

November 22, 2016

Melanie A. Bachman  
Acting Executive Director  
Connecticut Siting Council  
10 Franklin Square  
New Britain, CT 06051

**RE: Notice of Exempt Modification for T-Mobile / L700 Crown Site BU: 841289**  
**T-Mobile Site ID: CT11035E**  
**Located at: 170 Ingham Hill Road, Old Saybrook, CT 06475**  
**Latitude: 41° 18' 35.55"/ Longitude: -72° 23' 51.13"**

Dear Ms. Bachman,

T-Mobile currently maintains an omnidirectional canister antenna at the 163-foot level of the existing 150-foot monopole tower located at 170 Ingham Hill Road, Old Saybrook, CT. The tower is owned by Crown Castle. The property is owned by Carlo and Robert Lorenz. T-Mobile now proposes to remove the existing antenna. They will then install nine (9) new antennas on a new mount at the 140-foot level. They also propose to install three (3) remote radio units (non-antennas), three (3) TMAs, and one (1) hybrid fiber cable. The existing cables will be relocated to the new 140-foot level. All work is to be completed within the existing area.

This facility was approved by the Connecticut Siting Council on September 26, 1985 in Docket No. 51.2. The approval contained the following conditions.

1. The tower shall be no taller than necessary to provide the proposed service, and in no event shall exceed 150'.
2. A fence not lower than eight feet shall surround each tower and its associated equipment building;
3. The applicant or its successor shall notify the Council if and when directional antennas or any other equipment is added to any of these facilities;

4. The applicant or its successor shall permit, in accordance with representations made by it during the proceeding, public or private entities to share space on the facilities, for due consideration received, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing;
5. The facilities shall be constructed in accordance with all applicable federal, state, and municipal laws and regulations;
6. The applicant shall submit a development and management plan (D&M) for the Old Saybrook site pursuant to sections 16-50j-75 through 16-50j-77 of the regulations of state agencies, except that irrelevant items in section 16-50j-76 need only be identified as such. The D&M plan shall include erosion control measures, reseeding plans, and tree removal plans. The applicant shall comply with the reporting requirements of sections 16-50j-77 for both sites;
7. Construction activities shall take place during daylight working hours;
8. This decision and order shall be void and new the towers and associated equipment approved herein shall be dismantled and removed, or reapplication for any such new use shall be made to the Connecticut Siting Council before any such new use is made, if the towers do not provide or permanently cease to provide cellular service following completion of construction.
9. This decision and order shall be void if all construction authorized is not complete within three years of the issuance of this decision.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies §16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. §16-50j-72(b)(2). In accordance with R.S.C.A. § 16-50j-73, a copy of this letter is being sent to Mr. Carl Fortuna, Jr., First Selectman for the Town of Old Saybrook, as well as the property owner and the tower owner.

1. The proposed modifications will not result in an increase in the height of the existing tower.
2. The proposed modification will not require the extension of the site boundary.
3. The proposed modification will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.

4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communication Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, T-Mobile respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitutes an exempt modification under R.C.S.A. § 16-50j-72(b)(2). Please send approval/rejection letter to Attn: Amanda Goodall.

Sincerely,



Amanda Goodall

Real Estate Specialist

12 Gill Street, Suite 5800, Woburn, MA 01801

339-205-7017

[Amanda.Goodall@crowncastle.com](mailto:Amanda.Goodall@crowncastle.com)

Attachments:

Tab 1: Exhibit-1: Compound plan and elevation depicting the planned changes

Tab 2: Exhibit-2: Structural Modification Report

Tab 4: Exhibit-3: General Power Density Table report (RF Emissions Analysis Report)

cc: First Selectman Carl Fortuna, Jr.

Town of Old Saybrook

302 Main Street

Old Saybrook, CT 06475

Melanie A. Bachman

November 22, 2016

Page 4

Crown Castle (Tower Owner)

12 Gill Street, Suite 5800

Woburn, Ma 01801

Carol Lorenz (Property Owner)

PO BOX 351

CENTER OSSIPEE, NH 03814

DOCKET NO. 51

AN APPLICATION SUBMITTED BY THE SOUTHERN : CONNECTICUT SITING  
NEW ENGLAND TELEPHONE COMPANY FOR A :  
CERTIFICATE OF ENVIRONMENTAL COMPATIBILITY : COUNCIL  
AND PUBLIC NEED FOR THE CONSTRUCTION, :  
MAINTENANCE, AND OPERATION OF FACILITIES :  
TO PROVIDE CELLULAR SERVICE IN HARTFORD :  
AND MIDDLESEX COUNTIES. : September 26, 1985

D E C I S I O N A N D O R D E R

Pursuant to the foregoing opinion, the Council hereby directs that a certificate of environmental compatibility and public need as required by section 16-50k of the General Statutes of Connecticut be issued to Southern New England Telephone Company (SNET) for the construction, operation, and maintenance of a telecommunications tower and associated equipment building to provide cellular service at sites in Old Saybrook and Enfield, Connecticut.

The facilities shall be constructed, operated, and maintained as specified in this matter, and subject to the following conditions:

1. The towers shall be no taller than necessary to provide the proposed service, and in no event shall exceed
  - a) 150' at the Old Saybrook site; and
  - b) 150' at the Enfield site;
2. A fence not lower than eight feet shall surround each tower and its associated equipment building;
3. The applicant or its successor shall notify the Council if and when directional antennas or any other equipment is added to any of these facilities;
4. The applicant or its successor shall permit, in accordance with representations made by it during the proceeding, public or private entities to share space on the facilities, for due

consideration received, or shall provide any requesting entity with specific legal, technical, environmental, or economic reasons precluding such tower sharing;

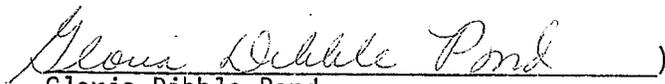
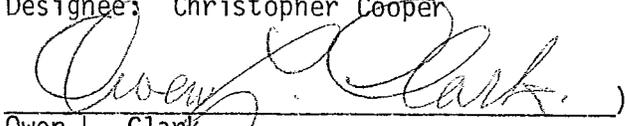
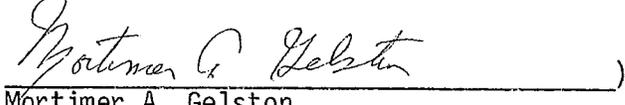
5. The facilities shall be constructed in accordance with all applicable federal, state, and municipal laws and regulations;
6. The applicant shall submit a development and management plan (D&M) for the Old Saybrook site pursuant to sections 16-50j-75 through 16-50j-77 of the regulations of state agencies, except that irrelevant items in section 16-50j-76 need only be identified as such. The D&M plan shall include erosion control measures, reseeding plans, and tree removal plans. The applicant shall comply with the reporting requirements of section 16-50j-77 for both sites;
7. Construction activities shall take place during daylight working hours;
8. This decision and order shall be void and the towers and associated equipment approved herein shall be dismantled and removed, or reapplication for any new use shall be made to the Connecticut Siting Council before any such new use is made, if the towers do not provide or permanently cease to provide cellular service following completion of construction;
9. This decision and order shall be void if all construction authorized is not completed within three years of the issuance of this decision.

Pursuant to section 16-50p of the General Statutes, we hereby direct that a copy of the opinion and decision and order be served on each person listed below. A notice of the issuance shall be published in the

C E R T I F I C A T I O N

The undersigned members of the Connecticut Siting Council hereby certify that they have heard this case or read the record thereof, and that we voted as follows:

Dated at New Britain, Connecticut, this 26th day of September, 1985.

<u>Council Members</u>	<u>Vote Cast</u>
 Gloria Dibble Pond Chairperson	Yes
_____ Commissioner John Downey Designee: Commissioner Peter G. Boucher	Absent
 Commissioner Stanley Pac Designee: Christopher Cooper	Yes
 Owen L. Clark	Yes
 Mortimer A. Gelston	Yes
 James G. Horsfall	Yes
 Pamela B. Katz	Yes
 William H. Smith	Yes
_____ Colin C. Tait	Absent

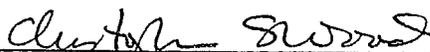
STATE OF CONNECTICUT  
COUNTY OF HARTFORD

)  
:  
)

ss. New Britain, September 26, 1985

I hereby certify that the foregoing is a true and correct copy of the decision and order issued by the Connecticut Siting Council, State of Connecticut.

ATTEST:

  
\_\_\_\_\_  
Christopher S. Wood, Executive Director  
Connecticut Siting Council

# 170 INGHAM HILL RD

**Location** 170 INGHAM HILL RD

**MBLU** 051/ 033/ / /

**Acct#** 00559800

**Owner** LORENZ CAROL J & ROBERT  
A

**Assessment** \$164,300

**Appraisal** \$285,500

**PID** 3322

**Building Count** 1

## Current Value

Appraisal			
Valuation Year	Improvements	Land	Total
2015	\$145,700	\$139,800	\$285,500
Assessment			
Valuation Year	Improvements	Land	Total
2015	\$102,000	\$62,300	\$164,300

## Owner of Record

**Owner** LORENZ CAROL J & ROBERT A

**Sale Price** \$0

**Co-Owner**

**Certificate**

**Address** P O BOX 351

**Book & Page** 0211/0890

CENTER OSSIPEE N H, NH 03814-0351

**Sale Date** 03/15/1984

## Ownership History

Ownership History				
Owner	Sale Price	Certificate	Book & Page	Sale Date
LORENZ CAROL J & ROBERT A	\$0		0211/0890	03/15/1984

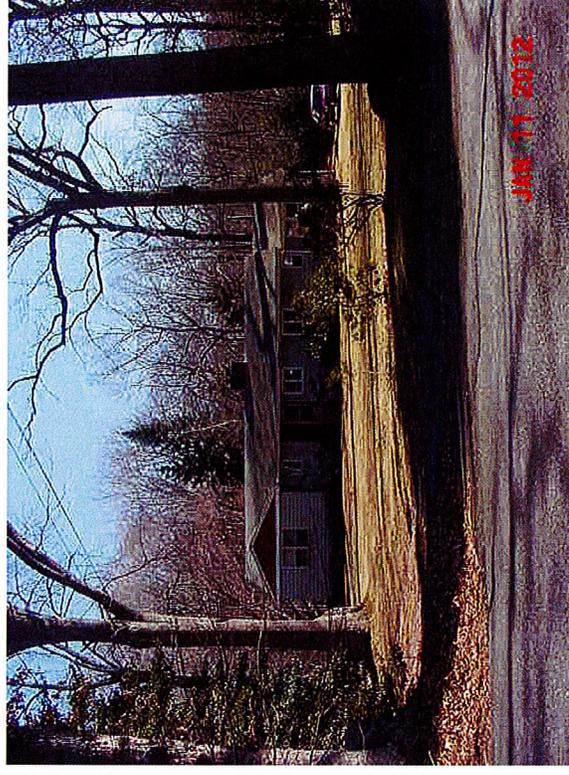
## Building Information

### Building 1 : Section 1

**Year Built:** 1959  
**Living Area:** 1,383

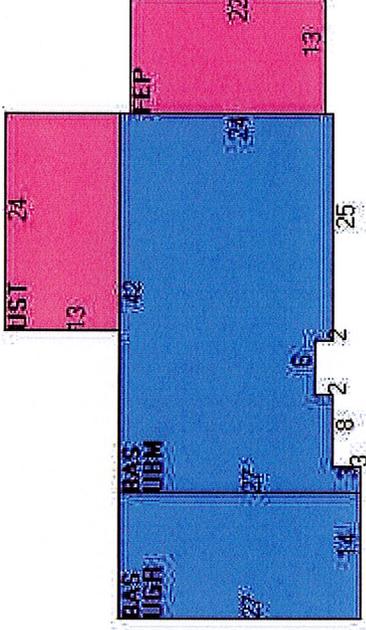
Building Attributes	
Field	Description
Style	Ranch
Model	Residential
Stories:	1 Story
Occupancy	1
Exterior Wall 1	Wood Shingle
Exterior Wall 2	
Roof Structure:	Gable/Hip
Roof Cover	Asph/F Gls/Cmp
Interior Wall 1	Plastered
Interior Wall 2	
Interior Flr 1	Viny//Asphalt
Interior Flr 2	

### Building Photo



(<http://images.vgsi.com/photos/OldSaybrookCTPhotos//\00\01>)

### Building Layout



Heat Fuel	Oil
Heat Type:	Hot Water
AC Type:	None
Total Bedrooms:	3 Bedrooms
Total Bthrms:	1
Total Half Baths:	1
Total Rooms:	6 Rooms

Building Sub-Areas (sq ft)		Legend	
Code	Description	Gross Area	Living Area
BAS	First Floor	1,383	1,383
FEP	Porch, Enclosed, Framed	286	0
UBM	Basement, Unfinished	1,005	0
UGR	Garage, Unfinished	378	0
UST	Utility, Storage, Unfinished	312	0
		3,364	1,383

### Extra Features

### Extra Features

### Legend









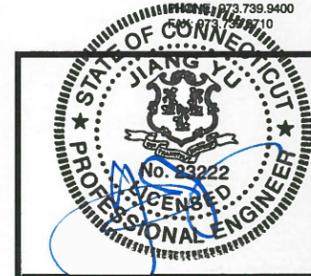
**CT11035E  
OLD SAYBROOK**

**CONSTRUCTION DRAWINGS**

0 11/22/16 ISSUED AS FINAL  
A 11/02/16 ISSUED FOR REVIEW

**Dewberry**

Dewberry Engineers Inc.  
600 PARSIPPANY ROAD  
SUITE 301  
PARSIPPANY, NJ 07054  
PHONE: 973.739.9400



JIANG YU, P.E.  
CONNECTICUT LICENSE NO. 0023222  
IT IS A VIOLATION OF LAW FOR ANY PERSON, UNLESS THEY ARE ACTING UNDER THE DIRECTION OF A LICENSED PROFESSIONAL ENGINEER TO ALTER THIS DOCUMENT.

DRAWN BY: JC

REVIEWED BY: BSH

CHECKED BY: GHN

PROJECT NUMBER: 50066258

JOB NUMBER: 50078136

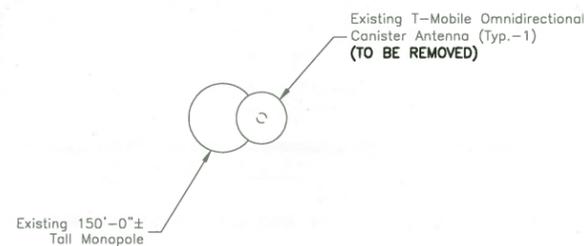
SITE ADDRESS:

170 INGHAM HILL ROAD  
OLD SAYBROOK, CT 06475  
MIDDLESEX COUNTY

SHEET TITLE

ANTENNA LAYOUTS &  
ELEVATIONS

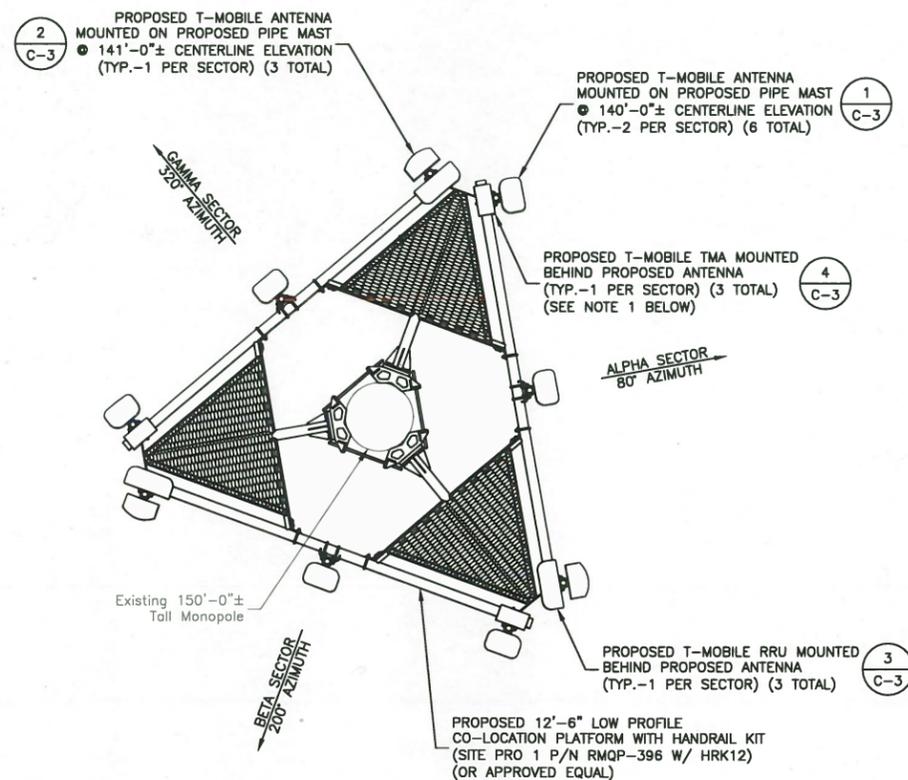
SHEET NUMBER



**EXISTING ANTENNA LAYOUT**

SCALE: N.T.S.

1



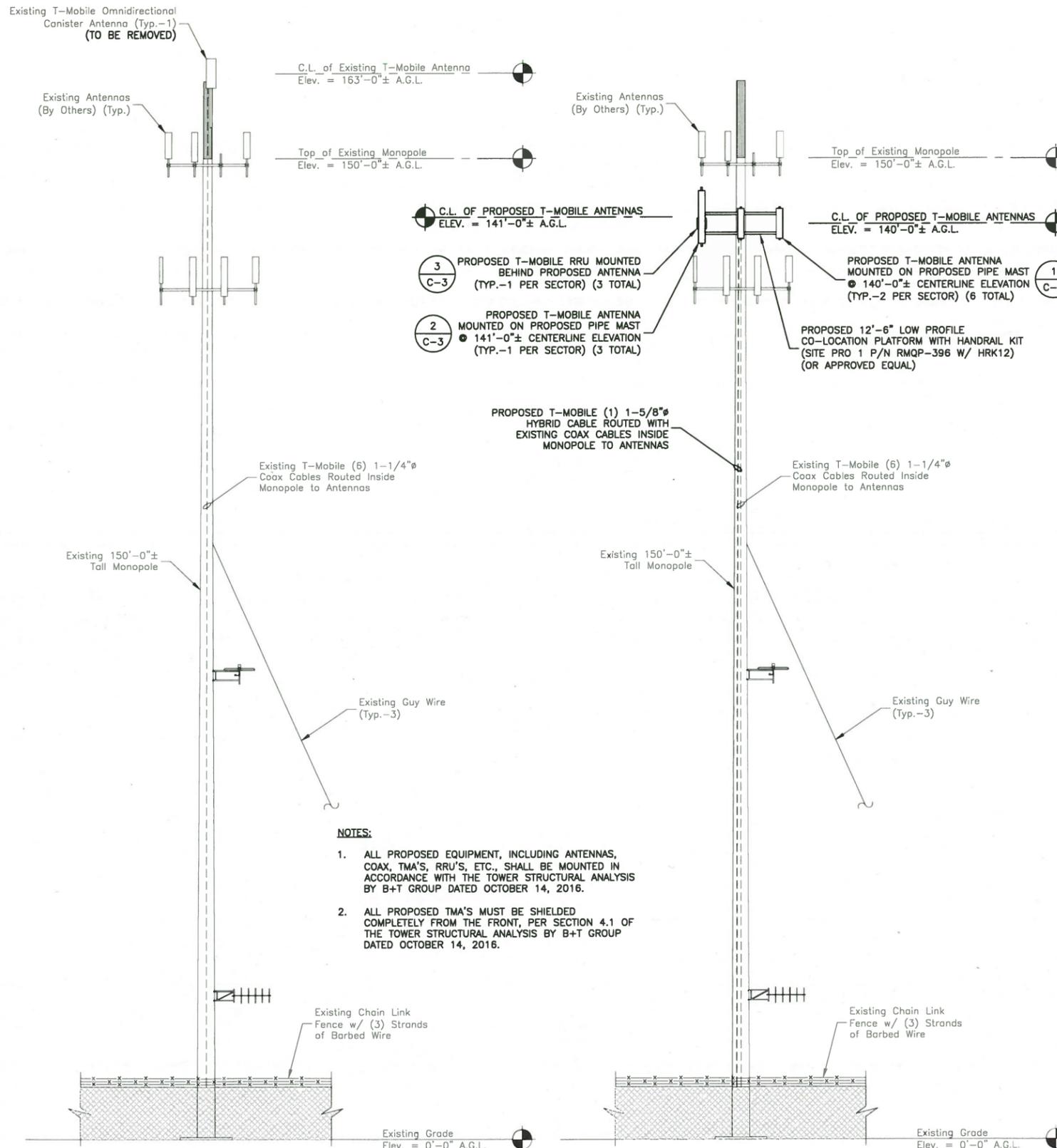
**PROPOSED ANTENNA LAYOUT**

SCALE: N.T.S.

2

**NOTE:**

- ALL PROPOSED TMA'S MUST BE SHIELDED COMPLETELY FROM THE FRONT, PER SECTION 4.1 OF THE TOWER STRUCTURAL ANALYSIS BY B+T GROUP DATED OCTOBER 14, 2016.



**NOTES:**

- ALL PROPOSED EQUIPMENT, INCLUDING ANTENNAS, COAX, TMA'S, RRU'S, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS BY B+T GROUP DATED OCTOBER 14, 2016.
- ALL PROPOSED TMA'S MUST BE SHIELDED COMPLETELY FROM THE FRONT, PER SECTION 4.1 OF THE TOWER STRUCTURAL ANALYSIS BY B+T GROUP DATED OCTOBER 14, 2016.

**EXISTING ELEVATION**

SCALE: 1"=20' FOR 11"x17"  
1"=10' FOR 22"x34"



3

**PROPOSED ELEVATION**

SCALE: 1"=20' FOR 11"x17"  
1"=10' FOR 22"x34"



4







October 14<sup>th</sup>, 2016

Sean Dempsey  
Crown Castle  
3530 Toringdon Way Suite 300  
Charlotte, NC 28277  
(704) 405-6565

B+T Group  
1717 S. Boulder, Suite 300  
Tulsa, OK 74119  
(918) 587-4630  
btwo@btgrp.com

**Subject:** Structural Analysis Report

**Carrier Designation:** *T-Mobile Co-Locate*  
**Carrier Site Number:** CT11035E  
**Carrier Site Name:** Old Saybrooksnetmobiliti\_1

**Crown Castle Designation:**  
**Crown Castle BU Number:** 841289  
**Crown Castle Site Name:** Old Saybrook  
**Crown Castle JDE Job Number:** 397965  
**Crown Castle Work Order Number:** 1305063  
**Crown Castle Application Number:** 362261 Rev. 1

**Engineering Firm Designation:** B+T Group Project Number: 93496.006.01

**Site Data:** 170 Ingham Hill Road, Old Saybrook, Middlesex County, CT  
Latitude 41° 18' 35.55", Longitude -72° 23' 51.13"  
150 Foot - Monopole Tower

Dear Sean Dempsey,

B+T Group is pleased to submit this “**Structural Analysis Report**” to determine the structural integrity of the above mentioned tower. This analysis has been performed in accordance with the Crown Castle Structural ‘Statement of Work’ and the terms of Crown Castle Purchase Order Number 953486, in accordance with application 362261, revision 1.

The purpose of the analysis is to determine acceptability of the tower stress level. Based on our analysis we have determined the tower stress level for the structure and foundation, under the following load case, to be:

LC7: Existing + Reserved + Proposed Equipment **Sufficient Capacity\***  
Note: See Table 1 and Table 2 for the proposed and existing/reserved loading, respectively.

**\*The structure has sufficient capacity once the loading condition specified in Section 4.1 has been satisfied.**

This analysis has been performed in accordance with the 2016 Connecticut State Building Code based upon an ultimate 3second gust wind speed of 135 mph converted to a nominal 3second gust wind speed of 105 mph per Section 1609.3 as required for use in the TIA222G Standard per Exception #5 of Section 1609.1.1. Exposure Category B and Risk Category II were used in this analysis.

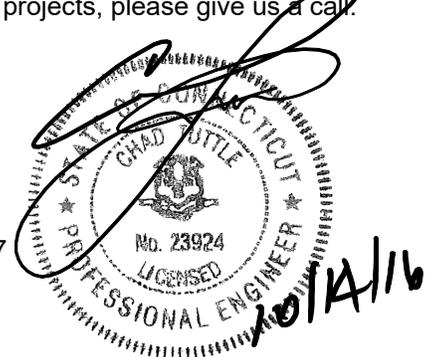
All equipment proposed in this report shall be installed in accordance with the attached drawings for the determined available structural capacity to be effective.

We at B+T Group appreciate the opportunity of providing our continuing professional services to you and Crown Castle. If you have any questions or need further assistance on this or any other projects, please give us a call.

Respectfully submitted by:  
B+T Engineering, Inc.

Tharun Cheriyan  
Project Engineer

Chad E. Tuttle, P.E.  
Engineer of Record  
COA: PEC.0001564 Expires: 02/10/2017



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tnxTower Output

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## 1) INTRODUCTION

This tower is a 150 ft. monopole designed by Engineered Endeavors, Inc. in June of 1998. The tower was originally designed for a wind speed of 85 mph per TIA/EIA-222-E. The tower has been modified multiple times and those modifications were incorporated in this analysis.

## 2) ANALYSIS CRITERIA

The structural analysis was performed for this tower in accordance with the requirements of TIA-222-G Structural Standards for Steel Antenna Towers and Antenna Supporting Structures using a 3-second gust wind speed of 105 mph with no ice, 50 mph with 0.75-inch ice thickness and 60 mph under service loads, exposure category B with topographic category 1 and crest height of 0 feet.

**Table 1 - Proposed Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
140.0	141.0	3	Andrew	LNX-6515DS-A1M	1	1-5/8	--
	140.0	3	Commscope	TMAT7LA-11A			
		3	Ericsson	AIR 21 B2A/B4P			
		3	Ericsson	AIR 21 B4A/B2P			
		3	Ericsson	RRUS 11 B12			
		1	--	RMQP-396 W/ HRK12			

**Table 2 - Existing and Reserved Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
160.0	163.0	1	Andrew	CSHAX-6516-R2	--	--	4
	160.0	1	--	Pipe Mount [PM 701-1]			
149.0	156.0	1	Andrew	KP4F-23A	--	--	1
	152.0	3	Andrew	SBNHH-1D65A	2	5/8	2
		1	Raycap	DC6-48-60-18-8F			
		3	Ericsson	WCS RRUS-32-B30			
		2	Kmw Comm.	AM-X-CD-14-65-00T-RET			
		1	Kmw Comm.	AM-X-CW-14-65-00T-RET			
	6	Powerwave Tech.	TT19-08BP111-001	12	1-1/4	7/8	
	3	Powerwave Tech.	7770.00				
149.0	1	--	Platform Mount [LP 403-1]				
148.0	150.0	6	Ericsson	RRUS 11	2	5/8	1
	148.0	1	--	Side Arm Mount [SO 102-3]			
	147.0	1	Raycap	DC6-48-60-18-8F			
140.0	140.0	--	--	--	6	1-1/4	3
130.0	133.0	3	alcatel lucent	RRH2X60-AWS	12	1-1/4	1
		3	Alcatel Lucent	RRH2X60-PCS			
		3	Antel	BXA-171085-8BF-EDIN-0			
		3	Antel	BXA-80080/4CF			
		3	Commscope	HBXX-6517DS-A2M			

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)	Note
		3	Commscope	LNx-6514DS-A1M			
		1	Rfs Celwave	DB-T1-6Z-8AB-0Z			
		6	Rfs Celwave	FD9R6004/2C-3L			
		1	--	Platform Mount [LP 403-1]			
71.0	72.0	1	Kathrein	FMO	1	1/2	1
	71.0	1	--	Side Arm Mount [SO 301-1]			
22.0	22.0	1	Maxrad	MYA-43012N	1	5/16	1
		1	--	Side Arm Mount [SO 701-1]			

Notes:

- 1) Existing Equipment
- 2) Reserved Equipment
- 3) Coax To Be Relocated from 160'; Considered in This Analysis
- 4) Equipment To Be Removed; Not Considered in This Analysis

**Table 3 - Design Antenna and Cable Information**

Mounting Level (ft)	Center Line Elevation (ft)	Number of Antennas	Antenna Manufacturer	Antenna Model	Number of Feed Lines	Feed Line Size (in)
158	158	1	Ems Wireless	TRR90-17	--	--
150	150	12	Allgon	7120.16	--	--
140	140	12	Allgon	7120.16	--	--
130	130	12	Allgon	7184.05	--	--
120	120	12	Allgon	7184.05	--	--

**3) ANALYSIS PROCEDURE**

**Table 4 - Documents Provided**

Document	Remarks	Reference	Source
Online Application	T-Mobile, Co-Locate Re# 1	362261	CCI Sites
Tower Manufacturer Drawings	EEL, Job No. 3503	4287398	CCI Sites
Tower Mapping	ReliaPOLE, Project No. 14-0703NEd	5204147	CCI Sites
Tower Modification Drawings	GPD, Date: 10/02/2008	4489382	CCI Sites
Post Modification Inspection	GPD, Date:03/04/2009	4489415	CCI Sites
Tower Modification Drawings	GPD, Date:12/15/2011	4478711	CCI Sites
Post Modification Inspection	HDG, Date: 03/19/2012	4468635	CCI Sites
Tower Modification Drawings	B+T Group, Date: 08/20/2015	5293057	CCI Sites
Post Modification Inspection	SGS, Date: 09/01/2015	5874000	CCI Sites
Tower Modification Drawings	B+T Group, Date: 05/06/2016	6254746	CCI Sites
Post Modification Inspection	SGS, Date: 09/07/2016	6444911	CCI Sites
Foundation Drawings	FDH Project No. 08-04159E N1	4591935	CCI Sites
Geotech Report	FDH Project No. 08-04159E G1	4468634	CCI Sites
Antenna Configuration	Crown CAD Package	Date: 10/12/2016	CCI Sites

### 3.1) Analysis Method

tnxTower (version 7.0.5.1), a commercially available analysis software package, was used to create a three-dimensional model of the tower and calculate member stresses for various loading cases. Selected output from the analysis is included in Appendix A.

### 3.2) Assumptions

- 1) Tower and structures were built in accordance with the manufacturer's specifications.
- 2) The tower and structures have been maintained in accordance with the manufacturer's specification.
- 3) The configuration of antennas, transmission cables, mounts and other appurtenances are as specified in Tables 1 and 2 and the referenced drawings.
- 4) Mount areas and weights are assumed based on photographs provided.
- 5) The existing base plate grout was not considered in this analysis.

This analysis may be affected if any assumptions are not valid or have been made in error. B+T Group should be notified to determine the effect on the structural integrity of the tower.

## 4) ANALYSIS RESULTS

**Table 5 - Section Capacity (Summary)**

Section No.	Elevation (ft)	Component Type	Size	Critical Element	P (K)	SF*P_allow (K)	% Capacity	Pass / Fail
L1	150 - 123.75	Pole	TP19.625x15.53x0.25	1	-9.265	1149.650	66.6	Pass
L2	123.75 - 110	Pole	TP21.77x19.625x0.482	2	-11.413	1427.660	89.9	Pass
L3	110 - 83	Pole	TP26.134x21.77x0.668	3	-253.777	2644.140	80.5	Pass
		Guy A@91.1	1 5/8	11	171.695	194.400	88.3	Pass
		Guy B@91.1	1 3/8	10	91.167	139.200	65.5	Pass
		Guy C@91.1	1 3/8	9	102.191	139.200	73.4	Pass
L4	83 - 67.5	Pole	TP28.64x26.134x0.545	4	-254.426	2190.530	98.4	Pass
L5	67.5 - 49.9	Pole	TP30.898x27.449x0.585	5	-258.029	2481.030	94.5	Pass
L6	49.9 - 33	Pole	TP33.66x30.898x0.644	6	-262.428	3057.690	80.4	Pass
L7	33 - 32.65	Pole	TP32.966x32.256x0.71	7	-268.417	3587.910	71.1	Pass
L8	32.65 - 0	Pole	TP38.29x32.966x0.438	8	-268.535	3377.690	74.4	Pass
							Summary	
						Pole (L4)	98.4	Pass
						Guy A (L3)	88.3	Pass
						Guy B (L3)	65.5	Pass
						Guy C (L3)	73.4	Pass
						<b>RATING =</b>	<b>98.4</b>	<b>Pass</b>

**Table 6 - Tower Component Stresses vs. Capacity – LC7**

Notes	Component	Elevation	% Capacity	Pass / Fail	
1	Flange Connections	110'	57.9	Pass	
1	Anchor Rods	Base	99.9	Pass	
1	Base Plate	Base	62.3	Pass	
1	Base Foundation	Structure	Base	21.1	Pass
		Soil	Base	75.0	Pass
1	Inner Guy Anchor Foundation	Anchor Rod	Base	88.9	Pass
		Soil	Base	72.4	Pass
1	Outer Guy Anchor Foundation	Anchor Rod	Base	53.0	Pass
		Soil	Base	68.6	Pass

<b>Structure Rating (max from all components) =</b>	<b>99.9%</b>
---	--------------

Notes:

- 1) See additional documentation in "Appendix C – Additional Calculations" for calculations supporting the % capacity consumed.

#### 4.1) Recommendations

The tower and its foundations have sufficient capacity **ONCE** the following condition has been met:

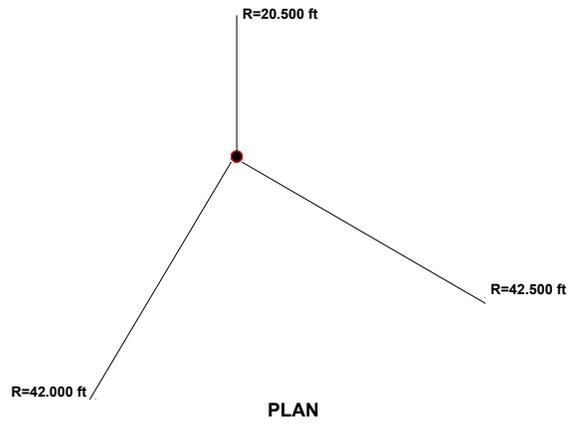
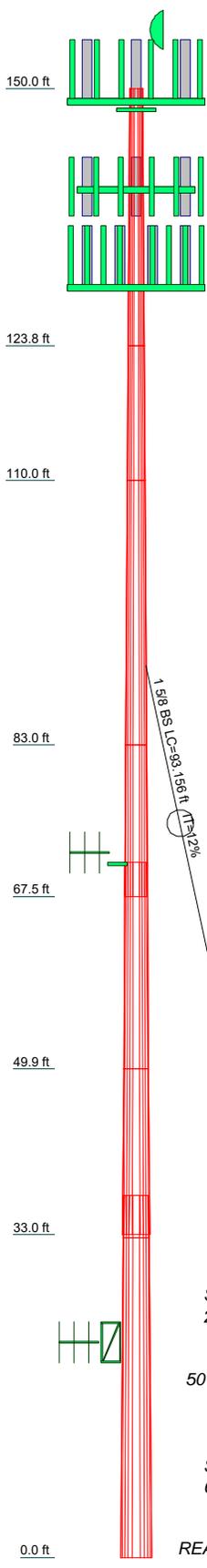
- Proposed TMEs at the 140' elevation must be shielded completely from the front.

No structural modifications will be necessary at this time.

**APPENDIX A**

**TNXTOWER OUTPUT**

Section	1	2	3	4	5	6	7	8
Length (ft)	26.250	13.750	27.000	15.500	21.100	16.900	4.360	32.650
Number of Sides	12	12	12	12	12	12	12	12
Thickness (in)	0.250	0.482	0.688	0.545	0.585	0.644	0.710	0.438
Socket Length (ft)				3.500		4.000		
Top Dia (in)	15.530	19.625	21.770	26.134	27.449	30.898	32.256	32.966
Bot Dia (in)	19.625	21.770	26.134	28.640	30.898	33.680	32.866	38.290
Grade	A572-65		42.536229ksi	42.204474ksi	42.356853ksi	42.993129ksi	42.99819ksi	A572-65
Weight (K)	1.2	1.4	4.2	2.4	3.7	3.6	1.0	5.5

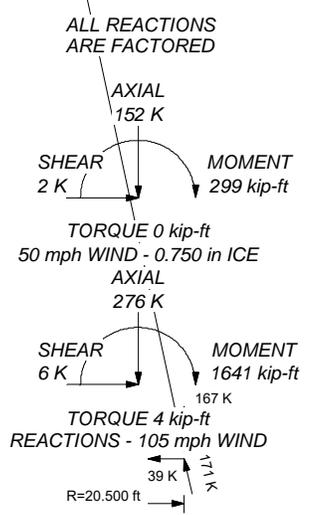


**MATERIAL STRENGTH**

GRADE	Fy	Fu	GRADE	Fy	Fu
A572-65	65 ksi	80 ksi	42.356853ksi	42 ksi	57 ksi
38.137985ksi	38 ksi	53 ksi	42.993126ksi	43 ksi	58 ksi
42.536229ksi	43 ksi	58 ksi	42.99819ksi	43 ksi	58 ksi
42.204474ksi	42 ksi	57 ksi			

**TOWER DESIGN NOTES**

1. Tower is located in Middlesex County, Connecticut.
2. Tower designed for Exposure B to the TIA-222-G Standard.
3. Tower designed for a 105 mph basic wind in accordance with the TIA-222-G Standard.
4. Tower is also designed for a 50 mph basic wind with 0.75 in ice. Ice is considered to increase in thickness with height.
5. Deflections are based upon a 60 mph wind.
6. Tower Structure Class II.
7. Topographic Category 1 with Crest Height of 0.000 ft
8. TOWER RATING: 98.4%



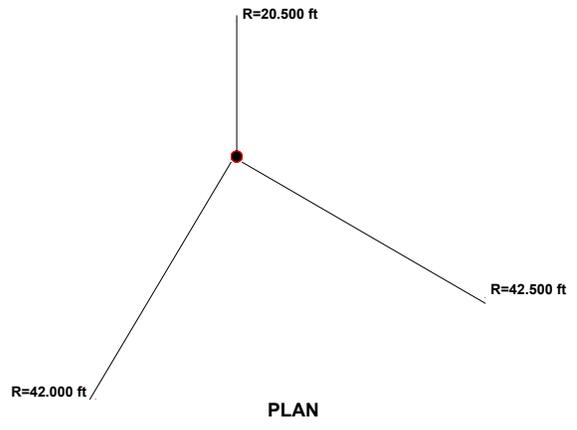
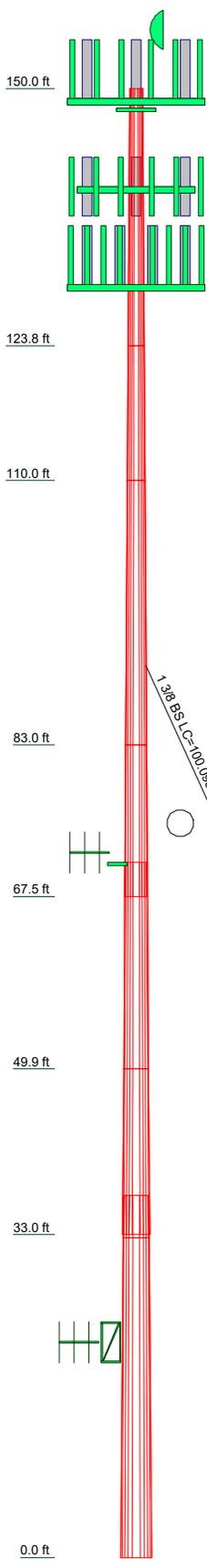
ALL REACTIONS ARE FACTORED

**B+T Group**  
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Job: <b>93496.006.01 - OLD SAYBROOK, CT (BU # 84128)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Cheriyan	App'd:
Code: TIA-222-G	Date: 10/14/16	Scale: NTS
Path:	Dwg No: E-1	

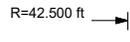
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Section	1	2	3	4	5	6	7	8
Length (ft)	26.250	13.750	27.000	15.500	21.100	16.900	4.360	32.650
Number of Sides	12	12	12	12	12	12	12	12
Thickness (in)	0.250	0.482	0.688	0.545	0.585	0.644	0.710	0.438
Socket Length (ft)				3.500		4.000		
Top Dia (in)	15.530	19.625	21.770	26.134	27.449	30.898	32.256	32.966
Bot Dia (in)	19.625	21.770	26.134	28.640	30.898	33.680	32.866	38.290
Grade	A572-65			42.536229ksi	42.204474ksi	42.356653ksi	42.983129ksi	42.99819ksi
Weight (K)	1.2	1.4	4.2	2.4	3.7	3.6	1.0	5.5



**DESIGNED APPURTENANCE LOADING**

TYPE	ELEVATION	TYPE	ELEVATION
Lighting Rod 5/8" x 5' (E)	168	Platform Mount [LP 301-1] (P-Includes 4 Mount pipes per sector)	140
7770.00 w/ Mount Pipe (E)	149	AIR 21 B2A/B4P (P)	140
7770.00 w/ Mount Pipe (E)	149	BXA-80080/4CF w/ Mount Pipe (E)	130
7770.00 w/ Mount Pipe (E)	149	BXA-80080/4CF w/ Mount Pipe (E)	130
AM-X-CW-14-65-00T-RET w/ Mount Pipe (E)	149	HBXX-6517DS-A2M w/ Mount Pipe (E)	130
AM-X-CD-14-65-00T-RET w/ Mount Pipe (E)	149	HBXX-6517DS-A2M w/ Mount Pipe (E)	130
AM-X-CD-14-65-00T-RET w/ Mount Pipe (E)	149	HBXX-6517DS-A2M w/ Mount Pipe (E)	130
(2) TT19-08BP111-001 (E)	149	LNX-6514DS-A1M w/ Mount Pipe (E)	130
(2) TT19-08BP111-001 (E)	149	LNX-6514DS-A1M w/ Mount Pipe (E)	130
SBNHH-1D65A w/ Mount Pipe (R)	149	LNX-6514DS-A1M w/ Mount Pipe (E)	130
SBNHH-1D65A w/ Mount Pipe (R)	149	BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	130
SBNHH-1D65A w/ Mount Pipe (R)	149	BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	130
WCS RRUS-32-B30 (R)	149	BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	130
WCS RRUS-32-B30 (R)	149	RRH2X60-PCS (E)	130
DC6-48-60-18-8F (R)	149	RRH2X60-PCS (E)	130
Platform Mount [LP 403-1] (E)	149	RRH2X60-AWS (E)	130
KP4F-23A (E)	149	RRH2X60-AWS (E)	130
(2) RRUS 11 (E)	148	RRH2X60-AWS (E)	130
(2) RRUS 11 (E)	148	RRH2X60-AWS (E)	130
DC6-48-60-18-8F (E-Offset per photo)	148	RRH2X60-AWS (E)	130
4' x 2" Pipe Mount (E)	148	(2) FD9R6004/2C-3L (E)	130
4' x 2" Pipe Mount (E)	148	(2) FD9R6004/2C-3L (E)	130
4' x 2" Pipe Mount (E)	148	(2) FD9R6004/2C-3L (E)	130
Side Arm Mount [SO 102-3] (E)	148	DB-T1-6Z-8AB-0Z (E)	130
(2) RRUS 11 (E)	148	Platform Mount [LP 403-1] (E)	130
AIR 21 B2A/B4P (P)	140	GPS (3"x7") (E-Per Photo)	130
AIR 21 B2A/B4P (P)	140	3' x 2" Pipe Mount (E-Per Photo)	130
AIR 21 B4A/B2P (P)	140	BXA-80080/4CF w/ Mount Pipe (E)	130
AIR 21 B4A/B2P (P)	140	Yagi (E-Per Photo)	71
LNX-6515DS-A1M (P)	140	4' x 2" Pipe Mount (E-For Yagi Per photo)	71
LNX-6515DS-A1M (P)	140	Side Arm Mount [SO 701-1] (E)	71
LNX-6515DS-A1M (P)	140	FMO (E)	71
TMAT7LA-11A (P)	140	Side Arm Mount [SO 301-1] (E)	71
TMAT7LA-11A (P)	140	Side Arm Mount [SO 701-1] (E)	22
RRUS 11 B12 (P)	140	4' x 2" Pipe Mount (E-For Yagi Per photo)	22
RRUS 11 B12 (P)	140	MYA-43012N (E)	22
RRUS 11 B12 (P)	140		

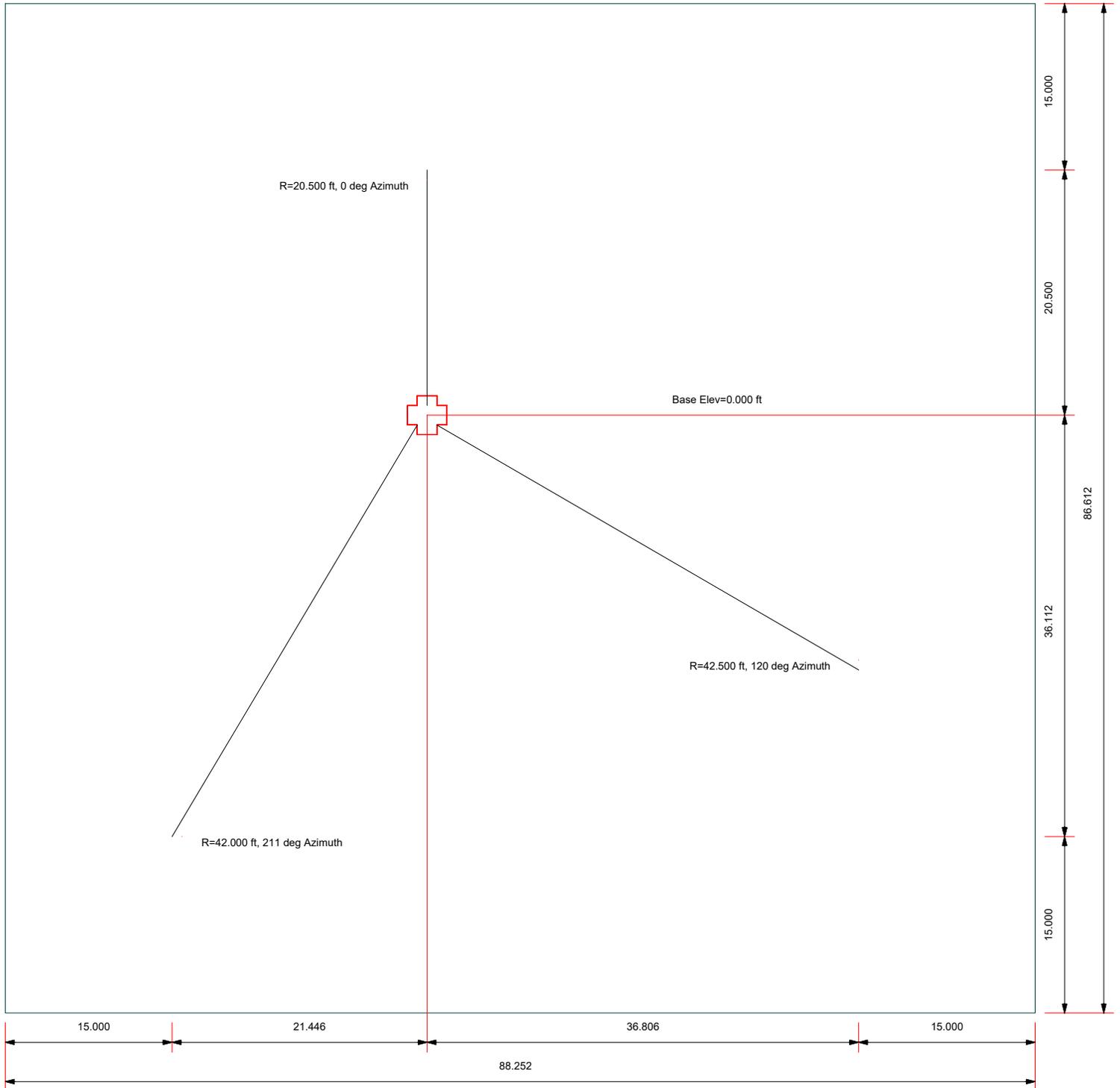


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 FAX: (918) 295 - 0265

Job: **93496.006.01 - OLD SAYBROOK, CT (BU # 84128)**  
 Project:  
 Client: Crown Castle      Drawn by: T. Cheriyan      App'd:  
 Code: TIA-222-G      Date: 10/14/16      Scale: NTS  
 Path:      Dwg No: E-1

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**Plot Plan**  
**Total Area - 0.18 Acres**



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Project:		
Client: Crown Castle	Drawn by: T. Cheriyan	App'd:
Code: TIA-222-G	Date: 10/14/16	Scale: NTS
Path:		Dwg No: E-2

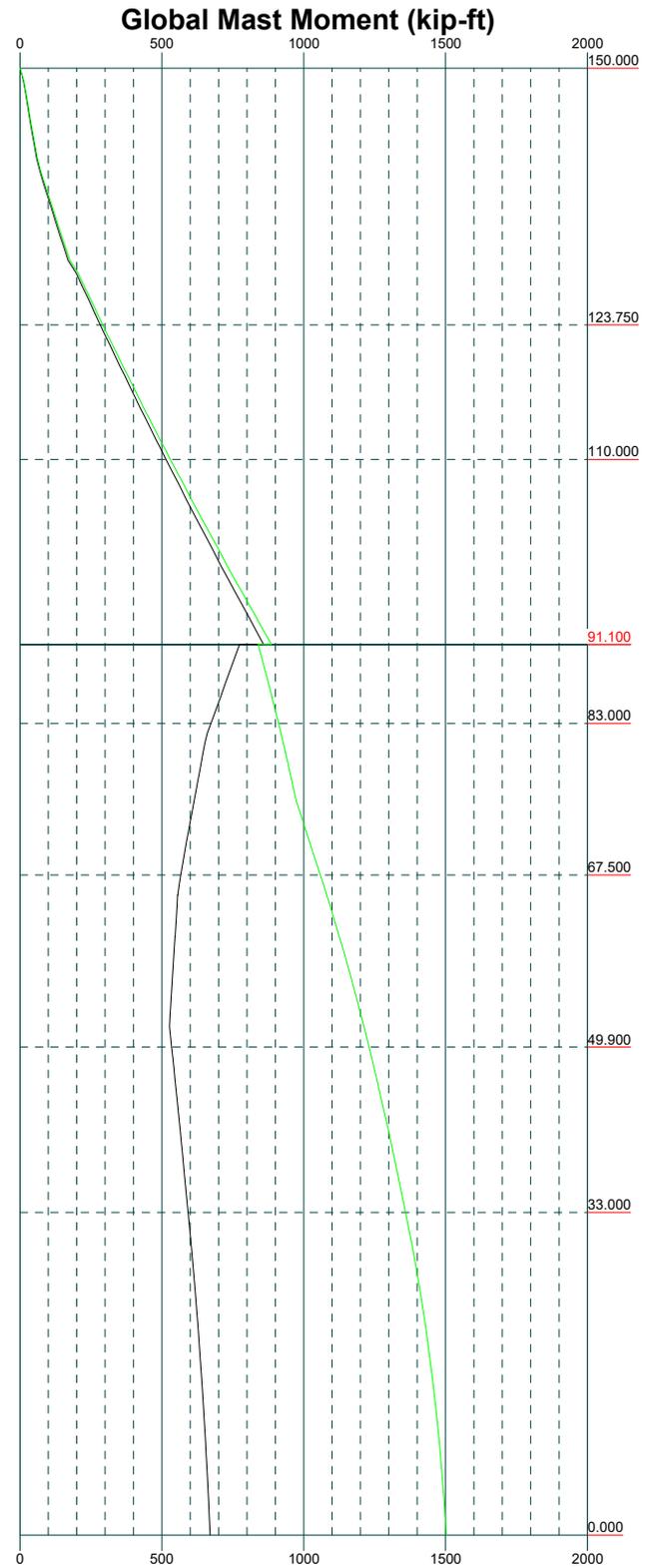
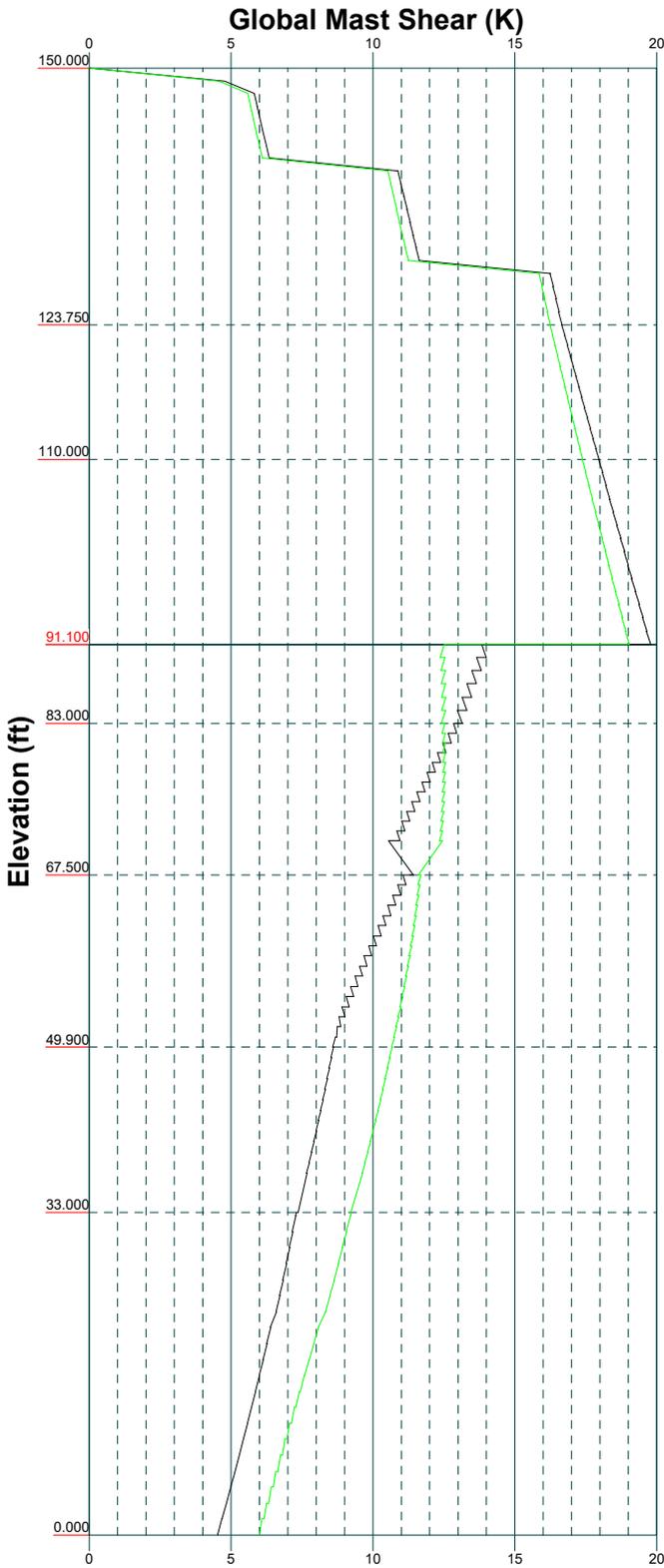
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Vx

Vz

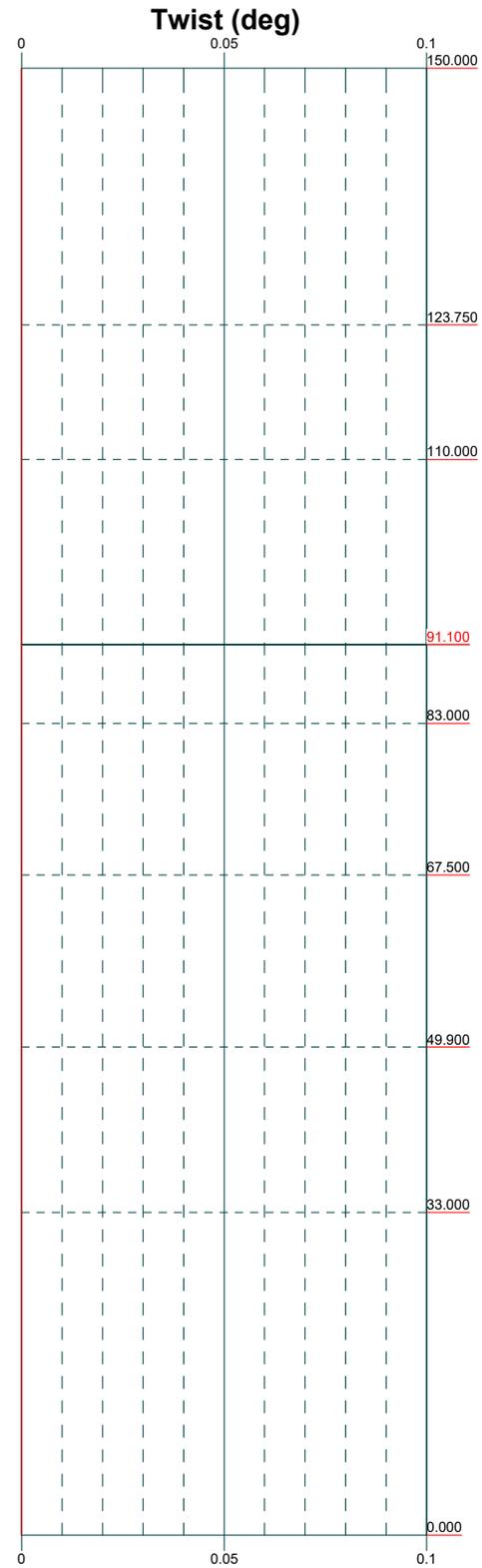
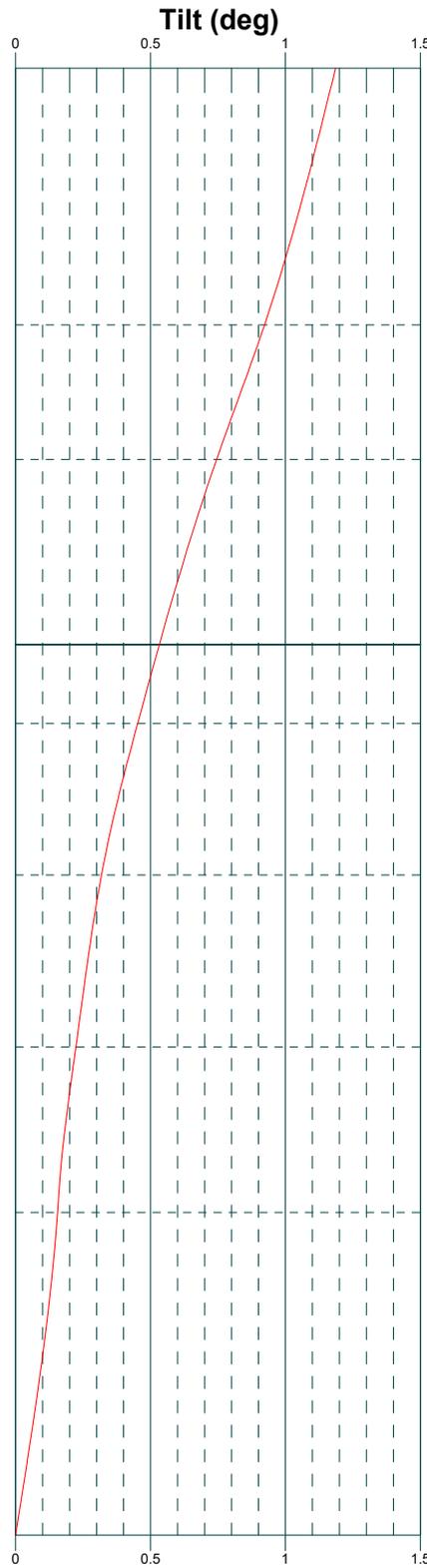
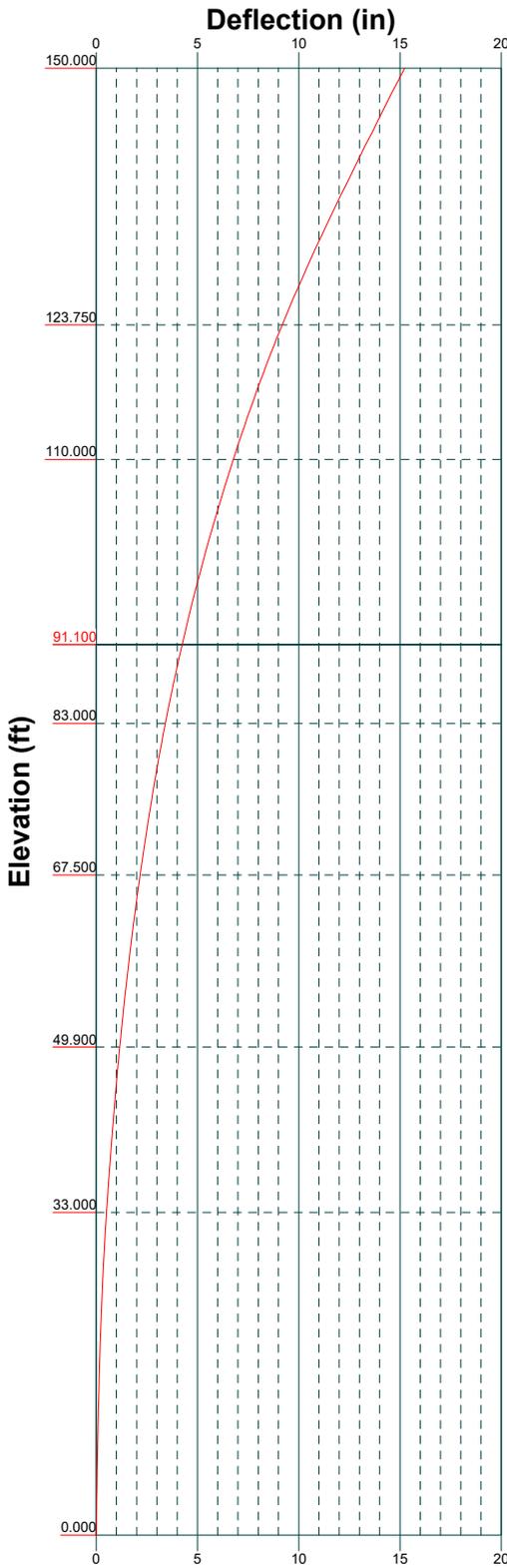
Mx

Mz



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 FAX: (918) 295 - 0265

Job: <b>93496.006.01 - OLD SAYBROOK, CT (BU # 84128)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Cheriyan	App'd:
Code: TIA-222-G	Date: 10/14/16	Scale: NTS
Path:	Dwg No: E-4	

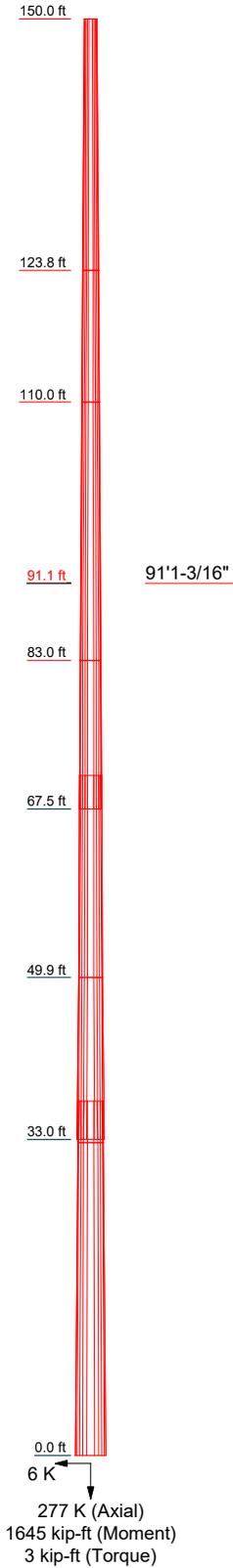


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 FAX: (918) 295 - 0265

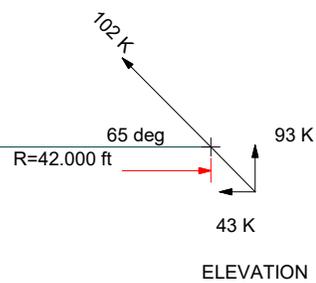
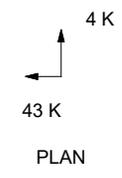
Job: <b>93496.006.01 - OLD SAYBROOK, CT (BU # 84128)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Cheriyan	App'd:
Code: TIA-222-G	Date: 10/14/16	Scale: NTS
Path:	Dwg No: E-5	

**Guy Tensions and Tower Reactions**  
**TIA-222-G - 105 mph/50 mph 0.750 in Ice Exposure B**

**Maximum Values**  
**Anchor 'C'@42 ft Azimuth 211 deg Elev 0 ft**  
**Plane through centroid of tower**



*1 3/8 BS, SF = 1.36, Tmax = 102.412 K, Lc = 99.887 ft, Lu = 99.784 ft, Ls = 100.160 ft*



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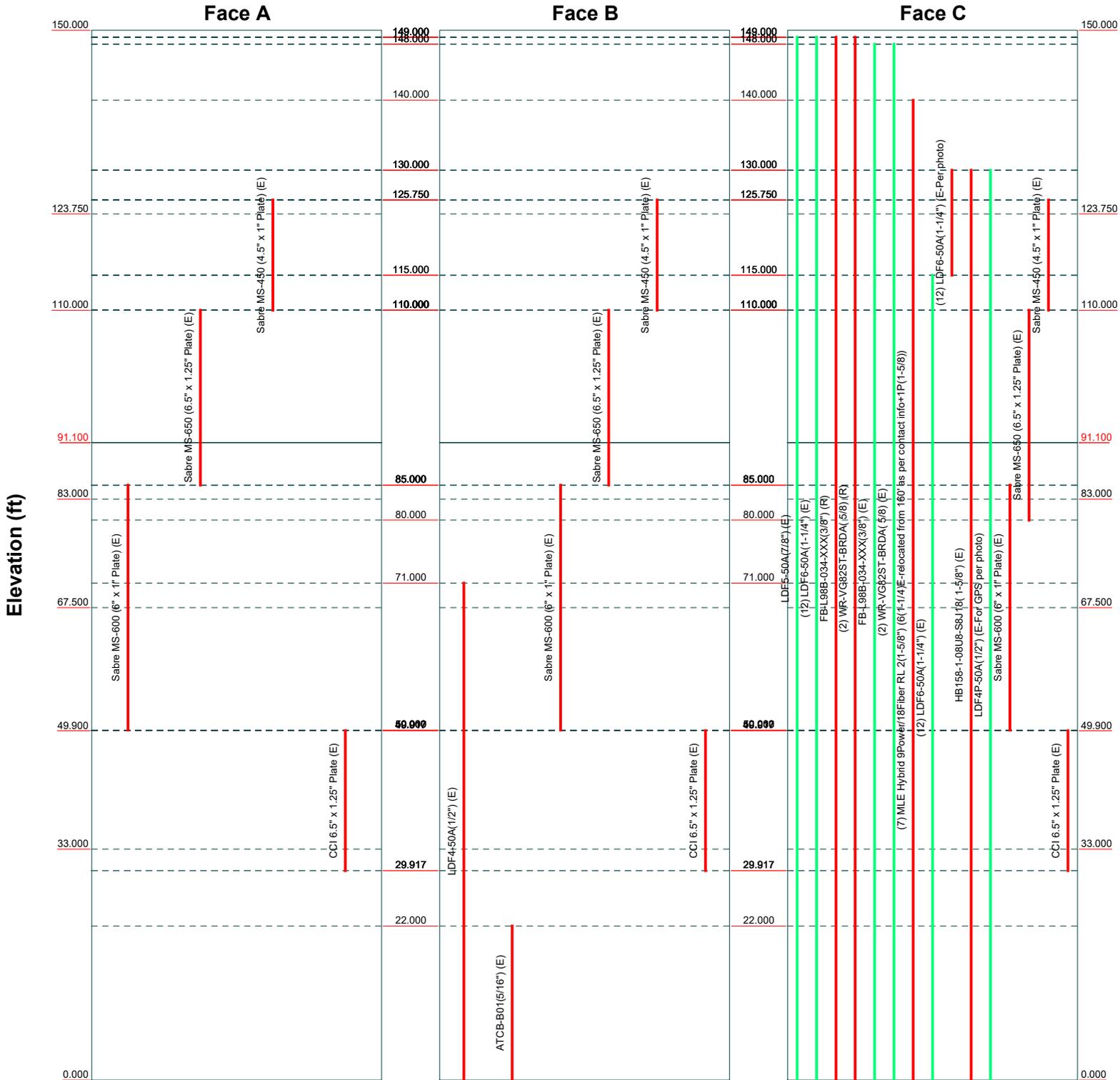
Job: <b>93496.006.01 - OLD SAYBROOK, CT (BU # 84128)</b>		
Project:		
Client: Crown Castle	Drawn by: T. Cheriyan	App'd:
Code: TIA-222-G	Date: 10/14/16	Scale: NTS
Path:	Dwg No: E-6	

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# Feed Line Distribution Chart

## 0' - 150'

— Round   
 — Flat   
 — App In Face   
 — App Out Face   
 — Truss Leg




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 FAX: (918) 295 - 0265

<b>Job:</b> 93496.006.01 - OLD SAYBROOK, CT (BU # 84128)		
<b>Project:</b>		
<b>Client:</b> Crown Castle	<b>Drawn by:</b> T. Cheriyan	<b>App'd:</b>
<b>Code:</b> TIA-222-G	<b>Date:</b> 10/14/16	<b>Scale:</b> NTS
<b>Path:</b>	<b>Dwg No:</b> E-7	

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<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b> 93496.006.01 - OLD SAYBROOK, CT (BU # 841289)	<b>Page</b> 1 of 23
	<b>Project</b>	<b>Date</b> 15:27:21 10/14/16
	<b>Client</b> Crown Castle	<b>Designed by</b> T. Cheriyan

## Tower Input Data

There is a pole section.

This tower is designed using the TIA-222-G standard.

The following design criteria apply:

Tower is located in Middlesex County, Connecticut.

Basic wind speed of 105 mph.

Structure Class II.

Exposure Category B.

Topographic Category 1.

Crest Height 0.000 ft.

Nominal ice thickness of 0.750 in.

Ice thickness is considered to increase with height.

Ice density of 56.000 pcf.

A wind speed of 50 mph is used in combination with ice.

Temperature drop of 50.000 °F.

Deflections calculated using a wind speed of 60 mph.

Pressures are calculated at each section.

Stress ratio used in pole design is 1.

Safety factor used in guy design is 1.

Local bending stresses due to climbing loads, feed line supports, and appurtenance mounts are not considered.

## Options

- |  |  |  |
|--|--|--|
| <ul style="list-style-type: none"> <li>Consider Moments - Legs</li> <li>Consider Moments - Horizontals</li> <li>Consider Moments - Diagonals</li> <li>Use Moment Magnification</li> <li>√ Use Code Stress Ratios</li> <li>√ Use Code Safety Factors - Guys</li> <li>Escalate Ice</li> <li>Always Use Max Kz</li> <li>Use Special Wind Profile</li> <li>Include Bolts In Member Capacity</li> <li>Leg Bolts Are At Top Of Section</li> <li>Secondary Horizontal Braces Leg</li> <li>Use Diamond Inner Bracing (4 Sided)</li> <li>SR Members Have Cut Ends</li> <li>SR Members Are Concentric</li> </ul> | <ul style="list-style-type: none"> <li>Distribute Leg Loads As Uniform</li> <li>Assume Legs Pinned</li> <li>√ Assume Rigid Index Plate</li> <li>√ Use Clear Spans For Wind Area</li> <li>Use Clear Spans For KL/r</li> <li>Retention Guys To Initial Tension</li> <li>√ Bypass Mast Stability Checks</li> <li>√ Use Azimuth Dish Coefficients</li> <li>√ Project Wind Area of Appurt.</li> <li>Autocalc Torque Arm Areas</li> <li>Add IBC .6D+W Combination</li> <li>Sort Capacity Reports By Component</li> <li>Triangulate Diamond Inner Bracing</li> <li>Treat Feed Line Bundles As Cylinder</li> </ul> | <ul style="list-style-type: none"> <li>Use ASCE 10 X-Brace Ly Rules</li> <li>Calculate Redundant Bracing Forces</li> <li>Ignore Redundant Members in FEA</li> <li>SR Leg Bolts Resist Compression</li> <li>All Leg Panels Have Same Allowable</li> <li>Offset Girt At Foundation</li> <li>√ Consider Feed Line Torque</li> <li>Include Angle Block Shear Check</li> <li>Use TIA-222-G Bracing Resist. Exemption</li> <li>Use TIA-222-G Tension Splice Exemption</li> <li style="background-color: #e0e0e0;">Poles</li> <li>√ Include Shear-Torsion Interaction</li> <li>Always Use Sub-Critical Flow</li> <li>Use Top Mounted Sockets</li> </ul> |
|--|--|--|

## Tapered Pole Section Geometry

Section	Elevation	Section Length	Splice Length	Number of Sides	Top Diameter	Bottom Diameter	Wall Thickness	Bend Radius	Pole Grade
	ft	ft	ft		in	in	in	in	
L1	150.000-123.75 0	26.250	0.000	12	15.530	19.625	0.250	1.000	A572-65 (65 ksi)
L2	123.750-110.00 0	13.750	0.000	12	19.625	21.770	0.482	1.926	38.137985ksi (38 ksi)
L3	110.000-83.000	27.000	0.000	12	21.770	26.134	0.668	2.674	42.536229ksi (43 ksi)
L4	83.000-67.500	15.500	3.500	12	26.134	28.640	0.545	2.181	42.204474ksi

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b>	<b>Page</b>	
		93496.006.01 - OLD SAYBROOK, CT (BU # 841289)	2 of 23
	<b>Project</b>		<b>Date</b>
		15:27:21 10/14/16	
	<b>Client</b>	<b>Designed by</b>	
	Crown Castle	T. Cheriyan	

Section	Elevation ft	Section Length ft	Splice Length ft	Number of Sides	Top Diameter in	Bottom Diameter in	Wall Thickness in	Bend Radius in	Pole Grade
L5	67.500-49.900	21.100	0.000	12	27.449	30.898	0.585	2.339	(42 ksi) 42.356853ksi
L6	49.900-33.000	16.900	4.000	12	30.898	33.660	0.644	2.575	(42 ksi) 42.993126ksi
L7	33.000-32.650	4.350	0.000	12	32.256	32.966	0.710	2.839	(43 ksi) 42.99819ksi
L8	32.650-0.000	32.650		12	32.966	38.290	0.438	1.750	(43 ksi) A572-65 (65 ksi)

### Tapered Pole Properties

Section	Tip Dia. in	Area in <sup>2</sup>	I in <sup>4</sup>	r in	C in	I/C in <sup>3</sup>	J in <sup>4</sup>	It/Q in <sup>2</sup>	w in	w/t
L1	16.078	12.300	366.566	5.470	8.045	45.567	742.762	6.054	3.492	13.968
	20.317	15.597	747.321	6.936	10.166	73.514	1514.274	7.676	4.590	18.358
L2	20.317	29.685	1388.536	6.853	10.166	136.590	2813.551	14.610	3.969	8.242
	22.538	33.011	1909.540	7.621	11.277	169.333	3869.246	16.247	4.544	9.435
L3	22.538	45.422	2581.534	7.554	11.277	228.923	5230.889	22.355	4.043	6.048
	27.056	54.817	4537.520	9.117	13.538	335.178	9194.246	26.979	5.212	7.797
L4	27.056	44.918	3754.287	9.161	13.538	277.322	7607.202	22.107	5.543	10.168
	29.650	49.316	4968.568	10.058	14.836	334.910	10067.666	24.272	6.215	11.4
L5	29.010	50.576	4658.971	9.618	14.219	327.665	9440.338	24.892	5.789	9.902
	31.988	57.068	6693.369	10.852	16.005	418.203	13562.580	28.087	6.714	11.483
L6	31.988	62.716	7327.136	10.831	16.005	457.801	14846.764	30.867	6.555	10.182
	34.847	68.442	9522.811	11.820	17.436	546.162	19295.797	33.685	7.296	11.332
L7	34.069	72.092	9157.532	11.294	16.709	548.069	18555.644	35.482	6.743	9.501
	34.129	73.714	9789.294	11.548	17.076	573.272	19835.764	36.280	6.933	9.768
L8	34.129	45.824	6188.656	11.645	17.076	362.414	12539.896	22.553	7.662	17.514
	39.641	53.325	9752.222	13.551	19.834	491.687	19760.646	26.245	9.089	20.775

Tower Elevation	Gusset Area (per face)	Gusset Thickness	Gusset Grade	Adjust. Factor A <sub>f</sub>	Adjust. Factor A <sub>r</sub>	Weight Mult.	Double Angle Stitch Bolt Spacing Diagonals	Double Angle Stitch Bolt Spacing Horizontals	Double Angle Stitch Bolt Spacing Redundants
ft	ft <sup>2</sup>	in					in	in	in
L1 150.000-123.7 50				1	1	1			
L2 123.750-110.0 00				1	1	0.931736			
L3 110.000-83.00 0				1	1	0.916808			
L4 83.000-67.500				1	1	0.948412			
L5 67.500-49.900				1	1	0.958676			
L6 49.900-33.000				1	1	0.94843			
L7 33.000-32.650				1	1	0.949707			
L8 32.650-0.000				1	1	1			



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Guy Elevation ft	Calc K Single Angles	Calc K Solid Rounds	Torque Arm		Pull Off		Diagonal	
			K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>	K <sub>x</sub>	K <sub>y</sub>
91.1	No	No			1	1	1	1

### Guy Data (cont'd)

Guy Elevation ft	Torque-Arm				Pull Off				Diagonal			
	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U	Bolt Size in	Number	Net Width Deduct in	U
91.1	0.625 A325N	0	0.000	0.75	0.625 A325N	0	0.000	0.75	0.625 A325N	0	0.000	0.75

### Guy Pressures

Guy Elevation ft	Guy Location	z ft	q <sub>z</sub> ksf	q <sub>z</sub> Ice ksf	Ice Thickness in
91.1	A	45.550	0.021	0.005	1.549
	B	45.550	0.021	0.005	1.549
	C	45.550	0.021	0.005	1.549

### Guy-Mast Forces (Excluding Wind) - No Ice

Guy Elevation ft	Guy Location	Chord Angle °	Guy Tension Top Bottom K	F <sub>x</sub> K	F <sub>y</sub> K	F <sub>z</sub> K	M <sub>x</sub> kip-ft	M <sub>y</sub> kip-ft	M <sub>z</sub> kip-ft
91.1	A	77.939	39.385	0.000	38.527	-8.177	-39.851	0.000	0.000
			38.880						
	B	65.527	28.201	10.053	25.702	5.804	13.293	0.000	-23.023
			27.840						
C	65.788	28.201	28.201	-5.868	25.754	9.881	22.904	0.000	13.603
			27.840						
			Sum:	<b>4.185</b>	89.982	<b>7.508</b>	<b>-3.654</b>	0.000	<b>-9.421</b>

### Guy-Mast Forces (Excluding Wind) - Ice

Guy Elevation ft	Guy Location	Chord Angle °	Guy Tension Top Bottom K	F <sub>x</sub> K	F <sub>y</sub> K	F <sub>z</sub> K	M <sub>x</sub> kip-ft	M <sub>y</sub> kip-ft	M <sub>z</sub> kip-ft
91.1	A	77.939	52.098	0.000	50.971	-10.776	-52.724	0.000	0.000

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Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F <sub>x</sub>	F <sub>y</sub>	F <sub>z</sub>	M <sub>x</sub>	M <sub>y</sub>	M <sub>z</sub>
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
	B	65.527	51.046 37.370 36.505	13.251	34.093	7.651	17.633	0.000	-30.541
	C	65.788	37.367 36.502	-7.734	34.160	13.023	30.380	0.000	18.043
			Sum:	<b>5.517</b>	119.225	<b>9.898</b>	<b>-4.711</b>	0.000	<b>-12.498</b>

### Guy-Mast Forces (Excluding Wind) - Service

Guy Elevation	Guy Location	Chord Angle	Guy Tension Top Bottom K	F <sub>x</sub>	F <sub>y</sub>	F <sub>z</sub>	M <sub>x</sub>	M <sub>y</sub>	M <sub>z</sub>
ft		°		K	K	K	kip-ft	kip-ft	kip-ft
91.1	A	77.939	39.385 38.880	0.000	38.527	-8.177	-39.851	0.000	0.000
	B	65.527	28.201 27.840	10.053	25.702	5.804	13.293	0.000	-23.023
	C	65.788	28.201 27.840	-5.868	25.754	9.881	22.904	0.000	13.603
			Sum:	<b>4.185</b>	89.982	<b>7.508</b>	<b>-3.654</b>	0.000	<b>-9.421</b>

### Guy-Tensioning Information

		Temperature At Time Of Tensioning															
		0 F		20 F		40 F		60 F		80 F		100 F		120 F			
Guy Elevation	H	V	Initial Tension K	Intercept ft													
ft	ft	ft	K	ft	K	ft	K	ft	K	ft	K	ft	K	ft	K	ft	
91.1	A	19.47	91.10	39.531	0.60	39.314	0.61	39.097	0.61	38.880	0.61	38.663	0.62	38.447	0.62	38.230	0.63
	B	41.47	91.10	29.654	0.67	29.049	0.68	28.444	0.69	27.840	0.71	27.236	0.72	26.633	0.74	26.029	0.76
	C	40.97	91.10	29.618	0.66	29.025	0.68	28.432	0.69	27.840	0.71	27.248	0.72	26.657	0.74	26.065	0.75

### Feed Line/Linear Appurtenances - Entered As Round Or Flat

Description	Sector	Component Type	Placement	Total Number	Number Per Row	Start/End Position	Width or Diameter	Perimeter	Weight
			ft				in	in	klf
FB-L98B-034-XXX(3/8") (R)	C	Surface Ar (CaAa)	149.000 - 0.000	1	1	0.200 0.210	0.394		0.000
WR-VG82ST-BRDA( 5/8) (R) *M*	C	Surface Ar (CaAa)	149.000 - 0.000	2	2	0.220 0.240	0.645		0.000
MLE Hybrid 9Power/18Fiber RL 2(1-5/8") (6(1-1/4)E-relocated from 160' as	C	Surface Ar (CaAa)	140.000 - 0.000	7	7	-0.450 -0.200	1.625		0.001

**tnxTower**

**B+T Group**  
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**Job**  
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**Client**  
 Crown Castle  
 Designed by  
 T. Cheriyan

Description	Sector	Component Type	Placement ft	Total Number	Number Per Row	Start/End Position	Width or Diameter in	Perimeter in	Weight klf
per contact info+1P(1-5/8))									
LDF6-50A(1-1/4") (E-Per photo)	C	Surface Ar (CaAa)	130.000 - 115.000	12	6	0.000 0.150	1.550		0.001
HB158-1-08U8-S8J18( 1-5/8") (E) *M*	C	Surface Ar (CaAa)	130.000 - 0.000	1	1	0.250 0.270	1.980		0.001
LDF4-50A(1/2") (E) *M*	B	Surface Ar (CaAa)	71.000 - 0.000	1	1	0.450 0.460	0.630		0.000
ATCB-B01(5/16") (E) *M* *M*	B	Surface Ar (CaAa)	22.000 - 0.000	1	1	0.470 0.480	0.315		0.000
**2014 Mod**									
Sabre MS-600 (6" x 1" Plate) (E)	A	Surface Af (CaAa)	85.000 - 50.000	1	1	0.000 0.100	6.000	14.000	0.000
Sabre MS-600 (6" x 1" Plate) (E)	B	Surface Af (CaAa)	85.000 - 50.000	1	1	0.000 0.100	6.000	14.000	0.000
Sabre MS-600 (6" x 1" Plate) (E) *M*	C	Surface Af (CaAa)	85.000 - 50.000	1	1	0.000 0.100	6.000	14.000	0.000
Sabre MS-650 (6.5" x 1.25" Plate) (E)	A	Surface Af (CaAa)	110.000 - 85.000	1	1	0.120 0.140	6.500	15.500	0.000
Sabre MS-650 (6.5" x 1.25" Plate) (E)	B	Surface Af (CaAa)	110.000 - 85.000	1	1	0.120 0.140	6.500	15.500	0.000
Sabre MS-650 (6.5" x 1.25" Plate) (E) *M*	C	Surface Af (CaAa)	110.000 - 80.000	1	1	0.120 0.140	6.500	15.500	0.000
Sabre MS-450 (4.5" x 1" Plate) (E)	A	Surface Af (CaAa)	125.750 - 110.000	1	1	0.200 0.240	4.500	11.000	0.000
Sabre MS-450 (4.5" x 1" Plate) (E)	B	Surface Af (CaAa)	125.750 - 110.000	1	1	0.200 0.240	4.500	11.000	0.000
Sabre MS-450 (4.5" x 1" Plate) (E) *M*	C	Surface Af (CaAa)	125.750 - 110.000	1	1	0.200 0.240	4.500	11.000	0.000
**2016 Mod**									
CCI 6.5" x 1.25" Plate (E)	A	Surface Af (CaAa)	49.917 - 29.917	1	1	-0.240 -0.200	6.500	15.500	0.000
CCI 6.5" x 1.25" Plate (E)	B	Surface Af (CaAa)	49.917 - 29.917	1	1	-0.240 -0.200	6.500	15.500	0.000
CCI 6.5" x 1.25" Plate (E) *M*	C	Surface Af (CaAa)	49.917 - 29.917	1	1	-0.240 -0.200	6.500	15.500	0.000

### Feed Line/Linear Appurtenances - Entered As Area

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C <sub>A</sub> A <sub>A</sub> ft <sup>2</sup> /ft	Weight klf
*M*								
LDF5-50A(7/8") (E)	C	No	Inside Pole	149.000 - 0.000	1	No Ice 1/2" Ice 1" Ice	0.000 0.000 0.000	0.000 0.000 0.001
LDF6-50A(1-1/4") (E)	C	No	Inside Pole	149.000 - 0.000	12	No Ice 1/2" Ice	0.000 0.000	0.001 0.001

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		<b>Designed by</b> T. Cheriyan	

Description	Face or Leg	Allow Shield	Component Type	Placement ft	Total Number		C <sub>AA</sub> ft <sup>2</sup> /ft	Weight klf
*M*						1" Ice	0.000	0.001
FB-L98B-034-XXX(3/8")	C	No	Inside Pole	148.000 - 0.000	1	No Ice	0.000	0.000
)						1/2" Ice	0.000	0.000
(E)						1" Ice	0.000	0.000
WR-VG82ST-BRDA(5/8)	C	No	Inside Pole	148.000 - 0.000	2	No Ice	0.000	0.000
(E)						1/2" Ice	0.000	0.000
(E)						1" Ice	0.000	0.000
*M*								
LDF6-50A(1-1/4")	C	No	Inside Pole	115.000 - 0.000	12	No Ice	0.000	0.001
(E)						1/2" Ice	0.000	0.001
(E)						1" Ice	0.000	0.001
*M*								
LDF4P-50A(1/2")	C	No	Inside Pole	130.000 - 0.000	1	No Ice	0.000	0.000
(E-For GPS per photo)						1/2" Ice	0.000	0.000
						1" Ice	0.000	0.000
*M*								
*M*								
*M*								

### Feed Line/Linear Appurtenances Section Areas

Tower Section	Tower Elevation ft	Face	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	150.000-123.750	A	0.000	0.000	1.500	0.000	0.000
		B	0.000	0.000	1.500	0.000	0.000
		C	0.000	0.000	31.286	0.000	0.422
L2	123.750-110.000	A	0.000	0.000	10.313	0.000	0.000
		B	0.000	0.000	10.313	0.000	0.000
		C	0.000	0.000	39.128	0.000	0.364
L3	110.000-83.000	A	0.000	0.000	29.083	0.000	0.000
		B	0.000	0.000	29.083	0.000	0.000
		C	0.000	0.000	71.854	0.000	0.714
L4	83.000-67.500	A	0.000	0.000	15.500	0.000	0.000
		B	0.000	0.000	15.720	0.000	0.001
		C	0.000	0.000	42.060	0.000	0.410
L5	67.500-49.900	A	0.000	0.000	17.518	0.000	0.000
		B	0.000	0.000	18.627	0.000	0.003
		C	0.000	0.000	43.987	0.000	0.466
L6	49.900-33.000	A	0.000	0.000	18.308	0.000	0.000
		B	0.000	0.000	19.373	0.000	0.003
		C	0.000	0.000	43.724	0.000	0.447
L7	33.000-32.650	A	0.000	0.000	0.379	0.000	0.000
		B	0.000	0.000	0.401	0.000	0.000
		C	0.000	0.000	0.906	0.000	0.009
L8	32.650-0.000	A	0.000	0.000	2.961	0.000	0.000
		B	0.000	0.000	5.711	0.000	0.007
		C	0.000	0.000	52.062	0.000	0.864

### Feed Line/Linear Appurtenances Section Areas - With Ice

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
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	Crown Castle	T. Cheriyan	

Tower Section	Tower Elevation ft	Face or Leg	Ice Thickness in	A <sub>R</sub> ft <sup>2</sup>	A <sub>F</sub> ft <sup>2</sup>	C <sub>AA</sub> In Face ft <sup>2</sup>	C <sub>AA</sub> Out Face ft <sup>2</sup>	Weight K
L1	150.000-123.750	A	1.729	0.000	0.000	2.181	0.000	0.024
		B		0.000	0.000	2.181	0.000	0.024
		C		0.000	0.000	70.382	0.000	1.257
L2	123.750-110.000	A	1.702	0.000	0.000	14.936	0.000	0.159
		B		0.000	0.000	14.936	0.000	0.159
		C		0.000	0.000	74.926	0.000	1.266
L3	110.000-83.000	A	1.669	0.000	0.000	38.097	0.000	0.380
		B		0.000	0.000	38.097	0.000	0.380
		C		0.000	0.000	130.646	0.000	2.147
L4	83.000-67.500	A	1.629	0.000	0.000	20.549	0.000	0.198
		B		0.000	0.000	21.909	0.000	0.214
		C		0.000	0.000	75.713	0.000	1.218
L5	67.500-49.900	A	1.589	0.000	0.000	23.224	0.000	0.224
		B		0.000	0.000	30.066	0.000	0.305
		C		0.000	0.000	81.062	0.000	1.336
L6	49.900-33.000	A	1.534	0.000	0.000	23.494	0.000	0.215
		B		0.000	0.000	29.744	0.000	0.286
		C		0.000	0.000	77.594	0.000	1.236
L7	33.000-32.650	A	1.499	0.000	0.000	0.487	0.000	0.004
		B		0.000	0.000	0.616	0.000	0.006
		C		0.000	0.000	1.607	0.000	0.026
L8	32.650-0.000	A	1.395	0.000	0.000	3.723	0.000	0.031
		B		0.000	0.000	21.715	0.000	0.214
		C		0.000	0.000	104.141	0.000	1.875

### Feed Line Center of Pressure

Section	Elevation ft	CP <sub>X</sub> in	CP <sub>Z</sub> in	CP <sub>X</sub> Ice in	CP <sub>Z</sub> Ice in
L1	150.000-123.750	0.275	0.859	0.089	0.968
L2	123.750-110.000	0.200	0.831	0.075	0.944
L3	110.000-83.000	0.230	0.593	0.119	0.807
L4	83.000-67.500	0.230	0.708	0.135	0.942
L5	67.500-49.900	0.325	0.671	0.275	0.955
L6	49.900-33.000	0.331	0.684	0.292	0.989
L7	33.000-32.650	0.335	0.692	0.296	1.003
L8	32.650-0.000	0.578	1.166	0.560	1.545

### Shielding Factor Ka

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L1	5	FB-L98B-034-XXX(3/8")	123.75 - 149.00	1.0000	1.0000
L1	6	WR-VG82ST-BRDA( 5/8)	123.75 - 149.00	1.0000	1.0000
L1	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	123.75 - 140.00	1.0000	1.0000
L1	15	LDF6-50A(1-1/4")	123.75 - 130.00	1.0000	1.0000

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	$K_a$ No Ice	$K_a$ Ice
L1	18	HB158-1-08U8-S8J18(1-5/8")	123.75 - 130.00	1.0000	1.0000
L1	37	Sabre MS-450 (4.5" x 1" Plate)	123.75 - 125.75	1.0000	1.0000
L1	38	Sabre MS-450 (4.5" x 1" Plate)	123.75 - 125.75	1.0000	1.0000
L1	39	Sabre MS-450 (4.5" x 1" Plate)	123.75 - 125.75	1.0000	1.0000
L2	5	FB-L98B-034-XXX(3/8")	110.00 - 123.75	1.0000	1.0000
L2	6	WR-VG82ST-BRDA( 5/8)	110.00 - 123.75	1.0000	1.0000
L2	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	110.00 - 123.75	1.0000	1.0000
L2	15	LDF6-50A(1-1/4")	115.00 - 123.75	1.0000	1.0000
L2	18	HB158-1-08U8-S8J18(1-5/8")	110.00 - 123.75	1.0000	1.0000
L2	37	Sabre MS-450 (4.5" x 1" Plate)	110.00 - 123.75	1.0000	1.0000
L2	38	Sabre MS-450 (4.5" x 1" Plate)	110.00 - 123.75	1.0000	1.0000
L2	39	Sabre MS-450 (4.5" x 1" Plate)	110.00 - 123.75	1.0000	1.0000
L3	5	FB-L98B-034-XXX(3/8")	83.00 - 110.00	1.0000	1.0000
L3	6	WR-VG82ST-BRDA( 5/8)	83.00 - 110.00	1.0000	1.0000
L3	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	83.00 - 110.00	1.0000	1.0000
L3	18	HB158-1-08U8-S8J18(1-5/8")	83.00 - 110.00	1.0000	1.0000
L3	29	Sabre MS-600 (6" x 1" Plate)	83.00 - 85.00	1.0000	1.0000
L3	30	Sabre MS-600 (6" x 1" Plate)	83.00 - 85.00	1.0000	1.0000
L3	31	Sabre MS-600 (6" x 1" Plate)	83.00 - 85.00	1.0000	1.0000
L3	33	Sabre MS-650 (6.5" x 1.25" Plate)	85.00 - 110.00	1.0000	1.0000
L3	34	Sabre MS-650 (6.5" x 1.25" Plate)	85.00 - 110.00	1.0000	1.0000
L3	35	Sabre MS-650 (6.5" x 1.25" Plate)	83.00 - 110.00	1.0000	1.0000
L4	5	FB-L98B-034-XXX(3/8")	67.50 - 83.00	1.0000	1.0000
L4	6	WR-VG82ST-BRDA( 5/8)	67.50 - 83.00	1.0000	1.0000
L4	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	67.50 - 83.00	1.0000	1.0000
L4	18	HB158-1-08U8-S8J18(1-5/8")	67.50 - 83.00	1.0000	1.0000
L4	20	LDF4-50A(1/2")	67.50 - 71.00	1.0000	1.0000
L4	29	Sabre MS-600 (6" x 1" Plate)	67.50 - 83.00	1.0000	1.0000
L4	30	Sabre MS-600 (6" x 1" Plate)	67.50 - 83.00	1.0000	1.0000
L4	31	Sabre MS-600 (6" x 1" Plate)	67.50 - 83.00	1.0000	1.0000
L4	35	Sabre MS-650 (6.5" x 1.25" Plate)	80.00 - 83.00	1.0000	1.0000
L4	42	CCI 6.5" x 1.25" Plate	67.50 - 49.92	1.0000	1.0000
L4	43	CCI 6.5" x 1.25" Plate	67.50 - 49.92	1.0000	1.0000
L4	44	CCI 6.5" x 1.25" Plate	67.50 - 49.92	1.0000	1.0000
L6	5	FB-L98B-034-XXX(3/8")	33.00 - 49.90	1.0000	1.0000
L6	6	WR-VG82ST-BRDA( 5/8)	33.00 - 49.90	1.0000	1.0000
L6	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	33.00 - 49.90	1.0000	1.0000
L6	18	HB158-1-08U8-S8J18(1-5/8")	33.00 - 49.90	1.0000	1.0000
L6	20	LDF4-50A(1/2")	33.00 - 49.90	1.0000	1.0000
L6	42	CCI 6.5" x 1.25" Plate	33.00 - 49.90	1.0000	1.0000

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b> 93496.006.01 - OLD SAYBROOK, CT (BU # 841289)	<b>Page</b> 10 of 23
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	<b>Client</b> Crown Castle	<b>Designed by</b> T. Cheriyan

Tower Section	Feed Line Record No.	Description	Feed Line Segment Elev.	K <sub>a</sub> No Ice	K <sub>a</sub> Ice
L6	43	CCI 6.5" x 1.25" Plate	33.00 - 49.90	1.0000	1.0000
L6	44	CCI 6.5" x 1.25" Plate	33.00 - 49.90	1.0000	1.0000
L8	5	FB-L98B-034-XXX(3/8")	0.00 - 32.65	1.0000	1.0000
L8	6	WR-VG82ST-BRDA( 5/8)	0.00 - 32.65	1.0000	1.0000
L8	11	MLE Hybrid 9Power/18Fiber RL 2(1-5/8")	0.00 - 32.65	1.0000	1.0000
L8	18	HB158-1-08U8-S8J18( 1-5/8")	0.00 - 32.65	1.0000	1.0000
L8	20	LDF4-50A(1/2")	0.00 - 32.65	1.0000	1.0000
L8	22	ATCB-B01(5/16")	0.00 - 22.00	1.0000	1.0000
L8	42	CCI 6.5" x 1.25" Plate	29.92 - 32.65	1.0000	1.0000
L8	43	CCI 6.5" x 1.25" Plate	29.92 - 32.65	1.0000	1.0000
L8	44	CCI 6.5" x 1.25" Plate	29.92 - 32.65	1.0000	1.0000

### Discrete Tower Loads

Description	Face or Leg	Offset Type	Offsets: Horz Lateral Vert ft ft ft	Azimuth Adjustment °	Placement ft	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight K
*M*								
*M*								
7770.00 w/ Mount Pipe (E)	A	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.746 1/2" Ice 6.179 1" Ice 6.607	4.254 5.014 5.711	0.055 0.103 0.157
7770.00 w/ Mount Pipe (E)	B	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.746 1/2" Ice 6.179 1" Ice 6.607	4.254 5.014 5.711	0.055 0.103 0.157
7770.00 w/ Mount Pipe (E)	C	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.746 1/2" Ice 6.179 1" Ice 6.607	4.254 5.014 5.711	0.055 0.103 0.157
AM-X-CW-14-65-00T-RET w/ Mount Pipe (E)	A	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.232 1/2" Ice 5.618 1" Ice 6.012	4.015 4.633 5.257	0.049 0.094 0.145
AM-X-CD-14-65-00T-RET w/ Mount Pipe (E)	B	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.232 1/2" Ice 5.618 1" Ice 6.012	4.015 4.633 5.257	0.035 0.080 0.131
AM-X-CD-14-65-00T-RET w/ Mount Pipe (E)	C	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.232 1/2" Ice 5.618 1" Ice 6.012	4.015 4.633 5.257	0.035 0.080 0.131
(2) TT19-08BP111-001 (E)	A	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 0.000 1/2" Ice 0.000 1" Ice 0.000	0.442 0.530 0.626	0.016 0.022 0.029
(2) TT19-08BP111-001 (E)	B	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 0.000 1/2" Ice 0.000 1" Ice 0.000	0.442 0.530 0.626	0.016 0.022 0.029
(2) TT19-08BP111-001 (E)	C	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 0.000 1/2" Ice 0.000 1" Ice 0.000	0.442 0.530 0.626	0.016 0.022 0.029
SBNHH-1D65A w/ Mount Pipe (R)	A	From Leg	4.000 0.000 3.000	0.000	149.000	No Ice 5.954 1/2" Ice 6.390 1" Ice 6.820	5.190 5.961 6.658	0.061 0.114 0.174

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		15:27:21 10/14/16	
<b>Client</b>	Crown Castle	<b>Designed by</b>	
		T. Cheriyan	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz	Vert					
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K
SBNHH-1D65A w/ Mount Pipe (R)	B	From Leg	4.000	0.000	0.000	149.000	No Ice 5.954	5.190	0.061
			0.000				1/2" Ice 6.390	5.961	0.114
			3.000				1" Ice 6.820	6.658	0.174
SBNHH-1D65A w/ Mount Pipe (R)	C	From Leg	4.000	0.000	0.000	149.000	No Ice 5.954	5.190	0.061
			0.000				1/2" Ice 6.390	5.961	0.114
			3.000				1" Ice 6.820	6.658	0.174
WCS RRUS-32-B30 (R)	A	From Leg	4.000	0.000	0.000	149.000	No Ice 3.314	2.424	0.077
			0.000				1/2" Ice 3.558	2.638	0.105
			3.000				1" Ice 3.809	2.860	0.136
WCS RRUS-32-B30 (R)	B	From Leg	4.000	0.000	0.000	149.000	No Ice 3.314	2.424	0.077
			0.000				1/2" Ice 3.558	2.638	0.105
			3.000				1" Ice 3.809	2.860	0.136
WCS RRUS-32-B30 (R)	C	From Leg	4.000	0.000	0.000	149.000	No Ice 3.314	2.424	0.077
			0.000				1/2" Ice 3.558	2.638	0.105
			3.000				1" Ice 3.809	2.860	0.136
DC6-48-60-18-8F (R)	A	From Leg	4.000	0.000	0.000	149.000	No Ice 0.917	0.917	0.019
			0.000				1/2" Ice 1.458	1.458	0.037
			3.000				1" Ice 1.643	1.643	0.057
Platform Mount [LP 403-1] (E)	C	None			0.000	149.000	No Ice 18.850	18.850	1.500
							1/2" Ice 24.300	24.300	1.797
							1" Ice 29.750	29.750	2.093
*M*									
(2) RRUS 11 (E)	A	From Leg	2.000	0.000	0.000	148.000	No Ice 2.784	1.187	0.048
			0.000				1/2" Ice 2.992	1.334	0.068
			2.000				1" Ice 3.207	1.490	0.092
(2) RRUS 11 (E)	B	From Leg	2.000	0.000	0.000	148.000	No Ice 2.784	1.187	0.048
			0.000				1/2" Ice 2.992	1.334	0.068
			2.000				1" Ice 3.207	1.490	0.092
(2) RRUS 11 (E)	C	From Leg	2.000	0.000	0.000	148.000	No Ice 2.784	1.187	0.048
			0.000				1/2" Ice 2.992	1.334	0.068
			2.000				1" Ice 3.207	1.490	0.092
DC6-48-60-18-8F (E-Offset per photo)	A	From Leg	2.000	0.000	0.000	148.000	No Ice 0.917	0.917	0.019
			0.000				1/2" Ice 1.458	1.458	0.037
			-1.000				1" Ice 1.643	1.643	0.057
4' x 2" Pipe Mount (E)	A	From Leg	2.000	0.000	0.000	148.000	No Ice 0.785	0.785	0.029
			0.000				1/2" Ice 1.028	1.028	0.035
			0.000				1" Ice 1.281	1.281	0.044
4' x 2" Pipe Mount (E)	B	From Leg	2.000	0.000	0.000	148.000	No Ice 0.785	0.785	0.029
			0.000				1/2" Ice 1.028	1.028	0.035
			0.000				1" Ice 1.281	1.281	0.044
4' x 2" Pipe Mount (E)	C	From Leg	2.000	0.000	0.000	148.000	No Ice 0.785	0.785	0.029
			0.000				1/2" Ice 1.028	1.028	0.035
			0.000				1" Ice 1.281	1.281	0.044
Side Arm Mount [SO 102-3] (E)	C	None			0.000	148.000	No Ice 3.000	3.000	0.081
							1/2" Ice 3.480	3.480	0.111
							1" Ice 3.960	3.960	0.141
*M*									
AIR 21 B2A/B4P (P)	A	From Leg	4.000	0.000	0.000	140.000	No Ice 5.924	4.219	0.083
			0.000				1/2" Ice 6.288	4.562	0.124
			0.000				1" Ice 6.659	4.913	0.170
AIR 21 B2A/B4P (P)	B	From Leg	4.000	0.000	0.000	140.000	No Ice 5.924	4.219	0.083
			0.000				1/2" Ice 6.288	4.562	0.124
			0.000				1" Ice 6.659	4.913	0.170
AIR 21 B2A/B4P (P)	C	From Leg	4.000	0.000	0.000	140.000	No Ice 5.924	4.219	0.083
			0.000				1/2" Ice 6.288	4.562	0.124
			0.000				1" Ice 6.659	4.913	0.170
AIR 21 B4A/B2P	A	From Leg	4.000	0.000	0.000	140.000	No Ice 5.924	4.219	0.083

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	<b>Project</b>						<b>Date</b>		15:27:21 10/14/16	
	<b>Client</b>		Crown Castle				<b>Designed by</b>		T. Cheriyan	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight
			Horz Lateral	Vert					
(P)			0.000						0.124
AIR 21 B4A/B2P	B	From Leg	4.000		0.000	140.000	No Ice	5.924	0.083
(P)			0.000				1/2" Ice	6.288	0.124
			0.000				1" Ice	6.659	0.170
AIR 21 B4A/B2P	C	From Leg	4.000		0.000	140.000	No Ice	5.924	0.083
(P)			0.000				1/2" Ice	6.288	0.124
			0.000				1" Ice	6.659	0.170
LNX-6515DS-A1M	A	From Leg	4.000		0.000	140.000	No Ice	11.409	0.050
(P)			0.000				1/2" Ice	12.027	0.116
			1.000				1" Ice	12.653	0.189
LNX-6515DS-A1M	B	From Leg	4.000		0.000	140.000	No Ice	11.409	0.050
(P)			0.000				1/2" Ice	12.027	0.116
			1.000				1" Ice	12.653	0.189
LNX-6515DS-A1M	C	From Leg	4.000		0.000	140.000	No Ice	11.409	0.050
(P)			0.000				1/2" Ice	12.027	0.116
			1.000				1" Ice	12.653	0.189
TMAT7LA-11A	A	From Leg	4.000		0.000	140.000	No Ice	0.000	0.022
(P)			0.000				1/2" Ice	0.000	0.029
			0.000				1" Ice	0.000	0.037
TMAT7LA-11A	B	From Leg	4.000		0.000	140.000	No Ice	0.000	0.022
(P)			0.000				1/2" Ice	0.000	0.029
			0.000				1" Ice	0.000	0.037
TMAT7LA-11A	C	From Leg	4.000		0.000	140.000	No Ice	0.000	0.022
(P)			0.000				1/2" Ice	0.000	0.029
			0.000				1" Ice	0.000	0.037
RRUS 11 B12	A	From Leg	4.000		0.000	140.000	No Ice	0.000	0.051
(P)			0.000				1/2" Ice	0.000	0.072
			0.000				1" Ice	0.000	0.095
RRUS 11 B12	B	From Leg	4.000		0.000	140.000	No Ice	0.000	0.051
(P)			0.000				1/2" Ice	0.000	0.072
			0.000				1" Ice	0.000	0.095
RRUS 11 B12	C	From Leg	4.000		0.000	140.000	No Ice	0.000	0.051
(P)			0.000				1/2" Ice	0.000	0.072
			0.000				1" Ice	0.000	0.095
Platform Mount [LP 301-1]	C	None			0.000	140.000	No Ice	30.100	1.589
(P-Includes 4 Mount pipes per sector)							1/2" Ice	40.800	2.029
							1" Ice	51.500	2.470
*M*									
BXA-80080/4CF w/ Mount Pipe	A	From Leg	4.000		0.000	130.000	No Ice	5.037	0.033
(E)			0.000				1/2" Ice	5.421	0.077
			3.000				1" Ice	5.813	0.127
BXA-80080/4CF w/ Mount Pipe	B	From Leg	4.000		0.000	130.000	No Ice	5.037	0.033
(E)			0.000				1/2" Ice	5.421	0.077
			3.000				1" Ice	5.813	0.127
BXA-80080/4CF w/ Mount Pipe	C	From Leg	4.000		0.000	130.000	No Ice	5.037	0.033
(E)			0.000				1/2" Ice	5.421	0.077
			3.000				1" Ice	5.813	0.127
HBXX-6517DS-A2M w/ Mount Pipe	A	From Leg	4.000		0.000	130.000	No Ice	8.765	0.067
(E)			0.000				1/2" Ice	9.342	0.137
			3.000				1" Ice	9.889	0.215
HBXX-6517DS-A2M w/ Mount Pipe	B	From Leg	4.000		0.000	130.000	No Ice	8.765	0.067
(E)			0.000				1/2" Ice	9.342	0.137
			3.000				1" Ice	9.889	0.215
HBXX-6517DS-A2M w/ Mount Pipe	C	From Leg	4.000		0.000	130.000	No Ice	8.765	0.067
(E)			0.000				1/2" Ice	9.342	0.137
			3.000				1" Ice	9.889	0.215

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b>		93496.006.01 - OLD SAYBROOK, CT (BU # 841289)		<b>Page</b>		13 of 23	
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	<b>Client</b>		Crown Castle		<b>Designed by</b>		T. Cheriyan	

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Vert						
			ft	ft	°	ft	ft <sup>2</sup>	ft <sup>2</sup>	K	
LNX-6514DS-A1M w/ Mount Pipe (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	8.411	7.082	0.065
			0.000				1/2" Ice	8.975	8.273	0.134
			3.000				1" Ice	9.505	9.185	0.211
LNX-6514DS-A1M w/ Mount Pipe (E)	B	From Leg	4.000	0.000	0.000	130.000	No Ice	8.411	7.082	0.065
			0.000				1/2" Ice	8.975	8.273	0.134
			3.000				1" Ice	9.505	9.185	0.211
LNX-6514DS-A1M w/ Mount Pipe (E)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	8.411	7.082	0.065
			0.000				1/2" Ice	8.975	8.273	0.134
			3.000				1" Ice	9.505	9.185	0.211
BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	3.179	3.353	0.029
			0.000				1/2" Ice	3.555	3.971	0.061
			3.000				1" Ice	3.930	4.595	0.099
BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	B	From Leg	4.000	0.000	0.000	130.000	No Ice	3.179	3.353	0.029
			0.000				1/2" Ice	3.555	3.971	0.061
			3.000				1" Ice	3.930	4.595	0.099
BXA-171085-8BF-EDIN-0 w/ Mount Pipe (E)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	3.179	3.353	0.029
			0.000				1/2" Ice	3.555	3.971	0.061
			3.000				1" Ice	3.930	4.595	0.099
RRH2X60-PCS (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.723	0.055
			0.000				1/2" Ice	0.000	1.901	0.075
			3.000				1" Ice	0.000	2.087	0.099
RRH2X60-PCS (E)	B	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.723	0.055
			0.000				1/2" Ice	0.000	1.901	0.075
			3.000				1" Ice	0.000	2.087	0.099
RRH2X60-PCS (E)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.723	0.055
			0.000				1/2" Ice	0.000	1.901	0.075
			3.000				1" Ice	0.000	2.087	0.099
RRH2X60-AWS (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.816	0.060
			0.000				1/2" Ice	0.000	2.052	0.083
			3.000				1" Ice	0.000	2.289	0.109
RRH2X60-AWS (E)	B	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.816	0.060
			0.000				1/2" Ice	0.000	2.052	0.083
			3.000				1" Ice	0.000	2.289	0.109
RRH2X60-AWS (E)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	0.000	1.816	0.060
			0.000				1/2" Ice	0.000	2.052	0.083
			3.000				1" Ice	0.000	2.289	0.109
(2) FD9R6004/2C-3L (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	0.314	0.076	0.003
			0.000				1/2" Ice	0.386	0.119	0.005
			3.000				1" Ice	0.466	0.169	0.009
(2) FD9R6004/2C-3L (E)	B	From Leg	4.000	0.000	0.000	130.000	No Ice	0.314	0.076	0.003
			0.000				1/2" Ice	0.386	0.119	0.005
			3.000				1" Ice	0.466	0.169	0.009
(2) FD9R6004/2C-3L (E)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	0.314	0.076	0.003
			0.000				1/2" Ice	0.386	0.119	0.005
			3.000				1" Ice	0.466	0.169	0.009
DB-T1-6Z-8AB-0Z (E)	A	From Leg	4.000	0.000	0.000	130.000	No Ice	4.800	2.000	0.044
			0.000				1/2" Ice	5.070	2.193	0.080
			3.000				1" Ice	5.348	2.393	0.120
Platform Mount [LP 403-1] (E)	C	None			0.000	130.000	No Ice	18.850	18.850	1.500
							1/2" Ice	24.300	24.300	1.797
							1" Ice	29.750	29.750	2.093
*M* FMO (E)	C	From Leg	2.000	0.000	0.000	71.000	No Ice	8.400	8.400	0.010
			0.000				1/2" Ice	8.815	8.815	0.181
			1.000				1" Ice	9.237	9.237	0.361
Side Arm Mount [SO 301-1] (E)	C	From Leg	1.000	0.000	0.000	71.000	No Ice	1.000	0.900	0.023
			0.000				1/2" Ice	1.390	1.420	0.033

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b>	93496.006.01 - OLD SAYBROOK, CT (BU # 841289)	<b>Page</b>	14 of 23
	<b>Project</b>		<b>Date</b>	15:27:21 10/14/16
	<b>Client</b>	Crown Castle		<b>Designed by</b>

Description	Face or Leg	Offset Type	Offsets:		Azimuth Adjustment	Placement	C <sub>AA</sub> Front	C <sub>AA</sub> Side	Weight	
			Horz	Lateral						Vert
*M*										
MYA-43012N (E)	C	From Leg	3.000	0.000	0.000	22.000	No Ice	0.620	0.620	0.005
			0.000				1/2" Ice	1.116	1.116	0.006
			0.000				1" Ice	1.612	1.612	0.008
4' x 2" Pipe Mount (E-For Yagi Per photo)	C	From Leg	3.000	0.000	0.000	22.000	No Ice	0.785	0.785	0.029
			0.000				1/2" Ice	1.028	1.028	0.035
			0.000				1" Ice	1.281	1.281	0.044
Side Arm Mount [SO 701-1] (E)	C	From Leg	1.500	0.000	0.000	22.000	No Ice	0.850	1.670	0.065
			0.000				1/2" Ice	1.140	2.340	0.079
			0.000				1" Ice	1.430	3.010	0.093
*M*										
Yagi (E-Per Photo)	A	From Leg	3.000	0.000	0.000	71.000	No Ice	0.058	0.058	0.010
			0.000				1/2" Ice	0.095	0.095	0.011
			0.000				1" Ice	0.140	0.140	0.013
4' x 2" Pipe Mount (E-For Yagi Per photo)	A	From Leg	3.000	0.000	0.000	71.000	No Ice	0.785	0.785	0.029
			0.000				1/2" Ice	1.028	1.028	0.035
			0.000				1" Ice	1.281	1.281	0.044
Side Arm Mount [SO 701-1] (E)	A	From Leg	1.500	0.000	0.000	71.000	No Ice	0.850	1.670	0.065
			0.000				1/2" Ice	1.140	2.340	0.079
			0.000				1" Ice	1.430	3.010	0.093
*M*										
GPS (3"x7") (E-Per Photo)	C	From Leg	4.000	0.000	0.000	130.000	No Ice	0.175	0.175	0.008
			0.000				1/2" Ice	0.234	0.234	0.010
			4.000				1" Ice	0.301	0.301	0.013
*M*										

## Dishes

Description	Face or Leg	Dish Type	Offset Type	Offsets:		Azimuth Adjustment	3 dB Beam Width	Elevation	Outside Diameter	Aperture Area	Weight	
				Horz	Lateral							Vert
KP4F-23A (E)	B	Grid	From Leg	1.000	0.000	0.000		149.000	4.000	No Ice	12.570	0.070
				0.000						1/2" Ice	13.090	0.140
				7.000						1" Ice	16.130	0.200
*M*												

## Load Combinations

Comb. No.	Description
1	Dead Only
2	1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy
3	1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy
4	1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy
5	1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy

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Comb. No.	Description
6	1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy
7	1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy
8	1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy
9	1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy
10	1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy
11	1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy
12	1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy
13	1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy
14	1.2 Dead+1.0 Ice+1.0 Temp+Guy
15	1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy
16	1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy
17	1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy
18	1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy
19	1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy
20	1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy
21	1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy
22	1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy
23	1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy
24	1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy
25	1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy
26	1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy
27	Dead+Wind 0 deg - Service+Guy
28	Dead+Wind 30 deg - Service+Guy
29	Dead+Wind 60 deg - Service+Guy
30	Dead+Wind 90 deg - Service+Guy
31	Dead+Wind 120 deg - Service+Guy
32	Dead+Wind 150 deg - Service+Guy
33	Dead+Wind 180 deg - Service+Guy
34	Dead+Wind 210 deg - Service+Guy
35	Dead+Wind 240 deg - Service+Guy
36	Dead+Wind 270 deg - Service+Guy
37	Dead+Wind 300 deg - Service+Guy
38	Dead+Wind 330 deg - Service+Guy

### Maximum Member Forces

Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
L1	150 - 123.75	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-25.933	-1.015	0.157
			Max. Mx	5	-9.519	-290.813	-4.794
			Max. My	8	-10.222	-2.540	-282.072
			Max. Vy	5	16.612	-290.813	-4.794
			Max. Vx	8	16.206	-2.540	-282.072
			Max. Torque	7			0.662
L2	123.75 - 110	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	14	-29.885	-1.575	-1.124
			Max. Mx	5	-11.748	-527.990	-8.945
			Max. My	8	-12.500	-3.827	-512.752
			Max. Vy	5	17.918	-527.990	-8.945
			Max. Vx	8	17.343	-3.827	-512.752
			Max. Torque	13			-0.657
L3	110 - 83	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-253.777	-873.943	-386.591
			Max. Mx	5	-237.191	-908.446	-35.052
			Max. My	8	-16.824	-5.709	-855.949
			Max. Vy	5	19.735	-883.396	-15.527
			Max. Vx	8	18.987	-5.709	-855.949
			Max. Torque				

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Section No.	Elevation ft	Component Type	Condition	Gov. Load Comb.	Axial K	Major Axis Moment kip-ft	Minor Axis Moment kip-ft
		Guy A	Max. Torque	6			4.645
			Bottom Tension	6	171.216		
			Top Tension	6	171.695		
			Top Cable Vert	6	167.208		
			Top Cable Norm	6	38.470		
			Top Cable Tan	6	6.371		
			Bot Cable Vert	6	-166.635		
			Bot Cable Norm	6	38.738		
			Bot Cable Tan	6	6.857		
		Guy B	Bottom Tension	12	90.809		
			Top Tension	12	91.167		
			Top Cable Vert	12	82.921		
			Top Cable Norm	12	37.888		
			Top Cable Tan	12	0.128		
			Bot Cable Vert	12	-82.349		
			Bot Cable Norm	12	38.274		
			Bot Cable Tan	12	0.128		
		Guy C	Bottom Tension	4	101.838		
			Top Tension	4	102.191		
			Top Cable Vert	4	93.045		
			Top Cable Norm	4	42.212		
			Top Cable Tan	4	1.934		
			Bot Cable Vert	4	-92.493		
			Bot Cable Norm	4	42.558		
			Bot Cable Tan	4	2.167		
L4	83 - 67.5	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-256.414	-1015.527	-443.755
			Max. Mx	6	-256.414	-1015.527	-443.755
			Max. My	2	-132.073	-2.917	670.658
			Max. Vy	6	12.886	-886.747	-391.732
			Max. Vx	2	12.536	-4.429	633.187
			Max. Torque	6			4.639
L5	67.5 - 49.9	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-262.419	-1225.948	-532.469
			Max. Mx	6	-262.419	-1225.948	-532.469
			Max. My	8	-167.287	-22.723	-564.603
			Max. Vy	6	11.119	-1066.278	-464.490
			Max. Vx	2	11.661	-10.601	480.537
			Max. Torque	6			3.889
L6	49.9 - 33	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-266.109	-1325.695	-577.217
			Max. Mx	6	-266.109	-1325.695	-577.217
			Max. My	6	-266.109	-1325.695	-577.217
			Max. Vy	12	8.580	298.645	130.391
			Max. Vx	2	10.644	-19.155	283.275
			Max. Torque	6			3.880
L7	33 - 32.65	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-268.527	-1356.762	-591.702
			Max. Mx	6	-268.527	-1356.762	-591.702
			Max. My	6	-268.527	-1356.762	-591.702
			Max. Vy	12	7.268	164.022	33.000
			Max. Vx	2	9.205	-26.908	114.828
			Max. Torque	6			3.876
L8	32.65 - 0	Pole	Max Tension	1	0.000	0.000	0.000
			Max. Compression	6	-276.412	-1498.710	-668.590
			Max. Mx	6	-276.412	-1498.710	-668.590
			Max. My	6	-276.412	-1498.710	-668.590
			Max. Vy	12	7.253	161.481	31.134
			Max. Vx	2	9.169	-27.065	111.610
			Max. Torque	6			3.876

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### Maximum Reactions

Location	Condition	Gov. Load Comb.	Vertical K	Horizontal, X K	Horizontal, Z K
Mast	Max. Vert	6	276.414	-2.015	-1.508
	Max. H <sub>x</sub>	3	133.398	1.660	-5.014
	Max. H <sub>z</sub>	8	185.304	-0.353	1.951
	Max. M <sub>x</sub>	21	-41.419	-0.384	0.695
	Max. M <sub>z</sub>	6	1498.710	-2.015	-1.508
	Max. Torsion	6	3.555	-2.015	-1.508
	Min. Vert	32	106.743	0.017	-0.134
	Min. H <sub>x</sub>	12	153.950	-4.488	-3.468
	Min. H <sub>z</sub>	4	205.275	-0.560	-5.935
	Min. M <sub>x</sub>	6	-668.591	-2.015	-1.508
	Min. M <sub>z</sub>	9	-268.824	-0.930	1.094
	Min. Torsion	9	-2.119	-0.930	1.094
	Guy C @ 42 ft Elev 0 ft Azimuth 211 deg	Max. Vert	9	-0.556	-0.056
Max. H <sub>x</sub>		10	-0.701	-0.001	0.222
Max. H <sub>z</sub>		4	-92.493	-23.595	35.485
Min. Vert		4	-92.493	-23.595	35.485
Min. H <sub>x</sub>		5	-88.357	-23.750	33.141
Min. H <sub>z</sub>		9	-0.556	-0.056	0.091
Guy B @ 42.5 ft Elev 0 ft Azimuth 120 deg	Max. Vert	6	-0.298	-0.005	-0.001
	Max. H <sub>x</sub>	12	-82.349	33.210	19.026
	Max. H <sub>z</sub>	12	-82.349	33.210	19.026
	Min. Vert	12	-82.349	33.210	19.026
	Min. H <sub>x</sub>	6	-0.298	-0.005	-0.001
	Min. H <sub>z</sub>	7	-0.457	0.128	-0.051
Guy A @ 20.5 ft Elev 0 ft Azimuth 0 deg	Max. Vert	2	-4.315	-0.004	-0.686
	Max. H <sub>x</sub>	10	-127.419	1.745	-28.876
	Max. H <sub>z</sub>	2	-4.315	-0.004	-0.686
	Min. Vert	6	-166.635	-6.857	-38.738
	Min. H <sub>x</sub>	6	-166.635	-6.857	-38.738
	Min. H <sub>z</sub>	6	-166.635	-6.857	-38.738

### Tower Mast Reaction Summary

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Dead Only	111.994	0.340	0.855	66.889	-40.150	-0.012
1.2 Dead+1.6 Wind 0 deg - No Ice+1.0 Guy	154.188	0.328	5.713	134.698	-39.431	-0.828
1.2 Dead+1.6 Wind 30 deg - No Ice+1.0 Guy	133.398	-1.660	5.014	141.956	-69.232	-0.661
1.2 Dead+1.6 Wind 60 deg - No Ice+1.0 Guy	205.275	0.560	5.935	446.927	-769.956	-0.327
1.2 Dead+1.6 Wind 90 deg - No Ice+1.0 Guy	259.683	1.118	4.269	633.795	-1286.445	-1.854

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	<p><b>Client</b></p> <p style="text-align: center;">Crown Castle</p>	<p><b>Designed by</b></p> <p style="text-align: center;">T. Cheriyan</p>

Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
1.2 Dead+1.6 Wind 120 deg - No Ice+1.0 Guy	276.414	2.015	1.508	668.591	-1498.710	-3.555
1.2 Dead+1.6 Wind 150 deg - No Ice+1.0 Guy	224.562	3.894	-0.732	445.398	-1081.558	-2.613
1.2 Dead+1.6 Wind 180 deg - No Ice+1.0 Guy	185.304	0.353	-1.951	283.717	-57.518	0.668
1.2 Dead+1.6 Wind 210 deg - No Ice+1.0 Guy	226.202	0.930	-1.094	384.371	268.824	2.119
1.2 Dead+1.6 Wind 240 deg - No Ice+1.0 Guy	237.791	3.313	0.550	398.163	239.998	1.732
1.2 Dead+1.6 Wind 270 deg - No Ice+1.0 Guy	200.471	4.402	2.341	271.977	104.912	0.451
1.2 Dead+1.6 Wind 300 deg - No Ice+1.0 Guy	153.950	4.488	3.468	114.254	-32.401	-0.583
1.2 Dead+1.6 Wind 330 deg - No Ice+1.0 Guy	157.015	2.680	5.168	133.707	-41.891	-0.730
1.2 Dead+1.0 Ice+1.0 Temp+Guy	129.413	0.270	0.585	54.727	-33.685	-0.005
1.2 Dead+1.0 Wind 0 deg+1.0 Ice+1.0 Temp+1.0 Guy	134.063	0.450	2.042	81.572	-35.623	-0.264
1.2 Dead+1.0 Wind 30 deg+1.0 Ice+1.0 Temp+1.0 Guy	131.557	-0.293	1.750	77.020	-39.580	-0.085
1.2 Dead+1.0 Wind 60 deg+1.0 Ice+1.0 Temp+1.0 Guy	136.749	-0.328	1.572	100.317	-103.881	-0.008
1.2 Dead+1.0 Wind 90 deg+1.0 Ice+1.0 Temp+1.0 Guy	147.490	0.302	1.261	134.858	-211.728	-0.017
1.2 Dead+1.0 Wind 120 deg+1.0 Ice+1.0 Temp+1.0 Guy	151.570	0.801	0.716	144.657	-261.987	-0.092
1.2 Dead+1.0 Wind 150 deg+1.0 Ice+1.0 Temp+1.0 Guy	137.965	0.488	-0.212	83.037	-146.266	-0.114
1.2 Dead+1.0 Wind 180 deg+1.0 Ice+1.0 Temp+1.0 Guy	128.372	0.384	-0.695	41.419	-50.203	0.016
1.2 Dead+1.0 Wind 210 deg+1.0 Ice+1.0 Temp+1.0 Guy	132.205	0.781	-0.428	50.049	-22.083	0.118
1.2 Dead+1.0 Wind 240 deg+1.0 Ice+1.0 Temp+1.0 Guy	136.351	1.469	0.132	59.646	-26.024	0.271
1.2 Dead+1.0 Wind 270 deg+1.0 Ice+1.0 Temp+1.0 Guy	136.886	1.582	0.744	62.434	-29.221	0.170
1.2 Dead+1.0 Wind 300 deg+1.0 Ice+1.0 Temp+1.0 Guy	137.648	1.440	1.324	66.758	-30.126	-0.097
1.2 Dead+1.0 Wind 330 deg+1.0 Ice+1.0 Temp+1.0 Guy	136.108	1.059	1.820	77.113	-36.609	-0.229
Dead+Wind 0 deg - Service+Guy	115.937	0.341	1.707	81.403	-40.180	-0.156
Dead+Wind 30 deg - Service+Guy	113.194	-0.042	1.578	79.176	-41.071	-0.182
Dead+Wind 60 deg - Service+Guy	110.304	-0.322	1.289	74.897	-43.086	-0.132
Dead+Wind 90 deg - Service+Guy	109.096	-0.336	0.905	72.352	-53.483	-0.071
Dead+Wind 120 deg - Service+Guy	109.727	-0.106	0.535	73.176	-71.884	-0.027
Dead+Wind 150 deg - Service+Guy	106.743	-0.017	0.134	56.056	-44.311	0.055
Dead+Wind 180 deg - Service+Guy	108.033	0.339	0.014	52.874	-40.581	0.129
Dead+Wind 210 deg - Service+Guy	110.734	0.713	0.129	54.661	-39.411	0.177
Dead+Wind 240 deg - Service+Guy	113.852	1.020	0.423	59.599	-39.164	0.129
Dead+Wind 270 deg -	116.455	1.131	0.851	66.821	-39.246	0.038

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Load Combination	Vertical K	Shear <sub>x</sub> K	Shear <sub>z</sub> K	Overturning Moment, M <sub>x</sub> kip-ft	Overturning Moment, M <sub>z</sub> kip-ft	Torque kip-ft
Service+Guy Dead+Wind 300 deg - Service+Guy	118.143	1.044	1.299	74.010	-38.222	-0.037
Service+Guy Dead+Wind 330 deg - Service+Guy	117.650	0.732	1.604	79.758	-39.659	-0.099

### Solution Summary

Load Comb.	Sum of Applied Forces			Sum of Reactions			% Error
	PX K	PY K	PZ K	PX K	PY K	PZ K	
1	0.000	-36.069	0.000	-0.000	36.069	0.000	0.000%
2	-0.049	-43.156	-29.586	0.049	43.156	29.586	0.000%
3	14.748	-43.097	-25.545	-14.748	43.097	25.545	0.000%
4	25.810	-43.025	-14.862	-25.810	43.025	14.861	0.001%
5	29.704	-42.960	0.053	-29.704	42.960	-0.053	0.000%
6	27.098	-42.905	15.685	-27.098	42.904	-15.685	0.000%
7	14.857	-42.871	25.697	-14.857	42.871	-25.696	0.000%
8	0.069	-42.885	29.595	-0.069	42.885	-29.595	0.000%
9	-14.689	-42.944	25.579	14.689	42.944	-25.579	0.000%
10	-25.793	-43.017	14.874	25.793	43.017	-14.874	0.000%
11	-29.704	-43.081	-0.032	29.704	43.081	0.032	0.000%
12	-27.064	-43.137	-15.665	27.064	43.137	15.665	0.000%
13	-14.839	-43.170	-25.707	14.839	43.170	25.707	0.000%
14	0.000	-76.429	0.000	0.000	76.429	0.000	0.000%
15	-0.207	-76.497	-6.532	0.207	76.497	6.532	0.000%
16	3.354	-76.469	-5.813	-3.354	76.469	5.813	0.000%
17	5.805	-76.434	-3.321	-5.805	76.434	3.321	0.000%
18	6.954	-76.401	0.013	-6.955	76.401	-0.013	0.000%
19	6.458	-76.373	3.732	-6.458	76.373	-3.732	0.000%
20	3.262	-76.355	5.631	-3.262	76.355	-5.631	0.000%
21	0.030	-76.361	6.466	-0.030	76.361	-6.466	0.000%
22	-3.351	-76.389	5.815	3.351	76.389	-5.815	0.000%
23	-5.949	-76.424	3.199	5.949	76.424	-3.199	0.000%
24	-7.027	-76.457	-0.130	7.027	76.457	0.130	0.000%
25	-6.525	-76.485	-3.771	6.525	76.485	3.771	0.000%
26	-3.400	-76.503	-5.635	3.400	76.503	5.635	0.000%
27	-0.009	-36.094	-5.402	0.009	36.094	5.402	0.000%
28	2.693	-36.083	-4.664	-2.693	36.083	4.664	0.000%
29	4.713	-36.070	-2.714	-4.713	36.070	2.714	0.000%
30	5.424	-36.058	0.010	-5.424	36.058	-0.010	0.000%
31	4.948	-36.048	2.864	-4.948	36.048	-2.864	0.001%
32	2.713	-36.041	4.692	-2.713	36.041	-4.692	0.000%
33	0.013	-36.044	5.404	-0.013	36.044	-5.404	0.000%
34	-2.682	-36.055	4.671	2.682	36.055	-4.671	0.000%
35	-4.710	-36.068	2.716	4.710	36.068	-2.716	0.000%
36	-5.424	-36.080	-0.006	5.424	36.080	0.006	0.000%
37	-4.942	-36.090	-2.860	4.942	36.090	2.860	0.000%
38	-2.710	-36.096	-4.694	2.710	36.096	4.694	0.000%

### Non-Linear Convergence Results

<p><b>tnxTower</b></p> <p><b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265</p>	<p><b>Job</b> 93496.006.01 - OLD SAYBROOK, CT (BU # 841289)</p>	<p><b>Page</b> 20 of 23</p>
	<p><b>Project</b></p>	<p><b>Date</b> 15:27:21 10/14/16</p>
	<p><b>Client</b> Crown Castle</p>	<p><b>Designed by</b> T. Cheriyan</p>

Load Combination	Converged?	Number of Cycles	Displacement Tolerance	Force Tolerance
1	Yes	4	0.00000001	0.00028035
2	Yes	5	0.00000001	0.00056951
3	Yes	6	0.00000001	0.00046512
4	Yes	8	0.00000001	0.00055372
5	Yes	10	0.00001998	0.00058266
6	Yes	11	0.00000001	0.00045521
7	Yes	9	0.00000001	0.00062715
8	Yes	7	0.00000001	0.00013406
9	Yes	8	0.00000001	0.00022309
10	Yes	8	0.00000001	0.00024555
11	Yes	7	0.00000001	0.00021682
12	Yes	6	0.00000001	0.00014677
13	Yes	6	0.00000001	0.00018485
14	Yes	5	0.00000001	0.00044921
15	Yes	5	0.00000001	0.00085939
16	Yes	6	0.00000001	0.00018082
17	Yes	8	0.00000001	0.00018073
18	Yes	8	0.00000001	0.00051729
19	Yes	8	0.00000001	0.00059832
20	Yes	8	0.00000001	0.00029900
21	Yes	7	0.00000001	0.00009855
22	Yes	6	0.00000001	0.00081406
23	Yes	6	0.00000001	0.00077116
24	Yes	6	0.00000001	0.00015063
25	Yes	6	0.00000001	0.00010530
26	Yes	5	0.00000001	0.00090585
27	Yes	4	0.00000001	0.00066111
28	Yes	4	0.00000001	0.00091753
29	Yes	5	0.00000001	0.00006393
30	Yes	6	0.00000001	0.00015111
31	Yes	6	0.00000001	0.00058356
32	Yes	5	0.00000001	0.00020056
33	Yes	4	0.00000001	0.00092114
34	Yes	4	0.00000001	0.00077709
35	Yes	4	0.00000001	0.00079631
36	Yes	4	0.00000001	0.00066515
37	Yes	4	0.00000001	0.00067571
38	Yes	4	0.00000001	0.00061501

### Maximum Tower Deflections - Service Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 123.75	13.473	31	1.110	0.003
L2	123.75 - 110	7.863	31	0.847	0.001
L3	110 - 83	5.666	31	0.672	0.001
L4	83 - 67.5	2.726	31	0.383	0.000
L5	71 - 49.9	1.901	31	0.282	0.000
L6	49.9 - 33	0.896	31	0.174	0.000
L7	37 - 32.65	0.493	31	0.127	0.000
L8	32.65 - 0	0.380	31	0.120	0.000

### Critical Deflections and Radius of Curvature - Service Wind

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	<b>Client</b> Crown Castle	<b>Designed by</b> T. Cheriyan

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
156.000	KP4F-23A	31	13.473	1.110	0.003	16638
149.000	7770.00 w/ Mount Pipe	31	13.244	1.101	0.003	16638
148.000	(2) RRUS 11	31	13.014	1.092	0.003	16638
140.000	AIR 21 B2A/B4P	31	11.200	1.019	0.002	8319
130.000	BXA-80080/4CF w/ Mount Pipe	31	9.066	0.918	0.002	4159
91.100	Guy	31	3.437	0.461	0.000	5529
71.000	FMO	31	1.901	0.282	0.000	9389
22.000	MYA-43012N	31	0.182	0.093	0.000	15777

### Maximum Tower Deflections - Design Wind

Section No.	Elevation ft	Horz. Deflection in	Gov. Load Comb.	Tilt °	Twist °
L1	150 - 123.75	135.231	6	8.818	0.119
L2	123.75 - 110	89.746	6	7.350	0.082
L3	110 - 83	70.014	6	6.364	0.059
L4	83 - 67.5	38.950	6	4.655	0.020
L5	71 - 49.9	28.338	6	3.814	0.009
L6	49.9 - 33	14.014	6	2.616	0.004
L7	37 - 32.65	7.819	6	1.986	0.003
L8	32.65 - 0	6.055	6	1.881	0.003

### Critical Deflections and Radius of Curvature - Design Wind

Elevation	Appurtenance	Gov. Load Comb.	Deflection in	Tilt °	Twist °	Radius of Curvature ft
156.000	KP4F-23A	6	135.231	8.818	0.145	3238
149.000	7770.00 w/ Mount Pipe	6	133.411	8.768	0.143	3238
148.000	(2) RRUS 11	6	131.591	8.718	0.142	3238
140.000	AIR 21 B2A/B4P	6	117.151	8.311	0.128	1617
130.000	BXA-80080/4CF w/ Mount Pipe	6	99.837	7.750	0.111	805
91.100	Guy	6	47.228	5.178	0.041	882
71.000	FMO	6	28.338	3.814	0.017	990
22.000	MYA-43012N	6	2.937	1.466	0.004	1019

### Guy Design Data

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual $T_u$ K	Allowable $\phi T_n$ K	Required S.F.	Actual S.F.
L3	91.100 (A)	1 5/8 BS	38.880	324.001	171.695	194.400	1.000	1.132 ✓
	(11)							
	91.100 (B) (10)	1 3/8 BS	27.840	232.000	91.167	139.200	1.000	1.527 ✓
	91.100 (C) (9)	1 3/8 BS	27.840	232.000	102.191	139.200	1.000	1.362 ✓

<b>tnxTower</b>  <b>B+T Group</b> 1717 S. Boulder, Suite 300 Tulsa, OK 74119 Phone: (918) 587 - 4630 FAX: (918) 295 - 0265	<b>Job</b>	93496.006.01 - OLD SAYBROOK, CT (BU # 841289)	<b>Page</b>	22 of 23
	<b>Project</b>		<b>Date</b>	15:27:21 10/14/16
	<b>Client</b>	Crown Castle	<b>Designed by</b>	T. Cheriyan

Section No.	Elevation ft	Size	Initial Tension K	Breaking Load K	Actual $T_u$ K	Allowable $\phi T_n$ K	Required S.F.	Actual S.F.
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### Compression Checks

### Pole Design Data

Section No.	Elevation ft	Size	L ft	$L_u$ ft	Kl/r	A $in^2$	$P_u$ K	$\phi P_n$ K	Ratio $\frac{P_u}{\phi P_n}$
L1	150 - 123.75 (1)	TP19.625x15.53x0.25	26.250	0.000	0.0	15.597	-9.265	1149.650	0.008
L2	123.75 - 110 (2)	TP21.77x19.625x0.482	13.750	0.000	0.0	33.011	-11.413	1427.660	0.008
L3	110 - 83 (3)	TP26.134x21.77x0.668	27.000	0.000	0.0	54.817	-253.777	2644.140	0.096
L4	83 - 67.5 (4)	TP28.64x26.134x0.545	15.500	0.000	0.0	45.770	-254.426	2190.530	0.116
L5	67.5 - 49.9 (5)	TP30.898x27.449x0.585	21.100	0.000	0.0	51.653	-258.029	2481.030	0.104
L6	49.9 - 33 (6)	TP33.66x30.898x0.644	16.900	0.000	0.0	62.716	-262.428	3057.690	0.086
L7	33 - 32.65 (7)	TP32.966x32.256x0.71	4.350	0.000	0.0	73.583	-268.417	3587.910	0.075
L8	32.65 - 0 (8)	TP38.29x32.966x0.438	32.650	0.000	0.0	45.824	-268.535	3377.690	0.080

### Pole Bending Design Data

Section No.	Elevation ft	Size	$M_{ux}$ kip-ft	$\phi M_{nx}$ kip-ft	Ratio $\frac{M_{ux}}{\phi M_{nx}}$	$M_{uy}$ kip-ft	$\phi M_{ny}$ kip-ft	Ratio $\frac{M_{uy}}{\phi M_{ny}}$
L1	150 - 123.75 (1)	TP19.625x15.53x0.25	296.534	451.558	0.657	0.000	451.558	0.000
L2	123.75 - 110 (2)	TP21.77x19.625x0.482	543.503	610.282	0.891	0.000	610.282	0.000
L3	110 - 83 (3)	TP26.134x21.77x0.668	955.633	1347.308	0.709	0.000	1347.308	0.000
L4	83 - 67.5 (4)	TP28.64x26.134x0.545	996.392	1148.817	0.867	0.000	1148.817	0.000
L5	67.5 - 49.9 (5)	TP30.898x27.449x0.585	1150.625	1368.608	0.841	0.000	1368.608	0.000
L6	49.9 - 33 (6)	TP33.66x30.898x0.644	1336.567	1859.975	0.719	0.000	1859.975	0.000
L7	33 - 32.65 (7)	TP32.966x32.256x0.71	1477.367	2321.067	0.637	0.000	2321.067	0.000
L8	32.65 - 0 (8)	TP38.29x32.966x0.438	1480.150	2226.133	0.665	0.000	2226.133	0.000

### Pole Shear Design Data

Section No.	Elevation ft	Size	Actual $V_u$ K	$\phi V_n$ K	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ kip-ft	$\phi T_n$ kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L1	150 - 123.75 (1)	TP19.625x15.53x0.25	16.991	574.823	0.030	0.556	915.617	0.001
L2	123.75 - 110 (2)	TP21.77x19.625x0.482	19.022	713.832	0.027	0.406	1237.458	0.000

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	<b>Project</b>	<b>Date</b> 15:27:21 10/14/16
	<b>Client</b> Crown Castle	<b>Designed by</b> T. Cheriyan

Section No.	Elevation ft	Size	Actual $V_u$ K	$\phi V_n$ K	Ratio $\frac{V_u}{\phi V_n}$	Actual $T_u$ kip-ft	$\phi T_n$ kip-ft	Ratio $\frac{T_u}{\phi T_n}$
L3	110 - 83 (3)	TP26.134x21.77x0.668	14.104	1322.070	0.011	4.640	2731.917	0.002
L4	83 - 67.5 (4)	TP28.64x26.134x0.545	13.501	1095.260	0.012	4.637	2329.433	0.002
L5	67.5 - 49.9 (5)	TP30.898x27.449x0.585	12.057	1248.160	0.010	3.889	2775.117	0.001
L6	49.9 - 33 (6)	TP33.66x30.898x0.644	9.204	1537.720	0.006	3.880	3771.450	0.001
L7	33 - 32.65 (7)	TP32.966x32.256x0.71	8.038	1797.130	0.004	3.876	4706.400	0.001
L8	32.65 - 0 (8)	TP38.29x32.966x0.438	7.797	1702.660	0.005	3.876	4513.900	0.001

### Pole Interaction Design Data

Section No.	Elevation ft	Ratio $P_u$ $\phi P_n$	Ratio $M_{ux}$ $\phi M_{ux}$	Ratio $M_{uy}$ $\phi M_{uy}$	Ratio $V_u$ $\phi V_n$	Ratio $T_u$ $\phi T_n$	Comb. Stress Ratio	Allow. Stress Ratio	Criteria
L1	150 - 123.75 (1)	0.008	0.657	0.000	0.030	0.001	0.666	1.000	4.8.2 ✓
L2	123.75 - 110 (2)	0.008	0.891	0.000	0.027	0.000	0.899	1.000	4.8.2 ✓
L3	110 - 83 (3)	0.096	0.709	0.000	0.011	0.002	0.805	1.000	4.8.2 ✓
L4	83 - 67.5 (4)	0.116	0.867	0.000	0.012	0.002	0.984	1.000	4.8.2 ✓
L5	67.5 - 49.9 (5)	0.104	0.841	0.000	0.010	0.001	0.945	1.000	4.8.2 ✓
L6	49.9 - 33 (6)	0.086	0.719	0.000	0.006	0.001	0.804	1.000	4.8.2 ✓
L7	33 - 32.65 (7)	0.075	0.637	0.000	0.004	0.001	0.711	1.000	4.8.2 ✓
L8	32.65 - 0 (8)	0.080	0.665	0.000	0.005	0.001	0.744	1.000	4.8.2 ✓

### Section Capacity Table

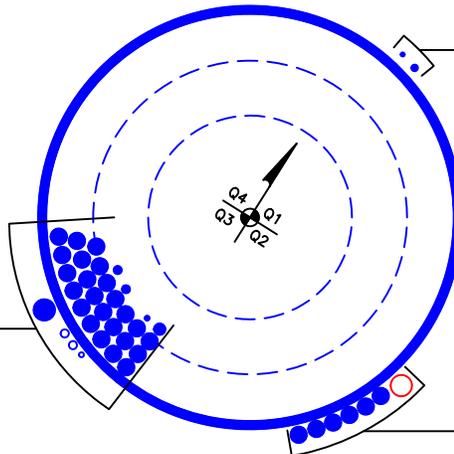
Section No.	Elevation ft	Component Type	Size	Critical Element	P K	$\phi P_{allow}$ K	% Capacity	Pass Fail
L1	150 - 123.75	Pole	TP19.625x15.53x0.25	1	-9.265	1149.650	66.6	Pass
L2	123.75 - 110	Pole	TP21.77x19.625x0.482	2	-11.413	1427.660	89.9	Pass
L3	110 - 83	Pole	TP26.134x21.77x0.668	3	-253.777	2644.140	80.5	Pass
		Guy A@91.1	1 5/8	11	171.695	194.400	88.3	Pass
		Guy B@91.1	1 3/8	10	91.167	139.200	65.5	Pass
		Guy C@91.1	1 3/8	9	102.191	139.200	73.4	Pass
L4	83 - 67.5	Pole	TP28.64x26.134x0.545	4	-254.426	2190.530	98.4	Pass
L5	67.5 - 49.9	Pole	TP30.898x27.449x0.585	5	-258.029	2481.030	94.5	Pass
L6	49.9 - 33	Pole	TP33.66x30.898x0.644	6	-262.428	3057.690	80.4	Pass
L7	33 - 32.65	Pole	TP32.966x32.256x0.71	7	-268.417	3587.910	71.1	Pass
L8	32.65 - 0	Pole	TP38.29x32.966x0.438	8	-268.535	3377.690	74.4	Pass
Summary								
Pole (L4)							98.4	Pass
Guy A (L3)							88.3	Pass
Guy B (L3)							65.5	Pass
Guy C (L3)							73.4	Pass
<b>RATING =</b>							<b>98.4</b>	<b>Pass</b>

**APPENDIX B**  
**BASE LEVEL DRAWING**

(INSTALLED)  
(1) 1-5/8" TO 130 FT LEVEL  
(12) 1-1/4" TO 130 FT LEVEL

(RESERVED)  
(1) 3/8" TO 149 FT LEVEL  
(2) 5/8" TO 149 FT LEVEL

(INSTALLED)  
(1) 3/8" TO 148 FT LEVEL  
(2) 5/8" TO 148 FT LEVEL  
(1) 7/8" TO 149 FT LEVEL  
(12) 1-1/4" TO 149 FT LEVEL



(INSTALLED)  
(1) 5/16" TO 22 FT LEVEL  
(1) 1/2" TO 71 FT LEVEL

(PROPOSED)  
(1) 1-5/8" TO 140 FT LEVEL  
(INSTALLED - TO BE RELOCATED FROM 160')  
(6) 1-1/4" TO 140 FT LEVEL

BUSINESS UNIT: 841289

**APPENDIX C**  
**ADDITIONAL CALCULATIONS**

PROJECT	<b>93496.007.01 - OLD SAYBROOK, CT</b>		
SUBJECT	<b>Bridge Stiffeners @ 110'</b>		
DATE	<b>10/14/16</b>	PAGE	1 OF 1



**B+T GRP**  
 1717 S. Boulder, Suite 300  
 Tulsa, OK 74159  
 (918) 587-4630

0

**Determine Load to Bridge Stiffener:**

**M = 545.8 k-ft** From Risa Model  
**I = 3417.9 in<sup>4</sup>** From AutoCAD Sketch  
**ybar = 14.630 in**  
**S = 233.63 in<sup>3</sup>** I/y  
**fc = 28.04 ksi** M/S  
**Ag = 8.125 in<sup>2</sup>**  
**Pu = 227.79 k** fc x Ag

<b>Stiffener Width</b>	<b>6.500 in</b>
<b>Stiffener Thickness</b>	<b>1.250 in</b>
<b>Stiffener Height</b>	<b>166.000 in</b>
<b>Fy</b>	<b>65 ksi</b>
<b>Fu</b>	<b>80 ksi</b>
<b>Step Width</b>	<b>3.00 in</b>
<b>Bolt Circle</b>	<b>25.50 in</b>
<b>Number of Bolts</b>	<b>12</b>
<b>Bolt Size</b>	<b>1</b>
<b>Gap @ Flange</b>	<b>6.00 in</b>

**Determine  $\Phi P_n$  (Allowable Axial Load):**

**Pn = Fcr x Ag** Eqn E3-1, AISC 13th Edition, Section E3.  
**K = 0.99**  
**I = 16.000 in** Unsupported Length  
**ly = 1.058 in<sup>4</sup>** Local Weak Axis Moment of Intertia  
**Ag = 8.125 in<sup>2</sup>** Stiffener Cross Sectional Area  
**ry = .361 in** Radius of Gyration (Weak Axis)  
**kl/r = 43.90**  
**4.71 x  $\sqrt{E/Fy}$  = 99.49** Limit State Equation for Flexural Buckling - AISC 13th Edition, Section E3.  
**Fe = 148.53 ksi** Eqn E3-4 - AISC 13th Edition, Section E3.  
 Elastic Critical Buckling Stress  
**Fcr = 54.12 ksi** Eqn E3-2, AISC 13th Edition, Section E3  
 Critical Buckling Stress  
**Pn = 439.73 k** Nominal Compressive Strength  
 **$\Phi P_n = 395.76 k$**  Allowable Compressive Strength **Unity% = 57.6 %**

**Tension Rupture Check:**

AISC 13th Edition, Chapter J4.1

**Hole Size = 1.25**  
**U = 1** Shear Lag Factor - Table D3.1 and TIA222-G  
**Ag = 8.125 in<sup>2</sup>** Gross Area  
**An = 6.563 in<sup>2</sup>** Net Area  
**Ae = 6.563 in<sup>2</sup>** Effective Area  
 **$\Phi R_n = 475.31 k$**  Tension Yielding: Eqn J4-1  
 **$\Phi R_n = 393.75 k$**  Tension Rupture: Eqn J4-2  
 **$\Phi R_n(\text{Equiv}) = 393.75 ksi$**   
**Unity% = 57.85 %**

**Moment to Existing Bolt Group:**

**S<sub>BG</sub> = 268.07 in<sup>3</sup>** # Bolts Acting **3**  
**ft = 24.43 ksi**  
**Ab = .785 in<sup>2</sup>**  
**T = 57.57 k**  
**Arm = 25.50 ksi**  
**M<sub>EQ</sub> = 122.3 k-ft** <-----Insert into Flange Spreadsheet

# Stiffened or Unstiffened, Exterior Flange Plate - Any Bolt Material TIA Rev G

## Site Data

BU#: 841289  
 Site Name: OLD SAYBROOK, CT  
 App #: 362261, Rev. 1

Reactions		
Mu	122.3	ft-kips
Axial, Pu:	11.422	kips
Shear, Vu:	19.12	kips
Elevation:	110	feet

Bolt Threads:	
X-Excluded	
$\phi V_n = \phi(0.55 A_b F_u)$	
$\phi = 0.75, \phi^* V_n$ (kips):	
38.88	

Pole Manufacturer: Other

Bolt Data		
Qty:	12	
Diameter (in.):	1	Bolt Fu: 120
Bolt Material:	A325	Bolt Fy: 92
N/A:	75	<-- Disregard
N/A:	55	<-- Disregard
Circle (in.):	25.5	

Plate Data		
Diam:	28	in
Thick, t:	1	in
Grade (Fy):	36	ksi
Strength, Fu:	58	ksi
Single-Rod B-eff:	5.83	in

Stiffener Data (Welding at Both Sides)		
Config:	0	*
Weld Type:	Fillet	
Groove Depth:	0.25	<-- Disregard
Groove Angle:	45	<-- Disregard
Fillet H. Weld:	0.3125	in
Fillet V. Weld:	0.3125	in
Width:	3	in
Height:	18	in
Thick:	0.75	in
Notch:	0.5	in
Grade:	36	ksi
Weld str.:	70	ksi

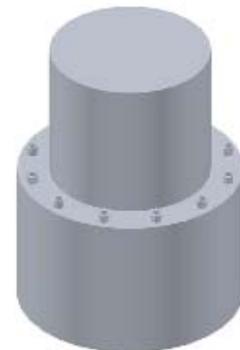
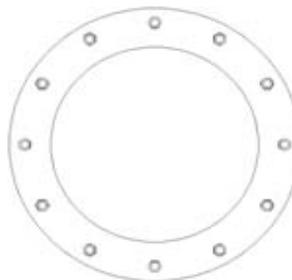
Pole Data		
Diam:	21.77	in
Thick:	0.22	in
Grade:	65	ksi
# of Sides:	12	"0" IF Round
Fu	80	ksi
Reinf. Fillet Weld	0	"0" if None

If No stiffeners, Criteria: TIA G <-Only Applicable to Unstiffened Cases

Flange Bolt Results		Rigid	
Bolt Tension Capacity, $\phi^* T_n, B1$ :	54.54 kips	$\phi^* T_n$	
Adjusted $\phi^* T_n$ (due to $V_u = V_u / Q_t$ ), B:	54.49 kips	$\phi T_n [(1 - (V_u / \phi V_n)^2)^{0.5}]$	
Max Bolt directly applied $T_u$ :	18.23 Kips		
Min. PL "tc" for B cap. w/o Pry:	1.000 in		
Min PL "treq" for actual T w/ Pry:	0.429 in		
Min PL "t1" for actual T w/o Pry:	0.578 in		
T allowable w/o Prying:	54.54 kips	$\alpha < 0$ case	
Prying Force, q:	0.00 kips		
Total Bolt Tension = $T_u + q$ :	18.23 kips		
Non-Prying Bolt Stress Ratio, $T_u / B$ :	33.5% Pass		

Exterior Flange Plate Results		Flexural Check		Rigid	
Compression Side Plate Stress:	16.8 ksi	TIA G		$\phi^* F_y$	
Allowable Plate Stress:	32.4 ksi	Comp. Y.L. Length:		13.28	
Compression Plate Stress Ratio:	51.8% Pass				
<b>No Prying</b>					
Tension Side Stress Ratio, $(treq/t)^2$ :	18.4% Pass				

n/a  
**Stiffener Results**  
 Horizontal Weld : n/a  
 Vertical Weld: n/a  
 Plate Flex+Shear,  $f_b / F_b + (f_v / F_v)^2$ : n/a  
 Plate Tension+Shear,  $f_t / F_t + (f_v / F_v)^2$ : n/a  
 Plate Comp. (AISC Bracket): n/a  
**Pole Results**  
 Pole Punching Shear Check: n/a



\* 0 = none, 1 = every bolt, 2 = every 2 bolts, 3 = 2 per bolt

\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

## Square, Stiffened / Unstiffened Base Plate, Any Rod Material - Rev. F / G

- Assumptions:** 1) Rod groups at corners. Total # rods divisible by 4. Maximum total # of rods = 48 (12 per Corner).  
 2) Rod Spacing = Straight Center-to-Center distance between any (2) adjacent rods (same corner)  
 3) Clear space between bottom of leveling nut and top of concrete **not** exceeding (1)\*(Rod Diameter)

### Site Data

BU#: 841289  
 Site Name: OLD SAYBROOK  
 App #: 362261 Rev. 1

### Anchor Rod Data

Eta Factor, $\eta$	0.5	TIA G (Fig. 4-4)
Qty:	8	
Diam:	2.25	in
Rod Material:	A615-J	
Yield, Fy:	75	ksi
Strength, Fu:	100	ksi
Bolt Circle:	44	in
Anchor Spacing:	6	in

### Plate Data

W=Side:	49	in
Thick:	2.5	in
Grade:	50	ksi
Clip Distance:	6	in

### Stiffener Data (Welding at both sides)

Configuration:	Unstiffened	
Weld Type:		**
Groove Depth:		in **
Groove Angle:		degrees
Fillet H. Weld:		<-- Disregard
Fillet V. Weld:		in
Width:		in
Height:		in
Thick:		in
Notch:		in
Grade:		ksi
Weld str.:		ksi

### Pole Data

Diam:	38.29	in
Thick:	0.4375	in
Grade:	65	ksi
# of Sides:	12	"0" IF Round

### Base Reactions

TIA Revision:	G	
Factored Moment, Mu:	1641	ft-kips
Factored Axial, Pu:	276	kips
Factored Shear, Vu:	6	kips

### Anchor Rod Results

TIA G --> Max Rod (Cu+ Vu/ $\eta$ ): 259.8 Kips  
 Axial Design Strength,  $\Phi * F_u * A_{net}$ : 260.0 Kips  
 Anchor Rod Stress Ratio: 99.9% **Pass**

### Base Plate Results

Base Plate Stress: 28.0 ksi  
 PL Design Bending Strength,  $\Phi * F_y$ : 45.0 ksi  
 Base Plate Stress Ratio: 62.3% **Pass**

### Flexural Check

### PL Ref. Data

Yield Line (in):	31.00
Max PL Length:	31.01

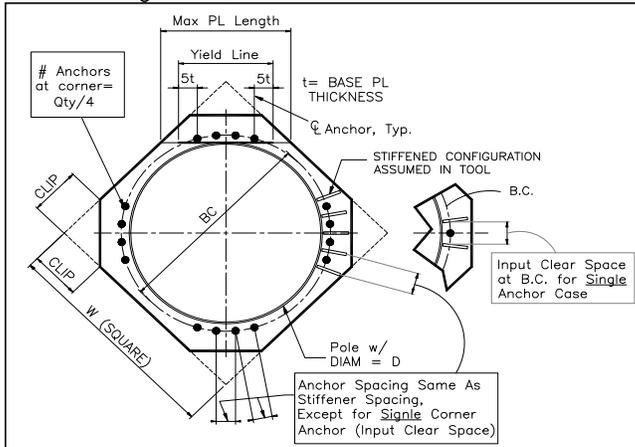
### N/A - Unstiffened

### Stiffener Results

Horizontal Weld : N/A  
 Vertical Weld: N/A  
 Plate Flex+Shear,  $f_b/F_b + (f_v/F_v)^2$ : N/A  
 Plate Tension+Shear,  $f_t/F_t + (f_v/F_v)^2$ : N/A  
 Plate Comp. (AISC Bracket): N/A

### Pole Results

Pole Punching Shear Check: N/A



\*\* Note: for complete joint penetration groove welds the groove depth must be exactly 1/2 the stiffener thickness for calculation purposes

PROJECT	<b>841289 - OLD SAYBROOK,CT</b>		
SUBJECT	<b>Foundation Analysis</b>		
DATE	<b>10/14/16</b>	PAGE	1 OF 1

## Monopole Pad & Pier Foundation Analysis

Rev. Type: **G**

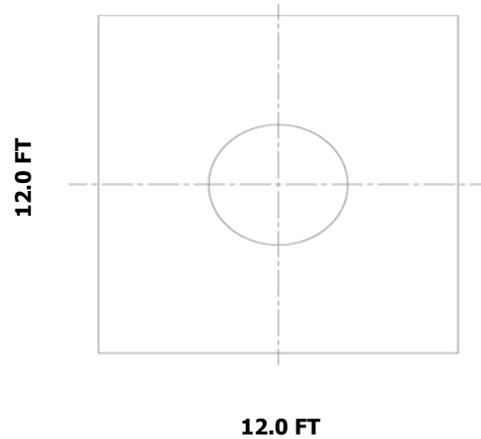
Design Loads:

Input factored loads

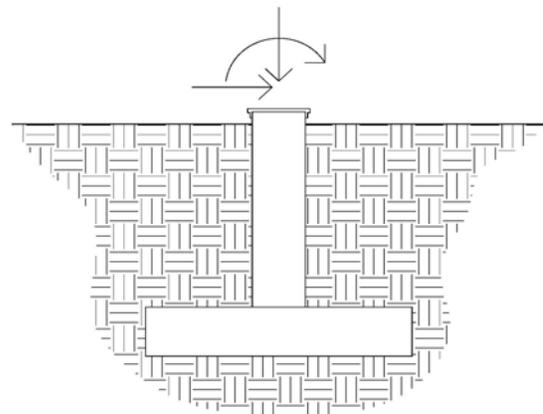
Shear:	<u>6.0</u>	kips
Moment:	<u>1,641.0</u>	ft-kips
Tower Height:	<u>150.0</u>	ft
Tower Weight:	<u>276.0</u>	kips

Pad & Pier Dimensions / Properties:

Pole Diameter at Base:	<u>38.29</u>	in
Bearing Depth:	<u>8.7</u>	ft
Pad Width:	<u>12.0</u>	ft
Neglected Depth:	<u>3.3</u>	ft
Thickness:	<u>2.5</u>	ft
Pier Diameter:	<u>8.0</u>	ft
Pier Height Above Grade:	<u>0.3</u>	ft
BP Dist. Above Pier:	<u>0.0</u>	in
Clear Cover:	<u>3.0</u>	in
Pier Rebar Size:	<u>11</u>	
Pier Rebar Quantity:	<u>44</u>	
Pier Tie Size:	<u>4</u>	
Tie Quantity:	<u>7</u>	
Rebar Yield Strength:	<u>60000</u>	psi
Concrete Strength:	<u>3000</u>	psi
Concrete Unit Weight:	<u>0.131502</u>	kcf



Elevation Overview



Soil Data:

Allowable Values

Soil Unit Weight:	<u>0.081</u>	kcf
Ult. Bearing Capacity:	<u>30.000</u>	ksf
Angle of Friction:	<u>42.000</u>	deg
Cohesion:	<u>0.000</u>	ksf
Passive Pressure:	<u>0.000</u>	ksf
Base Friction:	<u>0.400</u>	

\*\* Notes:

**Minimum steel has been assumed for Pad.**

### Summary of Results

Req'd Pier Diam.	OK
Overturning	75.0%
Shear Capacity	4.0%
Bearing	45.2%
Pad Shear - 2-way	20.1%
Pad Moment Capacity	21.1%
Pier Moment Capacity	13.4%

PROJECT	<b>841289 - OLD SAYBROOK, CT</b>
SUBJECT	<b>Guy Anchor Analysis</b>
DATE	<b>10/14/16</b>



## Deadman Guy Anchor Analysis Rev G

Design Loads:

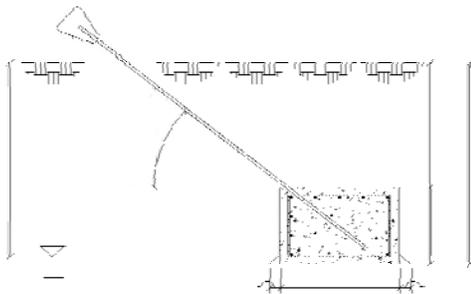
Uplift (Pv)	=	<u>167.00</u>	k
Shear (Ph)	=	<u>39.00</u>	k

Rev. G Reduction Factors:

Soil Friction	=	<u>0.75</u>
Soil Lateral	=	<u>0.75</u>
Soil Uplift	=	<u>0.75</u>
Dead Weight	=	<u>0.90</u>

Anchor Dims / Properties:

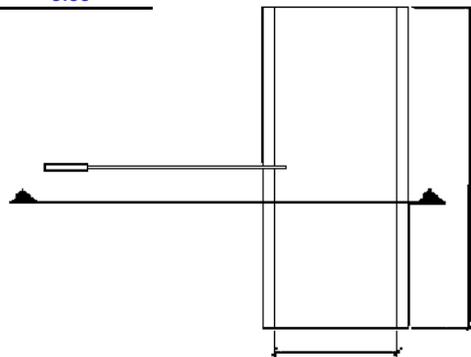
Anchor Radius	=	<u>20.50</u>	ft
Deadman Block Width ( W )	=	<u>5.00</u>	ft
Deadman Block Thickness ( H )	=	<u>2.00</u>	ft
Deadman Block Length ( L )	=	<u>37.00</u>	ft
Depth to BOC ( D )	=	<u>8.00</u>	ft
Concrete Density	=	<u>0.09</u>	kcf
Concrete Strength	=	<u>4000</u>	psi



Soil Data:

Frost Depth	=	<u>3.33</u>	ft
Ultimate Soil Friction	=	<u>0.00</u>	ksf

	Unit Wt. (pcf)	Angle (deg)	Cohesion (kcf)
Berm: 3'	<u>0.12</u>	<u>0.00</u>	<u>0.00</u>
Layer 1: 2.7'	<u>0.11</u>	<u>0.00</u>	<u>0.00</u>
Layer 2: 3.33'	<u>0.05</u>	<u>0.00</u>	<u>0.00</u>
Layer 3: 4'	<u>0.05</u>	<u>31.00</u>	<u>0.00</u>
Layer 4: 8'	<u>0.07</u>	<u>42.00</u>	<u>0.00</u>



Steel Reinforcement:

Bar Size	=	<u>9</u>	
No. of Bars in Top of Block	=	<u>13</u>	
No. of Bars in Front of Block	=	<u>4</u>	
Rebar Tensile Strength	=	<u>60000</u>	psi
Clear Cover	=	<u>3.00</u>	in
Strength Reduction Factor	=	<u>0.90</u>	

Anchor Shaft:

Shaft Diameter	=	<u>1.75</u>	in
Shaft Grade	=	<u>50</u>	ksi

Summary of Results	
Uplift	72.4%
Lateral	22.9%
Anchor Rod	88.9%
Rebar	OK

PROJECT	<b>841289 - OLD SAYBROOK, CT</b>
SUBJECT	<b>Guy Anchor Analysis</b>
DATE	<b>10/14/16</b>



## Deadman Guy Anchor Analysis Rev G

Design Loads:

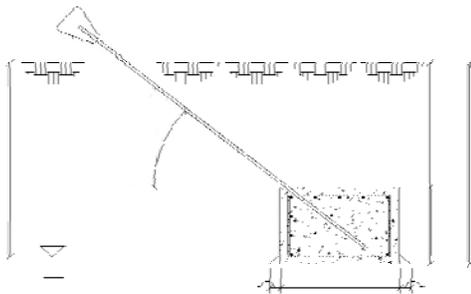
Uplift (Pv)	=	<u>92.00</u>	k
Shear (Ph)	=	<u>43.00</u>	k

Rev. G Reduction Factors:

Soil Friction	=	<u>0.75</u>
Soil Lateral	=	<u>0.75</u>
Soil Uplift	=	<u>0.75</u>
Dead Weight	=	<u>0.90</u>

Anchor Dims / Properties:

Anchor Radius	=	<u>42.00</u>	ft
Deadman Block Width ( W )	=	<u>5.00</u>	ft
Deadman Block Thickness ( H )	=	<u>2.00</u>	ft
Deadman Block Length ( L )	=	<u>30.00</u>	ft
Depth to BOC ( D )	=	<u>8.00</u>	ft
Concrete Density	=	<u>0.09</u>	kcf
Concrete Strength	=	<u>4000</u>	psi



Soil Data:

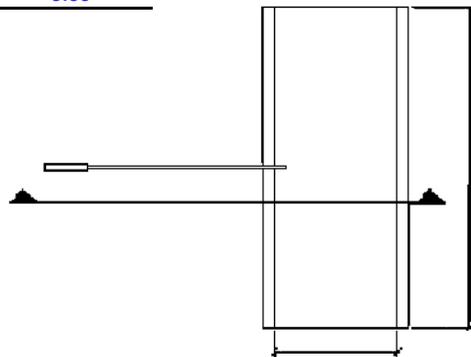
Frost Depth	=	<u>3.33</u>	ft
Ultimate Soil Friction	=	<u>0.00</u>	ksf

Unit Wt. (pcf)    Angle (deg)    Cohesion (kcf)

Layer 1: 2.7'	<u>0.11</u>	<u>0.00</u>	<u>0.00</u>
Layer 2: 3.33'	<u>0.05</u>	<u>0.00</u>	<u>0.00</u>
Layer 3: 4'	<u>0.05</u>	<u>31.00</u>	<u>0.00</u>
Layer 4: 8'	<u>0.07</u>	<u>42.00</u>	<u>0.00</u>

Steel Reinforcement:

Bar Size	=	<u>9</u>
No. of Bars in Top of Block	=	<u>13</u>
No. of Bars in Front of Block	=	<u>4</u>
Rebar Tensile Strength	=	<u>60000</u> psi
Clear Cover	=	<u>3.00</u> in
Strength Reduction Factor	=	<u>0.90</u>



Anchor Shaft:

Shaft Diameter	=	<u>1.75</u>	in
Shaft Grade	=	<u>50</u>	ksi

Summary of Results	
Uplift	68.6%
Lateral	32.7%
Anchor Rod	53.0%
Rebar	OK

RADIO FREQUENCY EMISSIONS ANALYSIS REPORT  
EVALUATION OF HUMAN EXPOSURE POTENTIAL  
TO NON-IONIZING EMISSIONS

T-Mobile Existing Facility

Site ID: CT11035E

Old Saybrook  
170 Ingham Hill Road  
Old Saybrook, CT 06475

**November 22, 2016**

**EBI Project Number: 6216005486**

Site Compliance Summary	
Compliance Status:	<b>COMPLIANT</b>
Site total MPE% of FCC general public allowable limit:	<b>6.02 %</b>

November 22, 2016

T-Mobile USA  
Attn: Jason Overbey, RF Manager  
35 Griffin Road South  
Bloomfield, CT 06002

Emissions Analysis for Site: **CT11035E – Old Saybrook**

EBI Consulting was directed to analyze the proposed T-Mobile facility located at **170 Ingham Hill Road, Old Saybrook, CT**, for the purpose of determining whether the emissions from the Proposed T-Mobile Antenna Installation located on this property are within specified federal limits.

All information used in this report was analyzed as a percentage of current Maximum Permissible Exposure (% MPE) as listed in the FCC OET Bulletin 65 Edition 97-01 and ANSI/IEEE Std C95.1. The FCC regulates Maximum Permissible Exposure in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The number of  $\mu\text{W}/\text{cm}^2$  calculated at each sample point is called the power density. The exposure limit for power density varies depending upon the frequencies being utilized. Wireless Carriers and Paging Services use different frequency bands each with different exposure limits, therefore it is necessary to report results and limits in terms of percent MPE rather than power density.

All results were compared to the FCC (Federal Communications Commission) radio frequency exposure rules, 47 CFR 1.1307(b)(1) – (b)(3), to determine compliance with the Maximum Permissible Exposure (MPE) limits for General Population/Uncontrolled environments as defined below.

General population/uncontrolled exposure limits apply to situations in which the general public may be exposed or in which persons who are exposed as a consequence of their employment may not be made fully aware of the potential for exposure or cannot exercise control over their exposure. Therefore, members of the general public would always be considered under this category when exposure is not employment related, for example, in the case of a telecommunications tower that exposes persons in a nearby residential area.

Public exposure to radio frequencies is regulated and enforced in units of microwatts per square centimeter ( $\mu\text{W}/\text{cm}^2$ ). The general population exposure limit for the 700 MHz Band is approximately 467  $\mu\text{W}/\text{cm}^2$ , and the general population exposure limit for the 1900 MHz (PCS) and 2100 MHz (AWS) bands is 1000  $\mu\text{W}/\text{cm}^2$ . Because each carrier will be using different frequency bands, and each frequency band has different exposure limits, it is necessary to report percent of MPE rather than power density.

Occupational/controlled exposure limits apply to situations in which persons are exposed as a consequence of their employment and in which those persons who are exposed have been made fully aware of the potential for exposure and can exercise control over their exposure. Occupational/controlled exposure limits also apply where exposure is of a transient nature as a result of incidental passage through a location where exposure levels may be above general population/uncontrolled limits (see below), as long as the exposed person has been made fully aware of the potential for exposure and can exercise control over his or her exposure by leaving the area or by some other appropriate means.

Additional details can be found in FCC OET 65.

## **CALCULATIONS**

Calculations were done for the proposed T-Mobile Wireless antenna facility located at **170 Ingham Hill Road, Old Saybrook, CT**, using the equipment information listed below. All calculations were performed per the specifications under FCC OET 65. Since T-Mobile is proposing highly focused directional panel antennas, which project most of the emitted energy out toward the horizon, all calculations were performed assuming a lobe representing the maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was focused at the base of the tower. For this report the sample point is the top of a 6-foot person standing at the base of the tower.

For all calculations, all equipment was calculated using the following assumptions:

- 1) 2 GSM channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 2) 2 UMTS channels (PCS Band - 1900 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 3) 2 UMTS channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 30 Watts per Channel.
- 4) 2 LTE channels (AWS Band – 2100 MHz) were considered for each sector of the proposed installation. These Channels have a transmit power of 60 Watts per Channel
- 5) 1 LTE channel (700 MHz Band) was considered for each sector of the proposed installation. This channel has a transmit power of 30 Watts.

- 6) Since the 2100 MHz UMTS radios are ground mounted there are additional cabling losses accounted for. For each ground mounted 2100 MHz UMTS RF path an additional 2.18 dB of loss was factored into the calculations for this cable loss. This is based on manufacturers Specifications for 169 feet of 1-1/4" coax cable on each path.
- 7) All radios at the proposed installation were considered to be running at full power and were uncombined in their RF transmissions paths per carrier prescribed configuration. Per FCC OET Bulletin No. 65 - Edition 97-01 recommendations to achieve the maximum anticipated value at each sample point, all power levels emitting from the proposed antenna installation are increased by a factor of 2.56 to account for possible in-phase reflections from the surrounding environment. This is rarely the case, and if so, is never continuous.
- 8) For the following calculations the sample point was the top of a 6-foot person standing at the base of the tower. The maximum gain of the antenna per the antenna manufactures supplied specifications minus 10 dB was used in this direction. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 9) The antennas used in this modeling are the **Ericsson AIR21 B4A/B2P & Ericsson AIR21 B2A/B4P** for 1900 MHz (PCS) and 2100 MHz (AWS) channels and the **Commscope LNX-6515DS-VTM** for 700 MHz channels. This is based on feedback from the carrier with regards to anticipated antenna selection. The **Ericsson AIR21 B4A/B2P** has a maximum gain of **15.9 dBd** at its main lobe at 1900 MHz and 2100 MHz. The **Ericsson AIR21 B2A/B4P** has a maximum gain of **15.9 dBd** at its main lobe at 1900 MHz and 2100 MHz. The **Commscope LNX-6515DS-VTM** has a maximum gain of **14.6 dBd** at its main lobe at 700 MHz. The maximum gain of the antenna per the antenna manufactures supplied specifications, minus 10 dB, was used for all calculations. This value is a very conservative estimate as gain reductions for these particular antennas are typically much higher in this direction.
- 10) The antenna mounting height centerline of the proposed antennas is **169 feet** above ground level (AGL).
- 11) Emissions values for additional carriers were taken from the Connecticut Siting Council active database. Values in this database are provided by the individual carriers themselves.
- 12) All calculations were done with respect to uncontrolled / general public threshold limits.

**T-Mobile Site Inventory and Power Data**

Sector:	A	Sector:	B	Sector:	C
Antenna #:	1	Antenna #:	1	Antenna #:	1
Make / Model:	Ericsson AIR21 B4A/B2P	Make / Model:	Ericsson AIR21 B4A/B2P	Make / Model:	Ericsson AIR21 B4A/B2P
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	169	Height (AGL):	169	Height (AGL):	169
Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)
Channel Count	2	Channel Count	2	Channel Count	2
Total TX Power(W):	120	Total TX Power(W):	120	Total TX Power(W):	120
ERP (W):	4,668.54	ERP (W):	4,668.54	ERP (W):	4,668.54
Antenna A1 MPE%	0.63	Antenna B1 MPE%	0.63	Antenna C1 MPE%	0.63
Antenna #:	2	Antenna #:	2	Antenna #:	2
Make / Model:	Ericsson AIR21 B2A/B4P	Make / Model:	Ericsson AIR21 B2A/B4P	Make / Model:	Ericsson AIR21 B2A/B4P
Gain:	15.9 dBd	Gain:	15.9 dBd	Gain:	15.9 dBd
Height (AGL):	169	Height (AGL):	169	Height (AGL):	169
Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)	Frequency Bands	1900 MHz (PCS) / 2100 MHz (AWS)
Channel Count	6	Channel Count	6	Channel Count	6
Total TX Power(W):	180	Total TX Power(W):	180	Total TX Power(W):	180
ERP (W):	6,081.57	ERP (W):	6,081.57	ERP (W):	6,081.57
Antenna A2 MPE%	0.82	Antenna B2 MPE%	0.82	Antenna C2 MPE%	0.82
Antenna #:	3	Antenna #:	3	Antenna #:	3
Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM	Make / Model:	Commscope LNX-6515DS-VTM
Gain:	14.6 dBd	Gain:	14.6 dBd	Gain:	14.6 dBd
Height (AGL):	169	Height (AGL):	169	Height (AGL):	169
Frequency Bands	700 MHz	Frequency Bands	700 MHz	Frequency Bands	700 MHz
Channel Count	1	Channel Count	1	Channel Count	1
Total TX Power(W):	30	Total TX Power(W):	30	Total TX Power(W):	30
ERP (W):	865.21	ERP (W):	865.21	ERP (W):	865.21
Antenna A3 MPE%	0.25	Antenna B3 MPE%	0.25	Antenna C3 MPE%	0.25

Site Composite MPE%	
Carrier	MPE%
T-Mobile (Per Sector Max)	1.71 %
AT&T	1.82 %
Verizon	2.24 %
Paging	0.25 %
<b>Site Total MPE %:</b>	<b>6.02 %</b>

T-Mobile Sector A Total:	1.71 %
T-Mobile Sector B Total:	1.71 %
T-Mobile Sector C Total:	1.71 %
<b>Site Total:</b>	<b>6.02 %</b>

T-Mobile_per sector	# Channels	Watts ERP (Per Channel)	Height (feet)	Total Power Density ( $\mu\text{W}/\text{cm}^2$ )	Frequency (MHz)	Allowable MPE ( $\mu\text{W}/\text{cm}^2$ )	Calculated % MPE
T-Mobile AWS - 2100 MHz LTE	2	2,334.27	169	6.32	AWS - 2100 MHz	1000	0.63%
T-Mobile AWS - 2100 MHz UMTS	2	706.51	169	1.91	AWS - 2100 MHz	1000	0.19%
T-Mobile PCS - 1950 MHz UMTS	2	1,167.14	169	3.16	PCS - 1950 MHz	1000	0.32%
T-Mobile PCS - 1950 MHz GSM	2	1,167.14	169	3.16	PCS - 1950 MHz	1000	0.32%
T-Mobile 700 MHz LTE	1	865.21	169	1.17	700 MHz	467	0.25%
						<b>Total:</b>	<b>1.71%</b>

## Summary

All calculations performed for this analysis yielded results that were **within** the allowable limits for general public exposure to RF Emissions.

The anticipated maximum composite contributions from the T-Mobile facility as well as the site composite emissions value with regards to compliance with FCC's allowable limits for general public exposure to RF Emissions are shown here:

T-Mobile Sector	Power Density Value (%)
Sector A:	1.71 %
Sector B:	1.71 %
Sector C:	1.71 %
T-Mobile Per Sector Maximum:	1.71 %
Site Total:	6.02 %
Site Compliance Status:	<b>COMPLIANT</b>

The anticipated composite MPE value for this site assuming all carriers present is **6.02%** of the allowable FCC established general public limit sampled at the ground level. This is based upon values listed in the Connecticut Siting Council database for existing carrier emissions.

FCC guidelines state that if a site is found to be out of compliance (over allowable thresholds), that carriers over a 5% contribution to the composite value will require measures to bring the site into compliance. For this facility, the composite values calculated were well within the allowable 100% threshold standard per the federal government.