G_H = L100$

Section Elevation	z	K_z	q_t	A_g	F	A_r	A_k	A_{kg}	Leg %	$C_A A_s$ In	$C_A A_s$ Out	$C_A A_s$ Face
L1 130.00-80.00	103.23	1.274	10	118.466	A	0.000	118.466	100.00	100.00	0.000	0.000	0.000
L2 80.00-34.83	56.73	1.123	9	156.516	A	0.000	156.516	100.00	100.00	0.000	0.000	0.000

inxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandusky, MI Phone: 801-990-1175 Fax: 801-990-1176		Project	7 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	2316.14	6743.56	6827.95	16387.65
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	31	27	22	
D _r		1	1	1	OTM
A _r	ft ²	118.466	156.516	147.094	476184.71
A _s	lb-ft	2619.89	3041.51	2302.12	7963.52
W	plf	52.40	67.33	68.05	
Crit. Face		C	C	C	

Tower Forces - No Ice - Wind Normal To Face

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	2316.14	6743.56	6827.95	16387.65
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	31	27	22	
D _r		1	1	1	OTM
A _r	ft ²	118.466	156.516	147.094	476184.71
A _s	lb-ft	2619.89	3041.51	2302.12	7963.52
W	plf	52.40	67.33	68.05	
Crit. Face		C	C	C	

Tower Forces - No Ice - Wind 60 To Face

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	2316.14	6743.56	6827.95	16387.65
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	31	27	22	
D _r		1	1	1	OTM
A _r	ft ²	118.466	156.516	147.094	476184.71
A _s	lb-ft	2619.89	3041.51	2302.12	7963.52
W	plf	52.40	67.33	68.05	
Crit. Face		C	C	C	

Tower Forces - No Ice - Wind 90 To Face

inxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandusky, MI Phone: 801-990-1175 Fax: 801-990-1176		Project	8 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	2316.14	6743.56	6827.95	16387.65
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	31	27	22	
D _r		1	1	1	OTM
A _r	ft ²	118.466	156.516	147.094	476184.71
A _s	lb-ft	2619.89	3041.51	2302.12	7963.52
W	plf	52.40	67.33	68.05	
Crit. Face		C	C	C	

Tower Forces - With Ice - Wind Normal To Face

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	6999.87	11812.46	11012.09	29824.43
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	5	4	4	
D _r		1	1	1	OTM
A _r	ft ²	1371.146	173.391	158.999	159459.09
A _s	lb-ft	895.90	995.28	753.04	2626.23
W	plf	17.92	22.03	21.73	
Crit. Face		C	C	C	

Tower Forces - With Ice - Wind 60 To Face

Section Elevation	f	L1	L2	L3	Sum Weight:
Self Weight	lb	6999.87	11812.46	11012.09	29824.43
Add Weight	lb	1512.00	1951.34	1461.46	4924.80
F _a		1	1	1	1
F _b		1	1	1	1
F _c		1	1	1	1
F _e		1	1	1	1
C _r	psf	5	4	4	
D _r		1	1	1	OTM
A _r	ft ²	1371.146	173.391	158.999	159459.09
A _s	lb-ft	895.90	995.28	753.04	2626.23
W	plf	17.92	22.03	21.73	
Crit. Face		C	C	C	

inxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandys, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	9 of 24
Client		Date	09:00:11 07/24/12
Designed by Lindsey Cahoon			

Tower Forces - With Ice - Wind 90 To Face

Section Elevation	f	Add Weight	Self Weight	F _a	e	C _r	q _r	D _r	D _h	A _s	F	w	Crit. Face
		lb	lb	c			psf			ft ²	lb	p/ft	
L1	130.00-80.00	1512.00	6999.87	A	1	1.2	5	1	1	137.146	893.90	17.92	C
L2	80.00-34.85	1951.34	11812.46	B	1	1.2	4	1	1	137.146	995.28	22.03	C
L3	34.83-1.00	1461.46	11012.09	C	1	1.2	4	1	1	175.391	735.04	21.73	C
Sum Weight:		4924.80	29824.43						OTM	159439.09	2656.23		

Tower Forces - Service - Wind Normal To Face

Section Elevation	f	Add Weight	Self Weight	F _a	e	C _r	q _r	D _r	D _h	A _s	F	w	Crit. Face
		lb	lb	c			psf			ft ²	lb	p/ft	
L1	130.00-80.00	1512.00	2316.14	A	1	0.65	10	1	1	118.466	843.88	16.88	C
L2	80.00-34.85	1951.34	6743.56	B	1	0.65	9	1	1	118.466	979.69	21.69	C
L3	34.83-1.00	1461.46	6827.95	C	1	0.65	7	1	1	156.516	741.52	21.92	C
Sum Weight:		4924.80	16387.63						OTM	155381.60	2565.09		

Tower Forces - Service - Wind 60 To Face

Section Elevation	f	Add Weight	Self Weight	F _a	e	C _r	q _r	D _r	D _h	A _s	F	w	Crit. Face
		lb	lb	c			psf			ft ²	lb	p/ft	
L1	130.00-80.00	1512.00	2316.14	A	1	0.65	10	1	1	118.466	843.88	16.88	C
L2	80.00-34.85	1951.34	6743.56	B	1	0.65	9	1	1	118.466	979.69	21.69	C
L3	34.83-1.00	1461.46	6827.95	C	1	0.65	7	1	1	156.516	741.52	21.92	C
Sum Weight:		4924.80	16387.63						OTM	155381.60	2565.09		

inxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandys, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	10 of 24
Client		Date	09:00:11 07/24/12
Designed by Lindsey Cahoon			

Section Elevation	f	Add Weight	Self Weight	F _a	e	C _r	q _r	D _r	D _h	A _s	F	w	Crit. Face
		lb	lb	c			psf			ft ²	lb	p/ft	
L3	34.83-1.00	1461.46	6827.95	A	1	0.65	7	1	1	147.094	741.52	21.92	C
L2	80.00-34.85	1951.34	6743.56	B	1	0.65	9	1	1	147.094	979.69	21.69	C
L3	34.83-1.00	1461.46	6827.95	C	1	0.65	7	1	1	153381.60	2565.09		
Sum Weight:		4924.80	16387.63						OTM	153381.60	2565.09		

Tower Forces - Service - Wind 90 To Face

Section Elevation	f	Add Weight	Self Weight	F _a	e	C _r	q _r	D _r	D _h	A _s	F	w	Crit. Face
		lb	lb	c			psf			ft ²	lb	p/ft	
L1	130.00-80.00	1512.00	2316.14	A	1	0.65	10	1	1	118.466	843.88	16.88	C
L2	80.00-34.85	1951.34	6743.56	B	1	0.65	9	1	1	118.466	979.69	21.69	C
L3	34.83-1.00	1461.46	6827.95	C	1	0.65	7	1	1	156.516	741.52	21.92	C
Sum Weight:		4924.80	16387.63						OTM	153381.60	2565.09		

Force Totals

Load Case	Vertical Forces	Sum of Forces X	Sum of Forces Y	Sum of Overturning Moments M _x	Sum of Overturning Moments M _y	Sum of Torques
	lb	lb	lb	lb-ft	lb-ft	lb-ft
Leg Weight	16387.63			0.00	0.00	
Brace Weight	0.00			0.00	0.00	
Total Member Self-Weight	16387.63			0.00	0.00	
Total Weight	29402.43			0.00	0.00	
Wind 0 deg - No Ice		0.00	-24283.00	-2777142.37	0.00	0.00
Wind 90 deg - No Ice		24283.00	0.00	2777142.37	-2277142.37	0.00
Wind 180 deg - No Ice		0.00	24283.00	2777142.37	0.00	0.00
Member Ice	13436.60			0.00	0.00	
Total Weight-ice	55997.72			0.00	0.00	
Wind 0 deg - Ice		0.00	-5965.42	-530412.40	0.00	0.00
Wind 90 deg - Ice		5965.42	0.00	530412.40	-530412.40	0.00
Wind 180 deg - Ice		0.00	5965.42	530412.40	0.00	0.00
Total Weight-ice	29402.43			0.00	0.00	
Wind 0 deg - Service		0.00	-7821.68	-733470.00	0.00	0.00
Wind 90 deg - Service		7821.68	0.00	733470.00	-733470.00	0.00
Wind 180 deg - Service		0.00	7821.68	733470.00	0.00	0.00

maxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	11 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice
3	0.9 Dead+1.6 Wind 0 deg - No Ice
4	1.2 Dead+1.6 Wind 90 deg - No Ice
5	0.9 Dead+1.6 Wind 90 deg - No Ice
6	1.2 Dead+1.6 Wind 180 deg - No Ice
7	0.9 Dead+1.6 Wind 180 deg - No Ice
8	1.2 Dead+1.0 Ice+1.0 Temp
9	0.9 Dead+1.0 Ice+1.0 Temp
10	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
11	0.9 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp
12	Dead+Wind 0 deg - Service
13	Dead+Wind 90 deg - Service
14	Dead+Wind 180 deg - Service

Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial lb	Major Axis Moment lb-ft	Minor Axis Moment lb-ft
L1	130 - 80	Pole	Max. Tension	1	0.00	0.00	0.00
			Max. Compression	8	-31665.90	-800243.56	-0.00
			Max. Mx	4	-12003.06	-800243.56	-0.00
			Max. My	6	-12003.06	-800243.56	-0.00
			Max. Vy	4	30826.71	-800243.56	-0.00
			Max. Vx	6	30826.71	-800243.56	-0.00
L2	80 - 34.83	Pole	Max. Tension	1	0.00	0.00	0.00
			Max. Compression	8	-4457.09	-22557.94	-0.00
			Max. Mx	2	-22557.94	-22557.94	0.00
			Max. My	4	35230.36	-22557.94	0.00
			Max. Vy	2	-35230.36	-22557.94	0.00
			Max. Vx	2	-35230.36	0.00	0.00
L3	34.83 - 1	Pole	Max. Tension	1	0.00	0.00	0.00
			Max. Compression	8	-6326.15	-3744951.8	0.00
			Max. Mx	4	-35253.14	-3744951.8	0.00
			Max. My	2	-35253.14	0.00	3744951.87
			Max. Vy	4	38878.01	-3744951.8	0.00
			Max. Vx	2	-38878.01	0.00	3744951.87

Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal X lb	Horizontal Z lb
Pole	Max. Vert	8	6326.15	0.00	0.00
	Max. H	14	29402.41	-7820.59	0.00
	Max. H	3	26462.12	0.00	38851.61

maxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	12 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Location	Condition	Gov. Load Comb.	Vertical lb	Horizontal X lb	Horizontal Z lb
	Max. Mx	2	3754951.87	0.00	38851.08
	Max. My	4	-38851.08	-38851.08	0.00
	Max. Tension	10	0.00	-5964.86	0.00
	Min. Vert	5	26462.12	-38851.61	0.00
	Min. H	7	26462.12	0.00	0.00
	Min. H	5	26462.12	0.00	-38851.61
	Min. Mx	6	-3754951.87	0.00	0.00
	Min. My	1	0.00	0.00	-38851.08
	Min. Tension	1	0.00	0.00	0.00

Tower Mast Reaction Summary

Load Combination	Vertical lb	Shear lb	Overturning Moment, Mx lb-ft	Overturning Moment, My lb-ft	Torque lb-ft
Dead Only	29402.43	0.00	0.00	0.00	0.00
1.2 Dead+1.6 Wind 0 deg - No Ice	35282.81	0.00	-38851.08	-3734951.87	0.00
0.9 Dead+1.6 Wind 0 deg - No Ice	26462.12	0.00	-38851.61	-3710118.76	0.00
1.2 Dead+1.6 Wind 90 deg - No Ice	35282.81	38851.08	0.00	0.00	-3754951.87
0.9 Dead+1.6 Wind 90 deg - No Ice	26462.12	38851.61	0.00	0.00	-3710118.76
1.2 Dead+1.6 Wind 180 deg - No Ice	35282.81	0.00	38851.08	3734951.87	0.00
0.9 Dead+1.6 Wind 180 deg - No Ice	26462.12	0.00	38851.61	3710118.76	0.00
1.2 Dead+1.0 Ice+1.0 Temp	6326.15	0.00	0.00	0.00	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	6326.14	0.00	-56175.91	0.00	0.00
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	6326.14	5964.86	0.00	0.00	-56175.91
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp	6326.14	0.00	5964.86	56175.91	0.00
Dead+Wind 0 deg - Service	29402.41	0.00	-7820.59	-749634.74	0.00
Dead+Wind 90 deg - Service	29402.41	7820.59	0.00	0.00	-749634.74
Dead+Wind 180 deg - Service	29402.41	0.00	7820.59	749634.74	0.00

Solution Summary

Load Comb.	PX lb	PY lb	PZ lb	Sum of Applied Forces	PX lb	PY lb	PZ lb	Sum of Reactions	% Error
1	0.00	0.00	0.00	29402.43	0.00	0.00	0.00	29402.43	0.000%
2	0.00	0.00	-38852.79	35282.81	0.00	0.00	38851.08	38851.08	0.000%
3	0.00	0.00	-38852.79	26462.12	0.00	0.00	38851.61	38851.61	0.000%
4	38852.79	-35282.81	0.00	-38851.08	-38851.08	35282.81	0.00	0.000%	
5	38852.79	-35282.81	0.00	-38851.61	-38851.61	35282.81	0.00	0.000%	
6	0.00	0.00	38852.79	26462.12	0.00	0.00	-38851.08	-38851.08	0.000%
7	0.00	0.00	38852.79	26462.12	0.00	0.00	-38851.61	-38851.61	0.000%
8	0.00	0.00	-26462.18	0.00	0.00	0.00	6326.15	6326.15	0.000%
9	0.00	0.00	-5964.86	0.00	0.00	0.00	5964.86	5964.86	0.000%
10	5964.86	-5964.86	0.00	-6326.15	0.00	0.00	6326.14	6326.14	0.001%

taxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	13 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Load Comb.	Converged?	Number of Cycles	Force Tolerance	Displacement Tolerance	Sum of Applied Forces	Sum of Reactions	FZ lb	FY lb	FZ lb	FY lb	% Error
1	Yes	6	0.00000001	0.00000001							
2	Yes	11	0.00003711	0.00008812							0.001%
3	Yes	11	0.00009901	0.00009949							0.004%
4	Yes	11	0.00009901	0.00009949							0.004%
5	Yes	11	0.00009901	0.00009949							0.004%
6	Yes	11	0.00009901	0.00009949							0.004%
7	Yes	11	0.00009901	0.00009949							0.004%
8	Yes	11	0.00009901	0.00009949							0.004%
9	Yes	11	0.00009901	0.00009949							0.004%
10	Yes	11	0.00009901	0.00009949							0.004%
11	Yes	11	0.00009901	0.00009949							0.004%
12	Yes	10	0.00009901	0.00009949							0.004%
13	Yes	10	0.00009901	0.00009949							0.004%
14	Yes	10	0.00009901	0.00009949							0.004%

Non-Linear Convergence Results

Load Combination	Converged?	Number of Cycles	Force Tolerance	Displacement Tolerance	Sum of Applied Forces	Sum of Reactions	FZ lb	FY lb	FZ lb	FY lb	% Error
1	Yes	6	0.00000001	0.00000001							
2	Yes	11	0.00003711	0.00008812							0.001%
3	Yes	11	0.00009901	0.00009949							0.004%
4	Yes	11	0.00009901	0.00009949							0.004%
5	Yes	11	0.00009901	0.00009949							0.004%
6	Yes	11	0.00009901	0.00009949							0.004%
7	Yes	11	0.00009901	0.00009949							0.004%
8	Yes	11	0.00009901	0.00009949							0.004%
9	Yes	11	0.00009901	0.00009949							0.004%
10	Yes	11	0.00009901	0.00009949							0.004%
11	Yes	11	0.00009901	0.00009949							0.004%
12	Yes	10	0.00009901	0.00009949							0.004%
13	Yes	10	0.00009901	0.00009949							0.004%
14	Yes	10	0.00009901	0.00009949							0.004%

Maximum Tower Deflections - Service Wind

Section No.	Elevation	Horiz. Deflection	Tilt	Twist
L1	130 - 80	18.100	1.2386	0.0000
L2	84.83 - 34.83	7.559	0.8603	0.0000
L3	41.33 - 1	1.747	0.3935	0.0000

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appearance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
132.50	Top Hat with (3) 4 ft. and (1) 6 ft. branches	12	18.100	1.2386	0.0000	39342
127.00	(4) Powerwave 7770.00 w/ Mount	12	17.338	1.2156	0.0000	39342
125.50	Pipe	12	16.998	1.2041	0.0000	39342
117.00	(2) Powerwave 7770.00 w/ Mount	12	14.819	1.1382	0.0000	15131
116.90	Pipe	12	14.794	1.1374	0.0000	15016
108.60	(2) Powerwave 7770.00 w/ Mount	12	12.762	1.0711	0.0000	9191
107.00	Pipe	12	12.379	1.0581	0.0000	8852

taxTower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	14 of 24
Client		Date	09:00:11 07/24/12
Lindsey Cahoon		Designed by	Lindsey Cahoon

Elevation	Appearance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
101.90	Pipe	12	11.185	1.0155	0.0000	6999
97.00	(2) Powerwave 7770.00 w/ Mount	12	10.080	0.9731	0.0000	5960
96.70	Pipe	12	10.014	0.9705	0.0000	5966
92.10	(12) 10 ft. branches	12	9.023	0.9791	0.0000	5189

Maximum Tower Deflections - Design Wind

Section No.	Elevation	Horiz. Deflection	Tilt	Twist
L1	130 - 80	90.105	6.1718	0.0000
L2	84.83 - 34.83	37.658	4.2876	0.0000
L3	41.33 - 1	8.704	1.9614	0.0000

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appearance	Gov. Load Comb.	Deflection	Tilt	Twist	Radius of Curvature
132.50	Top Hat with (3) 4 ft. and (1) 6 ft. branches	4	90.105	6.1718	0.0000	8051
127.00	(4) Powerwave 7770.00 w/ Mount	4	86.313	6.0572	0.0000	8051
125.50	Pipe	4	84.430	5.9999	0.0000	8051
117.00	(2) Powerwave 7770.00 w/ Mount	4	73.782	5.6717	0.0000	3095
116.90	Pipe	4	73.658	5.6678	0.0000	3071
108.60	(2) Powerwave 7770.00 w/ Mount	4	63.347	5.3379	0.0000	1878
107.00	Pipe	4	61.644	5.2727	0.0000	1747
101.90	(15) 8 ft. branches	4	55.703	5.0606	0.0000	1628
97.00	(2) Powerwave 7770.00 w/ Mount	4	50.208	4.8497	0.0000	1215
96.70	Pipe	4	49.873	4.8356	0.0000	1204
92.10	(12) 10 ft. branches	4	44.943	4.6306	0.0000	1057

Base Plate Design Data

Plate Thickness	Number of Bolts	Anchor Size	Actual Allowable Ratio	Actual Allowable Ratio	Actual Allowable Ratio	Condition
in	in	in	Ratio	Ratio	Ratio	Ratio
2.5000	14	2.2500	194088.02	199124.18	37.341	Bolt T 0.87
			222654.40	371266.50	45.000	

inx Tower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandh, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	15 of 24
Client		Date	09:00:11 07/24/12
		Designed by	Lindsey Cahoon

Plate Thickness	Number of Anchor Bolts	Anchor Bolt Size	Actual Allowable Ratio	Actual Allowable Ratio	Actual Allowable Ratio	Controlling Condition	Ratio
in	in	lb	lb	lb	lb	Stress	
			Compression	Plate	Stiffener	Stress	
			lb	lb	lb	Stress	
			0.87	0.54	0.83		✓

Compression Checks

Pole Design Data

Section No.	Elevation	Size			K/Lr	A	I _b	P _a	φ _p	Ratio
		L	L _c	L _r						
L1	130 - 127.623	50.00	0.00	0.0	12.7822	-208.50	915151.00	0.000		
	127.623 - 125.245				13.1783	-2417.66	934498.00	0.003		
	125.245 - 122.868				13.5745	-2616.74	953921.00	0.003		
	122.868 - 120.491				13.9706	-2821.17	972519.00	0.003		
	120.491 - 118.115				14.3668	-3030.94	990994.00	0.003		
	118.115 - 115.738				14.7630	-3240.82	1008140.00	0.004		
	115.738 - 113.362				15.1591	-3450.70	1025170.00	0.005		
	113.362 - 110.986				15.5553	-3660.58	1041670.00	0.005		
	110.986 - 108.610				15.9514	-3870.46	1057650.00	0.005		
	108.610 - 106.234				16.3476	-4080.34	1073110.00	0.006		
	106.234 - 103.858				16.7437	-4290.22	1088040.00	0.006		
	103.858 - 101.482				17.1399	-4500.10	1102440.00	0.007		
	101.482 - 99.106				17.5360	-4710.00	1116320.00	0.007		
	99.106 - 96.730				17.9322	-4920.00	1129680.00	0.008		
	96.730 - 94.354				18.3283	-5130.00	1142520.00	0.009		
	94.354 - 91.978				18.7245	-5340.00	1154830.00	0.009		
	91.978 - 89.602				19.1206	-5550.00	1166610.00	0.010		
	89.602 - 87.226				19.5168	-5760.00	1177870.00	0.010		
	87.226 - 84.850				19.9129	-5970.00	1188610.00	0.010		
	84.850 - 82.474				20.3090	-6180.00	120000.00	0.004		
	82.474 - 80.098				20.7051	-6390.00	121190.00	0.003		
	80.098 - 77.722				21.1012	-6600.00	122430.00	0.006		
	77.722 - 75.346				21.4973	-6810.00	123720.00	0.006		
L2	TP47.2726x33.2726x0.3125	50.00	0.00	0.0	40.33	0.00	40.33	0.00	0.0	
	80 - 77.8317				41.33 - 34.83					
	77.8317 - 75.7033				41.33 - 34.83					

inx Tower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandh, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	16 of 24
Client		Date	09:00:11 07/24/12
		Designed by	Lindsey Cahoon

Section No.	Elevation	Size			K/Lr	A	I _b	P _a	φ _p	Ratio
		L	L _c	L _r						
	75.7033 - 73.555				35.8236	-14703.00	2577990.00	0.006		
	73.555 - 71.4067				36.4203	-15182.90	2587530.00	0.006		
	71.4067 - 69.2583				37.0169	-15669.50	2616640.00	0.006		
	69.2583 - 67.11				37.6136	-16162.60	2646330.00	0.006		
	67.11 - 64.9617				38.2102	-16662.00	2676590.00	0.006		
	64.9617 - 62.8133				38.8069	-17167.80	2707420.00	0.006		
	62.8133 - 60.665				39.4035	-17679.80	2728820.00	0.006		
	60.665 - 58.5167				40.0002	-18198.00	2750800.00	0.007		
	58.5167 - 56.3683				40.5968	-18722.30	2782340.00	0.007		
	56.3683 - 54.22				41.1935	-19252.60	2808460.00	0.007		
	54.22 - 52.0717				41.7901	-19788.80	2834160.00	0.007		
	52.0717 - 49.9233				42.3868	-20331.00	2859420.00	0.007		
	49.9233 - 47.775				42.9834	-20879.00	2884250.00	0.007		
	47.775 - 45.6267				43.5800	-21432.90	2908660.00	0.007		
	45.6267 - 43.4783				44.1767	-21992.50	2932640.00	0.007		
	43.4783 - 41.33				44.7733	-22557.90	2956190.00	0.008		
L3	41.33 - 34.83				45.3785	-23128.30	3024640.00	0.004		
	34.83 - 33.0995				45.9836	-23699.10	3001710.00	0.004		
	33.0995 - 31.2689				46.4531	-25879.70	3020300.00	0.009		
	31.2689 - 29.4384				46.9476	-26566.70	3038400.00	0.009		
	29.4384 - 27.6079				47.4421	-26861.50	3056500.00	0.009		
	27.6079 - 25.7774				47.9366	-27358.20	3073910.00	0.009		
	25.7774 - 24.1468				48.4311	-27858.50	3091220.00	0.009		
	24.1468 - 22.3163				48.9256	-28362.70	3108250.00	0.009		
	22.3163 - 20.4858				49.4201	-28870.60	3124970.00	0.009		
	20.4858 - 18.6553				49.9146	-29382.20	3141410.00	0.009		
	18.6553 - 17.0247				50.4091	-29897.50	3157540.00	0.009		
	17.0247 - 15.2442				50.9036	-30416.60	3173390.00	0.010		
	15.2442 - 13.4637				51.3981	-30939.30	3188940.00	0.010		
	13.4637 - 11.6832				51.8926	-31465.70	3204200.00	0.010		
	11.6832 - 9.9027				52.3871	-31995.80	3219160.00	0.010		

tnx Tower		Page	19 of 24
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	08:00:11 07/24/12
Client		Designed by Lindsey Cahoon	

Section No.	Elevation	Size	M _x		Ratio		M _y		Ratio	
			lb-ft	φM _x	lb-ft	φM _y	lb-ft	φM _y	lb-ft	φM _y
	13.4637		3324491.67	3.403000.00	0.949	0.00	3503000.00	0.000	0.000	
	13.4637		11.6832			0.00	3552715.00	0.000	0.000	
	11.6832		3392238.33	3.523373.00	0.955	0.00	3552715.00	0.000	0.000	
	9.90263		9.90263			0.00	3601725.00	0.000	0.000	
	8.1221		3460283.33	3.601725.00	0.961	0.00	3601725.00	0.000	0.000	
	6.34158		3528566.67	3.651050.00	0.966	0.00	3651050.00	0.000	0.000	
	4.56105		3597108.33	3.700325.00	0.972	0.00	3700325.00	0.000	0.000	
	2.78058		3665900.00	3.749558.33	0.978	0.00	3749558.33	0.000	0.000	
	2.78058 - 1		3734950.00	3.798775.00	0.983	0.00	3798775.00	0.000	0.000	

Pole Shear Design Data

Section No.	Elevation	Size	Actual		φV _n		Actual		Ratio	
			V _n	lb	lb	φV _n	V _n	lb-ft	lb-ft	φV _n
L1	130 - 127.623		1326.99	457576.00	0.003	0.00	808665.00	0.000	0.000	
	127.623 -		8095.11	467399.00	0.017	0.00	851850.00	0.000	0.000	
	125.245		8283.57	476960.00	0.017	0.00	895625.00	0.000	0.000	
	122.868		8475.72	486260.00	0.017	0.00	939950.00	0.000	0.000	
	120.491		8671.49	495297.00	0.018	0.00	984783.33	0.000	0.000	
	118.113		13840.90	504072.00	0.027	0.00	1030083.33	0.000	0.000	
	115.736		14042.30	512585.00	0.027	0.00	1075791.67	0.000	0.000	
	113.358		14246.40	520856.00	0.027	0.00	1121891.67	0.000	0.000	
	110.981		14451.40	528826.00	0.027	0.00	1168316.67	0.000	0.000	
	108.604		19469.50	536535.00	0.036	0.00	1215025.00	0.000	0.000	
	106.226		19779.30	544018.00	0.036	0.00	1261991.67	0.000	0.000	
	103.849		22632.50	551221.00	0.041	0.00	1309150.00	0.000	0.000	
	101.472		22844.90	558162.00	0.041	0.00	1356475.00	0.000	0.000	
	99.0942		24601.50	564841.00	0.044	0.00	1403916.67	0.000	0.000	
	96.7168		27432.20	571238.00	0.048	0.00	1451425.00	0.000	0.000	
	94.3395		30186.50	577413.00	0.052	0.00	1498966.67	0.000	0.000	
	91.9621		30395.10	583306.00	0.052	0.00	1546491.67	0.000	0.000	
	89.5847		30612.50	589577.00	0.052	0.00	1593958.33	0.000	0.000	
	87.2074		30826.70	594306.00	0.052	0.00	1641325.00	0.000	0.000	

tnx Tower		Page	20 of 24
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	09:00:11 07/24/12
Client		Designed by Lindsey Cahoon	

Section No.	Elevation	Size	Actual		φV _n		Actual		Ratio	
			V _n	lb	lb	φV _n	V _n	lb-ft	lb-ft	φV _n
L2	84.83 - 80		12240.50	604407.00	0.020	0.00	1737058.33	0.000	0.000	
	84.83 - 80		19122.10	1233400.00	0.016	0.00	3480975.00	0.000	0.000	
	80 - 77.8317		31571.10	1248810.00	0.025	0.00	3586316.67	0.000	0.000	
	77.8317 -		31784.60	1264010.00	0.025	0.00	3693575.00	0.000	0.000	
	75.7033		31998.30	1278990.00	0.025	0.00	3801216.67	0.000	0.000	
	73.555		32212.20	1293760.00	0.025	0.00	3909708.33	0.000	0.000	
	71.4067		32426.30	1308530.00	0.025	0.00	4019016.67	0.000	0.000	
	69.2583		32640.60	1323360.00	0.025	0.00	4129108.33	0.000	0.000	
	67.111		32855.10	1336790.00	0.025	0.00	4239958.33	0.000	0.000	
	64.9617		33069.80	1350710.00	0.024	0.00	4351533.33	0.000	0.000	
	62.813		33284.80	1364410.00	0.024	0.00	4463791.67	0.000	0.000	
	60.666		33500.00	1377900.00	0.024	0.00	4576708.33	0.000	0.000	
	58.5167		33715.40	1391700.00	0.024	0.00	4690250.00	0.000	0.000	
	56.3683		33931.10	1404230.00	0.024	0.00	4804383.33	0.000	0.000	
	54.22		34147.00	1417080.00	0.024	0.00	4919063.33	0.000	0.000	
	52.0717		34363.10	1429710.00	0.024	0.00	5034308.33	0.000	0.000	
	49.9233		34579.60	1442130.00	0.024	0.00	5150053.33	0.000	0.000	
	47.775		34796.20	1454330.00	0.024	0.00	5266225.00	0.000	0.000	
	45.6267		35013.20	1466320.00	0.024	0.00	5382841.67	0.000	0.000	
	43.4783		35230.40	1478100.00	0.024	0.00	5499866.67	0.000	0.000	
	41.33		18564.80	1512320.00	0.012	0.00	5856950.00	0.000	0.000	
	41.33 - 34.83		17490.90	1500800.00	0.012	0.00	5734080.00	0.000	0.000	
	39.181		36159.20	1510000.00	0.024	0.00	5831216.67	0.000	0.000	
	37.033		36319.40	1519200.00	0.024	0.00	5929208.00	0.000	0.000	
	34.885		36478.50	1528150.00	0.024	0.00	6027346.67	0.000	0.000	
	32.7369		36636.50	1536950.00	0.024	0.00	6125700.00	0.000	0.000	
	30.5884		36793.40	1545610.00	0.024	0.00	6224158.00	0.000	0.000	
	28.4400		36949.30	1554120.00	0.024	0.00	6322733.33	0.000	0.000	
	26.2916		37104.00	1562490.00	0.024	0.00	6421416.67	0.000	0.000	
	24.1432		37257.70	1570700.00	0.024	0.00	6520174.67	0.000	0.000	
	22.0048		37410.40	1578770.00	0.024	0.00	6619000.00	0.000	0.000	
	19.8664		37561.90	1586690.00	0.024	0.00	6717866.67	0.000	0.000	

maxTower	Job	Page
	Project	Date
	Client	Designed by
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		21 of 24 09:00:11 07/24/12 Lindsey Cahoon

Section No.	Elevation	Size	Actual V_n	ϕV_n	Ratio $\frac{Actual V_n}{\phi V_n}$	Actual T_n	Ratio $\frac{Actual T_n}{\phi T_n}$	Criteria
	f		I_b	I_b		I_b-f	ϕT_n	
L1	130 - 127.623	0.000	0.004	0.000	0.015	1.000	4.8.2	4.8.2
	127.623 - 125.245	0.003	0.040	0.000	0.042	1.000	4.8.2	4.8.2
	125.245 - 122.868	0.003	0.081	0.000	0.084	1.000	4.8.2	4.8.2
	122.868 - 120.491	0.003	0.120	0.000	0.123	1.000	4.8.2	4.8.2
	120.491 - 118.113	0.003	0.156	0.000	0.159	1.000	4.8.2	4.8.2
	118.113 - 115.736	0.004	0.201	0.000	0.206	1.000	4.8.2	4.8.2
	115.736 - 113.358	0.005	0.254	0.000	0.259	1.000	4.8.2	4.8.2
	113.358 - 110.981	0.005	0.304	0.000	0.309	1.000	4.8.2	4.8.2
	110.981 - 108.604	0.005	0.330	0.000	0.336	1.000	4.8.2	4.8.2
	108.604 - 106.226	0.006	0.409	0.000	0.416	1.000	4.8.2	4.8.2
	106.226 - 103.849	0.006	0.468	0.000	0.475	1.000	4.8.2	4.8.2
	103.849 - 101.472	0.007	0.525	0.000	0.534	1.000	4.8.2	4.8.2
	101.472 - 99.0942	0.007	0.586	0.000	0.595	1.000	4.8.2	4.8.2
	99.0942 - 96.7168	0.008	0.645	0.000	0.655	1.000	4.8.2	4.8.2

Pole Interaction Design Data

Section No.	Elevation	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_u}{\phi M_n}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	130 - 127.623	0.000	0.014	0.000	0.000	0.015	1.000	4.8.2
	127.623 - 125.245	0.003	0.040	0.000	0.000	0.042	1.000	4.8.2
	125.245 - 122.868	0.003	0.081	0.000	0.000	0.084	1.000	4.8.2
	122.868 - 120.491	0.003	0.120	0.000	0.000	0.123	1.000	4.8.2
	120.491 - 118.113	0.003	0.156	0.000	0.000	0.159	1.000	4.8.2
	118.113 - 115.736	0.004	0.201	0.000	0.000	0.206	1.000	4.8.2
	115.736 - 113.358	0.005	0.254	0.000	0.000	0.259	1.000	4.8.2
	113.358 - 110.981	0.005	0.304	0.000	0.000	0.309	1.000	4.8.2
	110.981 - 108.604	0.005	0.330	0.000	0.000	0.336	1.000	4.8.2
	108.604 - 106.226	0.006	0.409	0.000	0.000	0.416	1.000	4.8.2
	106.226 - 103.849	0.006	0.468	0.000	0.000	0.475	1.000	4.8.2
	103.849 - 101.472	0.007	0.525	0.000	0.000	0.534	1.000	4.8.2
	101.472 - 99.0942	0.007	0.586	0.000	0.000	0.595	1.000	4.8.2
	99.0942 - 96.7168	0.008	0.645	0.000	0.000	0.655	1.000	4.8.2

maxTower	Job	Page
	Project	Date
	Client	Designed by
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		22 of 24 09:00:11 07/24/12 Lindsey Cahoon

Section No.	Elevation	Ratio $\frac{P_u}{\phi P_n}$	Ratio $\frac{M_u}{\phi M_n}$	Ratio $\frac{V_u}{\phi V_n}$	Ratio $\frac{T_u}{\phi T_n}$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
	f	P_u	M_u	V_u	T_u			
	96.7168 - 94.3395	0.009	0.713	0.000	0.000	0.724	1.000	4.8.2
	94.3395 - 91.9621	0.009	0.779	0.000	0.000	0.791	1.000	4.8.2
	91.9621 - 89.5847	0.010	0.848	0.000	0.000	0.860	1.000	4.8.2
	89.5847 - 87.2074	0.010	0.914	0.000	0.000	0.926	1.000	4.8.2
	87.2074 - 84.83	0.010	0.976	0.000	0.000	0.989	1.000	4.8.2
	84.83 - 80	0.004	0.422	0.000	0.000	0.427	1.000	4.8.2
L2	84.83 - 80	0.003	0.336	0.000	0.000	0.339	1.000	4.8.2
	80 - 77.8517	0.006	0.588	0.000	0.000	0.574	1.000	4.8.2
	77.8517 - 75.4703	0.006	0.589	0.000	0.000	0.595	1.000	4.8.2
	75.4703 - 73.0888	0.006	0.608	0.000	0.000	0.615	1.000	4.8.2
	73.0888 - 70.7074	0.006	0.627	0.000	0.000	0.633	1.000	4.8.2
	70.7074 - 68.3259	0.006	0.644	0.000	0.000	0.651	1.000	4.8.2
	68.3259 - 65.9444	0.006	0.661	0.000	0.000	0.668	1.000	4.8.2
	65.9444 - 63.5629	0.006	0.677	0.000	0.000	0.684	1.000	4.8.2
	63.5629 - 61.1814	0.006	0.692	0.000	0.000	0.699	1.000	4.8.2
	61.1814 - 58.8000	0.006	0.707	0.000	0.000	0.714	1.000	4.8.2
	58.8000 - 56.4185	0.007	0.720	0.000	0.000	0.728	1.000	4.8.2
	56.4185 - 54.0370	0.007	0.734	0.000	0.000	0.741	1.000	4.8.2
	54.0370 - 51.6555	0.007	0.747	0.000	0.000	0.754	1.000	4.8.2
	51.6555 - 49.2740	0.007	0.759	0.000	0.000	0.767	1.000	4.8.2
	49.2740 - 46.8925	0.007	0.771	0.000	0.000	0.779	1.000	4.8.2
	46.8925 - 44.5110	0.007	0.782	0.000	0.000	0.790	1.000	4.8.2
	44.5110 - 42.1295	0.007	0.795	0.000	0.000	0.801	1.000	4.8.2
	42.1295 - 39.7480	0.007	0.804	0.000	0.000	0.812	1.000	4.8.2
	39.7480 - 37.3665	0.008	0.814	0.000	0.000	0.823	1.000	4.8.2
	37.3665 - 34.9850	0.004	0.431	0.000	0.000	0.435	1.000	4.8.2

tinx Tower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	23 of 24
		Date	09:00:11 07/24/12
		Client	Designed by Lindsey Cahoon

tinx Tower		Job	Page
Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Project	24 of 24
		Date	09:00:11 07/24/12
		Client	Designed by Lindsey Cahoon

Section No.	Elevation ft	Ratio ϕP_n	Ratio ϕM_n	Ratio ϕV_n	Ratio ϕT_n	Ratio ϕP_n	Ratio ϕM_n	Ratio ϕV_n	Ratio ϕT_n	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L3	41.33 - 34.83	0.004	0.422	0.004	0.000	0.000	0.000	0.000	0.000	0.426	1.000	4.8.2 ✓
	34.83 - 33.0495	0.009	0.870	0.000	0.024	0.000	0.000	0.024	0.000	0.879	1.000	4.8.2 ✓
	33.0495 - 31.2689	0.009	0.877	0.000	0.024	0.000	0.000	0.024	0.000	0.886	1.000	4.8.2 ✓
	31.2689 - 29.4884	0.009	0.884	0.000	0.024	0.000	0.000	0.024	0.000	0.894	1.000	4.8.2 ✓
	29.4884 - 27.7079	0.009	0.891	0.000	0.024	0.000	0.000	0.024	0.000	0.901	1.000	4.8.2 ✓
	27.7079 - 25.9274	0.009	0.898	0.000	0.024	0.000	0.000	0.024	0.000	0.908	1.000	4.8.2 ✓
	25.9274 - 24.1468	0.009	0.905	0.000	0.024	0.000	0.000	0.024	0.000	0.915	1.000	4.8.2 ✓
	24.1468 - 22.3663	0.009	0.912	0.000	0.024	0.000	0.000	0.024	0.000	0.921	1.000	4.8.2 ✓
	22.3663 - 20.5858	0.009	0.918	0.000	0.024	0.000	0.000	0.024	0.000	0.928	1.000	4.8.2 ✓
	20.5858 - 18.8053	0.009	0.925	0.000	0.024	0.000	0.000	0.024	0.000	0.935	1.000	4.8.2 ✓
	18.8053 - 17.0247	0.010	0.931	0.000	0.024	0.000	0.000	0.024	0.000	0.941	1.000	4.8.2 ✓
	17.0247 - 15.2442	0.010	0.937	0.000	0.024	0.000	0.000	0.024	0.000	0.947	1.000	4.8.2 ✓
	15.2442 - 13.4637	0.010	0.943	0.000	0.024	0.000	0.000	0.024	0.000	0.953	1.000	4.8.2 ✓
	13.4637 - 11.6832	0.010	0.949	0.000	0.024	0.000	0.000	0.024	0.000	0.960	1.000	4.8.2 ✓
	11.6832 - 9.90263	0.010	0.955	0.000	0.024	0.000	0.000	0.024	0.000	0.966	1.000	4.8.2 ✓
	9.90263 - 8.1221	0.010	0.961	0.000	0.024	0.000	0.000	0.024	0.000	0.971	1.000	4.8.2 ✓
	8.1221 - 6.34158	0.010	0.966	0.000	0.024	0.000	0.000	0.024	0.000	0.977	1.000	4.8.2 ✓
	6.34158 - 4.56105	0.010	0.972	0.000	0.024	0.000	0.000	0.024	0.000	0.983	1.000	4.8.2 ✓
	4.56105 - 2.78053	0.011	0.978	0.000	0.024	0.000	0.000	0.024	0.000	0.989	1.000	4.8.2 ✓
	2.78053 - 1.00000	0.011	0.983	0.000	0.024	0.000	0.000	0.024	0.000	0.994	1.000	4.8.2 ✓

Section Capacity Table

Section No.	Elevation ft	Component Type	Size	Critical Element	P lb	ϕP_{nmax} lb	% Capacity	Pass/Fail
L1	130 - 80	Pole	T7552Lx10.1875	1	-12005.10	118860.00	98.9	Pass
L2	80 - 34.83	Pole	T747.2726x3.2726x0.3125	2	-22537.90	2956190.00	82.3	Pass

Program: Version 6.0.0.8 - 9/7/2011 File: N:\2012 Projects\U1223-Lesson_Camundiffs\U1223-226-121_611200_Watertown\ENG\TOWER\Watertown.rvt

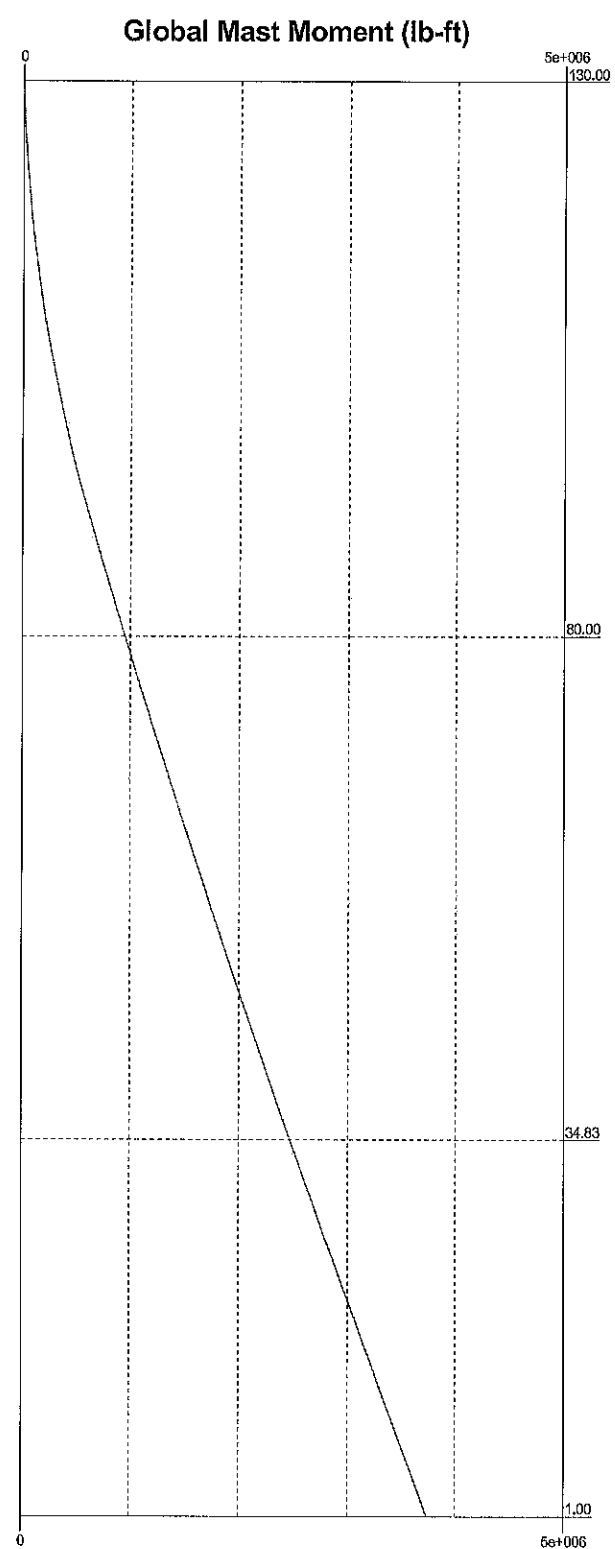
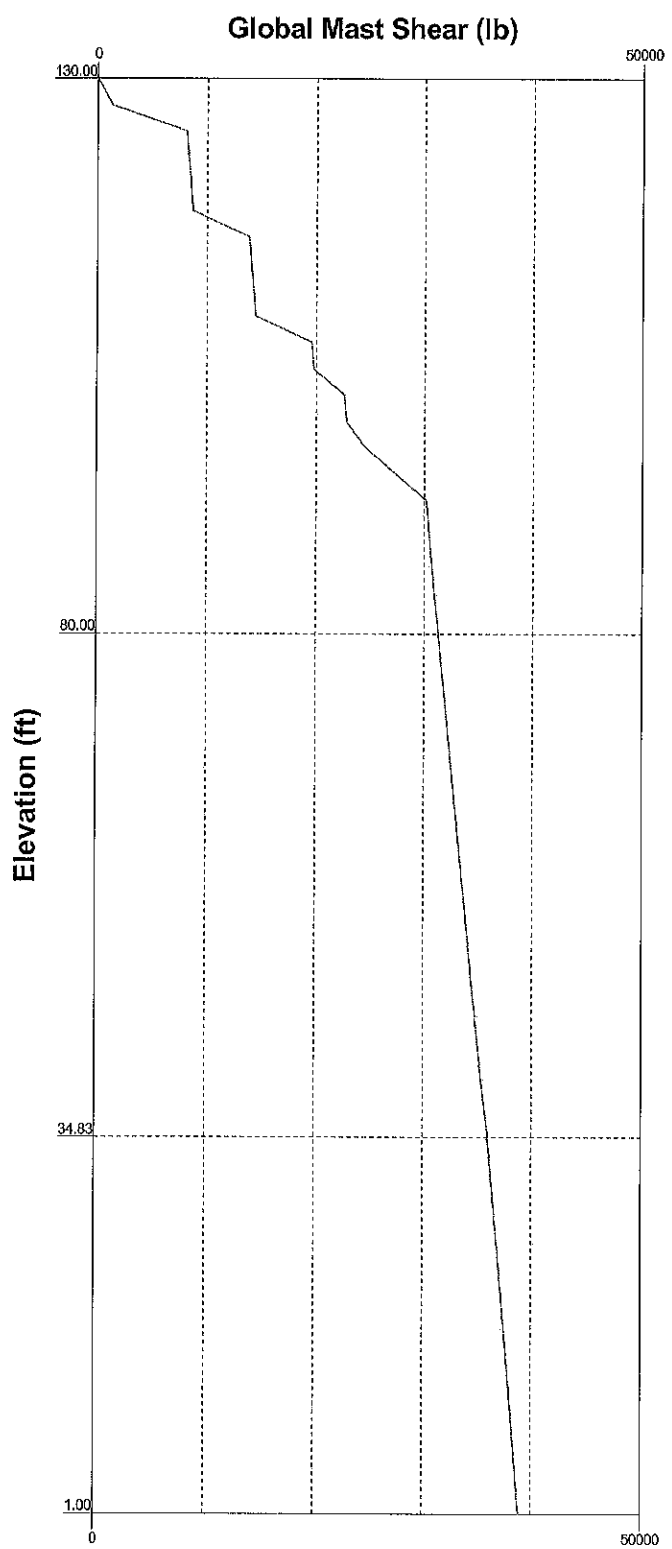
Section No. L3
Elevation ft 34.83 - 1
Component Type Pole
Size T7552Lx10.1875x0.3125
Critical Element 5
P lb -35253.10
 ϕP_{nmax} lb 3302770.00
% Capacity 99.4
Summary
Pole (L3) Pass
Base Plate 86.8 Pass
RATING = 99.4 Pass


Vx

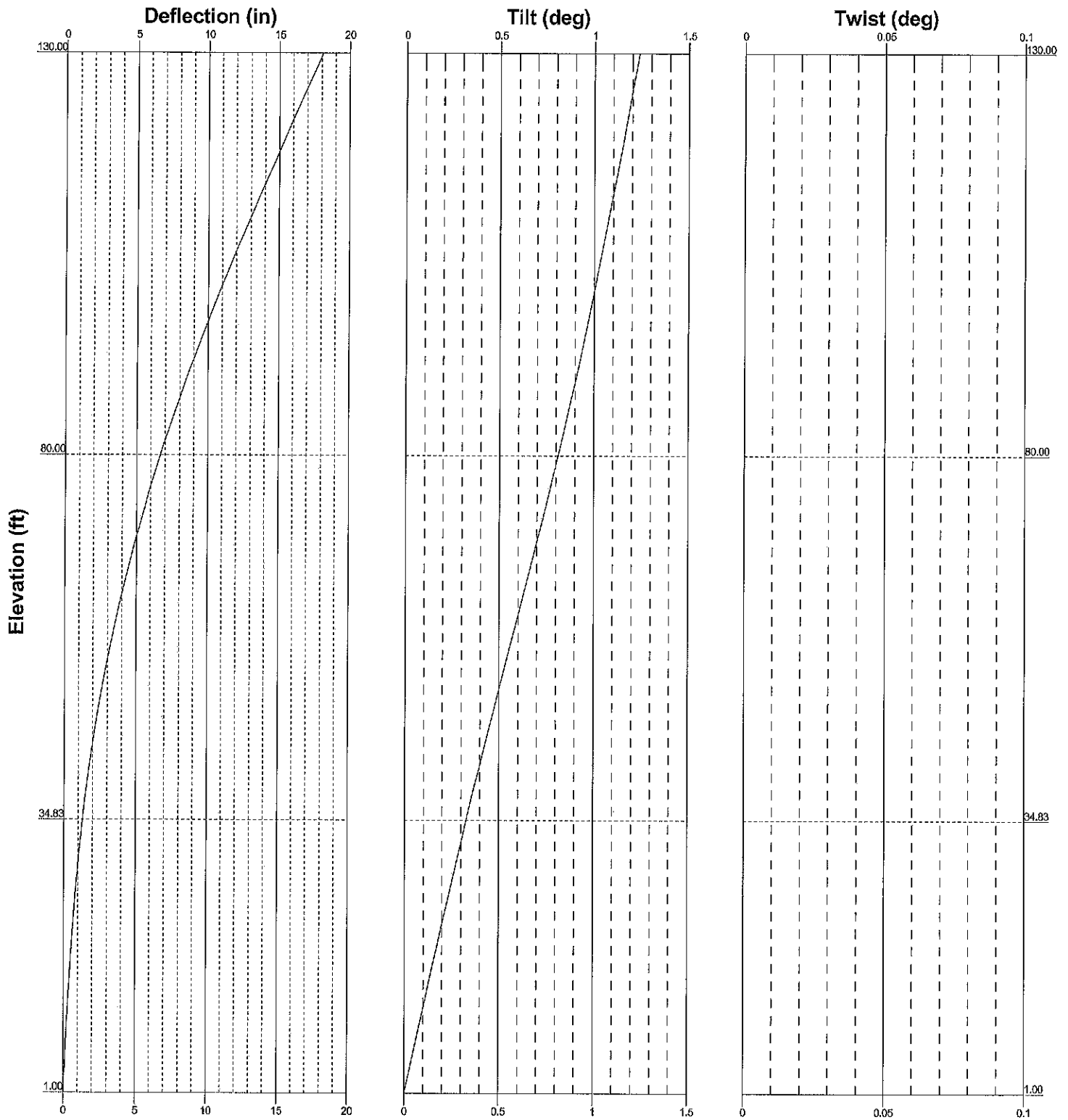
Vz


Mx

Mz

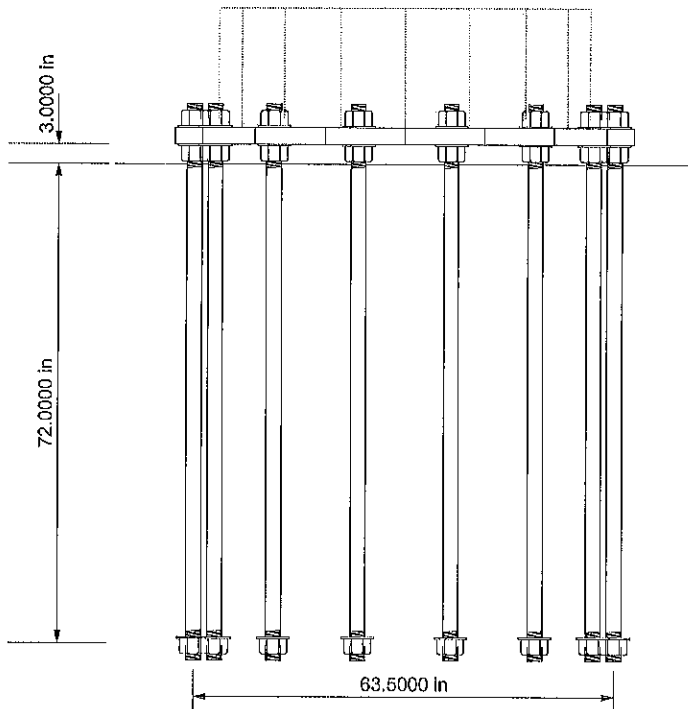
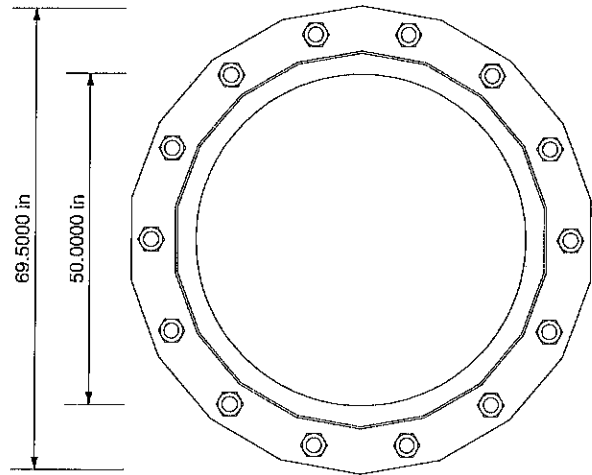


 <p>Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176</p>	Job:		
	Project:		
	Client:	Drawn by: Lindsey Cahoon	App'd:
	Code: TIA-222-G	Date: 07/24/12	Scale: NTS
	Path:	N:\2012 Projects\11223 Larson Cannon\11223-220-121 611200 Water tower\ENGTOWER\Water tower.dwg	




 <p>Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176</p>	Job:		
	Project:		
	Client:	Drawn by: Lindsey Cahoon	App'd:
	Code: TIA-222-G	Date: 07/24/12	Scale: NTS
	Path:	Dwg No. E-5	

N:\2012 Projects\TIA-222-G\Lesson Camp\Images\1223-229-121 611200 Water tower\ENGTOWER\Water tower.dwg



FOUNDATION NOTES

1. Plate thickness is 2.5000 in.
2. Plate grade is A572-50.
3. Anchor bolt grade is A615-75.
4. f_c is 6 ksi.

 Vector Structural Engineers 9138 S. State St., Suite 101 Sandy, UT Phone: 801-990-1175 FAX: 801-990-1176		Job:	
		Project:	
Client:		Drawn by: Lindsey Cahoon	App'd:
Code: TIA-222-G		Date: 07/24/12	Scale: NTS
Path:		Dwg No. F-1	
<small>N:\2012 Projects\11223 Loran Cancellation\11223-226-121 011206 Waterdown\ENGINEERING\Waterdown.dwg</small>			



JOB NO.: U1223-226-121
DATE: 07/24/12

DESIGNED: LCC
CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Seismic Base Shear Calculations:

Reactions From Wind:
V _u (kips): 38.9
W _t (kips): 29.4

Seismic Parameters:

Per California Building Code, 2010 Edition (2009 IBC), ASCE 7-05

Structure Height
130

Occupancy Category=	II	F _a =	1.60
Seismic Design Category=	D	F _v =	2.40
I _s =	1.00	S _{MS} =	0.40
Site Class=	D	S _{M1} =	0.16
R=	1.50	S _{DS} =	0.27
S _s =	0.250	S _{D1} =	0.10
S ₁ =	0.065		

Seismic Base Shear:

C _{S(MIN)} = 0.03	0.03	
C _{S(MIN)} = 0.8 x S ₁ / (R / I _s) =		(if S ₁ >= 0.6)
C _{S(MAX)} = S _{D1} / (T _a x (R / I _s)) =	0.09	
T _a = C _t x h _n ^x =	0.77	s
C _s = S _{DS} / (R / I _s) =	0.090	
V = C _s x W =	2.70	kips

Total Seismic Shear (V _u):	2.7	Kips
Total Wind Shear:	38.9	Kips

Base Shear From Wind Loading Governs

Reinforced Access Port Analysis

Reinforced Access Port:

Width, w:	10	inches
Height	30	inches
Thickness, t ₁ :	0.75	inches
Depth, d:	6	inches
Projection, p:	0.5	inches

Pole Shaft Loading:

M _u :	3735	kip-ft
P _u :	35.3	kips
V _u :	38.9	kips

Properties @ Access Port:

Flat-Flat Dia:	56.4	in
Pole Thickness, t ₂ :	0.3125	in

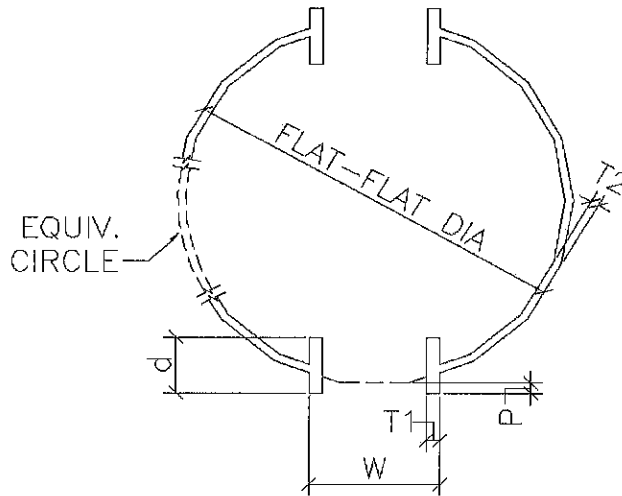
A _{PoleNoAccess} :	55.1	in ²
I _{PoleNoAccess} :	21653.0	in ⁴
S _{PoleNoAccess} :	767.8	in ³
A _{reinforced} :	66.8	in ²
I _{reinforced} :	21986.5	in ⁴
S _{reinforced} :	779.7	in ³

E:	29000	ksi
Rim F _y :	50	ksi
Pole F _y :	65	ksi

K:	1	
L:	130	ft
r:	18.14	in
F _y :	66.0	ksi
KL/r:	86.0	
λ _c :	1.3	
F _{cr} :	32.3	ksi

M _n :	4291.0	kip-ft
P _n :	2160.0	kip
V _n :	2205.2	kip
Interaction Check:	0.987	OKAY

Added Weight Per Port lbs



Note:

Section properties are based on an equivalent circular tube as shown in the illustration above. The outer diameter of the circle is equal to the flat-flat diameter of the polygon thus the properties are conservative.

Reinforced Access Port Analysis

Reinforced Access Port:

Width, w:	8 inches
Height	22 inches
Thickness, t_1 :	0.75 inches
Depth, d:	2 inches
Projection, p:	0.5 inches

Pole Shaft Loading:

M_u :	517 kip-ft
P_u :	11.0 kips
V_u :	30.2 kips

Properties @ Access Port:

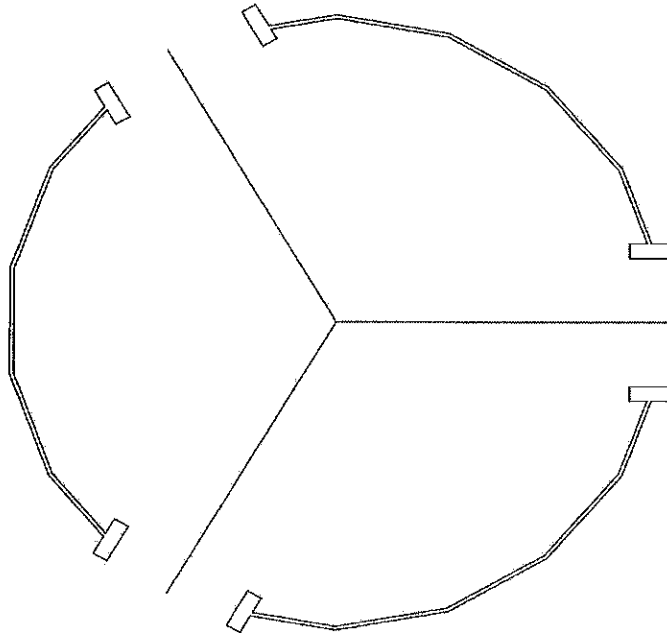
Flat-Flat Dia:	30.8 in
Pole Thickness, t_2 :	0.1875 in

$A_{PoleNoAccess}$:	18.0 in ²
$I_{PoleNoAccess}$:	2112.4 in ⁴
$S_{PoleNoAccess}$:	137.2 in ³
$A_{reinforced}$:	21.0 in ²
$I_{reinforced}$:	2637.2 in ⁴
$S_{reinforced}$:	171.2 in ³

K:	1
L:	130 ft
r:	11.21 in
F'_y :	69.4 ksi
KL/r:	139.2
λ_c :	2.2
F_{cr} :	9.7 ksi

M_n :	990.5 kip-ft
P_n :	203.9 kip
V_n :	728.7 kip

Interaction Check: 0.645 **OKAY**



E:	29000 ksi
Rim F_y :	50 ksi
Pole F_y :	65 ksi

Note:

Section properties are base on an equivalent circular tube as shown in the illustration above. The outer diameter of the circle is equal to the flat-flat diameter of the polygon thus the properties are conservative.

Added Weight Per Port 16 lbs



JOB NO.: U1223-226-121
DATE: 07/24/12

DESIGNED: LCC
CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Foundation Design

Anchorage Embedment Design

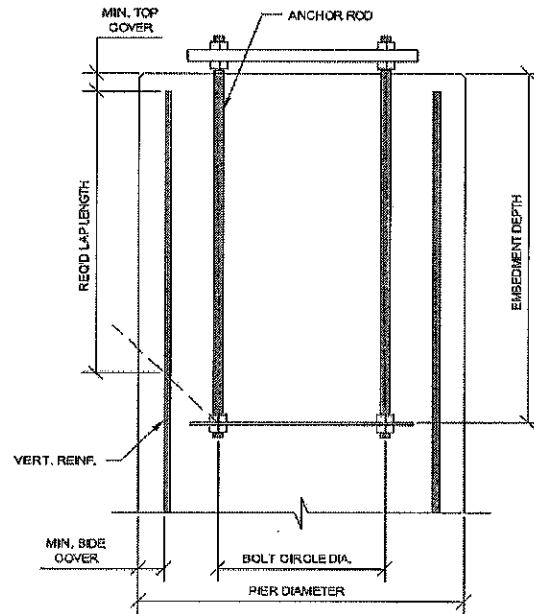
Vertical Bar Size:	#8
Conc. Comp. Strength:	4000 psi
Pier Diameter:	7 ft
Pier Depth:	4 ft
Top of Pier Elevation:	6 inches
Concrete Volume	6.4 yards
Side Conc. Cover:	4 inches
Top Conc. Cover:	3 inches
Bolt Circle Dia.:	63.5 inches
Horizontal Tie Size:	#5
# Anchor Rods:	14
Anchor Rod Dia:	2.25 inches

ψ_t (bar loc. factor):	1.0	ACI 12.2.4a
ψ_s (epoxy coating factor):	1.0	ACI 12.2.4b
ψ_s (bar size factor):	1.0	ACI 12.2.4.c
λ (concrete type factor):	1.0	ACI 12.2.4.d
Bar Diameter:	1.0 in	
Horiz. Tie Diameter:	0.6 in	
Min. Clr Dist. Btwn Anchor & Rod:	3.5 in	
Max. Clr Dist. Btwn Anchor & Rod:	7.6 in	
Req'd Lap Length:	37.0 in	ACI 12.2.2
Min. Required Embedment Depth:	49.2 in	

Available Pullout with Heavy Hex

Nut: 133963 lbs

$8 \cdot A_{brg} \cdot f_c$ - (Per ACI D15)



Required Lap Length + Max distance between anchor and rod + 0.5*Bar diameter + 0.5*Anchor diameter + Top cover

Transverse Reinforcement Design

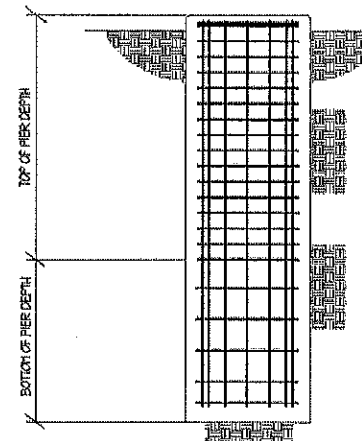
(see 2009 IBC Sections 1810.3.9.4.1 and 1810.3.9.4.2)

Seismic Design Category:	D
Site Class:	D

Type of Transverse Reinforcement:	Spiral
Transverse f_y :	40 ksi
Seismic Hooks Required?	Yes
Tie Size OK?	Yes

Spacing at Top of Pier:	2 in
Spacing at Bottom of Pier:	12 in

Total Pier Length	4.5 ft
Top Pier Length:	21 ft
Bottom Pier Length:	-16.5 ft





JOB NO.: U1223-226-121
DATE: 07/24/12

DESIGNED: LCC
CHECKED: JSP

SHEET

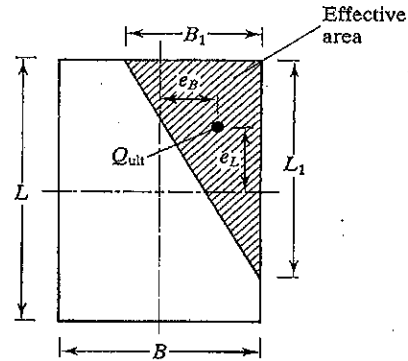
OF

PROJECT: WATERTOWN

Square Mat Foundation Design (Resultant Lies Outside Footing Kern)

Design Loads (Factored / ϕ_s):

Max. Base Shear, $V_u / 0.75$:	51.8	k
Max. Overturning Moment, $M_u / 0.75$:	4,979.9	k-ft
Max. Down, $P_{u-down} / 0.75$:	84.8	k
Structure Weight:	29.4	k
Moment Components, $M_y = M_x$:	3521.3	k-ft



Mat Properties:

Mat Width, $L = B$:	21.0	ft
Mat Thickness, t :	3.0	ft
Pier Diameter, b :	7.0	ft
Height of Pier:	4.5	ft
Depth of Soil Above Mat:	4.0	ft
Unit Weight of Soil:	110.0	pcf
Number of Legs:	1	

Volume of Concrete:	1496	ft ³
Volume of Concrete:	55.4	yd ³
Weight of Concrete:	224.4	k
Weight of Soil:	177.1	k

Soil Properties:

Allow. Bearing Pressure:	12,000	psf
Factor of Safety:	1	
1/3 increase for short term loads?	No	
Passive Pressure:	1200	pcf
Factor of Safety:	1	
Max. Passive Pressure (opt'l):		psf
1/3 increase for short term loads?	No	
Top Depth to Ignore:	0.0	ft

Eff. Bearing Pressure:	12000	psf
Coefficient of Friction:	0.70	
Factor of Safety:	1.5	
% Passive for Sliding:	100.00	
% Friction for Sliding:	0.00	

Check Bearing:

Total Moment, $M_y = M_x$:	3,796.1	k-ft
Total Axial Load, Q :	727.3	k
Load eccentricity, $e_L = e_B$:	5.22	ft
Effective Mat Brg Width, $B_1 = L_1$:	15.84	ft
Effective Area, $A' = 1/2(B_1)(L_1)$:	125.47	ft ²
Allowable axial load:	1506	k

Bearing Capacity OK.



JOB NO.: U1223-226-121
 DATE: 07/24/12

DESIGNED: LCC
 CHECKED: JSP

SHEET

OF

PROJECT: WATERTOWN

Square Mat Foundation Design (cont.)

Check Overturning:

Base Shear (1.6W), V_u :	38.9	k
Overturning Moment (1.6W), M_u :	3,735.0	k-ft
Down (0.9 D), P_u :	26.5	k
OTM about point P (1.6W):	4026.342	k-ft
Resisting Moment (0.9D):	4072.3	k-ft

Overturning OK.

Check Sliding:

Sliding Resistance from Friction:	0.0	k
Sliding Resistance from Passive:	113.4	k
Total Sliding Resistance:	113.4	k

Sliding resistance OK.

