

KENNETH C. BALDWIN

280 Trumbull Street Hartford, CT 06103-3597 Main (860) 275-8200 Fax (860) 275-8299 kbaldwin@rc.com Direct (860) 275-8345

Also admitted in Massachusetts

September 8, 2021

### Via Hand Delivery

Melanie A. Bachman, Esq. Executive Director/Staff Attorney Connecticut Siting Council 10 Franklin Square New Britain, CT 06051

Re: Docket No. 491 – Application of Cellco Partnership d/b/a Verizon Wireless For A Certificate Of Environmental Compatibility And Public Need For The Construction, Maintenance And Operation Of A Wireless Telecommunications Facility At 110 Yantic Lane, Norwich, Connecticut

Development and Management Plan Submission

### Dear Ms. Bachman:

Enclosed please find fifteen (15) copies of the following:

- 1. Final Development and Management ("D&M") Plans prepared by On-Air Engineering, LLC for the approved telecommunications facility at 110 Yantic Lane, Norwich, Connecticut, incorporating the Council's conditions of approval. Also enclosed are three (3) full size (24" x 36") sets of D&M plans.
- 2. Tower and Foundation design and calculations dated July 28, 2021, prepared by ROHN Products LLC.
- 3. Geotechnical Engineering Report prepared by Atlantic Consulting & Engineering, LLC dated May 14, 2021.

### Robinson+Cole

Melanie A. Bachman, Esq. September 8, 2021 Page 2

Together, this information constitutes the final D&M Plan submission for the approved telecommunications facility at 110 Yantic Lane in Norwich, Connecticut.

We respectfully request that this information be reviewed, and this matter be placed on the next available Siting Council agenda for approval. Please feel free to contact me if you have any questions or require additional information. Thank you.

Sincerely,

Kenneth C. Baldwin

Kung mu

KCB/kmd Enclosures Copy to:

Glenn Pianka, Bozrah First Selectman Peter A. Nystrom, Norwich Mayor Tim Parks, Verizon Wireless

# verizon

WIRELESS COMMUNICATIONS FACILITY

DEVELOPMENT AND MANAGEMENT PLAN DOCKET NO. 491

SITE NAME: NORWICH 4 CT

### 110 YANTIC LANE NORWICH, CT 06360

PRO.	JECT SUMMARY			
SITE NAME:	NORWICH 4 CT			
SITE ADDRESS:	110 YANTIC LANE NORWICH, CT 06360			
PROPERTY OWNER:	ROBERT W LARSEN 110 YANTIC LANE NORWICH, CT 06360			
PARCEL ID:	65-2-1			
TOWER COORDINATES:	41° 33' 08.50" N 72° 07' 33.20" W			
APPLICANT:	CELLCO PARTNERSHIP d.b.a. VERIZON WIRELESS 20 ALEXANDER DR. WALLINGFORD, CT 06492			
VERIZON WIRELESS CONTACTS:	MIKE HUMPHREYS - CONSTRUCTION STRUCTURE CONSULTING - SITE ACQUISITION			
LEGAL/REGULATORY COUNSEL:	KENNETH C. BALDWIN, ESQ. ROBINSON & COLE, LLP (860) 275-8345			

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	DRAWING SCHEDULE
SHEET NO.	SHEET DESCRIPTION
T-1	TITLE SHEET
C-0	SITE UTILITY PLAN
C-1	SITE PLAN
C-2	ENLARGED SITE PLANS
C-3	ENVIRONMENTAL NOTES & DETAILS
C-4	COMPOUND PLAN, NORTH ELEVATION & EQUIPMENT PLAN
C-5	ANTENNA PLAN & DETAILS
C-6	STRUCTURAL EQUIPMENT PLAN & ELEVATIONS
C-7	STRUCTURAL DETAILS
C-8	SITE DETAILS & CSC REPORTING NOTES

Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD, CT 06492



On Air Engineering, LLC

88 Foundry Pond Road Cold Spring, NY 10516 onair@optonline.net 201-456-4624



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**NEW BUILD MACRO** 

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NORWICH 4 CT

PROJECT INFORMATION:

MF

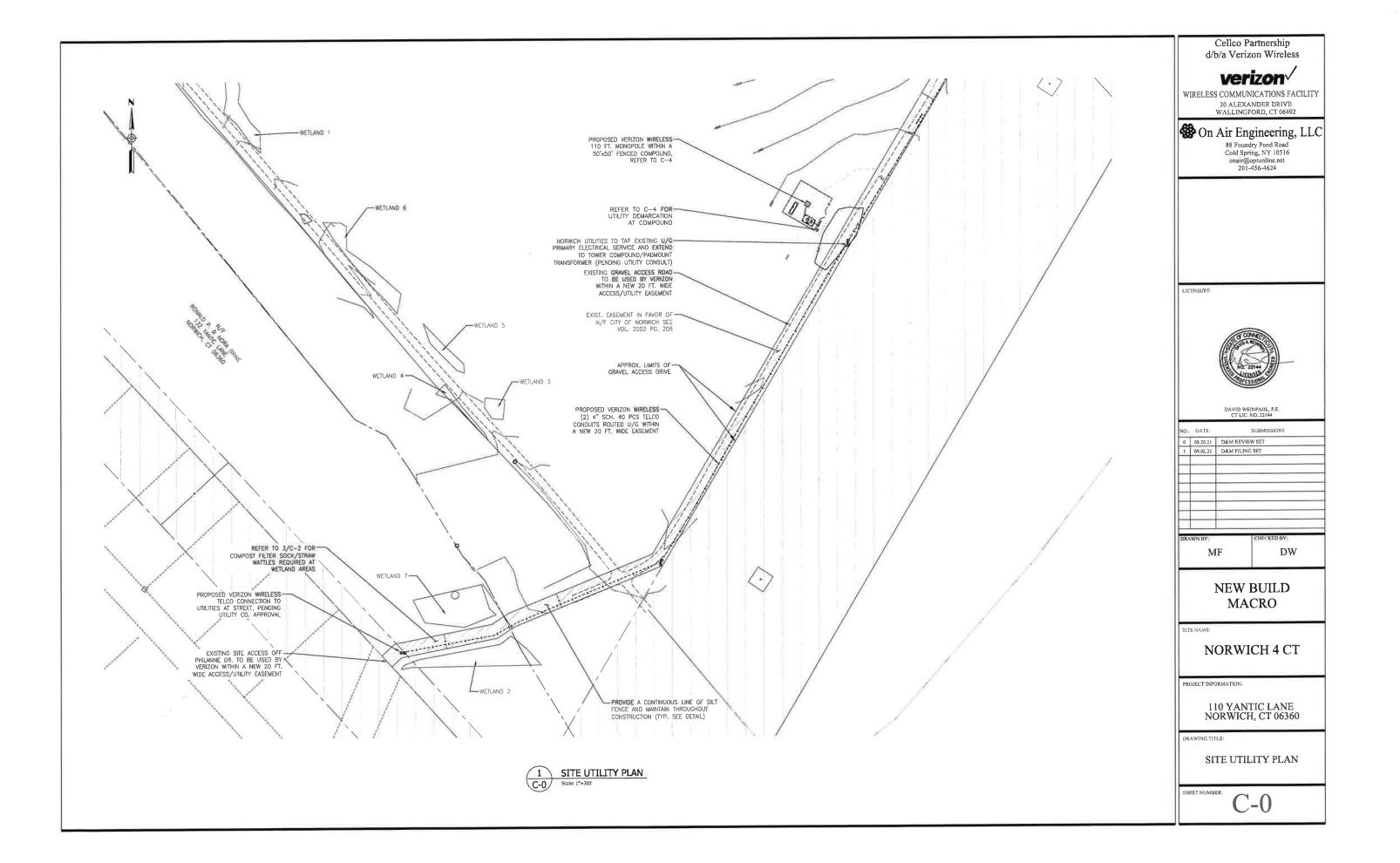
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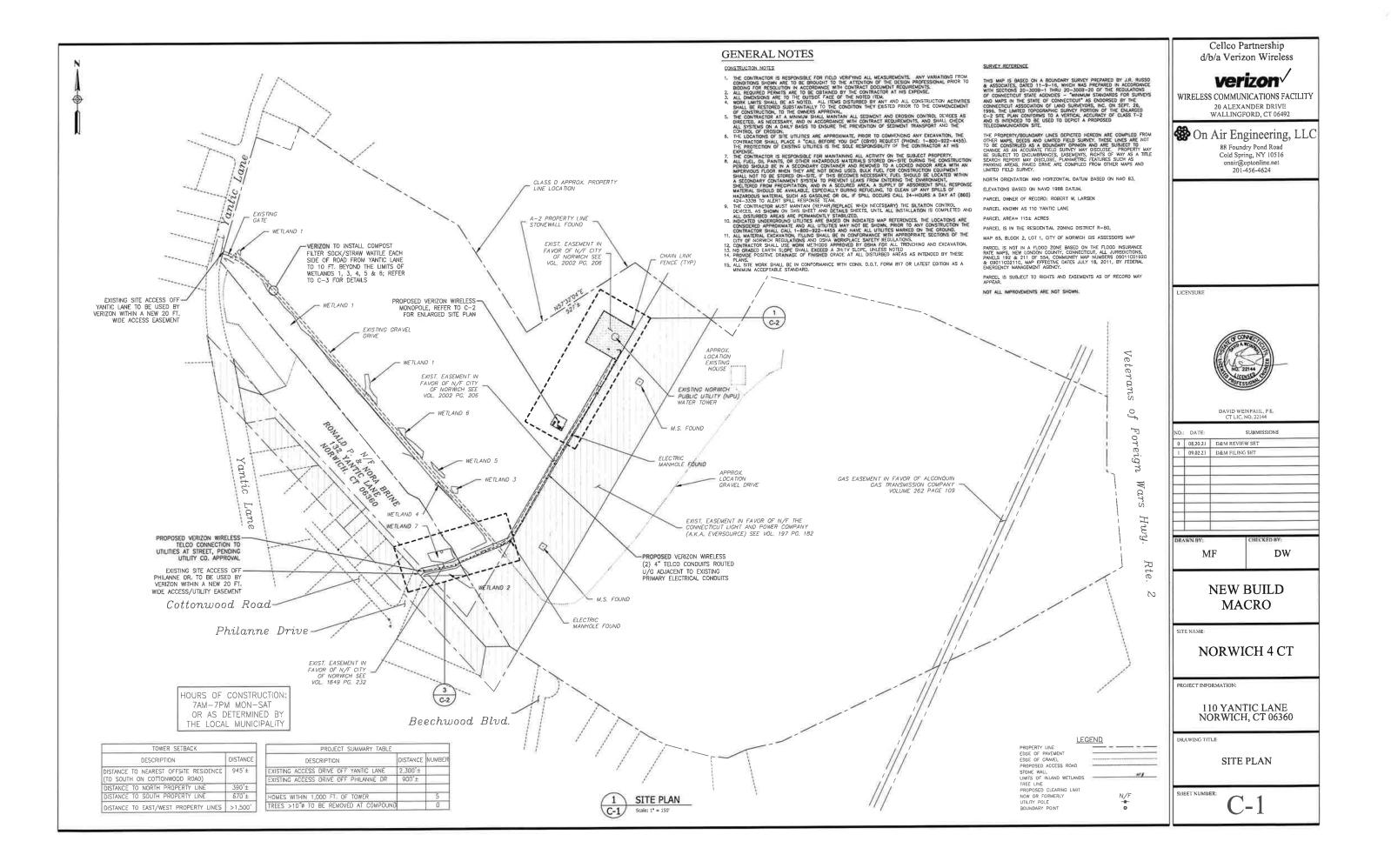
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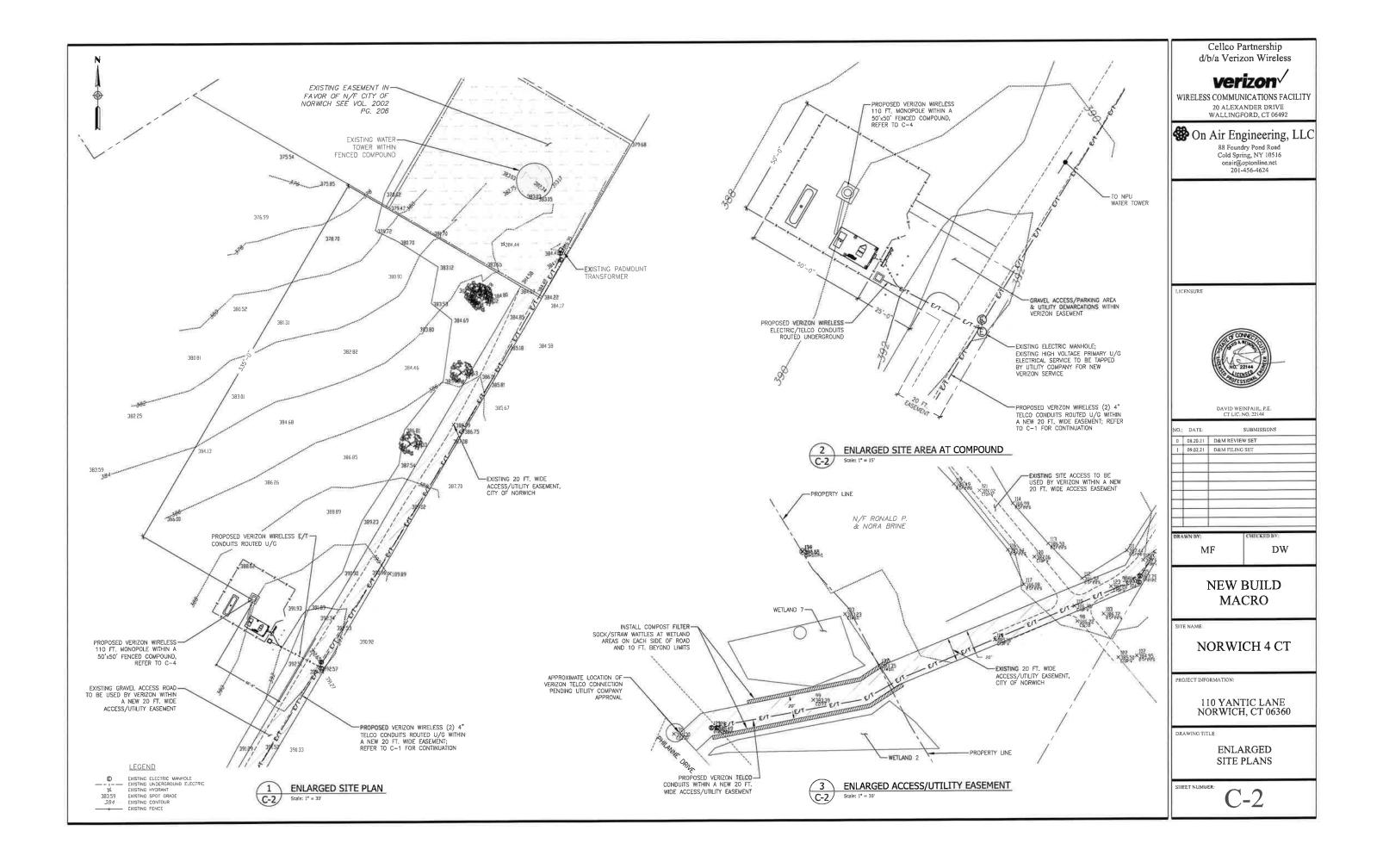
T-1

### PROJECT DESCRIPTION

- INSTALLATION OF A 110 FT, MONOPOLE/TOWER AND FENCED—IN COMPOUND AT GRADE INSTALLATION OF OUTDOOR CABINETS AND A PROPANE FUELED BACK—UP EMERGENCY GENERATOR ON A 18'-0"x10'-0" EQUIPMENT PAD WITHIN THE COMPOUND
- INSTALLATION OF (6) PANEL ANTENNAS AND ASSOCIATED DEVICES ON THE MONOPOLE INSTALLATION OF CABLING FROM EQUIP. CABINETS TO ANTENNAS
- ELECTRICAL & TELEPHONE CONNECTIONS TO EXISTING UTILITY DEMARCATION POINTS







### ENVIRONMENTAL NOTES

### WETLAND PROTECTION PLAN

AS A RESULT OF THE PROPOSED DEVELOPMENT'S LOCATION IN THE VICINITY OF WETLANDS, THE FOLLOWING BEST MANAGEMENT PRACTICES ("BMPS") ARE RECOMMENDED TO AVOID UNINTENTIONAL IMPACT TO WETLAND HABITATS DURING CONSTRUCTION ACTIVITIES...

A WETLAND SCIENTIST FROM ALL-POINTS TECHNOLOGY CORP. (APT) EXPERIENCED IN COMPLIANCE MONITORING OF CONSTRUCTION ACTIVITIES WILL SERVE AS THE ENVIRONMENTAL MONITOR FOR THIS PROJECT TO ENSURE THAT THE FOLLOWING BMPS ARE IMPLEMENTED PROPERLY, THIS PROTECTION PROGRAM SHALL BE IMPLEMENTED REGARDLESS OF TIME OF YEAR THE CONSTRUCTION ACTIVITIES OCCUR, ALL-POINTS TECHNOLOGY CORPORATION, P.C. (APT) WILL SERVE AS THE ENVIRONMENTAL MONITOR FOR THIS PROJECT TO ENSURE THAT WETLAND PROTECTION MEASURES ARE IMPLEMENTED PROPERLY, THE CONTRACTOR SHALL CONTACT DEAN CUSTAFSON, SENIOR WETLAND SCIENTIST AT APT, AT LEAST 5 BUSINESS DAYS PRIOR TO THE PRE-CONSTRUCTION MEETING, MR. GUSTAFSON CAN BE REACHED BY PHONE AT (860) 552-2033 OR VIA EMAIL AT DGUSTAFSON@ALLPOINTSTECH\_COM.

THE PROPOSED WETLAND PROTECTION PROGRAM CONSISTS OF SEVERAL COMPONENTS INCLUDING: EDUCATION OF ALL CONTRACTORS AND SUB-CONTRACTORS PRIOR TO INITIATION OF WORK ON THE SITE; USE OF APPROPRIATE EROSION CONTROL MEASURES TO CONTROL AND CONTAIN EROSION WHILE AVOIDING/MINIMIZING WILDLIFE ENTANGLEMENT; PERIODIC INSPECTION AND MAINTENANCE OF EROSION CONTROLS FOR THE PURPOSES OF ENSURING PROTECTION OF WETLAND RESOURCES; AND, REPORTING.

#### 1. CONTRACTOR EDUCATION:

- O PRIOR TO WORK ON SITE AND INITIAL DEPLOYMENT/MOBILIZATION OF EQUIPMENT AND MATERIALS, THE CONTRACTOR SHALL ATTEND AN EDUCATIONAL SESSION AT THE PRE-CONSTRUCTION MEETING WITH THE ENVIRONMENTAL MONITOR. THIS ORIENTATION AND EDUCATIONAL SESSION WILL CONSIST OF INFORMATION STRESSING THE ENVIRONMENTALLY SENSITIVE NATURE OF THE PROJECT AND PROXIMITY TO WETLAND RESOURCES AND THE NEED TO ENSURE THEIR PROTECTION THROUGHOUT THE DURATION OF THE CONSTRUCTION.
- 5 THE ENVIRONMENTAL MONITOR WILL ALSO POST CAUTION SIGNS THROUGHOUT THE PROJECT SITE AND MAINTAIN THEM FOR THE ENVIRONMENTALLY SENSITIVE NATURE OF THE WORK AREA
- CITHE CONTRACTOR WILL BE PROVIDED WITH THE ENVIRONMENTAL MONITOR'S CELL PHONE AND EMAIL CONTACT INFORMATION TO IMMEDIATELY REPORT ANY FAILURES OF EROSION CONTROLS OR RELEASES OF SEDIMENT INTO NEARBY WETLANDS.

### 2.FROSION AND SEDIMENTATION CONTROLS

- a, PLASTIC NETTING WITH LARGE MESH OPENINGS (> 1/4") USED IN A A,PLASTIC NETTING WITH LARGE MESH OPENINGS (> ½") USED IN A VARIETY OF EROSION CONTROL PRODUCTS (IE., EROSION CONTROL BLANKETS, FIBER ROLLS [WATTLES], REINFORCED SILT FENCE) HAS BEEN FOUND TO ENTANGLE WILDLIFE, INCLUDING REPTILES, AMPHIBIANS, BIRDS AND SMALL MAMMALS, NO PERMANENT EROSION CONTROL PRODUCTS OR REINFORCED SILT FENCE WILL BE USED ON THE PROJECT, TEMPORARY EROSION CONTROL PRODUCTS THAT WILL BE EXPOSED AT THE GROUND SURFACE REPRESENT A POTENTIAL FOR WILDLIFE ENTANGLEMENT WILL USE SITHER ROSION CONTROL BLANKETS AND FIBER ROLLS COMPOSED OF PROCESSED FIBERS MECHANICALLY BOUND TOGETHER TO FORM A CONTINUOUS MATRIX (NETLESS) OR NETTING WITH A MESH SIZE </E/>

  A CONTINUOUS MATRIX (NETLESS) OR NETTING WITH A MESH SIZE COMPOST FILTER SOCKS TO AVOID/MINIMIZE WILDLIFE ENTANGLEMENT.
- **BAINSTALLATION OF EROSION AND SEDIMENTATION CONTROLS, REQUIRED** SJINSTALLATION OF ENGSION AND SEDIMENTATION CONTROLS, REQUIRED, FOR EROSION CONTROL COMPLIANCE, SHALL BE PERFORMED BY THE CONTRACTOR FOLLOWING CLEARING ACTIVITIES AND PRIOR TO ANY EARTHWORK IN ACCORDANCE WITH THE PROJECT SITE PLANS. THE ENVIRONMENTAL MONITOR WILL INSPECT THE WORK ZONE AREA PRIOR TO AND FOLLOWING EROSION CONTROL BARRIER INSTALLATION TO FNSURE IT HAS BEEN SATISFACTORILY INSTALLED PRIOR TO THE
- C.THE CONTRACTOR SHALL HAVE ADDITIONAL EROSION AND SEDIMENTATION CONTROLS SHOULD FIELD CONDITIONS WARRANT EXTENDING TH CONTROLS AS RECOMMENDED BY THE ENVIRONMENTAL MONITOR.
- d.IN ADDITION TO REQUIRED DAILY INSPECTION BY THE CONTRACTOR, THE SIAN ADDITION TO REQUIRED DALET INSPECTION BY THE CONTRACTOR, TEROSION AND SEDIMENTATION CONTROLS WILL BE INSPECTED BY THE CONTRACTOR FOR TEARS OR BREECHES IN THE FABRIC FOLLOWING INSTALLATION AND FOLLOWING STORM EVENTS THAT PRODUCE A DISCHARGE, INSPECTIONS WILL BE CONDUCTED PERIODICALLY BY THE ENVIRONMENTAL MONITOR THROUGHOUT THE COURSE OF THE CONSTRUCTION PROJECT.
- e.ALL EROSION CONTROL MEASURES SHALL BE REMOVED WITHIN 30 DAYS OF COMPLETION OF WORK AND PERMANENT STABILIZATION OF SITE SOILS. OF COMPLETION OF WORK AND PERMANENT STABILIZATION OF STE SOILS, FF FIBER ROLLS, VMATTEES, STRAW BALES, OR OTHER NATURAL MATERIAL EROSION CONTROL PRODUCTS ARE USED, SUCH DEVICES WILL NOT BE LEFT IN PLACE TO BIODEGRADE AND SHALL BE PROMPTLY REMOVED AFTER SOILS ARE STABLE SO AS NOT TO CREATE A BARRIER TO MIGRATING WILDLIFE, SEED FROM SEEDING OF SOILS SHALL NOT BE SPREAD OVER FIBER ROLLS/WATTLES AS IT MAKES THEM HARDER TO REMOVE ONCE SOILS ARE STABILIZED BY VEGETATION.

#### 3.PETROLEUM MATERIALS STORAGE AND SPILL PREVENTION

- c. CERTAIN PRECAUTIONS ARE NECESSARY TO STORE PETROLEUM
  MATERIALS, REFUEL AND CONTAIN AND PROPERTY CLEAN UP ANY
  INADVERTENT FUEL OR PETROLEUM (I.E., OIL, HYDRAULG FLUID, ETC.)
  SPILL DUE TO THE PROJECT'S LOCATION IN PROXIMITY TO SENSITIVE
- b. A SPILL CONTAINMENT KIT CONSISTING OF A SUFFICIENT SUPPLY OF A SPILL CONTAINMENT KIT CONSISTING OF A SUFFICIENT SUPPLY OF ABSORBENT PADS AND ABSORBENT MATERIAL WILL BE MAINTAINED BY THE CONTRACTOR AT THE CONSTRUCTION SITE THROUGHOUT THE DURATION OF THE PROJECT, IN ADDITION, A WASTE DRUM WILL BE KEPT ON SITE TO CONTAIN ANY USED ABSORBENT PADS/MATERIAL FOR PROPER AND TIMELY DISPOSAL OFF SITE IN ACCORDANCE WITH APPLICABLE LOCAL, STATE, AND FEDERAL LAWS
- C. THE FOLLOWING PETROLEUM AND HAZARDOUS MATERIALS STORAGE AND REFUELING RESTRICTIONS AND SPILL RESPONSE PROCEDURES WILL BE ADHERED TO BY THE CONTRACTOR
- PETROLEUM AND HAZARDOUS MATERIALS STORAGE AND REFUELING
- 1. REFUELING OF VEHICLES OR MACHINERY SHALL TAKE PLACE ON AN IMPERVIOUS PAD WITH SECONDARY CONTAINMENT DESIGNED TO CONTAIN
- 2. ANY REFUELING DRUMS/TANKS OR HAZARDOUS MATERIALS THAT MUST BE KEPT ON SITE SHALL BE STORED ON AN IMPERVIOUS SUFFACE UTILIZING SECONDARY CONTAINMENT A MINIMUM OF 100 FEET FROM WETLANDS OR WATERCOURSES.
- ii. INITIAL SPILL RESPONSE PROCEDURES
- 1. STOP OPERATIONS AND SHUT OFF EQUIPMENT.
- 2 REMOVE ANY SOURCES OF SPARK OR FLAME.
- 3. CONTAIN THE SOURCE OF THE SPILL.
- 4. DETERMINE THE APPROXIMATE VOLUME OF THE SPILL
- 5. IDENTIFY THE LOCATION OF NATURAL FLOW PATHS TO PREVENT THE RELEASE OF THE SPILL TO SENSITIVE NEARBY WATERWAYS OR WETLANDS.
- 6. ENSURE THAT FELLOW WORKERS ARE NOTIFIED OF THE SPILL

### iii. SPILL CLEAN UP & CONTAINMENT

- 1. OBTAIN SPILL RESPONSE MATERIALS FROM THE ON-SITE SPILL RESPONSE KIT. PLACE ABSORBENT MATERIALS DIRECTLY ON THE RELEASE AREA.
- 2. LIMIT THE SPREAD OF THE SPILL BY PLACING ABSORBENT MATERIALS AROUND THE PERIMETER OF THE SPILL.
- 3. ISOLATE AND ELIMINATE THE SPILL SOURCE.
- 4. CONTACT THE APPROPRIATE LOCAL, STATE AND/OR FEDERAL AGENCIES, AS
- 5. CONTACT A DISPOSAL COMPANY TO PROPERLY DISPOSE OF CONTAMINATED MATERIALS

### iv. REPORTING

- COMPLETE AN INCIDENT REPORT.
- 2. SUBMIT A COMPLETED INCIDENT REPORT TO LOCAL, STATE, AND FEDERAL AGENCIES, AS REQUIRED, REPORTING

### 4. REPORTING:

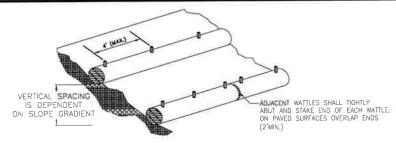
- NEPORTING:

  OINSPECTION REPORTS (BRIEF NARRATIVE AND APPLICABLE PHOTOS) WILL

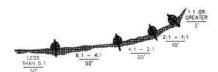
  BE PREPARED BY THE ENVIRONMENTAL MONITOR DOCUMENTING EACH
  INSPECTION AND SUBMITTED TO THE PERMITTEE FOR COMPILANCE
  VERIFICATION. ANY NON-COMPLIANCE OBSERVATIONS OF EROSION
  CONTROL MEASURES OR EVIDENCE OF EROSION OR SEDIMENT RELEASE
  WILL BE IMMEDIATELY REPORTED TO THE PERMITTEE AND ITS
- b.ANY INCIDENTS OF SIGNIFICANT RELEASE OF SEDIMENT OR OTHER MATERIALS INTO WETLAND RESOURCE AREAS SHALL BE REPORTED BY THE PERMITTEE WITHIN 24 HOURS TO THE CONNECTICUT SITING COUNCIL.
- CLANY OBSERVATIONS OF RARE SPECIES WILL BE REPORTED TO THE CONNECTICUT DEPARTMENT OF ENERGY AND ENVIRONMENTAL PROTECTION'S NATURAL DIVERSITY DATA BASE PROGRAM.
- diFOLLOWING COMPLETION OF THE PROJECT, A SUMMARY REPORT WILL BE PREPARED BY THE ENVIRONMENTAL MONITOR DOCUMENTING COMPLIANCE WITH THE WETLAND PROTECTION PLAN AND SUBMITTED TO THE PERMITTEE, WHO SHALL SUBMIT A COPY TO THE CONNECTICUT SITING COUNCIL.

### SEEDING SPECIFICATIONS-

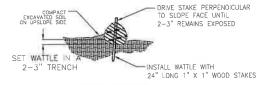
- ${\rm A_{\rm sc}}$  if ground has been previously mulched, mulch must be removed or additional nitrogen must be  ${\rm ADDED_{\rm sc}}$
- B. REMOVE ALL SURFACE STONES 2" OR LARGER AS WELL AS ALL DEBRIS SUCH AS WIRE. CABLE. TREE ROOTS, PIECES OF CONCRETE, CLODS, CLUMPS, OR OTHER UNSUITABLE MATERIAL
- C. APPLY FERTILIZER AT 7.5 POUNDS PER 1,000 SQUARE FEET AND LIME AT 200 POUNDS PER 1,000 SQUARE FEET UNLESS SOIL TESTING FOR REQUIREMENTS IS PERFORMED.
- D. NO MOWING IS TO BE UNDERTAKEN UNTIL THE MAJORITY OF THE VEGETATION IS AT LEAST 6" HIGH. MOWING SHOULD CUT THE TOP 1/3 OF VEGETATION. DO NOT UNDER ANY CIRCUMSTANCES CUT VEGETATION
- E. DO NOT APPLY ANY FORM OF WEED CONTROL UNTIL GRASS HAS BEEN
- F. THESE SEEDING MEASURES ARE NOT TO BE USED ON SLOPES IN EXCESS
- G. PERMANENT SEEDING MEASURES ARE TO BE USED INSTEAD OF TEMPORARY SEEDING MEASURES WHERE WORK IS TO BE SUSPENDED FOR A PERIOD OF TIME LONGER THAN 1 YEAR.
- H. IF THERE IS NO EROSION, BUT SEED SURVIVAL IS LESS THAN 10D PLANTS PER SQUARE FOOT AFTER 4 WEEKS OF GROWTH, RE-SEED AS
- ALL DISTURBED AREAS OUTSIDE THE PAVEMENT AREA SHALL BE LOAMED AND SEEDED IN ACCORDANCE WITH THE SUGGESTED SEEDING MIXTURES



### TYPICAL WATTLE INSTALLATION GUIDE



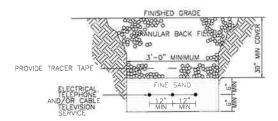
### TYPICAL WATTLE SPACING BASED ON SLOPE GRADIENT



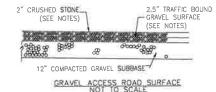
### ENRICHMENT DETAIL

### STRAW WATTLE INSTALLATION

STRAW WATTLE NOTES:



### BURIED CABLE TRENCH CROSS SECTION



### NOTE:

1 TRAFFIC BOUND GRAVEL SURFACE SHALL MEET CT DOT STANDARD SPECIFICATIONS M.02.06 GRADATION, GRADING "C"

2. CRUSHED STONE SHALL MEET CT DOT STANDARD SPECIFICATIONS  $M_{\rm s} D1_{\rm s} D1_{\rm s} D1_{\rm s} A1_{\rm s}$ 

### 4" CRUSHED STONE -60

1. BEGIN AT THE LOCATION WHERE THE WATTLE IS TO BE INSTALLED BY EXCAVATING A 2-3" DEEP BY 9" WIDE TRENCH ALONG THE CONTOUR OF THE SLOPE. EXCAVATED SOIL SHOULD BE PLACED UP-SLOPE FROM THE ANCHOR TRENCH,

2. PLACE THE WATTLE IN THE TRENCH SO THAT IT CONTOURS TO THE SOIL SUBFACE. COMPACT THE SOIL FROM THE EXCAVATED TRENCH AGAINST THE WATTLE ON THE UPHILL SIDE. ADJACENT WATTLES SHOULD TIGHTLY ABUT.

3. SECURE THE WATTLE WITH 24" LONG STAKES EVERY 3-4' WITH A STAKE ON EACH END, STAKES SHOULD BE DRIVEN THROUGH THE MIDDLE OF THE WATTLES LEAVING 2-3" OF STAKE EXTENDING ABOVE. THE WATTLE STAKES SHOULD BE DRIVEN PERPENDICULAR TO THE SLOPE FACE,

4. SECURE WATTLES PLACED ON PAVED SURFACES WITH SANDBAGS SPACED AT AN INTERVAL SUFFICIENT TO PREVENT MOVEMENT OF WATTLE AND TO ENSURE THAT ENDS OF ADJACENT WATTLES REMAIN TIGHTLY ABUTTED.

6" COMPACTED GRAVEL SUBBASE GRAVEL COMPOUND SURFACE

### NOTE:

1. CRUSHED STONE SHALL MEET CT DOT STANDARD SPECIFICATIONS M.01.01 NO.3.

### SUGGESTED SEEDING MIXTURES AND PRACTICES

AREAS WHERE SEED MIX APPLIES	SEEDING MIXTURES BY WEIG	ЭНТ	RATE PER 1,000 SQ. FT.	SEEDING DATES
ALL LAWN AREAS	RED FESCUES KENTUCKY BLUEGRASS PERENNIAL RYEGRASS	45% 45% 10%	1 LBS.	APRIL 1 - JUNE 15 OR AUG., 15 - OCT., 1
ROAD CUTS, FILLS, DIVERSION DITCHES, & STORMWATER BASINS	KENTUCKY TALL FESCUE REDTOP CREEPING RED FESCUE	47% 6% 47%	0,95 LBS.	APRIL 1 - JUNE 15 OR AUG, 15 - OCT, 1

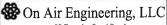
WHERE TREES ARE TO BE RETAINED, THE SEED MIXTURE SHOULD BE ADAPTED FOR SHADY CONDITIONS.

WITHIN 7 DAYS AFTER SUSPENSION OF GRADING WORK 1-1/2 LBS. TEMPORARY SEEDING ANNUAL RYFGRASS OR

Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD, CT 06493



88 Foundry Pond Road Cold Spring, NY 10516 201-456-4624



SUBMISSIONS 0 08 20 21 D&M REVIEW SET 1 09 02 21 D&M FILING SET

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NEW BUILD MACRO

SITE NAME:

NORWICH 4 CT

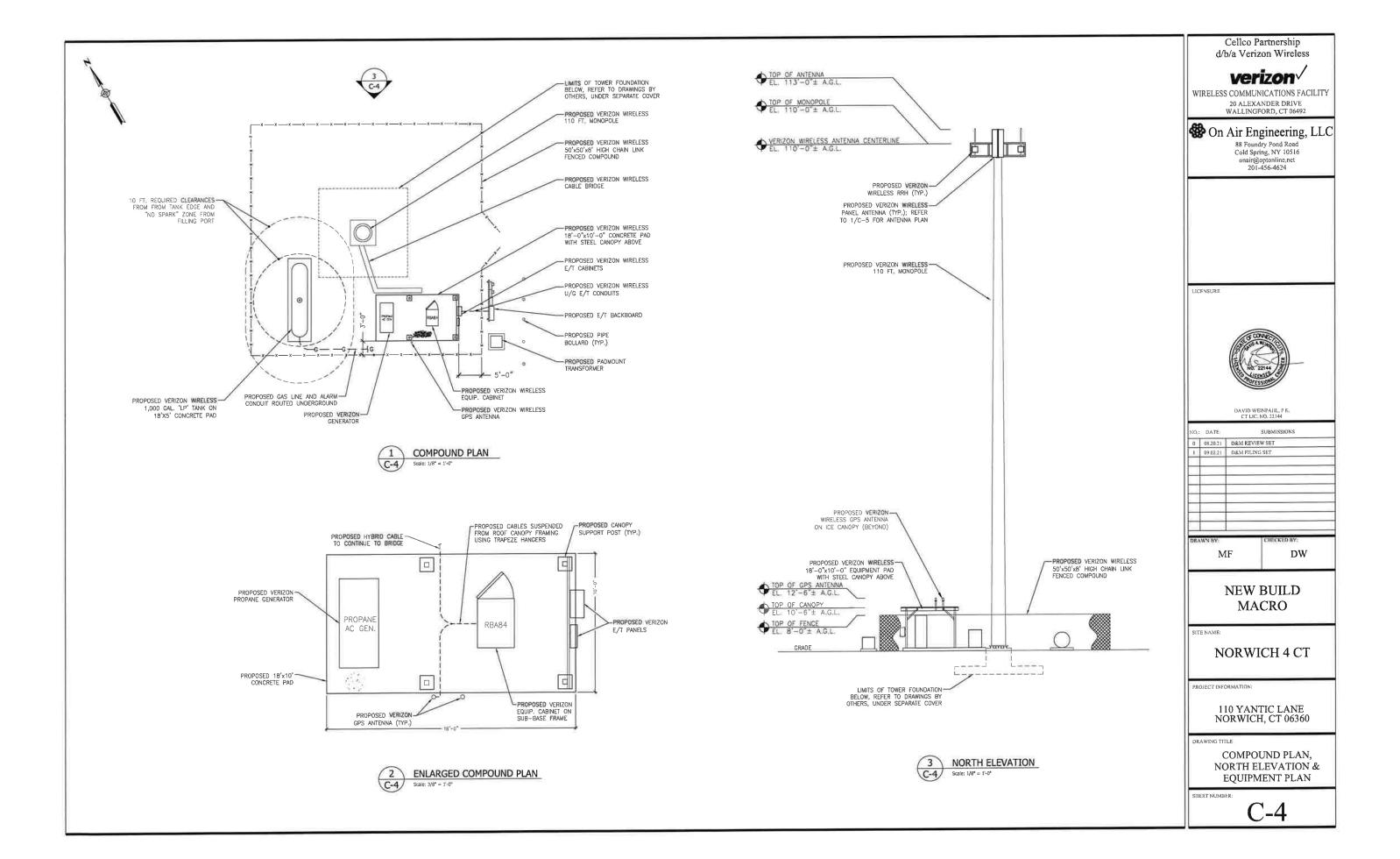
PROJECT INFORMATION:

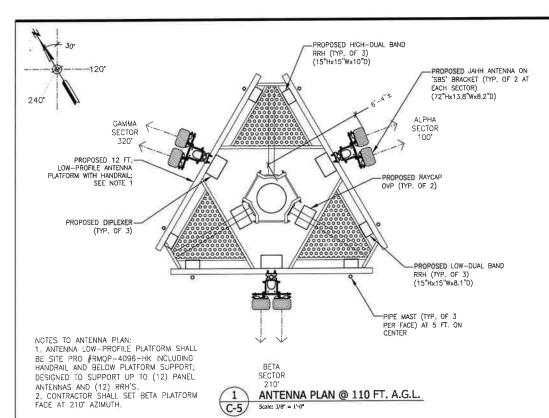
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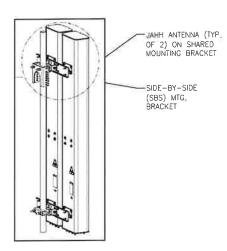
110 YANTIC LANE NORWICH, CT 06360

DRAWING TITLE

**ENVIRONMENTAL NOTES & DETAILS** 







	ANTENNA SPECIFICATION	NS
MODEL #	SIZE	ACCESSORY EQUIPMENT
JAHH-65B-R38	72"Hx13.8"Wx8.2"D; 80 LBS	SIDE-BY-SIDE MOUNTING BRACKET

2 ANTENNA DETAIL
C-5 Scale: N.T.S.



RRH	DIMENS	ONS AWS	/PCS (B66 <sub>/</sub>	/B2)
HEIGHT	WIDTH	DEPTH	WEIGHT	COLOR
15**	15"	10"	84.4 LBS	OFF WHITE





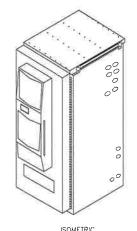
RRH	DIMENSI	ONS 700	/850 (B13/	B5)
HEIGHT	WIDTH	DEPTH	WEIGHT	COLOF
15"	15	8,1"	70.3 LBS	OFF WHITE





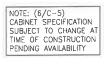
	EQUIPME	ENT SPEC	IFICATIONS	
MODEL #	LENGTH	WIDTH	HEIGHT	WEIGHT
QT025A 25kW	77"	34"	46"	1,414 LBS

5 25kW NAT. GAS GENERATOR Scale: N.T.S.



		130WETKIC		
	EQUIPM	NT SPEC	IFICATIONS	
MODEL #	HEIGHT	WIDTH	DEPTH	WEIGHT
RBA84	85,2"	32.0"	35.4"	1,955 LBS

6 RBA84 EQUIPMENT CABINET
C-5 Scale: 3/8" = 1'-0'

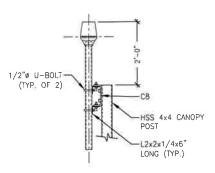




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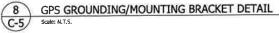
	EQUIPM	ENT SPEC	IFICATIONS	
MODEL #	HEIGHT	WIDTH	DEPTH	WEIGHT
760238731	6"	32"	36.63"	-





### NOTES:

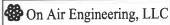
- 1. THE GPS ANTENNA MOUNT IS DESIGNED TO FASTEN TO A STANDARD 2-1/2\* DIAMETER, SCHEDULE 40, GALVANIZED STEEL OR STAINLESS STEEL PIPE. THE PIPE MUST NOT BE THREADED AT THE ANTENNA MOUNT END. THE PIPE SHALL BE CUT TO THE REQUIRED LENGTH (MINIMUM OF Z4 INCHES) USING A HAND OR ROTARY PIPE CUTTER TO ASSURE A SMOOTH AND PERPENDICULAR CUT, A HACK SAW SHALL NOT BE USED. THE CUT PIPE END SHALL BE DEBURRED AND SMOOTH IN ORDER TO SEAL AGAINST THE NEOPRENE GASKET ATTACHED TO THE ANTENNA MOUNT.
- 2. ATTACH TO POST NEAREST EQUIPMENT WITH CLEAN VIEW OF SKY.
- 3. PRIOR TO INSTALLATION CONTRACTOR SHALL TEST GPS LOCATION WITH HAND HELD AND MOVE GPS ANTENNA TO OTHER ICE BRIDGE POSTS AS REQUIRED TO ACHIEVE ADEQUATE SIGNAL, FAILURE TO ACHIEVE ADEQUATE SIGNAL WITH A HAND HELD GPS SHALL BE REPORTED TO CONSTRUCTION MANAGER AND ENGINEER TO DETERMINE ALTERNATE INSTALLATION LOCATION FOR GPS ANTENNA.



Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD, CT 06492



88 Foundry Pond Road Cold Spring, NY 10516 onair@optonline.net 201-456-4624

LICENS



DAVID WEINPALL, P.E.

10:	DATE:	SUBMISSIONS
0	08,20,21	D&M REVIEW SET
1	09.02.21	D&M FILING SET
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MF CHECKED BY:

DW

NEW BUILD MACRO

SITE NAME

NORWICH 4 CT

PROJECT INFORMATION:

110 YANTIC LANE NORWICH, CT 06360

DRAWING TITLE

ANTENNA PLAN & DETAILS

FET NUMBER

C-5

### GENERAL STRUCTURAL NOTES:

1. ALL EQUIPMENT SHALL BE INSTALLED PLUMB AND LEVEL.

2. ALL WIDE FLANGE STRUCTURAL STELL SHALL CONFORM WITH A992 SPECIFICATIONS. ALL STRUCTURAL STEEL SHALL BE FABRICATED AND ERECTED IN ACCORDANCE WITH THE LATEST AISC CODE AND ASTM SPECIFICATION, STEEL SHALL CONFORM TO ASTM A-36. PIPE SHALL CONFORM TO ASTM A-501 OR ASTM TYPE EOR S A-53 (GRADE B).

3. ALL CONNECTIONS OF STRUCTURAL STEEL MEMBERS SHALL BE MADE USING SPECIFIED WELDS WITH WELDING ELECTRODES E-70XX OR SPECIFIED HIGH STRENGTH BOLTS TO BE ASTM A325, THREAD EXCLUDED FROM SHEAR PLANE.

A ALL STEEL EXPOSED TO MOISTURE SHALL BE HOT DIPPED GALVANIZED AFTER FABRICATION PER ASTM A-123. ALL DAMAGED SURFACES, WELDED AREAS AND AUTHORIZED NON-GALVANIZED MEMBERS OR PARTS (EXISTING OR NEW) SHALL BE PAINTED WITH 2 COATS OF ZRC COLD GALVANIZING COMPOUND MANUFACTURED BY ZRC CHEMICAL PRODUCTS CO. QUINCY, MA, OR USE THERMAL SPRAYING WITH PLATTZINC 85/15 AS MANUFACTURED BY PLATT BROTHERS & COMPANY, WATERBURY, CT 1-800-752-8276.

5, ALL SHOP AND FIELD WELDING SHALL BE DONE BY WELDERS QUALIFIED AS DESCRIBED IN THE "AMERICAN WELDING SOCIETY'S STANDARD QUALIFICATION PROCEDURE" TO PERFORM THE TYPE OF WORK REQUIRED.

6, ALL PIPE SIZES ARE NOMINAL DIAMETER (INSIDE DIAMETER)

### CAST-IN-PLACE CONCRETE:

1. ALL CONCRETE WORK SHALL CONFORM TO THE LATEST EDITION OF THE ACI BUILDING CODE.

2. ALL CONCRETE SHALL ATTAIN 4000 PSI COMPRESSIVE

3. READY MIX: COMPLY WITH ACI-301 AND ASTM C-94. ALL CONCRETE EXPOSED TO THE GROUND OR WEATHER SHALL BE

4. COLD WEATHER CONCRETE POURING SHALL BE IN ACCORDANCE WITH ACI-306.

5. THROUGHOUT CONSTRUCTION THE CONCRETE WORK SHALL BE ADEQUATELY PROTECTED AGAINST DAMAGE DUE TO EXCESSIVE LOADING, CONSTRUCTION EQUIPMENT, MATERIALS OR THODS, ICE, RAIN, SNOW, EXCESSIVE HEAT AND FREEZING TEMPERATURES.

6 EARLY DRYING OUT OF CONCRETE, ESPECIALLY DURING THE FIRST 24 HOURS, SHALL BE CAREFULLY GUARDED AGAINST. ALL SURFACES SHALL BE PROTECTED USING MOIST CURING OR A MEMBRANE CURING AGENT APPLIED AS SOON AS FORMS ARE REMOVED OR FINISHING OPERATIONS ARE COMPLETE. CARE SHALL BE EXERCISED SO AS NOT TO DAMAGE

7. APPLY NON-SLIP BROOM FINISH IMMEDIATELY AFTER TROWEL FINISHING:

8. CONTRACTOR TO COORDINATE REQUIREMENTS OF STRUCTURAL, CIVIL, MECHANICAL AND ELECTRICAL DRAWINGS INCLUDING ANY AND ALL PENETRATIONS SPECIFIED PRIOR TO POURING CONCRETE.

9: CONTRACTOR SHALL PROVIDE A 3/4" CHAMFER ON ALL CONCRETE SLABS

### REINFORCING:

1. ALL REINFORCING BAR SHALL CONFORM TO THE LATEST ACI CODE AND DETAILING MANUAL

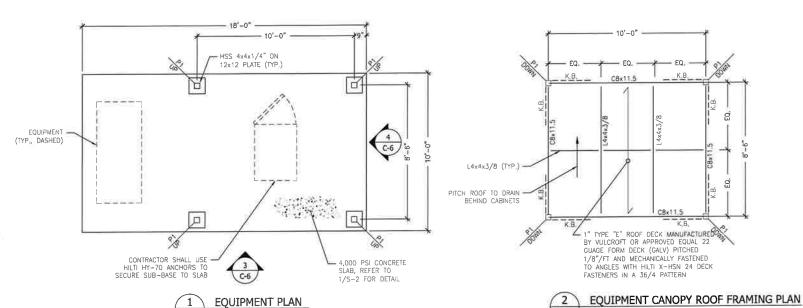
2. WHERE REINFORCING IS CALLED OUT IN THE CONSTRUCTION DOCUMENTS IT SHALL BE 3" CLEAR COVER (MINIMUM UNLESS OTHERWISE NOTED).

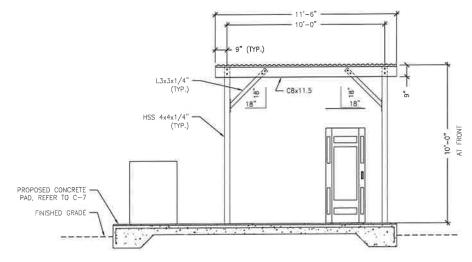
3. ALL BARS SHALL BE ASTM A-615, GRADE 60.

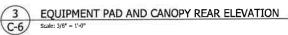
4. WELDED WIRE FABRIC SHALL BE ASTM A-185...

5. WHERE CONTINUOUS BARS ARE CALLED FOR, THEY SHALL BE RUN CONTINUOUSLY AROUND CORNERS AND LAPPED AT NECESSARY SPLICES OR HOOKED AT DISCONTINUOUS ENDS. LAP SHALL BE 40 BAR DIAMETERS.

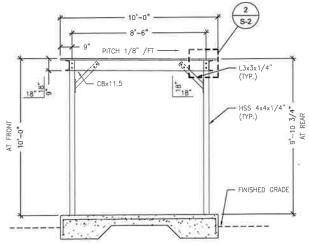
FOOTINGS SHALL BEAR ON UNDISTURBED SOIL AND /OR SUPERVISED COMPACTED FILL, FREE OF FROST, HAVING A MINIMUM ALLOWABLE BEARING CAPACITY OF 1 1/2 TONS PER SQUARE FOOT







Scale: 1/4" = 1'-0"



EQUIPMENT PAD AND CANOPY SIDE ELEVATION C-6 Scale: 3/8" = 1'-0"

PLAN NOTES

GENERAL C	DIMENSIONS, ELEVATIONS, EXISTING FRAMING MEMBER SIZES AND CONDITIONS PRIOR TO COMMENCEMENT OF WORK, NOTIFY ENGINEER OF ANY DISCREPANCIES BETWEEN THESE DRAWINGS AND EXISTING
CONDITIONS	56
SYMBOL	DESCRIPTION
-37	INDICATES HSS4x4x1/4 ASTM ASOO GR. B (Fy=48ksi) STEEL POST.
	INDICATES SPAN DIRECTION
K.B.	INDICATES L3x3x1/4 ASTM A36 (Fy=36ksi) STEEL ANGLE

Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD CT 06492



On Air Engineering, LLC

88 Foundry Pond Road Cold Spring, NY 10516 onair@optonline.net 201-456-4624

LICENSURE



DAVID WEINPALL, P.E.

NO.:	DATE:		SUBMISSIONS
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MF			DW

**NEW BUILD** MACRO

NORWICH 4 CT

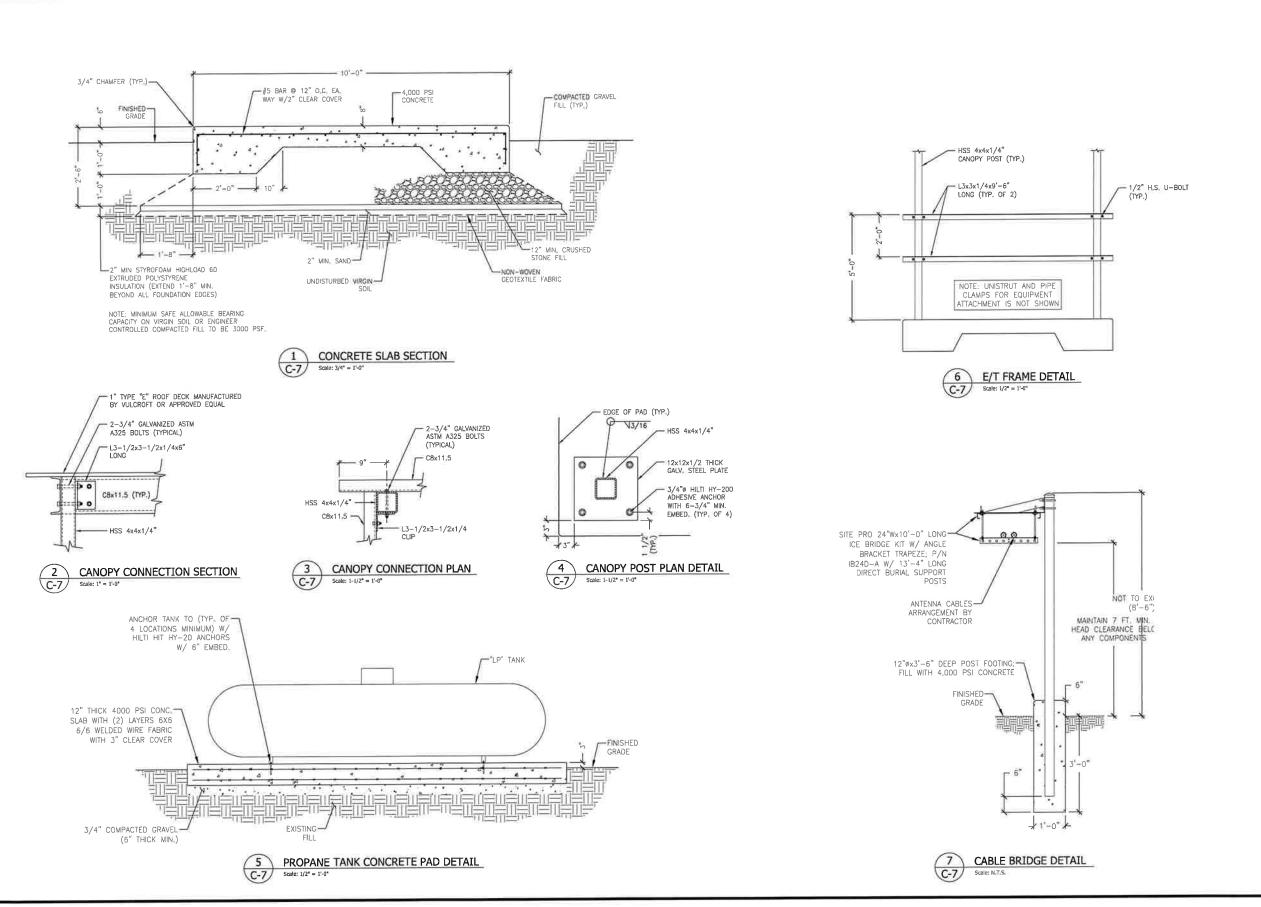
PROJECT INFORMATION:

110 YANTIC LANE NORWICH, CT 06360

DRAWING TITLE:

STRUCTURAL EQUIPMENT PLAN & ELEVATIONS

SITEET NUMBER:



Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD, CT 06492



On Air Engineering, LLC

88 Foundry Pond Road Cold Spring, NY 10516 onair@optonline.net 201-456-4624



DAVID WEINPAILL, P.E.

NO:	DATE:	SUBMISSIONS	
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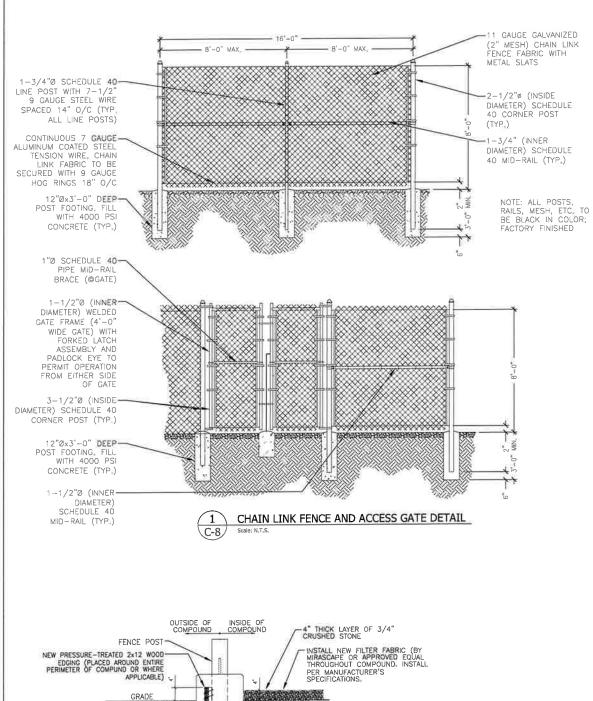
> **NEW BUILD** MACRO

NORWICH 4 CT

PROJECT INFORMATION:

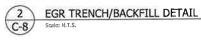
110 YANTIC LANE NORWICH, CT 06360

STRUCTURAL DETAILS



FINISHED GRADE TO MATCH EXISTING CONDITIONS. BACKFILL SHALL BE 'FREE-DRAINING MATERIAL' PER STATE OF CONN. D.O.T. STAND SPECS FOR ROADS, BRIDGE AND INCIDENTAL CONSTRUCTION FORM 814A - 1995 - SEC M.02.07: FREE DRAINING MATERIALS. #2 SOLID TINNED BARE COPPER. BACKELL SHALL BE-NATURAL CLAY. NOTES:

- ENGINEER SHALL INSPECT PLACEMENT OF EGR CONDUCTOR PRIOR TO BACKFILLING.
- MAINTAIN MIN. 2'-0" LINEAR CLEARANCE BETWEEN NATURAL CLAY BACKFILL AND THE FOLLOWING: FOUNDATION, UNDERGROUND PIPING/CONDUIT, UNDERGROUND SERVICES, IN THE CLEARNICE AREAS, USE EARTH BACKFILL INSTEAD.
- 3 EXERCISE HANDLING AND USE PRECAUTION OF BACKFILL MATERIAL PER MFR'S REQUIREMENTS.



SEC. 16-50J-77. REPORTING REQUIREMENTS

(a) SUPERVISORY PERSONNEL,
THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL SUBMIT TO THE
COUNCIL CONTACT INFORMATION FOR THE PERSONNEL OF THE CONTRACTOR ASSIGNED TO THE PROJECT.

(b) NOTICE.

(1) THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL PROVIDE THE COUNCIL, IN WRITING, WITH A MINIMUM OF TWO WEEKS ADVANCE NOTICE OF THE

BEGINNING OF:

(A) CLEARING AND ACCESS WORK, AND

(B) CONSTRUCTION OF THE TOWER AND ASSOCIATED EQUIPMENT.

(2) THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL PROVIDE THE COUNCIL WITH ADVANCE WRITTEN NOTICE WHENEVER A SIGNIFICANT MODIFICATION OF THE APPROVED D&M PLAN IN NECESSARY INCLUDING, BUT NOT LIMITED TO, A CHANGE IN THE LOCATION OF THE TOWER, ASSOCIATED EQUIPMENT, GUY WIRES, OR ACCESS ROAD, THE COUNCIL, OR ITS DESIGNEE SHALL PROMPTLY REVIEW THE CHANGES, AND THE COUNCIL SHALL APPROVE, MODIFY, OR DISAPPROVE THE CHANGES IN ACCORDANCE WITH SUBSECTION (d) OF SECTION 16-50J-75 OF THE REGULATIONS OF CONNECTICUT STATE AGENCIES. OF CONNECTICUT STATE AGENCIES

(3) THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL PROVIDE THE COUNCIL WITH A MONTHLY CONSTRUCTION PROGRESS REPORT, OR A CONSTRUCTION PROGRESS REPORT, OR A CONSTRUCTION PROGRESS REPORT AT THE TIME INTERVALS DETERMINED BY THE COUNCIL, INDICATING CHANGES AND DEVIATIONS FROM THE APPROVED D&M PLAN. THE COUNCIL MAY APPROVE THE CHANGES AND DEVIATIONS OR REQUEST CORRECTIONS OR MITIGATING MEASURES.

(4) THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL PROVIDE THE COUNCIL WITH WRITTEN NOTICE OF COMPLETION OF CONSTRUCTION AND SITE REHABILITATION.

(c) FINAL REPORT.
THE CERTIFICATE HOLDER, OR FACILITY OWNER OR OPERATOR, SHALL PROVIDE THE COUNCIL WITH A FINAL REPORT NOT LATER THAN 180 DAYS AFTER COMPLETION OF ALL SITE CONSTRUCTION AND SITE REHABILITATION. THIS FINAL REPORT SHALL

- (1) ALL AGREEMENTS WITH ABUTTERS OR OTHER PROPERTY OWNERS REGARDING SPECIAL MAINTENANCE PRECAUTIONS;
- (2) SIGNIFICANT MODIFICATIONS OF THE D&M PLAN THAT WERE REQUIRED BECAUSE OF THE PROPERTY RIGHTS OF UNDERLYING AND ADJOINING OWNERS OR FOR OTHER
- REASONS;
  (3) THE LOCATION OF CONSTRUCTION MATERIALS WHICH HAVE BEEN LEFT IN PLACE IN THE FORM OF CULVERTS, EROSION CONTROL STRUCTURES ALONG WATERCOURSES AND STEEP SLOPES, AND CORDUROY ROADS IN REGULATED WETLANDS;
  (4) THE LOCATION OF SPECIAL AREAS WHERE SPECIAL PLANTING AND RESEEDING

(5) AGREEMENTS BETWEEN THE CERTIFICATE HOLDER AND PUBLIC AGENCIES AUTHORIZING PUBLIC RECREATIONAL USE OF THE SITE TO THE EXTENT OF THE CERTIFICATE HOLDER'S PROPERTY RIGHTS THERETO.

- (d) THE FINAL REPORT SHALL INCLUDE THE ACTUAL CONSTRUCTION COST OF THE TOWER AND ASSOCIATED EQUIPMENT, INCLUDING, BUT NOT LIMITED TO, THE FOLLOWING COSTS;
- (1) CONSTRUCTION OF THE TOWER AND ASSOCIATED EQUIPMENT;
- (2) SITE REHABILITATION; AND
- (3) PROPERTY ACQUISITION FOR SITE OR ACCESS TO SITE.

FINISHED GRADE TO MATCH EXISTING CONDITIONS BACKFILL W/SUITABLE MATERIAL COMPACTED TO 95% MAXIMUM DENSITY (ASTM D 1557) CABLE WARNING TAPE (RED) COVER SCREENED SAND BEDDING BURIED CONDUIT(S) 12" NOTES:

1. THE CLEAN FILL SHALL PASS THROUGH A 3/8" MESH SCREEN AND SHALL NOT CONTAIN SHARP STONES. OTHER BACKFILL SHALL NOT CONTAIN ASHES, CINDERS, SHELLS, FROZEN MATERIAL, LOOSE DEBRIS OR STONES LARGER THAN 2" IN MAXIMUM DIMENSION.

2. WHERE EXISTING UTILITIES ARE LIKELY TO BE ENCOUNTERED, CONTRACTOR SHALL HAND DIG AND PROTECT EXISTING UTILITIES.

3. REFER TO PLANS FOR FINAL QUANTITY OF CONDUITS (POWER & TELCO).

4. ALL CONDUITS SEPARATIONS SHALL BE IN ACCORDANCE WITH MEC & UTILITY CO. REQUIREMENTS.



Cellco Partnership d/b/a Verizon Wireless



WIRELESS COMMUNICATIONS FACILITY 20 ALEXANDER DRIVE WALLINGFORD CT 06492



Cold Spring, NY 10516 ongir@optonline.net 201-456-4624

CENSURE



NO:	DATE:	SUBMISSIONS
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**NEW BUILD MACRO** 

**NORWICH 4 CT** 

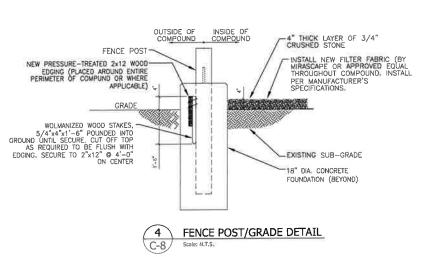
PROJECT INFORMATION:

110 YANTIC LANE NORWICH, CT 06360

DRAWING TITLE

SITE DETAILS & CSC REPORTING NOTES

SHEET NUMBER





1 Fairholm Avenue Peoria, IL 61603 USA Phone: (309)-566-3000 (309)-56G-3079 Fax:

DATE:

JULY 28, 2021

**PURCHASER: VERIZON WIRELESS** 

PROJECT:

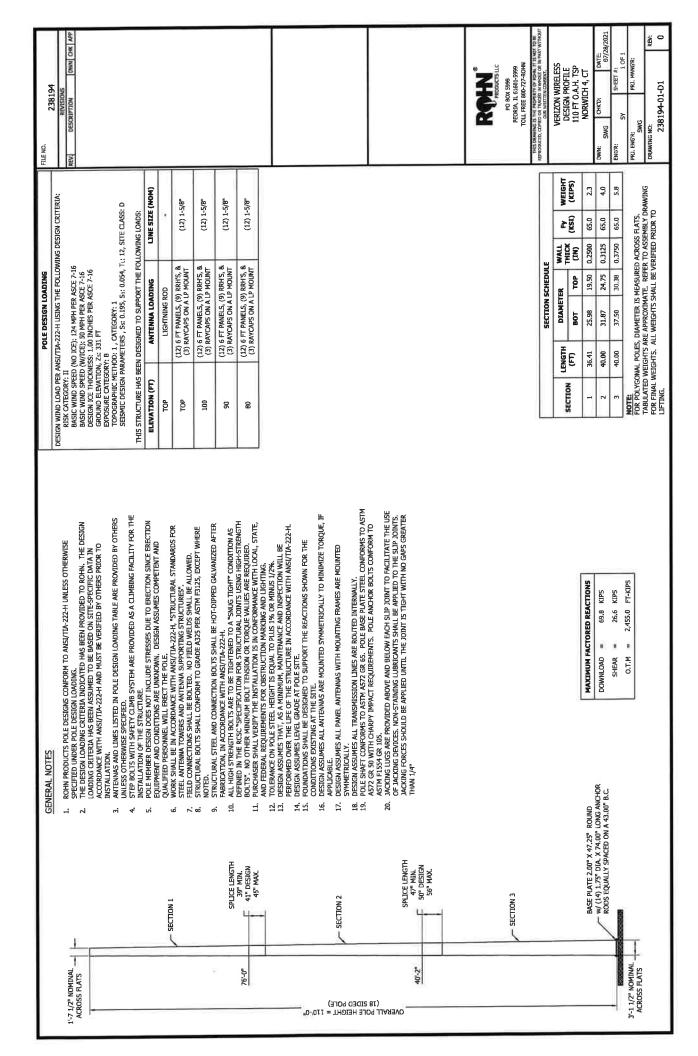
110FT TSP

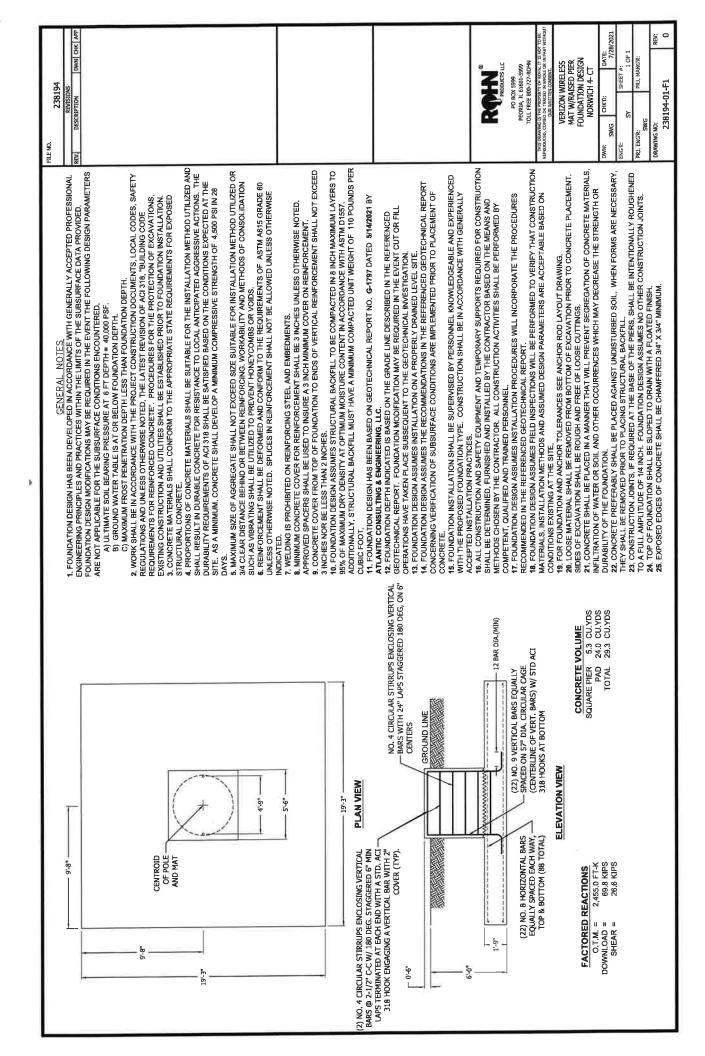
**NORWICH 4, CT** 

**FILE NUMBER: 238194** 

I CERTIFY THAT THE ATTACHED DRAWINGS WERE PREPARED UNDER MY SUPERVISION IN ACCORDANCE WITH THE DESIGN AND LOADING CRITERIA SPECIFIED BY THE PURCHASER AND THAT I AM A REGISTERED PROFESSIONAL ENGINEER UNDER THE LAWS OF THE STATE OF CONNECTICUT.









Licensed to: ROHN Products LLC

Peoria, IL

File: W:\Jobs\2021\238194\ENGINEERING\238194.out

Contract: 238194 Project: 110 FT O.A.H. TSP

Date and Time: 7/27/2021 3:51:12 PM

### Section A: PROJECT DATA

Project Title: Customer Name: 110 FT O.A.H. TSP VERIZON WIRELESS NORWICH 4- CT

Site:

238194 0 Contract No.: Revision: SWG

Engineer: Date: Time:

Jul 27 2021 03:50:45 PM

Design Standard:

ANSI/TIA-222-H-2017

### GENERAL DESIGN CONDITIONS

Start wind direction: End wind direction: Increment wind direction: Elevation above ground: Mean elevation of base of structure above	0.00 (Deg) 315.00 (Deg) 45.00 (Deg) 0.00 (ft) sea level Zs: 331.00 (ft)
Rooftop wind speed-up factor Ks: Gust Response Factor Gh: Risk category: Exposure category: Topographic category: Material Density: Young's Modulus: Poisson Ratio: Weight Multiplier:	1.00 1.10 II B 1 490.1(lbs/ft^3) 29000.0(ksi) 0.30 1.06

WIND ONLY CONDITIONS:	
Basic Wind Speed (No Ice):	124.00 (mph)
Directionality Factor Kd:	0.95
Importance Factor I:	1.00
Wind Load Factor:	1.00
Dead Load Factor:	1.20

WIND AND ICE CONDITIONS:	
Basic Wind Speed (With Ice):	50.00(mph)
Directionality Factor Kd:	0.95
Wind Load Importance Factor Iw:	1.00
Ice Thickness Importance Factor Ii:	1.00
Ice Thickness:	1.00 (in)
Ice Density:	56.19(lbs/ft^3)
Wind Load Factor:	1.00
Dead Load Factor:	1.20
Ice Load Factor:	1.00

WIND ONLY SERVICEABILITY CONDITIONS:	
Serviceability Wind Speed:	60.00(mph
Directionality Factor Kd:	0.85
Importance Factor I:	1.00
Wind Load Factor:	1.00
Dead Load Factor:	1.00

EARTHQUAKE CONDITIONS:	
Site class definition:	D
Spectral response acceleration Ss:	0.195
Spectral response acceleration S1:	0.054
Long-period transition period TL:	6.000
Accelaration-based site coefficient Fa:	1:600
Velocity-based site coefficient Fv:	2.400

Page A 1

Revision: 0

Site: NORWICH 4- CT

Engineer: SWG

**ENGINEERING** CHECKED BY: SY 07/28/2021



Desducts
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Peoria, IL

Revision: 0

Engineer: SWG

Site: NORWICH 4- CT

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Contract: 238194

Project: 110 FT O.A.H. TSP

Date and Time: 7/27/2021 3:51:12 PM

Design spectral response acceleration Sds: 0.208
Design spectral response acceleration Sd1: 0.086
Seismic analysis method: 1
Fundamental frequency of structure f1: 0.369
Total seismic shear Vs (Kips): 0.97

Analysis performed using: TowerSoft Finite Element Analysis Program



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Contract: 238194

Project: 110 FT O.A.H. TSP Date and Time: 7/27/2021 3:51:12 PM

Revision: 0

Site: NORWICH 4- CT

Engineer: SWG

### Section B: STRUCTURE GEOMETRY

Total (ft) 109.00	Height		tom Diamet n) 50		Diameter n) 50						
Sect:	Length	Overlap	Bot Dia.	Top Dia.	Thick.	Sides	Joint Type	Yield Stress	Mass	Calculated Taper	Corner Radius
No	(ft)	(ft)	(in)	(in)	(in)			(ksi)	(lbs)	(in/ft)	(in)
3 2 1	36.41 40.00 40.17	0.00 3.42 4.17	25.89 31.81 37.50	19.50 24.79 30.45	0.2500 0.3125 0.3750	18-sided 18-sided 18-sided	Telescopic Telescopic Flange	65.0 65.0 65.0	2339.4 4005.3 5795.1	0.17546 0.17546 0.17546	2.38 2.50 2.63
Total	Mass:								12139.7		



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Peoria, IL

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Contract: 238194

Project: 110 FT O.A.H. TSP

Date and Time: 7/27/2021 3:51:12 PM

Revision: 0

Site: NORWICH 4- CT

Engineer: SWG

### Section D: TRANSMISSION LINE DATA

Transmission Lines Position

No.	Bot El (ft)	Top El	Desc.	Radius (ft)	Az.	Orient.	No.	Shielded	Shielded Lines	Antenna
1 2 3 4	0.00 0.00 0.00 0.00	110.00 110.00 100.00 90.00 80.00	3/8" CABLE LDF7P-50A LDF7P-50A LDF7P-50A LDF7P-50A	2.00 0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00	0.00 0.00 0.00 0.00 0.00	1 12 12 12 12	No Yes Yes Yes Yes	0 12 12 12 12	

### Transmission Lines Details

No .	Desc.	Width (in)	Depth (in)	Unit Mass (lb/ft)
1	3/8" CABLE	0.38	0.38	1.00
2	LDF7P-50A	2.01	2.01	0.92
3	LDF7P-50A	2.01	2.01	0.92
4	LDF7P-50A	2.01	2.01	0.92
5	LDF7P-50A	2.01	2.01	0.92

Utilization of the cross-section for TX Lines: 33.14%



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Contract: 238194

Project: 110 FT O.A.H. TSP
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Revision: 0

Sîte: NORWICH 4- CT

Engineer: SWG

### Section F: POINT LOAD DATA

Structure Azimuth from North:0.00

### POINT LOADS

No.	Description	Elev.	Radius	Azim.	Orient,	Vertical Offset	Tx Line	Comments
1 2 3 4 5	LIGHTNING ROD CARRIER CARRIER CARRIER CARRIER CARRIER	(ft) 110.00 110.00 100.00 90.00 80.00	(ft) 0.00 0.00 0.00 0.00 0.00	(Deg) 0.0 0.0 0.0 0.0 0.0	(Deg) 0.0 0.0 0.0 0.0 0.0	(ft) 0.00 0.00 0.00 0.00 0.00		

### POINT LOADS WIND AREAS AND WEIGHTS

No.	Description	Frontal Bare Area (ft^2)	Lateral Bare Area (ft^2)	Frontal Iced Area (ft^2)	Lateral Iced Area (ft^2)	Weight Bare (Kips)	Weight Iced (Kips)	Gh
1 2 3 4	LIGHTNING ROD CARRIER CARRIER CARRIER CARRIER	1.00 132.50 132.50 132.50 132.50	1.00 132.50 132.50 132.50 132.50	2.00 195.50 195.50 195.50 195.50	2.00 195.50 195.50 195.50 195.50	0.10 3.95 3.95 3.95 3.95	0.20 10.60 10.60 10.60 10.60	1.10 1.10 1.10 1.10 1.10



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Revision: 0 Site: NORWICH 4- CT

Engineer: SWG

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Contract: 238194

Project: 110 FT O.A.H. TSP
Date and Time: 7/27/2021 3:51:12 PM

Section H: STRUCTURE DISPLACEMENT DATA
Load Combination Wind Only - Serviceability

Wind Dire	ection		Maximum displacements			
Elev. (ft)	N-S Disp (in)	W-E Disp (in)	Vert.Disp (in)	N-S Rot (deg)	W-E Rot (deg)	Twist Rot (deg)
109.00 102.40 95.80 89.20 82.60 72.59 66.10 59.62 59.62 40.17 36.00 30.00 24.00 18.00 12.00 6.00 0.00	24.3 21.8 19.3 16.8 14.5 12.3 11.2 9.3 7.5 5.9 4.5 3.3 2.7 1.8 1.2 0.7 0.3	-24.2 -21.7 -19.2 -16.8 -14.4 -12.2 -11.1 -9.2 -7.5 -5.9 -4.5 -3.3 -2.6 -1.8 -1.2 -0.7 -0.3 -0.1	-0.3 -0.2 -0.2 -0.2 -0.1 -0.1 -0.1 -0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	-1.83 -1.82 -1.79 -1.73 -1.65 -1.54 -1.36 -1.23 -1.09 -0.95 -0.80 -0.71 -0.59 -0.47 -0.35 -0.23 -0.11 0.00	-1.84 -1.83 -1.79 -1.74 -1.65 -1.54 -1.36 -1.23 -1.10 -0.95 -0.81 -0.71 -0.59 -0.47 -0.35 -0.23 -0.11	0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00



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Revision: 0

Engineer: SWG

Site: NORWICH 4- CT

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Contract: 238194

Project: 110 FT O.A.H. TSP
Date and Time: 7/27/2021 3:51:12 PM

Section K: POLE OUTPUT LOAD DATA Load Combination Max Envelope Maximum Wind Direction

Willia Direc	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
Elev. (ft)	Axial Ld. (kips)	Shear Ld. (kips)	Torque (kipsft)	Bend Mom. (kipsft)
(ft)  109.00 102.40 102.40 95.80 95.80 89.20 89.20 82.60 76.00 76.00 72.59 72.59 66.10 66.10 59.62 59.62 53.14 46.65 40.17 40.17 36.00	(kips)  11.92 11.92 19.92 19.92 26.29 26.29 37.23 37.23 45.18 45.18 50.53 50.53 50.53 51.70 51.70 53.23 54.63 54.63 55.53 57.53 57.53 57.53 58.76 58.76	(kips) 6.36 6.36 10.53 10.53 13.77 13.77 19.20 22.90 22.90 22.90 25.29 25.50 25.50 25.74 25.74 25.93 26.07 26.18 26.18 26.25 26.25	(kipsft)  0.00 0.00 0.01 0.01 0.02 0.01 0.03 0.02 0.04 0.03 0.05 0.07 0.06 0.07 0.06 0.07 0.07 0.07 0.07	(kipsft) 5.53 47.06 47.13 115.84 115.93 205.76 205.88 331.19 331.34 480.79 480.91 567.15 567.27 730.44 730.59 896.21 896.34 1062.39 1062.50 1230.46 1230.56 1399.35 1399.42 1508.03
36.00	60.37	26.32	0.07	1508.09
30.00	60.37	26.32	0.07	1665.14
30.00	62.29	26.39	0.07	1665.20
24.00	62.29	26.39	0.07	1821.93
24.00	63.91	26.42	0.07	1821.97
18.00	63.91	26.42	0.07	1979.90
18.00	65.56	26.43	0.07	1979.93
12.00	65.56	26.43	0.07	2138.11
12.00	67.24	26.43	0.07	2138.12
6.00	67.24	26.43	0.07	2296.49
6.00	68.94	26.42	0.07	2296.49
0.00	68.94	26.42	0.07	2454.97
Base	69.78	26.58	0.07	2454.98



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Contract: 238194
Project: 110 FT O.A.E. TSP
Date and Time: 7/27/2021 3:51:12 PM

Revision: 0 Site: NORWICE 4- CT Engineer: SWG

#### Section L: STRENGTH ASSESSMENT DATA Max Envelope Load Combination Maximum Wind Direction

Elev.	Axial Ld.	Axial Cap	Moment	Mom. Cap	Assess
(ft)	(kips)	(kips)	(kipsft)	(kipsft)	
(ft)  109.00 102.40 102.40 95.80 99.20 89.20 89.20 82.60 76.00 76.00 76.00 59.62 59.62 59.62 59.62 59.61 46.65 40.17 40.17 36.00 30.00 24.00 24.00 18.00 18.00 12.00 6.00	(kips)  11.92 11.92 19.92 19.92 26.29 37.23 45.18 45.18 50.53 51.70 53.23 53.23 54.63 56.06 56.06 56.05 57.53 58.76 60.37 60.37 60.29 63.91 65.56 65.56 67.24	(kips)  1134.81 1203.07 1203.07 1271.33 1339.59 1339.59 1407.85 1407.85 1407.85 1407.85 1407.85 1276.11 1476.11 1847.87 1931.70 1931.70 1931.70 2015.52 2015.52 20199.34 2099.34 2183.17 2266.99 2724.25 2817.35 2817.35 2817.35 2910.45 3003.54 3003.54 3096.64 3096.64 3096.64	(kipsft) 5.53 47.06 47.13 115.84 115.93 205.76 205.88 331.19 331.34 480.79 480.91 567.27 730.44 730.59 896.21 896.21 896.21 896.34 1062.50 1230.46 1399.35 1399.42 1508.09 1665.14 1665.20 1821.93 1821.97 1979.90 1979.93 2138.11 22396.49	(kipsft)  447.11 502.87 502.87 561.91 624.23 624.23 629.82 758.69 758.69 91037.48 1130.01 1226.50 1326.94 1431.33 1719.13 1431.33 1719.13 1839.35 1863.63 1963.63 1963.63 1963.63 2091.98 2224.39 2224.39 22360.87	0.017 0.098 0.101 0.213 0.339 0.344 0.493 0.650 0.653 0.613 0.718 0.719 0.807 0.808 0.881 0.942 0.992 0.992 0.992 0.992 0.991 0.918 0.940 0.941 0.941 0.959 0.959 0.974 0.985
6.00	68.94	3189.74	2296.49	2360.87	0.986
0.00	68.94	3282.84	2454.97	2501.40	0.994



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Revision: 0

Site: NORWICE 4- CT

Engineer: SWG

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Project: 110 FT O.A.H. TSP
Date and Time: 7/27/2021 3:51:12 PM

### Section M: SECTION PROPERTIES DATA

Elev. (ft)	Diam. (in)	Width (in)	Thick.	W/t	Area (in^2)	s (in^3)
109.0 102.4 102.4 95.8 95.8 89.2 82.6 76.0 72.6 66.1 66.1 66.1 46.7 40.2 40.2 40.0 30.0 24.0 18.0 12.0 66.0	19.5 20.7 20.7 21.8 23.0 23.0 24.1 25.3 25.4 26.5 27.7 28.8 29.9 31.8 31.8 32.2 33.3 33.3 33.3 33.3 35.4 36.4	2.33.33.36.6880019113355779907991133555555555555555555555555555555555	0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.250 0.313 0.313 0.313 0.313 0.313 0.313 0.313 0.313 0.313 0.313 0.375 0.375 0.375 0.375 0.375	11.8 12.6 13.4 13.4 14.2 15.0 15.8 16.3 12.3 13.6 13.6 13.6 14.9 14.9 15.5 15.9 17.7 13.7 13.7 13.7 13.7 14.1 14.6 14.6 15.1	15.3 16.2 17.1 17.1 18.0 18.9 18.9 20.3 24.9 226.0 27.1 27.1 28.3 29.4 29.4 29.4 330.5 31.2 36.7 37.9 39.2 40.4 41.7 41.7 42.9	72.22 81.22 90.76 90.76 100.82 111.42 111.42 111.42 122.54 122.54 128.51 153.26 167.57 182.52 182.52 198.10 214.32 231.19 242.36 277.67 297.09 237.69 337.89 337.89 359.28 359.28 359.28 381.32 381.32
0.0	37.5	5.9	0.375	15.6	44.2	404.02

Note: w/t values marked with \* (asterisk) indicate width to thickness exceeding maximum allowable values by standards.



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Contract: 238194

Project: 110 FT O.A.H. TSP

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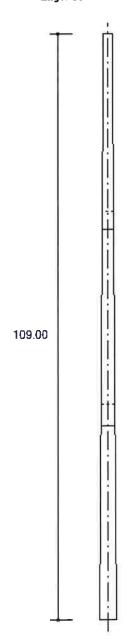
Revision: 0

Site: NORWICH 4- CT

Engineer: SWG

### **DESIGN SPECIFICATION**

Sct.	Length (ft)	Overlap (ft)	Top Dia (in)	.Bot Dia. (in)	Thick.
3	36.41	0.00	19.50	25.89	0.2500
2	40.00	3.42	24.79	31.81	0.3125
1	40.17	4.17	30.45	37.50	0.3750



### MAXIMUM BASE REACTIONS

Download (Kips)				
Shear (Kips)				
Moment (Kipsft)				

Customer: VERIZON WIRELESS
Project: 110 FT O.A.H. TSP
Site: NORWICH 4- CT

Engr. File: 238194

Build Code: ANSI/TIA-222-H-2016



### **Mat Foundation**

ver.2.2.15

### **Design Parameters**

			Load	Case		
Description	1	2	3	4	5	Service
Total Moment, ft-kips	2,454.98	2,408.22	684.00	96.79	94.03	510.40
Total Shear, kips	26.58	26.53	6.94	.98	.98	5.56
Total Tower Wt, kips	38.71	29.01	69.78	40.19	27.79	32.36
Max. Uplift, kips	N/A	N/A	N/A	N/A	N/A	N/A
Shear, kips	N/A	N/A	N/A	N/A	N/A	N/A
Max Download, kips	N/A	N/A	N/A	N/A	N/A	N/A
Shear	N/A	N/A	N/A	N/A	N/A	N/A
Soil L.F.	1.20	0.90	1.20	1.20	0.90	1.00
Concrete L.F.	1.20	0.90	1.20	1.20	0.90	1.00

Foundation	
Ht. AGL, ft	0.50
Depth, ft.	6.00
Pole	
Butt OD, ft	3.13
Offset, in	.00
Soil	N/A
Blow Count	N/A
Inplace Unit Wt, pcf	110.00
Submerged Unit Wt, pcf	60.00
Friction Angle, φ, deg.	30.00
Cohesion, ksf	N/A
Uplift Angle, deg.	30.00
Water Depth, ft	None
Ult Bearing Capacity, ksf	40.00

Mat	
Thickness, ft	1.75
Width, ft	19.25
EA, in	15.00
Batter, in/ft	0.00

Anchor Bolts	
Diameter, in	1.7500
No.	14
Length, in	74.00
Bolt Circle, in	42.88
Projection, in	9.00
Concrete	
28 Day Strength, ksi	4.50
Dry Unit Wt, pcf	150.00
Wet Unit Wt, pcf	88.00

Pier	
Height, ft	4.75
Diameter, ft	5.50
No. Piers	1
Shape	Square

Pocket	
Diameter, in	N/A
Thickness, ft	N/A

Rebar Fy	
Vertical, ksi	60.00
Circular, ksi	60.00
Horizontal, ksi	60.00

### **Results**

 $\begin{array}{lll} \phi \; M_N - \; \text{Parallel Axis} & 2,679.77 & \text{ft-kips} \\ \phi \; M_N - \; \text{Diagonal Axis} & 2,946.67 & \text{ft-kips} \\ \text{Moment} - \; \text{Interaction Ratio} & 0.963 & \end{array}$ 

 $\phi V_N$  – Lateral Load 73.99 kips

Lateral Load – Interaction Ratio 0.359

Final Mat Dimension : 19.25 x 19.25 x 1.75 ft. thick w/ (1) 5.50 ft. Square Pier

Final Pocket Dimension : Pockets not required

Total Volume of Concrete: 29.3 yd3

 Designed By:
 SWG
 Checked By:
 ENGINEERING CHECKED BY: SY

 Date:
 28 Jul,21 @ 08:05 AM
 Date:
 07/28/2021

Page

Customer: VERIZON WIRELESS
Project: 110 FT O.A.H. TSP
Site: NORWICH 4- CT

Engr. File: 238194

Build Code: ANSI/TIA-222-H-2016



### **Mat Foundation**

ver.2.2.15

### **OTM Capacity**

Controlling Load Case: 2 [Wind w/Min. Dead Load]

Foundation Width = 19.25 ft

 $M_U = 2,580.7$  ft-kips

	φM <sub>N</sub> , ft-kips	x, ft	N	σur
Parallel	2,679.8	1.925	0.100	10.78
Diagonal	2,946.7	6.087	0.224	10.78

 $\phi M_N = 2,679.77 \text{ ft-kips}$ 

IRatio = 0.963

 $\phi V_N = 73.99 \text{ kips}$ 

IRatio = 0.359

### **Mat Design**

 $\gamma_e = 121.67 \text{ pcf}$ 

·						Moment, f	t-kips/ft	Shear, ki	ips/ft
Exterior Slab	x, ft	N	σr, ksf	Ps kips	P <sub>su</sub> kips	DownLoad Side	Uplift Side	Download Side	Uplift Side
Parallel	2.515	0.131	6.17	17.67	0.00	71.71	26.91	14.96	6.93
Diagonal	7.867	0.289	4.83	17.67	0.00	45.53	16.07	16.42	5.56

Punching	Download			Uplift		Description	
Shear	Interior	Edge	Corner	Interior	Edge	Corner	Description
b <sub>o</sub> , ft	27.33	N/A	N/A	N/A	N/A	N/A	
Vsu, psi	97.86	N/A	N/A	N/A	N/A	N/A	2-Way Shear
φVc, psi	225.30	N/A	N/A	N/A	N/A	N/A	2-way Shear
IR	0.43	N/A	N/A	N/A	N/A	N/A	
0.5*M <sub>ut</sub> , ft-kips	774.4			N/A		Moment transfer to	
Be, ft	10.8			N/A		slab	
M <sub>u</sub> , ft-kips/ft	72.0			N/A			
	E	lge Distance	s: $a = 9.63$ ft.	b = 9.63  f	t. $c = 9$ .	63 ft.	

Summary	Max. Value	Utilization
Slab Moment, ft-kips/ft	72.03	0.956
Slab Shear, kips/ft	16.42	0.750
Punching Shear, psi	97.86	0.434
Soil Bearing Required, our, ksf	8.23	0.206

Mat Reinforceme	ent
Min. Steel Area (Strength)	.853 in <sup>2</sup> /ft.
Min. Steel Area (Temperature)	.227 in <sup>2</sup> /ft.
Steel Strain Actual	0.014
Minimum Steel Strain Required	0.005

22 - #8 Horizontal bars equally spaced @10.71 in., each way, top and bottom, total of 88,  $A_s = 0.898 \ in^2/ft$ 

Designed By:	SWG	Checked By:	ENGINEERING CHECKED BY: SY	
Date:	28 Jul.21 @ 08:05 AM	Date:	07/28/2021	
		====2		Page ii

**VERIZON WIRELESS** Customer: 110 FT O.A.H. TSP Project: Site: NORWICH 4- CT

238194 Engr. File:

ANSI/TIA-222-H-2016 Build Code:



### **Mat Foundation**

ver.2.2.15

### Pier Design

Controlling Load Case: 1 [Wind w/Max. Dead Load]

C = 38.71 kips

Vc = 26.58 kips

Mc = 2,581.24 ft-kips

T = .00 kips

Vt = .00 kips

Mt = .00 ft-kips

Fy = 60.00 ksi

Fyt = 60.00 ksi

L.F. = 1.00

H = 66.00 in.

Ds = 57.00 in.

F'c = 4.50 ksi

U = 1.00

Irs = Square

\*\*\* NOTE: Pier cross section is Square \*\*\*

### SUMMARY OF ANALYSIS

Minimum area of steel required  $= 21.846 \text{ in}^2$ 

(Rhomin = 0.0050)

Area of steel provided. Maximum steel area limit  $= 21.985 \text{ in}^2$  $= 273.696 \text{ in}^2$  (Rhoactual = 0.0050)(Rhomax = 0.0628)

(22) #9 Vertical Bars equally spaced w/ #5 Circular Ties @ 6" on center.

### CIRCULAR TIE DATA

Vu < 0.85\*Vc/2, shear reinforcement is not required

Use maximum tie spacing specified in ACI 318, Section 7.10.5 for compression reinforcement.

### DEVELOPMENT LENGTH MODIFIERS FOR BAR DEVELOPMENT

Modifier for tension development

Modifier for compression development = 0.603

REQUIRED Ld = MODIFIER \* BASIC Ld \* ACI 318 MODIFIERS, (12 in. min.)

Designed By: SWG

Date: 28 Jul,21 @ 08:05 AM

Checked By: Date:

**ENGINEERING** CHECKED BY: SY 07/28/2021

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## Geotechnical Engineering Report For:

Proposed Telecommunications Tower
Verizon Wireless
Site Name: Norwich 4 CT
110 Yantic Lane
Norwich, CT

Prepared for: David Weinpahl, PE On Air Engineering, LLC

Prepared by:
Atlantic Consulting & Engineering, LLC
525 John Street
Bridgeport, CT 06604

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4.00	SUBS	URFACE CONDITIONS
5.00	IMPLIC	CATIONS OF SUBSURFACE CONDITIONS
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APPENDIX B: SIESMIC SUMMARY

### 1.00 GENERAL SUMMARY

Based on the studies performed as discussed herein, we have prepared the following conclusions and recommendations.

- Variable density naturally deposited inorganic GLACIAL TILL deposits overlying ROCK are
  present in the portions of the proposed construction area that were investigated.
  Liquefaction potential is negligible based on density and gradation of soils, depth of water
  table and rock depth.
- The existing naturally deposited inorganic silt, sand and gravel materials can be used to support the bottom of footings and also may meet gradation requirements for re-use as structural fill.
- 3.) If required, raises in grade materials beneath the footings, slabs and pavement should consist of structural fill.

- 3.) Replacement fills for footing, slab and pavement support as required should consist of "structural fill" as defined in paragraph 7.30 and be placed and compacted to 95 percent of the optimum dry density per ASTM D-1557.
- 4.) Groundwater is NOT expected to impact portions the excavation or cut areas of the proposed project, however the water table is approximately 24 inches below the bottom of work elevation, so precautions must be taken.
- 5.) Footings shall be excavated to naturally deposited inorganic materials as defined herein and the grade can be raised using structural fill since the acceptable bearing material is below the frost line. Bearing surfaces within the proposed footing areas are to be at least 3.5 feet below the existing grade.
- 6.) Provided bearing surfaces are prepared as described herein, an allowable soil bearing capacity of 6,000 pounds per square foot may be used for design purposes in sizing the footings and foundations. If structural fill is used to raise the bearing grade, 6,000 pounds per square foot can be used in the design.
- 7.) If the tower footings are constructed on rock, the bearing capacity can be up to 20 tons per square foot, based on the RQD hardness. Preparation of the bearing surfaces should be approved by the geotechnical engineer.
- 8.) All work to prepare in-place materials and to construct foundation systems should be performed under the observation of the geotechnical engineer. Specific important details of our geotechnical engineering study and recommendations are enclosed herein.

### 2.00 INTRODUCTION

This report presents the results of an engineering study performed by Atlantic Consulting & Engineering (ACE), at the site of the proposed tower on 110 Yantic Lane in Norwich, CT. Included in this report are a summary of subsurface conditions observed and the implications of these conditions with respect to the design and construction of the proposed structure. Please note that this report is subject to the limitations contained in Section 8.00.

### 2.10 OBJECTIVE OF STUDY

The objective of our scope of services was to explore subsurface conditions within the proposed compound area and develop geotechnical recommendations for the design of the foundation support for the proposed structure. Included are design criteria for proposed slab on grade and pavement sections.

### 2.20 GEOTECHNICAL SCOPE OF SERVICES

The scope of services performed by ACE to meet the above stated objectives for geotechnical services included the following:

- Inspection of the test boring and probes conducted by Soiltesting, Inc., on May 10, 2021.
- Evaluation of the soil samples and the rock core that were taken on site.
- Recommendations were prepared for foundation support for the proposed structure.
- Recommendations for slab and pavement section design have been prepared.
- General recommendations have been made as to earthwork and foundation construction procedures to be followed during the construction phase of this project.

### 2.30 SITE AND PROJECT DESCRIPTION

Verizon is constructing a 110 foot tall monopole to the south of the water tower. The subject site is located on the eastern side of Yantic Lane. Residences are located to the west and to the south of the site along Cottonwood Lane and Philanne Drive. Route 2 borders the northern portion of the site and the Norwich Public Utilities water company as well as the water tower is located to the east. The road/driveway enters from the east. Borings and probes were drilled to the southwest corner of the site where the new tower is proposed (see plan)

### 3.00 SUBSURFACE EXPLORATIONS

Subsurface explorations performed for this project consisted of hollow stem augured borings. Borings were terminated in rock deposits.

Test borings were located and drilled by Soiltesting, Inc. Approximate locations of borings are shown on the Boring Location Plan. One (1) test boring and four (4) probes were advanced throughout the site. Copies of the test boring logs are included in Appendix A, along with a boring location plan. Test boring locations should be considered accurate only to the degree implied by measuring method used to determine them. The test borings were conducted using a truck mounted drill rig. Soil samples from the test borings and rock were classified both on site and in the lab.

### 4.00 SUBSURFACE CONDITIONS

All explorations revealed GLACIAL TILL and ROCK beneath the surface. Loose to Medium dense sand and gravel with mixed silt along with deeper rock was predominant throughout the exploratory effort. The material is compact and stable to work on and is desirable as bearing material and should be prepared as outlined below. Since the material is a GLACIAL TILL DEPOSIT, if prepared properly, the soil can be assigned 3 tons per square foot bearing capacity. Groundwater will probably not affect the excavation work and stability of in situ soils if the excavation proceeds with caution.

### 5.00 IMPLICATIONS OF SUBSURFACE CONDITIONS

### 5.10 GLACIAL TILL DEPOSITS (3a)

Throughout the site beginning immediately beneath the surface, a naturally deposited GLACIAL TILL was encountered. The material is a medium compact brown sand and gravel mix. This material ranges in depth from the surface to a depth of 5 feet at the center point of the tower to up to 9 feet below grade 10 feet offset from the Center Point. The characteristics of this material make it suitable for footing support, and this can be the design bearing material for the project. Some of this material may meet the structural fill requirements outlined in section 7.30 and therefore could be reused as structural fill for raises in grade beneath footings and slabs, furthermore it appears to be suitable to raise the grade in paved areas and below slabs provided the final 8 inches area prepared in accordance with Paragraph 7.30 below.

### 5.20 **ROCK**

Rock and/or boulders were encountered below the glacial till the refusal was encountered as shallow as 5 feet at the center location and as deep as 9.5 feet. The RQD was low based on the 5-foot core that was taken. The proposed foundation can also be set on the rock and a bearing capacity of 20 tons per square foot can be used for design.

### 5.30 GROUNDWATER

Groundwater was NOT encountered. Therefore, it should not affect the excavation and construction activities.

### 6.00 DESIGN OBSERVATIONS

It is our recommendation that excavation extend to a depth and be pinned into the rock. Footings shall be pinned into the rock; If the foundation is on rock, the minimum excavation is 12 inches below grade. If the pad is designed to bear on rock and soil, then precautions should be taken for the rock-to-soil interface. If unsuitable materials are encountered at that elevation, then they must be removed followed by replacement with suitable compacted structural fill beneath the bottom of strip and pier footings (if necessary) or construction of the footings directly on the GLACIAL TILL Stratum.

If the in-place material is determined by the Geotechnical Engineer to be acceptable after visual observations, then areas beneath the slabs can be prepared as described in Section 7.10. Where bearing surfaces require a raise in grade, structural fill can be placed above the existing alluvial deposits as described in Section 7.30.

### 6.10 SPREAD FOOTINGS, PAD or PIERS

Construction of the tower will most likely require establishing a deep rock foundation with anchors to prevent over turning. Blasting or hydraulic hoe ramming may be required to attain the depths needed for proper support. The rock appears to be too dense to excavate using a backhoe. Construction on rock surfaces is shown in Figure 1.

For any other buildings that may be planned, Excavation to naturally deposited inorganic materials is an effective approach for this project due to the relatively shallow depth of the unsuitable materials in the major portion of the construction area. Spread footings, PIERS or PAD can bear directly on TILL deposits, ROCK or structural fill can be used to raise the grade

to a minimum of 42 inches below finish grade if raising the grade is required. There could possibly be an excavation below grade to remove the unsuitable soils. When structural fill is used to raise the grade to the bottom of footing, the compacted area shall extend 12 inches beyond the edge of the footing for every 12 inches of structural fill placed, for example if 2 feet of fill were used to raise the grade for a 4x4 footing, the actual area of structural fill should be 8x8 (2 feet along each side).

### 6.20 SLAB ON GRADE

For ay ancillary buildings, it is recommended that a 4 to 6 inch slab on grade be used to support minor floor loads if required. The slab should over-lie 8 inches of free draining sand and gravel. Which can also be accomplished by the following: excavate 8 inches below bottom of slab having the Geotechnical Engineer observe proof rolling prior to placement of and compaction testing of the structural fill or free draining sand.

### 6.30 PAVED AREAS

The subgrade soil for pavement will consist of varying depths of the existing glacial till and rock. Our proposed pavement cross section consists of the following:

### Roadways and Auto Parking Areas

4 - inch
4 - inch
8 - inch
Two 2" Bituminous Concrete Courses (Class 1 and 2)
Processed Aggregate Base
Structural fill placed on compacted subgrade proof rolled prior to lift

placement with a 12 ton vibratory roller with vibrator if proof rolling the bearing stratum.

The above cross section is considered acceptable provided the existing materials are proofrolled and approved by the engineer. All subsequent replacement fills required beneath the sub-base should consist of compacted structural fill. Areas where weaving is observed should be locally excavated and the grade raised using structural fill. Given the fact that some paved areas may be within the loose fill, the depth of excavation depth may need to be increased to attain stable supporting soils. Proof-rolling in the presence of the engineer will enable determination of the stability of that soil.

### 6.40 SEISMIC CHARACTERISTICS & LIQUEFACTION POTENTIAL

For structural design, the IBC Seismic Site Soil Classification is considered to be "B". The mapped spectral response acceleration for 1 second period is S1=0.054 and for short periods Ss=0.196. For transfer of ground shear into the naturally deposited inorganic sands, a factor of 0.35 can be assumed. See Seismic Summary in Appendix B. If the pad is designed on rock, then the seismic coefficients change.

Based on the results of the borings and the Standard Penetration Testing and soil sampling, the subsurface conditions at the site should be considered as having NEGLIGIBLE potential for liquefaction due to the density and gradation of the silt and sand coupled with the shallow depth of the rock.

### 6.50 SOIL LATERAL LOADS

Any walls will need to be designed for **passive**, **active** and **at-rest pressures**. To obtain K values, the  $\emptyset$  of the soil is needed. For the loose sands and fill  $\emptyset$ =26° can be used; for structural fill,  $\emptyset$ =37° can be used; for existing naturally deposited inorganic alluvial deposits.  $\emptyset$ =33° can be used. Submerged or saturated soil pressure used in design shall include the weight of buoyant soil plus hydrostatic loading which reduces capacity of the soils.

### 7.00 CONSTRUCTION AND EARTHWORK CONSIDERATIONS

Development of the proposed site may require substantial rock removal. Grading problems may also occur if the work is carried out in wet weather due to the silt content of some of the onsite materials. The recommendations presented in this report are predicated upon site preparations, foundation wall construction, floor slabs and pavement construction monitored under controlled conditions and the direction of the geotechnical consultant.

It is recommended that placement of the concrete for piers and footings take place shortly following the preparation of the design bearing surface, since the introduction of water may adversely affect its structural characteristics. Dewatering should take place throughout the operation if excavation near the water table takes place.

### 7.10 FLOOR SLABS

Prior to placement of new structural fill, or free-draining sand, gravel base course materials, all deleterious materials, including topsoil and fill should be removed from within the limits of the building to the minimum depth below finish floor as determined by the structural engineer. The exposed subgrade materials should then be proof rolled with a minimum of 4 passes of a 10-ton roller in the presence of the undersigned. Any observed soft or weaving areas should be locally excavated and replaced with compacted structural fill. The final 8 inches of free draining sand and gravel shall be placed as defined in section 7.30. A 4-to-6-inch slab on grade is recommended for the use described herein, depending on the proposed loading.

### 7.20 PAVEMENTS

Prior to placement of new pavement section materials, the in-place materials should be removed to a <u>minimum depth of 8 inches</u> below the bottom of finish pavement grades unless the alluvial stratum is encountered at which point it may remain in place. Existing bearing surfaces should be proof rolled and subgrade should then be prepared as outlined under Section 7.10 and 7.30. Raises in grade below pavement section materials should be performed using structural fill, acceptable on-site material and processed base as described in section 6.30

### 7.30 MATERIALS, PLACEMENT AND COMPACTION

Structural fill to be used in backfilling within the building areas below footings and pavements, below the recommended 8-inch sand-gravel floor slab base course, and beneath the recommended pavement section, should be free from ice, snow, roots, stumps, and other deleterious materials. Structural fill should consist of a sandy GRAVEL or gravely SAND material having a liquid limit and plasticity limit not exceeding 40 and 15, respectively, and conform to the following gradation requirements:

Sieve Size	Percent Finer by Weight
3.5 inch	100
No. 4	30 - 65
No. 10	20 - 50
No. 40	5 - 30
No. 100	0 - 10

**Free draining sand and gravel** for the pavement base course, whether existing or to be placed, should be free of ice, snow, roots, stumps, rubbish, and other deleterious materials and should consist of hard durable sand and gravel conforming to the following gradation requirements:

Sieve Size	Percent Finer by Weight
2 inch	100
1/2 inch	50 - 85
No. 4	40 - 75
No. 50	8 - 28
No. 100	0 - 10

All building areas, structural fill base course free draining sand-gravel fill, pavement base course and pavement sub-base material, should be placed in lifts not exceeding 8 inches in loose lift thickness and should be compacted to at least 95 percent of maximum dry density per ASTM D-1557. New structural fill required exterior to structural element (footings, foundation or retaining walls and pavements) zone of bearing should be compacted to at least 93 percent of the maximum dry density per ASTM D-1557.

If it is necessary to re-use existing acceptable on-site materials, compaction can be carried out by placing the material in lifts not exceeding 6 inches and should be compacted to a minimum of 95 percent of maximum dry density per ASTM D-1557. This cannot be conducted in wet weather, nor if the moisture content of the material is at a level where the desired compaction cannot be physically achieved. Modified Proctor testing, ASTM D-1557, will have to be conducted on samples of any fill desired to be reused. All reused material shall be free of roots, stumps, ice, snow, organic and any other deleterious materials.

### 7.40 CONSTRUCTION MONITORING SERVICES

It is recommended that Atlantic Consulting & Engineering and Fairfield Testing Laboratory be retained to provide geotechnical engineering and construction monitoring services during the excavation, foundation, and construction phases of the project. The purpose of these services is to observe compliance with the design concepts, contract documents, and geotechnical recommendations and to allow orderly design changes during construction in the event that subsurface conditions differ from those anticipated prior to the start of construction.

# Geotechnical Engineering Report for 110 Yantic Lane, Norwich, CT May 14, 2021

During construction, the Atlantic Consulting & Engineering and Fairfield Testing Laboratories field representatives are recommended to be engaged to provide controlled inspections including with the following:

- 1. Observe the general progress of site work.
- 2. Perform the required field control tests for earthwork, including proof-rolling sub-grades and placement of structural fill.
- Observe earthwork operations to ensure that the minimum compactive effort and maximum lift height restrictions are enforced. Certify rock anchoring and provide pull out testing, if required.
- 4. Observe, evaluate, and judge the suitability of prepared bearing surfaces as well as any possibility of using existing fill materials below slabs.
- 5. Observe and evaluate unanticipated subsurface conditions, when and where encountered and alternate procedures, which are proposed to address those unanticipated subsurface conditions.
- 7. Provide site monitoring for temporary storm water runoff, if necessary.

### 8.00 FINAL COMMENTS

This report has been prepared for specific application to the subject project in accordance with generally accepted soil and foundation engineering practices. No other warranty, expressed or implied, is made. In the event that any changes in the nature, design or location of structures are planned, the conclusions and recommendations contained in the report should not be considered valid, unless the changes are reviewed and conclusions of this report modified or verified in writing.

The analyses and recommendations submitted in this report are based in part upon the data obtained from the referenced test borings. The nature and extent of variations between explorations may not become evident until construction. In order to take full responsibility for information generated in this report, this geotechnical engineer shall be present to certify all bearing surfaces, acceptable bearing elevations and test the compaction of structural fill. If variations then appear evident, it will be necessary to re-evaluate the recommendation of this report.

Atlantic Consulting & Engineering should perform a general review of final design and specifications in order to determine that earthwork and foundation recommendations have been properly interpreted and implemented in the design specifications.

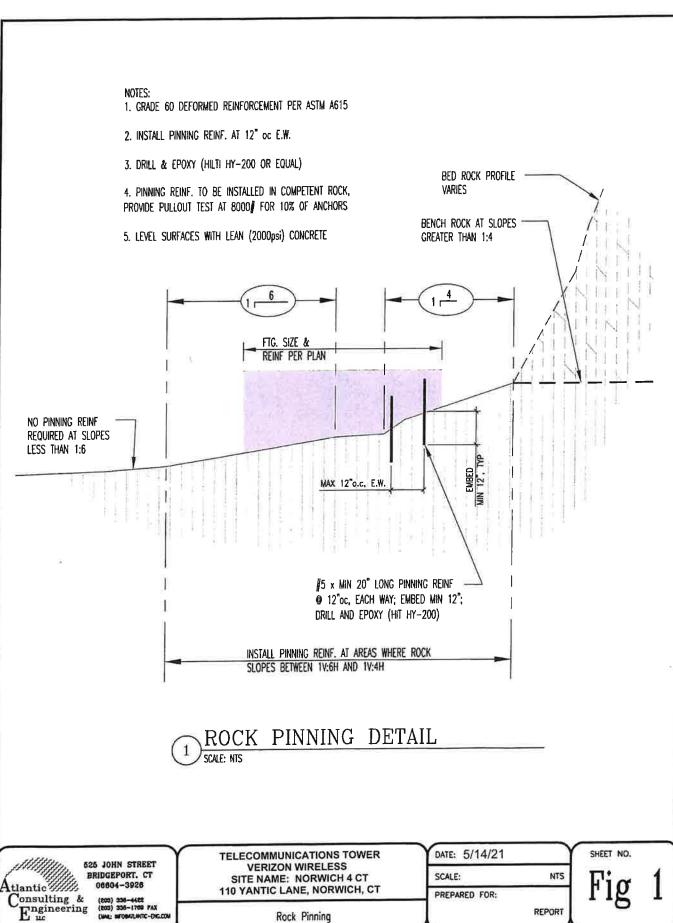
Submitted by

James E. Quill, CT PE# 14358

James E. Quill, PE

## Figure 1

**Rock Pinning Plan** 



Rock Pinning

REPORT

BITE AND IS NOT TO BE USED FOR ANY OTHER PURPOSE, LOCATION OR OWNER WITHOUT WISITEN CONSENT OF THE ENCAREST

## Figure 2

**Boring Location Plan** 

**WATER TANK** P-2 10' B-1 10' 10' P-1 P-3 ACCESS ROAD BORING LOCATION PLAN CELL TOWER 110 YANTIC LANE NORWICH, CT

## **APPENDIX A**

Boring Logs B-1
Probes P-1 through P-4

Conducted on May 10, 2021

SOILTESTING, INC.						CLIENT: Atlantic Consulting and Engineering						SHEET_1_OF_1 HOLE NO. B-1				
OXFORD, CT 06478							PROJE	ECT NO	O	G-1797						
CT (203) 888-4531							PROJECT NAME			Prop	osed Cell	Tower		BORING LOCATIONS		
NY (914) 946-4850											onwood 8	Philann	е	per sketch		
FO	FOREMAN - DRILLER							LOGITHOIT			/ich					
	MK/ao													OCCUPATION OF THE PROPERTY OF		
INS	PECTOR										CASING	SAMPLER SS	CORE BAR	OFFSET DATE START 5/10/21		
							1	TYPE			HSA 4 1/4"	1 3/8"	2"	DATE FINISH 5/10/21		
	OUND W						SIZE I.D. HAMMER WT.			-	4 /4	140#	BIT	SURFACE ELEV		
	None_F1 _FT_AF				JURS				MER VV MER FA			30"	DIA	GROUND WATER ELEV.		
AI_	F1_AF	· IEK_						1 17-VIVIIV	ALIVIA							
				SAM	PLE						DEMOILT	SIRAIA	EIELD ID	ENTIFICATION OF SOIL REMARKS		
_	CASING							NS PE		CORE	OR	CHANGE	INCL C	COLOR, LOSS OF WASH WATER,		
DEPTH	BLOWS	NO	Туре	PEN	REC			SAMP		TIME PER FT	CONSIST	DEPTH	111025	SEAMS IN ROCK, ETC.		
	PER FOOT					DEPTH @ BOT	0 - 6	6 - 12	12- 18	(MIN)	MOIST	ELEV				
$\vdash$	F001	1	SS	24"	10"		1	11			moist		6" Topsoil			
							2	2			v loose		Brn F Sand	am Silt		
			-			-	-				-					
5					-						1	5'0"	Cobbles an	d Boulders		
		2	ss	1"	1"	5'1"	50/1"					5'6"	E.O.B 5'6"	FUSAL 5'6"		
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30											1					
	NOTE: Subsoil conditions revealed by this investigation represent conditions at specific locations and may not represent conditions															
GP	at other locations or times.  GROUND SURFACE TOFT. USEDCASING THENCASING TOFT. HOLE NO. B-1								FT. HOLE NO. B-1							
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WC	R = WEI	SHT C	F RC	DS		WOH =	WEIGH	T OF H	IAMME	R & RO	DS			C = COARSE M = MEDIUM		
SS	= SPLIT	TUBE	SAME	PLER	CE - 1	H.S.A: =	HOLL	OW ST = 10 -	20%	IGEK SOME =	20 - 35%	AND =35 - 5	50%	F = FINE		
FR	PROPORTIONS USED: TRACE = 0 - 10% LITTLE = 10 - 20% SOME = 20 - 35% AND =35 - 50% F = FINE															

SOILTESTING, INC.						CLIENT: Atlantic Consulting and Engineering					SHEET 1 OF 1 HOLE NO. P-1-4					
140 OXFORD RD. OXFORD, CT 06478							PROJECT NO. G-1797				1 1,14					
										Proposed Cell Tower				BORING LOCATIONS	_	
		•	3) 88				PROJECT NAME			-	nwood &		e	per Plan		
NY (914) 946-4850 FOREMAN - DRILLER							LOCATION			Norw		· · · · · · · · · · · · · · · · · · ·		Por Const		
MK/ao							LOCATION			CT					_	
INSPECTOR											CASING	SAMPLER	CORE BAR	OFFSET		
							TYPE				HSA SS			DATE START 5/10/21	_	
GE	OUND W	ATER	OBSE	RVA	TION	S	SIZE I.D.				4 1/4" 1 3/8"			DATE FINISH 5/10/21		
	FT_AF						HAMMER WT			Γ.		140#	BIT	SURFACE ELEV.		
	 FTAF							HAMN	IER FA	LL		30"		GROUND WATER ELEV.		
F				SAM											-	
	- 1		1	SAIVI T	PLC	1					ז וופאווע	SIRAIA	FIELD ID	ENTIFICATION OF SOIL REMARKS	S	
1 =	CASING						BLOWS PER 6 IN ON SAMPLER (FORCE ON TUBE)			CORE	OR	CHANGE		INCL. COLOR, LOSS OF WASH WATER,		
DEPTH	BLOWS PER	NO	Туре	PEN	REC	DEPTH				TIME PER FT	CONSIST	DEPTH	SEAMS IN ROCK, ETC.			
^	FOOT					@ BOT		6 - 12		(MIN)	MOIST	ELEV				
-													P-1			
														*		
			_						-	-						
5												5'0"		FUSAL 5'0"		
													E.O.B 5'0"			
					-				-				P-2			
		-								-			-2			
5												5'0"		FUSAL 5'0"		
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1																
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									-							
1												100000				
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1													P-4			
_ ا		_		_	-				-			5'6"	AUGER RE	FUSAL 5'6"		
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	NOTE: Subsoil conditions revealed by this investigation represent conditions at specific locations and may not represent conditions															
						at othe	er loca	ations	or tir	nes.						
	OUND SU				-	5 (0.05) U.S.	SED_	T - T'	INWAL	_CASIN	G THEN V = VANE		ASING TO _	FT. HOLE NO. P-1-4		
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TWOK - WEIGHT OF NODS								M = MEDIUM								
l <sub>PR</sub>	PROPORTIONS USED: TRACE = 0 - 10% LITTLE = 10 - 20% SOME = 20 - 35% AND = 35 - 50% F = FINE															

## <u>APPENDIX B</u>

Seismic Summary

(B) (B) (B)





### 110 Yantic Ln, Norwich, CT 06360, USA

Latitude, Longitude: 41.5543284, -72.13074540000001





Map data ©2021

Date	5/19/2021, 2:07:46 PM
Design Code Reference Document	ASCE7-16
Risk Category	II
Site Class	B - Rock

Туре	Value	Description
SS	0.196	MCE <sub>R</sub> ground motion. (for 0.2 second period)
S <sub>1</sub>	0.054	MCE <sub>R</sub> ground motion. (for 1.0s period)
S <sub>MS</sub>	0.176	Site-modified spectral acceleration value
S <sub>M1</sub>	0.043	Site-modified spectral acceleration value
S <sub>DS</sub>	0.117	Numeric seismic design value at 0.2 second SA
S <sub>D1</sub>	0.029	Numeric seismic design value at 1.0 second SA

-DI		
Туре	Value	Description
SDC	Α	Seismic design category
Fa	0.9	Site amplification factor at 0.2 second
$F_{v}$	0.8	Site amplification factor at 1.0 second
PGA	0.108	MCE <sub>G</sub> peak ground acceleration
F <sub>PGA</sub>	0.9	Site amplification factor at PGA
PGA <sub>M</sub>	0.097	Site modified peak ground acceleration
$T_L$	6	Long-period transition period in seconds
SsRT	0.196	Probabilistic risk-targeted ground motion. (0.2 second)
SsUH	0.206	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration
SsD	1.5	Factored deterministic acceleration value. (0.2 second)
S1RT	0.054	Probabilistic risk-targeted ground motion. (1.0 second)
S1UH	0.059	Factored uniform-hazard (2% probability of exceedance in 50 years) spectral acceleration.
S1D	0.6	Factored deterministic acceleration value. (1.0 second)
PGAd	0.5	Factored deterministic acceleration value. (Peak Ground Acceleration)
C <sub>RS</sub>	0.948	Mapped value of the risk coefficient at short periods
C <sub>R1</sub>	0.925	Mapped value of the risk coefficient at a period of 1 s

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