STATE OF CONNECTICUT CONNECTICUT SITING COUNCIL

IN RE:

APPLICATION OF HOMELAND TOWERS, LLC AND NEW CINGULAR WIRELESS PCS, LLC d/b/a AT&T FOR A CERTIFICATE OF ENVIRONMENTAL COMPATIBILITY AND PUBLIC NEED FOR THE June 14, 2021 CONSTRUCTION, MAINTENANCE, AND Α OPERATION OF **TELECOMMUNICATIONS** FACILITY AT ONE OF TWO SITES IN THE TOWN OF KENT. CONNECTICUT

DOCKET NO. 488

HOMELAND TOWERS, LLC AND NEW CINGULAR WIRELESS PCS, LLC d/b/a AT&T **DEVELOPMENT & MANAGEMENT PLAN**

Homeland Towers, LLC, the Certificate Holder in the above-referenced Docket, respectfully submits the following Development & Management Plan ("D&M Plan") documents and materials for Site B 93 Richards Road, the certificated site:

Homeland Towers, LLC cover letter dated June 9, 2021;

AT&T Commitment Letter dated June 9, 2021;

Geotechnical Investigation Report by Delta Oaks Group dated December 31, 2020;

Structural Drawings by Valmont Structures dated May 19, 2021 with Structural Calculations by Bennet & Pless;

Polar Power, Inc Emergency Generator Specifications;

KMW Antenna Specifications and Ericsson Remote Radio Head (RRH) Specifications;

Paint color samples; and

Two full-sized sets and 15 half-sized sets of D&M Plan Drawings prepared by All-Points Technology Corporation dated June 9, 2021 and signed and sealed by Robert Charles Burns, CT P.E. license no. 20071.

CERTIFICATE OF SERVICE

I hereby certify that on this day the foregoing was sent electronically to the Connecticut Siting Council and to the service list below with one original and fifteen (15) hard copies sent to the Connecticut Siting Council via overnight mail:

Keith R. Ainsworth, Esq. Law Offices of Keith R. Ainsworth, Esq. 51 Elm Street, Suite 201 New Haven, CT 06510-2049

Anthony F. DiPentima, Esq. Michael D. Rybak, Jr., Esq. Guion, Stevens & Rybak, LLP 93 West Street P.O. Box 338 Litchfield, CT 06759

Daniel E. Casagrande, Esq. Cramer & Anderson, LLP 30 Main Street, Suite 204 Danbury, CT 06810 (203) 744-1234 dcasagrande@crameranderson.com

Daniel S. Rosemark, Esq. Rosemark Law, LLC 100 Mill Plain Rd., Third Floor Danbury, CT 06811 (203) 297-8574 daniel@rosemark.law

June 14, 2021

ucie Chrocchio

Lucia Chiocchio Cuddy & Feder LLP 445 Hamilton Ave,14th Floor White Plains, NY 10601 (914)-761-1300 Attorneys for the Applicants

cc: Homeland Towers; AT&T; APT; C Squared; Christopher B. Fisher, Esq.



June 9, 2021

<u>Via Federal Express</u> Honorable John Morissette, Presiding Officer And Members of the Connecticut Siting Council Ten Franklin Square New Britain, CT 06051

Re: Docket No. 488 – Homeland Towers LLC (HT) and New Cingular Wireless PCS, LLC d/b/a AT&T Development & Management Plan- Tower Facility at 93 Richards Road, Kent CT (CT757).

Dear Presiding Officer Morissette and Members of the Siting Council,

Homeland Towers ("HT") respectfully requests that you please accept for review and Council approval this Development & Management Plan ("D&M Plan") filing for the Facility as approved in Docket No. 488.

Tower, Compound & Other Equipment

Enclosed are fifteen (15) sets of 11"x17" Development & Management Plans dated 6/9/2021 prepared by All Points Technology Corporation. Two full-sized sets of the Development & Management Plans are also enclosed. These plans are being filed in accordance with the Council's Decision and Order dated December 3, 2020 ("Decision and Order"). The D&M Plan incorporates a 135' tall monopole as provided for in the Siting Council's Decision and Order in this Docket. AT&T will initially install six (6) panel antennas, nine (9) RRH's and two (2) squid boxes at a centerline of 131' above grade level ("AGL"). The monopole will be painted a two-tone color scheme, brown-gray (PL Shadow Beige) #2257) on bottom and gray-blue (PL White Smoke #1201) on the top. Antennas and mounting equipment will be painted the same color as the upper portion of the tower. All plantings will be warranted for three years. As shown on Sheet A-1 of the enclosed D&M Plans, the monopole is designed with a yield point at 51' AGL to ensure that the tower setback radius remains within the property boundaries. Attached please also find a geotechnical study dated December 31, 2020 prepared by Delta Oaks Group as well as a structural design report for the tower and foundation dated April 28, 2021 prepared by Ambor Structures. Specifications for AT&T's antennas and generator are also provided along with color swatches for the two-tone tower.

The proposed D&M Plan also includes construction plans for the site clearing, drainage, and erosion and sedimentation control measures consistent with the 2002 Connecticut Guidelines for Soil Erosion and Sediment Control as amended.

Per 2(a) of the Decision and Order, attached is a letter dated June 9, 2021 from AT&T stating their firm commitment to install their associated wireless equipment at the facility upon completion of construction.

Required Notifications

In accordance with the provisions of RCSA Section 16-50j-77, Homeland Towers hereby notifies the Council of its intention to begin site work immediately after Council approval of the D&M Plan. Construction of the tower and other site improvements will commence upon issuance of a local building permit. The supervisor for all construction related matters on this project is Ray Vergati with Homeland Towers, LLC located at 9 Harmony Street, 2nd Floor, Danbury, CT 06810 and can be reached by telephone at 203-297-6345.



We respectfully request that this matter be included on the Council's next available agenda for review and approval. Thank you for your consideration of the enclosed.

Sincerely,

Raymond Vergati rv@homelandtowers.us

Enclosures

cc: Honorable Jean Speck, First Selectman, Town of Kent Manny Vicente, Homeland Towers LLC Brian Leyden, AT&T Scott Chasse, P.E., APT Lucia Chiocchio, Esq., Cuddy & Feder LLP



June 9, 2021

Re: Connecticut Siting Council Docket No. 488 Homeland Towers, LLC and New Cingular Wireless PCS, LLC d/b/a AT&T Certificate of Environmental Compatibility and Public Need for the construction, maintenance, and operation of a telecommunications facility located at 93 Richards Road, Kent, Connecticut AT&T's Use of the Approved Facility

Dear Ms. Bachman:

In accordance with condition 2a of the Siting Council's Decision and Order ("D&O") in Docket No. 488, this letter serves as AT&T's commitment to install and operate its wireless facility on the approved monopole facility upon completion of construction by Homeland Towers, LLC. AT&T anticipates that its Kent facility will be operational within the eighteen-month timeframe included in the D&O.

Thank you for your consideration of this information.

Very truly yours,

Brian Leyden

Sr. Manager, Real Estate & Construction AT&T Mobility New England

cc: Homeland Towers LLC SAI Lucia Chiocchio, Esq

> AT&T Mobility 550 Cochituate Road Suites 13 & 14 Framingham, MA 01701



GEOTECHNICAL INVESTIGATION REPORT

December 31, 2020

Prepared For:

InSite Wireless Group, LLC



Kent CT757 Proposed 154-Foot Monopole Tower 93 Richards Road, Kent (Litchfield County), Connecticut 06785 Latitude N 41° 42' 31.0" Longitude W 73° 25' 13.7"

> Delta Oaks Group Project GEO20-07686-08 Revision 0 <u>geotech@deltaoaksgroup.com</u>

Performed By:

Justin Brosseau, E.I.

Reviewed By:







INTRODUCTION

This geotechnical investigation report has been completed for the proposed 154-foot monopole tower located at 93 Richards Road in Kent (Litchfield County), Connecticut. The purpose of this investigation was to provide engineering recommendations and subsurface condition data at the proposed tower location. A geotechnical engineering interpretation of the collected information was completed and utilized to suggest design parameters regarding the adequacy of the structure's proposed foundation capacity under various loading conditions. This report provides the scope of the geotechnical investigation; geologic material identification; results of the geotechnical laboratory testing; and design parameter recommendations for use in the design of the telecommunication facility's foundation and site development.

SITE CONDITION SUMMARY

The proposed tower and compound are located in a clearing on a heavily wooded hill exhibiting a gradually sloping topography from the east to west across the tower compound and subject property.

<u>REFERENCES</u>

- Survey Drawings, prepared by All-Points Technology Corporation, dated February 5, 2020
- TIA Standard (TIA-222-G), dated August 2005

SUBSURFACE FIELD INVESTIGATION SUMMARY

The subsurface field investigation was conducted through the advancement of three mechanical soil test borings to the auger refusal depth of 3.0, 3.0, and 4.5 feet bgs in borings B-1 through B-3, respectively. Samples were obtained at selected intervals in accordance with ASTM D 1586. The sampling was conducted at the staked centerline of the proposed tower. Upon encountering auger refusal 5.0 feet of rock coring was conducted in accordance with ASTM D 2113. Soil and rock samples were transported to our laboratory and classified by a geotechnical engineer in accordance with ASTM D 2487. A detailed breakdown of the material encountered in our subsurface field investigation can be found in the boring logs presented in the Appendix of this report.

Additional testing was performed on selected samples in accordance with ASTM D 7012 (Unconfined Compressive Strength – Rock). Laboratory data can be found in the Appendix of this report.

A boring plan portraying the spatial location of the boring in relation to the proposed tower, tower compound and immediate surrounding area can be found in the Appendix.



SUBSURFACE CONDITION SUMMARY

The following provides a general overview of the site's subsurface conditions based on the data obtained during our field investigation.

FILL

Topsoil was encountered during the subsurface field investigation from the existing ground surface at a depth of 0.7 feet bgs in boring B-1 and 0.3 feet bgs in borings B-2 and B-3.

SOIL

The residual soil encountered in the subsurface field investigation began at a depth of 0.7 feet bgs in boring B-1 and 0.3 feet bgs in borings B-2 and B-3 and consisted of silty sand. The materials ranged from a very loose to very dense relative density.

Auger advancement refusal was encountered during the subsurface field investigation at a depth of 3.0, 3.0, and 4.5 feet bgs in borings B-1 through B-3, respectively.

ROCK

Rock was encountered during the subsurface investigation at a depth of 3.0 feet bgs in boring B-2. The rock can be described as highly to moderately fractured, moderately weathered, hard gneiss.

SUBSURFACE WATER

At the time of drilling, subsurface water was not encountered during the subsurface investigation. However, subsurface water elevations can fluctuate throughout the year due to variations in climate, hydraulic parameters, nearby construction activity and other factors.

FROST PENETRATION

The frost penetration depth for Litchfield County, Connecticut is 40 inches (3.3 feet).

CORROSIVITY

Soil resistivity was performed in accordance with ASTM G187 with a test result of 171,000 ohmscm.



FOUNDATION DESIGN SUMMARY

In consideration of the provided tower parameters and the determined soil characteristics, Delta Oaks Group recommends utilizing a shallow foundation and/or drilled shaft foundation for the proposed structure. The strength parameters presented in the following sections can be utilized for design of the foundation.

GENERAL SUBSURFACE STRENGTH PARAMETERS

Boring	Depth (bgs)	USCS	Moist/Buoyant Unit Weight (pcf)	Phi Angle (degrees)	Cohesion (psf)
D 1	0.0 - 0.7	TOPSOIL	105	0	0
B-1	0.7 – 3.0	SM	130	40	0

Boring	Depth (bgs)	USCS	Moist/Buoyant Unit Weight (pcf)	Phi Angle (degrees)	Cohesion (psf)
	0.0 - 0.3	TOPSOIL	105	0	0
B-2	0.3 – 3.0	SM	130	40	0
	3.0 - 8.0	GNEISS	140	0	12,000

Boring	Depth (bgs)	USCS	Moist/Buoyant Unit Weight (pcf)	Phi Angle (degrees)	Cohesion (psf)
	0.0 - 0.3	TOPSOIL	105	0	0
В-З	0.3 – 2.0	SM	105	29	0
	2.0 - 4.5	SM	130	40	0

- The unit weight provided assumes overburden soil was compacted to a minimum of 95% of the maximum dry density as obtained by the standard Proctor method (ASTM D 698) and maintained a moisture content within 3 percent of optimum
- The values provided for phi angle and cohesion should be considered ultimate.



SUBSURFACE STRENGTH PARAMETERS – SHALLOW FOUNDATION

Boring	Dimensions (feet)	Depth (feet bgs)	Net Ultimate Bearing Capacity (psf)
В-2	Greater than 5.0 x 5.0	Greater than 3.3	30,000

- Delta Oaks Group recommends the foundation bear a minimum of 3.3 feet bgs or entirely on bedrock.
- A sliding friction factor of 0.35 can be utilized along the base of the proposed foundation.
- The bearing capacity can be increased by 1/3 for transient loading.
- An Ultimate Passive Pressure Table with a reduction due to frost penetration to a depth of 3.3 feet bgs is presented on the following page.
- Delta Oaks Group recommends an appropriate factor of safety be utilized for the design of the foundation.



Soil Lay	yers (feet)	ATE PASSIVE Moist Unit Weight	Phi Angle	Cohesion	PV	KP	Ph
Тор	0.0	105	0	0	0.00	1.00	0.00
Bottom	0.3	105	0	0	31.50	1.00	15.75
Тор	0.3	130	40	0	31.50	4.60	72.43
Bottom	3.0	130	40	0	382.50	4.60	879.54
Тор	3.0	140	0	12000	382.50	1.00	12191.25
Bottom	3.3	140	0	12000	424.50	1.00	12212.25
Тор	3.3	140	0	12000	424.50	1.00	24424.50
Bottom	10.0	140	0	12000	1362.50	1.00	25362.50



SUBSURFACE STRENGTH PARAMETERS - DRILLED SHAFT FOUNDATION

Boring	Depth (bgs)	Net Ultimate Bearing Capacity (psf)	Ultimate Skin Friction - Compression (psf)	Ultimate Skin Friction - Uplift (psf)
	0.0 – 3.3	_	_	-
R O	3.3 - 4.0	79,970	4,800	4,800
B-2	4.0 - 6.0	79,950	4,800	4,800
	6.0 - 8.0	79,930	4,800	4,800

- The top 3.3 feet of soil should be ignored due to the frost penetration and the potential soil disturbance during construction.
- The bearing capacity can be increased by 1/3 for transient loading.
- The values presented assume the concrete is cast-in-place against earth walls and any casing utilized during construction of the foundation was removed.
- Delta Oaks Group recommends an appropriate factor of safety be utilized for the design of the foundation.





SUBSURFACE STRENGTH PARAMETERS – SUPPORT STRUCTURE FOUNDATION

Boring	Depth (bgs)	Net Ultimate Bearing Capacity (psf)	Minimum Design Footing Width (ft)	Modulus of Subgrade Reaction (pci)
В-З	3.5	15,000	2.0	225

- Delta Oaks Group recommends utilizing a slab on grade in conjunction with continuous perimeter footings that bear on residual soil or properly compacted structural fill placed in accordance with the recommendations provided in the CONSTRUCTION section of this report.
- The slab on grade should be properly reinforced to prevent concrete cracking and shrinkage.
- The foundation should bear a minimum of 3.5 feet bgs or entirely on bedrock.
- A sliding friction factor of 0.35 can be utilized along the base of the proposed foundation.
- An Ultimate Passive Pressure Table is presented on the following page. An appropriate reduction should be considered in accordance with local building code frost penetration depth.
- Delta Oaks Group recommends an appropriate factor of safety be utilized for the design of the foundation.



	ULTIMATE PASSIVE PRESSURE VS. DEPTH - SUPPORT STRUCTURE FOUNDATION							
Soil La	yers (feet)	Moist Unit Weight	Phi Angle	Cohesion	PV	KP	Ph	
Тор	0.0	105	0	0	0.00	1.00	0.00	
Bottom	0.3	105	0	0	31.50	1.00	15.75	
Тор	0.3	105	29	0	31.50	2.88	45.39	
Bottom	2.0	105	29	0	210.00	2.88	302.62	
Тор	2.0	130	40	0	210.00	4.60	482.89	
Bottom	3.3	130	40	0	379.00	4.60	871.49	
Тор	3.3	130	40	0	379.00	4.60	1742.99	
Bottom	10.0	130	40	0	1250.00	4.60	5748.64	

ULTIMATE PASSIVE PRESSURE VS. DEPTH – SUPPORT STRUCTURE FOUNDATION



CONSTRUCTION

SITE DEVELOPMENT

The proposed access road and tower compound should be evaluated by a Geotechnical Engineer, or their representative, after the removal or "cutting" of the areas to design elevation but prior to the placement of any structural fill material to verify the presence of unsuitable or weak material. Unsuitable or weak materials should be undercut to a suitable base material as determined by a Geotechnical Engineer, or their representative. Backfill of any undercut area(s) should be conducted in accordance with the recommendations provided in the *STRUCTURAL FILL PLACEMENT* section of this report.

Excavations should be sloped or shored in accordance and compliance with OSHA 29 CFR Part 1926, Excavation Trench Safety Standards as well as any additional local, state and federal regulations.

STRUCTURAL FILL PLACEMENT

Structural fill materials should be verified, prior to utilization, to have a minimum unit weight of 110 pcf (pounds per cubic foot) when compacted to a minimum of 95% of its maximum dry density and within plus or minus 3 percentage points of optimum moisture. Materials utilized should not contain more than 5 percent by weight of organic matter, waste, debris or any otherwise deleterious materials. The Liquid Limit should be no greater than 40 with a Plasticity Index no greater than 20. Structural fill material should contain a maximum particle size of 4 inches with 20 percent or less of the material having a particle size between 2 and 4 inches. Backfill should be placed in thin horizontal lifts not to exceed 8 inches (loose) in large grading areas and 4 inches (loose) where small handheld or walk-behind compaction equipment will be utilized. The potential suitability of on-site materials to be utilized as fill should be evaluated by a Geotechnical Engineer, or their representative just prior to construction.

During construction structural fill placement should be monitored and tested. This should include at minimum, visual observation as well as a sufficient amount of in-place field density tests by a Geotechnical Engineer, or their representative. Materials should be compacted to a minimum of 95% of the maximum dry density as determined by ASTM D 698 (standard Proctor method). Moisture contents should be maintained to within plus or minus 3 percentage points of the optimum moisture content.

SHALLOW FOUNDATIONS

Foundation excavation(s) should be evaluated by a Geotechnical Engineer, or their representative, prior to reinforcing steel and concrete placement. This evaluation should include visual observation to verify a level bearing surface; vertical side-walls with no protrusions, sloughing or caving; and the exposed bearing surface is free of deleterious material, loose soil and standing water. Excavation dimensions should be verified and testing performed on the exposed bearing surface to verify compliance with design recommendations. Bearing testing should be conducted in accordance with ASTM STP399 (Dynamic Cone Penetrometer). A 6-inch layer of compacted crushed stone should be installed prior to reinforcing steel and concrete placement. If subsurface water is encountered during excavation dewatering methods such as sump pumps or well points may be required.



DRILLED SHAFT FOUNDATIONS

Drilled shaft foundations (caissons) are typically installed utilizing an earth auger to reach the design depth of the foundation. Specialized roller bits or core bits can be utilized to penetrate boulders or rock. The equipment utilized should have cutting teeth to result in an excavation with little or no soil smeared or caked on the excavation sides with spiral-like corrugated walls. The drilled shaft design diameter should be maintained throughout the excavation with a plumbness tolerance of 2 percent of the length and an eccentricity tolerance of 3 inches from plan location. A removable steel casing can be installed in the shaft to prevent caving of the excavation sides due to soil relaxation. Upon completion of the drilling and casing placement, loose soils and subsurface water greater than 3-inches in depth should be removed from the bottom of the excavation for the "dry" installation method. The drilled shaft installation should be evaluated by a Geotechnical Engineer, or their representative, to verify suitable end bearing conditions, design diameter and bottom cleanliness. The evaluation should be conducted immediately prior to as well as during concrete placement operations.

The drilled shaft should be concreted as soon as reasonably practical after excavation to reduce the deterioration of the supporting soils to prevent potential caving and water intrusion. A concrete mix design with a slump of 6 to 8 inches employed in conjunction with the design concrete compressive strength should be utilized for placement. Super plasticizer may be required to obtain the recommended slump range. During placement, the concrete may fall freely through the open area in the reinforcing steel cage provided it does not strike the reinforcing steel and/or the casing prior to reaching the bottom of the excavation. The removable steel casing should be extracted as concrete is placed. During steel casing removal a head of concrete should be maintained above the bottom of the casing to prevent soil and water intrusion into the concrete below the bottom of the casing.

If subsurface water is anticipated and/or weak soil layers are encountered drilled shafts are typically installed utilizing the "wet" method by excavating beneath a drilling mud slurry. The drilling mud slurry is added to the drilled shaft excavation after groundwater has been encountered and/or the sides of the excavation are observed to be caving or sloughing. Additional inspection by a Geotechnical Engineer, or their representative, during the "wet" method should consist of verifying maintenance of sufficient slurry head, monitoring the specific gravity, pH and sand content of the drilling slurry, and monitoring any changes in the depth of the excavation between initial approval and just prior to concreting.

Concrete placement utilizing the "wet" method is conducted through a tremie pipe at the bottom of the excavation with the drilling mud slury level maintained at a minimum of 5 feet or one shaft diameter, whichever is greater, above the ground water elevation. The bottom of the tremie should be set one tremie pipe diameter above the excavation. A closure flap at the bottom of the tremie or a sliding plug introduced into the tremie before the concrete is recommended to reduce the potential contamination of the concrete by the drilling mud slury. The bottom of the tremie must be maintained in the concrete during placement. Additional concrete should be placed through the tremie causing the slury to overflow from the excavation in order to reduce the potential for the development of "slury pockets" remaining in the drilled shaft.



QUALIFICATIONS

The design parameters and conclusions provided in this report have been determined in accordance with generally accepted geotechnical engineering practices and are considered applicable to a rational degree of engineering certainty based on the data available at the time of report preparation and our practice in this geographic region. All recommendations and supporting calculations were prepared based on the data available at the time of report preparation and knowledge of typical geotechnical parameters in the applicable geographic region.

The subsurface conditions used in the determination of the design recommendations contained in this report are based on interpretation of subsurface data obtained at specific boring locations. Irrespective of the thoroughness of the subsurface investigation, the potential exists that conditions between borings will differ from those at the specific boring locations, that conditions are not as anticipated during the original analysis, or that the construction process has altered the soil conditions. That potential is significantly increased in locations where existing fill materials are encountered. Additionally, the nature and extent of these variations may not be evident until the commencement of construction practices to confirm that the site conditions do not differ from those conditions anticipated in design. If such variations are encountered, Delta Oaks Group should be contacted immediately in order to provide revisions and/or additional site exploration as necessary

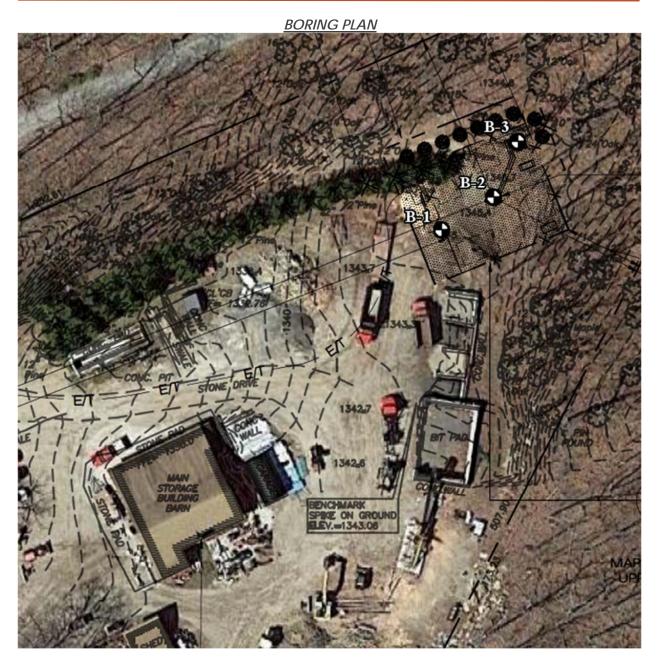
Samples obtained during our subsurface field investigation will be retained by Delta Oaks Group for a period of 30 days unless otherwise instructed by InSite Wireless Group, LLC. No warranty, expressed or implied, is presented.

Delta Oaks Group appreciates the opportunity to be of service for this Geotechnical Investigation Report. Please do not hesitate to contact Delta Oaks Group with any questions or should you require additional service on this project.



<u>APPENDIX</u>

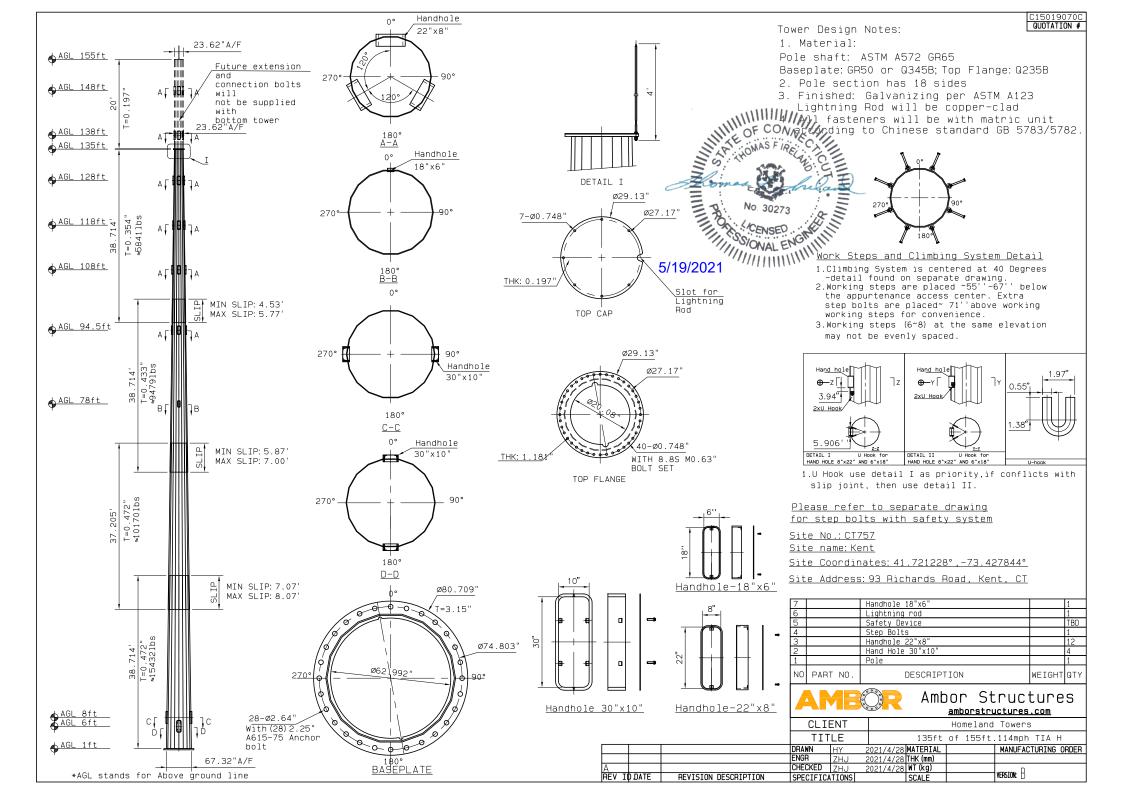


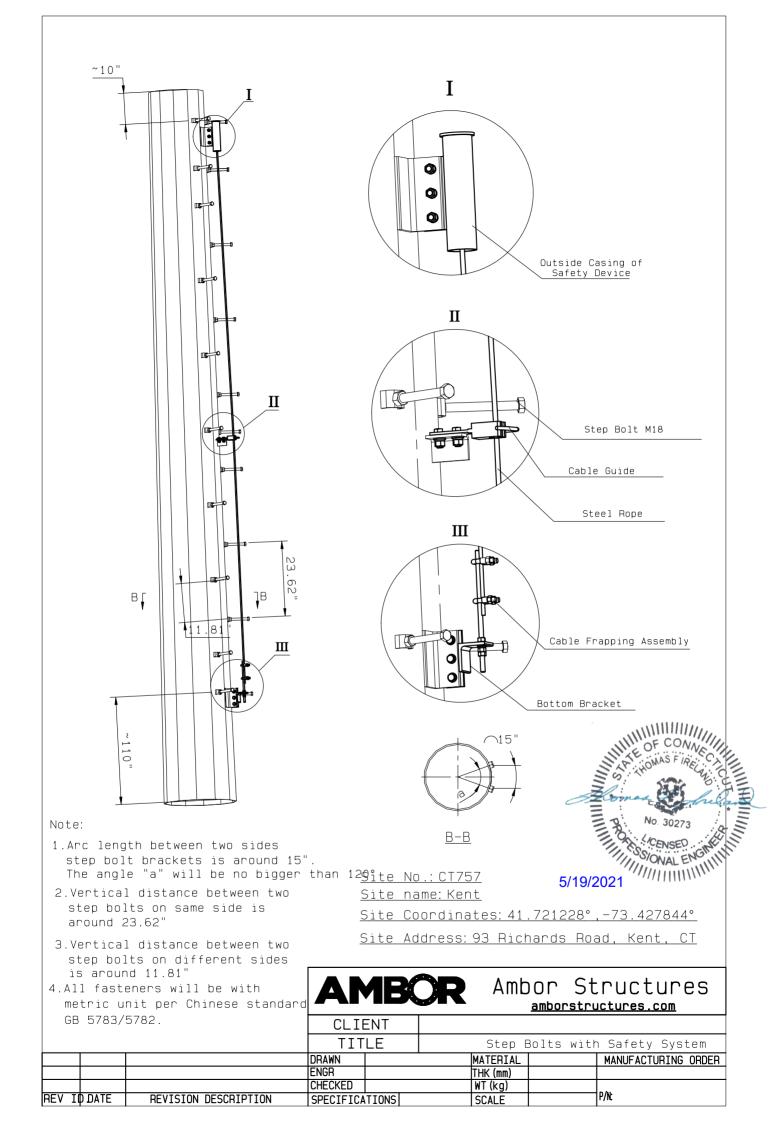


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2.5	Dark gray, with gravel, no clay					34	50/4"		100							
	GNEISS, gray, highly to moderately fractured, moderately weathered, hard					REC	ROD									
5.0	COMPRESSIVE STRENGTH 6,030 psi @ 4.5					98%	85%									_
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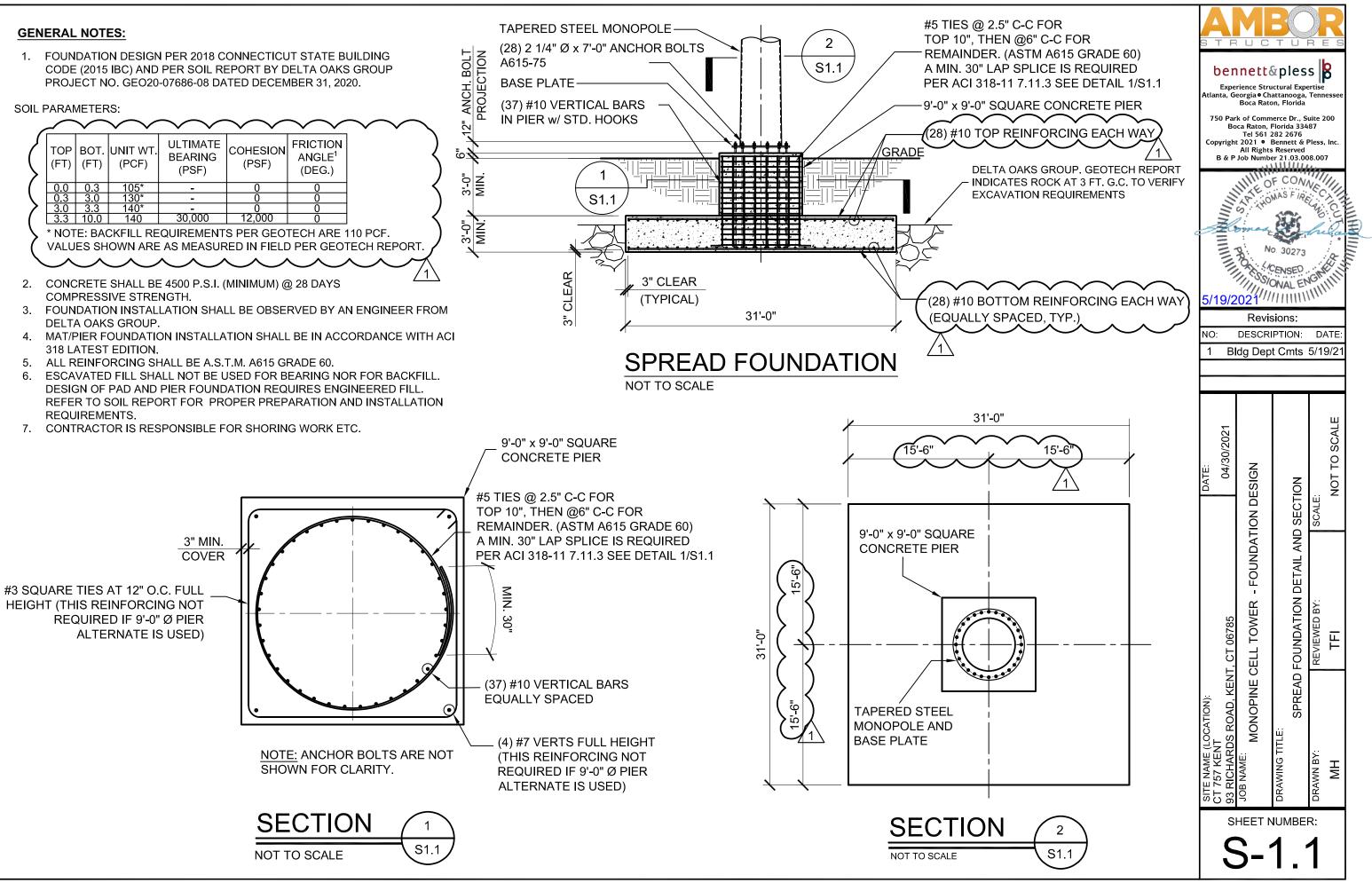
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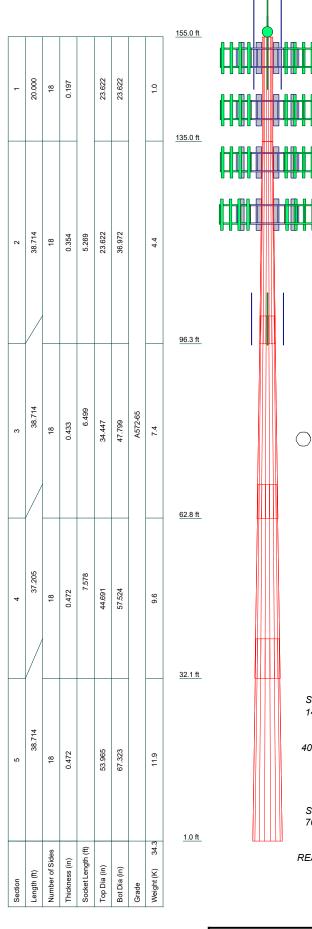




		CISO190708 QUOTATION #
· · · · · · · · · · · · · · · · · · ·	TITLE Templat	e for 135ft of 155ft.114mph TIA H
	ENGR ZHJ 2021/4/16 TH	NTERIAL MANUFACTURING ORDER
REV ID DATE REVISION DESCRIPTION	CHECKED ZHJ 2021/4/16 WI SPECIFICATIONS SC	CALE VERSION: A

1. FOUNDATION DESIGN PER 2018 CONNECTICUT STATE BUILDING CODE (2015 IBC) AND PER SOIL REPORT BY DELTA OAKS GROUP PROJECT NO. GEO20-07686-08 DATED DECEMBER 31, 2020.





DESIGNED APPURTENANCE LOADING

TYPE	ELEVATION	TYPE	ELEVATION
Microwave Mount	156	200 sq ft	141
2ft Dish	156	150 sq ft	131
20' Whip	155	150 sq ft	121
20' Whip	155	10' Whip	101
20' Whip	155	10' Whip	101
4' Ligntning Rod	155	10' Whip	101
200 sq ft	151		

MATERIAL STRENGTH

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi			

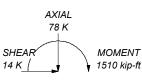
TOWER DESIGN NOTES

- Tower is located in Litchfield County, Connecticut.
 Tower designed for Exposure C to the TIA-222-H Standard.
 Tower designed for a 114 mph basic wind in accordance with the TIA-222-H Standard.
 Tower is also designed for a 40 mph basic wind with 1.00 in ice. Ice is considered to instrume in the instrument in the instrument.
- increase in thickness with height.

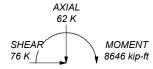
 Deflections are based upon a 60 mph wind.
 Tower Risk Category II.
 Topographic Category 5 with Crest Height of 400.000 ft
 Installation per TIA/EIA-222 and AISC Specifications.
 Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards.

- Top of baseplate is 1ft AGL.
 TOWER RATING: 97.8%

ALL REACTIONS ARE FACTORED



TORQUE 0 kip-ft 40 mph WIND - 1.000 in ICE



TORQUE 0 kip-ft REACTIONS - 114 mph WIND



	Bennett & Pless	^{000.} 135ft
	750 Park of Commerce Blvd. Ste 200	Project: CT7
	Doca Natori	^{Client:} Insite
Experience Structural Expertise	Phone: (561) 452-3316	Code: TIA-2
	FAX:	Path:

	^{Job:} 135ft of 155ft.114m		
00	Project: CT757 Kent		
	^{Client:} Insite	^{Drawn by:} jbozzetto	App'd:
	^{Code:} TIA-222-H	^{Date:} 05/19/21	Scale: NTS
	Path:	1718 CT 327 Kert - 152 MP-Biol dect comments 2015-05-19/C150160/VC CT327 Kert 1358 of 1528, 114moh TJA	Dwg No. E-1

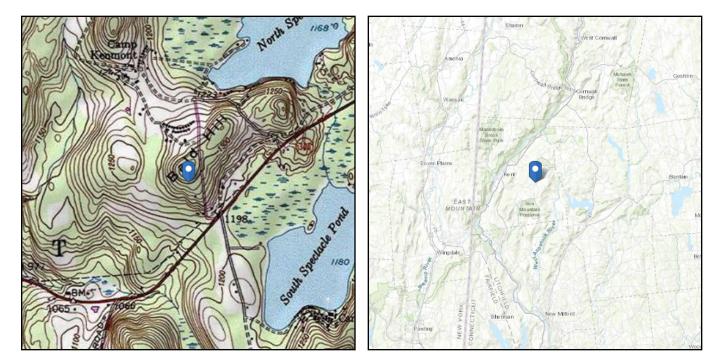


Location

ASCE 7 Hazards Report

Standard:ASCE/SEI 7-16Risk Category:IISoil Class:D - Default (see
Section 11.4.3)

Latitude: 41.721228 Longitude: -73.427844



Wind

Results:

Wind Speed:	114 Vmph
10-year MRI	75 Vmph
25-year MRI	84 Vmph
50-year MRI	89 Vmph
100-year MRI	95 Vmph
Data Source:	ASCE/SEI 7-16, Fig. 26.5-1B and Figs. CC.2-1–CC.2-4, and Section 26.5.2
Date Accessed:	Fri Apr 30 2021

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-16 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is not in a hurricane-prone region as defined in ASCE/SEI 7-16 Section 26.2.



....

Results:

Ice Thickness:	1.00 in.
Concurrent Temperature:	15 F
Gust Speed:	40 mph
Data Source:	Standard ASCE/SEI 7-16, Figs. 10-2 through 10-8
Date Accessed:	Fri Apr 30 2021

Ice thicknesses on structures in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

Values provided are equivalent radial ice thicknesses due to freezing rain with concurrent 3-second gust speeds, for a 500-year mean recurrence interval, and temperatures concurrent with ice thicknesses due to freezing rain. Thicknesses for ice accretions caused by other sources shall be obtained from local meteorological studies. Ice thicknesses in exposed locations at elevations higher than the surrounding terrain and in valleys and gorges may exceed the mapped values.

The ASCE 7 Hazard Tool is provided for your convenience, for informational purposes only, and is provided "as is" and without warranties of any kind. The location data included herein has been obtained from information developed, produced, and maintained by third party providers; or has been extrapolated from maps incorporated in the ASCE 7 standard. While ASCE has made every effort to use data obtained from reliable sources or methodologies, ASCE does not make any representations or warranties as to the accuracy, completeness, reliability, currency, or quality of any data provided herein. Any third-party links provided by this Tool should not be construed as an endorsement, affiliation, relationship, or sponsorship of such third-party content by or from ASCE.

ASCE does not intend, nor should anyone interpret, the results provided by this Tool to replace the sound judgment of a competent professional, having knowledge and experience in the appropriate field(s) of practice, nor to substitute for the standard of care required of such professionals in interpreting and applying the contents of this Tool or the ASCE 7 standard.

In using this Tool, you expressly assume all risks associated with your use. Under no circumstances shall ASCE or its officers, directors, employees, members, affiliates, or agents be liable to you or any other person for any direct, indirect, special, incidental, or consequential damages arising from or related to your use of, or reliance on, the Tool or any information obtained therein. To the fullest extent permitted by law, you agree to release and hold harmless ASCE from any and all liability of any nature arising out of or resulting from any use of data provided by the ASCE 7 Hazard Tool.

tnxTower	Job	125th of 155th 114mmb TIA LL	Page 1 of 14
		135ft of 155ft.114mph TIA-H	1 01 14
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project	CT757 Kent	Date 15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Tower Input Data

The tower is a monopole.

This tower is designed using the TIA-222-H standard. The following design criteria apply: Tower is located in Litchfield County, Connecticut. Tower base elevation above sea level: 1354.000 ft. Basic wind speed of 114 mph. Risk Category II. Exposure Category C. Crest Height: 400.000 ft. Rigorous Topographic Factor Procedure for wind speed-up calculations is used. Topographic Feature: Flat Topped Hill. Slope Distance L: 1900.000 ft. Distance from Crest x: 0.000 ft. Horizontal Distance Downwind: No. Nominal ice thickness of 1.000 in. Ice thickness is considered to increase with height. Ice density of 56.00 pcf. A wind speed of 40 mph is used in combination with ice. Temperature drop of 50.00 °F. Deflections calculated using a wind speed of 60 mph. Installation per TIA/EIA-222 and AISC Specifications.. Tower members are "hot dipped" galvanized in accordance with ASTM A123 and ASTM A153 Standards... Top of baseplate is 1ft AGL. A non-linear (P-delta) analysis was used. Pressures are calculated at each section. Stress ratio used in pole design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

Options

Consider Moments - Legs Consider Moments - Horizontals Consider Moments - Diagonals Use Moment Magnification ↓ Use Code Stress Ratios ↓ Use Code Safety Factors - Guys Escalate Ice Always Use Max Kz Use Special Wind Profile ↓ Include Bolts In Member Capacity ↓ Leg Bolts Are At Top Of Section		ibute Leg Loads As Uniform me Legs Pinned me Rigid Index Plate Clear Spans For Wind Area Clear Spans For KL/r nsion Guys To Initial Tension ass Mast Stability Checks Azimuth Dish Coefficients ext Wind Area of Appurt. calc Torque Arm Areas IBC .6D+W Combination	,	Use ASCE 10 X-Brace Ly Rules Calculate Redundant Bracing Forces Ignore Redundant Members in FEA SR Leg Bolts Resist Compression All Leg Panels Have Same Allowable Offset Girt At Foundation Consider Feed Line Torque Include Angle Block Shear Check Use TIA-222-H Bracing Resist. Exemption Use TIA-222-H Tension Splice Exemption Poles
 ✓ Secondary Horizontal Braces Leg Use Diamond Inner Bracing (4 Sided) SR Members Have Cut Ends SR Members Are Concentric 	Sort 0 √ Trian Treat	Capacity Reports By Component ngulate Diamond Inner Bracing t Feed Line Bundles As Cylinder re KL/ry For 60 Deg. Angle Legs	V	Include Shear-Torsion Interaction Always Use Sub-Critical Flow Use Top Mounted Sockets Pole Without Linear Attachments Pole With Shroud Or No Appurtenances Outside and Inside Corner Radii Are

Known

tnxTower	Job	135ft of 155ft.114mph TIA-H	Page 2 of 14
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project	CT757 Kent	Date 15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

	Tapered Pole Section Geometry								
Section	Elevation	Section Length	Splice Length	Number of	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
L1	<u>Jt</u> 155.000-135.00	<u></u>	<i>Jt</i>	Sides	<i>in</i>	in	<i>in</i>	in	1572 (5
LI	155.000-135.00 0	20.000	0.00	18	23.622	23.622	0.197	0.787	A572-65 (65 ksi)
L2	135.000-96.286	38.714	5.27	18	23.622	36.972	0.354	1.417	A572-65 (65 ksi)
L3	96.286-62.841	38.714	6.50	18	34.447	47.799	0.433	1.732	A572-65
L4	62.841-32.136	37.205	7.58	18	44.691	57.524	0.472	1.890	(65 ksi) A572-65
									(65 ksi)
L5	32.136-1.000	38.714		18	53.965	67.323	0.472	1.890	A572-65
									(65 ksi)

Tapered F	ole Pro	perties
-----------	---------	---------

Section	Tip Dia.	Area	Ι	r	С	I/C	J	It/Q	w	w/t
	in	in^2	in ⁴	in	in	in ³	in⁴	in ²	in	
L1	23.956	14.636	1014.681	8.316	12.000	84.557	2030.697	7.319	3.811	19.36
	23.956	14.636	1014.681	8.316	12.000	84.557	2030.697	7.319	3.811	19.36
L2	23.932	26.168	1789.842	8.260	12.000	149.154	3582.040	13.086	3.534	9.973
	37.488	41.182	6976.559	12.999	18.782	371.449	13962.299	20.595	5.884	16.605
L3	36.757	46.754	6833.843	12.075	17.499	390.529	13676.678	23.382	5.300	12.239
	48.470	65.108	18454.722	16.815	24.282	760.017	36933.728	32.560	7.650	17.666
L4	47.584	66.308	16380.185	15.698	22.703	721.491	32781.923	33.160	7.034	14.889
	58.338	85.550	35179.193	20.253	29.222	1203.860	70404.675	42.783	9.293	19.669
L5	57.380	80.214	28998.276	18.990	27.414	1057.782	58034.708	40.114	8.666	18.344
	68.289	100.244	56598.363	23.732	34.200	1654.923	113271.199	50.132	11.017	23.32

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A_f	Adjust. Factor A _r	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft^2	in					in	in	in
L1				1	1	1			
155.000-135.0									
00									
L2				1	1	1			
135.000-96.28									
6									
L3				1	1	1			
96.286-62.841									
L4				1	1	1			
62.841-32.136									
L5				1	1	1			
32.136-1.000									

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tnxTower		3 of 14	
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project	CT757 Kent	Date 15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Feed Line/Linear Appurtenances - Entered As Area

Description	Face	Allow	Exclude	Component	Placement	Total		$C_A A_A$	Weight
	or	Shield	From	Туре		Number			
	Leg		Torque		ft			ft^2/ft	klf
			Calculation						
LDF-50A (1 5/8	С	No	Yes	Inside Pole	155.000 - 5.000	4	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
LDF-50A (1 5/8	С	No	Yes	Inside Pole	151.000 - 5.000	14	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
LDF-50A (1 5/8	С	No	Yes	Inside Pole	141.000 - 5.000	12	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
LDF-50A (1 5/8	С	No	Yes	Inside Pole	131.000 - 5.000	16	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
LDF-50A (1 5/8	С	No	Yes	Inside Pole	121.000 - 5.000	16	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
LDF-50A (1 5/8	С	No	Yes	Inside Pole	101.000 - 5.000	3	No Ice	0.000	0.00
FOAM)							1/2" Ice	0.000	0.00
							1" Ice	0.000	0.00
Safety line 3/8	С	No	Yes	CaAa (Out	155.000 - 1.000	1	No Ice	0.037	0.00
				Of Face)			1/2" Ice	0.137	0.00
							1" Ice	0.238	0.00
Step pegs	С	No	Yes	CaAa (Out	155.000 - 1.000	1	No Ice	0.075	0.00
				Of Face)			1/2" Ice	0.175	0.00
							1" Ice	0.275	0.00

Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation	Face	A_R	A_F	C _A A _A In Face	$C_A A_A$ Out Face	Weight
	ft		ft^2	ft^2	ft^2	ft^2	K
L1	155.000-135.000	А	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	2.250	0.34

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tnxTower		135ft of 155ft.114mph TIA-H	4 of 14
Bennett & Pless	Project		Date
750 Park of Commerce Blvd. Ste 200		CT757 Kent	15:26:03 05/19/21
Boca Raton	Client	lu e ite	Designed by
Phone: (561) 452-3316 FAX:		Insite	jbozzetto

Tower	Tower	Face	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation				In Face	Out Face	
	ft		ft^2	ft^2	ft^2	ft^2	Κ
L2	135.000-96.286	А	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	4.355	1.81
L3	96.286-62.841	А	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	3.763	1.84
L4	62.841-32.136	А	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	3.454	1.69
L5	32.136-1.000	А	0.000	0.000	0.000	0.000	0.00
		В	0.000	0.000	0.000	0.000	0.00
		С	0.000	0.000	0.000	3.503	1.50

Feed Line/Linear Appurtenances Section Areas - With Ice

Tower	Tower	Face	Ice	A_R	A_F	$C_A A_A$	$C_A A_A$	Weight
Section	Elevation	or	Thickness			In Face	Out Face	
	ft	Leg	in	ft^2	ft^2	ft^2	ft^2	Κ
L1	155.000-135.000	А	1.332	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	12.909	0.45
L2	135.000-96.286	А	1.324	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	24.851	2.02
L3	96.286-62.841	А	1.304	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	21.469	2.02
L4	62.841-32.136	А	1.266	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	19.469	1.85
L5	32.136-1.000	А	1.166	0.000	0.000	0.000	0.000	0.00
		В		0.000	0.000	0.000	0.000	0.00
		С		0.000	0.000	0.000	19.272	1.66

Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
			ft ft ft	0	ft		ft^2	ft ²	Κ
Microwave Mount	С	None	<u> </u>	0.00	156.000	No Ice 1/2" Ice 1" Ice	2.500 0.000 0.000	2.500 0.000 0.000	0.08 0.10 0.13
4' Ligntning Rod	С	From Face	$0.000 \\ 0.00 \\ 2.00$	0.00	155.000	No Ice 1/2" Ice 1" Ice	0.420 0.000 0.000	$0.420 \\ 0.000 \\ 0.000$	0.02 0.01 0.02
20' Whip	А	From Face	2.000 0.00 0.00	0.00	155.000	No Ice 1/2" Ice 1" Ice	4.380 0.000 0.000	4.380 0.000 0.000	$0.06 \\ 0.08 \\ 0.10$
20' Whip	В	From Face	2.000	0.00	155.000	No Ice	4.380	4.380	0.06

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Bennett & Pless	Project		Date
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Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Description	Face or Leg	Offset Type	Offsets: Horz Lateral	Azimuth Adjustment	Placement		$C_A A_A$ Front	C _A A _A Side	Weight
			Vert ft ft ft	0	ft		ft ²	ft^2	Κ
			0.00			1/2" Ice	0.000	0.000	0.08
			0.00			1" Ice	0.000	0.000	0.10
20' Whip	С	From Face	2.000	0.00	155.000	No Ice	4.380	4.380	0.06
			0.00			1/2" Ice	0.000	0.000	0.08
*****			0.00			1" Ice	0.000	0.000	0.10
200 sq ft	С	None		0.00	151.000	No Ice	200.000	200.000	2.90
						1/2" Ice	220.000	220.000	3.10
						1" Ice	240.000	240.000	3.30
*****	C	N		0.00	1.41.000	NT	200.000	200.000	2.00
200 sq ft	С	None		0.00	141.000	No Ice 1/2" Ice	200.000 220.000	200.000	2.90
						1/2" Ice 1" Ice	220.000	220.000 240.000	3.10
*****						1 ^m Ice	240.000	240.000	3.30
150 sq ft	С	None		0.00	131.000	No Ice	150.000	150.000	2.20
-						1/2" Ice	170.000	170.000	2.40
						1" Ice	190.000	190.000	2.60

150 sq ft	С	None		0.00	121.000	No Ice	150.000	150.000	2.20
						1/2" Ice	170.000	170.000	2.40
						1" Ice	190.000	190.000	2.60

10' Whip	А	From Face	2.000	0.00	101.000	No Ice	2.200	2.200	0.03
			0.00			1/2" Ice	0.000	0.000	0.05
1013371	P	F F	0.00	0.00	101.000	1" Ice	0.000	0.000	0.07
10' Whip	В	From Face	2.000	0.00	101.000	No Ice	2.200	2.200	0.03
			0.00			1/2" Ice	0.000	0.000	0.04
101 3375	C	EE.	0.00	0.00	101.000	1" Ice	0.000	0.000	0.05
10' Whip	С	From Face	2.000	0.00	101.000	No Ice 1/2" Ice	2.200 0.000	2.200	0.03
			$\begin{array}{c} 0.00\\ 0.00\end{array}$			1/2" Ice 1" Ice	0.000	$0.000 \\ 0.000$	0.04 0.05
			0.00			1 Ice	0.000	0.000	0.05

Dishes											
Description	Face or Leg	Dish Type	Offset Type	Offsets: Horz Lateral Vert	Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter		Aperture Area	Weight
				ft	0	0	ft	ft		ft^2	Κ
2ft Dish		Paraboloid	None		0.00		156.000	2.000	No Ice	3.140	0.03
		w/Shroud (HP)							1/2" Ice	3.410	0.05
									1" Ice	3.680	0.07

Load Combinations

Comb. No. Description

1 Dead Only

	Job	Page
tnxTower	135ft of 155ft.114mph TIA-H	6 of 14
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project CT757 Kent	Date 15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	Client Insite	Designed by jbozzetto

Comb.	Description
No.	
2	1.2 Dead+1.0 Wind 0 deg - No Ice
3	0.9 Dead+1.0 Wind 0 deg - No Ice
4	1.2 Dead+1.0 Wind 30 deg - No Ice
5	0.9 Dead+1.0 Wind 30 deg - No Ice
6	1.2 Dead+1.0 Wind 60 deg - No Ice
7	0.9 Dead+1.0 Wind 60 deg - No Ice
8	1.2 Dead+1.0 Wind 90 deg - No Ice
9	0.9 Dead+1.0 Wind 90 deg - No Ice
10	1.2 Dead+1.0 Wind 120 deg - No Ice
11	0.9 Dead+1.0 Wind 120 deg - No Ice
12	1.2 Dead+1.0 Wind 150 deg - No Ice
13	0.9 Dead+1.0 Wind 150 deg - No Ice
14	1.2 Dead+1.0 Wind 180 deg - No Ice
15	0.9 Dead+1.0 Wind 180 deg - No Ice
16	1.2 Dead+1.0 Wind 210 deg - No Ice
17	0.9 Dead+1.0 Wind 210 deg - No Ice
18	1.2 Dead+1.0 Wind 240 deg - No Ice
19	0.9 Dead+1.0 Wind 240 deg - No Ice
20	1.2 Dead+1.0 Wind 270 deg - No Ice
21	0.9 Dead+1.0 Wind 270 deg - No Ice
22	1.2 Dead+1.0 Wind 300 deg - No Ice
23	0.9 Dead+1.0 Wind 300 deg - No Ice
24	1.2 Dead+1.0 Wind 330 deg - No Ice
25	0.9 Dead+1.0 Wind 330 deg - No Ice
26 27	1.2 Dead+1.0 Ice+1.0 Temp
	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp
28 29	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp
30	1.2 Dead+1.0 Wind 40 deg+1.0 Ice+1.0 Temp 1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp
32	1.2 Dead + 1.0 Wind 120 deg + 1.0 Ice + 1.0 Temp 1.2 Dead + 1.0 Wind 150 deg + 1.0 Ice + 1.0 Temp
33	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp
34	1.2 Dead+1.0 Wind 100 deg+1.0 Ice+1.0 Temp
35	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp
36	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp
37	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp
38	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp
39	Dead+Wind 0 deg - Service
40	Dead+Wind 30 deg - Service
41	Dead+Wind 60 deg - Service
42	Dead+Wind 90 deg - Service
43	Dead+Wind 120 deg - Service
44	Dead+Wind 150 deg - Service
45	Dead+Wind 180 deg - Service
46	Dead+Wind 210 deg - Service
47	Dead+Wind 240 deg - Service
48	Dead+Wind 270 deg - Service
49	Dead+Wind 300 deg - Service
50	Dead+Wind 330 deg - Service

Section No.	Maximum Member Forces							
	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment	
				Comb.	K	kip-ft	kip-ft	
L1	155 - 135	Pole	Max Tension	1	0.00	0.00	0.00	
			Max. Compression	26	-11.19	0.00	-0.02	
			Max. Mx	8	-4.39	-356.24	-0.02	
			Max. My	14	-4.39	0.00	-356.26	

tnxTower	Job	135ft of 155ft.114mph TIA-H	Page 7 of 14
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project	CT757 Kent	Date 15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Section No.	Elevation ft	Component Type	Condition	Gov. Load	Axial	Major Axis Moment	Minor Axis Moment
	·			Comb.	K	kip-ft	kip-ft
			Max. Vy	8	31.39	-356.24	-0.02
			Max. Vx	14	31.39	0.00	-356.26
			Max. Torque	8			-0.03
L2	135 - 96.2861	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-25.79	0.00	-0.02
			Max. Mx	8	-15.02	-1987.09	-0.02
			Max. My	14	-15.02	0.00	-1987.11
			Max. Vy	8	56.72	-1987.09	-0.02
			Max. Vx	14	56.72	0.00	-1987.11
			Max. Torque	8			-0.03
L3	96.2861 - 62.8412	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-38.79	0.08	0.02
			Max. Mx	8	-27.13	-3915.79	-0.02
			Max. My	14	-27.13	0.00	-3915.82
			Max. Vy	8	62.64	-3915.79	-0.02
			Max. Vx	14	62.64	0.00	-3915.82
			Max. Torque	8			-0.03
L4	62.8412 - 32.1358	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-54.47	0.08	0.02
			Max. Mx	8	-41.28	-5856.40	-0.02
			Max. My	14	-41.28	0.00	-5856.42
			Max. Vy	8	68.31	-5856.40	-0.02
			Max. Vx	14	68.31	0.00	-5856.42
			Max. Torque	8			-0.03
L5	32.1358 - 1	Pole	Max Tension	1	0.00	0.00	0.00
			Max. Compression	26	-77.97	0.08	0.02
			Max. Mx	8	-62.45	-8645.53	-0.02
			Max. My	14	-62.45	0.00	-8645.55
			Max. Vy	8	75.60	-8645.53	-0.02
			Max. Vx	14	75.60	0.00	-8645.55
			Max. Torque	8			-0.03

Maximum Reactions

Location	Condition	Gov. Load	Vertical K	Horizontal, X K	Horizontal, Z K
		Comb.	K	K	K
Pole	Max. Vert	33	77.97	0.00	-13.86
	Max. H _x	20	62.50	75.57	0.00
	Max. Hz	2	62.50	0.00	75.57
	Max. M _x	2	8645.51	0.00	75.57
	Max. M _z	8	8645.53	-75.57	0.00
	Max. Torsion	20	0.03	75.57	0.00
	Min. Vert	13	46.87	-37.78	-65.44
	Min. H _x	8	62.50	-75.57	0.00
	Min. Hz	14	62.50	0.00	-75.57
	Min. M _x	14	-8645.55	0.00	-75.57
	Min. Mz	20	-8645.53	75.57	0.00
	Min. Torsion	8	-0.03	-75.57	0.00

tnxTower	Job 135ft of 155ft.114mph TIA-H	Page 8 of 14
Bennett & Pless 750 Park of Commerce Blvd. Ste 200	Project CT757 Kent	Date 15:26:03 05/19/21
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Load Combination	Vertical	Shear _x	Shear _z	Overturning Moment, M _x	Overturning Moment, M _z	Torque
	K	Κ	K	kip-ft	kip-ft	kip-ft
Dead Only	52.08	0.00	0.00	0.02	0.00	0.00
1.2 Dead+1.0 Wind 0 deg - No Ice	62.50	0.00	-75.57	-8645.51	0.00	0.00
0.9 Dead+1.0 Wind 0 deg - No	46.87	0.00	-75.57	-8588.75	0.00	0.00
Ice 1.2 Dead+1.0 Wind 30 deg - No	62.50	37.78	-65.44	-7487.23	-4322.77	0.02
Ice	02.50	57.78	-05.44	-7487.25	-+322.11	0.02
0.9 Dead+1.0 Wind 30 deg - No	46.87	37.78	-65.44	-7438.07	-4294.38	0.01
Ice 1.2 Dead+1.0 Wind 60 deg - No	62.50	65.44	-37.78	-4322.74	-7487.25	0.03
Ice	16.05	(- - - -	25 50	1001.04	5 12 0 00	0.02
0.9 Dead+1.0 Wind 60 deg - No Ice	46.87	65.44	-37.78	-4294.36	-7438.09	0.03
1.2 Dead+1.0 Wind 90 deg - No	62.50	75.57	0.00	0.02	-8645.53	0.03
Ice 0.9 Dead+1.0 Wind 90 deg - No	46.87	75.57	0.00	0.02	-8588.76	0.03
Ice		15.51	0.00	0.02	0500.70	0.05
1.2 Dead+1.0 Wind 120 deg -	62.50	65.44	37.78	4322.79	-7487.25	0.03
No Ice 0.9 Dead+1.0 Wind 120 deg -	46.87	65.44	37.78	4294.40	-7438.09	0.03
No Ice	(2.50	27.70	65.44	7497 29	1222 77	0.02
1.2 Dead+1.0 Wind 150 deg - No Ice	62.50	37.78	65.44	7487.28	-4322.77	0.02
0.9 Dead+1.0 Wind 150 deg -	46.87	37.78	65.44	7438.11	-4294.38	0.01
No Ice 1.2 Dead+1.0 Wind 180 deg -	62.50	0.00	75.57	8645.55	0.00	0.00
No Ice						
0.9 Dead+1.0 Wind 180 deg - No Ice	46.87	0.00	75.57	8588.78	0.00	0.00
1.2 Dead+1.0 Wind 210 deg -	62.50	-37.78	65.44	7487.28	4322.77	-0.02
No Ice 0.9 Dead+1.0 Wind 210 deg -	46.87	-37.78	65.44	7438.11	4294.38	-0.01
No Ice	40.87	-37.78	05.44	/430.11	4294.38	-0.01
1.2 Dead+1.0 Wind 240 deg -	62.50	-65.44	37.78	4322.79	7487.25	-0.03
No Ice 0.9 Dead+1.0 Wind 240 deg -	46.87	-65.44	37.78	4294.40	7438.09	-0.03
No Ice	(2 , 5)		0.00	0.02	0.645.50	0.00
1.2 Dead+1.0 Wind 270 deg - No Ice	62.50	-75.57	0.00	0.02	8645.53	-0.03
0.9 Dead+1.0 Wind 270 deg -	46.87	-75.57	0.00	0.02	8588.76	-0.03
No Ice 1.2 Dead+1.0 Wind 300 deg -	62.50	-65.44	-37.78	-4322.74	7487.25	-0.03
No Ice						
0.9 Dead+1.0 Wind 300 deg - No Ice	46.87	-65.44	-37.78	-4294.36	7438.09	-0.03
1.2 Dead+1.0 Wind 330 deg -	62.50	-37.78	-65.44	-7487.23	4322.77	-0.02
No Ice	46.87	-37.78	-65.44	-7438.07	4294.38	-0.01
0.9 Dead+1.0 Wind 330 deg - No Ice	40.87	-37.78	-05.44	-7438.07	4294.38	-0.01
1.2 Dead+1.0 Ice+1.0 Temp	77.97	0.00	0.00	-0.02	0.08	0.00
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp	77.97	0.00	-13.86	-1510.37	0.08	-0.00
1.2 Dead+1.0 Wind 30 deg+1.0	77.97	6.93	-12.01	-1308.02	-755.09	-0.00
Ice+1.0 Temp 1.2 Dead+1.0 Wind 60 deg+1.0	77.97	12.01	-6.93	-755.20	-1307.91	-0.00
Ice+1.0 Temp						
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp	77.97	13.86	0.00	-0.02	-1510.26	0.00
1.2 Dead+1.0 Wind 120	77.97	12.01	6.93	755.15	-1307.91	0.00
deg+1.0 Ice+1.0 Temp						

tnxTower	Job	135ft of 155ft.114mph TIA-H	Page 9 of 14
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Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Load Combination	Vertical	Shear _x	Shearz	Overturning Moment, M_x	Overturning Moment, M _z	Torque
	Κ	K	K	kip-ft	kip-ft	kip-ft
1.2 Dead+1.0 Wind 150	77.97	6.93	12.01	1307.97	-755.09	0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 180	77.97	0.00	13.86	1510.32	0.08	0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 210	77.97	-6.93	12.01	1307.97	755.25	0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 240	77.97	-12.01	6.93	755.15	1308.08	0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 270	77.97	-13.86	0.00	-0.02	1510.42	-0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 300	77.97	-12.01	-6.93	-755.20	1308.08	-0.00
deg+1.0 Ice+1.0 Temp						
1.2 Dead+1.0 Wind 330	77.97	-6.93	-12.01	-1308.02	755.25	-0.00
deg+1.0 Ice+1.0 Temp						
Dead+Wind 0 deg - Service	52.08	0.00	-18.73	-2139.16	0.00	0.00
Dead+Wind 30 deg - Service	52.08	9.36	-16.22	-1852.57	-1069.59	0.00
Dead+Wind 60 deg - Service	52.08	16.22	-9.36	-1069.57	-1852.59	0.01
Dead+Wind 90 deg - Service	52.08	18.73	0.00	0.02	-2139.19	0.01
Dead+Wind 120 deg - Service	52.08	16.22	9.36	1069.61	-1852.59	0.01
Dead+Wind 150 deg - Service	52.08	9.36	16.22	1852.61	-1069.59	0.00
Dead+Wind 180 deg - Service	52.08	0.00	18.73	2139.21	0.00	0.00
Dead+Wind 210 deg - Service	52.08	-9.36	16.22	1852.61	1069.59	-0.00
Dead+Wind 240 deg - Service	52.08	-16.22	9.36	1069.61	1852.59	-0.01
Dead+Wind 270 deg - Service	52.08	-18.73	0.00	0.02	2139.19	-0.01
Dead+Wind 300 deg - Service	52.08	-16.22	-9.36	-1069.57	1852.59	-0.01
Dead+Wind 330 deg - Service	52.08	-9.36	-16.22	-1852.57	1069.59	-0.00

Solution	Summary

	Sui	n of Applied Force.	5		Sum of Reaction	is	
Load	PX	PY	PZ	PX	PY	PZ	% Error
Comb.	K	K	K	K	K	K	
1	0.00	-52.08	0.00	0.00	52.08	0.00	0.000%
2	0.00	-62.50	-75.57	0.00	62.50	75.57	0.000%
3	0.00	-46.87	-75.57	0.00	46.87	75.57	0.000%
4	37.78	-62.50	-65.44	-37.78	62.50	65.44	0.000%
5	37.78	-46.87	-65.44	-37.78	46.87	65.44	0.000%
6	65.44	-62.50	-37.78	-65.44	62.50	37.78	0.000%
7	65.44	-46.87	-37.78	-65.44	46.87	37.78	0.000%
8	75.57	-62.50	0.00	-75.57	62.50	0.00	0.000%
9	75.57	-46.87	0.00	-75.57	46.87	0.00	0.000%
10	65.44	-62.50	37.78	-65.44	62.50	-37.78	0.000%
11	65.44	-46.87	37.78	-65.44	46.87	-37.78	0.000%
12	37.78	-62.50	65.44	-37.78	62.50	-65.44	0.000%
13	37.78	-46.87	65.44	-37.78	46.87	-65.44	0.000%
14	0.00	-62.50	75.57	0.00	62.50	-75.57	0.000%
15	0.00	-46.87	75.57	0.00	46.87	-75.57	0.000%
16	-37.78	-62.50	65.44	37.78	62.50	-65.44	0.000%
17	-37.78	-46.87	65.44	37.78	46.87	-65.44	0.000%
18	-65.44	-62.50	37.78	65.44	62.50	-37.78	0.000%
19	-65.44	-46.87	37.78	65.44	46.87	-37.78	0.000%
20	-75.57	-62.50	0.00	75.57	62.50	0.00	0.000%
21	-75.57	-46.87	0.00	75.57	46.87	0.00	0.000%
22	-65.44	-62.50	-37.78	65.44	62.50	37.78	0.000%
23	-65.44	-46.87	-37.78	65.44	46.87	37.78	0.000%
24	-37.78	-62.50	-65.44	37.78	62.50	65.44	0.000%
25	-37.78	-46.87	-65.44	37.78	46.87	65.44	0.000%
26	0.00	-77.97	0.00	0.00	77.97	0.00	0.000%

tnxTower	Job 135ft of 155ft.114mph TIA-H	Page 10 of 14
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	Sum of Applied Forces				Sum of Reactions			
Load	PX	PY	PZ	PX	ΡŶ	PZ	% Error	
Comb.	Κ	Κ	Κ	Κ	Κ	Κ		
27	0.00	-77.97	-13.86	0.00	77.97	13.86	0.000%	
28	6.93	-77.97	-12.01	-6.93	77.97	12.01	0.000%	
29	12.01	-77.97	-6.93	-12.01	77.97	6.93	0.000%	
30	13.86	-77.97	0.00	-13.86	77.97	0.00	0.000%	
31	12.01	-77.97	6.93	-12.01	77.97	-6.93	0.000%	
32	6.93	-77.97	12.01	-6.93	77.97	-12.01	0.000%	
33	0.00	-77.97	13.86	0.00	77.97	-13.86	0.000%	
34	-6.93	-77.97	12.01	6.93	77.97	-12.01	0.000%	
35	-12.01	-77.97	6.93	12.01	77.97	-6.93	0.000%	
36	-13.86	-77.97	0.00	13.86	77.97	0.00	0.000%	
37	-12.01	-77.97	-6.93	12.01	77.97	6.93	0.000%	
38	-6.93	-77.97	-12.01	6.93	77.97	12.01	0.000%	
39	0.00	-52.08	-18.73	0.00	52.08	18.73	0.000%	
40	9.36	-52.08	-16.22	-9.36	52.08	16.22	0.000%	
41	16.22	-52.08	-9.36	-16.22	52.08	9.36	0.000%	
42	18.73	-52.08	0.00	-18.73	52.08	0.00	0.000%	
43	16.22	-52.08	9.36	-16.22	52.08	-9.36	0.000%	
44	9.36	-52.08	16.22	-9.36	52.08	-16.22	0.000%	
45	0.00	-52.08	18.73	0.00	52.08	-18.73	0.000%	
46	-9.36	-52.08	16.22	9.36	52.08	-16.22	0.000%	
47	-16.22	-52.08	9.36	16.22	52.08	-9.36	0.000%	
48	-18.73	-52.08	0.00	18.73	52.08	0.00	0.000%	
49	-16.22	-52.08	-9.36	16.22	52.08	9.36	0.000%	
50	-9.36	-52.08	-16.22	9.36	52.08	16.22	0.000%	

		Non-Li	near Conve	rgence Resu
Load	Converged?	Number	Displacement	Force
Combination		of Cycles	Tolerance	Tolerance
1	Yes	4	0.00000001	0.00000001
2	Yes	4	0.00000001	0.00012664
3	Yes	4	0.00000001	0.00004978
4	Yes	6	0.00000001	0.00001034
5	Yes	5	0.00000001	0.00014483
6	Yes	6	0.00000001	0.00001033
7	Yes	5	0.00000001	0.00014469
8	Yes	4	0.00000001	0.00012719
9	Yes	4	0.00000001	0.00005008
10	Yes	6	0.00000001	0.00001035
11	Yes	5	0.00000001	0.00014487
12	Yes	6	0.00000001	0.00001034
13	Yes	5	0.00000001	0.00014473
14	Yes	4	0.00000001	0.00012664
15	Yes	4	0.00000001	0.00004978
16	Yes	6	0.00000001	0.00001034
17	Yes	5	0.00000001	0.00014473
18	Yes	6	0.00000001	0.00001035
19	Yes	5	0.00000001	0.00014487
20	Yes	4	0.00000001	0.00012719
21	Yes	4	0.00000001	0.00005008
22	Yes	6	0.00000001	0.00001033
23	Yes	5	0.00000001	0.00014469
24	Yes	6	0.00000001	0.00001034
25	Yes	5	0.00000001	0.00014483
26	Yes	4	0.00000001	0.00000001
27	Yes	5	0.00000001	0.00007229

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0.000			15511 01 155		
Benn	nett & Pless	Project			Date
	ommerce Blvd. Ste 200		СТ	757 Kent	15:26:03 05/19/2
	oca Raton (561) 452-3316 FAX:	Client		Designed by jbozzetto	
28	Yes	5	0.00000001	0.00008454	
29	Yes	5	0.00000001	0.00008454	
30	Yes	5	0.00000001	0.00007228	
31	Yes	5	0.0000001	0.00008454	
32	Yes	5	0.0000001	0.00008454	
33	Yes	5	0.0000001	0.00007229	
34	Yes	5	0.0000001	0.00008455	
35	Yes	5	0.0000001	0.00008455	
36	Yes	5	0.0000001	0.00007230	
37	Yes	5	0.00000001	0.00008455	
38	Yes	5	0.00000001	0.00008455	
39	Yes	4	0.00000001	0.00005790	
40	Yes	5	0.00000001	0.00002627	
41	Yes	5	0.00000001	0.00002625	
42	Yes	4	0.00000001	0.00005792	
43	Yes	5	0.00000001	0.00002629	
44	Yes	5	0.00000001	0.00002626	
45	Yes	4	0.00000001	0.00005790	
46	Yes	5	0.00000001	0.00002626	
47	Yes	5	0.00000001	0.00002629	
48	Yes	4	0.00000001	0.00005792	
49	Yes	5	0.00000001	0.00002625	
50	Yes	5	0.00000001	0.00002627	

Maximum Tower Deflections - Service Wind

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	ft	Comb.	0	0
L1	155 - 135	2.90	45	2.25	0.00
L2	135 - 96.2861	2.13	45	2.07	0.00
L3	101.555 - 62.8412	1.11	45	1.38	0.00
L4	69.3406 - 32.1358	0.48	45	0.82	0.00
L5	39.7139 - 1	0.15	45	0.42	0.00

Critical Deflections and Radius of Curvature - Service Wind

Elevation	Appurtenance	Gov. Load	Deflection	Tilt	Twist	Radius of Curvature
ft		Comb.	ft	0	0	ft
156.000	2ft Dish	45	2.90	2.25	0.00	12492
155.000	4' Ligntning Rod	45	2.90	2.25	0.00	12492
151.000	200 sq ft	45	2.74	2.22	0.00	12492
141.000	200 sq ft	45	2.35	2.14	0.00	4461
131.000	150 sq ft	45	1.99	2.01	0.00	3068
121.000	150 sq ft	45	1.65	1.82	0.00	2937
101.000	10' Whip	45	1.09	1.37	0.00	2752

Maximum Tower Deflections - Design Wind

tnxTower	Job	135ft of 155ft.114mph TIA-H	Page 12 of 14
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Boca Raton Phone: (561) 452-3316 FAX:	Client	Insite	Designed by jbozzetto

Section	Elevation	Horz.	Gov.	Tilt	Twist
No.		Deflection	Load		
	ft	ft	Comb.	0	0
L1	155 - 135	11.68	14	9.06	0.00
L2	135 - 96.2861	8.59	14	8.36	0.00
L3	101.555 - 62.8412	4.46	14	5.59	0.00
L4	69.3406 - 32.1358	1.94	14	3.31	0.00
L5	39.7139 - 1	0.61	14	1.72	0.00

Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov.	Deflection	Tilt	Twist	Radius of
		Load		0	0	Curvature
ft		Comb.	ft	0	0	ft
156.000	2ft Dish	14	11.68	9.06	0.00	3251
155.000	4' Ligntning Rod	14	11.68	9.06	0.00	3251
151.000	200 sq ft	14	11.04	8.96	0.00	3251
141.000	200 sq ft	14	9.48	8.65	0.00	1158
131.000	150 sq ft	14	8.02	8.12	0.00	792
121.000	150 sq ft	14	6.68	7.35	0.00	752
101.000	10' Whip	14	4.41	5.54	0.00	695

Base Plate Design Data

Plate	Number	Anchor Bolt	Actual	Actual	Actual	Actual	Controlling	Critical
Thickness	of Anchor Bolts	Size	Allowable Ratio Bolt Tension K	Allowable Ratio Concrete Stress ksi	Allowable Ratio Plate Stress ksi	Allowable Ratio Stiffener Stress ksi	Condition	Ratio
in		in						
3.150	28	2.250	158.46	3.64	32.90		Plate	0.73
			243.58 0.65	6.12 0.60	45.00 0.73			~

Compression Checks

			Ро	le Des	sign I	Data			
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	Ratio P_u
	ft		ft	ft		in ²	Κ	Κ	ϕP_n
L1	155 - 135 (1)	TP23.622x23.622x0.197	20.000	0.000	0.0	14.636	-4.39	856.21	0.005
L2	135 - 96.2861 (2)	TP36.972x23.622x0.354	38.714	0.000	0.0	39.139	-15.02	2289.63	0.007
L3	96.2861 - 62.8412 (3)	TP47.799x34.447x0.433	38.714	0.000	0.0	62.027	-27.13	3628.56	0.007
L4	62.8412 - 32.1358 (4)	TP57.524x44.691x0.472	37.205	0.000	0.0	81.631	-41.28	4775.38	0.009

	tnxTowe	Job	1	35ft of 1	55ft.11	4mph TIA	-H		Page 13	of 14
750 P	Bennett & Ple. Park of Commerce Blu		Project CT757 Kent							3 05/19/21
	Boca Raton Phone: (561) 452-3 FAX:	316 Client			Insite	9			Designed jbo:	by zzetto
G	FI , ·	0.	T	I	¥1/		D		D. (;	
Section No.	Elevation	Size	L	L_u	Kl/r	A	P_u	ϕP_n	$Ratio P_u$	
	ft		ft	ft		in ²	Κ	Κ	ϕP_n	
L5	32.1358 - 1 (5)	TP67.323x53.965x0.472	38.714	0.000	0.0	100.244	-62.45	5864.28	0.011	

Pole Bending Design Data

Section No.	Elevation	Size	M_{ux}	ϕM_{nx}	Ratio M _{ux}	M_{uy}	ϕM_{ny}	$Ratio M_{uy}$
	ft		kip-ft	kip-ft	ϕM_{nx}	kip-ft	kip-ft	ϕM_{ny}
L1	155 - 135 (1)	TP23.622x23.622x0.197	356.26	492.09	0.724	0.00	492.09	0.000
L2	135 - 96.2861 (2)	TP36.972x23.622x0.354	1987.11	2059.71	0.965	0.00	2059.71	0.000
L3	96.2861 - 62.8412 (3)	TP47.799x34.447x0.433	3915.82	4170.92	0.939	0.00	4170.92	0.000
L4	62.8412 - 32.1358 (4)	TP57.524x44.691x0.472	5856.42	6440.43	0.909	0.00	6440.43	0.000
L5	32.1358 - 1 (5)	TP67.323x53.965x0.472	8645.58	9052.92	0.955	0.00	9052.92	0.000

Pole Shear Design Data

Section No.	Elevation	Size	Actual V_u	ϕV_n	Ratio V_u	Actual T_u	ϕT_n	Ratio T_u
	ft		Κ	K	ϕV_n	kip-ft	kip-ft	ϕT_n
L1	155 - 135 (1)	TP23.622x23.622x0.197	31.39	256.86	0.122	0.02	526.95	0.000
L2	135 - 96.2861 (2)	TP36.972x23.622x0.354	56.72	686.89	0.083	0.00	2093.43	0.000
L3	96.2861 - 62.8412 (3)	TP47.799x34.447x0.433	62.64	1088.57	0.058	0.00	4301.78	0.000
L4	62.8412 - 32.1358 (4)	TP57.524x44.691x0.472	68.31	1432.61	0.048	0.02	6829.78	0.000
L5	32.1358 - 1 (5)	TP67.323x53.965x0.472	75.60	1759.28	0.043	0.02	10299.58	0.000

Pole Interaction Design Data

Section No.	Elevation	Ratio P_u	Ratio M _{ux}	Ratio M _{uy}	Ratio V_u	Ratio T_u	Comb. Stress	Allow. Stress	Criteria
	ft	ϕP_n	ϕM_{nx}	ϕM_{nv}	ϕV_n	ϕT_n	Ratio	Ratio	
L1	155 - 135 (1)	0.005	0.724	0.000	0.122	0.000	0.744	1.000	4.8.2 🖌
L2	135 - 96.2861 (2)	0.007	0.965	0.000	0.083	0.000	0.978	1.000	4.8.2 🖌
L3	96.2861 - 62.8412 (3)	0.007	0.939	0.000	0.058	0.000	0.950	1.000	4.8.2 🖌
L4	62.8412 - 32.1358 (4)	0.009	0.909	0.000	0.048	0.000	0.920	1.000	4.8.2 🖌
L5	32.1358 - 1 (5)	0.011	0.955	0.000	0.043	0.000	0.967	1.000	4.8.2 🖌

<i>tnxTower</i>		Page
inx i ower	135ft of 155ft.114mph TIA-H	14 of 14
Bennett & Pless Proje	ct	Date
750 Park of Commerce Blvd. Ste 200	CT757 Kent	15:26:03 05/19/21
Boca Raton Phone: (561) 452-3316 FAX:	t Insite	Designed by jbozzetto

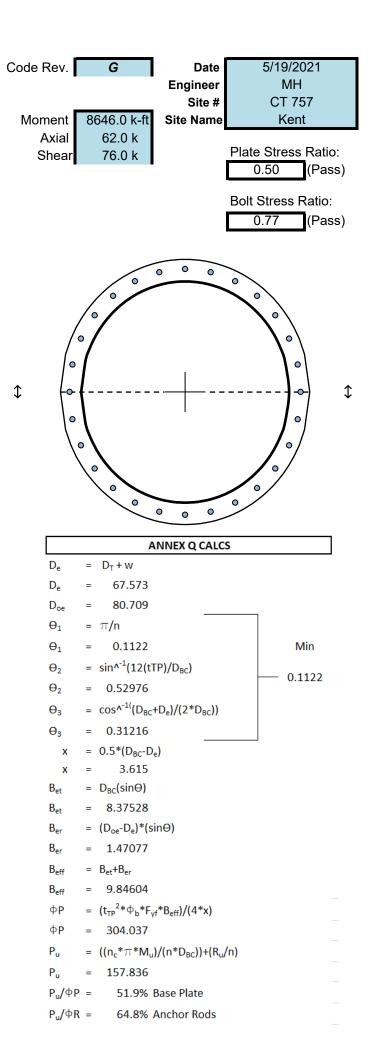
Section No.	Elevation	Ratio P_u	Ratio M _{ux}	Ratio M _{uy}	$Ratio V_u$	Ratio T_u	Comb. Stress	Allow. Stress	Criteria
	ft	ϕP_n	ϕM_{nx}	ϕM_{ny}	ϕV_n	ϕT_n	Ratio	Ratio	

Section Capacity Table

Section	Elevation	Component	Size	Critical	Р		%	Pass
No.	ft	Туре		Element	K	K	Capacity	Fail
L1	155 - 135	Pole	TP23.622x23.622x0.197	1	-4.39	856.21	74.4	Pass
L2	135 - 96.2861	Pole	TP36.972x23.622x0.354	2	-15.02	2289.63	97.8	Pass
L3	96.2861 - 62.8412	Pole	TP47.799x34.447x0.433	3	-27.13	3628.56	95.0	Pass
L4	62.8412 - 32.1358	Pole	TP57.524x44.691x0.472	4	-41.28	4775.38	92.0	Pass
L5	32.1358 - 1	Pole	TP67.323x53.965x0.472	5	-62.45	5864.28	96.7	Pass
							Summary	
						Pole (L2)	97.8	Pass
						Base Plate	73.1	Pass
						RATING =	97.8	Pass

Program Version 8.0.9.0 - 4/12/2021 File:Y:/Shared/Projects/2021/21.03.000 - Boca Raton/21.03.008.xxx - Ambor/21.03.008.007 - C15019070B CT 757 Kent - 155' MP/Bldg dept comments 2021-05-19/C15019070C.CT757 Kent.135ft of 155ft.114mph TIA H_rev1.eri

_		_	
Í	Plate Type	Baseplate	
te	Pole Diameter	67.323	
Pla	Pole Thickness	0.472	in
ge	Plate Diameter	80.709	in
Base/Flange Plate	Plate Thickness	3.15	in
Ē	Plate Fy	50	ksi
ase	Weld Length	0.3125	in
ñ	ϕ_s Resistance	843.20	
	Applied	422.10	k-in
	#	0	
Stiffeners			
			-
	#	28	
	Bolt Circle	74.803	in
	(R)adial / (S)quare	R	
	D . (0.05	
	Diameter	2.25	
Bolts	Hole Diameter	2.64	IN
ğ	Туре	A615-75	
	Fy		ksi
	Fu	100	
	ϕ_s Resistance	259.82	
	Applied	200.28	k
	#	0	
•			
en			
em			
nforcement			
Re			
	#	0	
	#	0	
s			
20 M			
a E			
Extra Bolts 0			
Ĩ			



Anchor bolt length calculation

PROJECT/ POLE TYPE:

Monopole

Reference: According to the code ACI 318-14 (25.4.2.3), for deformed bars, we can get below information:

The user may easily construct simple, useful expressions. For example, in all structures with normalweight concrete $(\lambda = 1.0)$, uncoated reinforcement ($\psi_e = 1.0$), No. 7 or larger bottom bars ($\psi_t = 1.0$) with $f_c' = 4000$ psi and Grade 60 reinforcement, the equations reduce to

$$\ell_d = \frac{(60,000)(1.0)(1.0)}{20(1.0)\sqrt{4000}} d_b = 47d_b$$

or

$$\ell_d = \frac{3(60,000)(1.0)(1.0)}{40(1.0)\sqrt{4000}}d_b = 71d_b$$

Thus, as long as minimum cover of d_b is provided along with a minimum clear spacing of $2d_b$, or a minimum clear cover of d_b and a minimum clear spacing of d_b are provided along with minimum ties or stirrups, then $\ell_d = 47d_b$. The penalty for spacing bars closer or providing less cover is the requirement that $\ell_d = 71d_b$.

Many practical combinations of side cover, clear cover, and confining reinforcement can be used with 12.2.3 to produce significantly shorter development lengths than allowed by 12.2.2. For example, bars or wires with minimum clear cover not less than $2d_b$ and minimum clear spacing not less than $4d_b$ and without any confining reinforcement would have a $(c_b + K_{tr})/d_b$ value of 2.5 and would require a development length of only $28d_b$ for the example above.

So when the project satisfy below requirements:

- 1. The anchor bolts is for No.7 or larger bottom bars.
- 2. With minimum clear cover not less than 2db and minimum clear spacing not less than 4db.
- 3. Compressive strength of the concrete is 4000 psi.

4. Deformed bar is grade 60

The development length Ld should be

 $l_d \geq 28 d_b$

where db is the bar diameter

For this project,			
Rebar size	$d_{b} =$	1.270	in
Grade of bar	Fy=	60	ksi
Usage of bar	=	1.00	
The required development length of rebars:			
ld= Fy/60*usage*db*28	=	35.56	in
Clear cover	=	3.0	in
Tie size	=	0.625	in
Anchor bolt size	=	2.250	in
Anchor bolt circle diameter	=	74.803	in
Anchor bolt template diameter	=	80.803	in
Seismic Design Category	=	В	
Min. inside bend dia. plus standard/seismic hook length (ACI 318-14 25.3.2)	=	0.000	
Min. Rebar cage diameter	=	86.073	in
Min. Caisson Diameter	=	7.883	ft
Caisson diameter used	=	8.0	ft
Clear spacing between rebar and anchor bolt	=	3.875	in
The req'd minimum anchor bolt length with 12" length protrusion	=	53.27	in
	Calcu	ulate by :	МН
	Date	:	4/30/2021

_			
	Plate Type	Flange @ 135.0 ft	Code Rev. G Date 5/19/2021
θ	Pole Diameter	23.62 in	Engineer MH
Base/Flange Plate	Pole Thickness	0.354 in	Site # CT 757
е	Plate Diameter	29.13 in	Moment 356.3 k-ft Site Name Kent
ng	Plate Thickness	1.181 in	Axial 4.4 k
Γla	Plate Fy	50 ksi	Shear 31.4 k
se	Weld Length	0.3125 in	Required Flange Thickness:
Ba	ϕ_s Resistance	29.11 k-in	0.90 in OK
	Applied	17.01 k-in	0.00 111 011
-	#	0	
		· ·	
Stiffeners			
ene			
tiff			0 0 0 0 0 0
S			
-			
	#	40	
	Bolt Circle	27.17 in	
	(R)adial / (S)quare	R	
			↓ 0
	Diameter	0.625 in	
	Hole Diameter	0.748 in	
Bolts	Туре	A325	
	Fy	92 ksi	
	Fu	120 ksi	
	ϕ_{s} Resistance	20.34 k	00000
	Applied	15.62 k	
-	#	0	
		,	
orcement			
ner			Plate Stress Ratio:
cer			0.58 (Pass)
for			(1.000)
Reinf			Bolt Stress Ratio:
œ			0.77 (Pass)
	#	0	0.11 (Fass)
	#		
_			
0			
olts			
۳ B			
Extra Bolts			
Ш			

PROJECT No:	21.03.008.007	ENG:	MH
PROJECT NAME:	CT 757 - Kent	CHK:	TFI
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TIA-222-H

SINGLE GLOBAL FOUNDATION WITH PIER(s) CHECKS - MONOPOLE

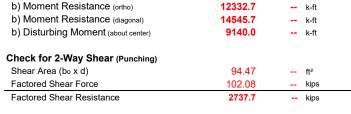
ilobal To	ower Reactions	Factored Loads		Calculated R	eactions Fa	actored Resist	ance			SF=2.23
Code Rev	Maximum Moment	8,646.00	k-ft	Disturbing Moment	9,140.0	10,188.6	k-ft	PASS	89.7%	[GOVERNS]
TIA-H	Axial Load	62.00	kips	Maximum Bearing	3.27	22.50	kips	PASS	14.5%	
	Shear Load	76.00	kips	Lateral (Sliding)	76.00	9,514.25	kips	PASS	0.8%	
				Pad Shear	521.7	1,165.1	kips	PASS	44.8%	
				Punching Shear	102.1	2,737.7	kips	PASS	3.7%	
	Pier Rebar Check	8,912.0	k-ft	Flexural Capacity		10,139.1	k-ft	PASS	87.9%	
	Pad Rebar Required	(24) # 10 @ 1	l5.91 in	Actual Pad Rebar		(28) # 10 bars	5	PASS	84.7%	

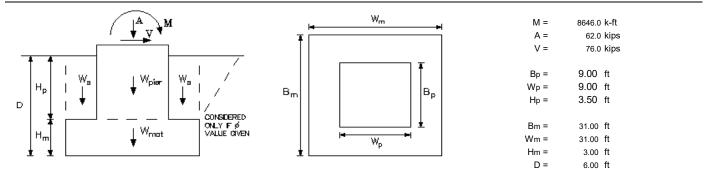
*Note: TIA-222-H Section 9.4.2 controls PASS **96.4%**

Soil Parameters	Soils Report		Pier Geometry		Pad Geome	try	
Cohesion	12000.0 psf (574.6 l	kPa)	Qty of Piers	1	Width (Bm)	31.00	ft
φ	0.0 °		Width (Bp)	9.00 ft	Width (Wm)	31.00	ft
Frost/Ignored Depth	3.30 ft (1.01 r	n)	Height (Hp)	3.50 ft	Height (Hm)	3.00	ft
Water Level	99.00 ft (30.18	m)	Pier above grade	0.50 ft	Depth (D)	6.00	ft
Soil Dry Density (γ _{drv})	0.135 kcf (21.2 k	N/m ³)	Pier Type	R (Rnd or Sq)	CofG Diff.		ft
Soil Sub Density (γ_{sub})	0.073 kcf (11.40 k	,	(use equivalent squ	are for pad flexure)			
All. Bearing Pressure	15.000 ksf (718.2 k	,	Rebar	Pier		Pad	
Bearing Safety Factor	2		Rebar Type	ASTM		ASTM	
Concrete Parameters			Cover to Tie	3.00 inches	Bar Size	10	
f'c	4.500 ksi (31.0 M	lPa)	Pier Tie Size	5	Bar Qty	28	
fy	60.00 ksi (413.7	,	Pier Vertical Size	10	Pad bar gty i	s one layer in	
Dry Density (γ _{dry})	0.150 kcf (23.6 k	N/m ³)	Pier Vertical Qty	37 0.51%		rection	
Sub Density (γ_{sub})	0.088 kcf (13.8 k	N/m ³)					
	Concrete (115.0cuyd)				TIA-H	EIA-F	
Volume of Concrete/Soil	1 Pier Mat	Soil	Calculations		Method	Method	
Depth (above)	0.50	ft	Axial Download	(factored)	62.0		kips
Depth (dry)	3.00 3.00	3.00 ft	Wgt of Concrete	(not factored)	465.8		kips
Depth (submerged)	0.00 0.00	0.00 ft	Wgt of Soil	(not factored)	363.4		kips
Volume (above)	31.81	ft ³	Total Download (P	1) (1.2D No wdg)	1057.1		kips
Volume (dry)	190.85 2,883.00	2692.15 ft ³	Total Download (Pa	2) (0.9D No wdg)	792.9	1	kips
Volume (submerged)	0.00 0	0.00 ft ³	Passive Force Mor	ment	494.0		k-ft
Total	223 2883	2692 ft ³	Bearing Capacity C	Check			
Pad Flexure			Calculate ecc e = N		8.18	'	ft
Distance (edge to pier)	11.000 ft		1) q _{max} = Ortho Dii	rection	2.33		ksf
B' = 3/2(B-2e)	11.916 ft		2) q _{max} = Diagonal	Direction	2.80		ksf
Force	<u>691.0</u> kips		Calculate ecc e = N	//P 1 (0.9D+1.6W)	10.90	'	ft
Disturbing Moment	4116.96 kip-ft		1) q _{max} = Ortho Dii	rection	2.78		ksf
Ku	137.09	Wgt of Rebar	2) q _{max} = Diagonal	Direction	3.27		ksf
ρ	0.00259	15,722 lbs	q factored		22.50		ksf
$4/3 \cdot \rho$ if $\rho < \rho$ min	0.00345				(2 • 0.75)		
ρ min ≥ 0.0018	0.00180	24 Qty	Overturning Stabil				
As Required (based on ρ)	29.963 in ²	<u>15.91</u> in c/c	 a) Resisting Mome 	()	15.5		ft
As Actual	35.560 in² φMn=	4,861 kip-ft	 a) Moment Resista 		10188.6		k-ft
		84.7%	a) Disturbing Mom	ent (about edge)	9140.0		k-ft
Note: The moment is derived from a mon	nent diagram that considers th	e ortho					
qmax trapezoidal distribution under	neath the pad to edge of squa	are pier.	 b) Moment Resista 	INCE (ortho)	12332.7	1	k-ft
			b) Moment Resista	INCE (diagonal)	14545.7	1	k-ft
			b) Disturbing Mom	ent (about center)	9140.0	1	k-ft
Check for 1-Way Shear			Check for 2-Way S	hear (Punching)			

neck for 1-way Shear	
Shear Area (b x d) =	80.41
E - stand de la seu fanse	504.00

Shear Area (b x d) =	80.41	 ft²
Factored shear force =	521.68	 kips
Factored shear resistance	1165.1	 kips





TIA-222-H Section 9.4.2 Calculations

					Two-Way S	hear (Compres	sion)				
	Pler Diameter:		d _{pier1} =	d _{pior} * 12 in / ft					d _{pier1} =	108.00	in
Equivalent	Square Pier Diarneter:		d _{pior_sq} =	√π/2*dpier					d _{piw_sq} =	95.71	in
Avg. Effective Dep	th for Punching Shear.		d _{c,2} =	T - cc _{pad} - AVE	RAGE(0.5 * @	_{مر} , 1.5 * d _{درم})			d _{ر2} =	31.73	in
Are	of Concrete in Shear.		A, =	((dpier1 + dc_	2)*PI()) * dc_2				A, =	13928.67	in ²
Eq. Square Arei	of Concrete in Shear:		A _{c.10} =	(4*(dpier_sq+	dc_2))*dc_2				A.,=	16175.00	in ²
Facto	of transfer of Moment		Y _f =	1/(1+(2/3)*√(d	pier1/dpier1))				Y _f =	0.60	
Factor of transfer of	of eccentricity of Shear:		Y., =	1-Yr					Y. =	0.40	
	applied at base of Pier.			M _{u,comp} * 12 in						106944.00	kip*in
				mu_comp 12 III					m _y –	100044.00	Ng III
			Two-V	Vay Shear (Co	mpression, Fle	exural Compone	nt) [TOP REIN	NFORCEMENT]			
	Bar Spacing:		Bs_pad_top =	(W.dir2*12 - 2	* ccpad - VLOO	KUP(IF(Rectan)	gularPadBoole	ean=TRUE,spt	B _{s_pad_top} =	13.51	in
Fraction of	Bars in Effective Width:		m_effective_top =	IF(b_pad=W.d	ir2,mptop,12*b	_pad/Bs_pad_to	p)		m_efective_top =	15.99	
Area of S	teel in Effective Width:		As_effective_top =	VLOOKUP(IF(RectangularPa	dBoolean=TRUE	E,sptop2,sptop	p),Reff\$A\$2:\$C	A _{s_efective_top} =	20.31	in*
Depth of Equival	ent Rectangular Stress Block:		a_efective_top =	A _{s_effective_top} * F	y / (0.85 * F'c *	b_ _{siab} *12)			a_stocive_top =	1.47	in
Distance fro	m Top to Nuetral Axis:		C_effective_top =	a_effective_top /β;	and				C_effective_top =	1.74	
	Effective depth:		d _{c_kop} =	T *12 - ccpad ·	1.5 * VLOOKU	P(IF(Rectangula	rPadBoolean	=TRUE,sptop2	d _{c_top} =	31.095	in
	Strain in Steel:		Es_effective_top =	0.003 * (dc_to	p - c_effective_	top) / c_effective	top		£ _{s_efective_top} =	0.05077	in/in
Flexure Stre	ngth Reduction Factor:	qfi	EX_effective_top =	IF(cs_top>=ct,	0.9,IF(Es_top<	=EC,0.65,0.65+(0	.9-0.65)*((ɛs_	top-cc)/(ct-cc))))	offex_efective_top =	0.9	
Nor	inal Flexural Strength:	1	An_effective_top =	A _{t_offective_tap} * (F _y) * (dc_top - a	efective_top / 2)* (1	/12)		M _{n_effective_top} =	3082.39	ft-kips
		-	la atacia na =	offex_effective	* Mn_effective				φM _{n_effective_top} =	2774.15	ft-kips
De	sign Flexural Strength:	Ŷ	and and the ob								
De	sign Flexural Strength: Applied Moment			Yf"Mu_comp					Yf"M _{u_comp} =	5347.2	ft-kips

8340-100 series RUGGED POWER



Founded in 1979 Polar Power specialized in solar photovoltaic systems, solar air conditioning and refrigeration. We developed and provided photovoltaic charging controls for telecommunications in the 1980s along with DC generators for the military. In 1994 we were first to provide DC generators with remote control and monitoring to the telecommunications industry.

Polar's success is based on engineering generators to meet the very specific needs of each application. Telecom site optimization is best met with the DC generator technology as the loads and batteries are DC. It makes no sense to install an AC generator and convert the output to DC. The AC generators are designed for a wide range of applications and they are not specifically produced for telecom applications so there are issues with reliability, space, and fuel efficiency.

Polar can save you considerable time and cost in permitting, installing, purchasing, and maintaining a backup generator. We reduce CAPEX and OPEX costs while improving backup reliability.

Intertek 4003706 Conforms to UL STD 2200 Certified to CSA STD C22.2 No. 100

Meets EPA Emission Regulations CA/MA Emissions Compliant

2 year standard warranty

Available Models:

• 8340-100-LP-15-03 LPG 15 kW -48 VDC



The concepts and features behind Polar's Hybrid application generator for telecommunications include:

SMALL FOOTPRINT. Polar's DC generator is considerably smaller in size than an AC generator. You can now backup sites that could not accommodate an AC generator. Smaller also means less cost for space leasing.

LOW MAINTENANCE. Due to oversized oil sump, and oil/fuel filtration system.

LOW ACOUSTIC NOISE. <62 dBA @ 7 meters for LPG, and low vibration so as not to disturb the local residents or building landlords.

LIGHTWEIGHT. Up to 1/3 the weight of a comparable AC generator.

CORROSION RESISTANT. All-aluminum enclosure with stainless hardware for low maintenance, and long service life.

FUEL EFFICIENT. Up to 85% fuel savings due to smaller engine displacement, high efficiency alternator, and variable speed operation.

RODENT RESISTANT. Small animals can quickly destroy a generator set by gnawing on wires, fuel lines, radiator hoses, etc. Cooling air inlets and outlets have perforated aluminum screens to keep small rodents and large insects out. Stainless steel wire braid is placed over fuel and radiator lines to prevent damage.

SUPERCAPACITOR STARTER. Failure to start is the number one problem plaguing generator reliability and typically this is caused by a bad starting battery. Polar unique design has replaced the starting battery with a Super Capacitor. Capacitors are more reliable and last longer than batteries (10-15 year life).

LONG LIFE. Controls and wire harnesses are designed to exceed a 20 year life. Higher grade, longer life electrical wire (UL 3173), weather tight connectors, gold plated connector pins on signal circuits. No transfer switches are required.

ADVANCED MONITORING. Remote diagnostics, control, and monitoring. Ethernet and RS232 standard, with optional SNMP.



COMPARING THE COST OF AC vs DC

	AC	DC
Transfer switch required	Yes	No
Permitting costs	\$\$	\$
Shipping to site and installation cost	\$\$	\$
Site preparation/reinforcing struc- tures	\$\$\$	\$
Ethernet/RS232 remote control and monitoring	Extra	Standard
8220 ALTERNATOR FEATURES		

• No mechanical adjustments

- Very lightweight
- High quality electrical output
- Voltage and current regulation
- Up to 94% efficiency

8220 ALTERNATOR SPECIFICATIONS

Permanent Magnets, NdFeB
46.5/21
Variable engine speed
3 phase/32 poles
350
Pull fuse block, sized for each generator kW
44 to 62
130 to 180 / 3.68 to 5.1
100,000+

ENCLOSURE

Model	88-25-0100
Туре	Weather Protective
Materials	Marine Grade Aluminum
Door Hardware	Pad Locked with Removable Side Panels
Mounting	Secure Mounting Tabs

PERMITTING IS FACILITATED

- Small engine horsepower
- DC generator is fully isolated from the utility grid
- No transfer switch
- Low acoustic noise
- Incorporates all requirements made by local Fire Marshals
- Class 220° C insulation
- Anodized type III process for aluminum parts
- Nickel plating for steel parts
- Stator is varnished

STARTER SUPERCAPACITOR SPECIFICATIONS

Model	20-16-0001
Storage Rating (Farads)	500
Voltage (VDC)	13-14.4
Weight (lb/kg)	12.1/5.5
Operating Temperature (°C/°F)	-40 to 65 / -40 to 149
Service Life (year)	10 to 15

CHARGER SPECIFICATIONS

Model	00-10-0015
Input Voltage (VDC)	28.8 to 60
Output Voltage (VDC)	14 to 14.4
Recharge time from 0 VDC (min)	10
Recharge time from 8 VDC (min)	2
Weight (lb/kg)	2.2/1

SOUND EMISSIONS

Contact us for current sound data.



SPECIFICATIONS NATURAL GAS and LPG

Engine Model	Natural Gas - Kubota DG972 LPG - Kubota WG972
Cylinders	3 In-line
Displacement (L)	0.962
Bore (in./mm)	2.93/74.5
Stroke (in./mm)	2.9/73.6
Intake Air System	Naturally Aspirated
Engine HP	18
Emissions Compliance	EPA and CARB Certified
Variable RPM	2650 to 3150

ENVIRONMENTAL

Operating Temperature (°C/°F)	-40 to 72 or -40 to 162
Operating Humidity %	100
Cold Start Aids	Glow Plugs

PROPANE ENGINE FUEL CONSUMPTION

	Output (kW)	gal/hr	L/hr
	4	0.97	3.67
	5	1.1	4.16
	6	1.26	4.77
Kubota 972	7	1.475	5.58
	8	1.69	6.4
	9	1.945	7.36
	10	2.2	8.33
	12	2.52	9.54
	15	3.55	13.44

POWER ADJUSTMENT FOR AMBIENT CONDITIONS

Temperature Deration	1% derate for every 5.6 °C (10 °F) above 25 °C (77 °F)
Altitude Deration	3% derate for every 300 m (1000 ft) above 91 m (300 ft)

WEIGHTS AND DIMENSIONS

Dry Weight (lb/kg)	680/308
Dimensions (LxWxH) (in/cm)	54 x 38 x 38/137 x 97 x 97

ENGINE LUBRICATION SYSTEM

Oil Filter Type	Full flow spin-on canister
Oil Capacity	3.7 L - DG972/WG972
Oil Pressure Switch	Yes
Oil Pressure Transducer	Optional

ENGINE COOLING SYSTEM

Туре	Pressurized Aluminum Radiator
Water Pump	Belt-driven, Pre-lubed, self-sealing
Fan Type	Electric Fans
Airflow CFM or M ³ /hr	1300 or 2200
Fan Mode	Pusher
Temperature Switch	Yes

FUEL SYSTEM

Туре	Natural Gas or Propane
Fuel Tank/Line	Supplied By Customer
Max Fuel Flow Rate (BTU/hr)	15 kW - 340,000



Pressure Chart

Minimum	Recommended	Maximum
0.14 psi	0.39 psi	0.5 psi
4 in H2O	11 in H2O	13.9 in H2O
10 mbar	27.4 mbar	34.5 mbar



ENGINE COOLING

System coolant capacity (gal/L)	2.2/8.3
Maximum operation air temperature on radiator (°C/°F)	54/129
Maximum ambient temperature (°C/°F)	49/120

COMBUSTION REQUIREMENTS

EXHAUST

Exhaust flow at rated output (cfm/cmm)	90/2.55
Exhaust temperature at rated output (°C/°F)	480/900

CONTROLLER FEATURES

Controller Type	Supra Model 250
4-Line Plain Text LCD Display Engine Run Hours Indication Programmable Start Delay Run/Alarm/Maintenance Logs	Simple user interface for ease of operation
Engine Run Hours Indication	Standard
Programmable Start Delay	Standard
Run/Alarm/Maintenance Logs	Standard
Engine Start Sequence	Cyclic cranking: 5 sec on, 45 sec rest (3 attempts maximum)
Starter Supercapacitor Charger	
Automatic Voltage Regulation with Over and Under Voltage Protection	Standard
Automatic Low Oil Pressure/High Oil Temperature Shutdown Overcrank/Overspeed	Standard
Overcrank/Overspeed	Standard
Automatic High Engine Temperature Shutdown Field Upgradeable Firmware Glow Plug Delay	Standard
Field Upgradeable Firmware	Standard
Glow Plug Delay	Automatic With Temperature
Engine Start Delay	Adjustable, Set at 60 sec
Return to Utility Delay	Adjustable, Set at 60 sec
Engine Cooldown	Adjustable, Set at 60 sec
Return to Utility Delay Engine Cooldown Exerciser	Programmable, weekly/bi-weekly

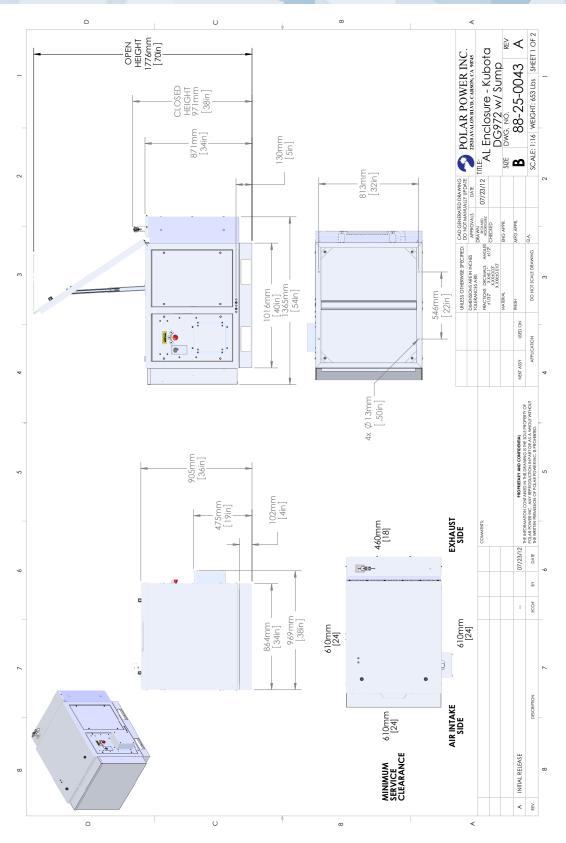
WARNING ALARMS

Low/High Supercapacitor Voltage	Standard
High Water Temperature	Standard
Low Oil Pressure	Standard

CONTACT CLOSURE FOR REMOTE INDICATION (PN 84-12-0640)

Shutdown Alarm	Optional
Warning Alarm	Optional
Engine Run	Optional
E-Stop Depressed	Optional









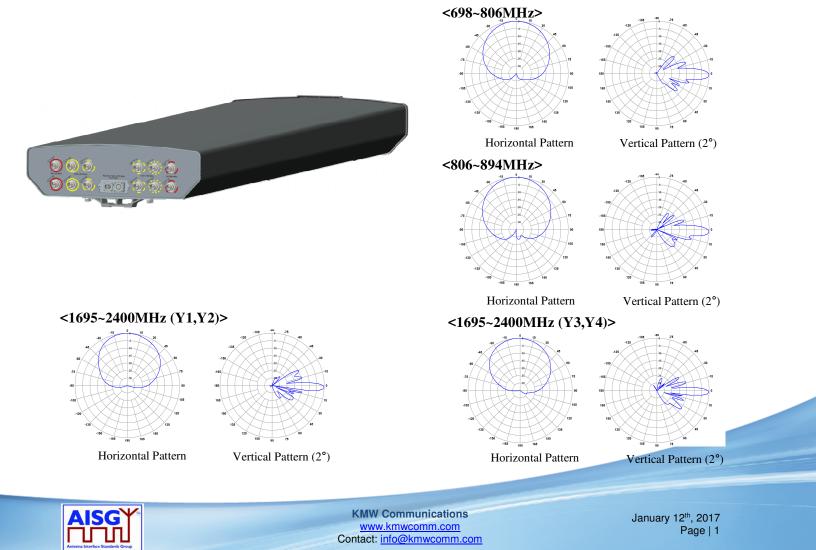
EPBQ-654L8H8-L2

12-Port Multi-Band Antenna / 8' / 65°

698 ~ 894MHz, XX-pol., H67° / V9.3°, ET:2~12° 1695 ~ 2400MHz, XXXX-pol., H61° / V8.1°, ET: 2~12°

Electrical Specification

Frequency(MHz)		698~806	806~894	1695~1850	1850~1910	1910~2180	2300~2400
Impedance(Ω)		50	50	50	50	50	50
Polarization		±45°	±45°	±45°	±45°	±45°	±45°
Gain(dBi)		15.9	16.2	16.9	17.3	17.7	17.8
Beam width—	Horizontal	67°	66°	61°	60°	60°	60°
	Vertical	9.3°	8.7°	8.1°	7.8°	7.4°	6.8°
VSWR		≤1.5:1	≤1.5:1	≤1.5:1	≤1.5:1	≤1.5:1	≤1.5:1
Front-to-Back Ratio(dB)		>25	>25	>25	>25	>25	>25
Electrical Down tilt		2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°	2° ~ 12°
Isolation Ports	s(dB)	≥25	≥25	≥25	≥25	≥25	≥25
Isolation Frequency(dB)		≥30	≥30	≥30	≥30	≥30	≥30
Cross Pole Discrimination		7 dB @ ±60°					
		15.0 dB @ 0°					
Side Lobe Suppression		> 16dB					
(Up to 10° from Boresight)							
PIM (2x20w, dBc)		≤ -150	≤ -150	≤ -150	≤ -150	≤ -150	≤ -150
Input Power(W)		400	400	300	300	300	300



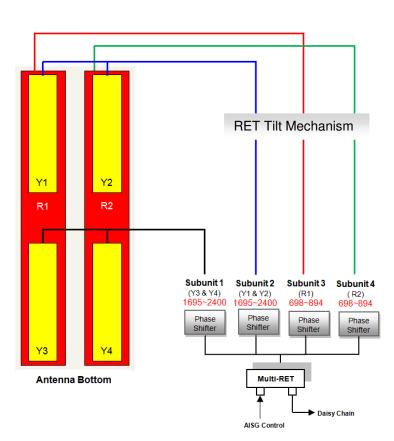




EPBQ-654L8H8-L2

12-Port Multi-Band Antenna / 8' / 65°

698 ~ 894MHz, XX-pol., H67° / V9.3°, ET:2~12° 1695 ~ 2400MHz, XXXX-pol., H61° / V8.1°, ET: 2~12°



Mechanical Specification

Dimension (W×D×H)	21.0×6.3×96.0 inches (533×160×2438 mm)	
Weight (Without clamp)	86.0lbs (39.0kg)	
Connector	12 x 4.3-10 (Female), Long Neck (4 x 698-894 8 x 1695-2400MHz)	
Max Wind Speed	150 mph	
WindLoad (@100 mph)	1994N, 598N, 1994N (Front , Side , Rear)	



Correlation Table

Frequency range	Array	Connector
698-894 MHz	R1	4.3-10 Female
698-894 MHz	R2	4.3-10 Female
1695-2400 MHz	Y1	4.3-10 Female
1695-2400 MHz	Y2	4.3-10 Female
1695-2400 MHz	Y3	4.3-10 Female
1695-2400 MHz	Y4	4.3-10 Female

*Note

- Gain can vary and the values stated are typical
- Environmental Compliance: IP 65 for Radome & IP 67 for Connectors
- RET Motor Configuration: Field Replaceable RET Electronic Control Module RET Motor is internal to antenna & not field replaceable
- Compliant with AISG: AISG2.0
- Accessory: Standard Mounting Kit is included (Mechanical Down Tilt, KCLDM1B30000 is sold separately)



KMW Communications www.kmwcomm.com Contact: info@kmwcomm.com



RRUS 4449 B5, B12 DATA SHEET

For Turf Vendors

2018-10-18 Rev B

RRUS 4449 B5, B12



> B5, B12

- B5 TX = 869 894 MHz, B12 TX = 729 746 MHz
- B5 RX = 824 849 MHz, B12 RX = 699 716 MHz

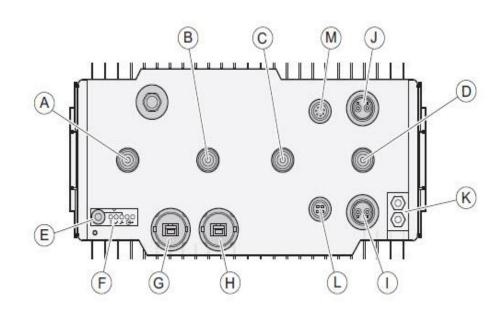
Both frequency bands are combined to transmit/receive out the same RF connectors.

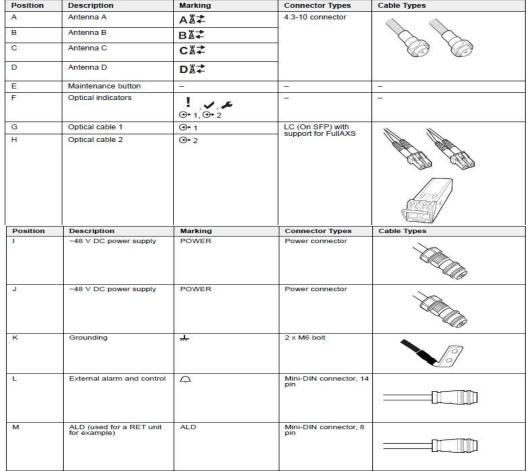
- CPRI 2 ports x 2.5/4.9/9.8/10.1 Gbps. Install 2 SFP7s and connect 2 fiber pair to the RRUS 4449 during initial install. 2nd CPRI is reserved for 5G NR deployment later. Do not connect SFP7 to DUL20.
- > Only use Ericsson supplied and approved SFP7s RDH10265/25.
 - Install 2 SFP RDH 10265/3 for CPRI length 1.4 km 10 km
 - Install SFP7 (pair): RDH 102 70/1 and RDH 102 70/2 (bi-directional SFP7 for CPRI length > 10 km
- > 2 external alarm inputs
- > Max wind load @ 50m/sec = 260 N
- Breaker size = 2x25A, DC Power Consumption = 1440 W (for dimensioning). Both power connections must be connected and operational for the radio to operate. Each power feed must support 900W.
- > 40mm horizontal separation required for side by side mounting
- > 200mm separation required from antenna backplane to radio
- > 400mm vertical outdoor/indoor separation required between 2 radios
- > 500mm vertical separation below antenna
- > Min, Max DC cable size from squid to radio = 10,8 AWG
 - Adapter is required for 2-wire connection
 - Shielded DC cable is required
- > Ground cable size = 2AWG
- > Dimensions (incl. handles, feet and sunshield, w/o fan unit)
 - Height: 17.9" (455 mm)
 - Width: 13.19" (335 mm)
 - Depth: 9.44" (240 mm)
- > Weight, excl. mounting hardware = 71 lbs (32 kg)



RRUS 4449 B5,12 CONNECTION INTERFACES



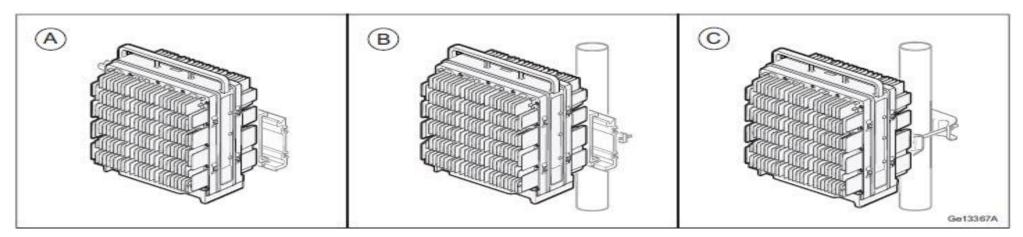




CPRI, RET/AISG port, and ALD port caps have lanyards attached to the radio. DC and RF ports have protective caps to be removed when DC, RF connected to radio.

RRUS 4449 MOUNTING OPTIONS





Installation Method	Description Wall installation	
A		
В	Pole installation	
С	Pole installation with single pole clamp	



ERICSSON



RRUS 4478 B14 DATA SHEET

For Turf Vendors

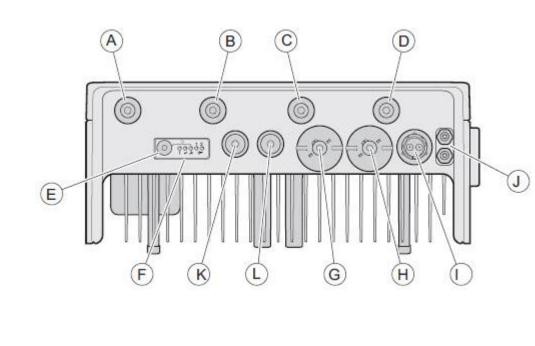
2017-11-01 Rev F

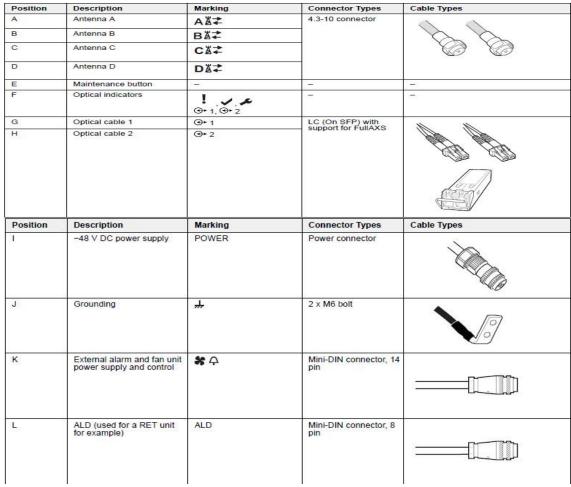
RRUS 4478 B14

- > B14
 - TX = 758 768 MHz
 - RX = 788 798 MHz
- CPRI 2 ports x 2.5/4.9/9.8/10.1 Gbps. Install 1 SFP and connect 1 fiber pair to the RRUS 4478 during initial install.
- Only use Ericsson supplied and approved SFPs RDH10265/25 until 12/1/2017, after use RDH10247/25
- > 2 external alarm inputs
- > Max wind load @ 50m/sec = 260N
- > Breaker size = 25A, DC Power Consumption = 650W (for dimensioning)
- > 200mm horizontal separation required for side by side mounting
- > 200mm separation required from antenna backplane to radio
- > 500mm/800mm vertical outdoor/indoor separation required
- > Min, Max DC cable size from squid to radio = 10,8 AWG
 - Adapter is required for 2-wire connection
 - Shielded DC cable is required
- > Ground cable size = 2AWG
- > Dimensions (incl. handles, feet and fan unit)
 - Height: 18.1" (460 mm)
 - Width: 13.4" (342 mm)
 - Depth: 8.26" (210 mm)
- > Weight, excl. mounting hardware = 59.4 lbs (27 kg)



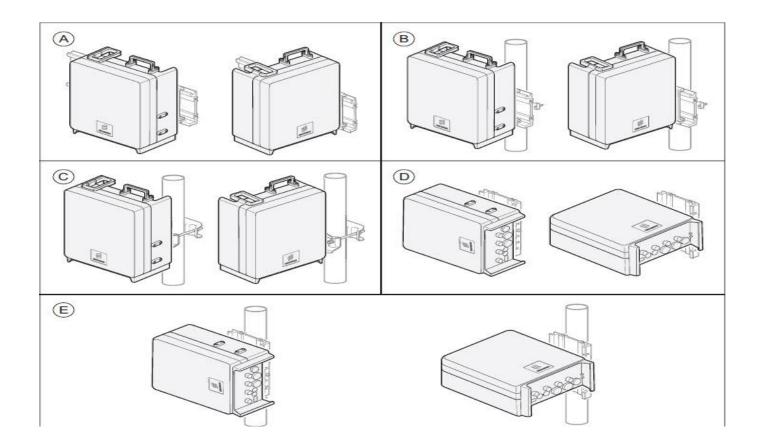
RRUS 4478 B14 CONNECTIONINTERFACESNTERFACESNTERFACES





CPRI, RET/AISG port, and ALD port caps have lanyards attached to the radio. DC and RF ports have protective caps to be removed when DC, RF connected to radio.

RRUS 4478 B14 MOUNTING OPTIONS





ERICSSON



RRUS 4415 B30 DATA SHEET

For Turf Vendors

2019-10-03 Rev C

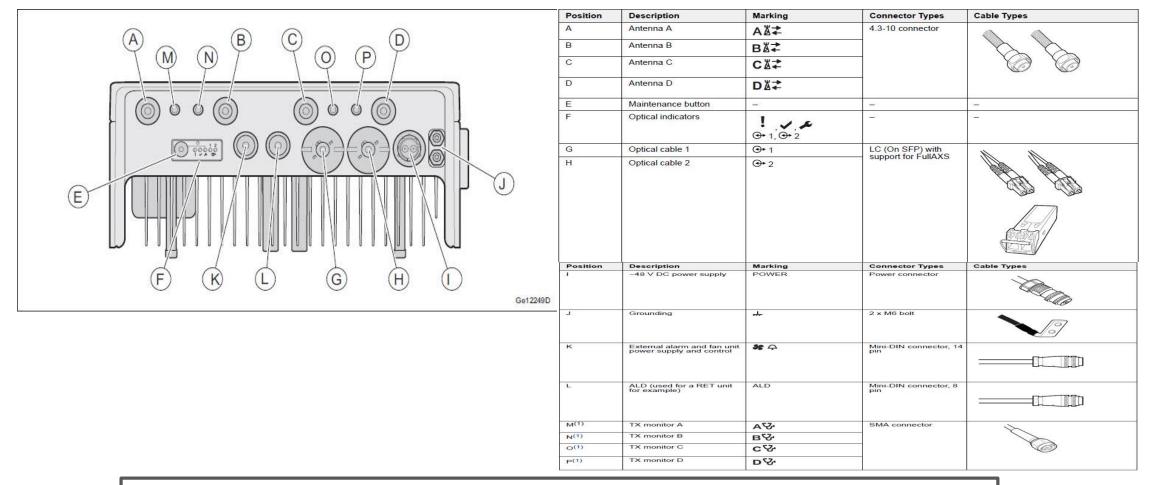
RRUS 4415 B30

- > B30 A+ B
 - TX = 2350 2360 MHz
 - RX = 2305 2315 MHz
- CPRI 2 ports x 2.5/4.9/9.8/10.1 Gbps. Install 2 SFPs and connect 2 fiber pair to the RRUS 4415 during initial install.
- Only use Ericsson supplied and approved SFP3 RDH10247/25
 Exception: SFP7 RDH 10265/3 for CPRI 1.4km to 10km
 - Exception: SFP7 (pair): RDH 102 70/1 and RDH 102 70/2 for CPRI > 10km
- > 2 external alarm inputs
- > Max wind load @ 50m/sec = 260N
- > Breaker size = 25A, DC Power Consumption = 670 W (for dimensioning)
- > 200mm horizontal minimum separation required for side by side mounting
- > 200mm separation minimum required from antenna backplane to radio
- > 400mm vertical minimum outdoor/indoor separation required between 2 radios
- > 500mm vertical separation below antenna
- > Min, Max DC cable size from squid to radio = 10,8 AWG
 - Adapter is required for 2-wire connection
 - Shielded DC cable is required
- > Ground cable size = 2AWG
- > Dimensions (incl. handles, feet and sunshield, w/o fan unit)
 - Height:16.5" (420 mm)
 - Width: 13.4" (342 mm)
 - Depth: 5.9" (123 mm)
- > Weight, excl. mounting hardware = 47.4 lbs (21.5 kg)



RRUS 4415 B30 CONNECTION INTERFACES

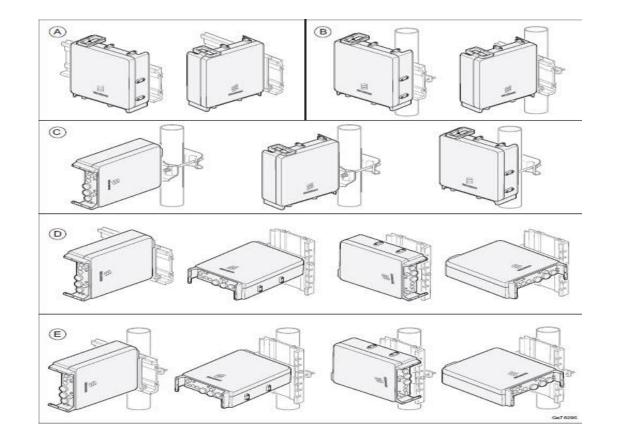




CPRI, RET/AISG port, and ALD port caps have lanyards attached to the radio. DC and RF ports have protective caps to be removed when DC, RF connected to radio.

RRUS 4415 MOUNTING OPTIONS





RRUS 32 Datasheet for Turf Vendors | Commercial in confidence | Rev A | 2016-01-21 | Page 4



ERICSSON

DATA SHEET

DC Surge Protection Solutions DC9-48-60-24-8C-EV Overvoltage Protection and Fiber Distribution/Cable Management Solution

Rooftop / Towertop

The DC9-48-60-24-8C-EV is designed to provide the ultimate coordination between the SPD and the RRH/RRU by offering industry-leading low-clamping voltage of 160V and extremely robust protection for use in a high DC voltage environment. Capable of providing 12.5kA (10/350 µs) max per circuit surge capacity for up to 9 -48V DC circuits.





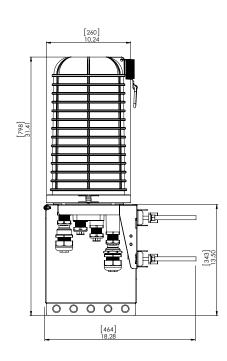
Features

- Provides discrete protection for nine individual -48V DC circuits
- Maximum impulse current 12.5kA 10/350 µs
- Fiber connections for up to 24 fiber pair
- · Simplifies inter-connectivity and cable management for DC conductors
- UL 1449 4th Edition Type 2 protective device for DC applications
- IEC 61643-11 Class I protection
- · Copper-coated lid to reduce power line interference
- Patented design
- Patented Strikesorb technology ensures lowest let-through voltage available in the industry, providing enhanced coordination with the RRH/RRU
- Raycap recommends that DC protection system be installed within 5 meters of the radio

Benefits

- Strikesorb modules are fully recognized to UL 1449 4th Edition, and IEC 61643-11 Safety Standards, meeting all intermediate and high current fault requirements to facilitate use in original equipment manufacturers (OEM) applications
- · Strikesorb offers unique maintenance-free protection against direct lightning currents
- Design provides maximum flexibility for installation
- NEMA 4X enclosure

Strikesorb is a registered trademark of Raycap © 2019 Raycap All rights reserved. G02-01-515 190212





www.raycap.com

DC Surge Protection Solutions **DC9-48-60-24-8C-EV**

Overvoltage Protection and Fiber Distribution/Cable Management Solution

powered by Strikesorb[®]

Electrical			
Model Number	DC9-48-60-24-8C-EV		
CEQ / ANT Number	CEQ.21427		
Number of Circuits Protected	9		
Surge Protective Device (SPD) Type per UL 1449 4th Edition	Туре 2		
Surge Protection Class as per IEC 61643-11	Class I		
Nominal Operating DC Voltage [U _n]	-48 VDC		
Nominal Discharge Current [In] per UL 1449 4th Edition	20 kA 8/20 µs		
Maximum Impulse (Lightning) Current [I _{imp}] per IEC 61643-11	12.5 kA 10/350 µs		
Maximum Continuous Operating DC Voltage $[U_c]$ (MCOV)	60 VDC		
Voltage Protection Level $[U_p]$ at 12.5kA per IEC 61643-11	160 V		
Voltage Protection Level $[U_p]$ at 5kA per IEC 61643-11	145 V		
Voltage Protection Rating (VPR) per UL 1449 4th Edition	330 V		
Suppression Technology	MOV		
Strikesorb Module Type 2CA (UL 1449 4th edition)	30-V1-2CEV		
Protection Modes: Normal Mode	-48V to Return		
Common Mode	Return to Ground		
Mechanical			
Connection Terminal (Suppression) Method (for all power cables)	Compression lug 2 hole, #10, 5/8 pitch, #12 – #4 AWG [3.3 – 21.15 mm ²]		
Connection Terminal (Terminal Block) Method Copper	#12 to #4 AWG [3.3 – 21.15 mm ²]		
Fiber Connection Method	LC-LC Single Mode		
Environmental Ingress Protection (IP) Rating	IP 68		
Operating Temperature (°C)	-40° C to +100° C		
Storage Temperature (°C)	-70° C to +80° C		
Cold Temperature Cycling IEC 61300-2-22	-30° C to +60° C 200 hrs @5 PSI		
Resistance to Aggressive Materials CEI IEC 61073-2	Including Acids and Bases		
UV Protection ISO 4892-2 Method A	Xenon-Arc 2160 hrs		
Enclosure Type	Outdoor NEMA 4X		
Enclosure Dimensions (LxWxH)	18.28"×10.24"×31.4" [464×260×797 mm]		
Weight*	System: 18.5 lbs [8.39 kg] Mount: 10.2 lbs [4.62 kg] Total: 28.7 lbs [13.02 kg]		
Combined Wind Loading Sustained Gust	150 mph Sustained: 105.7 lbs [470 N] 195 mph Gust: 213.6 lbs [950 N]		
Optional Kits Available			
Trunk Gland Kit A CEQ.21428	Oval Gasket for 4AWG and 6AWG Trunk		
Trunk Gland Kit B CEQ.21429	Oval Gasket for (2) 4AWG Trunks		
Trunk Gland Kit C CEQ.21434	Oval Gasket for (2) 8AWG Trunks		
Standards Compliance & Certifications			
NEBS certified to: GR-63-CORE Issue 4, GR-1089-CORE Issue	6, GR-3108-CORE Issue 3, GR-487-CORE Issue 4, ATT-TP-76200 Issue 18		
Strikesorb modules are compliant to the following Surge Protection Device Standards:			

b modules are compliant to the following Surge Protection Device Standards: Standards: UL 1449 4th Edition: 2011, IEC 61643-11: 2011, EN 61643-11: 2012,

IEEE C62.11: 2005, IEEE C62.41: 2002, IEEE C62.45: 2002, NEMA-LS-1

Certifications: UL, VDE, CE

AWG=American Wire Gauge

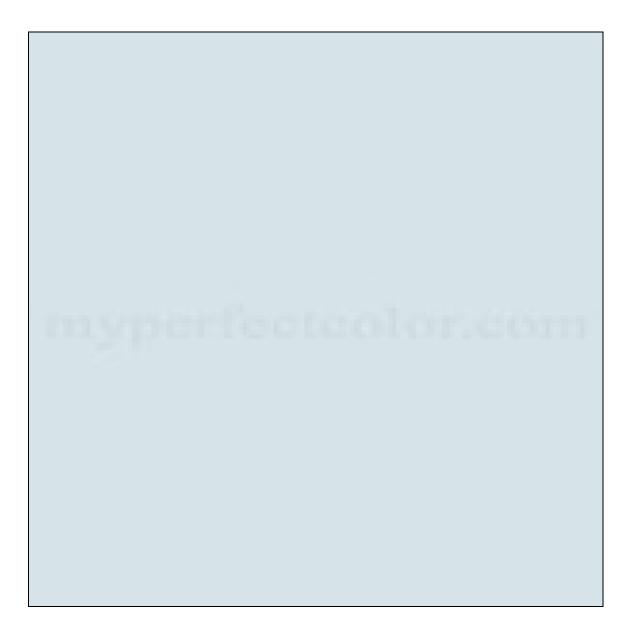


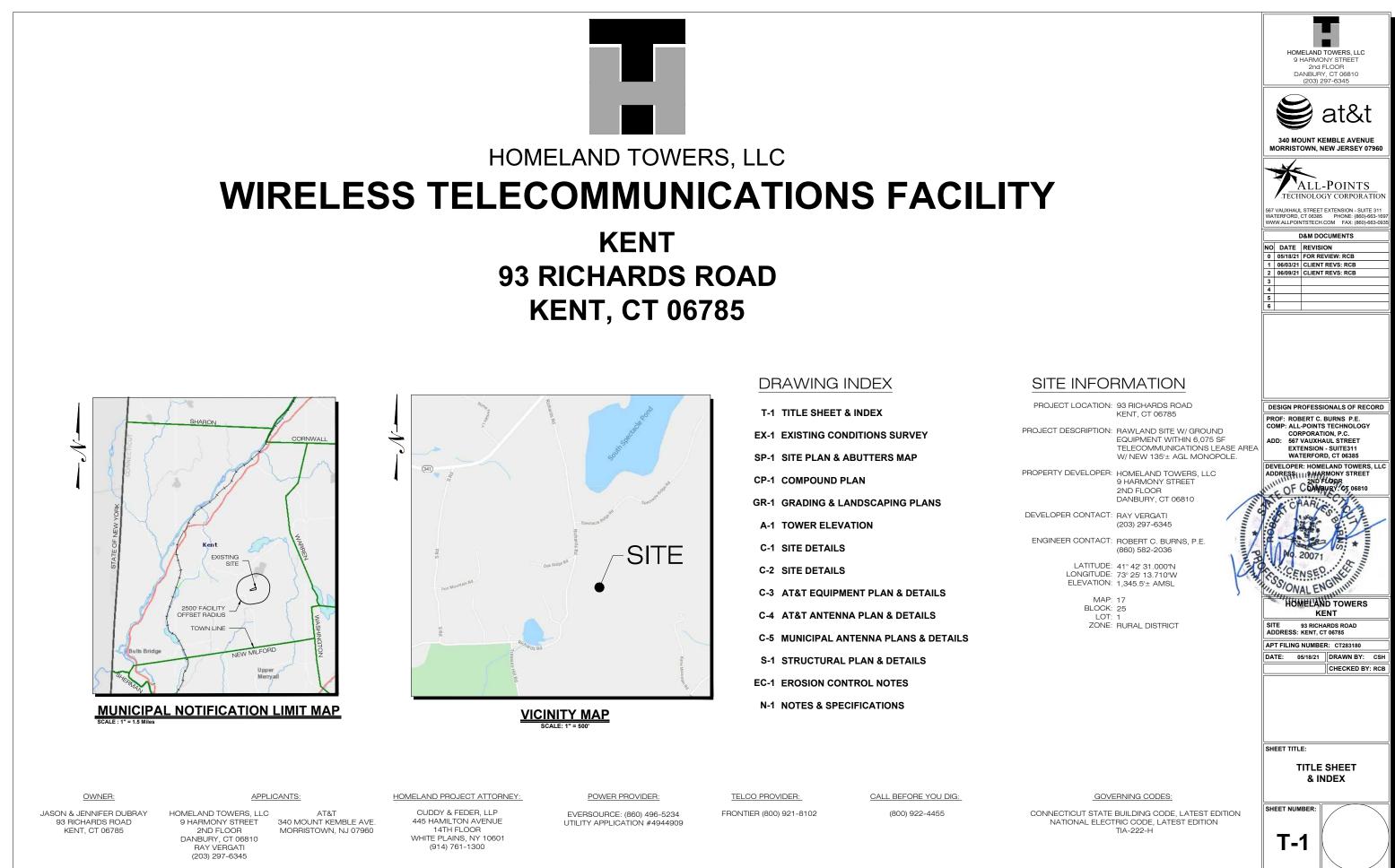


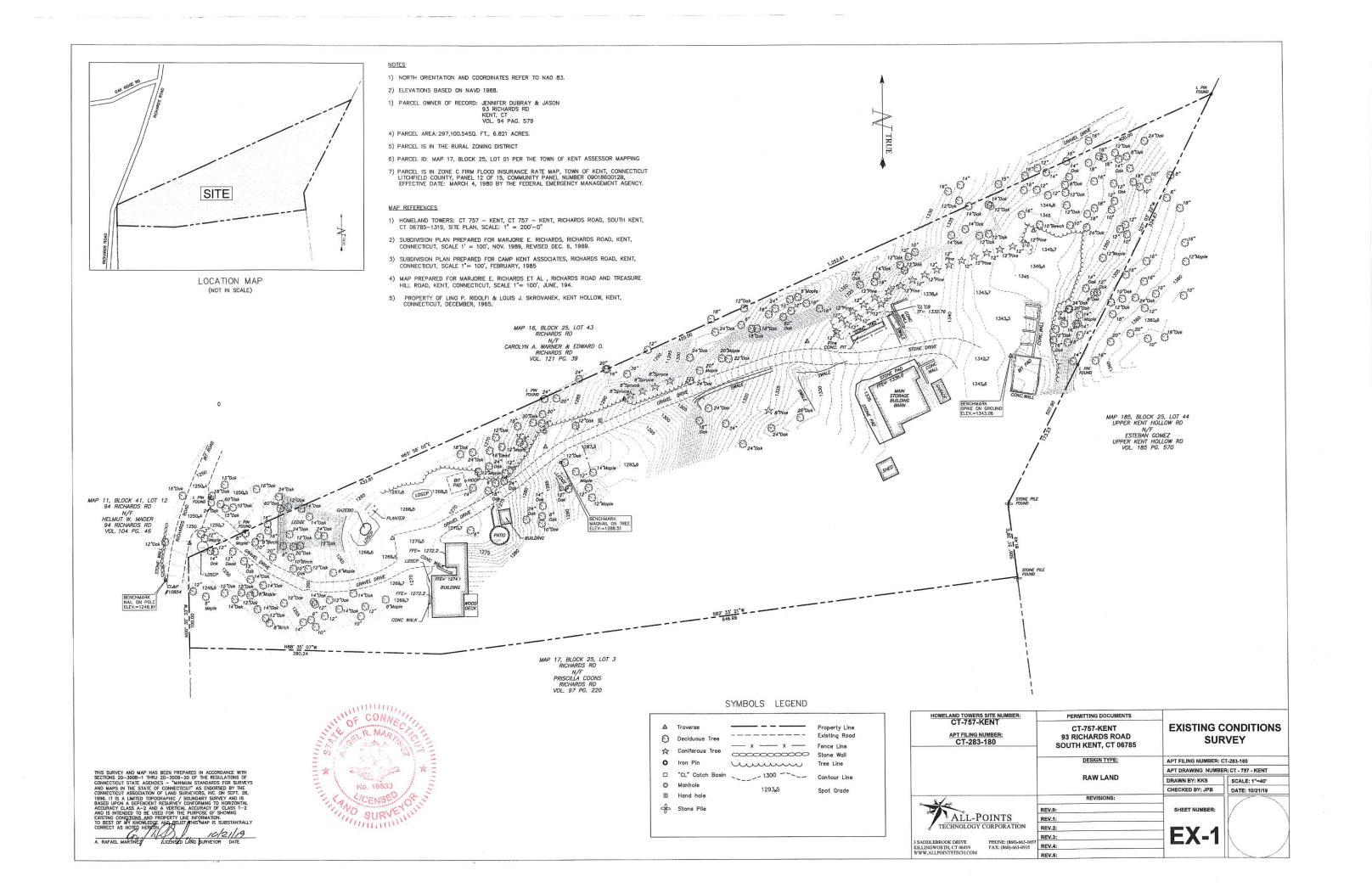


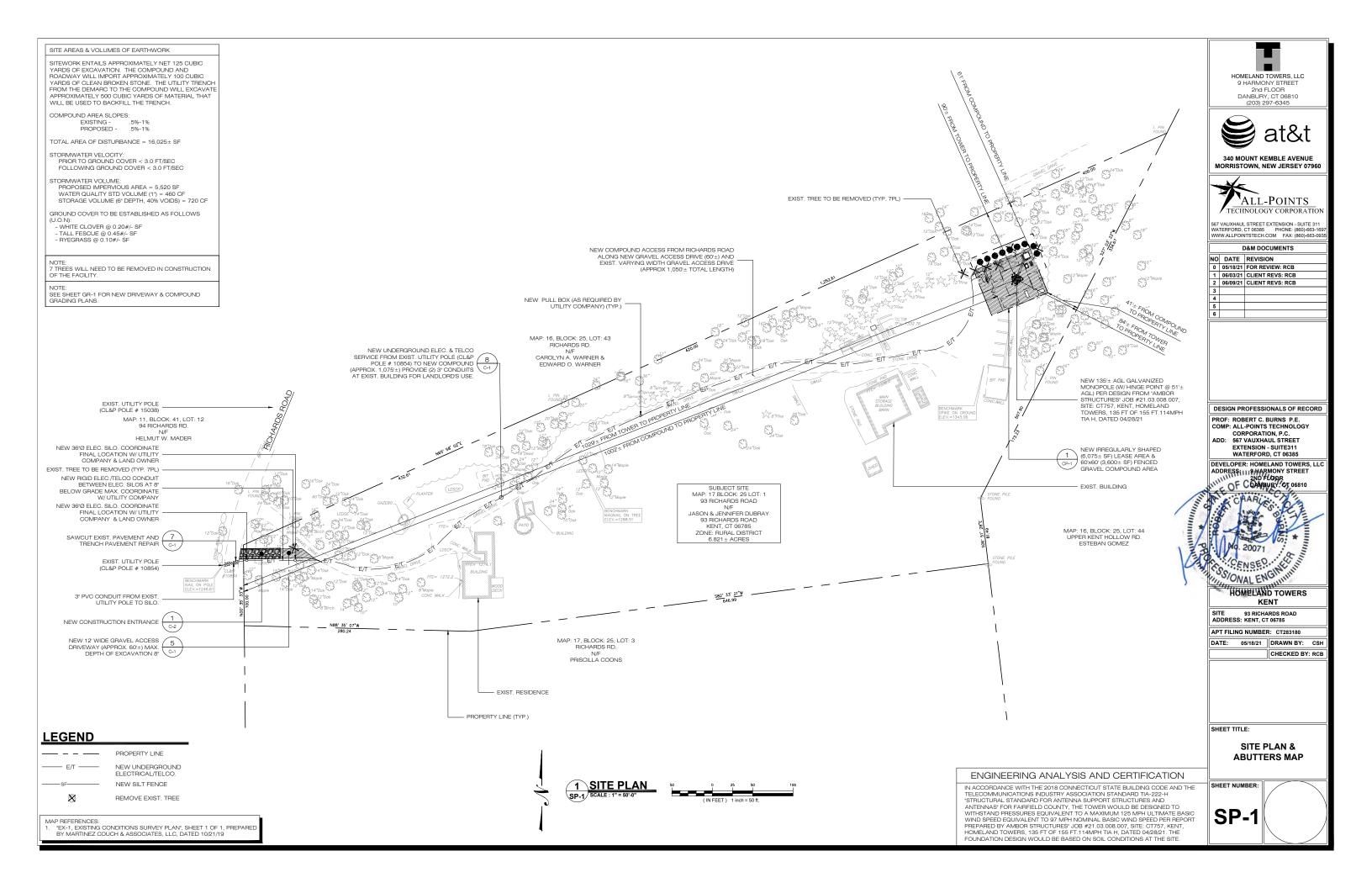
Match of Pratt and Lambert™ 2257 Shadow Beige *

PL1201 – White S	Color Name: White Smoke Color Number: 26-02	RGB Value: R: 218 G: 229
	Color Collection (s): Clean Colors	B: 235
myperfecteolor.com	Color Information: Pratt & Lambert (1201)	Hex Value: dae5eb





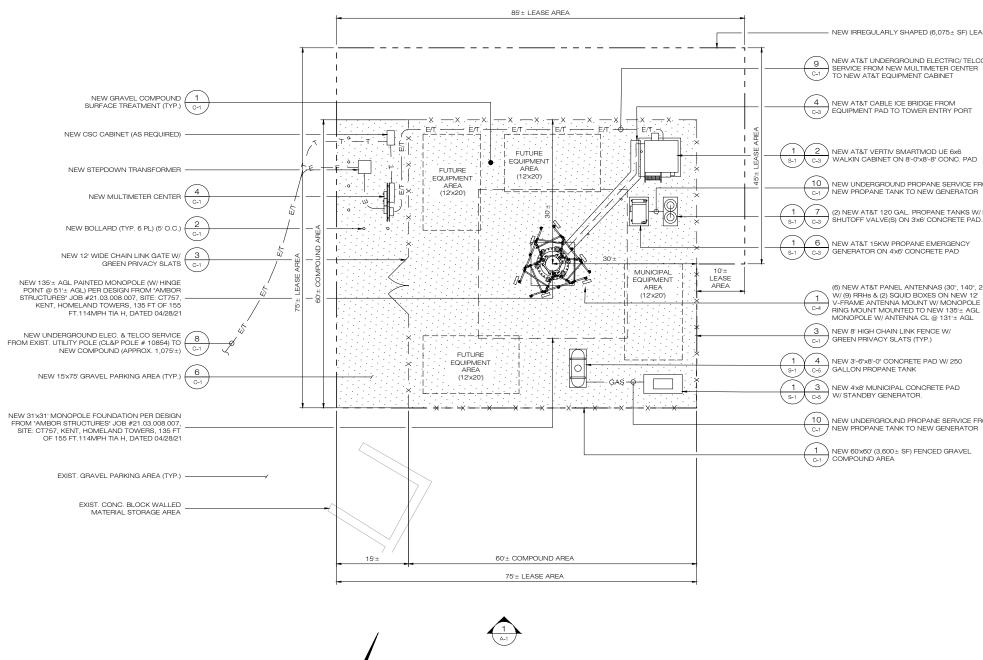






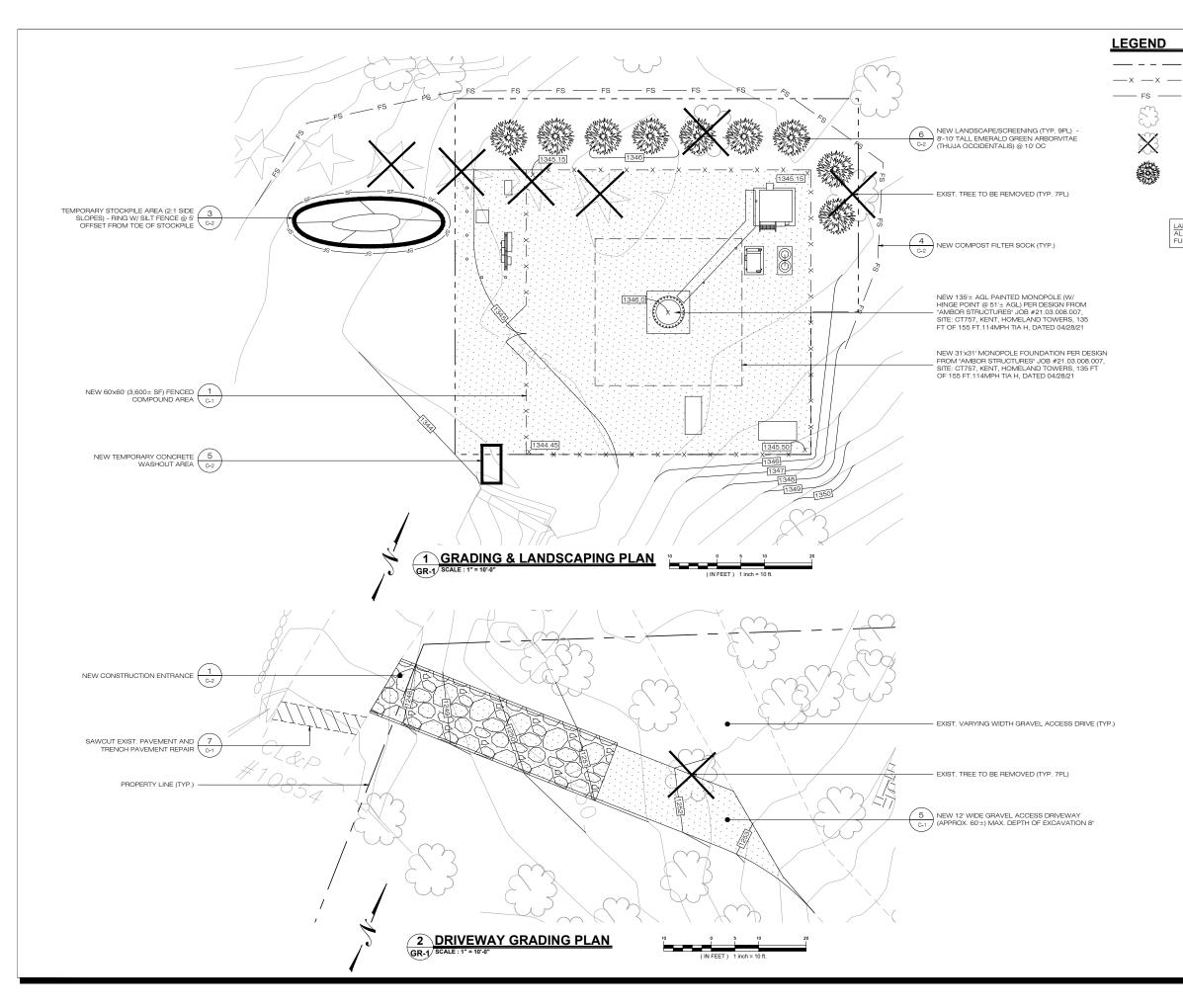
_____ —x —x —x —

TOWER PAINTING NOTE: LOWER PORTION OF TOWER TO BE PAINTED A BROWN-GRAY COLOR AND THE UPPER PORTION A GRAY-BLUE COLOR.



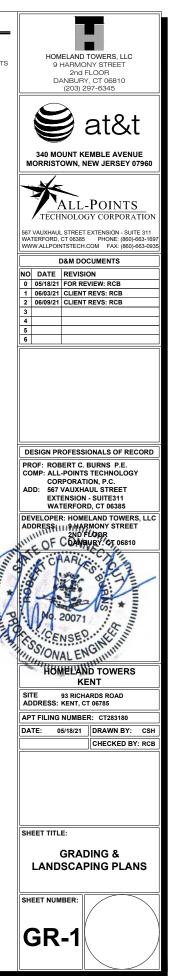
1 CP-1 SCALE : 1" = 10-0"

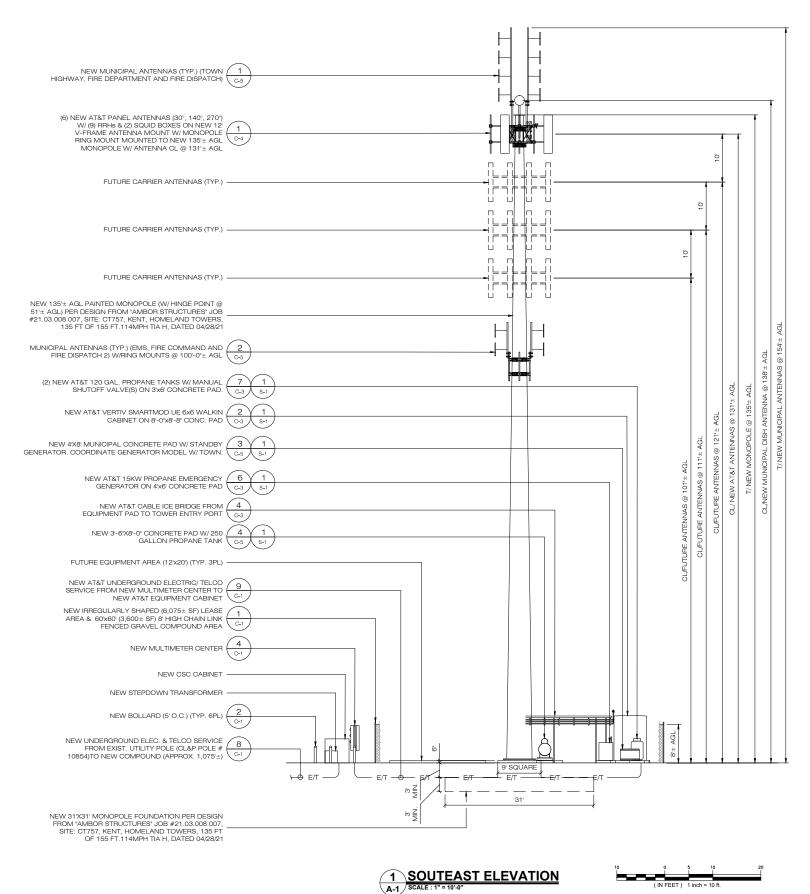
SQUIPMENT CABINET SQUIPMENT SQUIPMENT CABINET SQUIPMENT SQUIPMENT SQUIPMENT SQUIPMENT SQUIPMENT SQUIPM	LEGEND		
		NEW LEASE LINE	9 HARMONY STREET 2nd FLOOR
	— GAS — GAS —		😂 at&t
NEW MALLINETER CENTER ULIVERING CENTER LE ICE BRIDDE FROM 3 TO TOWER BUTTY PORT ILE ICE BRIDDE FROM 3 TO TOWER BUTTY PORT IN SAMPTWOOLE LEM ET ON S-098-9° CONC. PAD OUN S-099-9° CONC. PAD O		REA	
3 10 TOWER EVERY FORT NO DATE NO NO PROFESSIONALS OF RECORD NO NO PROFESS	NEW MULTIMETER CENTER		WATERFORD, CT 06385 PHONE: (860)-663-1697
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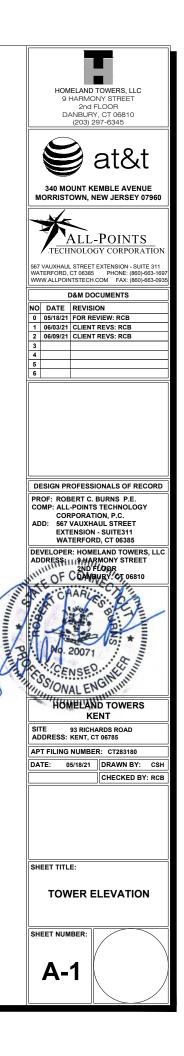
PROPERTY LINE 8' HIGH CHAIN LINK FENCE W/ GREEN PRIVACY SLATS FILTER SOCK EXIST. TREE TO REMAIN EXIST. TREE TO BE REMOVED NEW 8'-10' TALL EMERALD GREEN ARBORVITAE

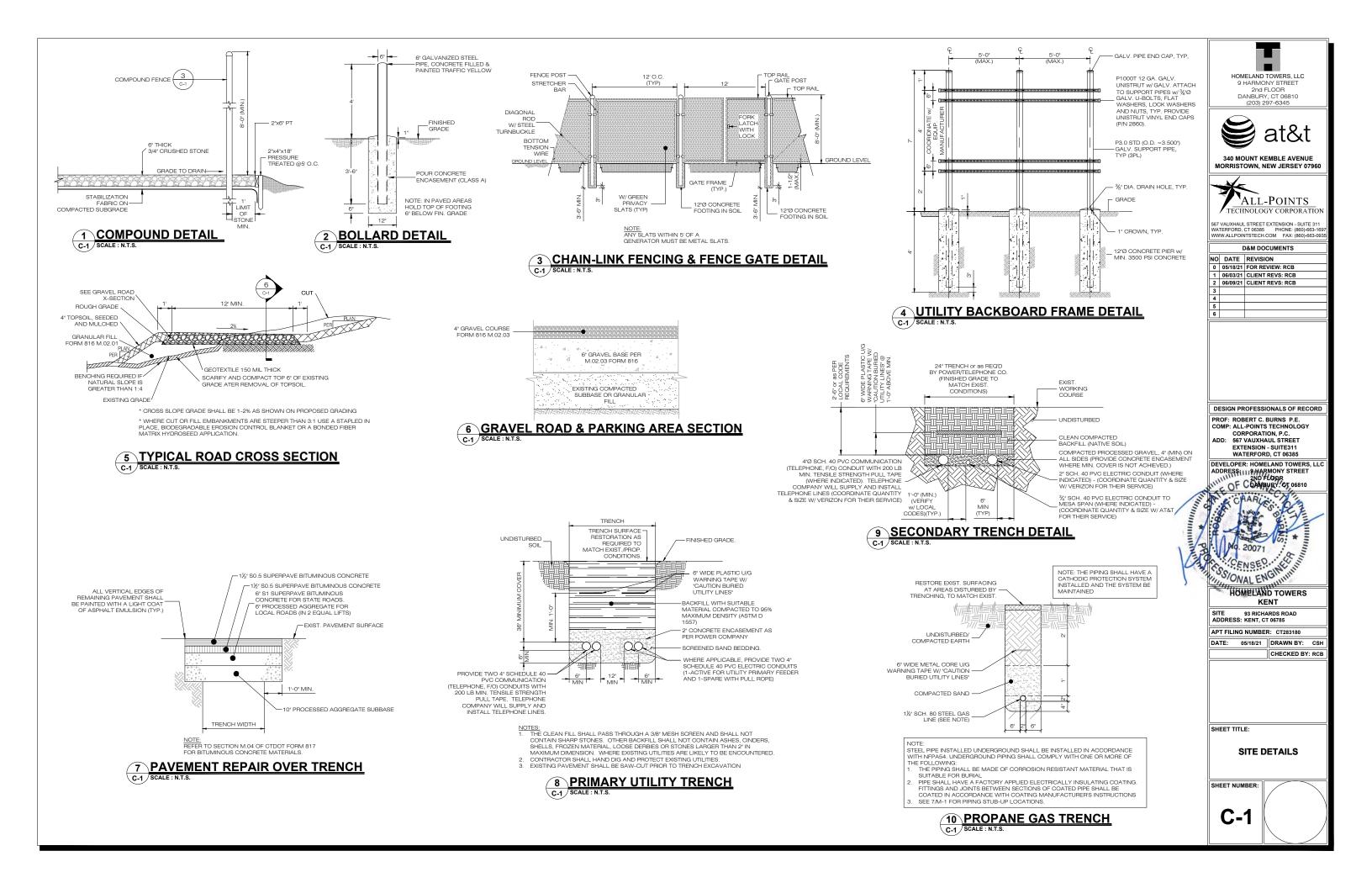
LANDSCAPE NOTE: ALL NEW LANDSCAPING WILL BE FULLY WARRANTED FOR 3 YEARS

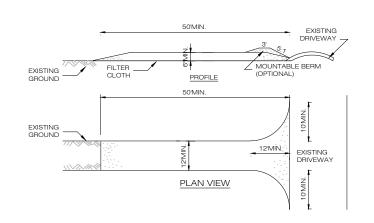




TOWER PAINTING NOTE: LOWER PORTION OF TOWER TO BE PAINTED A BROWN-GRAY COLOR AND THE UPPER PORTION A GRAY-BLUE COLOR.

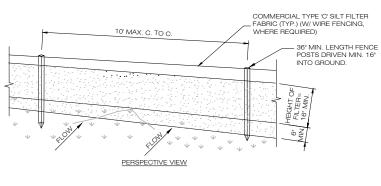


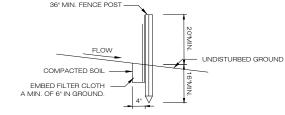




- CONSTRUCTION SPECIFICATIONS: 1. STONE SIZE USE 1-4 INCH STONE, OR RECLAIMED OR RECYCLED CONCRETE EQUIVALENT
- 2. LENGTH NOT LESS THAN 50 FEET (EXCEPT ON A SINGLE RESIDENCE LOT WHERE A 30 FOOT MINIMUM LENGTH WOULD APPLY).
- 3. THICKNESS NOT LESS THAN SIX (6) INCHES.
- 4. WIDTH TWELVE (12) FOOT MINIMUM, BUT NOT LESS THAN THE FULL WIDTH AT POINTS WHERE INGRESS OR EGRESS OCCURS. TWENTY-FOUR (24) FOOT IF SINGLE ENTRANCE TO SITE.
- 5. GEOTEXTILE WILL BE PLACED OVER THE ENTIRE AREA PRIOR TO PLACING OF STONE.
- 6. SURFACE WATER ALL SURFACE WATER FLOWING OR DIVERTED TOWARD CONSTRUCTION ACCESS SHALL BE PIPED BENEATH THE ENTRANCE. IF PIPING IS IMPRACTICAL, A MOUNTABLE BERM WITH 5:1 SLOPES WILL BE PERMITTED.
- 7 MAINTENANCE THE ENTRANCE SHALL BE MAINTAINED IN A CONDITION WHICH WILL PREVENT TRACKING OR FLOWING OF SEDIMENT ONTO PUBLIC RIGHTS-OF-WAY, ALL SEDIMENT SPILLED, DROPPED, WASHED OR TRACKED ONTO PUBLIC RIGHTS-OF-WAY MUST BE REMOVED IMMEDIATELY.
- 8. WHEN WASHING IS REQUIRED, IT SHALL BE DONE ON A AREA STABILIZED WITH STONE AND WHICH DRAINS INTO AN APPROVED SEDIMENT TRAPPING DEVICE.
- 9. PERIODIC INSPECTION AND NEEDED MAINTENANCE SHALL BE PROVIDED AFTER EACH RAIN.



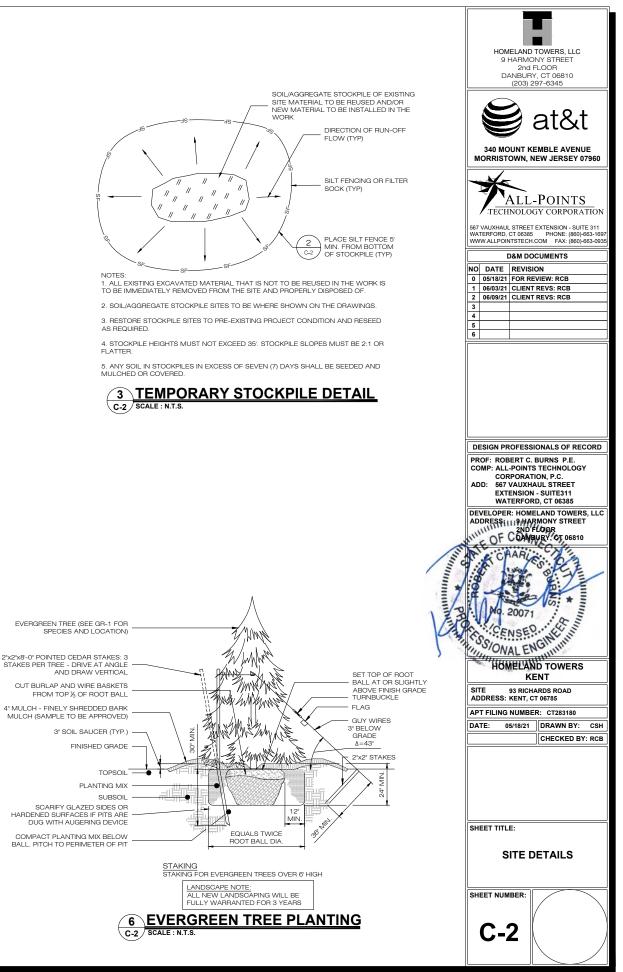


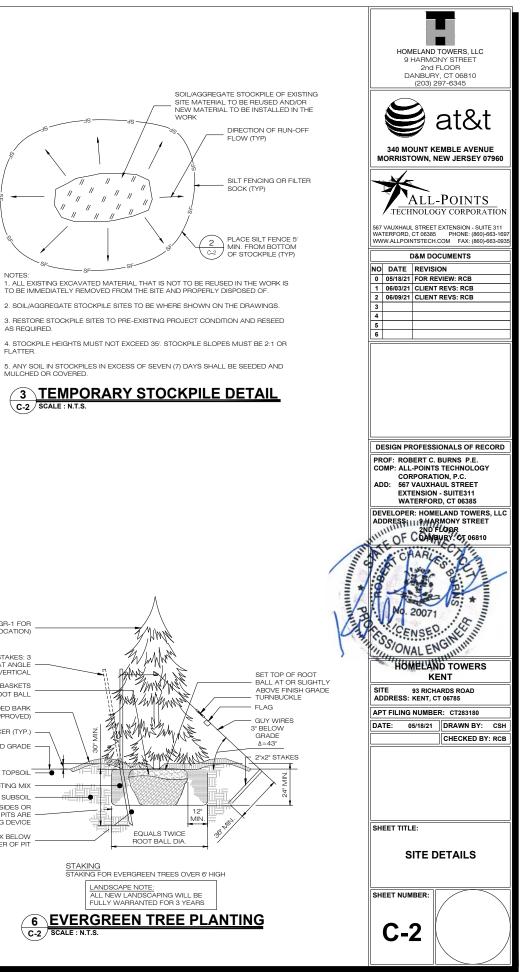


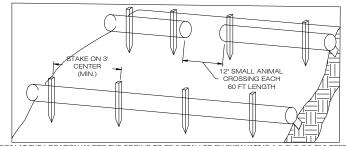
SECTION VIEW

- CONSTRUCTION SPECIFICATIONS 1. POSTS SHALL BE STEEL EITHER "T" OR "U" TYPE OR HARDWOOD.
- 2 WHEN TWO SECTIONS OF FILTER CLOTH ADJOIN EACH OTHER THEY WHEN TWO SECTIONS OF PILLER OLD IT A DUDINE AND FOR THE THE T SHALL BE OVERLAPPED BY SIX INCHES AND FOLDED. FILLER CLOTH SHALL BE EITHER FILTER X, MIRAFI 100X, STABILINKA T140N, OR APPROVED EQUIVALENT.
- 3. PREFABRICATED UNITS SHALL BE GEOFAB, ENVIROFENCE, OR APPROVED EQUIVALENT
- 4. MAINTENANCE SHALL BE PERFORMED AS NEEDED AND MATERIAL REMOVED WHEN "BULGES" DEVELOP IN THE SILT FENCE.





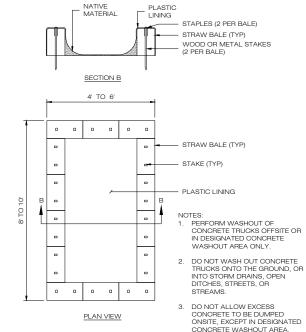


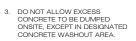


1. BEGIN AT THE LOCATION WHERE THE SOCK IS TO BE INSTALLED BY EXCAVATING A 2-3 (6-7 5 CM) DEEP X 9' (22.9 CM) WIDE TRENCH ALONG THE CONTOUR OF THE SLOPE. EXCAVATED SOIL SHOULD BE PLACED UP SLOPE FROM THE ANCHOR TRENCH.

2. PLACE THE SOCK IN THE TRENCH SO THAT IT CONTOURS TO THE SOIL SURFACE. COMPACT SOIL FROM THE 22. PLACE THE SOCK IN THE INENOTION TO THAT IT CONTOORS TO THE SOLE SUB-RACE. COMPACT SOLE HOM THE EXCAVATED TRENCH AGAINST THE SOCK ON THE UPHILL SIDE. SOCKS SHALL BE INSTALLED IN 60 FT CONTINUOUS LENGTHS WITH ADJACENT SOCKS TIGHTLY ABUT. EVERY 60 FT THE SOCK ROW SHALL BE SPACED 12 INCHES CLEAR, END TO END, FOR AMPHIBIAN AND REPTILE TRAVEL. THE OPEN SPACES SHALL BE STAGGERED MID LENGTH OF THE NEXT DOWN GRADIENT SOCK.
3. SECURE THE SOCK WITH 18-24' (45.7-61 CM) STAKES EVERY 3-4' (0.9-1.2 M) AND WITH A STAKE ON EACH END. STAKE SHOLLD BE DRIVEN THROUGH THE MIDDLE OF THE SOCK LEAVING AT LEAST 2-3' (6-7 5 CM) OF STAKE EXTENDING ABOVE THE SOCK. STAKES SHOULD BE DRIVEN PERPENDICULAR TO THE SLOPE FACE.







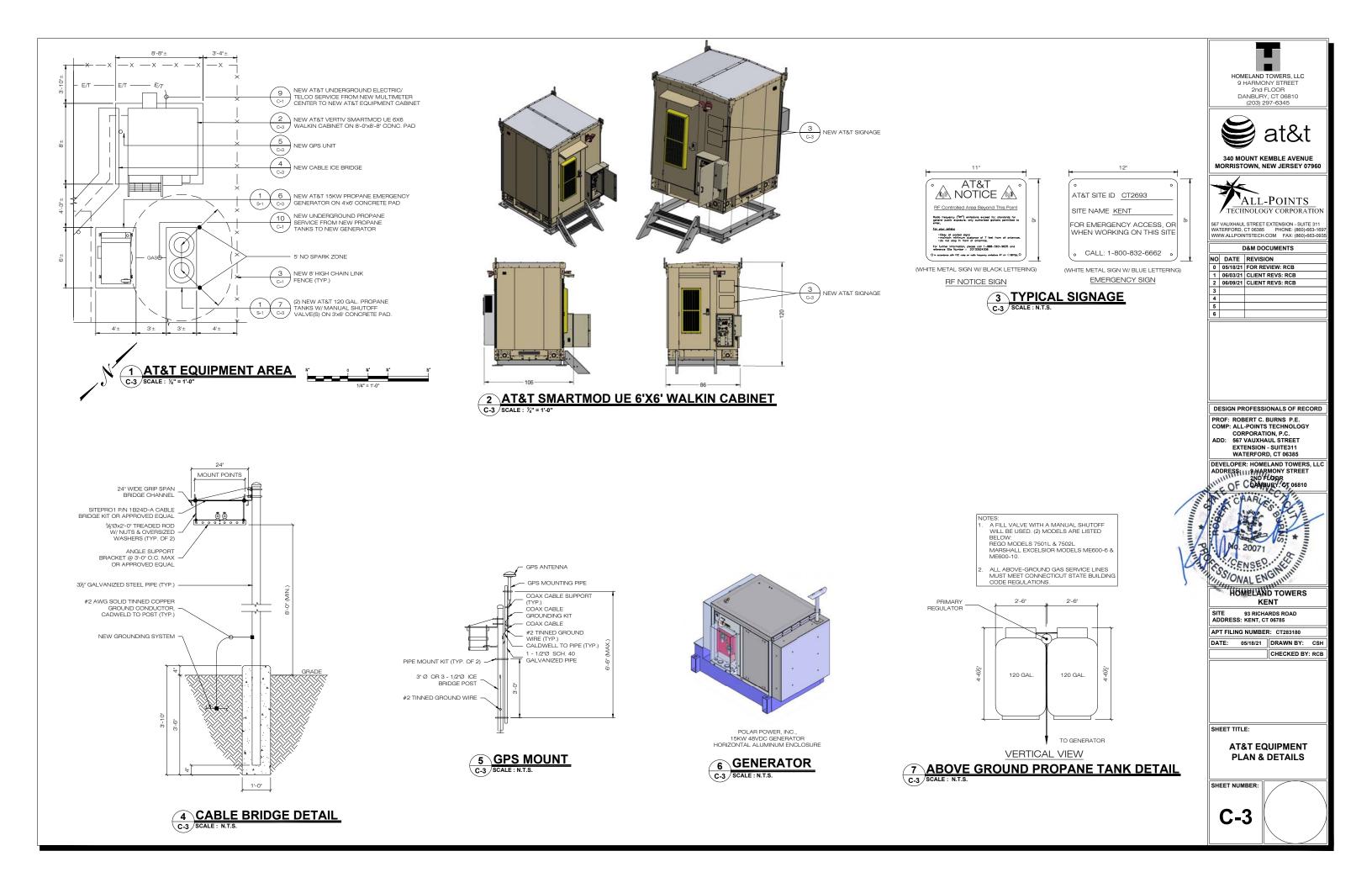


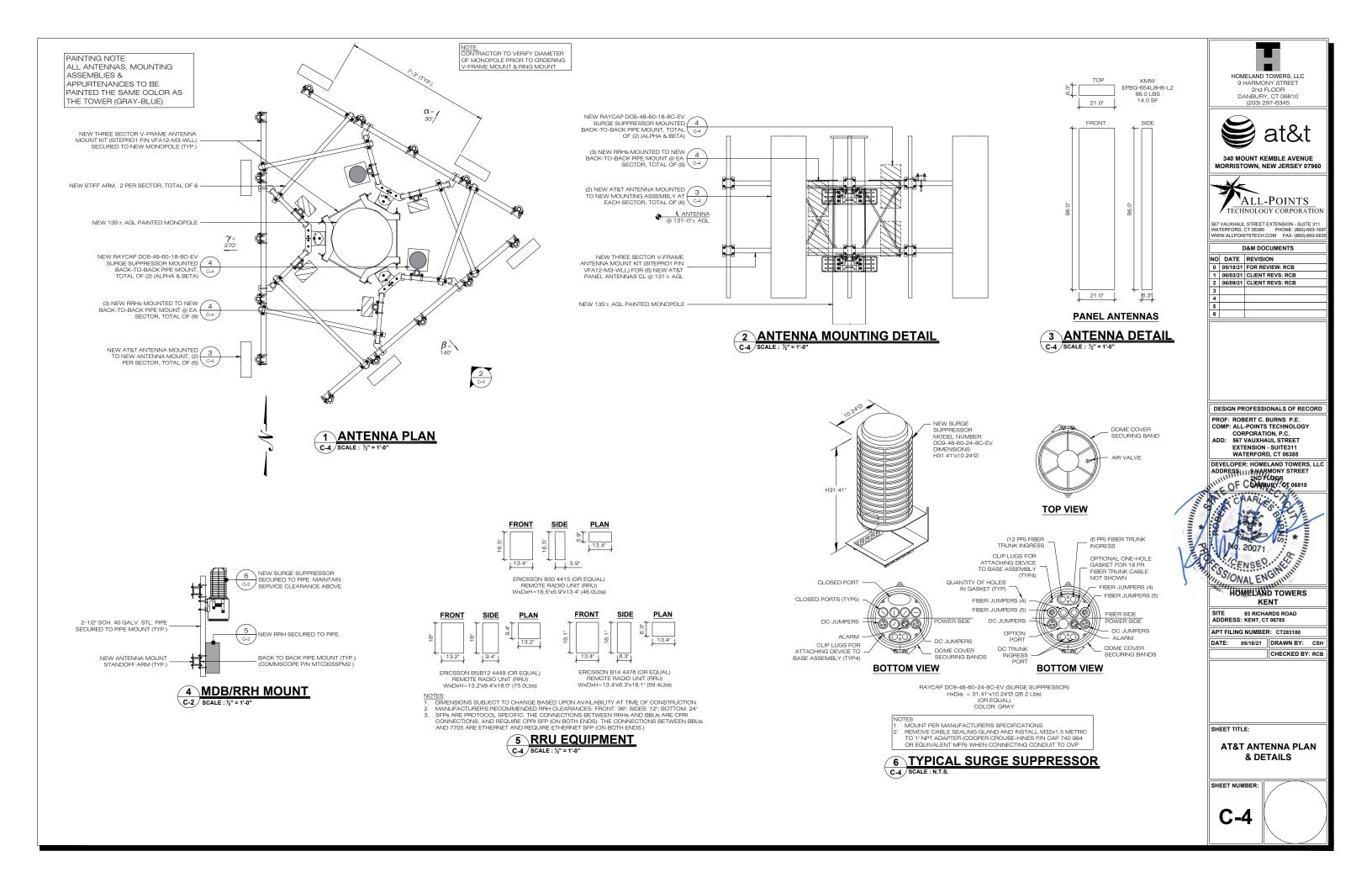
- CONCRETE WASHOUT AREA.

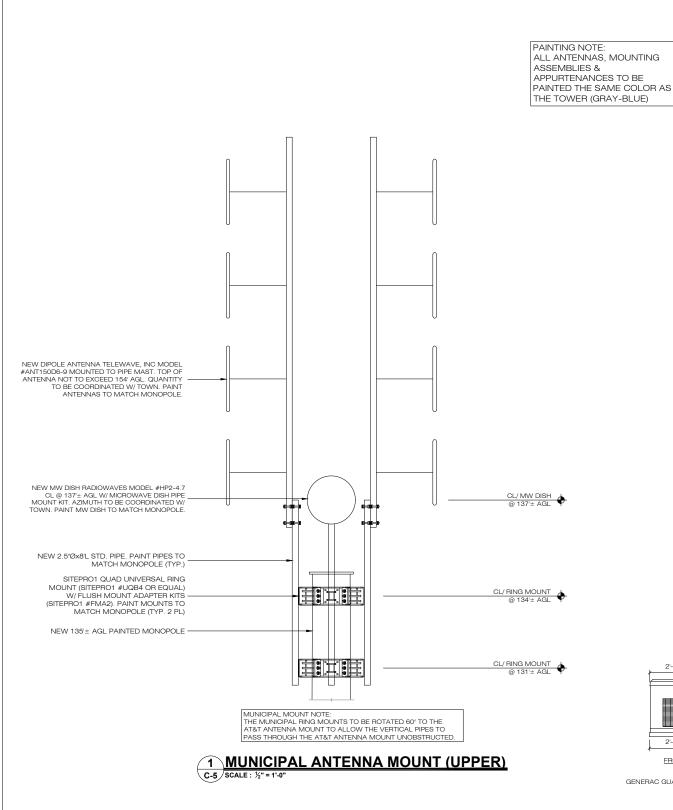


CONCRETE WASHOUT DETAIL SCALE : N.T.S.

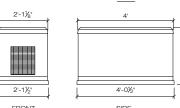
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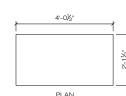


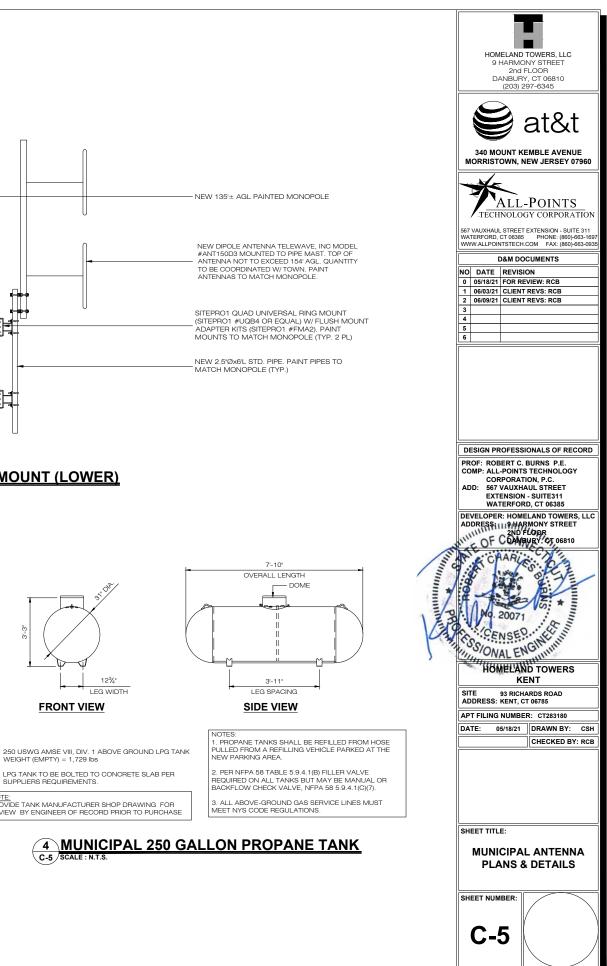


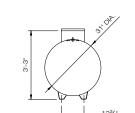


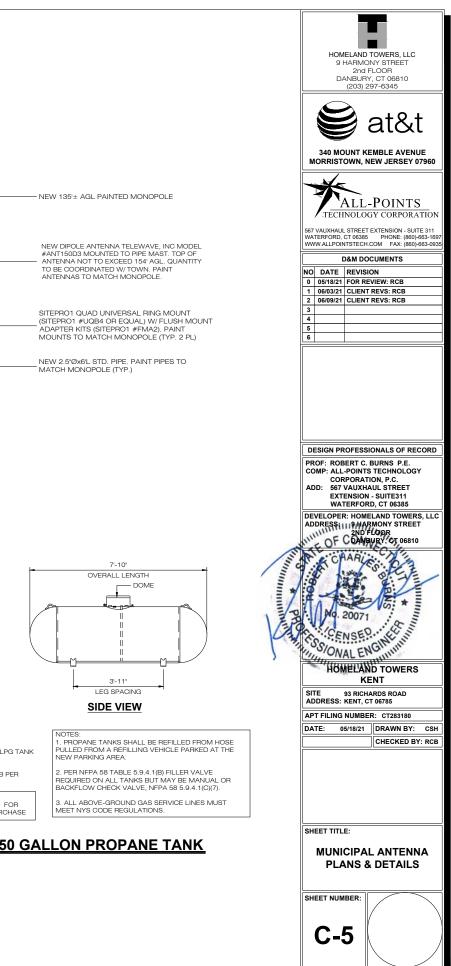




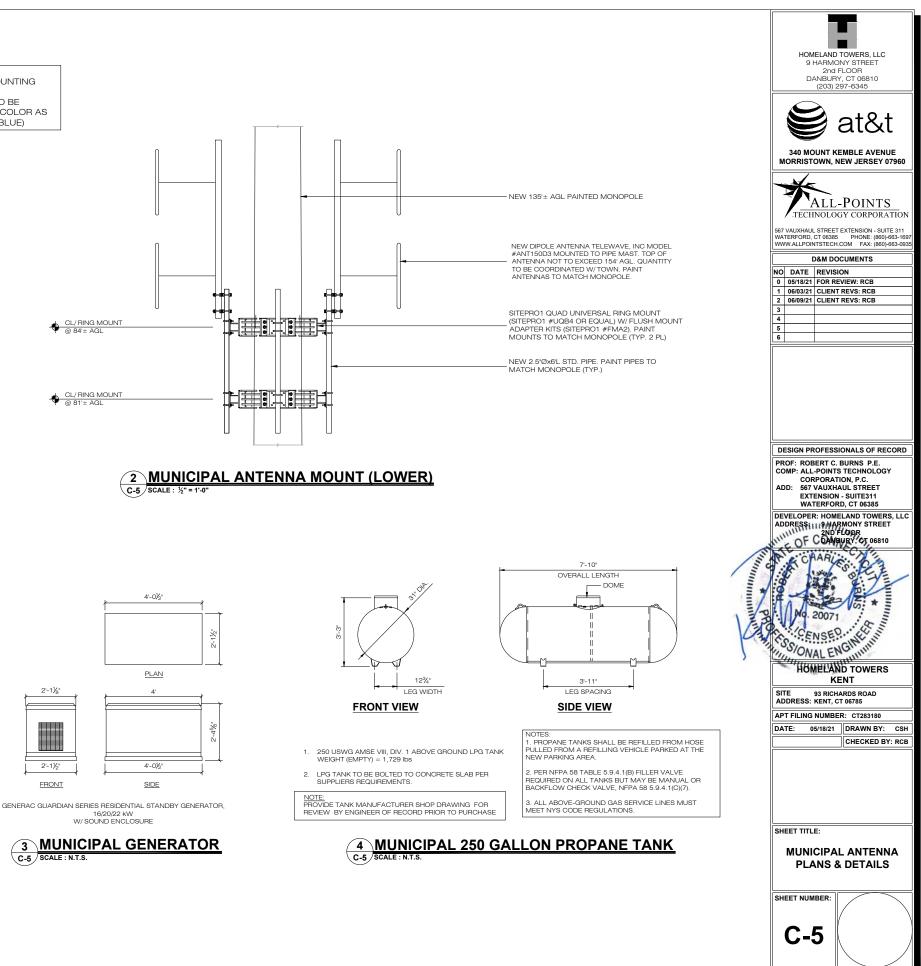


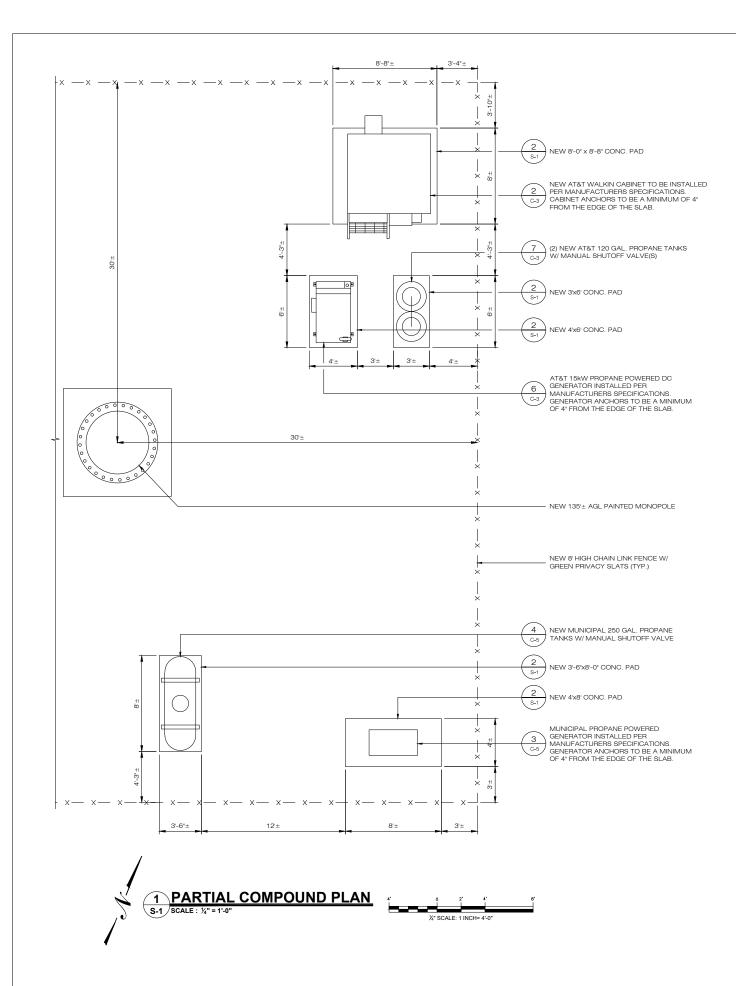


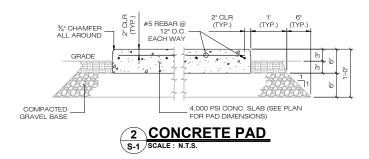


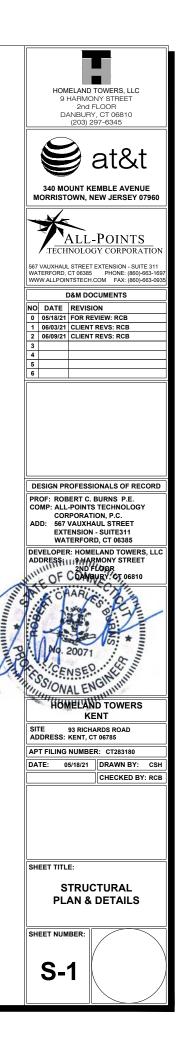


C-5 SCALE : 1/2" = 1'-0









EROSION CONTROL NOTES

- THE CONTRACTOR SHALL CONSTRUCT ALL SEDIMENT AND EROSION CONTROLS IN ACCORDANCE WITH THE 2002 CONNECTICUT GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL, LATEST EDITION, IN ACCORDANCE WITH THE CONTRACT DOCUMENTS, AND AS DIRECTED BY THE TOWN OF WATERTOWN, PERMITTER, AND/OR SWPCP MONITOR, ALL PERIMETER SEDIMENTATION AND EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO THE START OF CLEARING AND GRUBBING AND DEMOLITION OPERATIONS.
- 2 THESE DRAWINGS ARE ONLY INTENDED TO DESCRIBE THE SEDIMENT AND EROSION CONTROL MEASURES FOR THIS SITE. SEE CONSTRUCTION IAL INFORMATION. ALL TEMPORARY EROSION AND SEDIMENT CONTROL MEASURES SHOWN ON THE EROSION & SELDENCE FOR ADULT INFORUMENTATION AS REQUIRED BY THE ENGINEER THE CONTRACTOR SHALL BE PRESENDED FOR THE RESULT OF THE ADULT AND THE ADULT ADULT
- 3. A BOND OR CREDIT MAY BE REQUIRED TO BE POSTED WITH THE GOVERNING AUTHORITY FOR THE EROSION CONTROL INSTALLATION
- 4. THE CONTRACTOR SHALL APPLY THE MINIMUM EROSION & SEDIMENT CONTROL MEASURES SHOWN ON THE PLAN IN CONJUNCTION WITH CONSTRUCTION SEQUENCING, SUCH THAT ALL ACTIVE WORK ZONES ARE PROTECTED. ADDITIONAL AND/OR ALTERNATIVE SEDIMENT AND EROSION CONTROL MEASURES MAY BE INSTALLED DURING THE CONSTRUCTION PERIOD IF FOUND NECESSARY BY THE CONTRACTOR, OW SITE ENGINEER, MUNICIPAL OFFICIALS, OR ANY GOVERNING AGENCY. THE CONTRACTOR SHALL CONTACT THE OWNER AND APPROPRIATE GOVERNING AGENCIES FOR APPROVAL IF ALTERNATIVE CONTROLS OTHER THAN THOSE SHOWN ON THE PLANS ARE PROPOSED BY THE
- . THE CONTRACTOR SHALL TAKE EXTREME CARE DURING CONSTRUCTION SO AS NOT TO DISTURB UNPROTECTED WETLAND AREAS OR INSTALLED SEDIMENTATION AND EROSION CONTROL MEASURES. THE CONTRACTOR SHALL INSPECT ALL SEDIMENT AND EROSION CONTROLS WEEKLY AND WITHIN 24 HOURS OF A STORM WITH A RAINFALL AMOUNT OF 0.25 INCHES OR GREATER TO VERIFY THAT THE CONTROLS ARE OPERATING PROPERLY AND MAKE REPAIRS AS NECESSARY IN A TIMELY MANOR.
- 6. THE CONTRACTOR SHALL KEEP A SUPPLY OF EROSION CONTROL MATERIAL (SILT FENCE, COMPOST FILTER SOCK, EROSION CONTROL BLANKET, ETC.) ON-SITE FOR PERIODIC MAINTENANCE AND EMERGENCY REPAIRS.
- ALL FILL MATERIAL PLACED ADJACENT TO ANY WETLAND AREA SHALL BE GOOD QUALITY, WITH LESS THAN 5% FINES PASSING THROUGH A #200 SIEVE (BANK RUN), SHALL BE PLACED IN MAXIMUM ONE FOOT LIFTS, AND SHALL BE COMPACTED TO 95% MAX. DRY DENSITY MODIFIED PROCTOR OR AS SPECIFIED IN THE CONTRACT SPECIFICATIONS.
- PROTECT EXISTING TREES THAT ARE TO BE SAVED BY FENCING, ORANGE SAFETY FENCE, CONSTRUCTION TAPE, OR EQUIVALENT FENCING/TAPE. ANY LIMB TRIMMING SHOULD BE DONE AFTER CONSULTATION WITH AN ARBORIST AND BEFORE CONSTRUCTION BEGINS IN THAT AREA, FENCING SHALL BE MANITAINED AND REPARED DURING CONSTRUCTION.
- 9. CONSTRUCTION ENTRANCES (ANT)-TRACKING PADS) SHALL BE INSTALED PRIOR TO ANY STRE EXCAVATION OR CONSTRUCTION ACTIVITY AND SHALL BE MAINTAINED THROUGHOUT THE DURATION OF ALL CONSTRUCTION FEQUIPED. THE LOCATION OF THE TRACKING PADS MAY CHANGE AS VARIOUS PHASES OF CONSTRUCTION ARE COMPLETED. CONTRACTOR SHALL ENSURE THAT ALL VEHICLES EXITING THE SITE ARE PASSING OVER THE ANT-TRACKING PADS PRIOR TO EXISTING.
- 10. ALL CONSTRUCTION SHALL BE CONTAINED WITHIN THE LIMIT OF DISTURBANCE, WHICH SHALL BE MARKED WITH SILT FENCE, SAFETY FENCE, HAY BALES, RIBBONS, OR OTHER MEANS PRIOR TO CLEARING. CONSTRUCTION ACTIVITY SHALL REMAIN ON THE UPHILL SIDE OF THE SEDIMENT BARRIER UNLESS WORK IS SPECIFICALLY CALLED FOR ON THE DOWNHILL SIDE OF THE BARRIER.
- 11. NO CUT OR FILL SLOPES SHALL EXCEED 2:1 EXCEPT WHERE STABILIZED BY ROCK FACED EMBANKMENTS OR EROSION CONTROL BLANKETS. ALL SLOPES SHALL BE SEEDED AND BANKS WILL BE STABILIZED IMMEDIATELY UPON COMPLETION OF FINAL GRADING UNTIL TURF IS ESTABLISHED.
- 12. DIRECT ALL DEWATERING PUMP DISCHARGE TO A SEDIMENT CONTROL DEVICE CONFORMING TO THE GUIDELINES WITHIN THE APPROVED LIMIT OF DISTURBANCE IF RECURRED DISCHARGE TO STORM DRAINS OR SURFACE WATERS FROM SEDIMENT CONTROLS SHALL BE CLEAR AND APPROVED BY THE FERMITTE OR MUNICIPALITY.
- 13. THE CONTRACTOR SHALL MAINTAIN A CLEAN CONSTRUCTION SITE AND SHALL NOT ALLOW THE ACCUMULATION OF RUBBISH OR CONSTRUCTION DEBRIS ON THE SITE. PROPER SANITARY DEVICES SHALL BE MAINTAINED ON-SITE AT ALL TIMES AND SECURED APPROPRIATELY. THE CONTRACTOR SHALL TAKE ALL NECESSARY PRECAUTIONS TO AVOID THE SPILLAGE OF FUEL OR OTHER POLLUTANTS ON THE CONSTRUCTION SITE AND SHALL ADHERE TO ALL APPLICABLE POLICIES AND REGULATIONS RELATED TO SPILL PREVENTION AND
- 14. MINIMIZE LAND DISTURBANCES. SEED AND MULCH DISTURBED AREAS WITH TEMPORARY MIX AS SOON AS PRACTICABLE (2 WEEK MAXIMUM UNSTABILIZED PERIOD) USING PERENNIAL RYEGRASS AT 40 LBS PER ACRE. MULCH ALL CUT AND FILL SLOPES AND SWALES WITH LOOSE HAY AT A RATE OF 2 TONS PER ACRE. IF NECESSARY, REPLACE LOOSE HAY ON SLOPES WITH EROSION CONTROL BLAIXER'S ON JUTE (LOTM MODERATELY GRADED AREAS, ISLANDS, AND TEMPORARY CONSTRUCTION STAGING AREAS MAY BE HYDROSEEDED WITH TACKIFIER.
- 15. SWEEP AFFECTED PORTIONS OF OFF SITE ROADS ONE OR MORE TIMES A DAY (OR LESS FREQUENTLY IF TRACKING IS NOT A PROBLEM) DURING CONSTRUCTION. FOR DUST CONTROL, PERIODICALLY MOISTEN EXPOSED SOIL SURFACES WITH WATER ON UNPAVED TRAVELWAYS TO KEEP THE TRAVELWAYS DAMP. CALCIUM CHLORIDE MAY ALSO BE APPLIED TO ACCESS ROADS. DUMP TRUCK LOADS EXITING THE SITE SHALL BE
- 16. VEGETATIVE ESTABLISHMENT SHALL OCCUR ON ALL DISTURBED SOIL, UNLESS THE AREA IS UNDER ACTIVE CONSTRUCTION, IT IS COVERED IN STONE OR SCHEDULED FOR PAVING WITHIN 30 DAYS. TEMPORARY SEEDING OR NON-LIVING SOIL PROTECTION OF ALL EXPOSED SOILS AND SLOPES SHALL BE INITIATED WITHIN THE FIRST 7 DAYS OF SUSPENDING WORK IN AREAS TO BE LEFT LONGER THAN 30 DAYS
- ILL PERMANENT AND TEMPORARY SEDIMENT CONTROL DEVICES IN EFFECTIVE CONDITION THROUGHOUT THE CONSTRUCTIO ON COMPLETION OF WORK SWEEP CONCRETE PAGE, CLEAN THE STORMWATER MANAGEMENT SYSTEMS AND REMOVE ALL Y SEDIMENT CONTROLS ONCE THE SITE IS FULLY STABLIZED AND APPROVAL HAS BEEN RECEIVED FROM PERMITTEE OR THE MUNICIPALITY
- 18. SEEDING MIXTURES SHALL BE NEW ENGLAND SEMI-SHADE GRASS AND FORBS MIX (SEE SITE DETIALS SHEET DN-1), OR APPROVED EQUAL BY

SEDIMENT & EROSION CONTROL NARRATIVE

- THE PROJECT INCLUDES THE INSTALLATION OF A 135 ± AGL PAINTED MONOPOLE WITH ASSOCIATED GROUND MOUNTEI EQUIPMENT. ALL DISTURBED AREAS ARE TO BE SEEDED AND STABILIZED PRIOR TO THE INSTALLATION OF THE PROPOSE
- THE PROPOSED PROJECT INVOLVES THE FOLLOWING CONSTRUCTION:
- CONSTRUCTION OF 135 MONOPOLE.
 CONSTRUCTION OF 60x60' (3,600± SF) FENCED EQUIPMENT COMPOUND W/ GRAVEL SURFACE TREATMENT AND ASSC UTILITIES.
- D. CONSTRUCTION OF 60'± 12' WIDE GRAVEL ACCESS DRIVE.
- D. CONSTRUCTION OF 60°± 12° WIDE GRAVEL ACCESS DRIVE.
 E. CONSTRUCTION OF 8°0°×8°0° CONCRETE EQUIPMENT PAD, 4'×6° CONCRETE EQUIPMENT PAD, 3°×6°×6° CONCRETE EQUIPMENT PAD, 4'×6° CONCRETE PAD WITH 250 GALLON PROPANE TANK.
 F. THE STABILIZATION OF PERVIOUS DISTURBED AREAS WITH PERMANENT GRASS TREATMENTS.
- FOR THIS PROJECT, THERE ARE APPROXIMATELY 16,025± SF OF THE SITE BEING DIST
- 3. A GEOTECHNICAL ENGINEERING REPORT HAS BEEN COMPLETED FOR THIS PROJECT AND WILL BE AVAILABLE UNDER SEP
- 4. IT IS ANTICIPATED THAT CONSTRUCTION WILL BE COMPLETED IN APPROXIMATELY 12 WEEKS
- 5. REFER TO THE CONSTRUCTION SEQUENCING AND EROSION AND SEDIMENTATION NOTES FOR INFORMATION REGARDING SEQUENCING OF MAJOR OPERATIONS IN THE ON-SITE CONSTRUCTION PHASES.
- MEASURES ARE BASED UPON ENGINEERING PRACTICE, JUDGEMENT AND THE APPLICABLE SECTIONS OF THE 2002 CONNEC GUIDELINES FOR SOIL EROSION AND SEDIMENT CONTROL.
- DETAILS FOR THE TYPICAL EROSION AND SEDIMENTATION MEASURES ARE SHOWN ON PLAN SHEET C-2 OR PROVIDED AS SEPARATE SUPPORT DOCUMENTATION FOR REVIEW IN THIS PLAN.
- 8. CONSERVATION PRACTICES TO BE USED DURING CONSTRUCTION AREA
- STAGED CONSTRUCTION; MINIMIZE THE DISTURBED AREAS DURING CONSTRUCTION;
- STABILIZE DISTURBED AREAS AS SOON AS POSSIBLE WITH TEMPORARY OR PERMANENT MEASURES;

D. MINIMIZE IMPERVIOUS AREAS;
 E. UTILIZE APPROPRIATE CONSTRUCTION EROSION AND SEDIMENTATION MEASURES.

SUGGESTED CONSTRUCTION SEQUENCE

- THE FOLLOWING SUGGESTED SEQUENCE OF CONSTRUCTION ACTIVITIES IS PROJECTED BASED UPON ENGINEERING JUDGEMENT AND BEST MANAGEMENT PRACTICES. THE CONTRACTOR MAY ELECT TO ALTER THE SEQUENCING TO BEST MEET THE CONSTRUCTION SCHEDULE, THE EXISTING SITE ACTIVITIES AND WEATHER CONDITIONS. CONTRACTOR TO HIRE SURVEYOR FOR PROJECT STAKEOUT AS NEEDED THROUGHOUT CONSTRUCTION ACTIVITIES.
- CONTACT THE OWNER TO SCHEDULE A PRE-CONSTRUCTION MEETING. PHYSICALLY FLAG THE TREES TO BE REMOVED IN THE FIELD AS NECESSARY TO FACILITATE THE PRE-CONSTRUCTION MEETING.
- CONDUCT A PRE-CONSTRUCTION MEETING TO DISCUSS THE PROPOSED WORK AND EROSION AND SEDIMENTATION CONTROL MEASURES. THE MEETING SHOULD BE ATTENDED BY THE OWNER, THE OWNER REPRESENTATIVES), THE GENERAL CONTRACT DESIGNATE SUB-CONTRACTORS AND THE PERSON, OR PERSONS, RESPONSIBLE FOR THE IMPLEMENTATION, OPERATION, MONITORING AND MAINTENANCE OF THE EROSION AND SEDIMENTATION MEASURES. THE CONSTRUCTION PROCEDURES FOR THE ENTIRE PROJECT SHALL BE REVIEWED AT THIS MEETING
- NOTIFY THE OWNER AT LEAST FORTY-EIGHT (48) HOURS PRIOR TO COMMENCEMENT OF ANY DEMOLITION, CONSTRUCTION OR REGULATED ACTIVITY ON THIS PROJECT. NOTIFY CALL BEFORE YOU DIG CONNECTICUT AT (800) 922-4455.
- 4. CLEAR AND GRUB AS REQUIRED, TO INSTALL THE PERIMETER EROSION AND SEDIMENTATION CONTROL MEASURES AND, IF APPLICABLE, TREE PROTECTION
- 5. INSTALL CONSTRUCTION ENTRANCE.
- 6. PERFORM THE REMAINING CLEARING AND GRUBBING AS NECESSARY, REMOVE CUT WOOD AND STUMPS, CHIP BRUSH AND STOCKPILE FOR FUTURE USE OR REMOVE OFF-SITE. REMOVE AND DISPOSE OF DEMOLITION DEBRIS OFF-SITI
- 7. TEMPORARILY SEED DISTURBED AREAS NOT UNDER CONSTRUCTION FOR THIRTY (30) DAYS OR MORE
- 8. EXCAVATE AND GRADE NEW ACCESS DRIVE.
- 9. EXCAVATE AND ROUGH GRADE EQUIPMENT COMPOUND
- 10 EXCAVATE FOR TOWER FOUNDATION & FOUIPMENT PADS
- 11. FINALIZE ACCESS ROAD GRADES.
- 12. PREPARE SUBGRADE AND INSTALL FORMS, STEEL REINFORCING, & CONCRETE FOR TOWER FOUNDATION & EQUIPMENT PADS
- 13. INSTALL BURIED GROUND RINGS, GROUND RODS, GROUND LEADS, UTILITY CONDUITS & UTILITY EQUIPMENT
- 14. BACKFILL TOWER FOUNDATION
- 15 EBECT MONOPOLE
- 16. INSTALL TELECOMMUNICATIONS EQUIPMENT ON TOWER & COMPOUND.
- 17. INSTALL COMPOUND GRAVEL SURFACES.
- 18. FINALIZE GRADES. INSTALL GRAVEL SURFACES. PAVE ACCESS DRIVE
- 19. INSTALL FENCING.
- 20. CONNECT GROUNDING LEADS & LIGHTNING PROTECTION
- 21. FINAL GRADE AROUND COMPOUND.
- 22. LOAM & SEED DISTURBED AREAS OUTSIDE COMPOUND, AS REQUIRED.
- 23. TEST ALL NEW EQUIPMENT.
- 24. AFTER THE SITE IS STABILIZED AND WITH THE APPROVAL OF THE OWNER, REMOVE PERIMETER EROSION AND SEDIMENTATION

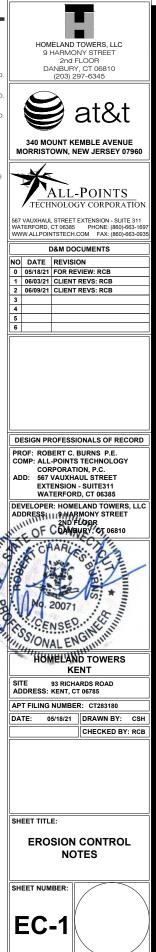
25. PERFORM FINAL PROJECT CLEANUP.

THE ESTIMATED TIME FOR THE COMPLETION OF THE WORK IS APPROXIMATELY TWELVE (12) WEEKS. THE EXACT PROCESS MAY VARY DEPENDING ON THE CONTRACTORS & SUBCONTRACTORS AVAILABILITY TO COMPLETE WORK & WEATHER DELAYS.

	CONSTRUCTION OPERATION AND MAINTENANCE PLAN - BY CONTRACTOR			
D	E&S MEASURE	INSPECTION SCHEDULE		
ED	CONSTRUCTION ENTRANCE	DAILY		
SOCIATED	HAY BALES	WEEKLY & WITHIN 24 HOURS OF RAINFALL $> 0.2^{\circ}$		
PMENT PAD.	SILT FENCE	WEEKLY & WITHIN 24 HOURS OF RAINFALL > 0.2*		
INENT FAD,	SILT SACKS	WEEKLY & WITHIN 24 HOURS OF RAINFALL $> 0.2^{\circ}$		
PARATE	TOPSOIL/BORROW STOCKPILES	DAILY		
	WATER BARS	DAILY		
G	TEMPORARY DIVERSION DITCHES	DAILY & WITHIN 24 HOURS OF RAINFALL > 0.2°		
CTICUT	TEMPORARY SEDIMENT TRAPS/BASINS	WEEKLY & WITHIN 24 HOURS OF RAINFALL $> 0.2^{\circ}$		
AS	TEMPORARY SOIL PROTECTION	WEEKLY & WITHIN 24 HOURS OF RAINFALL > 0.2"		

MAINTENANCE REQUIRED

- PLACE ADDITIONAL STONE, EXTEND THE LENGTH OR REMOVE AND REPLACE THE STONE. CLEAN PAVED SURFACES OF TRACKED SEDIMENT.
- REPAIR/REPLACE WHEN FAILURE, OR OBSERVED DETERIORATION, IS OBSERVED REMOVE SILT WHEN IT REACHES 1/2 THE HEIGHT OF THE BALE.
- REPAIR/REPLACE WHEN FAILURE, OR OBSERVED DETERIORATION, IS OBSERVED REMOVE SILT WHEN IT REACHES 1/2 THE HEIGHT OF THE FENCE.
- REPAIR/REPLACE WHEN FAILURE, OR OBSERVED DETERIORATION, IS OBSERVED REMOVE SILT WHEN IT REACHES 1/2 THE HEIGHT OF THE SACK. REPAIR/REPLACE SEDIMENT BARRIERS AS NECESSARY
- REPAIR/RESHAPE AS NECESSARY. REMOVE SILT WHEN IT REACHES 1/2 THE HEIGHT OF THE WATER BAR
- REPAIR/RESHAPE AS NECESSARY. REVIEW CONDITIONS IF REPETITIVE FAILURES
- REMOVE SEDIMENT WHEN IT REACHES 1/2 OF THE MINIMUM REQUIRED WET STORAGE VOLUME.
- REPAIR ERODED OR BARE AREAS IMMEDIATELY. RESEED AND MULCH.



DESIGN BASIS: 30VERNING CODES/DESIGN STANDARDS: 2015 IBC/2018 CONNECTICUT STATE BUILDING CODE NATIONAL ELEC TIA-222-H TRIC CODE DESIGN CRITERIA: ISK CATEGORY (2018 CSBC TABLE 1604.5) (TIA-222-H, TABLE 2-1) SNOW LOAD: ROUND, P_g: 30 PSF (2018 CSBC APPENDIX N) VINIMUM FLAT 30 PSF (2018 CSBC SECT. 1608.1.1) VIND LOADS: UTIMATE BASIC VIND SPEED, VULT: 114 MPH (TIA-222-H, ANNEX B) KPOSURE CATEGORY C (2015 IBC SECT. 1609.4) ICE LOADS: ICE THICKNESS. t: 1.00 IN (TIA-222-H. ANNEX B) CE THICKNESS MPORTANCE FACTOR, I: 1.0 (TIA-222-H, ANNEX B) VOMINAL BASIC WIND SPEED W/ ICE, VI 40 MPH (TIA-222-H, ANNEX B) SECOND GUS EISMIC LOAD: EFER TO SECTION 1613 OF THE 2015 IBC/2018 CONNECTICUT TATE BUILDING CODE FOR SEISMIC CLASSIFICATION AND DADING DETERMINATION. 4 CONCRETE: 01 GENERAL: USED IN THESE SPECIFICATIONS INCLUDE THE NG: AMERICAN CONCRETE INSTITUTE AMERICAN WATIONAL STANDARDS INSTITUTE AMERICAN WELDING SOCIET AMERICAN ISOCIETY OF CIVIL ENGINEERS AMERICAN STANDARDS AND TESTING METHODS CONCRETE REINFORMS TESTING METHODS L CONCRETE USED SHALL BE 4000 PSI (28 DAY COM
 ORTLAND CEMENT:
 ASTM C150, T1

 JGGREGATE:
 ASTM C33, 1 INCH MAX

 VATER:
 POTABLE

 DMIXTURE:
 NON-CHLORIDE

 IB:
 R5*
 INTERNATIONAL CODE COUNCIL EVALUATION SERVICE TELECOMMUNICATIONS INDUSTRY ASSOCIATION UNDERWITERS LABORATORIES ICC-ES TIA IL UNDERWIFTERS LABORATORIES IC NATIONAL ELECTRICAL CODE IFPA NATIONAL FIRE PROTECTION ASSOCIATION OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION SHA OCCUPATIONAL SAFETY AND HEALTH ADMINISTRATION FIN INDIVIDUAL TRADE, DISCOLUBE, AND CONTRACTOR SHALL LUDE THESE GENERAL SPECIFICATIONS. LIMP. 4 INCH ENGINEER IS ON TRESPONSIBLE FOR NOR A GUARANTOR OF THE FALLING CONTRACTORS WORK, ADEQUACY OF ANY SITE MONENT, SUPERVISION OF ANY WORK, AND SAFETY IN, ON, OR JUT THE WORK SITE. REFERENCE HEREIN TO AN OR EQUAL ITEM, THAT EQUAL ITEM LL BE PRE-APPROVED BY THE CONSTRUCTION MANAGER BEFORE ALLATION EFOLLOWING MINIMUM CONCRETE COVER SHALL BE ROVIDED FOR REINFORCING STEEL:
 CONCRETE CAST AGAINST EARTH = 3 IN. CONCRETE EXPOSED TO EARTH OR WEATHER:
 #6 AND LARGER = 2 IN. STALLATION LL TRADES SHALL COORDINATE THEIR WORK WITH ALL OTHER TRADES NO OTHER WORK AND CONDITIONS AS APPROPRATE OR REQUIRED TO VIDI CONFLICTS. RESOLVE AND COORDINATE ALL CONFLICTS WITH LA FRECTEE WORK AND STEC OFFENTIONS. COORDINATION WITH THE LA FRECTE WORK AND STEC OFFENTIONS. COORDINATION WITH THE TE SHALL BE WITH THE OWNER, OR OWNERS SPECIFIED DEPRESENTATIVE, FOR EVENTIMING BELIATED TO THE INSTALLATION OF •• #5 AND SMALLER = 1 1/2 IN. RESENTATIVE, FUH EVEN I THING I ALL APPLICABLE S PROJECT. WORK SHALL BE IN STRICT ACCORDANCE WITH ALL APPLICABLE TIONS OF ALL APPLICABLE CODES AND SHALL BE ACCEPTABLE TI SLAB AND WALL = 3/4 IN.
 BEAMS AND COLUMNS = 1 1/2 IN. DINCRETE FOOTINGS SHALL BE CAST AGAINST LEVEL, DIMPACTED, NON-FROZEN BASE SOIL FREE OF STANDING ANCHORS: TALLATION OF ANY WORK. TIRACTORS SHALL VERIFY ALL DIMENSIONS AND CONDITIONS IN THE LD PRIOR TO FABRICATION AND ERECTION OF ANY MATERIAL. THE INDERES RHALL BE NOTHER FOR INSPECTIONS PHICAT DO LOSING INTERTING AND OF ANY CONDITIONS WHICH PRECLUDE MULETION OF THE WORK IN ACCOMMANCE WITH THE CONTRACT CUMENTS. INTRACTOR SHALL VISIT THE SITE TO MANAGE AND GAIN APPROVAL R ALL TENANT DISRUPTIONS, POWER OLTAGES, WORK SCHEDULES, NITION OF WORK AREA AND WORK STORAGE, PROPER LDINGSTE ACCESS, NOISE AND CLEANLINESS RECURREMENTS WITH BUILDINGSTE MAKAGEMENT PROFIT O ALL WORK. ANY RUPTIONS SHALL BE KEPT TO A MINIMUM AND SHALL BE LEMENTED OILV, UPON WITHTEN APPROVAL OF THE OWNER. CTOR SHALL SAFEGUARD AGAINST CREATING ANY HAZARI ENANT EGRESS OR COMPROMISING SITE SECURITY AFFECTING TEWART EGRESS OR COMPROMISING SITE SECURITY RESORDES. ALL BELOWGRADE WORK AND ANY SURFACE WORK IN A REW AREA FOR STRUCTURES OR VEHICLES. CONTRACTOR SHALL REW AREA FOR STRUCTURES ON VEHICLES. CONTRACTOR SHALL STRUCTURES, CONDUITS, AND PRELINES IN THE AREA. ALL DISTING SEWER, WATER, OS, BLECTRIS, INEER OTIC, AND OTHER REVER, WATER, OS, BLECTRIS, INEER OTIC, AND OTHER ANDERGOUND UTLITES IDENTIFIED OR ENCOUNTERED, SHALL BE REVER, WATER, OS, BLECTRIS, INTER CONTRACTOR IS RESONSIBLE FOR REVER, WATER, OS, BLECTRIS, INTER CAUNON SHOLD, BLEUED BY THE ANDERGOUND ON INTIRES. ISCHMENG CAUNON SHOLD BE USED BY THE REVER, WATER, OS, BLECTRIS, INTER CAUNON SHOLD BE USED BY THE REVERS, REPLACEMENT, AND ALL ANDAGES DUE TO DAMAGE OF TILTIES BY HIS OFERATIONS. ALL EDSTING AND EVE OULPHENT AND MATERIAL LOCATIONS, ROUTING, ORIENTATION, MOUNTING, SPECIFICATIONS AND GENERAL STALLES ON AND STRUCTURES COST, DAMAGES DUE TO DAMAGE OF TELD PRIOT TO ANY INSTALLATION. ANY DIFFERENCES THAT MAY CAUSES SONGIUSC, COST, OR GUALLATION ANY DIFFERENCES THAT MAY CAUSES SONGING COST, OR GUALLATION ANY DIFFERENCES THAT MAY CAUSES SONGIUSC, COST, OR GUALLATION OF THE CONNERNED ONTOTION FOR THE ATTEMINON OF THE OWNER ON ENGINEER PROTO TO ANY WORK. LERED FRONCE THERE TO SHALL BE REMOVIDENT TO THE ATTEMINATE COST, OR GUALLATION OF THE CONNERNED AND THE DE MONOT TO THE RED PROTO TO ANY INSTALLATION. TENTION OF THE OWNER OR ENGINEER PRIOR TO ANY WORK. LE REFERENCES HEREIN TO VERIFICATION OF ANY COMMON OF I-LD, PLANS, OR SPECIFICATIONS PRIOR TO ANY WORK SHALL BEI LL REPRONSIBILITY OF THE CONTRACTOR, ANY ADD ALL ADDITIO DIPOLATIONS, CHANGES, REPARE, OR DEMOLITION AS A RESULT DIPOLATIONS, CHANGES, REPARE, OR DEMOLITION AS A RESULT ENTINO OF THE CONTRACTOR WITHOUT DELAY, COST, OR WAGES IN QUALITY.

NOTES THIS SHEET SHALL APPLY UNLESS SPECIFICALLY NOTED IERWISE ON THE INCLUDED DRAWINGS OR IN SEPARATE PROJEC ICIFICATIONS AS APPLICABLE. ALL SPECIFICATIONS SHALL BE VSIDERED REQUIRED UNLESS APPROVED EQUAL BY THE OWNER, VSTRUCTION MANAGER, OR ENGINEER AS APPLICABLE. WORDS "PROVIDE" OR "INSTALL" SHALL MEAN FURNISH AND TALL.

PROVED SAFE MANNER. L SURPLUS MATERIAL SHALL BE REMOVED FROM THE SITE PROMPTLY HEN DEEMED TO BE SURPLUS. HEN DEEMIEL TO BE SURFLUS. ENY CONTRACTOR SHALL BE RESPONSIBLE FOR THE PROTECTION O SWORK AND NEWLY INSTALLED OR EXISTING WORK, INCLUDING OTECTION OF THE SITE, ALL STRUCTURES, AND ALL OCCUPANTS. RNISH, INSTALL, MAINTAIN, AND REMOVE AS APPROPRIATE, ALL OPRIATE BARRIERS, SAFETY GUARDS, SIGNAGE, AND SECURITY AS RED. CONTRACTOR SHALL BE RESPONSIBLE FOR THEIR RESPECTIVE PERMITS, INSPECTIONS, TESTING, CERTIFICATES, AND ALL GENERIC OF SAME REQUIRED FOR OWNERLEING OF AND LGAL PANOV OF THE INNSHED PROJECT. DINTRACTORS SHALL PROVIDE ALL NECESSARY TOOLS, FIXTURES, ZES, MATERIALS, JOB ADS, AND PERSONNEL REQUIRED FOR THE TION OF THEIR WORK. WICES, MATERIALS, JOB ADS, AND PERSONNEL REQUIRED FOR THE CUTION OF THEM WORK. AND AND A CONTRACTOR SHALL GUARANTER ALL MATERIALS AND REMONSING THE MATERIA AFER ANCEPTIALS OF THE NOTALLATION BY OWNER WALL BE REPERSONNED BY LICENSED CONTRACTORS IN THE DE HAVING JURGECTOR LE DATING JURISUCTION. / DEVIATION, MODIFICATION, ADDITION, OR CHANGE IN DESIGN LL NOT BE MADE WITHOUT WRITTEN APPROVAL OF THE OWNER OF INFER. INEER. CONTRACTORS SHALL SUBMIT SHOP DRAWINGS OF ALL EQUIPMEN MATERIALS TO THE ENGINEER FOR APPROVAL PRIOR TO RECATION AND INSTALLATION, AND SHALL NOT PROCEED UNTIL NEER APPROVAL IN WRITING IS RETURNED. EACH CONTRACTOR LL MANTAIN ON JOB STATE A COMPLETE SET OF SHOP DRAWINGS I ANY DEVINTIONS FROM THE ORIGINAL DESIGN SHALL BE NOTED. NNOPACIONERI INFRODUNDUI. L'ATTERNALS COUPERIENT, TOOLS, AND ITEMS UNDER THE INTRACTORS RESPONSIBILITY ON THE JOBSITE SHALL BE EQUATELY SEQURED, MAINTAINED, AND PROTECTED, SO AS NOT TO COME DAMAGED OR CREATE ANY HAZARD TO PERSONNEL OR OFFERTY. E CONTRACTORS HOURS OF WORK SHALL BE IN ACCORDANCE WITH-CAL CODES AND ORDINANCES AND BE APPROVED BY THE OWNER. JAL CODES AND DRAINANCES AND BE APPROVED BY THE OWNER. TITACTOR SHALL PROVIDE SAFETY TRAINING FOR ALL OF HIS CREW DI NSUBE THAT EVERY CREW MEMBER POLLOWS SAVE WORK COTICES. SAFETY TRAINING SHALL INCLUDE, BUT NOT BE LIMITED TO, L PROTECTION, CONFINED SPACE ENTRY, ELECTRICAL SAFETY, AND NONHINGEXCAVATION SAFETY WHERE SUCH WORK IS EXECUTED OR COUNTERED. . TEMPORARY WORK REQUIRED OR SPECIFIED AS A PART OF THIS SRK, SHALL MEET ALL OF THE SAME REQUIREMENTS AS PERMANEN TALLATIONS, SHALL MEET ALL APPLICABLE COOR REQUIREMENTS D SHALL BE COMPLETELY REMOVED AFTER ITS PURPOSES HAVE DI STRUET N SERVED. / EXISTING UTILITY, SERVICE, STRUCTURE, EQUIPMENT, OR FIXTURE STRUCTING THE WORK SHALL BE REMOVED AND/OR RELOCATED AS ECTED BY THE CONSTRUCTION MANAGER. ECOTED BY THE CONSTRUCTION MANAGER. SEESTOS & ISCOUNTERED DURING WORK EXECUTION, NITRACTOR SHALL IMMEDIATELY NOTIFY THE CONSTRUCTION NAGER AND CEASE ALL ACTIVITIES IN AFFECTED AREAS UNTIL TIFIED BY THE CONSTRUCTION TO RESUME OFERATIONS. IST ELECTIFICAL AND MECHANICAL FIXTURES, PINING, WRING DI EQUIPMENT OBSTRUCTION THE WORK SHALL BE REMOVED DIOR RELOCATE. AND MECHANICAL FIXTURES, PINING, WRING DID RELOCTIONAL AND MECHANICAL FIXTURES, PINING, WRING DID RELOCTAL AND MECHANICAL FIXTURES, PINING, WRING DID RELOCTAL AND MECHANICAL FIXTURES, PINING, WRING DID RELOCATED AS DIRECTED BY THE CONSTRUCTION MICH AND THE WORK OF THE PINING MUST BE ORDINATED WITH OWNER. LOCATIONS SHALL INCLUDE THE GENERAL EGERATIONS HEREIN. L CONCRETE CONSTRUCTION SHALL BE DONE IN ACCORDANCE TH THE AMERICAN CONCRETE INSTITUTE (ACI) CODES 301 & 318, TEST REVISION. RENGTH). THE CONCRETE MIX SHALL BE BASED ON USING THE ILLOWING MATERIALS AND PARAMETERS: LL CONCRETE EXPOSED TO FREEZING WEATHER SHALL DNTAIN ENTRAINED AIR PER ACI 211 TABLE 4.2.1 OF ACI 318-05. INI AIR INI HARINELI AIR IVER AUZ 211 LABLE 4.2.1 OF AUZ 318-02 LEINENGROND STEEL SHALL BE ASTM A615, G 60 EFORMED, WELDED WIRE FABRIO SHALL CONFORM TO ASTM 86 WELDED STEEL WIRE FABRIC SHALL CONFORM TO ASTM BO WELDED STEEL WIRE FABRIC SHALL CONFORMAL BE CLASS ID ALL HOCKS SHALL BE ACI STANDARD LINO, REINFORCING RS SHALL BE COLD BENT WHERE REQUIRED AND TIED (NOT ELDED). CONCRETE NOT EXPOSED TO EARTH OR WEATHER OR NOT
 CAST AGAINST THE GROUND: 3/4 IN. CHAMFER SHALL BE PROVIDED AT ALL EXPOSED EDGES CONCRETE, IN ACCORDANCE WITH ACI 301 SECTION 4.2.4. NCRETE SHALL BE PLACED IN A UNIFORM MANNER AND INSOLIDATED IN PLACE. TIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS IN. NISION ANCHORS SHALL BE USED WHERE ATTACHING TO CRETE. MASONRY MOUNTS SHALL HAVE INJECTION ADHESIVE HORING. NISION BOLTS SHALL BE HILTI KWIK BOLT 3 OR EQUAL. MINIMUM NATA-KING JOINT SHALL BE HILT KWIK BOLT 3 OR EQUAL. MINMUM AVAILABLE JOINT SHALL BE HILT KWIK BOLT 3 OR EQUAL. MINMUM BANGKING JOINT SHALL BE HILT KWIK BOLT 3 OR EQUAL. MINMUM SHALL BE LITH IN-70 OR EQUAL. WITH HARDED ROD AND SOREEN TUBES. NOTORING IN BRICKS WITH HOLES SHALL HAVE AND/GRIS SHACED 2 ONE/TETE BRICKS MITH HOLES SHALL MARATIN. 2 COMPLETE BRICKS MITH HOLES SHALL MARATIN. 2 COMPLETE MILL BE EMPEDDED 3-12 INOVES MINMUM. AND/ORNING IN FOLLOW ORDETETE BLICKS WITH HOLES SHALL MARATIN. BRICKS JOINT HOLE WILL BE EMPEDDED 3-12 INOVES MINMUM. AND/ORNING IN FOLLOW ORDETETE LICKS VIELL BUS SHALL MARATIN. MONORING IN HOLLOW ONGERTE ELOCKS VIELL BE SHALL HAVE AND/ORGE AND/ORDET HOLDOW ONGERTETE LICKS WITH HOLES SHALL BUS SHALL MARTIN HOLDOW ONGERTE ELOCKS AND HALL BE HILT HITH YAZO OR EQUAL. MITH THRADED JUEDTON AND/ESINE AND/ORDIN IN SCLID MARANIAM POR BLOCK CELL SHALL LIEDTON AND/ESINE AND/ORDIN IN SCLID MARANIAM POR BLOCK CELL BOLGES SHALL BE HILT HITH YAZO OR BLOCH. MITH THRADED OL. MARTATA 12 INO/ESIS BEIWEEN AND/ORDS AND ALL FREE BEDGES STANMAM SPACING BETWEEN AND/ORDS SI BLOCHSS SI DICHSS BECOMMENDATIONS AND SHALL NOT BE INSTALLED IN MORTAN JOINTS. BECOMMENDATIONS AND SHALL NOT BE INSTALLED IN MORTAN JOINTS. TING SHALL BE ATTACHED USING FOUR GRATING CLAMPS OR 1/4

5 POST-INSTALLED ANCHORS: HERE INDICATED ON THE DRAWINGS, POST-INSTA 3 SHALL CONSIST OF THE FOLLOWING ANCHOR TY D IN ACCORDANCE WITH THEIR RESPECTIVE (CC-E) URACTURERS PUBLISHED INSTALLATION INSTRUC INSTALED IN ACCOREDANCE WITH THEIR RESPECTIVE (CC-ES REPORT ADMALIANCE INSTALLATION INSTALLINGUE INSTALLINGUE INSTALLION INSTALLINGUE ESIVE ANCHORS INSTALLED IN A HORIZONTALLY OR UPWARDLY INED ORIENTATION INTO CONCRETE AND SUPPORTING A SUSTA SION LOAD SHALL BE INSTALLED BY A CERTIFIED ADHESIVE AI ALLER, PER SECTION 9.2.2 OF ACI-318-14. INSTALLER SHALL TIFIED THROUGH THE ACI(CRSI ADHESIVE ANCHOR INSTALLER TIFICATION PROGRAM. HORS SHALL BE INSTALLED PER MANUFACTURERS OMMENDATIONS AND SHALL NOT TO BE INSTALLED IN MORTAR IIS. ER OSHA 29 CFR 1926.1153 SILICA DUST CONTROL REGULATIONS, EP USING 25 OFF 1320 TTO SULDA DOUT OCU IN DC PEDIDOLTION DE MOLES FOR DOST INSTALLED ANCHORS IN CONCORETE AND DNMY SHALL BE INSTALLED USING HILT SAFE SET INSTALLATION EN WHICH COMPRISES OF A CODE APPROVED HILT HOLLOW DI ND VACUUM. ALTERNATE INSTALLATION METHODS ARE ALSO WED WITH AN APPROVED DUSTLESS SYSTEM THAT MAINTAINS A DUST EMISSION BELOW THE PERMISSIBLE LEVELS. IGTOR SHALL ARRANCE AN ANCHOR MANUFACTURERS ENTATIVE TO PROVIDE ON-STEE ANCHOR INSTALLATION G FOR ALL OF THEIR ANCHORING PRODUCTS SPECIFIED. IGTOR SHALL SUBMIT DOCUMENTED CONFIRMATION THAT ALL CONTRACTORS PERSONNEL INSTALLING ANCHORS HAVE ID THE RECURED TRAINING PROR TO THE COMMENCEMENT OF NTINUOUS OR PERIODIC SPECIAL INSPECTION FOR POST INSTALLED CHORS SHALL BE PERFORMED IN ACCORDANCE WITH SECTION 4.4 OF THE ICC-ES REPORT FOR THE INDIVIDUAL ANCHOR. SPECIAL PECTOR SHALL BE NOTIFIED PRIOR TO COMMENCEMENT OF WORK COORDINATE INSPECTION EFFORTS. STEEL: FICATIONS SHALL INCLUDE THE GENERAL SPECIFICATION
 TERIALS:

 IDB FLANGE
 ASTM A992, GR 50

 JBING
 ASTM A500, GR 8

 PE
 ASTM A53, GR B

 DLTS
 ASTM A32, GR B

 RATINA 32, GR B
 TYPE GW-2 (1-1/4'3/16' BARS)

 QSTING METALS
 ASTM A38
 COSE: LEDGLTS, ANCHORS AND MISCELLANEOUS HARDWARE EXPOSED TO MEANERS SHALL BE GALVANEZED IN ACCORDANCE WITH ASTM 153 INFO COATING (FON-DIP) ON IRON AND STELL HARDWARE) MARGED GALVANEZED SHERE WITH COAD ZACK, GALVANEON ANAGED GALVANEZED SHERE WITH COAD ZACK, GALVANEON ANAGED GALVANEZED SHERE WITH COAD ZACK, GALVANEON HIL DANAEED SHORE WITH COAD ZACK, GALVANEON MARGED GALVANEZED SHERE WITH COAD ZACK, GALVANEON HIL DANAEED SHORE OF FIELD. HIL DANAEED SHORE OF GALVANEZED STELL HARDWARE WITH COAD ZACK, GALVANEON HIL DANAEED SHORE OF GALVANEZED STELL MARGED GALVANEZED SHERE WITH COAD ZACK, GALVANEON HIL DANAEED SHORE OF GALVANEZED STELL WITH SAME MARGED GALVANEZED SHERE GALVANEZED STELL WITH SAME MARGED GALVANEZED SHERE SHORE GALVANE ACTION, AVY SUCH THOUTHAL STELLS IN OT FERMITIED XCEPT WITH THE PRIOR PPROVAL OF THE ENANGERER. VITACTOR TO REMOVE AND RE-INSTALL ALL FIRE PROOFING AS JUNEED DURING COURS INTOCIDION. S TEELE STRUCTURE SHALL BE DESIGNED TO BE SELF-SUPPORTING D STABLE AFTER COMPLETION. IT IS THE CONTRACTORS SOLE SPONSIBILITY TO DETERMINE ERECTION PROCEDURE AND SEQUENCE D TO INSURE THE SAFETY OF THE BUILDING AND ITS COMPONENT TIS DURING ERECTION. NTS DOHING ENECTION. LL STEEL ELEMENTS SHALL BE INSTALLED PLUMB AND LEVEL. DWER MANUFACTURERS DESIGNS SHALL PREVAIL FOR TOWER. NNECTIONS SHALL BE DESIGNED BY THE FABRICATOR AND NSTRUCTED IN ACCORDANCE WITH THE LATEST EDITION OF WUAL OF STEEL CONSTRUCTION". CONNECTIONS SHALL BE DVIDED TO CONFORM TO THE REQUIREMENTS OF TYPE 2 DE THE AIS VUED TO CONFORM TO THE REQUIREMENTS OF TYPE 2 NOTIFICITION NOTIFICITION LOCATES AND ADDRESS AND ADDRESS AND BOATS ALL HAVE NAMMAN AT WORKERS AND BOATS ALL HAVE NAMMAN TWO BOATS LOCK WARKERS AND CONTRECTION ALL HAVE NAMMAN TWO BOATS LOCK WARKERS AND CONTRECTION ALL HAVE NAMMAN TWO BOATS LOCK WARKERS AND CONTRECTION ALL HAVE NAMMAN TWO BOATS LOCK WARKERS AND CONTRECTION ALL HAVE NAMMAN TWO BOATS LOCK WARKERS AND CONTRECTION ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AND

SIGN CONNECTIONS AT BEAM ENDS FOR 10 KIPS (MIN). U-BOLTED CONNECTIONS SHALL BE COMPLETED WITH DOUBLE 'S OR A LOCK WASHER.

IS OR A LOCK WASHER. WRACTOR SHALL COMEY VITH AWS CODE FOR PROCEEDURES. REARANCE AND QUALITY OF WRLIDS, AND WELDING PROCESSES WIF/CATOR PROCEEDURES. MIF/CATOR PROCEEDURES ARCHING DAWAVED GALVARUES SUBJECTS SUBJECTS OF A CAND CARVED AND CARVED AND CARVED AND CARVED WITH AWS. RTIFIED WELDER IN ACCORDANCE WITH AWS. AL ALL PENETRATIONS AND SEAMS BETWEEN MASONRY AND STEEL TH DOW CORNING 780 SILICONE BUILDING SEALANT OR EQUAL.

7 THERMAL & MOISTURE PROTECTION: HESE SPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS

Hele SPACIFICATIONS SHALL INCLUDE THE LEARNED SPECIFICATIONS FERRIN ALL EPSETTATIONS THROUGH BULLENG WAILS, FLOORE NO GELBACS, WITH LISTED AND ACCEPTED MATERIALS TO MANOTAN RE FRE PARTIO OF THE DASING ASSEMELY. ALL HELL MATERIAL HALL BE SHAPED, FITTED, AND PERMANENTLY SECURED IN PLACE. RESTOPHING SHALL BE INSTALLED IN ACCORD WITH ASTME 514. LIT OPEO FILE FOAM OR AN FRE BARRIER PRODUCTS, OR EQUAL, HALL BE USED TO LL ALL VODE AND CAVITIES AND SHALL BE RESTOPHING SHALL BYSTEM INMERGIN AS PRACTICABLE AFTER NEETOPING SHALL BE VERTILED AS SOCIED.

ENETRATIONS ARE MADE AND EQUIPMENT INSTALLED. INSTALLES. INSTALLED. INSTALLED. INSTALLED. INSTALLED. INSTALLES. INSTALLED. INSTALLED. INSTALLED. INSTALLED. INSTALLES. INSTALLED. INSTALL. ARRANGE FOR OWNER INSTALLES. INSTALLED. INSTALL. ARRANGE FOR OWNER INSTALLED. INSTALL. INSTALL. ARRANGE FOR OWNER INSTALLED. INSTALL. INSTALL. ARRANGE FOR OWNER INSTALLED. INSTALL. ARRANGE FOR OWNER, FOR OWNER INSTALLED. INSTALL. INSTALL. ARRANGE FOR OWNER, FOR OWNER INSTALLED. INSTALLED. INSTALL. INSTALLED. INSTALLED. INSTALLED. INSTALL. INSTALLED. INSTALLED. INSTALL. INSTALL. INSTALLED. INSTALLED. INSTALLED. INSTALLED.

LI PENETRATIONS INTO OR THROUGH BUILDING, SHELTER, EQUIPMENT ABINET, AND SIMILAR ENCLOSURE EXTERIOR WALLS, SHALL BE SEALE ITH SILICONE SEALER.

6 ELECTRICAL: SHALL INCLUDE THE GENERAL SPE

'RICAL CONDUCTORS: ATION SHALL BE MINIMUM 600V TYPE THHN, THWN-2, OR

NORW. BRANCH CROLIT COORDUCTORS BIALL BE SOFT DRAWN 99% MINIMUM CONDUCTIVITY PROFERLY REFINED COPPER REEDER GROUT CONDUCTORS ANALL BE ETHER OF COPPER OR REFERRING TO CONDUCTORS ANALL BE ETHER OF COPPER OR PROFENDATION OF THE APPLICATION, OR AS SPRCIPALLY NOTED OFFERMINENTLY LABEL OR TAG ALL CONDUCTORS WITH HER OFFERMINENTLY LABEL OR TAG ALL DECODUCES VIBIL & A PASSI-IFFELICIENT ALL LECADOUCES SPLCIES, AND CONDUT, RACEWAY, WREWAYS, DUCTS, ETC. SHALL BE LISTED 3 SUITABLE FOR THE APPLICATION. ONLY THE FOLLOWING CONDUT: APPROVED AND LISTED FOR THE APPLICATION SHALL BE SEPTABLE:

CEPTABLE: • ELECTRICAL METALLIC TUBING (EMT). • COMPRESSION COUPLINGS AND CONNECTORS ONLY MADE UP WERNCH TIGHT.

WHENCH TIGHT. FLEXIBLE METAL CONDUIT (FMC) AND LIQUIDTIGHT FLEXIBLE METAL CONDUIT (LEMC)

CONDUT (LIMG). FINAL CONVECTIONS TO VIBRATING OR ADJUSTABLE EQUIPMENT INCLUDING, BUT NOT LIMITE DI O, LIGHT EQUIPMENT INCLUDING, BUT NOT LIMITE DI O, LIGHT FINITURES, IN-LO LIMIT, TRANSPORMERS, MOTORA, ETC. OR WHERE INCID AL VINITED STELL, ROSSI ALL IFITTINGS, CONVECTORS, AND COUPLINGS SHALL BE THIERADED MADE LP WIENCH TIGHT. RIGID POLYWINY, COLORDER (PV) SCHEDULE 40 OR SCHEDULE 80. NUMY BE LUSED FOR SERVICES, EXTERIOR, BELOW GRADE, AND WET LOCATIONS.

SHALL NOT BE USED IN CONCRETE SLABS NOR EXPOSED WITHIN A BUILDING OR STRI ICTUPE

ETAL-CLAD CABLE (MC)

BUILDING OR STRUCTURE. • URTAL-CLAD CABLE MO) • ONCEALED INSTALLATIONS ONLY. • UNTEN A DUE WITH SMOOTH OF CORPULATED METAL JACKET AND NO JUTES COLUMN THE METAL MARKET AND NO JUTES COLUMN THE METAL MARKET WE A FINAL CONNECTION TO EQUIPMENT NOT MOUNTED IN CR MARKET FINISH MATTERIAL. INCLAESE CODES THAT BONDS ALL HAVE A SEPARATE OPERLY SIZED AND MARKED GROUNDING CONDUCTOR, PER PLCAELE CODES THAT BONDS ALL HAVE A SEPARATE OPERLY SIZED AND MARKED GROUNDING CONDUCTOR, PER PLCAELE CODES THAT BONDS ALL HAVE A SEPARATE INCLAESE CODES THAT BONDS ALL HAVE A SEPARATE PREVENTION ELISTER SEAS A GROUNDING OF BONDS MOUNTEL. NOT BE LIEDE AS A GROUNDING OF BONDS STRUCTURE. IFT IS TO BE ADDED OF REALACED AS A PART OF THE PREVENTION ELISTER SERVICE IS TO REMAN, CONTRACTOR SHALL EE STRUCTURATION SHALL GREEF FROM, COOREINATE WITH, AND UNIMENT SHALL RES SPECIES FOR AND AS A PREVOED BY THE LOCAL LINY WHERE APPLICABLE. IN I WHERE APPLICABLE. EQUIPMENT, ENCLOSURES, ETC. SHALL BE SUITABLE FOR THE ALLED ENVIRONMENT, MINIMUM NEMA 3R FOR ALL EXTERIOR ALLATIONS.

ALLATIONS. NG DEVICES SHALL BE SPECIFICATION GRADE AND WIRING DEVICE EN PLATES SHALL BE PLASTIC WITH ENGRAVING AS SPECIFIED. OR SHALL BE IVORY. ALL DEVICES AND COVER PLATES SHALL BE NE SAME MANUFACTURER.

HE SAME MANUFACTURER. FIRE-RATED PENETRATIONS SHALL BE SEALED USING A SUITABLE) LISTED FIRE SEALING DEVICE OR GROUT THAT WILL MAINTAIN THE RATING OF THE STRUCTURE PENETRATED. E POLIDO OF THE DIROTHED ENGENDRE ENGENDRED VOIDE PERMANENTLY AFFXED KORGAVED NAMEPLATES FOR ALL DE REQUIRED LABELING AND ON ALL PAVELS, METERING, CONVECTS, AND ELECTRICAL SOURCE WITH A DENTIFIES UIRNENT SERVED, ELECTRICAL SOURCE WITH CIRCUIT NITRICATION, AND VOLTAGES WITHIN.

INTER-ANDING AND VOLTAGES WITHIN. EDITICAL CONTRACTOR IS RESPONSIBLE FOR ALL FINAL MINIATIONS TO ALL EQUIPMENT. ELECTRICAL APPURTENANCES THAT ARE DISCONNECTED SHALL BE ELECTRICAL APPURTENANCES THAT ARE DISCONNECTED SHALL BE MELETELY REMOVED WITH EXISTING STRUCTURES TO REMAIN, AREDE, FINISHER, PLLED, PARTINE, DTC. ALL PARE SCHEDULES, IMPLET LABELING, AND CODE-REQUIRED LABELING, SHALL BE HIED AND APPOREPTLY COMPLETED TO MATCH THE INSTALLATION.

GROUNDING: ERE SPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS

IN. UND ALL SYSTEMS AND EQUIPMENT IN ACCORDANCE WITH BEST ISTRY PRACTICE, THE REQUIREMENTS OF THE NIFPA 70 NATIONAL JURTIONS. CODE (NEO), AND ALL OTHER APPLICABLE CODES AND JUATIONS.

ROUNDING ELECTRODES PRESENT AT EACH SERVICE L BE BONDED TOGETHER TO FORM THE GROUNDING E

HALL BE BOARDED TOGETHER TO FORM THE GROUNDING ELECTROCE STEM. LI COUPRENT ENCLOSURES, DEVICES, AND CONDUITS SHALL BE ROUGHED BY THE INSTALLATION OF A SEPARATE GROUNDING BY CODE ON IS OF THE SZE INXICATED ON THE DRAWINGS, SHALL BE ROUGH CONTINUOUS IN LEARDY AND SHALL NOT BUILDED AS A ROUNDING OF ROUGH CONTINUOUS IN LEARDY AND SHALL AND TE USED AS A GROUNDING OF ROUGH CONTINUOUS IN LEARDY AND SHALL NOT BUILDED AS A GROUNDING OF ROUGHE CONTINUOUS IN LEARDY AND SHALL NOT BUILDED AS A GROUNDING OF ROUGHEL CONTINUES IN SHALL NOT BUILDED AS A GROUNDING OF ROUGHEL CONTINUES IN SHALL NOT BUILDED AS A ROUNDING OF ROUGHEL CONTINUES IN SHALL NOT BUILDED AS A ROUNDING OF ROUGHEL CONTINUES IN SHALL NOT BUILDED AS A ROUNDING OF ROUGHEL CONTINUES IN SHALL NOT BUILDED AS A ROUNDING ROUGHEL CONTINUES IN CONTINUES AND TO AN ROUGHEL CONTINUES TO A GROUNDING DIS SECOFED OR SHALL NOT ROUGHEL CONTINUES TO A GROUNDING DIS CONJULIOTORS INMINIANE RUGHEL CONTINUES TO A GROUNDING DIS CONJULITORS INFORMATIONE RUGHEL ROUNDING AND LOAD SIDE BONDING CONJULITORS SIZE ADOWN THE STANDARD FOR THE ORDING CONJULTORS SIZE ADOWN THE STANDARD FOR THE ORDING CONJULTERS SIZE AD

VICE MAIN BONDING JUMPERS AND GROUNDING ELECTRODE DUCTORS SHALL BE SIZED AND INSTALLED PER THE MINIMUM OF APPLICABLE CODES AND REGULATIONS.

6 LIGHTNING PROTECTION: LIGHTNING FPOTECTION: SE SPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS THE GROUNDING SPECIFICATIONS HEREIN. LIGHTNING PROTECTION GROUNDING SYSTEM (LPGS) SHALL ISIST OF BONDING ALL EQUIPMENT AND CONDUCTIVE STRUCTURES COALUED SINGLE-POINT GROUNDING CONNECTIONS TYPORALLY

ONDUCTORS: - MIN # 2 AVM 0 SOLD JARE TINNED COPPER (BSTC) FOR ALL - MIN # 2 AVM 0 SOLD JOINTON - MIN # 2 AVM 0 SOPERI GREEN STRANDED FOR BOXDING STRUCTURES, AND FOR INTER-SYSTEM BOXDING OF NOWULL LEMENTS SUCH 6 SCRUUD BART 0 GROUND BAR - MIN # A AVM 0 COPPER GREEN STRANDED OR ALL EQUIPMENT BOXDING.

BUNDING. INSTALL ALL IN-GROUND CONDUCTORS IN THE SAME HORIZONTAL PLANE OR IN A DOWNWARD DIRECTION AWAY FROM THE TOWER

FUARE OF IR A DOWNWARD DIRECTION AWAY FROM THE TOWER AND EGUIPHENT AREAS. • AVOID LONG FUAS. MAKE DIRECT RUNS 6.8 MUCHAS POSSIBLE • THORAN FUAS POSSIBLE CONTRACT AND A STRUCTURE THEORIGAN FUAS STRUCTURE CONTRACT WITH A STRUCTURE MAKE ALL CONNECTIONS IN CONTACT WITH EARTH WITH EXCITI FERMOWERLING. MAKE LLO THER CONNECTIONS WITH CONNECTORS. ON LOSS AND SMILLA OTHER CONNECTIONS SMILL BE HORECONT. OR LOSS AND SMILLA OTHER CONNECTIONS SMILL BE HORECONT. OR LOSS AND SMILLA OTHER CONNECTIONS SMILL BE HORECONT. OR LOSS AND SMILLA OTHER CONNECTIONS SMILL BE HORECONT. OR DOWNOOD CONNECTION TOWARD EARTH.

BE HORZORIAL, ON DOWNWARD TOWARDS EARTH. ALL CONDUCTORS PASSING FROM ABOVE-GROUND TO IN-GROUNE CONNECTIONS, WHERE EXPOSED, SHALL BE COVERED AND PROTECTED WITH A NON-METALLIC CONDUIT SEALED AT BOTH ENDS.

ENDS. IF 2 OR MORE IN-GROUND CONDUCTOS ARE IN THE SAME PATH (2 2000 CUTCH ADDING FOILLOWING ANOTHER RING OR RINGS OVERLAPPING, BONDING FOLLOWING ANOTHER F RADIAL, OR SIMILAR), COMBINE WITH A SHARED SINGLE

IENT AND TOWER GROUND BINGS SHALL BE ALL INTERVIENT AND LAVERY AND ANNUAL DESIGNAL DESIGNAL DESIGNAL ANN CONDUCTIVE COLLECT ON STRUCTURE WITHIN 5 FEET OF EQUIPMENT GROUND RINGS AND WITHIN 20 FEET OF TOWER GROUND RINGS. • INSTALLED MINIMUM 18 INDHES FROM FOUNDATIONS, FOOTINGS, AND SIMULAR.

ALL IN-GROUND RINGS, RADIALS, BONDS CONNECTING THEM

ID ALL SIMILAR GROUNDING: • UNI 30 INCHES BELOW GRADE, OR 6 INCHES BELOW THE FROST LINE, WHICHEVER IS GREATER DEFTH. • UNI 2 FEET FROM FOUNDATIONS, FOOTNAS, OTHER GROUNDING SYSTEMS, AND SIMILAR STRUCTURES, EXCEPT WHEN MAKING A EOND TO ANY OF THESE STRUCTURES, EXCEPT WHEN MAKING A

FOR INSTALLED DIRECT LEL TO THE IN-GROUNI

> I TOWER LEG SHALL BE BONDED TO ITS RING. SINGLE-LEGGI ERS. OR MONOPOLES. SHALL HAVE 2 BONDS ON OPPOSITE SIDES. BOND TO TOWER BASE, NOT TO VERTICAL TOWER STRUCTURE, AWAY FROM TOWER MOUNTING HARDWARE. EACH BOND SHALL HAVE A CORRESPONDING GROUND ROD ON THI

RING. • ACH BOND SHALL CONSIST OF 2 CONDUCTORS FROM THE TOWER TO ITS RING WITH EACH CONDUCTOR DIRECTED IN OPPOSITE DIRECTIONS WITH A PARALLEL CONNECTION ON THE RING ON OPPOSITE SIDES OF THE GROUND ROD.

V. VATIONS FOR FOOTINGS SHALL BE CUT LEVEL TO THE REQUIREE IT AND TO UNDISTURBED SOIL. REPORT UNSUITABLE SOIL DITIONS TO THE CONSTRUCTION MANAGER NCH EXCAVATIONS SHALL BE BACKELLED AT THE END OF EACH

EXCAVATION & FILL

-45% WITH PASS #10 25% WITH PASS #40 10% WITH PASS #100

NOLLIDE THE GENERAL SPEC

THEN: UTRACTOR SHALL GRADE ONLY AREAS SHOWN TO BE MODIFIED IT OF THES WORK AND ONLY TO THE EXTENT FEQUIRED TO SHED IF, AND WATER LOW AWAY FROM SITE. ALL MADE SLOPES SHO IE STEEPER THAN 31 (HORIZONTAL-VERTICAL) SEDMENTATIO 1 EPOSION CONTROLS SHOWN AND SEPCIFIED SHALL BE ABLISHED BEFORE STRIPPING EXISTING VEGETATION.

ANIC MATERIAL AND DEBRIS SHALL BE STRIPPED AND STOCKPILED IRE ADDING FILL MATERIAL.

UNE ADDING FILL MATERIAL. FILL OR EMBANKMENT MATERIAL SHALL BE PLACED ON FROZEN UND. FROZEN MATERIALS, SNOW OR ICE SHALL NOT BE PLACED I FILL OR EMBANKMENT.

FILL SHALL BE PLACED IN ONE FOOT LIFTS AND COMPACTED IN 2E. STRUCTURAL FILL SHALL BE COMPACTED TO 95% OF ITS MUM DRY UNIT WEIGHT TESTED IN ACCORDANCE WITH ASTM

. ER FOUNDATION EXCAVATION, BACKFILL AND COMPACTION SH N ACCORDANCE WITH TOWER MANUFACTURER'S DESIGNS AND SIFICATIONS

VIC OR CRUSHED GRAVEL SHALL CONSIST OF TOUGH, DURABLE TRICLES OF CRUSHED GRAVEL SHALL CONSIST OF TOUGH, DURABLE TRICLES OF CRUSHED GRAVEL SHALL SHALL

DATION. CESSED AGGREGATE BASE SHALL CONSIST OF COURSE AND FINE REGATES COMBINED AND MIXED SO THAT THE RESULTING

GREGATES COMBINED AND MIXED SO THAT THE RESULTING TERAL CONFORMS TO THE GRADUITS. COURSE AGGREGATE SHALL EITHER GRAVEL OR BROKEN STONE AND FINE AGGREGATE SHALL INSIST OF SAND. NIK GRAVEL FILL SHALL PASS WITH THE FOLLOWING SIZE SQUARE SH SIEVES: 5-00% WITH FASS 1/8' -5-0% WITH FASS 1/8'

K GRAVEL BASE SHALL PASS WITH THE FOLLOWING SIZE SQUARE

DIRECTIONS WITH A PARALLEL CONNECTION ON THE RING ON OPPOSITS DESC IN THE GROUND ROD. CURPACIENT AREA CROUNDING: CURPACIENT AREA CROUNDING: DESCRIPTION AND ADDRESS AND ADDRESS AND ADDRESS SERVICE AND ADDRESS AND ADDRESS AND ADDRESS SERVICE AND ADDRESS AND ADDRESS AND ADDRESS ADDRESS AND ADDRESS AN

BONDS, KND SMILAR. A COMMON PRATICE IS TO PLACE 4 RADALS FROM THE TOWER RING TO THE 4 CORNERS OF THE AVAILABLE AREA. INIMIMUM, BOND ALL COMPOUND CONDUCTIVE FERCE CORNER TS AND GATE POSTS TO THE LPGS. PREFERABLY, INSTALL A UND RING THAT FOLLOWS THE FERCE LINE, BONDING ALL CORSTS TO

ANTENNAS & CABLES: SESPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS

SEED. CONTRACT LOSS SINGLE INCLUEE INE CIRCUME DE CONTRACTOR SINGLE INCLUEE INCLUEE INCLUEENT ADDRESSIONS SINGLES, JUMPERS, CONNECTORS, GROUNDING STRAPS, ANTENNAS, BLES, JUMPERS, CONNECTORS, GROUNDING STRAPS, ANTENNAS, INST AND HARDWARE ALL MATERIALS SHALL BE INSPECTED BY THE INTRACTOR FOR DAMAGE UPON DELIVERY, JUMPERS SHALL BE PHELD AT INTERVIEW OF AN EXPECTIVE STRAPS TO A INSPECT AND AND ADDRESSION SINGLESS AND ADDRESS AND ADDR

ENNA CABLES SHALL BE UNIQUELY COLOR-CODED AT THE ENNAS, BOTH SIDES OF EQUIPMENT SHELTER WALL, AND JUMPER ILES AT THE EQUIPMENT.

BLES AT THE EQUIPMENT. E CONTRACTOR SHALL FURNISH AND INSTALL ALL CONNECTORS, SOCIATED CABLE MOUNTING AND GROUNDING HARDWARE, WALL UNITS, STANDOFFS, AND ALL ASSOCIATED HARDWARE TO INSTALL C CABLES AND ANTENNAS TO THE MANUFACTURERS AND OWNERS

NNA CABLES SHALL BE FOAM DIELECTRIC COAXIAL CABLES AS

LLUWS: = PASE STATION ANTENNAS: = 7.8° DIAMETER FOR CABLE LENGTHS UP TO 100 FT. = 1-3° DIAMETER FOR CABLE LENGTHS GREATER THAN 100 FT. = 7.8° DIAMETER FOR CABLE LENGTHS UP TO 200 FT. = 1-3° DIAMETER FOR CABLE LENGTHS GREATER THAN 200 FT.

DING RADIUS FOR COAXIAL CABLES SHALL BE:

 15 FT FOR 7/8" COAXIAL CABLES.
 25 FT FOR 1-5/8" COAXIAL CABLES. LE SHALL ER INSTALLED WITH A MINIMUM NUMBER OF BENDS 3/E POSSIBLE. CABLE SHALL NOT BE LEFT UNTERMINATED AND 1. BE SALED MIMEDIATELY ATTER BEING INSTALLED. 2/TERICG CABLE CONVECTIONS SHALL BE COVERED WITH A EMPRICIS FLUGNG NT.

TRACTOR SHALL VERIFY EXACT LENGTH AND DIRECTION OF TRAVEL 3LD PRIOR TO CONSTRUCTION

E SHALL BE FURNISHED AND INSTALLED WITHOUT SPLICES AND I CONNECTORS AT EACH END. CABLE TRAY:

SE SPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS ILE TRAY SHALL BE MADE OF EITHER CORROSION RESISTANT METAL WITH A CORROSION RESISTANT FINISH.

BLE TRAY SHALL BE OF LADDER TRAY MPED TO SIDE RAILS. TYPE WITH FLAT COVER 3LE LADDER SHALL BE SIZED TO FIT ALL CABLES IN ACCORDANCE 'H NEC AND NEMA 11-15-84.

E LADDER TRAYS SHALL BE NEMA CLASS 12A BY PW INDUSTRIES, OR EQUAL.

ILE LADDER TRAY SHALL BE SUPPORTED IN ACCORDANCE WITH

. WORKWANSHIP SHALL CONFORM TO THESE REQUIREMENTS AND . LOCAL CODES AND STANDARDS TO ENSURE SAFE AND ADEQUATE JUNDING SYSTEM.

 bank
 <td PASS WITH THE FOLLOWING SIZE SQUARE
 SBH SIEVES:

 0-100%
 WITH PASS 3-1/2"

 5-95%
 WITH PASS 1-1/2"

 0-75%
 WITH PASS 3/4"

 5-45%
 WITH PASS 1/4"

 -20%
 WITH PASS #40

 -12%
 WITH PASS #100
 RIAL SHALL BE FREE OF ORGANIC MATERIAL, ICE, TRASH AND EFER TO GEOTECHNICAL ENGINEERING AS APPLICABLE FOR IATERIAL REQUIREMENTS. SEDIMENTATION & EROSION CONTROL:

NELIMIENT ALL ONSTITUCT. LL SEDMENT AND EROSION TROLEN NACCORRANCE WITH THE 2020 CONNECTICUT GUIDELINES NACCORRANCE WITH THE 2020 CONNECTICUT GUIDELINES ORDANCE WITH THE CONTRACT DOQUMENTS AND AS DIFECTE DATA TERMS PUMP DISCHARCE TO A SEDMENT CONTROL DIRECT ALL EMPORANY SEDMENT TRAPS OR GRASS FLICTERS WITHIN THE EMPORANY SEDMENT TRAPS OR GRASS FLICTERS WITHIN THE EMPORANY SEDMENT TRAPS OR GRASS SHALL BE CLEAR AND OVEL DINT OF DIMENENT IESE SPECIFICATIONS SHALL INCLUDE THE GENERAL SPECIFICATIONS

EN. TRACTOR SHALL MINIMIZE DISTURBANCE TO EXIST. SITE DURING ISTRUCTON, EROSION CONTROL MEASURES, IF REQUIRED DURING ISTRUCTON, SHALL BE IN CONFORMANCE WITH THE LOCAL SELINES FOR EROSION AND SEDIMENTATION CONTROL TS OF CLEARING AND GRUBBING SHALL BE CLEARLY MARKED ORE COMMENDING WITH SUCH WORK.

UNE DEVINE TRANSISTER OF THE DEVINE OF THE DEVINE AND A DEVINE THE DEVINE OF THE DEVIN

S THE CONTRACTOR'S RESPONSIBILITY TO MAINTAIN SEC MEASURES ROUGHOUT DURATION OF PROJECT UNTIL DISTURBED LAND IS OROUGHLY VEGETATED

HARDOARD V YEGETANED HARDOARD V SEGETANED ALLIEG OT HE SEG SYSTEMS SHALL BE CORPECTED MAREDATELY ND SUPPLEMENTED WTH ADDITIONAL MEASINES AS NEEDED. OF SOLS SHALL BE STARLISHED STRAW MALCH, JUTE NETMS STRANSFER STRAES ARE ESTARLISHED STRAW MALCH, JUTE NETMS STRANSFER STRAES AND STRANSFER AND STRANSFER AND STRANSFER STRANSFER STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER AND STRANSFER AND STRANSFER STRENSFER AND STRANSFER AND STRANSFER



