



QC Development

PO Box 916

Storrs, CT 06268

860-670-9068

Mark.Roberts@QCDevelopment.net

September 27, 2019

Melanie A. Bachman
Executive Director
Connecticut Siting Council
10 Franklin Square
New Britain, CT 06051

Notice of Exempt Modification – New Cingular Wireless PCS, LLC (AT&T) – CT2490
886 Main Street, East Hartford, CT 06108
N 41.76944444
W 72.64277778

Dear Ms. Bachman:

AT&T currently maintains nine (9) antennas at the rooftop level (112' and 120' AGL) of the 11-story apartment building at 886 Main Street, East Hartford, CT. The property is owned by Hartford East Associates. AT&T now intends to add three (3) CCI HPA-65R-BU66A antennas and (3) Ericsson B25 4415 Remote Radio Units (RRU).

This facility was approved by the Connecticut Siting Council in Petition # 324 on August 9, 1994 and AT&T's shared use of the facility was approved on September 19, 2014 (IS-CING-043-140822). These approvals included no conditions that could feasibly be violated by this proposed modification, including total facility height and mounting restrictions. This modification therefore complies with the aforementioned approvals.

Please accept this letter as notification pursuant to Regulations of Connecticut State Agencies § 16-50j-73, for construction that constitutes an exempt modification pursuant to R.C.S.A. § 16-50j-72(b)(2). In accordance with R.C.S.A. § 16-50j-73, a copy of this letter is being sent to Ms. Marcia LeClerc, Mayor of the Town of East Hartford, and the East Hartford Development & Planning Department as well as the property owner.

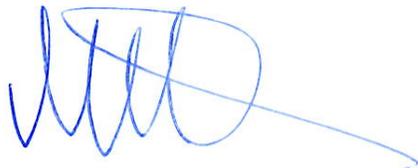
The planned modifications to the facility fall squarely within those activities explicitly provided for in R.C.S.A. § 16-50j-72(b)(2).

1. The proposed modifications will not result in an increase in the height of the existing structure.
2. The proposed modifications will not require the extension of the site boundary.
3. The proposed modifications will not increase noise levels at the facility by six decibels or more, or to levels that exceed state and local criteria.
4. The operation of the replacement antennas will not increase radio frequency emissions at the facility to a level at or above the Federal Communications Commission safety standard.
5. The proposed modifications will not cause a change or alteration in the physical or environmental characteristics of the site.
6. The existing structure and its foundation can support the proposed loading.

For the foregoing reasons, AT&T respectfully submits that the proposed modifications to the above-referenced telecommunications facility constitute an exempt modification under R.C.S.A. § 16-50j-72(b)(2).

Please feel free to call me at (860) 670-9068 with any questions regarding this matter. Thank you for your consideration.

Sincerely,



Mark Roberts
QC Development
Consultant for AT&T

Attachments

cc: Mayor Marcia LeClerc - Elected Official
Jeffrey Cormier – Town Planner
Hartford East Associates - Property Owner

Power Density

Existing Loading on Tower

Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm ²)	Freq. Band (MHz ^{**})	Limit S (mW/cm ²)	%MPE
Other Carriers*							5.85%
AT&T LTE	1	1476	107	0.0520	700	0.4667	1.12%
AT&T LTE	1	1000	107	0.0353	850	0.5667	0.62%
AT&T 5G	1	1000	107	0.0353	850	0.5667	0.62%
AT&T LTE	2	3664	107	0.2583	1900	1.0000	2.58%
AT&T LTE	1	3837	107	0.1353	2100	1.0000	1.35%
AT&T LTE	1	1285	107	0.0453	2300	1.0000	0.45%
Site Total							12.60%

*Per CSC Records (available upon request, includes calculation formulas)

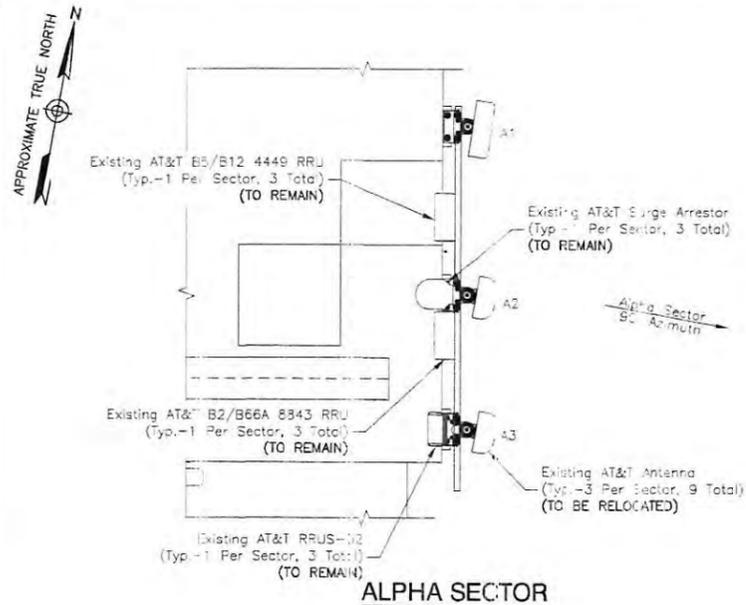
** If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880

Proposed Loading on Tower

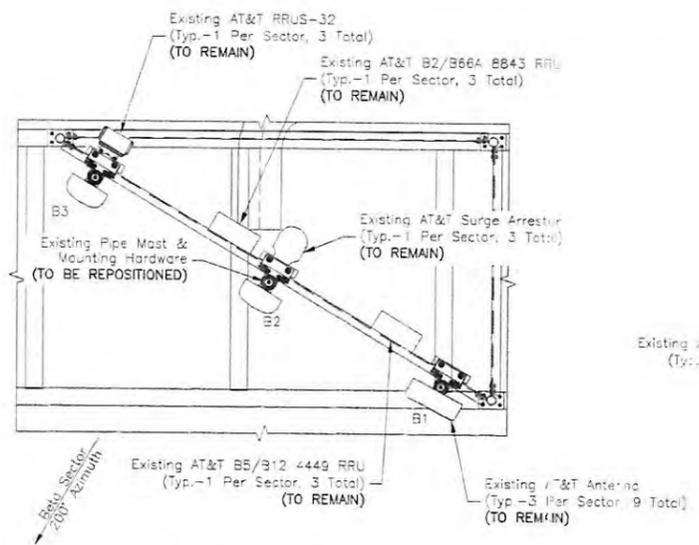
Carrier	# of Channels	ERP/Ch (W)	Antenna Centerline Height (ft)	Power Density (mW/cm ²)	Freq. Band (MHz ^{**})	Limit S (mW/cm ²)	%MPE
Other Carriers*							5.85%
AT&T LTE	1	1476	112	0.0472	700	0.4667	1.01%
AT&T LTE	1	1000	112	0.0320	850	0.5667	0.56%
AT&T 5G	1	1000	112	0.0320	850	0.5667	0.56%
AT&T LTE	2	3664	112	0.2345	1900	1.0000	2.35%
AT&T LTE	1	4842	112	0.1550	1900	1.0000	1.55%
AT&T LTE	1	3837	112	0.1228	2100	1.0000	1.23%
AT&T LTE	1	1285	112	0.0411	2300	1.0000	0.41%
Site Total							13.53%

*Per CSC Records (available upon request, includes calculation formulas)

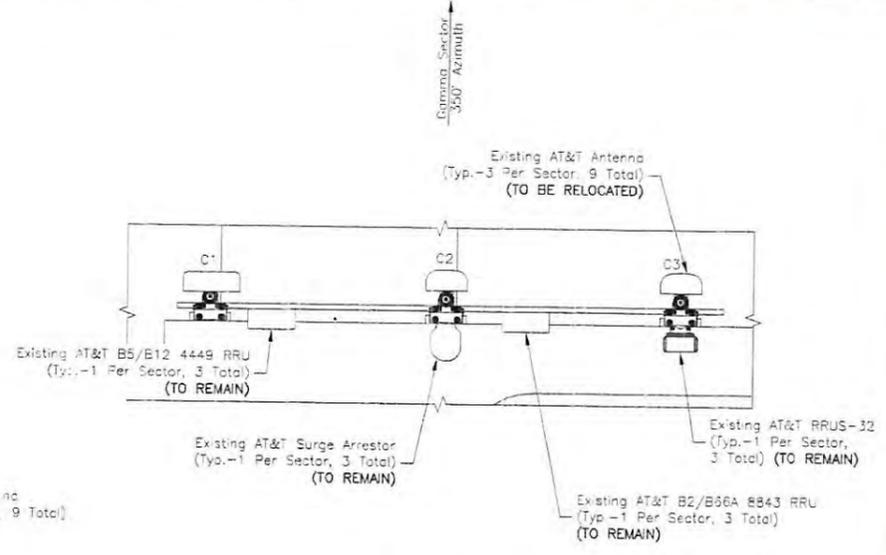
** If a range of frequencies are used, such as 880-894, enter the lowest value, i.e. 880



ALPHA SECTOR



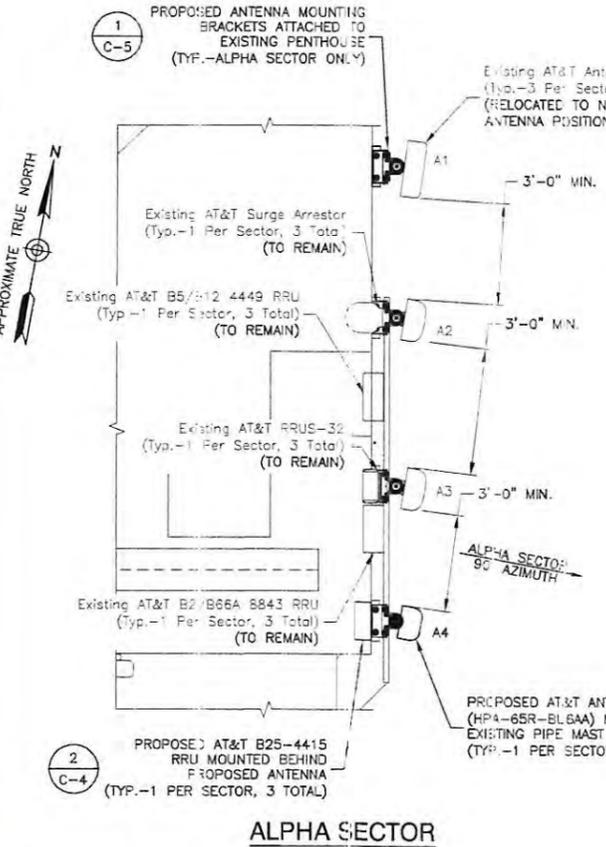
BETA SECTOR



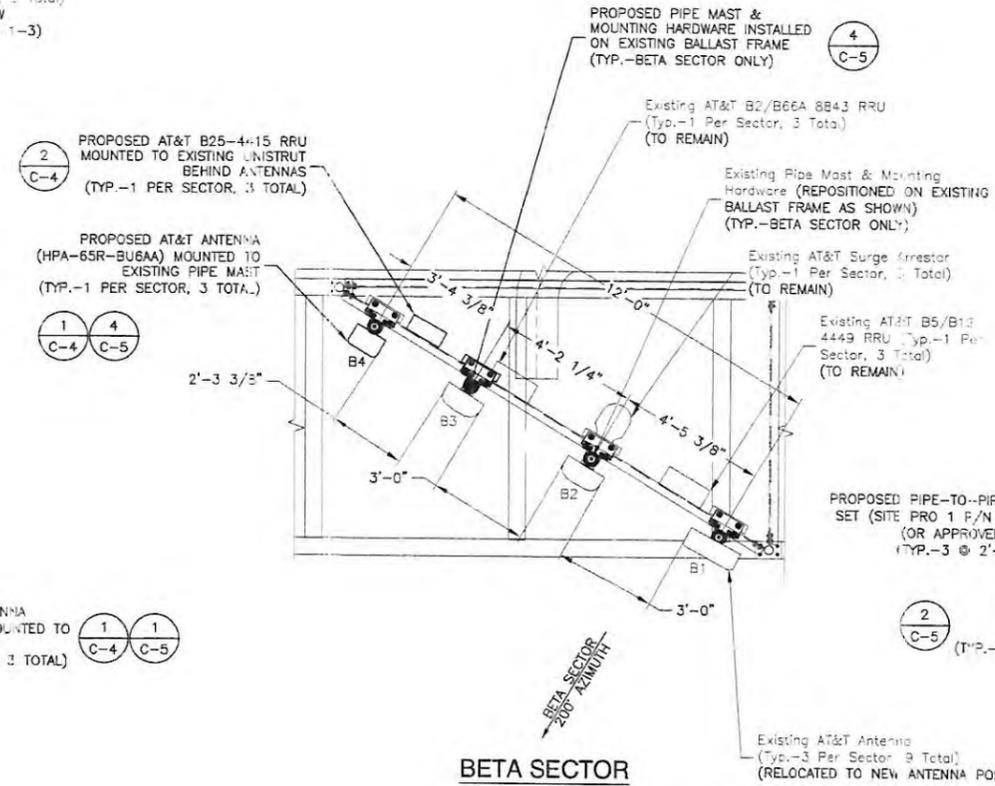
GAMMA SECTOR

EXISTING ANTENNA PLAN

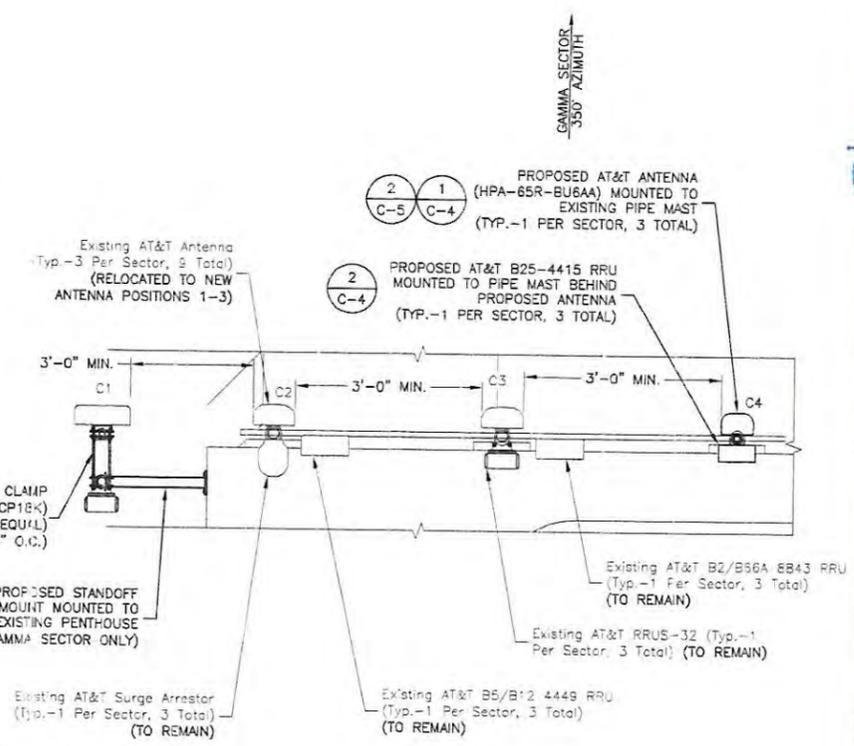
SCALE: 3/16"=1' FOR 11"x17"
3/8"=1' FOR 22"x34"



ALPHA SECTOR



BETA SECTOR



GAMMA SECTOR

PROPOSED ANTENNA PLAN

SCALE: 3/16"=1' FOR 11"x17"
3/8"=1' FOR 22"x34"



- NOTES:**
1. MAINTAIN A MINIMUM 3'-0" SEPARATION BETWEEN ALL EXISTING & PROPOSED ANTENNAS.
 2. ALL PROPOSED EQUIPMENT, INCLUDING ANTENNAS, COAX, SURGE ARRESTORS, TMA'S, RRU'S, ETC., SHALL BE MOUNTED IN ACCORDANCE WITH THE TOWER STRUCTURAL ANALYSIS & MODIFICATION DRAWINGS BY DEWBERRY ENGINEERS INC. DATED 09/16/19.
 3. ALL EXISTING ALPHA & GAMMA SECTOR ANTENNAS TO BE SHIFTED OVER 1 POSITION TO THE NEW ANTENNA POSITIONS 1-3 AS SHOWN TO ALLOW FOR PROPOSED ANTENNA TO BE INSTALLED AT POSITION 4.
 4. EXISTING BETA SECTOR ANTENNAS AT POSITIONS 2 & 3 TO BE RELOCATED AS SHOWN TO ACCOMMODATE AT&T SPACING REQUIREMENTS. PROPOSED BETA SECTOR ANTENNA TO BE INSTALLED AT POSITION 4 AS SHOWN.



500 ENTERPRISE DRIVE SUITE 3A
ROCKY HILL, CT 06067



12 INDUSTRIAL WAY
SALEM, NH 03079

**CT2490
EAST HARTFORD
MAIN STREET**

CONSTRUCTION DRAWINGS

0	09/23/19	ISSUED AS FINAL
B	09/17/19	REVISED PER COMMENTS
A	08/13/19	ISSUED FOR REVIEW



Dewberry Engineers Inc.
600 PARSIPPANY ROAD
SUITE 301
PARSIPPANY, NJ 07054
PHONE: 973.739.9400
FAX: 973.739.9716

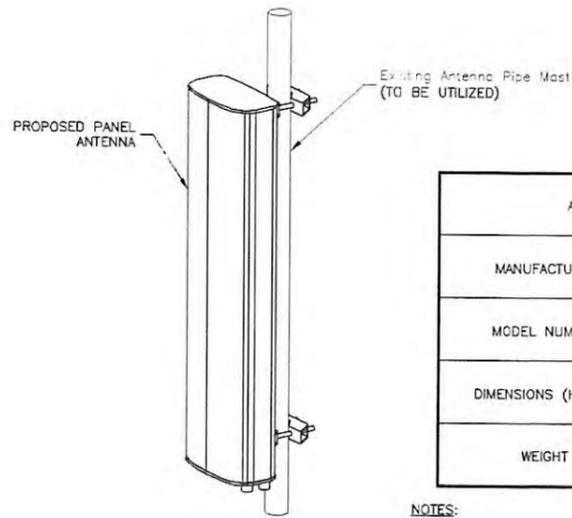


DRAWN BY:	BJR
REVIEWED BY:	BSH
CHECKED BY:	GHN
PROJECT NUMBER:	50055106
JOB NUMBER:	50093847
SITE ADDRESS:	

886 MAIN STREET
EAST HARTFORD, CT
06108
HARTFORD COUNTY

EXISTING & PROPOSED
ANTENNA LAYOUTS

C-3



ANTENNA SPECIFICATIONS	
MANUFACTURER	CCI
MODEL NUMBER	HPA-65R-BU6AA
DIMENSIONS (HxWxD)	71.0" x 11.7" x 7.6"
WEIGHT	51.0 LBS

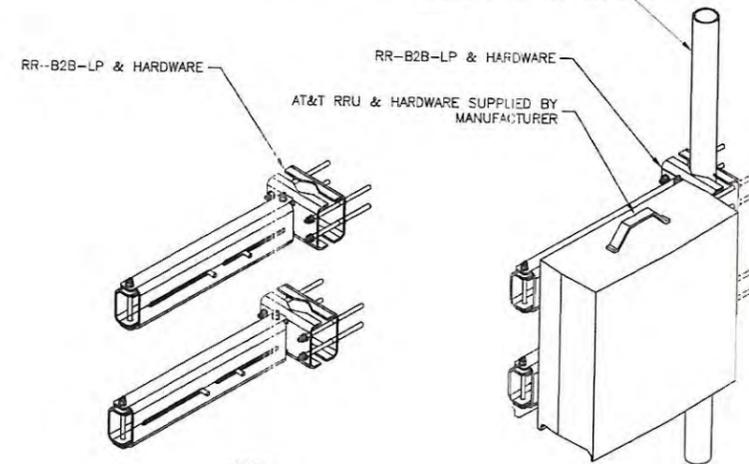
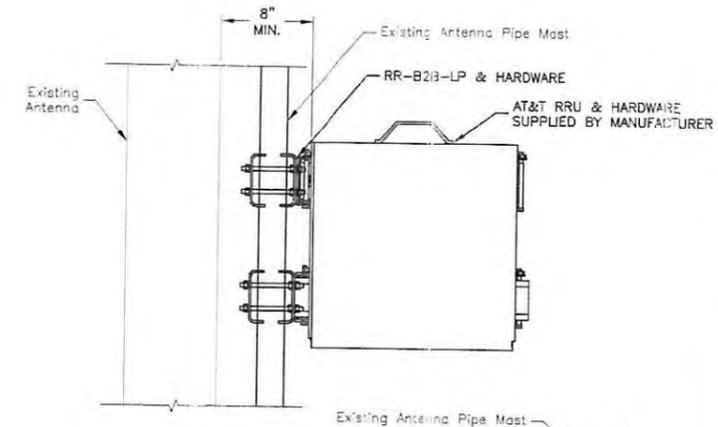
- NOTES:
1. MOUNT ANTENNA PER MANUFACTURER'S RECOMMENDATIONS.
 2. WEIGHT INCLUDES MOUNTING BRACKETS.

ANTENNA DETAIL
SCALE: N.T.S. ①



- ERICSSON RRU B25 4415
- RRU NOTES:
1. MOUNT EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.
 2. GROUND EQUIPMENT AND MOUNTS PER MANUFACTURER'S RECOMMENDATIONS AND AT&T STANDARDS.
 3. CONFIRM REQUIRED EQUIPMENT WITH THE LATEST RFDS.

REMOTE RADIO UNIT DETAIL
SCALE: N.T.S. ②



- NOTES:
1. 8" MIN. BETWEEN BACK OF ANTENNA & RRU UNIT.
 2. CONTRACTOR TO COMPLY WITH MANUFACTURER'S INSTRUCTIONS TO ENSURE THAT ALL RRU UNITS RECEIVE ELECTRICAL POWER WITHIN 2-HOURS OF BEING REMOVED FROM THE MANUFACTURER'S PACKAGING. DO NOT OPEN RRU UNITS IN THE RAIN.

RRU DUAL BRACKET MOUNT DETAIL
SCALE: N.T.S. ③

ANTENNA SCHEDULE									
SECTOR	EXISTING/PROPOSED	BAND	ANTENNA	ANTENNA TIP HEIGHT	AZIMUTH	TMA/C PLEXER	RRU	FEEDER	RAYCAP
A1	EXISTING	LTE 700 BC/850/AWS	KATHREIN 800-10965	120'-0"	90°	-	(E) ERICSSON RRU B5/B12 4449	FIBER	(E) (1) RAYCAP DC6-48-60-18-8C
A2	EXISTING	LTE PCS	CCI OPA-65R-LCUU-H6	120'-0"	90°	-	(E) ERICSSON RRU B2/B:6A 8843	FIBER	
A3	EXISTING	LTE WCS	CCI OPA-65R-LCUU-H6	120'-0"	90°	-	(E) ERICSSON RRU 32	FIBER	
A4	PROPOSED	LTE PCS E & C5	CCI HPA-65R-BU66A	120'-0"	90°	-	(P) ERICSSON RRU B25 4415	FIBER	
B1	EXISTING	LTE 700 BC/850/AWS	KATHREIN 800-10965	112'-0"	200°	-	(E) ERICSSON RRU B5/B12 4449	FIBER	(E) (1) RAYCAP DC6-48-60-18-8C
B2	EXISTING	LTE PCS	CCI OPA-65R-LCUU-H6	112'-0"	200°	-	(E) ERICSSON RRU B2/B:6A 8843	FIBER	
B3	EXISTING	LTE WCS	CCI OPA-65R-LCUU-H6	112'-0"	200°	-	(E) ERICSSON RRU 32	FIBER	
B4	PROPOSED	LTE PCS E & C5	CCI HPA-65R-BU66A	112'-0"	200°	-	(P) ERICSSON RRU B25 4415	FIBER	
C1	EXISTING	LTE 700 BC/850/AWS	KATHREIN 800-10965	120'-0"	350°	-	(E) ERICSSON RRU B5/B12 4449	FIBER	(E) (1) RAYCAP DC6-48-60-18-8C
C2	EXISTING	LTE PCS	CCI OPA-65R-LCUU-H6	120'-0"	350°	-	(E) ERICSSON RRU B2/B:6A 8843	FIBER	
C3	EXISTING	LTE WCS	CCI OPA-65R-LCUU-H6	120'-0"	350°	-	(E) ERICSSON RRU 32	FIBER	
C4	PROPOSED	LTE PCS E & C5	CCI HPA-65R-BU66A	120'-0"	350°	-	(P) ERICSSON RRU B25 4415	FIBER	



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SUITE 301
PARSIPPANY NJ 07054
PHONE: 973.739.9400
FAX: 973.739.9710



DRAWN BY: BJR

REVIEWED BY: BSH

CHECKED BY: GHN

PROJECT NUMBER: 50055106

JOB NUMBER: 50093847

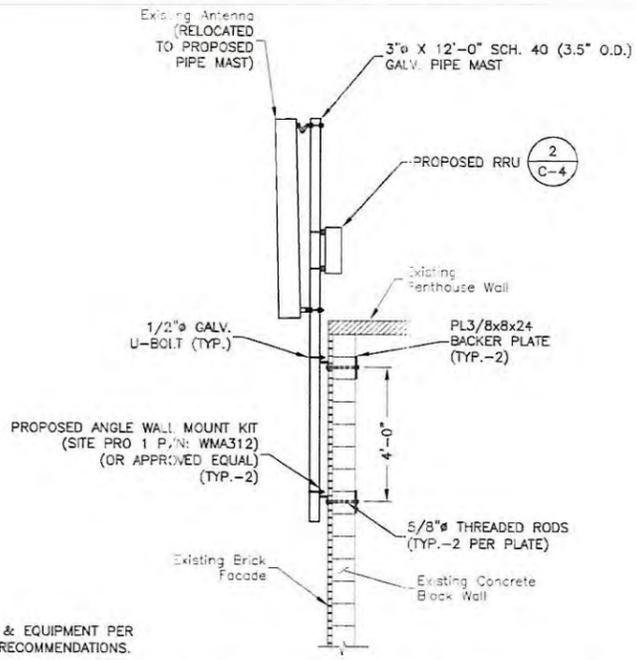
SITE ADDRESS:

886 MAIN STREET
EAST HARTFORD, CT
06108
HARTFORD COUNTY

SHEET TITLE

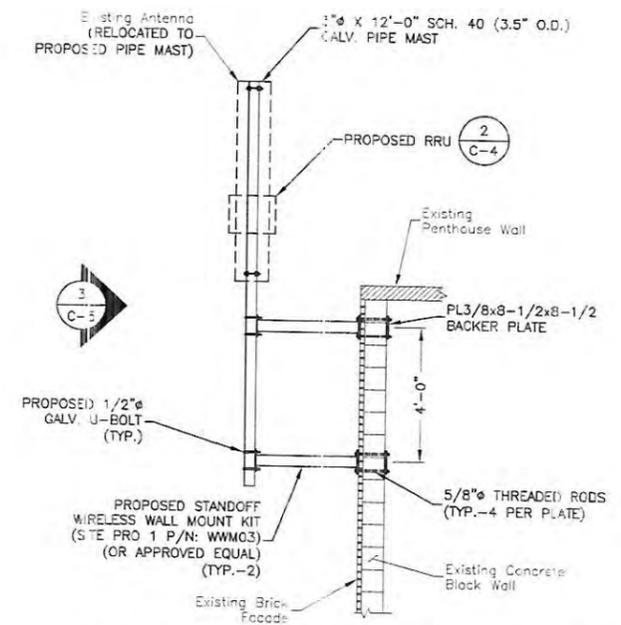
CONSTRUCTION
DETAILS I

SHEET NUMBER



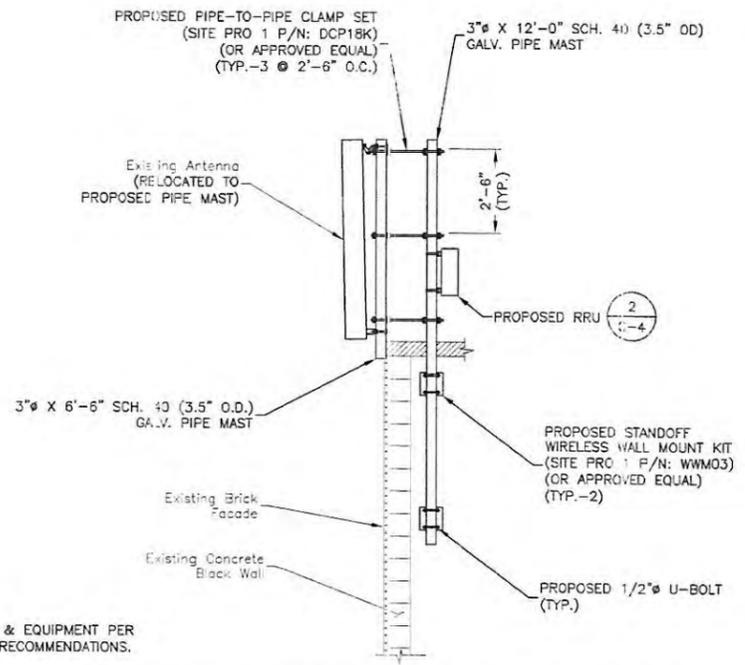
ALPHA SECTOR MOUNTING DETAIL 1
 SCALE: 3/16"=1' FOR 11"x17"
 3/8"=1' FOR 22"x34"
 0' 2' 4' 6'

NOTE:
 1. MOUNT ANTENNAS & EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.



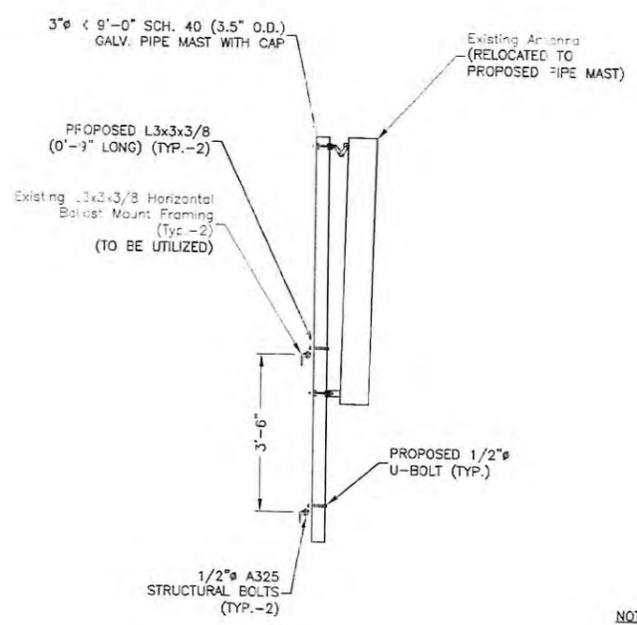
GAMMA SECTOR MOUNTING DETAIL 2
 SCALE: 3/16"=1' FOR 11"x17"
 3/8"=1' FOR 22"x34"
 0' 2' 4' 6'

NOTE:
 1. MOUNT ANTENNAS & EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.



GAMMA SECTOR MOUNTING DETAIL II 3
 SCALE: 3/16"=1' FOR 11"x17"
 3/8"=1' FOR 22"x34"
 0' 2' 4' 6'

NOTE:
 1. MOUNT ANTENNAS & EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.



BETA SECTOR MOUNTING DETAIL 4
 SCALE: 1/4"=1' FOR 11"x17"
 1/2"=1' FOR 22"x34"
 0' 1' 2' 4'

NOTE:
 1. MOUNT ANTENNAS & EQUIPMENT PER MANUFACTURER'S RECOMMENDATIONS.



500 ENTERPRISE DRIVE SUITE 3A
 ROCKY HILL, CT 06067



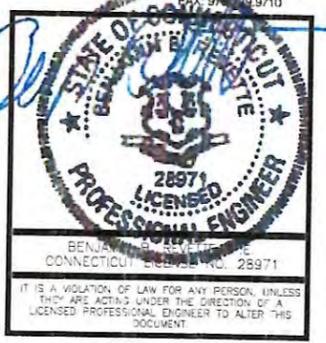
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CONSTRUCTION DRAWINGS	
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DRAWN BY:	BJR
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SITE ADDRESS:	

886 MAIN STREET
 EAST HARTFORD, CT
 06108
 HARTFORD COUNTY

SHEET TITLE	CONSTRUCTION DETAILS II
SHEET NUMBER	

C-5

Structural Analysis Report and Design Calculations For a Wireless Telecommunications facility

Site ID #: CT2490
Site Address: 886 Main Street
Hartford, CT 06108

Prepared for:
SAI Communications, Inc.
12 Industrial Way
Salem, NH 03079

Rev. 1

September 16, 2019

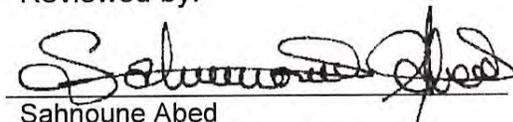
Prepared by:
Dewberry Engineers Inc.
600 Parsippany Road
Parsippany, NJ 07054
Dewberry Project Number: 50093847

Analysis Condition	Utilization	Pass/Fail
Existing Mount (Alpha)	24.4% (Strength)	Pass
Existing Mount (Beta)	N/A	Pass
Existing Mount (Gamma)	24.4% (Strength)	Pass
Proposed Mount (Gamma)	37.8% (Strength)	Pass

Prepared by:


Cory Senney
Graduate Engineer

Reviewed by:


Sahnoune Abed
Structural Project Engineer

Reviewed by:



Benjamin B. Revette, P.E.
Connecticut Professional Engineer
License No.: 28971

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1.0 INTRODUCTION AND PROJECT SUMMARY

The objective of this report is to assess the structural integrity of the installation of new antennas and associated equipment on existing cantilevered mast pipe mounts in the Alpha and Gamma Sectors, and on a proposed mast pipe mount attached to an existing ballast platform in the Beta Sector. Additionally, the structural integrity of a proposed stand-off mount supporting a relocated antenna will be assessed in this report.

The existing structure is 100 ft tall building located in East Hartford, CT. There are currently existing antennas and support equipment mounted to cantilevered pipe mounts in the Alpha and Gamma Sectors, and to a ballast steel frame in the Beta Sector. The proposed Alpha and Gamma equipment will be attached at an approximate antenna centerline of 117 ft A.G.L. and the proposed Beta equipment will be attached at an approximate antenna centerline of 109 ft A.G.L. The telecommunication upgrade is proposed by AT&T and managed by SAI Communications, Inc.

The installation of all antennas, equipment, cables and accessories are to be performed in accordance with construction drawings prepared by Dewberry Engineers Inc.

2.0 EXISTING AND PROPOSED ANTENNAS & EQUIPMENT

Currently, each sector contains the following equipment:

- Two (2) CCI OPA-65R-LCUU-H6 panel antennas measuring 72"H x 14.8"W x 7.4"D weighing 73 lbs each **to remain**
- One (1) Kathrein 800-10965 panel antenna measuring 78.7"H x 20.0"W x 6.9"D weighing 108.6 lbs **to remain**
- One (1) RRUS B5/B12 4449 measuring 17.9"H x 13.2"W x 9.4"D weighing 71 lbs **to remain**
- One (1) RRUS B2/B66A 8843 measuring 14.9"H x 13.2"W x 10.9"D weighing 72 lbs **to be remain**
- One (1) RRUS-32 measuring 26.7"H x 12.1" W x 6.7"D weighing 60 lbs each **to remain**
- One (1) Raycap DC6-48-60-18-8C measuring 26.0"Hx 9.0"D weighing 31.8 lbs **to remain**

The following equipment is proposed at each sector:

- One (1) CCI HPA-65R-BU6AA measuring 71"H x 11.7"W x 7.6"D weighing 51 lbs
- One (1) RRUS B25 4415 measuring 16.5"H x 13.4"W x 5.9"D weighing 46 lbs

Table 1: Appurtenance Loading at Rooftop		
Elev.	Status	Appurtenance Description
109'	Final	(2) CCI OPA-65R-LCUU-H6
109'	Final	(1) Kathrein 800-10965
109'	Final	(1) CCI HPA-65R-BU6AA
109'	Final	(1) RRUS B25 4415
109'	Final	(1) RRUS-32
109'	Final	(1) Raycap DC6-48-60-18-8C
109'	Final	(1) RRUS B5/B12 4449
109'	Final	(1) RRUS B2/B66A 8843
117'	Final	(4) CCI OPA-65R-LCUU-H6
117'	Final	(2) Kathrein 800-10965
117'	Final	(2) CCI HPA-65R-BU6AA
117'	Final	(2) RRUS B25 4415
117'	Final	(2) RRUS-32
117'	Final	(2) Raycap DC6-48-60-18-8C
117'	Final	(2) RRUS B5/B12 4449
117'	Final	(2) RRUS B2/B66A 8843

3.0 CODES, STANDARDS, AND REFERENCES

The structure was analyzed and the proposed installation designed per the provisions of the following Codes and standards:

- *International Building Code (IBC) 2015, International Council*
- *2018 Connecticut State Building Code – Amendments to IBC 2015*
- *TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas*
- *Steel Construction Manual 14th Edition, American Institute of Steel Construction*
- *ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers*
- *TMS 402-11/ACI530-11/ASCE 5-11 Building Code Requirements for Masonry Structures*
- *Construction Drawings by Hudson Design Group , dated November 8th, 2016*
- *Structural Analysis by Hudson Design Group, dated February 14, 2014*
- *Radio Frequency Data Sheet (RFDS) by AT&T, dated September 19th, 2018*

4.0 LOADING AND PERFORMANCE CRITERIA

The following Code-specified strength limit state load combinations were considered in the analysis of the antenna mounts (*TIA-222-H*):

1. $1.2D + 1.0W$
2. $1.2D + 1.0D_i + 1.0W_i$
3. $1.4D$

The following Code-specified serviceability load combination was considered in the deflection of the antenna mounts (*TIA-222-H*):

4. $1.0D + 1.0W_{\text{service}}$

The following load combination was considered for the stability of the Beta Sector Ballast Mount (*ASCE 7-10*):

1. $1.0D + 0.6W$

Where:

- D = Dead Load
- D_i = Ice Dead Load
- W = Wind Load
- W_i = Ice Wind Load
- W_{service} = Service Wind Load

The following site-specific design parameters were considered in this analysis per the provisions of *TIA-222-H*:

- Class. ii
- Exposure: B
- Design Wind Speed: 123 mph *ATC Wind Speed*
- Design Ice Wind Speed: 50 mph
- Design Ice Thickness: 1.5 in
- Gust Effect Factor: 0.85 *Section 2.6.9.1*
- Wind Direction Probability Factor: 0.95 *Table 2-2*
- Serviceability Wind Speed: 60 mph *Sect. 2.8.3*

5.0 CALCULATIONS

Calculations for this analysis and the design of the installation are included in the Appendices of this report.

6.0 CONCLUSIONS, COMMENTARY, AND RECOMMENDATIONS

The analysis concludes that the proposed antennas and associated equipment are **adequate** for the proposed installation with the most unfavorable loading condition.

The existing cantilever pipe mounts used to support the proposed and existing equipment at the Alpha and Gamma sectors are loaded to **24.4%** of their strength capacity. The proposed stand-off frame in the Gamma sector is loaded to **37.8%** of its strength capacity. The existing steel ballast frame used to support the proposed and existing equipment at the Beta sector passes stability checks, based on a **minimum Factor of Safety of 1.5**. Based on engineering judgement, the overall stability of the Beta sector governs the design of the ballast frame, not the strength of the steel members.

Existing roof structure appears to be in fair condition at the locations of the proposed equipment.

Dewberry Engineers Inc. reserves the right to add to or modify this report if more information becomes available. The conclusions reached by Dewberry Engineers Inc. in this report are only applicable to the previously mentioned existing structural elements supporting the proposed wireless telecommunications installation. The results of this report are based on the assumption that existing structural elements have been installed per the original design documents, have been well maintained and are uncompromised. This report does not imply that a thorough inspection of the existing structure has been performed. Any deviation of the support condition, loading, location, placement, equipment configuration, etc., will require Dewberry Engineers Inc. to generate an additional structural analysis.

APPENDIX A

Analysis of Alpha and Gamma Sector Mast Pipe Mount

Overview

The Alpha and Gamma Sector antenna frames are composed of three cantilevered pipes, thru-bolted into the existing penthouse wall. The pipes are attached with horizontal unistrut members, which support antenna equipment. Since the unistrut is not a structural member, only the cantilevered pipes shall be checked, with the equipment loads from the unistrut being applied to the cantilevered pipe.

Design Criteria and References

1. International Building Code (IBC) 2015, International Code Council
2. 2018 Connecticut State Building Code - Amendments to IBC 2015
3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

Equipment Dead Loads

	Description	Dimensions (in)			Weight (lb)
		W	D	H	
Antennas/RRHs	CCI HPA-65R-BU6AA	11.70	7.60	71.00	51.00
	Ericsson RRUS B25 4415	13.40	5.90	16.50	46.00
	Ericsson RRUS B2/B66A 8843	13.20	10.90	14.90	72.00

*Bold = Proposed

Structural Members

Member	Dimensions (in)						Weight (lb/ft)
	d	b _t	t _f	t _w	I.D.	O.D.	
3" XS Pipe					3.07	3.50	7.55

Analysis of Alpha and Gamma Sector Mast Pipe Mount
Wind Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
$V_{max} =$	123.00	Design Wind Speed	ASCE 7-10, Appendix D
$V_i =$	50.00	Design Ice Wind Speed	TIA-222-H, Annex B-9
$K_d =$	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	II	Risk Category	TIA-222-H, Table 2-1
$I =$	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
$I_{ice\ thick} =$	1.00	Importance Factor (Ice Thickness)	TIA-222-H, Table 2-3
$z = h =$	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	B	Exposure Category	TIA-222-H, Section 2.6.5.1.2
$z_g =$	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
$a =$	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
$K_{z\ (min)} =$	0.70	Minimum Value for K_z	TIA-222-H, Table 2-4
$K_c =$	0.90	Terrain Constant	TIA-222-H, Table 2-4
$K_i =$	N/A	Topographic Constant	TIA-222-H, Table 2-5
$K_z =$	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
$e =$	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
$f =$	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
$H =$	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
$K_h =$	N/A	$e^{-(f+z)/H}$ Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
$K_{zt} =$	1.00	$= [1 + ((K_c * K_i) / K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
$K_{iz} =$	1.13	$= (z/33)^{0.10} \leq 1.4$ Height Escalation Factor	TIA-222-H, Section 2.6.10
$G_h =$	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
$K_a =$	0.9	Shielding Factor	TIA-222-H, Section 16.6
$t_i =$	1.50	Design Ice Thickness (in)	TIA-222-H, Annex B-9
$t_{iz} =$	3.40	$2 t_i (I_{ice\ thick}) K_{iz} (K_{zt})^{0.35}$ Thickness of Radial Glaze Ice	TIA-222-H, Section 2.6.10
$q_{z\ design} =$	34.23	$= 0.00256 (K_z) (K_{zt}) (K_d) (K_a) (V_{max}^2) (I)$	TIA-222-H, Section 2.6.11.6
$q_{z\ ice} =$	5.66	$= 0.00256 (K_z) (K_{zt}) (K_d) (K_a) (V_i^2)$	TIA-222-H, Section 2.6.11.6



Analysis of Alpha and Gamma Sector Mast Pipe Mount

Wind Service Load and Maintenance Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
$V_{service} =$	60.00	Design Service Wind Speed	TIA-222-H, Section 2.8.3
$V_{maintenance} =$	30.00	Design Maintenance Wind Speed	TIA-222-H, Section 16.3
$K_d =$	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	II	Risk Category	TIA-222-H, Table 2-1
$I =$	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
$z = h =$	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	B	Exposure Category	TIA-222-H, Section 2.6.5.1.2
$z_g =$	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
$a =$	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
$K_z (min) =$	0.70	Minimum Value for K_z	TIA-222-H, Table 2-4
$K_c =$	0.90	Terrain Constant	TIA-222-H, Table 2-4
$K_t =$	N/A	Topographic Constant	TIA-222-H, Table 2-5
$K_z =$	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
$e =$	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
$f =$	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
$H =$	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
$K_h =$	N/A	$e^{-(f*H)}$ Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
$K_{zt} =$	1.00	$= [1 + ((K_c * K_t) / K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
$G_h =$	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
$K_a =$	0.9	Shielding Factor	TIA-222-H, Section 16.6
$q_z service =$	8.14	$= 0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{service}^2)(I)$	TIA-222-H, Section 2.6.11.6
$q_z maintenance =$	2.04	$= 0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{maintenance}^2)(I)$	TIA-222-H, Section 2.6.11.6



Analysis of Alpha and Gamma Sector Mast Pipe Mount

Equipment Wind Loads (TIA-222-H)

$$F_A = q_z \text{ design } G_H (EPA)_A$$

$$(EPA)_A = C_e A_a$$

$$F_{A, ice} = q_z \text{ ice } G_H (EPA)_{A, ice}$$

$$(EPA)_{A, ice} = C_e A_{a, ice}$$

TIA-222-H, Section 2.6.11.2, Applies to Strength, Service & Maintenance Conditions

Ice Condition

Equipment	No Ice		Ice		Strength (lbs)		Ice (lbs)		Service (lbs)	
	(EPA) _A (Normal)	(EPA) _A (Tangent)	(EPA) _A (Normal)	(EPA) _A (Tangent)	F _A (Normal)	F _A (Tangent)	F _A (Normal)	F _A (Tangent)	F _A (Normal)	F _A (Tangent)
CCI HPA-65R-BU6AA	7.84	5.54	9.92	7.62	268.24	189.57	56.08	43.11	63.83	45.11
Ericsson RRUS B25 4415	1.84	0.82	2.67	1.45	63.06	28.07	15.07	8.18	15.01	6.68
Ericsson RRUS B2/B66A 8843	1.64	1.35	2.42	2.07	56.10	46.32	13.67	11.73	13.35	11.02

The proposed antenna frame layout consists of two RRH's, one of which is mounted directly behind the proposed antenna, and the other to unistrut spanning in between the antennas. For simplicity, the loads of 1.5 RRUS will be applied to the pipe STAAD model

Structure Wind Loads (TIA-222-H)

Wind loads on structural elements will be applied linearly: $w_{wind} = q_z \text{ design } C_s G_H d$, with d being the structure depth or diameter. A conservative Ca value of 1.2 will be used for pipes. This same equation will be used for the service condition, with the service wind load being used, and ice condition, with the ice wind load and ice structure depth/diameter being used.

Member	d (ft)	d _{ice} (ft)	C _s	w _{wind} (lb/ft)	w _{wind ice} (lb/ft)	w _{wind ser} (lb/ft)
3" XS Pipe	0.38	0.63	1.2	15.40	4.24	3.66

Analysis of Alpha and Gamma Sector Mast Pipe Mount
Ice Dead Loads

Equipment	Volume (cf)	Volume _{w/ice} (cf)	Volume _{ice} (cf)	W _{ice} (lb)
CCI HPA-65R-BU6AA	3.65	6.67	3.02	169.08
Ericsson RRUS B25 4415	0.75	1.65	0.89	49.96
Ericsson RRUS B2/B66A 8843	1.24	2.33	1.09	61.15

Structural Member	Perimeter (lf)	Perimeter _{w/ice} (lf)	Area _{ice} (sf)	W _{ice} (lb/ft)
3" XS Pipe	1.18	1.96	0.20	11.00

Load Combinations (TIA-222-H)

- | | | |
|----|--------------------------|----------------------|
| 1. | $1.2D + 1.0W_o$ | Strength Limit State |
| 2. | $1.2D + 1.0D_i + 1.0W_i$ | Strength Limit State |
| 3. | 1.4D | Strength Limit State |
| 4. | $1.0D + 1.0W_s$ | Service Limit State |



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Client AT&T

Job Information

	Engineer	Checked	Approved
Name:	CS	SA	
Date:	9/16/2019	9/17/2019	

Project ID	
Project Name	

Structure Type SPACE FRAME

Number of Nodes	7	Highest Node	7
Number of Elements	6	Highest Beam	6

Number of Basic Load Cases	8
Number of Combination Load Cases	7

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	DI
Primary	3	W(X)O
Primary	4	W(Z)O
Primary	5	W(X)I
Primary	6	W(Z)I
Primary	7	W(X)S
Primary	8	W(Z)S
Combination	9	1.2D + 1.0W(X)O
Combination	10	1.2D + 1.0W(Z)O
Combination	11	1.2D + 1.0DI + 1.0W(X)I
Combination	12	1.2D + 1.0DI + 1.0W(Z)I
Combination	13	1.4D
Combination	14	1.0D + 1.0W(X)S
Combination	15	1.0D + 1.0W(Z)S



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Part **Alpha & Gamma Sectors**

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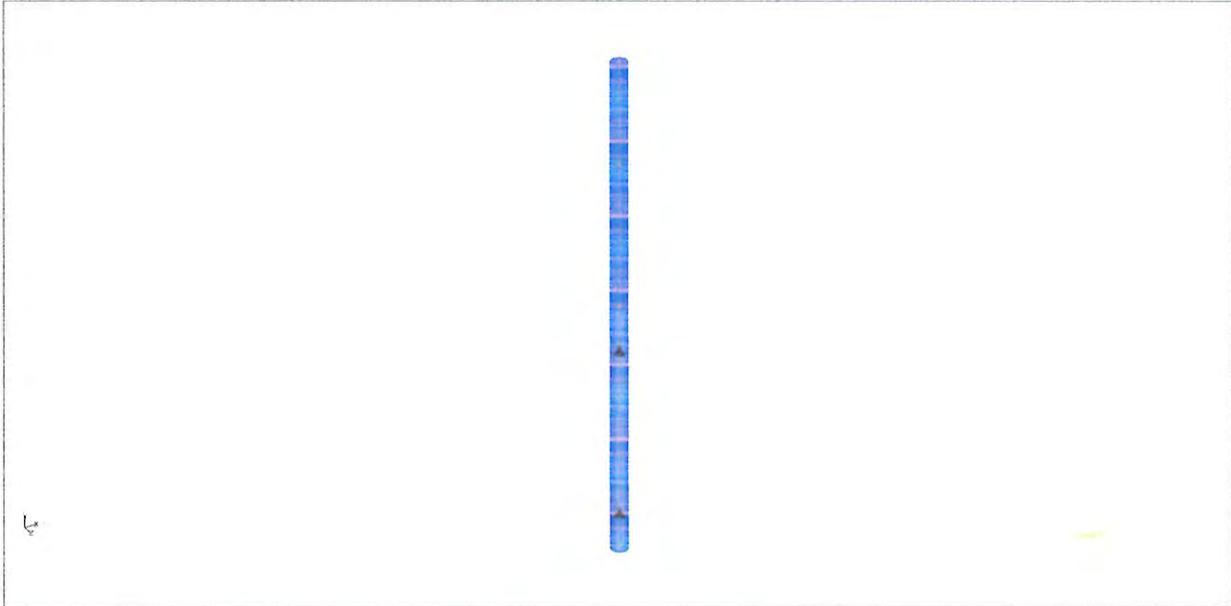
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Model

Nodes

Node	X (ft)	Y (ft)	Z (ft)
1	0	0	0
2	0	1.000	0
3	0	5.000	0
4	0	6.000	0
5	0	8.500	0
6	0	9.500	0
7	0	12.000	0

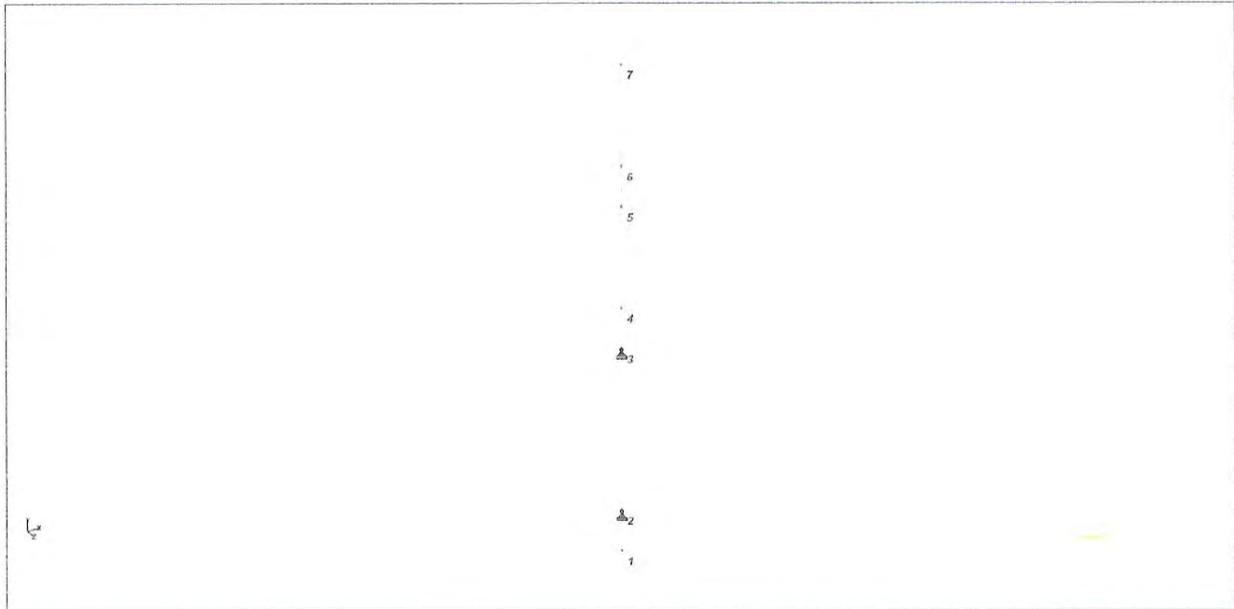


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Nodes

Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	2	1.000	1	0
2	2	3	4.000	1	0
3	3	4	1.000	1	0
4	4	5	2.500	1	0
5	5	6	1.000	1	0
6	6	7	2.500	1	0

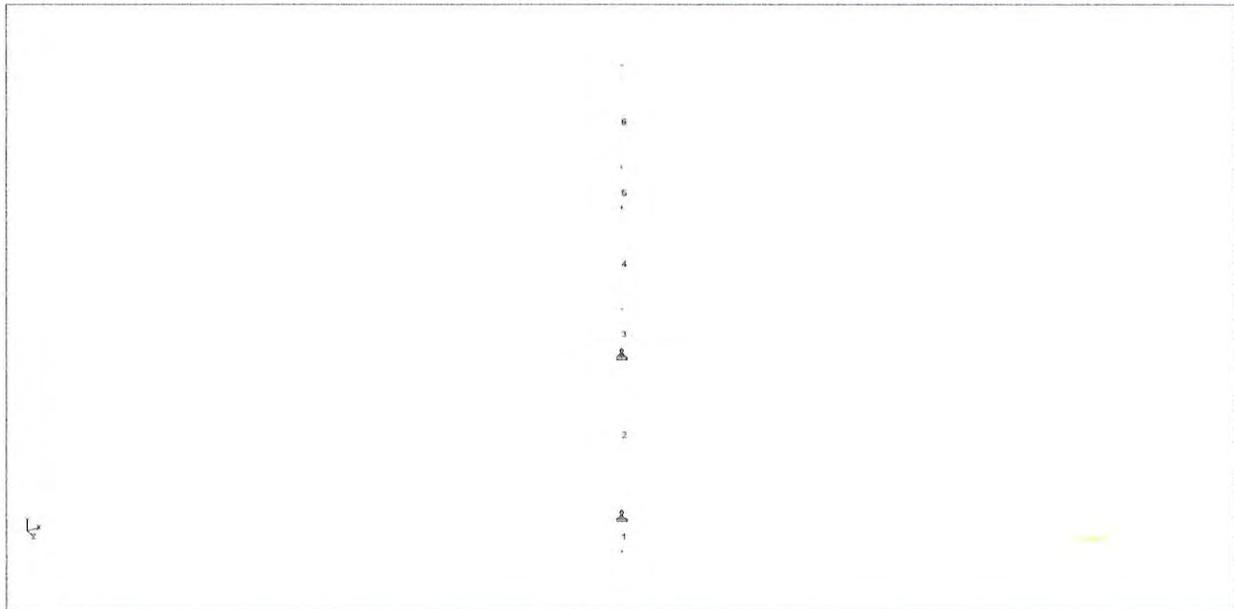


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Members

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
1	PIPS30	2.100	2.850	2.850	5.689	STEEL

Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E-6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E-6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E-6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E-6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E-6
7	STEEL	29E+3	0.300	0.000283	6E-6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
2	Fixed	Fixed	Fixed	-	-	-
3	Fixed	Fixed	Fixed	-	-	-



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Releases

There is no data of this type.

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	DI	Dead
3	W(X)O	Wind
4	W(Z)O	Wind
5	W(X)I	Wind
6	W(Z)I	Wind
7	W(X)S	Wind
8	W(Z)S	Wind

1 DL : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	-	-0.0255	-	-	-	-
5	-	-0.059	-	-	-	-
6	-	-0.059	-	-	-	-
7	-	-0.0255	-	-	-	-

1 DL : Selfweight

Direction	Factor	Assigned Geometry
Y	-1.000	ALL

2 DI : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	-	-0.08454	-	-	-	-
5	-	-0.0556	-	-	-	-
6	-	-0.0556	-	-	-	-
7	-	-0.08454	-	-	-	-



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2 DI : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI lbf/ft	GY	-1.100	-	-	-	-
2	UNI lbf/ft	GY	-1.100	-	-	-	-
3	UNI lbf/ft	GY	-1.100	-	-	-	-
4	UNI lbf/ft	GY	-1.100	-	-	-	-
5	UNI lbf/ft	GY	-1.100	-	-	-	-
6	UNI lbf/ft	GY	-1.100	-	-	-	-

3 W(X)O : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	0.095	-	-	-	-	-
5	0.0372	-	-	-	-	-
6	0.0372	-	-	-	-	-
7	0.095	-	-	-	-	-

3 W(X)O : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI lbf/ft	GX	15.400	-	-	-	-
2	UNI lbf/ft	GX	15.400	-	-	-	-
3	UNI lbf/ft	GX	15.400	-	-	-	-
4	UNI lbf/ft	GX	15.400	-	-	-	-
5	UNI lbf/ft	GX	15.400	-	-	-	-
6	UNI lbf/ft	GX	15.400	-	-	-	-

4 W(Z)O : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	-	-	-0.134	-	-	-
7	-	-	-0.134	-	-	-

5 W(X)I : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	0.02156	-	-	-	-	-
5	0.01	-	-	-	-	-
6	0.01	-	-	-	-	-
7	0.02156	-	-	-	-	-



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5 W(X)I : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI	lbf/ft	GX	4.240	-	-	-
2	UNI	lbf/ft	GX	4.240	-	-	-
3	UNI	lbf/ft	GX	4.240	-	-	-
4	UNI	lbf/ft	GX	4.240	-	-	-
5	UNI	lbf/ft	GX	4.240	-	-	-
6	UNI	lbf/ft	GX	4.240	-	-	-

6 W(Z)I : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	-	-	-0.02804	-	-	-
7	-	-	-0.02804	-	-	-

7 W(X)S : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	0.02256	-	-	-	-	-
5	0.00885	-	-	-	-	-
6	0.00885	-	-	-	-	-
7	0.02256	-	-	-	-	-

7 W(X)S : Beam Loads

Beam	Type	Direction	Fa	Da (ft)	Fb	Db	Ecc. (ft)
1	UNI	lbf/ft	GX	3.660	-	-	-
2	UNI	lbf/ft	GX	3.660	-	-	-
3	UNI	lbf/ft	GX	3.660	-	-	-
4	UNI	lbf/ft	GX	3.660	-	-	-
5	UNI	lbf/ft	GX	3.660	-	-	-
6	UNI	lbf/ft	GX	3.660	-	-	-

8 W(Z)S : Node Loads

Node	FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
4	-	-	-0.03192	-	-	-
7	-	-	-0.03192	-	-	-



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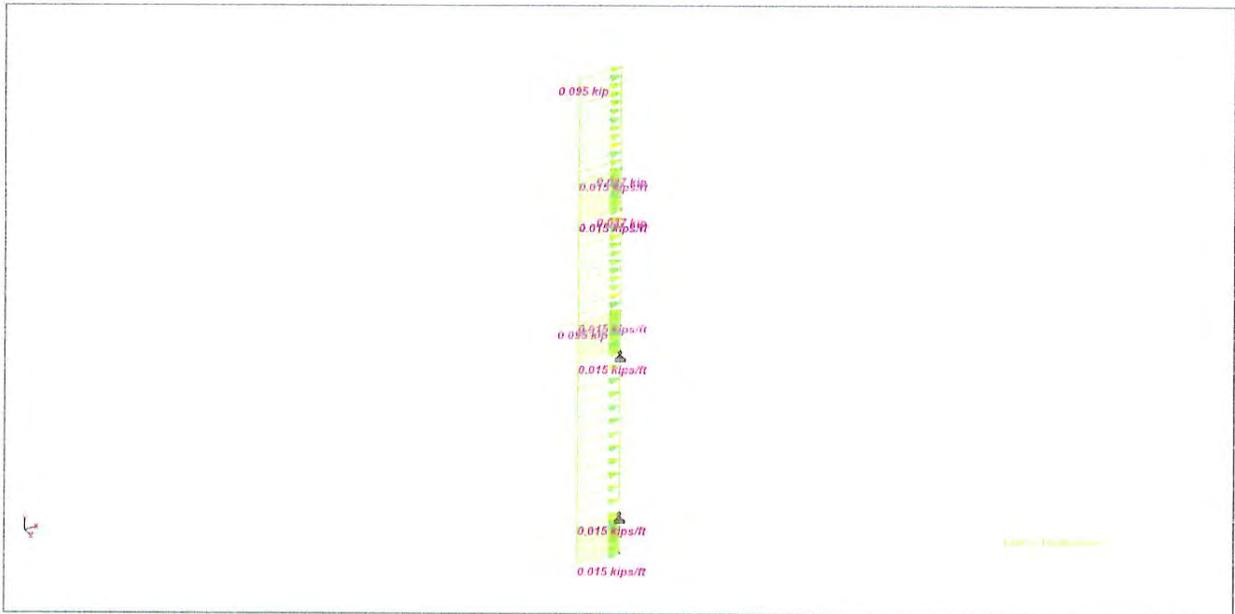
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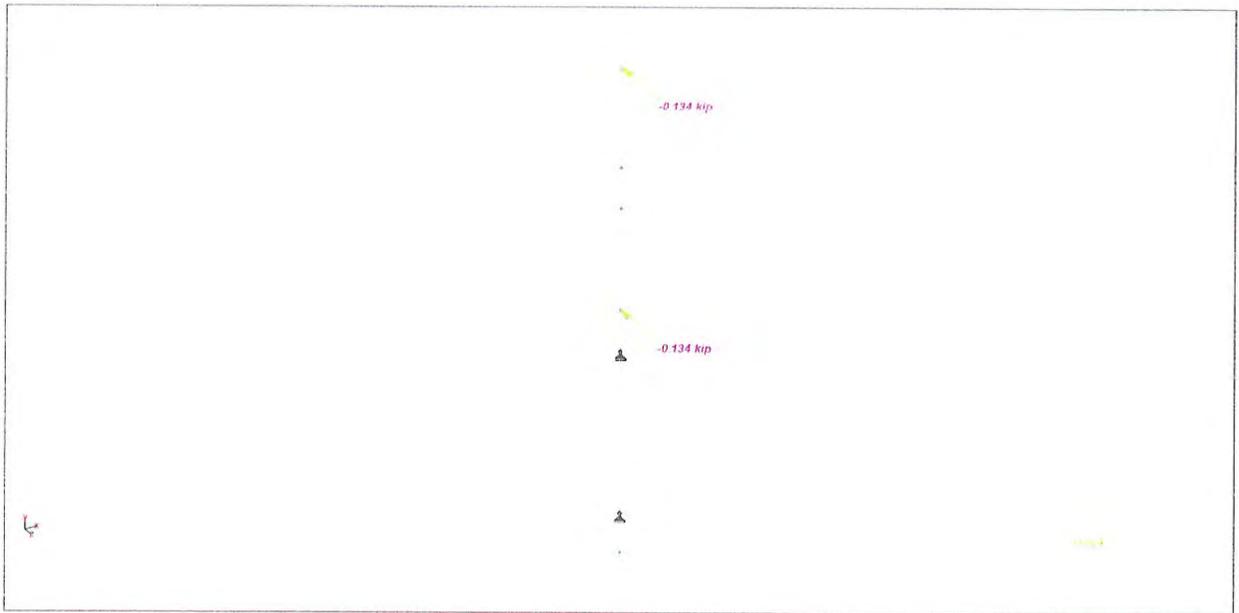
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Load Case 3



Load Case 4



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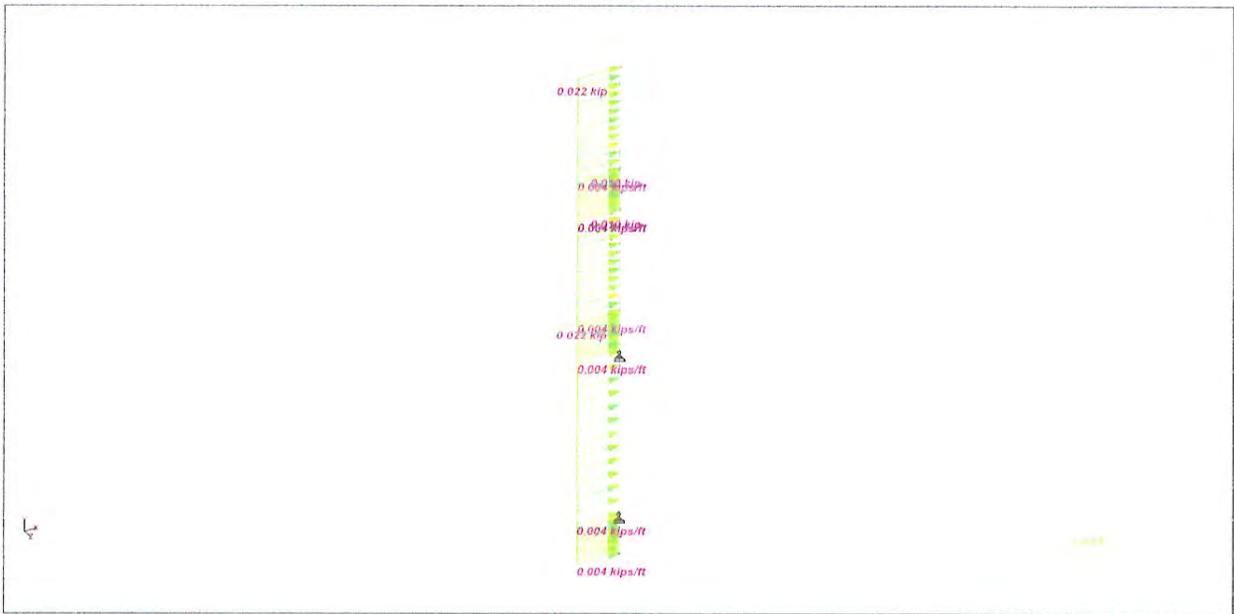
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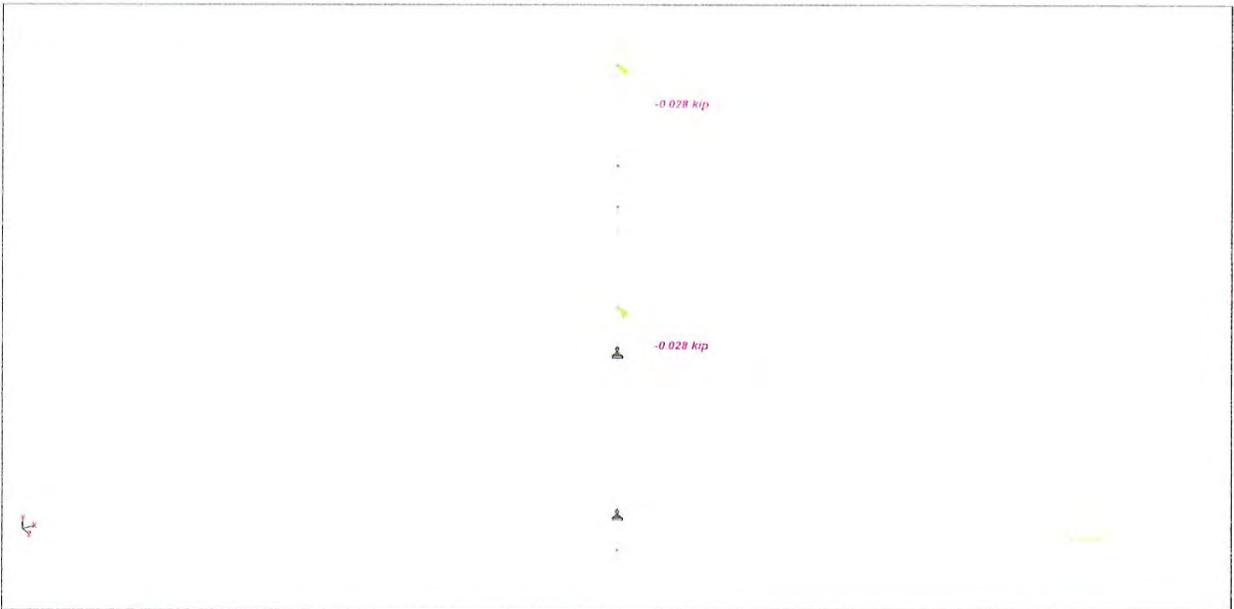
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Load Case 5



Load Case 6



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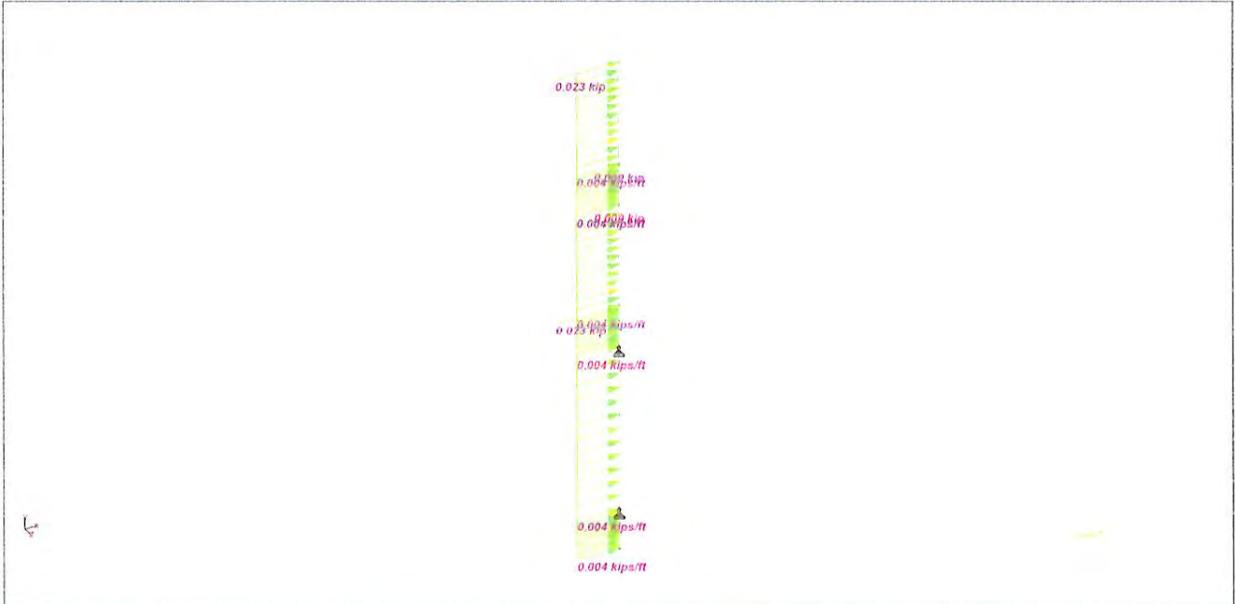
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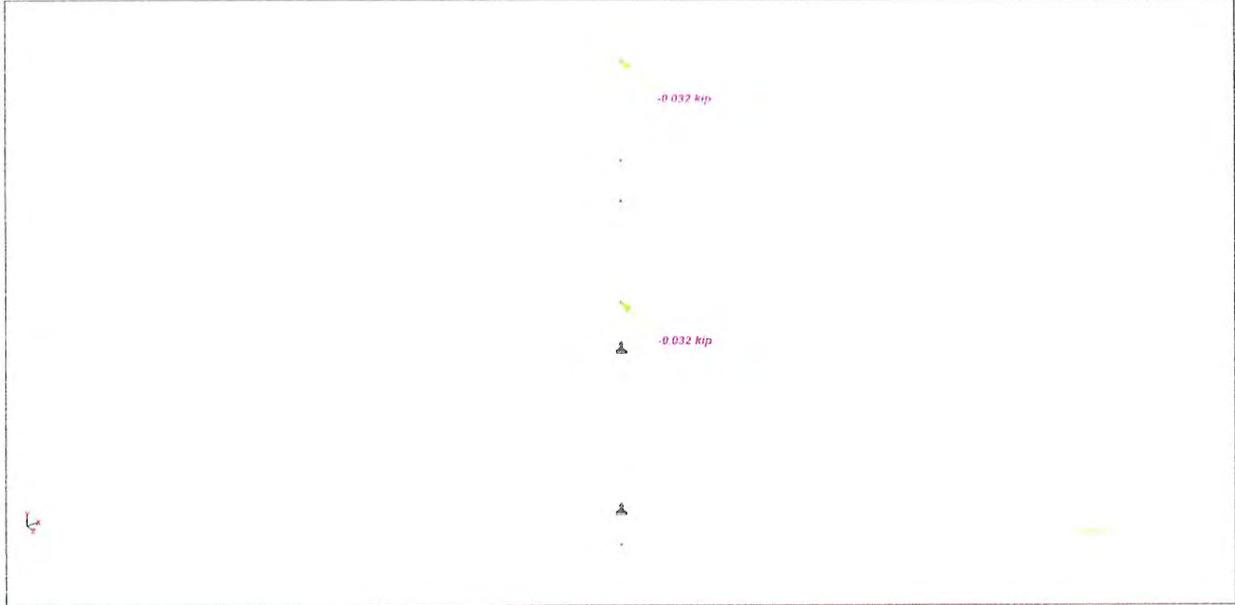
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Load Case 7



Load Case 8



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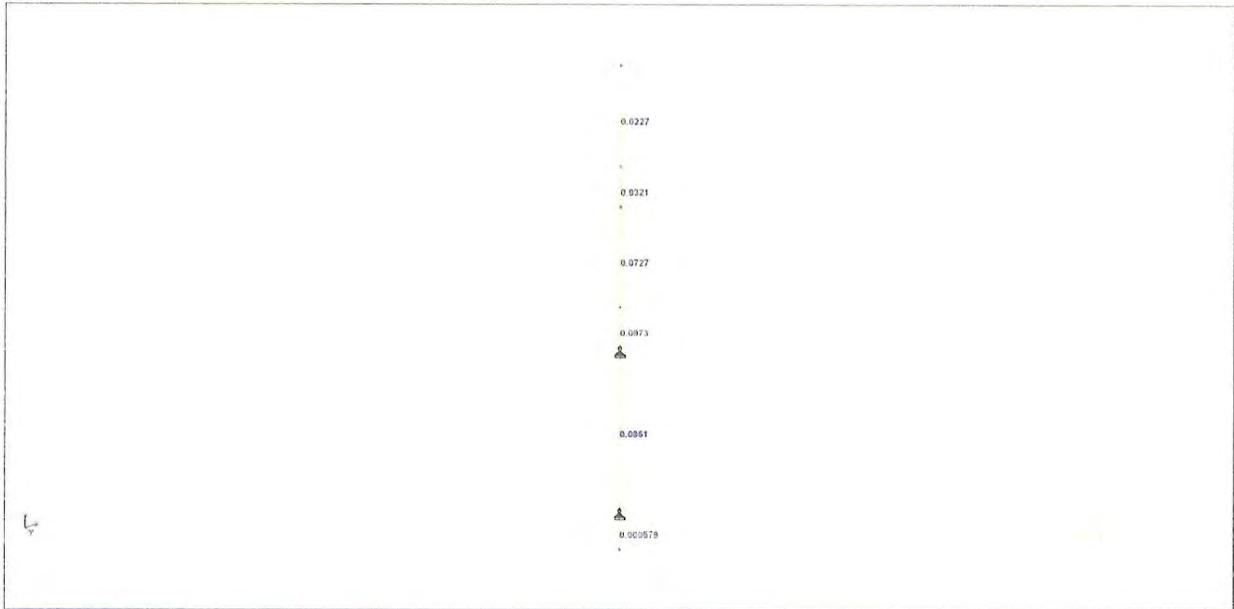
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Utilization Ratio

Beam	Analysis Property	Design Property	Actual Ratio	Allowable Ratio	Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
1	PIPS30	PIPS30	0.001	1.000	0.001	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
2	PIPS30	PIPS30	0.243	1.000	0.243	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
3	PIPS30	PIPS30	0.244	1.000	0.244	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
4	PIPS30	PIPS30	0.183	1.000	0.183	LRFD-H1-1B-	9	2.100	2.850	2.850	5.700
5	PIPS30	PIPS30	0.080	1.000	0.080	LRFD-H1-1B-	10	2.100	2.850	2.850	5.700
6	PIPS30	PIPS30	0.057	1.000	0.057	LRFD-H1-1B-	10	2.100	2.850	2.850	5.700

Failed Members

There is no data of this type.



Envelope Utilization Ratio



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Part Alpha & Gamma Sectors

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Date 9/16/2019

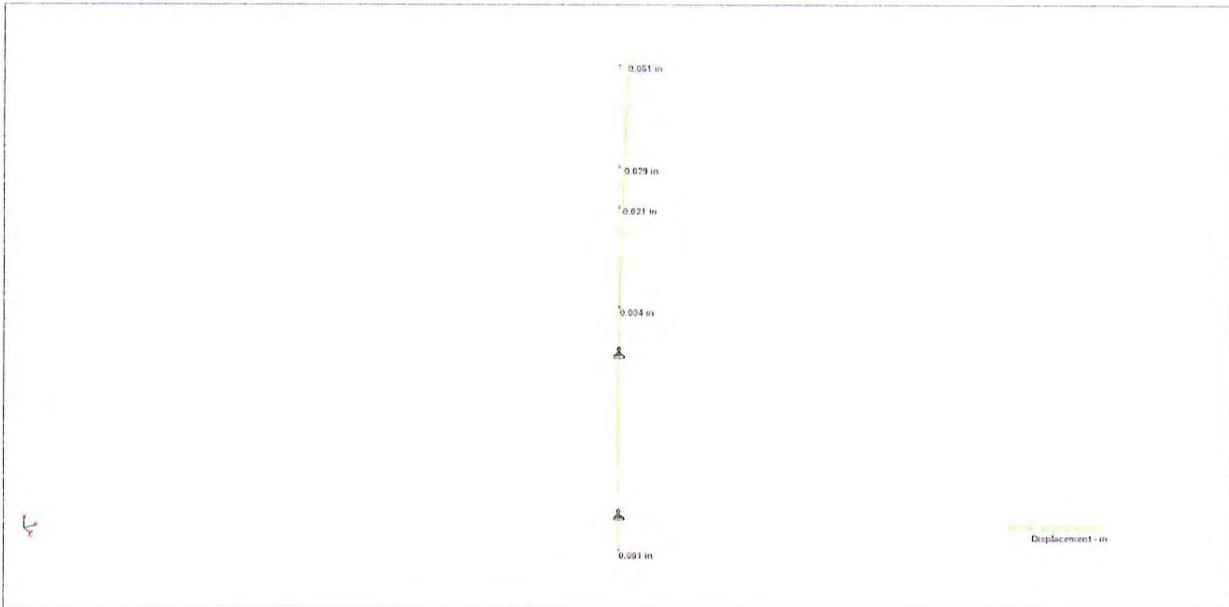
Chd SA

Client AT&T

File Alpha & Gamma Sector.s Date/Time 16-Sep-2019 11:42

Node Displacement Summary

	Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
Max X	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010
Min X	1	1:DL	0	-0.000	0	0.000	0	0	0
Max Y	2	1:DL	0	0	0	0	0	0	0
Min Y	7	11:1.2D + 1.0D	0.168	-0.000	0	0.168	0	0	-0.002
Max Z	1	1:DL	0	-0.000	0	0.000	0	0	0
Min Z	7	4:W(Z)O	0	0	-0.542	0.542	-0.008	0	0
Max rX	1	4:W(Z)O	0	0	-0.015	0.015	0.001	0	0
Min rX	7	4:W(Z)O	0	0	-0.542	0.542	-0.008	0	0
Max rY	1	1:DL	0	-0.000	0	0.000	0	0	0
Min rY	1	1:DL	0	-0.000	0	0.000	0	0	0
Max rZ	1	3:W(X)O	0.019	0	0	0.019	0	0	0.002
Min rZ	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010
Max Rst	7	3:W(X)O	0.679	0	0	0.679	0	0	-0.010



Displacement

Displacement Check
Antenna Pipe Mast (3 1/2" O.D. Pipe):
Max Displacement = 0.679"
(Node 7)
Allowable Displacement = 1.5% cantilever = 1.08"
0.697" < 1.26" -- OK



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Part **Alpha & Gamma Sectors**

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By **CS**

Date **9/16/2019**

Chd **SA**

Client **AT&T**

File **Alpha & Gamma Sectors.s**

Date/Time **16-Sep-2019 11:42**

Reaction Summary

	Node	L/C	Horizontal	Vertical	Horizontal	Moment		
			FX (kip)	FY (kip)	FZ (kip)	MX (kip in)	MY (kip in)	MZ (kip in)
Max FX	2	3:W(X)O	0.310	0	0	0	0	0
Min FX	3	3:W(X)O	-0.759	0	0	0	0	0
Max FY	3	11:1.2D + 1.0D	-0.190	0.570	0	0	0	0
Min FY	2	3:W(X)O	0.310	0	0	0	0	0
Max FZ	3	4:W(Z)O	0	0	0.536	0	0	0
Min FZ	2	4:W(Z)O	0	0	-0.268	0	0	0
Max MX	2	1:DL	0	0.021	0	0	0	0
Min MX	2	1:DL	0	0.021	0	0	0	0
Max MY	2	1:DL	0	0.021	0	0	0	0
Min MY	2	1:DL	0	0.021	0	0	0	0
Max MZ	2	1:DL	0	0.021	0	0	0	0
Min MZ	2	1:DL	0	0.021	0	0	0	0

Analysis of Alpha and Gamma Sector Mast Pipe MountDesign Criteria

1. TMS 402-11/ACI 530-11/ASCE 5-11 Building Code Requirements for Masonry Structures
2. ACI -318-11 Building Code Requirements for Structural Concrete
3. AISC 360-10 Specifications for Structural Steel Buildings

References

Refer to construction drawings by Hudson Design Group, dated November 8, 2016 for pipe mount connection details (Bolt diameter field verified by Dewberry Engineers Inc. on 07/26/2019)

Thru Bolt Check

$M =$	2.28 kip-in	F_x * (1/2 Angle depth), See Appendix A-28 for F_x
$d =$	9.50 in	Spacing of Thru Bolts
$T =$	0.24 kip	Tension in 5/8" Thru Bolt
$f_{y \text{ thru bolt}} =$	0.78 ksi	Tensile Stress in Thru Bolt --> OK BY INSPECTION
$F_x =$	0.759	See Appendix A-28
$V_{\text{thru bolt}} =$	0.38 kip	Shear at 5/8" Thru Bolt
$f_{v \text{ thru bolt}} =$	1.24 ksi	Shear Stress in Thru Bolt --> OK BY INSPECTION

Penthouse Wall Global Check

Based on Engineering Judgement, the loads produced by the antenna mounting pipes is negligible on the penthouse CMU and steel stud walls

APPENDIX B

Analysis of Gamma Sector Stand-off Frame

Overview

The existing C1 position antenna in the gamma sector is going to be relocated to a proposed 3'-0" stand-off frame. The antenna will be mounted to a 3" diameter sch. 40 pipe, which will be U-bolted to the proposed stand-off frame, and proposed stand-off frame will be thru-bolted to the existing penthouse wall. Only the 4" diameter pipe will be checked for strength.

Design Criteria and References

1. International Building Code (IBC) 2015, International Code Council
2. 2018 Connecticut State Building Code - Amendments to IBC 2015
3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

Equipment Dead Loads

	Description	Dimensions (in)			Weight (lb)
		W	D	H	
Antennas/RRHs	Kathrein 800-10965	20.00	6.90	78.70	108.60
	RRU 4415 B25	13.40	5.90	16.50	46.00

*Bold = Proposed

Structural Members

Member	Dimensions (in)						Weight (lb/ft)
	d	b _f	t _f	t _w	I.D.	O.D.	
3" STD Pipe					3.07	3.50	7.58
HSS4X4X1/4*	4.00	4.00		0.233			12.21

*Approximate member size for Site Pro 1 Standoff Arm

Analysis of Gamma Sector Stand-off Frame
Wind Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
$V_{max} =$	123.00	Design Wind Speed	ASCE 7-10, Appendix D
$V_i =$	50.00	Design Ice Wind Speed	TIA-222-H, Annex B-9
$K_d =$	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	II	Risk Category	TIA-222-H, Table 2-1
$I =$	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
$I_{ice\ thick} =$	1.00	Importance Factor (Ice Thickness)	TIA-222-H, Table 2-3
$z = h =$	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	B	Exposure Category	TIA-222-H, Section 2.6.5.1.2
$Z_g =$	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
$a =$	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
$K_{z\ (min)} =$	0.70	Minimum Value for K_z	TIA-222-H, Table 2-4
$K_c =$	0.90	Terrain Constant	TIA-222-H, Table 2-4
$K_t =$	N/A	Topographic Constant	TIA-222-H, Table 2-5
$K_z =$	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
$e =$	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
$f =$	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
$H =$	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
$K_h =$	N/A	$e^{-(f+z)/H}$ Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
$K_{zt} =$	1.00	$= [1 + ((K_c * K_t) / K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
$K_{iz} =$	1.13	$= (z/33)^{0.10} \leq 1.4$ Height Escalation Factor	TIA-222-H, Section 2.6.10
$G_h =$	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
$K_a =$	0.9	Shielding Factor	TIA-222-H, Section 16.6
$t_i =$	1.50	Design Ice Thickness (in)	TIA-222-H, Annex B-9
$t_{iz} =$	3.40	$2 t_i (I_{ice\ thick}) K_{iz} (K_{zt})^{0.35}$ Thickness of Radial Glaze Ice	TIA-222-H, Section 2.6.10
$Q_z\ design =$	34.23	$= 0.00256 (K_z) (K_{zt}) (K_d) (K_a) (V_{max}^2) (I)$	TIA-222-H, Section 2.6.11.6
$Q_z\ ice =$	5.66	$= 0.00256 (K_z) (K_{zt}) (K_d) (K_a) (V_i^2)$	TIA-222-H, Section 2.6.11.6

Analysis of Gamma Sector Stand-off Frame
Wind Service Load and Maintenance Load Design Criteria (Per TIA-222-H)

Notation	Value	Description	Reference
$V_{service} =$	60.00	Design Service Wind Speed	TIA-222-H, Section 2.8.3
$V_{maintenance} =$	30.00	Design Maintenance Wind Speed	TIA-222-H, Section 16.3
$K_d =$	0.95	Wind Direction Probability Factor	TIA-222-H, Table 2-2
Class	II	Risk Category	TIA-222-H, Table 2-1
$I =$	1.00	Importance Factor (Without Ice)	TIA-222-H, Table 2-3
$z = h =$	117.00	A.G.L. Elevation (ft)	Max. Center of Appurtenance
Exp. Cat.	B	Exposure Category	TIA-222-H, Section 2.6.5.1.2
$z_g =$	1200.00	Nominal Height of Atmospheric Boundary Layer	TIA-222-H, Table 2-4
$a =$	7.00	3-Second Gust Wind Speed Power Law Exponent	TIA-222-H, Table 2-4
$K_z (min) =$	0.70	Minimum Value for K_z	TIA-222-H, Table 2-4
$K_c =$	0.90	Terrain Constant	TIA-222-H, Table 2-4
$K_t =$	N/A	Topographic Constant	TIA-222-H, Table 2-5
$K_z =$	1.03	Velocity Pressure Coefficient	TIA-222-H, Section 2.6.5.2
Topo. Cat.	1.00	Topographic Category	TIA-222-H, Section 2.6.5.2
$e =$	2.72	Natural Logarithmic Base	TIA-222-H, Section 2.6.2
$f =$	N/A	Height Attenuation Factor	TIA-222-H, Table 2-5
$H =$	N/A	Height of Crest Above Surrounding Terrain (ft)	TIA-222-H, Section 2.6.6.2.1
$K_h =$	N/A	$e^{-(f+z)/H}$ Height Reduction Factor	TIA-222-H, Section 2.6.6.2.1
$K_{zt} =$	1.00	$= [1 + ((K_c * K_t) / K_h)]^2$ Topographic Factor	TIA-222-H, Section 2.6.6.2.1
$G_h =$	1.0	Gust Effect Factor	TIA-222-H, Section 2.6.9.1
$K_a =$	0.9	Shielding Factor	TIA-222-H, Section 16.6
$q_{z,service} =$	8.14	$= 0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{service}^2)(I)$	TIA-222-H, Section 2.6.11.6
$q_{z,maintenance} =$	2.04	$= 0.00256(K_z)(K_{zt})(K_d)(K_a)(V_{maintenance}^2)(I)$	TIA-222-H, Section 2.6.11.6



**Analysis of Gamma Sector Stand-off Frame
Equipment Wind Loads (TIA-222-H)**

TIA-222-H, Section 2.6.11.2, Applies to Strength, Service & Maintenance Conditions

Ice Condition

$$F_A = q_{z, design} G_n (EPA)_A$$

$$(EPA)_A = C_e A_b$$

$$F_A = q_{z, ice} G_n (EPA)_{A, ice}$$

$$(EPA)_{A, ice} = C_e A_{s, ice}$$

Equipment	No Ice		Ice		Strength (lbs)		Ice (lbs)		Service (lbs)	
	(sf)		(sf)		F _A (Normal)	F _A (Tangent)	F _A (Normal)	F _A (Tangent)	F _A (Normal)	F _A (Tangent)
	(EPA) _A (Normal)	(EPA) _A (Tangent)	(EPA) _A (Normal)	(EPA) _A (Tangent)						
Kathrein 800-10965	13.81	5.83	16.27	8.18	472.79	199.65	92.01	46.24	112.50	47.51
RRU 4415 625	1.76	0.85	2.54	1.43	60.10	29.15	14.34	8.09	14.30	6.94
Antennas/RHs										

Structure Wind Loads (TIA-222-H)

Wind loads on structural elements will be applied linearly: $w_{wind} = q_{z, design} C_e G_n d$, with d being the structure depth or diameter. A conservative C_e value of 1.2 will be used for pipes and 2.0 for HSS. This same equation will be used for the service condition, with the service wind load being used, and ice condition, with the ice wind load and ice structure depth/diameter being used.

Member	d (ft)	d _{ice} (ft)	C _e	w _{wind} (lb/ft)	w _{wind, ice} (lb/ft)	w _{wind, ser} (lb/ft)
3" STD Pipe	0.29	0.54	1.2	11.98	3.68	2.85
HSS4X4X1/4*	0.33	0.58	2.0	22.82	6.60	5.43

Analysis of Gamma Sector Stand-off Frame
Ice Dead Loads

Equipment	Volume (cf)	Volume _{w/ice} (cf)	Volume _{ice} (cf)	W _{ice} (lb)
Kathrein 800-10965	6.29	10.77	4.48	250.91
RRU 4415 B25	0.75	1.65	0.89	49.96

Structural Member	Perimeter (lf)	Perimeter _{w/ice} (lf)	Area _{ice} (sf)	W _{ice} (lb/ft)
3" STD Pipe	0.92	1.70	0.16	9.16
HSS4X4X1/4*	1.33	2.33	0.23	12.83

Load Combinations (TIA-222-H)

- | | | |
|----|--|----------------------|
| 1. | 1.2D + 1.0W _o | Strength Limit State |
| 2. | 1.2D + 1.0D _i + 1.0W _i | Strength Limit State |
| 3. | 1.4D | Strength Limit State |
| 4. | 1.0D + 1.0W _s | Service Limit State |



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Job No 50093840	Sheet No B - 1	Rev
Part Alpha & Gamma Sectors		
Ref		
By CS	Date 9/10/2019	Chd BK
File Gamma Sector Standoff.s	Date/Time 10-Sep-2019 13:30	

Job Title CT2490 - East Hampton Main Street

Client AT&T

Job Information

	Engineer	Checked	Approved
Name:	CS	BK	
Date:	9/10/2019	9/12/2019	8/15/2019

Project ID	
Project Name	

Structure Type SPACE FRAME

Number of Nodes	9	Highest Node	12
Number of Elements	6	Highest Beam	10

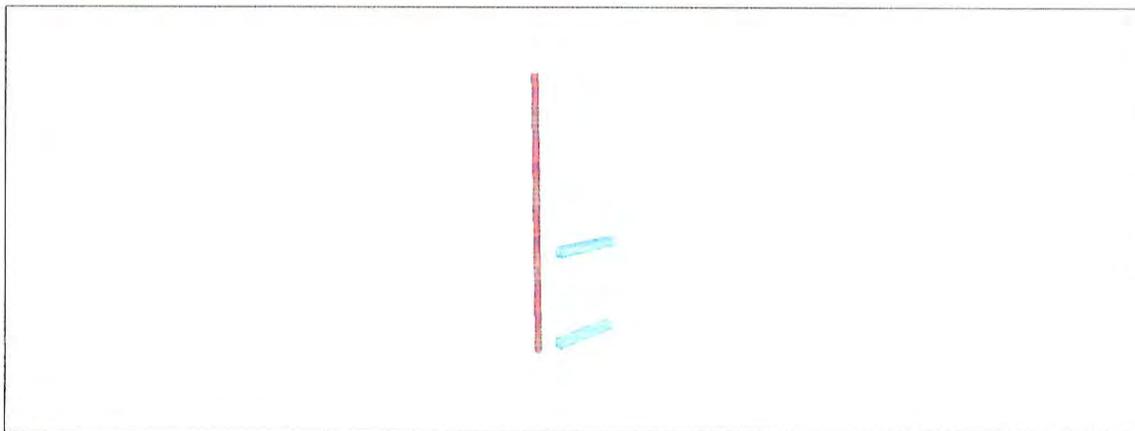
Number of Basic Load Cases	5
Number of Combination Load Cases	5

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	DI
Primary	3	W
Primary	4	W(l)
Primary	5	W(S)
Combination	6	1.2D + 1.0W
Combination	7	1.2D + 1.0DI + 1.0W(l)
Combination	8	1.4D
Combination	9	1.0D + 1.0W(S)



3D Rendered View



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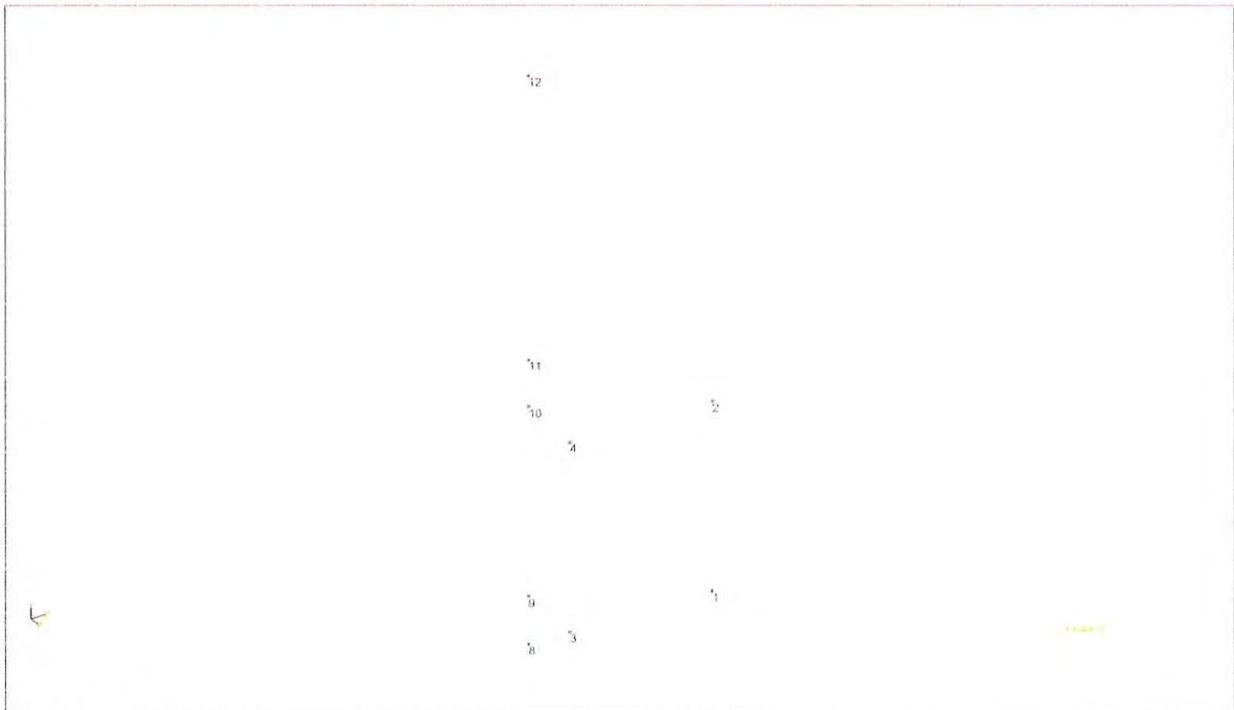
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File **Gamma Sector Standoff.s**

Date/Time **10-Sep-2019 13:30**

Nodes

Node	X (ft)	Y (ft)	Z (ft)
1	0	0	0
2	0	4.000	0
3	-3.000	0	0
4	-3.000	4.000	0
8	-3.000	-1.000	-1.500
9	-3.000	0	-1.500
10	-3.000	4.000	-1.500
11	-3.000	5.000	-1.500
12	-3.000	11.000	-1.500



Node Layout



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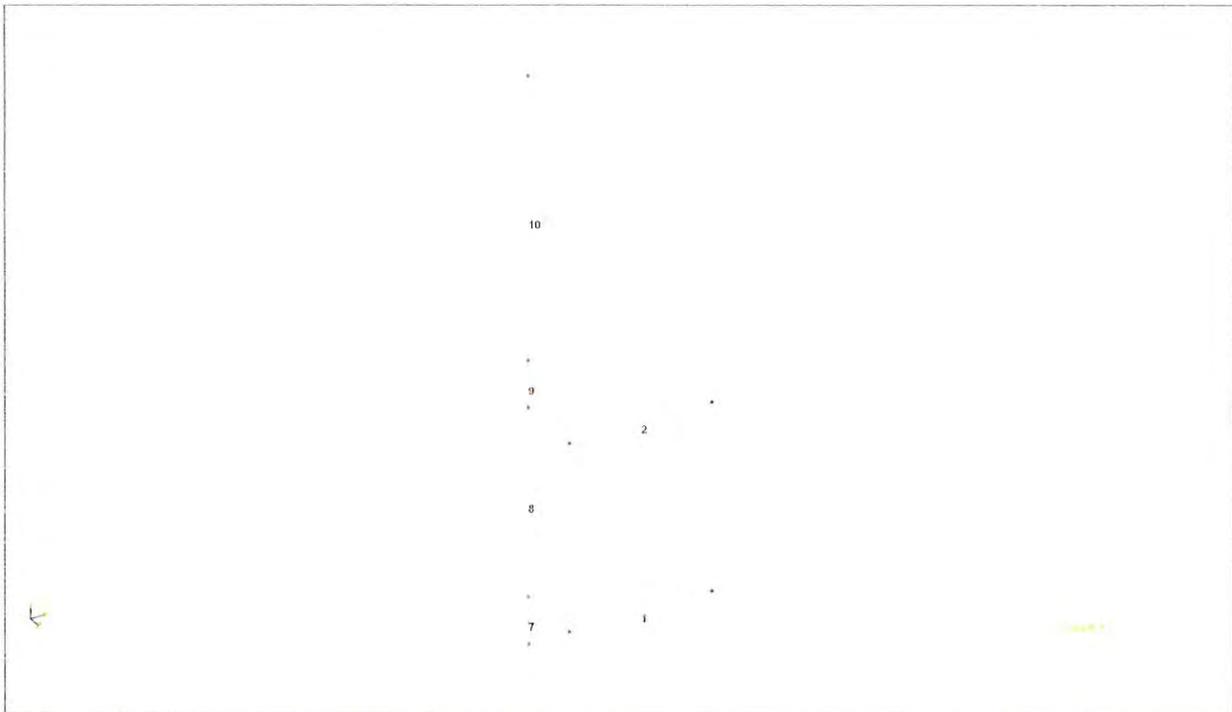
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Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	3	3.000	2	0
2	2	4	3.000	2	0
7	8	9	1.000	1	0
8	9	10	4.000	1	0
9	10	11	1.000	1	0
10	11	12	6.000	1	0



Beam Layout

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
1	PIPS30	2.100	2.850	2.850	5.689	STEEL
2	HSST4X4X0.125	1.770	4.400	4.400	6.797	STEEL



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Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (1°/F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E-6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E-6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E-6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E-6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E-6
7	STEEL	29E+3	0.300	0.000283	6E-6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip·ft/deg)	rY (kip·ft/deg)	rZ (kip·ft/deg)
1	Fixed	Fixed	Fixed	-	Fixed	-
2	Fixed	Fixed	Fixed	-	Fixed	-

Releases

There is no data of this type.

Primary Load Cases

Number	Name	Type
1	DL	Dead
2	DI	Dead
3	W	Wind
4	W(I)	Wind
5	W(S)	Wind



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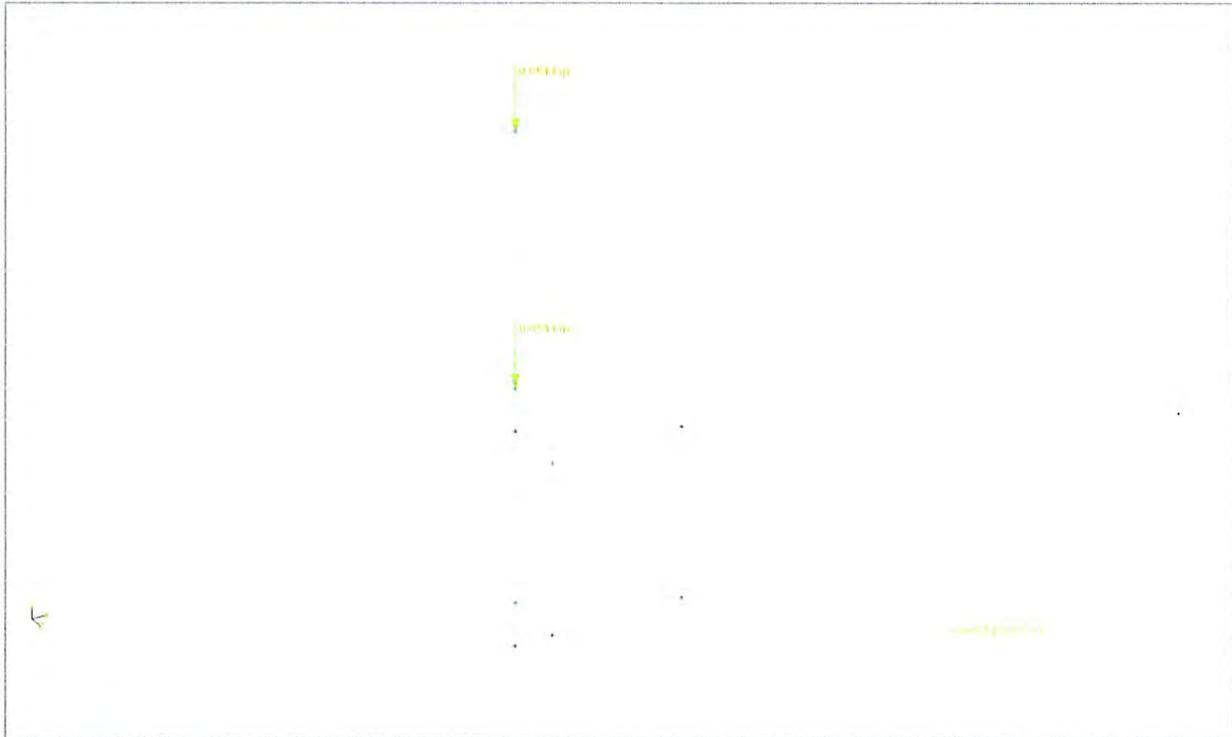
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Part Alpha & Gamma Sectors		
Ref		
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Combination Load Cases

Comb.	Combination L/C Name	Primary	Primary L/C Name	Factor
6	1.2D + 1.0W	1	DL	1.20
		3	W	1.00
7	1.2D + 1.0DI + 1.0W(I)	1	DL	1.20
		2	DI	1.00
		4	W(I)	1.00
8	1.4D	1	DL	1.40
9	1.0D + 1.0W(S)	1	DL	1.00
		5	W(S)	1.00
10	1D+1WL(Z)	1	DL	1.00
		3	W	1.00



Load Case 1



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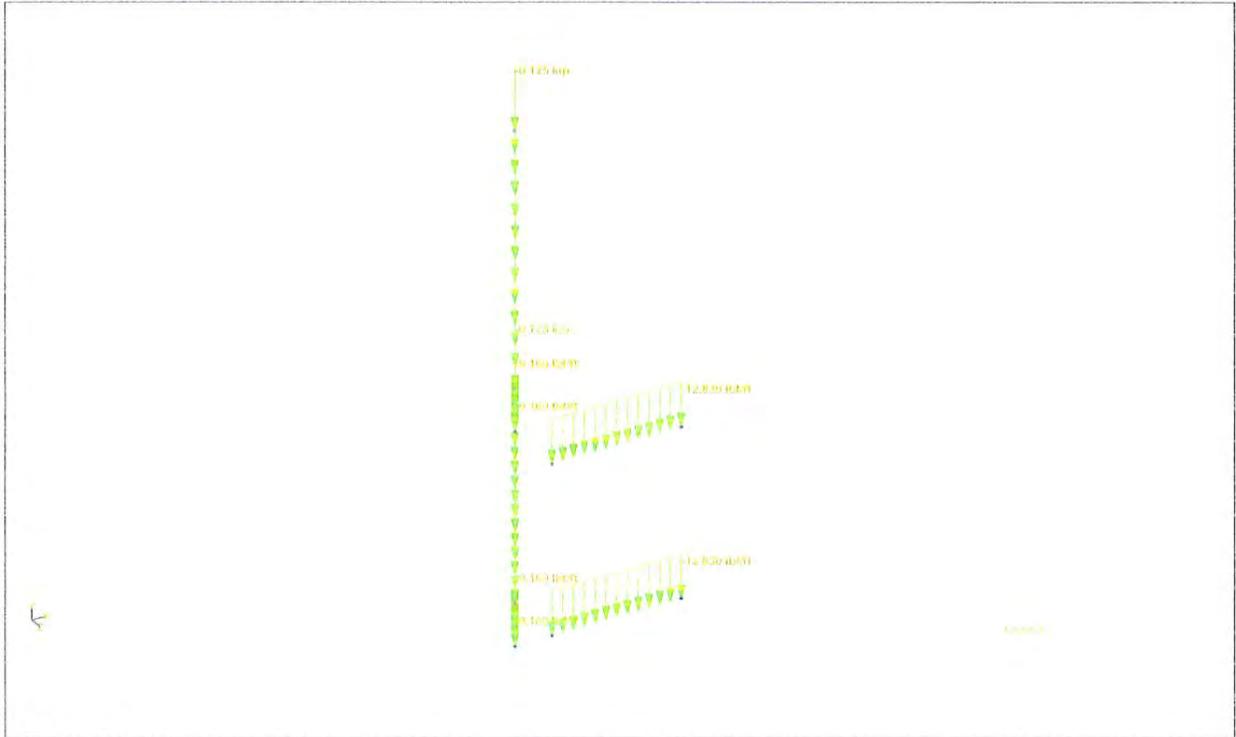
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Load Case 2



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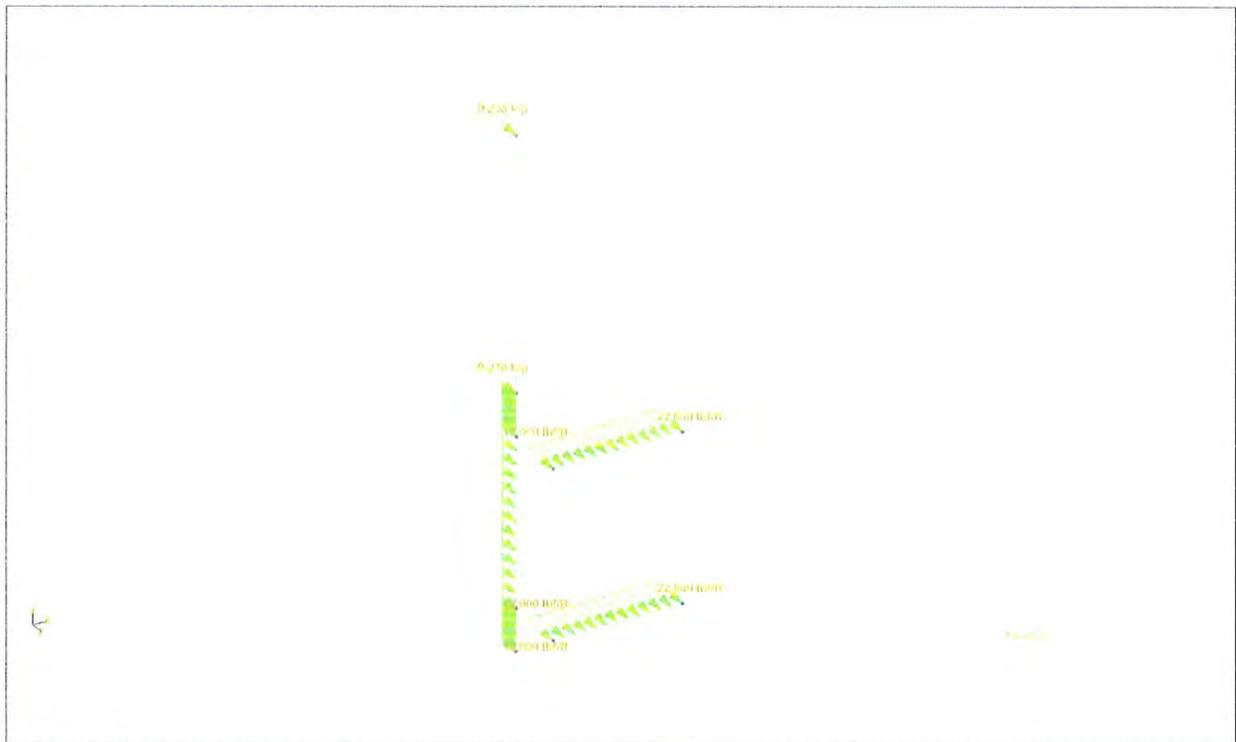
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Load Case 3



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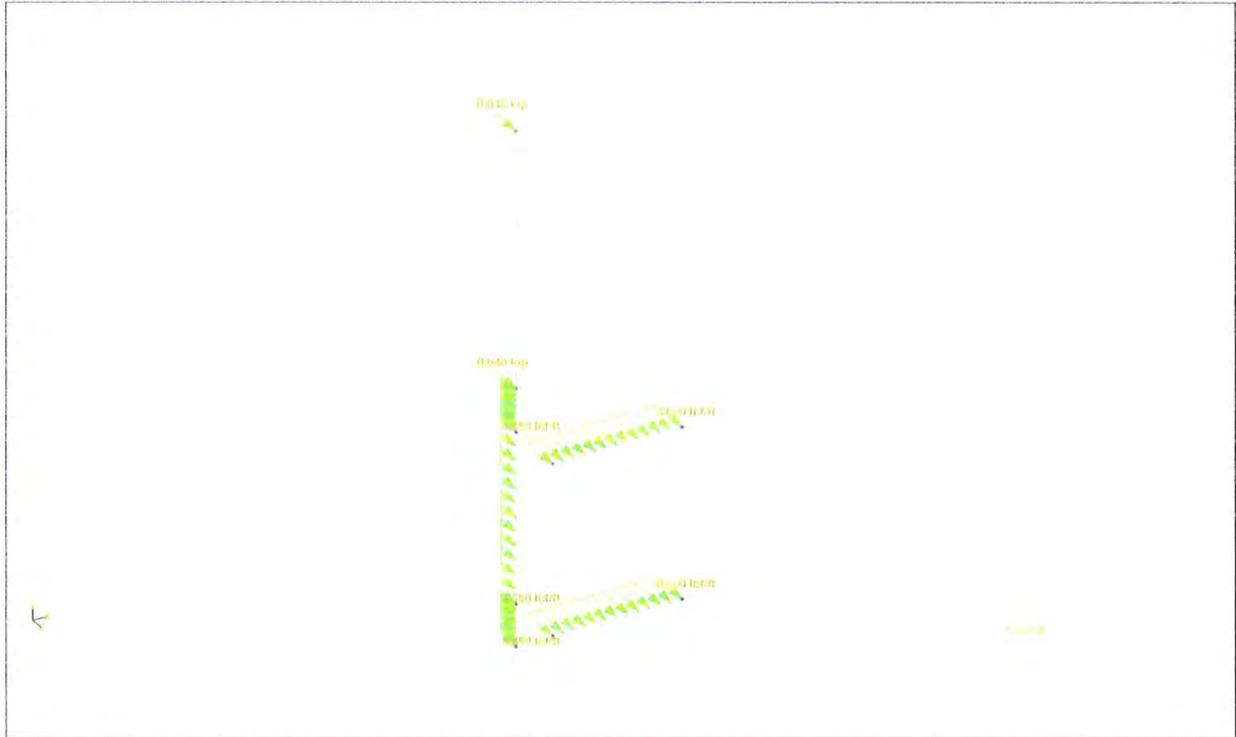
Date 9/10/2019

Chd BK

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File Gamma Sector Standoff.t

Date/Time 10-Sep-2019 13:30



Load Case 4

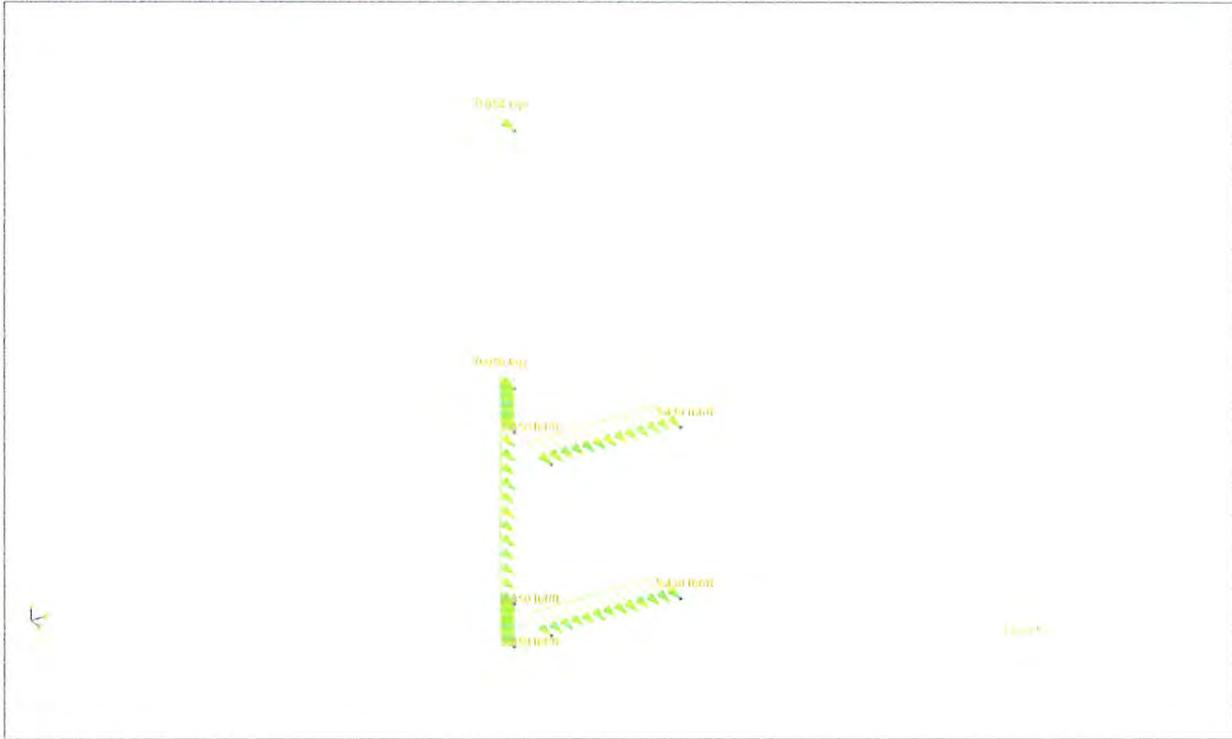


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Part Alpha & Gamma Sectors		
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File Gamma Sector Standoff.s	Date/Time 10-Sep-2019 13:30	

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Load Case 5

Utilization Ratio

Beam	Analysis Property	Design Property	Actual Ratio	Allowable Ratio	Ratio (Act./Allow.)	Clause	L/C	Ax (in ²)	Iz (in ⁴)	Iy (in ⁴)	Ix (in ⁴)
1	HSST4X4X0	HSST4X4X0	0.209	1.000	0.209	HSS FLEX+A	7	1.770	4.400	4.400	6.910
2	HSST4X4X0	HSST4X4X0	0.378	1.000	0.378	HSS BEND Y	3	1.770	4.400	4.400	6.910
7	PIPS30	PIPS30	0.001	1.000	0.001	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700
8	PIPS30	PIPS30	0.301	1.000	0.301	LRFD-H1-1B-	3	2.100	2.850	2.850	5.700
9	PIPS30	PIPS30	0.322	1.000	0.322	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700
10	PIPS30	PIPS30	0.241	1.000	0.241	LRFD-H1-1B-	6	2.100	2.850	2.850	5.700

Failed Members

There is no data of this type.



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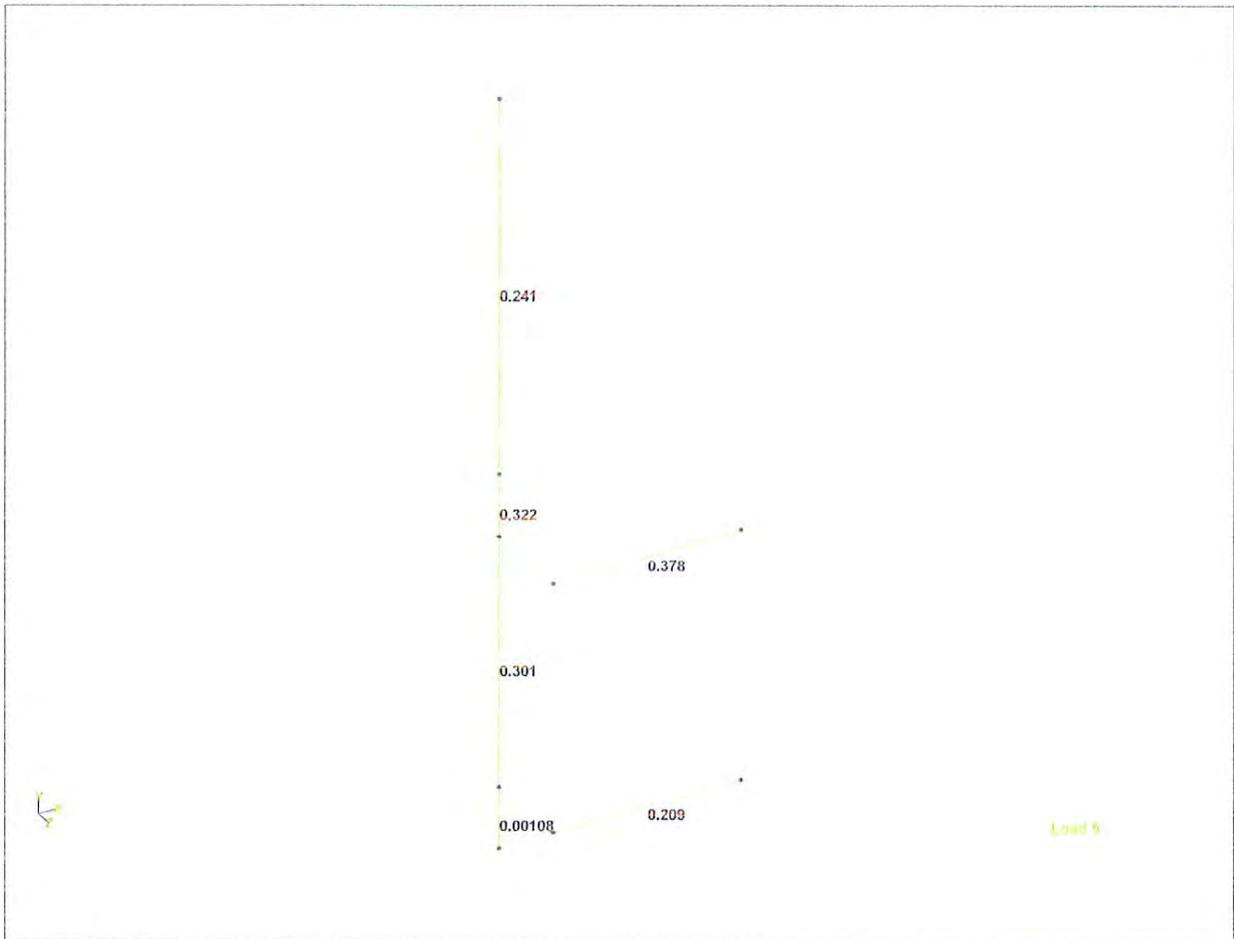
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File **Gamma Sector Standoff.s**

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Utilization Ratio



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Part Alpha & Gamma Sectors

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Node Displacements

Node	L/C	X (in)	Y (in)	Z (in)	Resultant (in)	rX (rad)	rY (rad)	rZ (rad)
11	1:DL	-0.012	-0.036	0.001	0.038	-0.000	0.000	0.001
	2:DI	-0.022	-0.068	0.002	0.07118	-0.000	0.000	0.001
	3:W	-0.095	0.011	0.194	0.217	0.009	0.004	0.003
	4:W(l)	-0.019	0.002	0.038596	0.043	0.002	0.001	0.000
	5:W(S)	-0.023	0.003	0.046	0.052	0.002	0.001	0.001
	6:1.2D + 1.0W	-0.109	-0.032	0.196	0.226	0.009	0.004	0.003
	7:1.2D + 1.0DI	-0.055	-0.109	0.042	0.129	0.002	0.002	0.002
	8:1.4D	-0.016	-0.050	0.001	0.053	-0.000	0.000	0.001
	9:1.0D + 1.0W(l)	-0.034	-0.033	0.047	0.067	0.002	0.001	0.001
12	1:DL	-0.053	-0.036	-0.006	0.064	-0.000	0.000	0.001
	2:DI	-0.100	-0.068	-0.009	0.121	-0.000	0.000	0.001
	3:W	-0.280	0.011	1.222	1.254	0.017	0.004	0.003
	4:W(l)	-0.055	0.002	0.238	0.245	0.003	0.001	0.000
	5:W(S)	-0.067	0.003	0.291	0.298	0.004	0.001	0.001
	6:1.2D + 1.0W	-0.344	-0.033	1.216	1.264	0.017	0.004	0.003
	7:1.2D + 1.0DI	-0.219	-0.109	0.222	0.330	0.003	0.002	0.002
	8:1.4D	-0.074	-0.050	-0.008	0.090	-0.000	0.000	0.001
	9:1.0D + 1.0W(l)	-0.120	-0.034	0.285	0.311	0.004	0.001	0.001

Relative Displacement Check

Antenna Pipe Mast (3 1/2" O.D. Pipe):

Max Displacement = 1.038"

(Node 12 with respect to 11)

Allowable Displacement = 1.5% cantilever = 1.260"

1.038" < 1.26" -- OK



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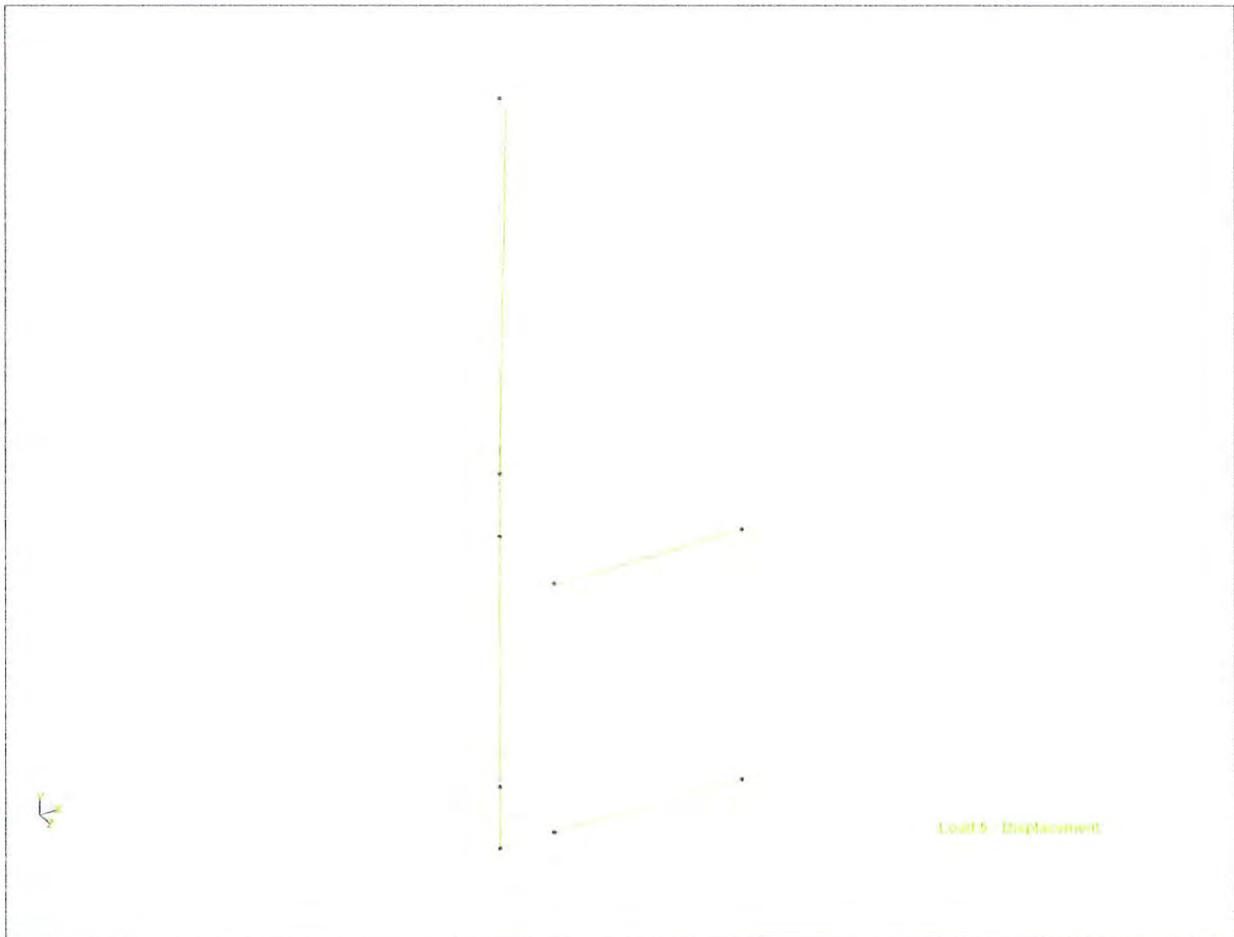
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Displacement



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Reactions

Node	L/C	Horizontal	Vertical	Horizontal	Moment		
		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	1:DL	-0.159	0.115	-0.073	0	-0.421	0
	2:DI	-0.300	0.219	-0.135	0	-0.745	0
	3:W	0.000	-0.098	0.368	0	9.034	0
	4:W(I)	0.000	-0.019	0.06116	0	1.496	0
	5:W(S)	0.000	-0.023	0.08766	0	2.150	0
	6:1.2D + 1.0W	-0.191	0.040	0.281	0	8.528	0
	7:1.2D + 1.0DI	-0.491	0.338	-0.162	0	0.246	0
	8:1.4D	-0.223	0.161	-0.102	0	-0.590	0
	9:1.0D + 1.0W	-0.159	0.092	0.015	0	1.729	0
2	1:DL	0.159	0.115	0.073	0	0.421	0
	2:DI	0.300	0.219	0.135	0	0.745	0
	3:W	-0.000	0.098	-1.050	0	-31.109	0
	4:W(I)	-0.000	0.019	-0.215	0	-6.315	0
	5:W(S)	0	0.023	-0.250	0	-7.402	0
	6:1.2D + 1.0W	-0.191	0.237	-0.963	0	-30.603	0
	7:1.2D + 1.0DI	0.491	0.376	0.008	0	-5.065	0
	8:1.4D	0.223	0.161	0.102	0	0.590	0
	9:1.0D + 1.0W	0.159	0.139	-0.177	0	-6.981	0

Analysis of Gamma Sector Stand-off Frame**Design Criteria**

1. TMS 402-11/ACI 530-11/ASCE 5-11 Building Code Requirements for Masonry Structures
2. ACI -318-11 Building Code Requirements for Structural Concrete
3. AISC 360-10 Specifications for Structural Steel Buildings

References

Refer to construction drawings by Dewberry Engineers Inc.

Thru Bolt Check

$M_y =$	2.59 kip-ft	Max moment at thru-bolt connection (4 Bolts)
$d =$	6.00 in	Bolt Spacing
$F_x =$	0.19 kip	Tensile Reaction at thru-bolt connection (4 Bolts)
$T =$	2.64 Kip	Tension at critical bolt (5/8"dia)
$F_y =$	0.24 kip	Vertical Shear Reaction at thru-Bolt connection (4 bolts)
$F_z =$	0.98 kip	Hor. Shear Reaction at thru-Bolt connection (4 bolts)
$V =$	1.00 kip	Shear at critical bolt (5/8"dia)
$f_t =$	8.61 ksi	Tensile Stress at critical bolt (5/8"dia)
$f_v =$	3.27 ksi	Shear Stress at critical bolt (5/8"dia)

Thru-Bolts OK by Inspection**Penthouse Wall Check**

Based on Engineering Judgement, the loads produced by the antenna mounting pipes is negligible on the penthouse CMU and steel stud walls

7:14 PM

9/12/2019

C:\Users\csenney\Desktop\MA By CS\Appendix B - Analysis of Gamma Sector Stand-off Frame\Gamma Sector Stand-off Frame - Reaction Check

APPENDIX C

Analysis of Beta Sector Ballast FrameOverview

The existing equipment on the ballast frame consists of (3) antennas, (3) RRUS and (1) surge arrestor. New equipment, which consists of (1) antenna and (1) RRU, will be mounted to a new 3" diameter pipe, which will be attached to the existing ballast frame.

Design Criteria and References

1. International Building Code (IBC) 2015, International Code Council
2. 2018 Connecticut State Building Code - Amendments to IBC 2015
3. TIA-222-H, Structural Standard for Antenna Supporting Structures and Antennas
4. Steel Construction Manual 14th Edition, American Institute of Steel Construction
5. ASCE 7-10 Minimum Design Loads for Buildings and Other Structures, American Society of Civil Engineers
6. Existing building plans by The Robinson Green Baretta Corporation, dated December 1982
7. Construction Drawings by Hudson Design Group, dated November 8th, 2016
8. Radio Frequency Data Sheet (RFDS) by AT&T, dated December 24th, 2018

STAAD Model Assumptions

1. Wind pressure applied normal to the short and long sides of the ballast frame governs for sliding and overturning
2. Although the antenna frame is oriented roughly 30° from the direction of wind, the calculated wind forces will be applied normal to the longspan side of the frame for simplicity (slightly conservative)
3. Since the proposed pipe mast that the new antenna and RRU are going to be mounted to is braced in two directions, and the weight of the additional equipment and new steel is negligible with regard to the strength and serviceability of the ballast frame, only the global stability needs to be investigated.
4. The RAD center for the Beta Sector is 109', which is 8 feet lower than the Alpha/Gamma Sector RAD centers (117'). Since the difference in wind pressure is less than 1 psf, the design wind pressures calculated in Appendices A & B will be used for the Beta Sector Analysis:

$$q_{z \text{ design}} = 34.23 \text{ psf} \quad \text{See Appendices A\&B}$$

Use ASCE 7-10 ASD Load Combo 1.0D + 0.6W for stability check:

$$q_{z \text{ design}} = 20.54 \text{ psf} \quad 0.6*W, \text{ to be used for Beta Sector Stability Check}$$

Minimum F.S. = 1.5 for Overturning and Sliding

Existing frame rests on load bearing walls. Based on engineering judgement, the existing load bearing walls are OK

Analysis of Beta Sector Ballast Frame
Equipment Dead Loads

	Description	Dimensions (in)			Weight (lb)
		W	D	H	
Antennas/RRHs	CCI HPA-65R-BU6AA	11.70	7.60	71.00	51.00
	Kathrein 800-10965	20.00	6.90	78.70	108.60
	CCI OPA-65R-LCUU-H6	14.80	7.40	72.00	73.00
	RRUS B25 4415	13.40	5.90	16.50	46.00
	RRUS B2/B12 4449	13.20	9.40	17.90	71.00
	RRUS B2/B66A 8843	13.20	10.90	14.90	72.00
	RRUS-32	12.10	6.70	26.70	60.00
	Raycap DC6-48-60-18-8C		9.00	26.00	31.80

*Bold = Proposed

Structural Members

Member	Dimensions (in)						Weight (lb/ft)
	d	b _f	t _f	t _w	I.D.	O.D.	
W12X19	12.2	4.01	0.35	0.235			19.00
W6X25	6.38	6.08	0.455	0.32			25.00
L3X3X3/8	3	3	0.375	0.375			7.20
3" STD Pipe					3.07	3.50	7.58

*Bold = Proposed



**Analysis of Beta Sector Ballast Frame
Force Coefficients for Appurtenances, Without Ice (TIA-222-H)**

Equipment	Dimensions (ft)			Area (A _n) (Normal) (sf)	Area (A _t) (Tangent) (sf)	Aspect Ratio (Normal)	Aspect Ratio (Tangent)	C Table 2-9	C _{an} (Normal) Table 2-9	C _{at} (Tangent) Table 2-9
	Width (Normal)	Length (tangent)	Height (or Span)							
CCI HPA-65R-BUGAA	0.98	0.63	5.92	5.77	3.75	6.07	9.34		1.36	1.48
Kathrein 800-10965	1.67	0.58	6.56	10.93	3.77	3.94	11.41		1.26	1.55
CCI OPA-65R-LCUU-H6	1.23	0.62	6.00	7.40	3.70	4.86	9.73		1.31	1.49
RRUS B25 4415	1.12	0.49	1.38	1.54	0.68	1.23	2.80		1.20	1.21
RRUS B2/B12 4449	1.10	0.78	1.49	1.64	1.17	1.36	1.90		1.20	1.20
RRUS B2/B66A 8843	1.10	0.91	1.24	1.37	1.13	1.13	1.37		1.20	1.20
RRUS-32	1.01	0.56	2.23	2.24	1.24	2.21	3.99		1.20	1.27
Raycap DC6-48-60-18-8C		0.75	2.17		1.63		2.89			1.22

Antennas/RRHs



**Analysis of Beta Sector Ballast Frame
Equipment Wind Loads (TIA-222-H)**

$$F_A = q_z \cdot G_h \cdot G_e \cdot (EPA)_A$$

$$(EPA)_A = C_e \cdot A_d$$

TIA-222-H, Section 2.6.11.2,

$G_h = 1.0$ (See Appendices A & B)

Equipment	No Ice		Ice		Strength (lbs)		Ice (lbs)		Service (lbs)		Maintenance (lbs)	
	(EPA) _A (Normal)	(EPA) _A (Tangent)	(EPA) _A (Normal)	(EPA) _A (Tangent)	F _A (Normal)	F _A (Tangent)						
CCI HPA-65R-BU6AA	7.84	5.54			160.96	113.75						
Kathrein 800-10965	13.81	5.83			283.71	119.80						
CCI OPA-65R-LCUU-H6	9.66	5.52			198.35	113.30						
RRUS B25-4415	1.84	0.82			37.84	16.84						
RRUS B2/B12 4449	1.97	1.40			40.44	28.80						
RRUS B2/B66A 8843	1.64	1.35			33.66	27.80						
RRUS-32	2.69	1.57			55.29	32.30						
Raycap DCG-48-60-18-8C		1.98				40.63						

*Wind loads shown reflect 0.6*W



Analysis of Beta Sector Ballast Frame

Structure Wind Loads (TIA-222-H)

Wind loads on structural elements will be applied linearly: $\omega_{wind} = q_{z, design} C_a G_r d$, with d being the structure depth or diameter. A conservative C_a value of 1.2 will be used for pipes, and 2/0 for W-Shapes and Angles.

Member	d (ft)	d _{ice} (ft)	C _a	ω_{wind} (lb/ft)	$\omega_{wind, ice}$ (lb/ft)	$\omega_{wind, ser}$ (lb/ft)	$\omega_{wind, m}$ (lb/ft)
W12X19	1.02		2.0	41.76			
W6X25	0.53		2.0	21.84			
L3X3X3/8	0.25		2.0	10.27			
3" STD Pipe	0.29		1.2	7.19			

*Wind loads shown reflect 0.6*W



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Part Beta Sector		
Ref		
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Job Title CT2490 - East Hampton Main Street

Client AT&T

Job Information

	Engineer	Checked	Approved
Name:	CS	BK	
Date:	9/10/2019	9/12/2019	

Project ID	
Project Name	

Structure Type SPACE FRAME

Number of Nodes	61	Highest Node	66
Number of Elements	92	Highest Beam	102

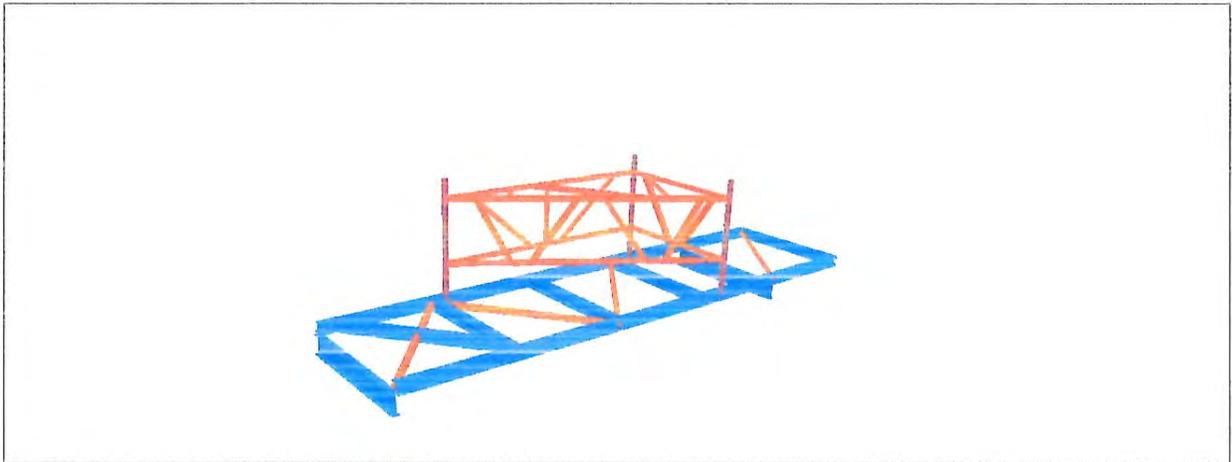
Number of Basic Load Cases	3
Number of Combination Load Cases	2

Included in this printout are data for:

All	The Whole Structure
-----	---------------------

Included in this printout are results for load cases:

Type	L/C	Name
Primary	1	DL
Primary	2	WIND(Z)
Primary	3	WIND(X)
Combination	4	1.0D + 1.5W(Z)
Combination	5	1.0D + 1.5W(X)



3D Rendered View



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Nodes

Node	X (ft)	Y (ft)	Z (ft)
1	0	0	0
2	0	0	7.667
3	30.625	0	0
4	30.625	0	7.667
5	6.125	0	0
6	12.250	0	0
7	18.375	0	0
8	24.500	0	0
9	6.125	0	7.667
10	12.250	0	7.667
11	18.375	0	7.667
12	24.500	0	7.667
13	6.875	0	0
14	19.875	0	0
15	19.875	0	7.667
16	6.875	2.000	0
17	19.875	2.000	0
18	19.875	2.000	7.667
19	6.875	5.500	0
20	19.875	5.500	0
21	19.875	5.500	7.667
22	6.875	6.500	0
23	19.875	6.500	0
24	19.875	6.500	7.667
27	8.207	5.500	0.785
28	12.729	5.500	3.452
29	14.021	5.500	4.214
30	18.543	5.500	6.881
31	9.822	2.000	1.738
32	10.683	2.000	2.246
33	16.067	2.000	5.421
34	16.928	2.000	5.929
35	18.375	5.500	0
36	13.375	5.500	0
37	8.375	5.500	0
38	14.375	2.000	0
39	12.375	2.000	0
40	13.375	2.000	0
41	19.875	5.500	6.708
42	19.875	5.500	0.958
43	19.875	2.000	4.333
44	19.875	2.000	3.333
45	9.746	5.500	1.693
46	17.004	5.500	5.973
47	16.142	5.500	5.465



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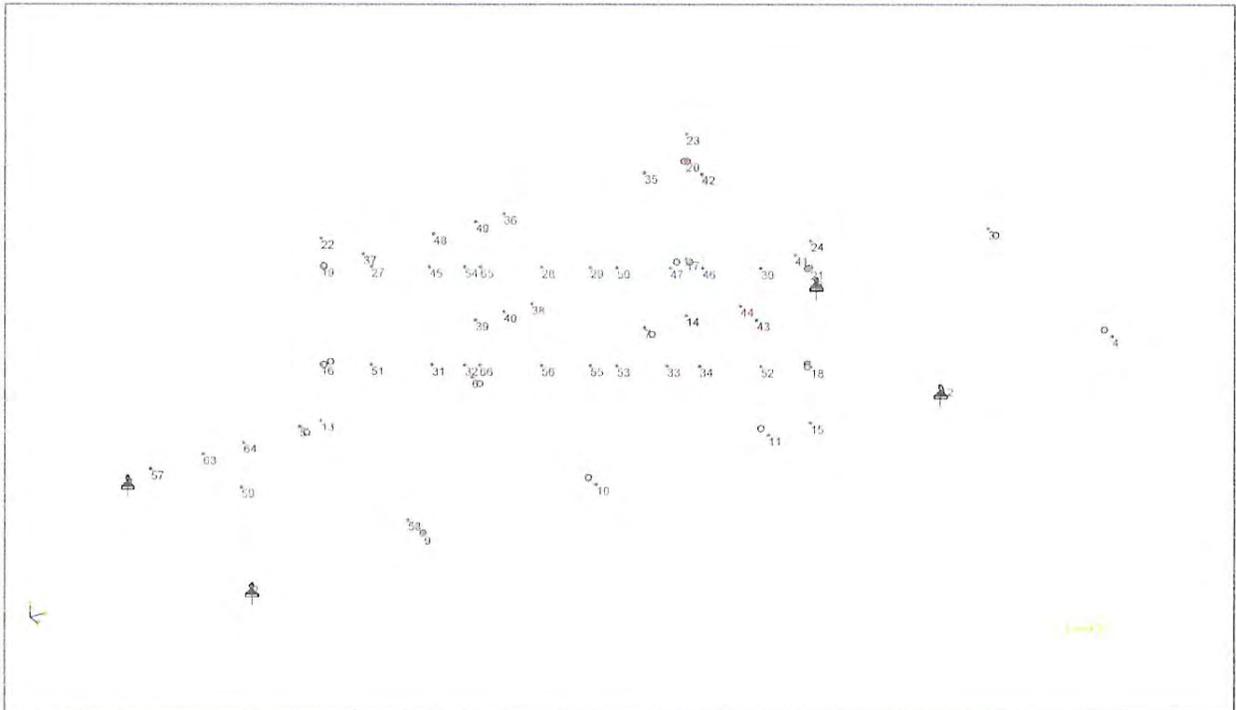
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Nodes Cont...

Node	X (ft)	Y (ft)	Z (ft)
48	10.875	5.500	0
49	12.375	5.500	0
50	14.721	5.500	4.627
51	8.207	2.000	0.785
52	18.543	2.000	6.881
53	14.721	2.000	4.627
54	10.683	5.500	2.246
55	14.021	2.000	4.214
56	12.729	2.000	3.453
57	0.830	0	0
58	6.125	0	6.667
59	2.696	0	2.349
63	2.696	0	0
64	4.125	0	0
65	11.105	5.500	2.495
66	11.087	2.000	2.484



Node Layout



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Beams

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
1	1	57	0.830	1	0
2	2	9	6.125	1	0
3	1	2	7.667	2	0
4	3	4	7.667	1	0
5	5	13	0.750	1	0
6	6	7	6.125	1	0
7	7	14	1.500	1	0
8	8	3	6.125	1	0
9	9	10	6.125	1	0
10	10	11	6.125	1	0
11	11	15	1.500	1	0
12	12	4	6.125	1	0
13	5	58	6.667	1	0
14	6	10	7.667	1	0
15	7	11	7.667	1	0
16	8	12	7.667	2	0
17	2	5	9.813	3	45
18	5	10	9.813	3	45
19	10	7	9.813	3	45
21	12	3	9.813	3	45
22	13	6	5.375	1	0
23	14	8	4.625	1	0
24	15	12	4.625	1	0
25	13	16	2.000	4	0
26	16	19	3.500	4	0
27	19	22	1.000	4	0
28	14	17	2.000	4	0
29	17	20	3.500	4	0
30	20	23	1.000	4	0
31	15	18	2.000	4	0
32	18	21	3.500	4	0
33	21	24	1.000	4	0
35	18	43	3.333	3	45
36	17	38	5.500	3	45
37	19	27	1.546	3	45
38	21	41	0.958	3	45
39	20	35	1.500	3	45
43	28	29	1.500	3	45
44	29	50	0.813	3	45
45	30	21	1.546	3	45
46	16	51	1.546	3	45
47	31	32	1.000	3	45
48	32	66	0.469	3	45
49	33	34	1.000	3	45
50	34	52	1.875	3	45



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Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
51	27	31	3.971	3	45
52	32	28	4.230	3	45
53	29	33	4.230	3	45
54	34	30	3.971	3	45
55	35	36	5.000	3	45
56	36	49	1.000	3	45
57	37	19	1.500	3	45
58	38	40	1.000	3	45
59	39	16	5.500	3	45
60	37	39	5.315	3	45
61	35	38	5.315	3	45
62	40	39	1.000	3	45
63	36	40	3.500	3	45
64	41	42	5.750	3	45
65	42	20	0.958	3	45
66	43	44	1.000	3	45
67	44	17	3.333	3	45
68	42	44	4.230	3	45
69	41	43	4.230	3	45
70	45	54	1.088	3	45
71	46	30	1.787	3	45
72	47	46	1.000	3	45
73	48	37	2.500	3	45
74	45	48	2.035	3	45
75	46	42	5.779	3	45
76	49	48	1.500	3	45
77	49	47	6.638	3	45
78	50	29	0.813	3	45
79	51	31	1.875	3	0
80	52	18	1.546	3	0
81	53	55	0.813	3	0
82	54	65	0.490	3	45
83	55	53	0.813	3	0
84	56	55	1.499	3	45
85	57	63	1.866	1	0
86	58	9	1.000	1	0
87	57	59	3.000	5	0
88	59	58	5.514	5	0
92	63	64	1.429	1	0
94	64	5	2.000	1	0
95	27	45	1.787	3	45
96	50	47	1.650	3	45
97	29	50	0.813	3	45
99	53	33	1.563	3	0
100	55	53	0.813	3	45



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Sheet No
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Part Beta Sector

Job Title CT2490 - East Hampton Main Street

Ref

By CS

Date 9/10/2019

Chd BK

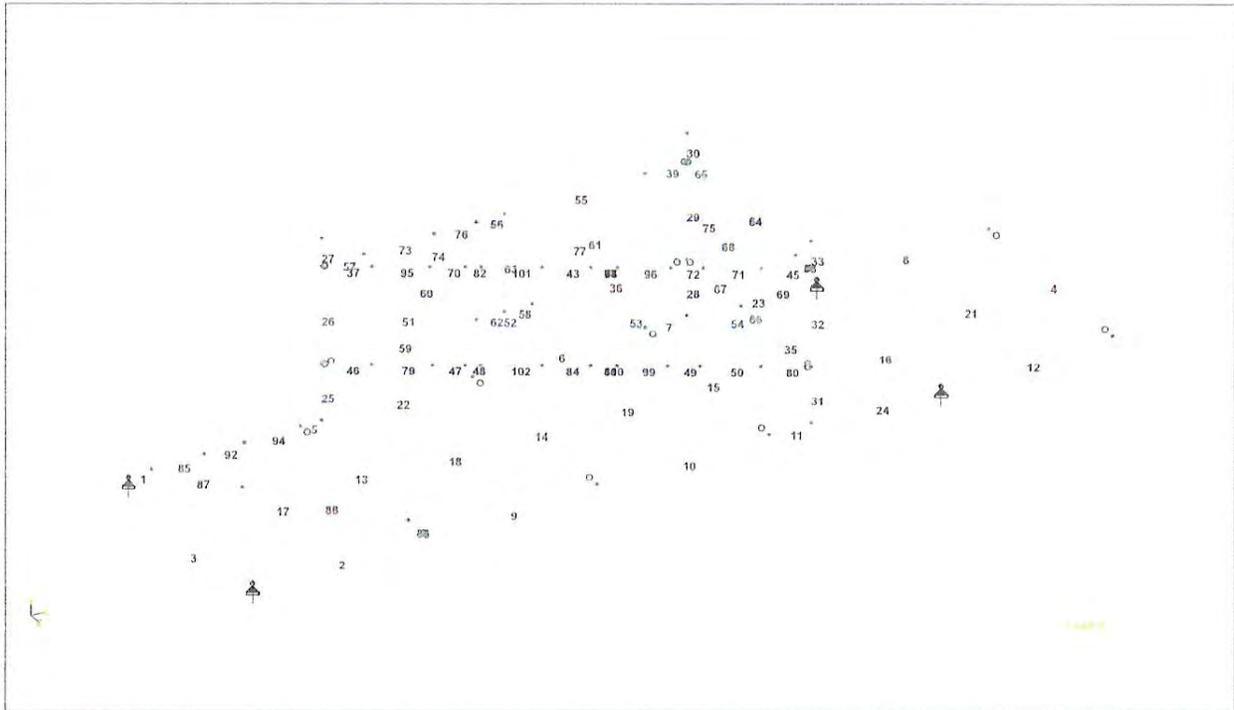
Client AT&T

File Beta Sector.std

Date/Time 11-Sep-2019 10:37

Beams Cont...

Beam	Node A	Node B	Length (ft)	Property	β (degrees)
101	65	28	1.885	3	45
102	66	56	1.907	3	45



Beam Layout

Section Properties

Prop	Section	Area (in ²)	I _{yy} (in ⁴)	I _{zz} (in ⁴)	J (in ⁴)	Material
1	W6X25	7.340	17.100	53.400	0.461	STEEL
2	W12X19	5.570	3.760	130.000	0.180	STEEL
3	L30306	2.110	2.793	0.727	0.102	STEEL
4	PIPS30	2.100	2.850	2.850	5.689	STEEL
5	W6X15	4.430	9.320	29.100	0.101	STEEL



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Job Title CT2490 - East Hampton Main Street

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Materials

Mat	Name	E (kip/in ²)	v	Density (kip/in ³)	α (1/°F)
1	CONCRETE	3.15E+3	0.170	8.68e-05	5.5E-6
2	ALUMINUM	10E+3	0.330	9.8e-05	12.8E-6
3	STEEL_50_KSI	29E+3	0.300	0.000283	6.5E-6
4	STAINLESSSTEEL	28E+3	0.300	0.000283	9.9E-6
5	STEEL_36_KSI	29E+3	0.300	0.000283	6.5E-6
6	STEEL_275_NMM2	29.7E+3	0.300	0.000	6.67E-6
7	STEEL	29E+3	0.300	0.000283	6E-6
8	STEEL_355_NMM2	29.7E+3	0.300	0.000	6.67E-6

Supports

Node	X (kip/in)	Y (kip/in)	Z (kip/in)	rX (kip*ft/deg)	rY (kip*ft/deg)	rZ (kip*ft/deg)
1	Fixed	Fixed	Fixed	-	-	-
2	Fixed	Fixed	Fixed	-	-	-
8	Fixed	Fixed	Fixed	-	-	-
12	Fixed	Fixed	Fixed	-	-	-

Releases

Beam ends not shown in this table are fixed in all directions.

Beam	Node	x	y	z	rx	ry	rz
4	3	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
4	4	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
13	5	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
14	6	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
14	10	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
15	7	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
15	11	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
35	18	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
36	17	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
37	19	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
38	21	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
39	20	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
45	21	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
46	16	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
57	19	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
59	16	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
65	20	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
67	17	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
80	18	Fixed	Fixed	Fixed	Pin	Fixed	Fixed
86	9	Fixed	Fixed	Fixed	Pin	Fixed	Fixed



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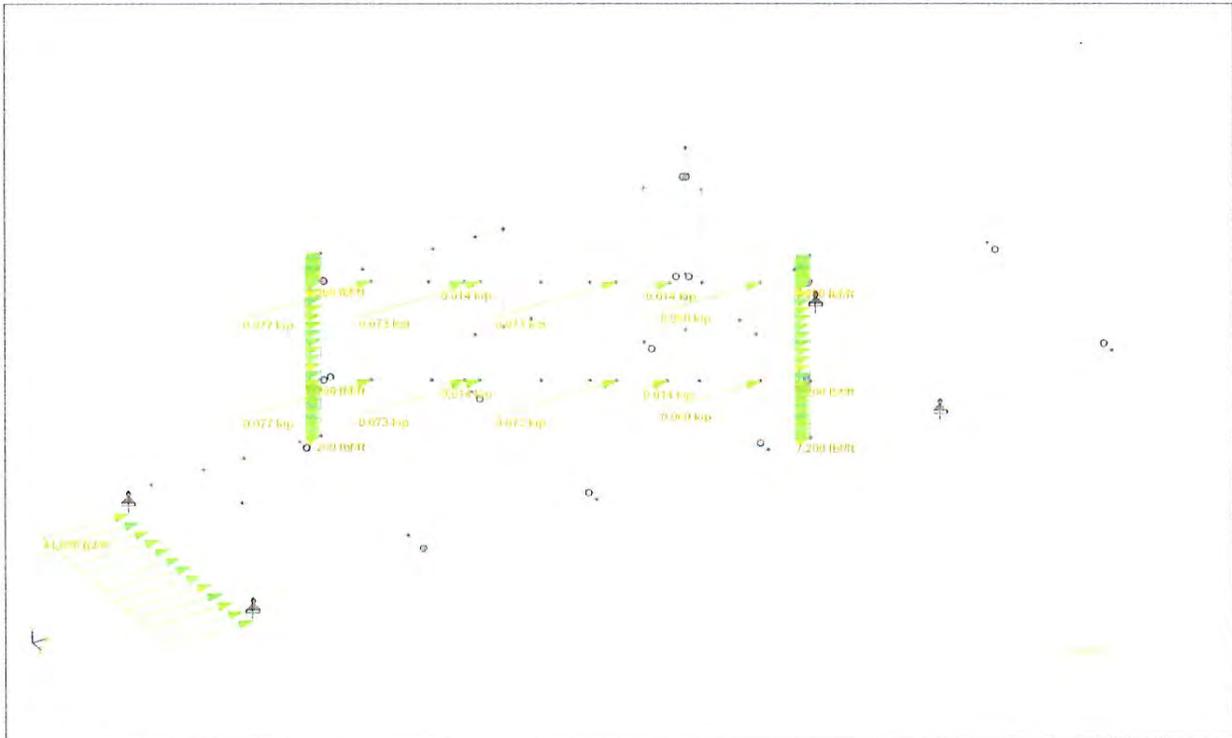
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Wind Load (X)

Reactions

Node	L/C	Horizontal			Moment		
		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
1	1:DL	0.683	1.213	-0.110	0	0	0
	2:WIND(Z)	1.722	0.107	0.448	0	0	0
	3:WIND(X)	-0.381	-0.088	-0.096	0	0	0
	4:1.0D + 1.5Wl	3.266	1.373	0.562	0	0	0
	5:1.0D + 1.5Wl	0.111	1.080	-0.253	0	0	0
2	1:DL	-0.012	0.669	0.163	0	0	0
	2:WIND(Z)	-1.788	-0.107	1.110	0	0	0
	3:WIND(X)	-0.250	-0.009	0.090	0	0	0
	4:1.0D + 1.5Wl	-2.693	0.509	1.828	0	0	0
	5:1.0D + 1.5Wl	-0.387	0.655	0.297	0	0	0
8	1:DL	-0.513	1.314	-0.164	0	0	0
	2:WIND(Z)	0.479	0.567	0.287	0	0	0
	3:WIND(X)	-0.179	0.088	0.014	0	0	0
	4:1.0D + 1.5Wl	0.205	2.165	0.267	0	0	0
	5:1.0D + 1.5Wl	-0.782	1.446	-0.142	0	0	0
12	1:DL	-0.158	1.447	0.111	0	0	0
	2:WIND(Z)	-0.414	-0.567	0.213	0	0	0



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Reactions Cont...

Node	L/C	Horizontal		Vertical	Moment		
		FX (kip)	FY (kip)	FZ (kip)	MX (kip'in)	MY (kip'in)	MZ (kip'in)
	3:WIND(X)	-0.225	0.009	-0.008	0	0	0
	4:1.0D + 1.5W(-0.778	0.596	0.431	0	0	0
	5:1.0D + 1.5W(-0.496	1.461	0.098	0	0	0

Z-Direction Wind governs for Sliding and Overturning

Per Construction Drawings by Hudson Design Group dated 11/08/2016, ballast is adhered to roof paver

Coef. of Friction = 0.8

Total weight 4.643 kip

Total sliding force = 3.088 kip (Sum of Fz Reactions)

$0.8 \times 4.643 = 3.715 > 3.088 \text{ kip} \rightarrow \text{Sliding OK}$

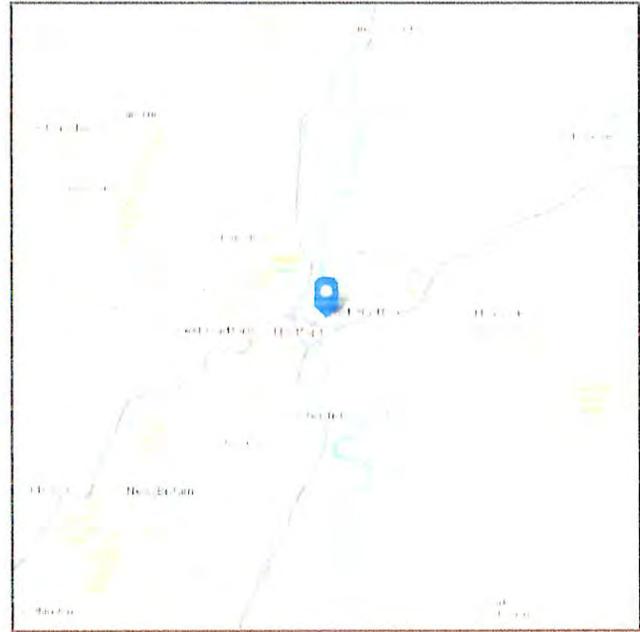
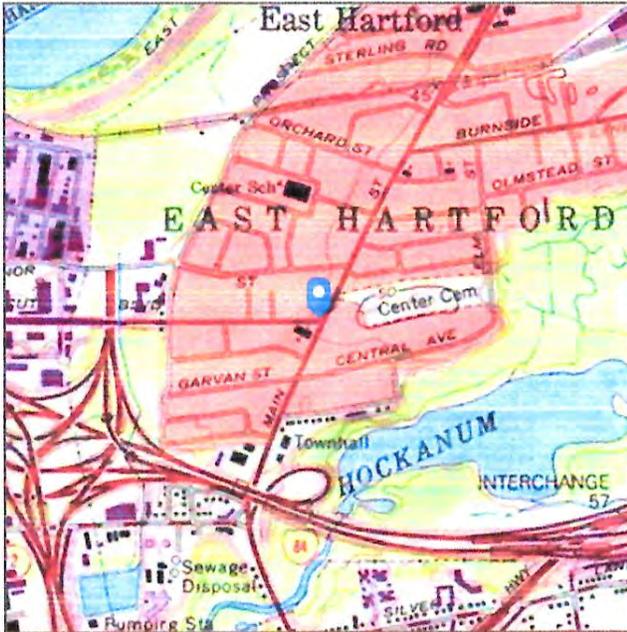
APPENDIX D

ASCE 7 Hazards Report

Address:
886 Main St
East Hartford, Connecticut
06108

Standard: ASCE/SEI 7-10
Risk Category: II
Soil Class:

Elevation: 40.7 ft (NAVD 88)
Latitude: 41.769404
Longitude: -72.64371



Wind

Results:

Wind Speed:	123 Vmph
10-year MRI	77 Vmph
25-year MRI	86 Vmph
50-year MRI	93 Vmph
100-year MRI	100 Vmph

Data Source: ASCE/SEI 7-10, Fig. 26.5-1A and Figs. CC-1–CC-4, incorporating errata of March 12, 2014

Date Accessed: Wed Sep 11 2019

Value provided is 3-second gust wind speeds at 33 ft above ground for Exposure C Category, based on linear interpolation between contours. Wind speeds are interpolated in accordance with the 7-10 Standard. Wind speeds correspond to approximately a 7% probability of exceedance in 50 years (annual exceedance probability = 0.00143, MRI = 700 years).

Site is in a hurricane-prone region as defined in ASCE/SEI 7-10 Section 26.2. Glazed openings need not be protected against wind-borne debris.

Mountainous terrain, gorges, ocean promontories, and special wind regions should be examined for unusual wind conditions.

SECTOR F	SECTOR E	SECTOR D	SECTOR C	SECTOR B	SECTOR A
MAIN					
Section 6 - RBS GENERAL INFORMATION - Existing					
19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME
RBS ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
CTS COMMON ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
CELL ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
STATION NAME	19 SITE ID				
43 DROT SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
DOWNLOTTID	19 SITE ID				
CELL SITE TYPE	19 SITE ID				
SITE TYPE	19 SITE ID				
BTS LOCATION ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
BTS STATION TYPE	19 SITE ID				
EQUIPMENT NAME	19 SITE ID				
DISABLED PRIORITY	19 SITE ID				
Section 6 - RBS GENERAL INFORMATION - Final					
19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME	19 SITE NAME
RBS ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
CTS COMMON ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
CELL ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
STATION NAME	19 SITE ID				
43 DROT SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
DOWNLOTTID	19 SITE ID				
CELL SITE TYPE	19 SITE ID				
SITE TYPE	19 SITE ID				
BTS LOCATION ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID	19 SITE ID
BTS STATION TYPE	19 SITE ID				
EQUIPMENT NAME	19 SITE ID				
DISABLED PRIORITY	19 SITE ID				

Section 10 - CIB/SAC - Pending											
LT	LT	LT	LT	LT	LT	LT	LT	LT	LT	LT	LT
201796	201797	201798	201799	201800	201801	201802	201803	201804	201805	201806	201807
SECTION A - CIB/SAC											
SECTION B											
SECTION C											
SECTION D											
SECTION E											
SECTION F											
COMM											
LT	LT	LT	LT	LT	LT	LT	LT	LT	LT	LT	LT
201796	201797	201798	201799	201800	201801	201802	201803	201804	201805	201806	201807
SECTION A - CIB/SAC											
SECTION B											
SECTION C											
SECTION D											
SECTION E											
SECTION F											
COMM											

Section 10 - CIB/SAC - Final

Section 15 - CURRENT RADIO COUNTS (existing)

	151 EST. 2006	152 EST. 1990	153 EST. 1985	154 EST. 1980	155 EST. 1975	156 EST. 1970	157 EST. 1965	158 EST. 1960	159 EST. 1955	160 EST. 1950	161 EST. 1945	162 EST. 1940	163 EST. 1935	164 EST. 1930	165 EST. 1925	166 EST. 1920	167 EST. 1915	168 EST. 1910	169 EST. 1905	170 EST. 1900	
SECTION A RADIO COUNTS																					
SECTION B																					
SECTION C																					
SECTION D																					
SECTION E																					
SECTION F																					
TOTAL																					

Section 14 - NEW PROPOSED T1 COUNTS

LTE B7Caker									
# T1s									
LINK PROFILE									
RF COMBINING									
FIBER or ETHERNET									
Tx Beam Model									
Tx Beam QTY									
RAM, EDU, Beam, Stack									
RAN TCO Beam, QTY									
SRU Beam Model									
SRU Beam QTY									
RRU - location									
RRU - UPEID									
DC CABLE									
DC Power Om. Bnd									
Bundled Fiber Cable									
Bundled DC Cable									

PORT 1	21 344 B 1/20 1	C 1 02 00 00 2	C 1 02 00 00 2	1 E 1300	1 1 4	100	8	750	0 2 3	0	3501 277	12
ANTENNA POSITION 1	21 344 B 1/20 1	C 1 02 00 00 1	C 1 02 00 00 1	1 E 1300	1 1 4	100	8	750	0 2 3	0	3501 277	12
PORT 2	21 344 B 1/20 1	C 1 02 00 00 2	C 1 02 00 00 2	1 E 1300	1 1 4	100	8	750	0 2 3	0	3501 277	12
ANTENNA POSITION 2	21 344 B 1/20 1	C 1 02 00 00 1	C 1 02 00 00 1	1 E 1300	1 1 4	100	8	750	0 2 3	0	3501 277	12

PORT 2	21344 C 100.4 0.4	C 102400 SC 2	C 102400 SC 2	L.T. 1000	MC 1000AH/ 04 1.4	100	4	750	0.1	0	3611757	30
ASTORIA PORTDOCK 3	21344 C 1023.4 0.4	C 102400 SC 1	C 102400 SC 1	L.T. 1025	MC 2000AH/ 04 1.8	100	4	750	0.1	0	12052005	30

Section 10A - PLANNED PROPOSED TOWER CONFIGURATION - SECTOR A (OF 0/10)

ANTENNA POSITION 10 LEFT TO RIGHT FROM BACK OF ANTENNA unless otherwise specified	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
Equating Antenna							
ANTENNA MAKE, MODEL							
ANTENNA VENDOR							
ANTENNA SIZE IN 3' W X F							
ANTENNA HEIGHT							
ANTENNA AZIMUTH							
ANTENNA TILT							
ANTENNA TYP. HEIGHT							
ANTENNA TYP. AZIMUTH							
ANTENNA TYP. TILT							
FEEDER AMOUNT							
VERTICAL SEPARATION FROM ANTENNA ABOVE (TOP TO TOP)							
VERTICAL SEPARATION FROM ANTENNA BELOW (TOP TO TOP)							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA TO LEFT, CENTERLINE IS CENTERLINE							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA TO RIGHT, CENTERLINE IS CENTERLINE							
HORIZONTAL SEPARATION FROM ANOTHER ANTENNA (which antenna #, # of inches)							
ANTENNA RET. MODEL, QTY, MODEL							
SOURCE ADDRESS OR QTY, MODEL							
DIVIDER, QTY, MODEL							
SUPPLIER, QTY, MODEL							
FEEDER RET. CONTROL UNIT, QTY, MODEL							
DC BLOCK, QTY, MODEL							
TRIAL/LA, QTY, MODEL							
CURRENT FUNCTION FOR TMA, QTY, MODEL							
PSU, QTY, TMA, QTY, MODEL							
FILTER, QTY, MODEL							
POWER TRUNK, QTY, MODEL							
DC TRUNK, QTY, MODEL							
REPEATER, QTY, MODEL							
RRH - 700 band, QTY, MODEL							
RRH - 800 band, QTY, MODEL							
RRH - 1900 band, QTY, MODEL							
RRH - AWS band, QTY, MODEL							
RRH - 600 band, QTY, MODEL							
Additional RRH #1 - 800 band, QTY, MODEL							
Additional RRH #2 - 800 band, QTY, MODEL							
Additional Component 1, QTY, MODEL							
Additional Component 2, QTY, MODEL							
Additional Component 3, QTY, MODEL							
Local Market Note 1							
Local Market Note 2							
Local Market Note 3							
Local Market Note 4							
USED (MHz)							
ATOLL TWD							
ATOLL TWD SA 1							
ATOLL TWD SA 2							
ATOLL TWD SA 3							
TECHNOLOGY							
FREQUENCY							
ANTENNA ATOLL							
ANTENNA GAIN							
ELECTRICAL AZIMUTH							
ELECTRICAL TILT							
RPL LOCATION (Longitude)							
FEEDER TYPE							
FEEDER LENGTH (ft)							
FEEDER LOSS (dB)							
TRIPLESER or LLC (QTY)							
TRIPLESER or LLC (MODEL)							
SCRAMBLER MODULE							
HATCHPLATE POWER (Watts)							
ERP (Watts)							
Antenna RET. Name							
CABLE NUMBER							
CABLE ID (Name)							
PORT #							
PORT 1							
PORT 2							
PORT 3							
PORT 4							

Section 108 - PLANNED PROPOSED TOWER CONFIGURATION - SECTOR B

ANTENNA POSITION 0 LEFT IS FRONT FROM BACK OF ANTENNA UNLESS OTHERWISE SPECIFIED	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
Equality Antenna							
ANTENNA MAKE / MODEL							
ANTENNA VENDOR							
ANTENNA SIZE IN X W X D							
ANTENNA HEIGHT							
ANTENNA AZIMUTH							
MAGNETIC DECLINATION							
RADIATION CENTER (ft)							
ANTENNA TIP HEIGHT							
METROPOLITAN DISTRICT							
FEDERATION							
VERTICAL SEPARATION FROM ANTENNA ABOVE (TOP TO TOP)							
VERTICAL SEPARATION FROM ANTENNA BELOW (TOP TO TOP)							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA TO LEFT CENTERLINE (CENTERLINE)							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA TO RIGHT CENTERLINE (CENTERLINE)							
HORIZONTAL SEPARATION FROM ANOTHER ANTENNA (INDICATE ANTENNA # IF APPLICABLE)							
ANTENNA RET. MET. QTY MODEL							
STORAGE ANTENNA QTY MODEL							
DIPLER QTY MODEL							
SUPPLIER QTY MODEL							
ANTENNA RET. CONTROL UNIT QTY MODEL							
DC BLOCK QTY MODEL							
TRIALING QTY MODEL							
CURRENT INDUCTOR FOR TNA QTY MODEL							
PSU FOR TNA QTY MODEL							
ALTER QTY MODEL							
SOUP QTY MODEL							
FIBER TRUNK QTY MODEL							
DC TRUNK QTY MODEL							
REFRIGERATOR QTY MODEL							
RRH-750 band QTY MODEL							
RRH-800 band QTY MODEL							
RRH-1900 band QTY MODEL							
RRH-AW2 band QTY MODEL							
RRH-1-WC band QTY MODEL							
Address RRH #1 - any band QTY MODEL							
Address RRH #2 - any band QTY MODEL							
Additional Components 1 QTY MODEL							
Additional Components 2 QTY MODEL							
Additional Components 3 QTY MODEL							
Local Number Node 1							
Local Number Node 2							
Local Number Node 3							

PORT SPECIFIC FIELDS	PORT NUMBER	USED (CS99)	USED (ASB)	ATOLL TXID	ATOLL CELL ID	TYPE/F	TECHNOLOGY / FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RPL LOCATION (Longitude)	FEDERATION TYPE	FEDERATION LENGTH (feet)	FIBER	TRIPLES OF LLC (QTY)	TRIPLES OF LLC (MODEL)	SCRAMBLER MODULE?	HATCH/PLATE POWER (Watts)	ERP (Watts)	Antenna RET. Name	CABLE NUMBER	CABLE ID (string)	
PORT 1							1.7, 1900	800A-1900MHz	300	300	0	152	16.73	0						1500.050				
PORT 2							1.7, 1900	800A-1900MHz	300	300	0	152	16.73	0						1500.050				
PORT 3							1.7, 1900	800A-1900MHz	300	300	0	152	16.73	0						1500.050				

Section 16C - PLANNED PROPOSED TOWER CONFIGURATION - SECTOR C

ANTENNA POSITION #	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7
LEFT TO RIGHT FROM BACK OF ANTENNA (unless otherwise specified)							
Existing Antenna?							
ANTENNA MAKE / MODEL				ROCKWELL BULLOCK			
ANTENNA VENDOR				CD			
ANTENNA SIZE (H x W x D)				18X11 X 7'6"			
ANTENNA WEIGHT				51			
AZIMUTH				380			
BUSINESS DECLARATION				140			
RADIATION CENTER TYPE				140			
ANTENNA TOP HEIGHT				0			
MEDIA/SIGNAL DIRECTION							
FEDERATION							
VERTICAL SEPARATION FROM ANTENNA ABOVE (TOP TO TOP)							
VERTICAL SEPARATION FROM ANTENNA BELOW (TOP TO TOP)							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA (LEFT CENTERLINE IS CENTERLINE)							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA (RIGHT CENTERLINE IS CENTERLINE)							
HORIZONTAL SEPARATION FROM ANOTHER ANTENNA (INDICATE ANTENNA #, IF APPLICABLE)							
ANTENNA RET. MAKE / QTY / MODEL				BE41P			
SOURCE AMPLIFIER QTY / MODEL							
DUPLEXER QTY / MODEL							
COUPLER QTY / MODEL							
ANTENNA RET. CONTROL UNIT QTY / MODEL				1'E 97H			
DC BLOCK QTY / MODEL							
TRIALS QTY / MODEL							
CURRENT INDUCTORS FOR TMA QTY / MODEL							
PBU QTY / TRAF QTY / MODEL							
FILTER QTY / MODEL							
SWAMP QTY / MODEL							
FIBER TRUNK QTY / MODEL							
DC TRUNK QTY / MODEL							
REPEATER QTY / MODEL							
RRL 1 750 band 1 QTY / MODEL							
RRL 1 800 band 1 QTY / MODEL							
RRL 1 800 band 2 QTY / MODEL							
RRL 1 800 band 3 QTY / MODEL							
RRL 1 800 band 4 QTY / MODEL							
RRL 1 800 band 5 QTY / MODEL							
RRL 1 800 band 6 QTY / MODEL							
RRL 1 800 band 7 QTY / MODEL							
RRL 1 800 band 8 QTY / MODEL							
RRL 1 800 band 9 QTY / MODEL							
RRL 1 800 band 10 QTY / MODEL							
RRL 1 800 band 11 QTY / MODEL							
RRL 1 800 band 12 QTY / MODEL							
RRL 1 800 band 13 QTY / MODEL							
RRL 1 800 band 14 QTY / MODEL							
RRL 1 800 band 15 QTY / MODEL							
RRL 1 800 band 16 QTY / MODEL							
RRL 1 800 band 17 QTY / MODEL							
RRL 1 800 band 18 QTY / MODEL							
RRL 1 800 band 19 QTY / MODEL							
RRL 1 800 band 20 QTY / MODEL							
RRL 1 800 band 21 QTY / MODEL							
RRL 1 800 band 22 QTY / MODEL							
RRL 1 800 band 23 QTY / MODEL							
RRL 1 800 band 24 QTY / MODEL							
RRL 1 800 band 25 QTY / MODEL							
RRL 1 800 band 26 QTY / MODEL							
RRL 1 800 band 27 QTY / MODEL							
RRL 1 800 band 28 QTY / MODEL							
RRL 1 800 band 29 QTY / MODEL							
RRL 1 800 band 30 QTY / MODEL							
RRL 1 800 band 31 QTY / MODEL							
RRL 1 800 band 32 QTY / MODEL							
RRL 1 800 band 33 QTY / MODEL							
RRL 1 800 band 34 QTY / MODEL							
RRL 1 800 band 35 QTY / MODEL							
RRL 1 800 band 36 QTY / MODEL							
RRL 1 800 band 37 QTY / MODEL							
RRL 1 800 band 38 QTY / MODEL							
RRL 1 800 band 39 QTY / MODEL							
RRL 1 800 band 40 QTY / MODEL							
RRL 1 800 band 41 QTY / MODEL							
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RRL 1 800 band 97 QTY / MODEL							
RRL 1 800 band 98 QTY / MODEL							
RRL 1 800 band 99 QTY / MODEL							
RRL 1 800 band 100 QTY / MODEL							
Additional Component 1 QTY / MODEL							
Additional Component 2 QTY / MODEL							
Additional Component 3 QTY / MODEL							
Local Market Note 1							
Local Market Note 2							
Local Market Note 3							

PORT SPECIFIC FEEDS	PORT NUMBER	USED (MHz)	USED (MHz)	ATOLL TYP	ATOLL CELL ID	TYPE/P	TECHNOLOGY	FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	FEEDER TYPE	FEEDER LENGTH (ft)	FEEDER QTY	TRIPLODER OF LLC (QTY)	TRIPLODER OF LLC (MODEL)	SCF/MSCPA MODULE	HATCH/PLATE POWER (Watts)	ERP (Watts)	Antenna RET. Name	CABLE NUMBER	CABLE DISCREG	
PORT 1		17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	
PORT 2		17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	
PORT 3		17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	17340-1900-4	
ANTENNA POSITION 4																								
PORT 4																								

Section 16.5A - SCORING TOWER CONFIGURATION - SECTOR A (OF 6) (M) Section 17A - FINAL TOWER CONFIGURATION - SECTOR A (OF 6) (M)

ANTENNA POSITION 8 MPT to MPT from MPT #1 (OTM) unless otherwise specified	ANTENNA POSITION 1	ANTENNA POSITION 2	ANTENNA POSITION 3	ANTENNA POSITION 4	ANTENNA POSITION 5	ANTENNA POSITION 6	ANTENNA POSITION 7																
ANTENNA MAKE, MODEL (NO. USE)	024.001.0224.6	024.001.0224.6	024.001.0224.6	024.001.0224.6	024.001.0224.6	024.001.0224.6	024.001.0224.6																
ANTENNA VENDOR	CDI	CDI	CDI	CDI	CDI	CDI	CDI																
ANTENNA SIZE (H x W x D)	70"x48"x4	70"x48"x4	70"x48"x4	70"x48"x4	70"x48"x4	70"x48"x4	70"x48"x4																
ANTENNA HEIGHT	70	70	70	70	70	70	70																
AZIMUTH	90	90	90	90	90	90	90																
RAISE TO DECLINATION																							
PADATION CENTER (FEET)	140	140	140	140	140	140	140																
ANTENNA TIP HEIGHT	140	140	140	140	140	140	140																
MECHANICAL DOWNTILT	0	0	0	0	0	0	0																
FEDERATION																							
VERTICAL SEPARATION FROM ANTENNA ABOVE (TOP TO TOP)																							
VERTICAL SEPARATION FROM ANTENNA BELOW (TOP TO TOP)																							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA (LEFT, CENTERLINE IS CENTRALINE)																							
HORIZONTAL SEPARATION FROM CLOSEST ANTENNA (RIGHT)																							
HORIZONTAL SEPARATION FROM ANOTHER ANTENNA (OTHER ANTENNA #, # OF ANTENNAS)																							
ANTENNA RET. METER (OTM) MODEL	Blank	Blank	Blank	Blank	Blank	Blank	Blank																
SINGLE AMPLIFIER (OTM) MODEL	Blank	Blank	Blank	Blank	Blank	Blank	Blank																
DUPLEXER (OTM) MODEL	Blank	Blank	Blank	Blank	Blank	Blank	Blank																
DUALIZER (OTM) MODEL	Blank	Blank	Blank	Blank	Blank	Blank	Blank																
ANTENNA RET. CONTROL UNIT (OTM) MODEL	LT. 93H	LT. 93H	LT. 93H	LT. 93H	LT. 93H	LT. 93H	LT. 93H																
DC BLOCK (OTM) MODEL																							
TRIALING (OTM) MODEL																							
CURRENT FUSE/GUARD FOR TMA (OTM) MODEL																							
FRU FOR TRAS (OTM) MODEL																							
FILTER (OTM) MODEL																							
SOUD (OTM) MODEL																							
FEEDER TRUNK (OTM) MODEL																							
DC TRUNK (OTM) MODEL																							
REPEATER (OTM) MODEL																							
RRH - 700 band (OTM) MODEL	RRH-700 band (OTM) MODEL																						
RRH - 800 band (OTM) MODEL	RRH-800 band (OTM) MODEL																						
RRH - 1900 band (OTM) MODEL	RRH-1900 band (OTM) MODEL																						
RRH - AWS band (OTM) MODEL	RRH-AWS band (OTM) MODEL																						
RRH - AWS band (OTM) MODEL	RRH-AWS band (OTM) MODEL																						
Additional Component 1 (OTM) MODEL																							
Additional Component 2 (OTM) MODEL																							
Additional Component 3 (OTM) MODEL																							
Local Market Note 1																							
Local Market Note 2																							
Local Market Note 3																							
PORT SPECIFIC FIELDS	PORT NUMBER	USED (MHz)	USED (MHz)	ATOLL TX ID	ATOLL CELL ID	TX BWP	TECHNOLOGY	FREQUENCY	ANTENNA ATOLL	ANTENNA GAIN	ELECTRICAL AZIMUTH	ELECTRICAL TILT	RFL LOCATION (Elevation/ Azimuth)	FEDERATION TYPE	FEDERATION LENGTH (Meters)	FEAR (OTM) MODULE	TRIPLEXER or LLC (OTM)	SCF/MCM/CA MODULE	HATCH/PLATE POWER (Watts)	ERP (Watts)	ANTENNA RET. Name	CABLE NUMBER	CABLE ADDRESS
ANTENNA POSITION 1	PORT 1	11344.850.50	11344.850.50	0130497.74.1	0130497.74.1	1E.700	1E.700	1417.000	80010005.710M	14.7	90	5	700	FEAR	2				14.7000	1000			
	PORT 2	11344.850.50	11344.850.50	0130497.74.1	0130497.74.1	1E.700	1E.700	1417.000	80010005.849M	15.5	90	9	700	FEAR	0				15.5000	1000			
	PORT 3	11344.850.50	11344.850.50	0130497.74.1	0130497.74.1	1E.700	1E.700	1417.000	80010005.117M	13.3	90	9	700	FEAR	0				13.3000	1000			
	PORT 4	11344.850.50	11344.850.50	0130497.74.1	0130497.74.1	1E.700	1E.700	1417.000	80010005.849M	15.5	90	9	700	FEAR	0				15.5000	1000			



OctoPort Multi-Band Antenna

OPA-65R-LCUU-H6

SPECIFICATIONS

Electrical

Ports	2 x Low Band Ports for 698-787 MHz	2 x Low Band Ports for 824-894 MHz	4 x High Band Ports for 1710-2360 MHz			
Frequency Range	698-787 MHz	824-894 MHz	1850-1990 MHz	1710-1755/2110-2170 MHz	2305-2360 MHz	
Gain	13.8 dBi	14.6 dBi	17.0 dBi	16.3 dBi	17.4 dBi	17.6 dBi
Azimuth Beamwidth (-3dB)	66°	61°	60°	68°	64°	60°
Elevation Beamwidth (-3dB)	12.2°	10.3°	5.7°	6.3°	5.1°	4.5°
Electrical Downtilt	0° to 10°	0° to 10°	0° to 8°	0° to 8°	0° to 8°	0° to 8°
Elevation Sidelobes (1st Upper)	< -17 dB	< -18 dB	< -19 dB	< -19 dB	< -18 dB	< -18 dB
Front-to-Back Ratio @180°	> 30 dB	> 27 dB	> 32 dB	> 32 dB	> 35 dB	> 35 dB
Front-to-Back Ratio over ± 20°	> 27 dB	> 25 dB	> 27 dB	> 27 dB	> 28 dB	> 28 dB
Cross-Polar Discrimination (at Peak)	> 22 dB	> 22 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Cross-Polar Discrimination (at ± 60°)	> 16 dB	> 14 dB	> 17 dB	> 17 dB	> 17 dB	> 17 dB
Cross-Polar Port-to-Port Isolation	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB	> 25 dB
Voltage Standing Wave Ratio (VSWR)	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1	< 1.5:1
Passive Intermodulation (2x20W)	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc	≤ -150 dBc
Input Power Continuous Wave (CW)	500 watts	500 watts	300 watts	300 watts	300 watts	300 watts
Polarization	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°	Dual Pol 45°
Input Impedance	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms	50 ohms
Lightning Protection	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground	DC Ground

Mechanical

Dimensions (LxWxD)	72.3x14.4x7.3 in (1836x366x185 mm)
Survival Wind Speed	> 150 mph (> 241 kph)
Front Wind Load	243 lbs (1081 N) @ 100 mph (161 kph)
Side Wind Load	140 lbs (622 N) @ 100 mph (161 kph)
Equivalent Flat Plate Area	9.5 ft ² (0.9 m ²)
Weight *	56.9 lbs (25.8 kg)
RET System Weight	6.6 lbs (3.0 kg)
Connector	8 x 7-16 DIN female long neck
Mounting Pole	2 to 5 in (5 to 12 cm)

* Weight excludes mounting and RET

RRUS 32 B30



PRELIMINARY

- > WCS A+B blocks
 - TX = 2350 -- 2360 MHz
 - RX = 2305 -- 2315 MHz
- > RF output 4 x 25 Watts
- > 4T4R FDD
- > 10 MHz IBW for LTE
- > CPRI 2 ports x 10 Gbps
- > Dimensions (incl. feet and sunshield)
 - Height: 26.7" (678 mm)
 - Width: 12.1" (306 mm)
 - Depth: 6.7" (171 mm)
- > Weight, excl. mounting hardware
 - 60 lbs (23 kg)

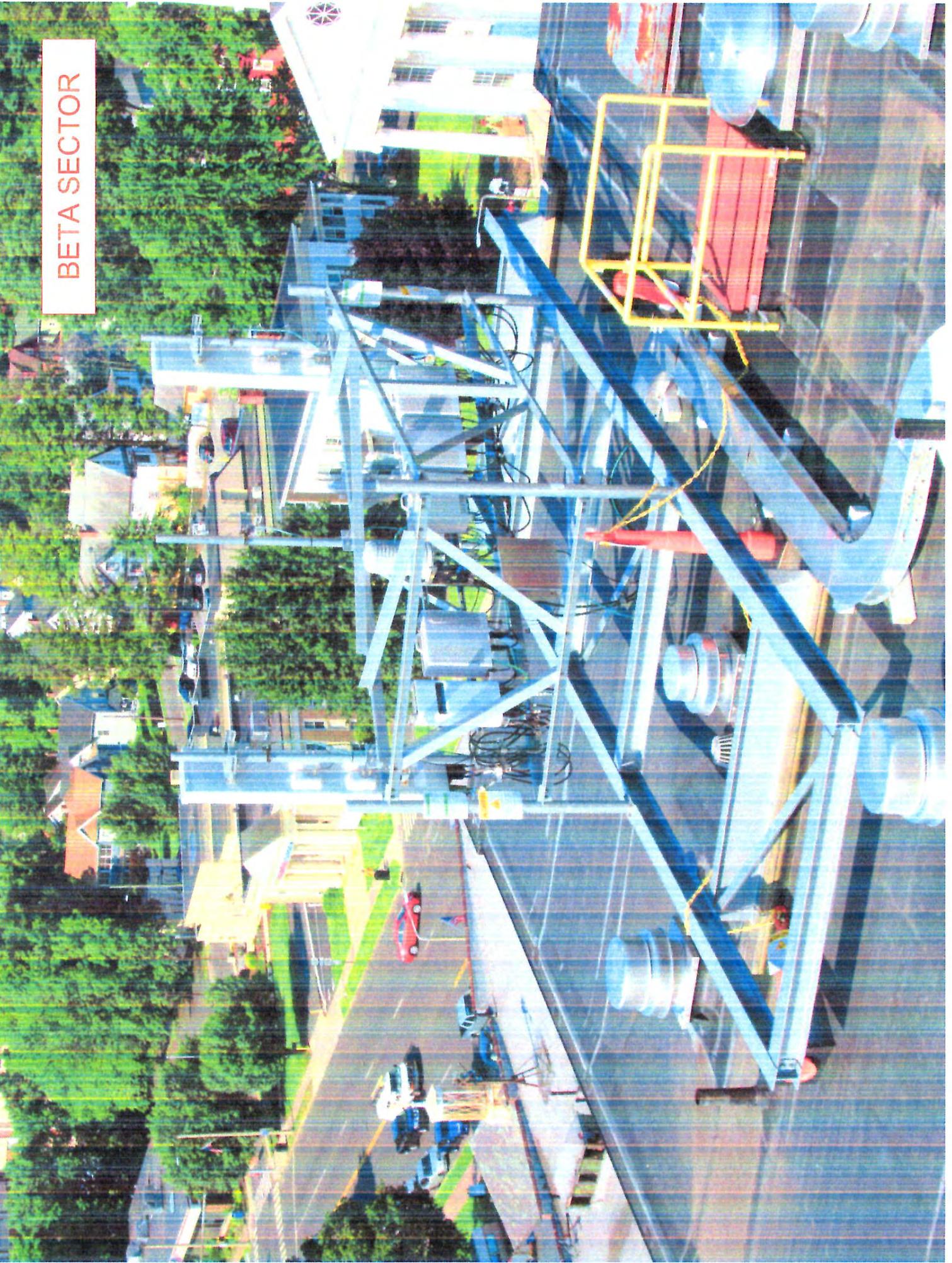


APPENDIX E

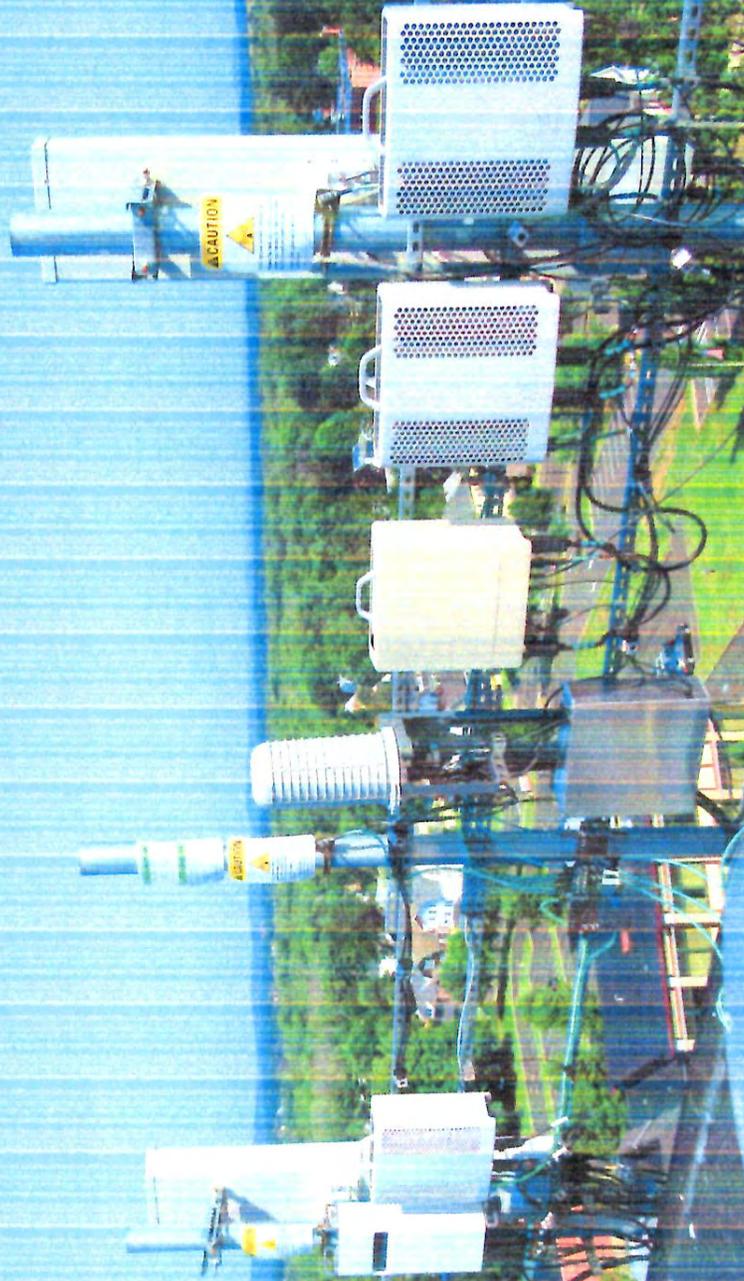
ALPHA SECTOR



BETA SECTOR



GAMMA SECTOR



Town of East Hartford Property Summary Report

886 MAIN ST

MAP LOT:	13-332	CAMA PID:	8733
LOCATION:	886 MAIN ST		
OWNER NAME:	HARTFORD EAST ASSOCIATION		



8733 03/27/2016

OWNER OF RECORD
HARTFORD EAST ASSOCIATION
954 WARWICK AVE
WARWICK, RI 02888

LIVING AREA:	97981	ZONING:	B5	ACREAGE:	1.19
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SALES HISTORY

OWNER	BOOK / PAGE	SALE DATE	SALE PRICE
HARTFORD EAST ASSOCIATION	27/ 37	01-Jan-1900	\$0.00

CURRENT PARCEL ASSESSMENT

TOTAL:	\$6,440,000.00	IMPROVEMENTS:	\$6,076,700.00	LAND:	\$363,300.00
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ASSESSING HISTORY

FISCAL YEAR	TOTAL VALUE	IMPROVEMENT VALUE	LAND VALUE
2018	\$6,440,000.00	\$6,076,700.00	\$363,300.00
2017	\$5,390,000.00	\$5,026,700.00	\$363,300.00
2016	\$4,760,000.00	\$4,396,700.00	\$363,300.00
2015	\$4,760,000.00	\$4,396,700.00	\$363,300.00
2014	\$5,943,560.00	\$5,580,260.00	\$363,300.00

Town of East Hartford Property Summary Report

886 MAIN ST

MAP LOT:	13-332	CAMA PID:	8733
LOCATION:	886 MAIN ST		
OWNER NAME:	HARTFORD EAST ASSOCIATION		

BUILDING # 1

YEAR BUILT	1983	EXT WALL 1	Brick
STYLE	High Rise	INT WALLS 1	Drywall
MODEL	Comm/Ind	HEAT FUEL	Gas
STORIES	11	HEAT TYPE	Forced Hot Air
OCCUPANCY	Apt w/ Elevator	AC TYPE	Unit
ROOF	Flat	BEDROOMS	
ROOF COVER	Rubber	FULL BATHS	0
FLOOR COVER 1	Mixed	HALF BATHS	
% BSMT	null	TOTAL ROOMS	120
% FIN BSMT	null	% REC RM	null
% SEMI FIN	null	% ATTIC FINISH	null
BSMT GARAGE	null	FIREPLACES	null



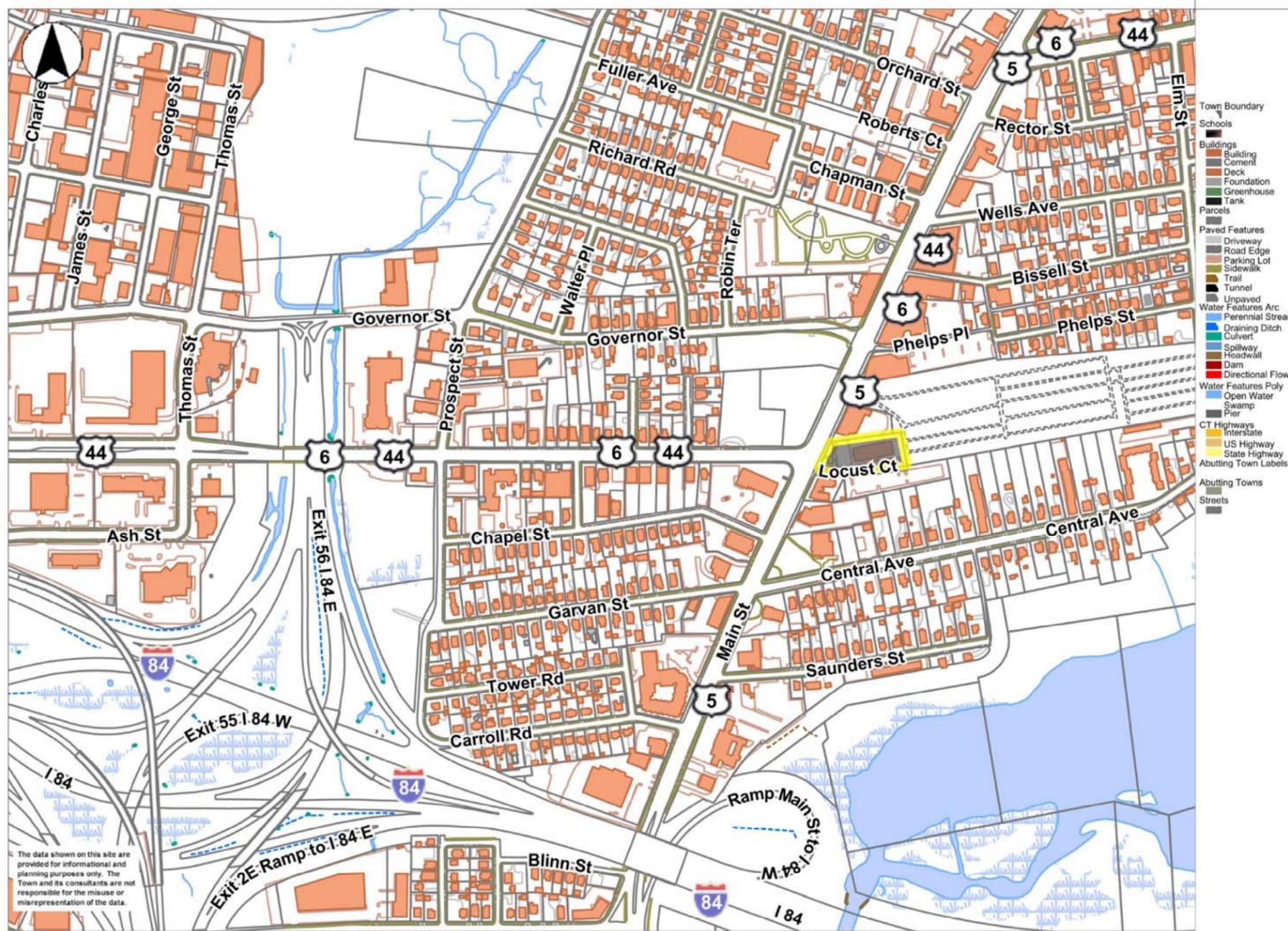
8733 03/27/2016

EXTRA FEATURES

DESCRIPTION	CODE	UNITS
Sprinklers-Wet	SPR1	97981 S.F.
Elevator Pass	ELV1	2 UNITS

OUTBUILDINGS

DESCRIPTION	CODE	UNITS
FR/SHED		90 SF



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East Hartford MapsOnline



STATE OF CONNECTICUT

CONNECTICUT SITING COUNCIL

136 Main Street, Suite 401
New Britain, Connecticut 06051-4225
Phone: 827-7682

Petition No. 324

Metro Mobile CTS of Hartford, Inc.
886 Main Street
East Hartford, CT

Staff Report
August 9, 1994

On July 29, 1994, Connecticut Siting Council (Council) member Daniel P. Lynch, Jr., Council staff member Stephen M. Howard, and Thomas Krummenacker representing Metro Mobile CTS of Hartford, Inc. (Metro Mobile), met at the site of the proposed cellular telecommunications facility at 886 Main Street, East Hartford, Connecticut.

Metro Mobile is proposing to install nine panel antennas, three each at three locations on the building. Each antenna is approximately 35 inches in height, 12 inches wide, and five inches deep. Three of the nine antennas would be attached to the building facade just below the roof line. Three additional antennas would be attached to the facade of the elevator penthouse on the roof of the building, below the penthouse roof line. The remaining three antennas would be mounted on pipes, approximately five feet in length, to be attached to the top of the elevator penthouse. Equipment associated with antennas would be located inside an 18-foot by 25-foot equipment room which would be constructed within a leased area on the ground floor of the building. The antennas would be attached at levels ranging from 99 feet above ground level to approximately 117 feet above ground level. The antennas would not extend beyond the height of the existing chimneys, vents, and television antennas on the penthouse roof. The building is not listed on any historical or architectural register, nor would it require any structural modification to support the proposed installations.

The maximum (i.e., "worst case") radio frequency power density calculations, assuming 19 channels operating simultaneously at 100 watts effective radiated power in an omni directional pattern, at the closest occupied floor of the building which is approximately 15 feet below the lowest antenna mounting point, indicate that the cellular antennas would emit 0.1186 milliwatts per square centimeter or 20.3 percent of the current ANSI standard. This calculation does not take into account the directional nature of the proposed antennas, which would likely result in a lower actual radio frequency power density at this occupied level.

Metro Mobile contends that the proposed construction would not have a substantial adverse environmental effect and therefore would not require a Certificate of Environmental Compatibility and Public Need from the Council.

Stephen M. Howard
Siting Analyst

SMH:mmb
SP324sr.doc



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MARK J ROBERTS
 QC DEVELOPMENT
 PO BOX 916
 STORRS CT 06268-0916

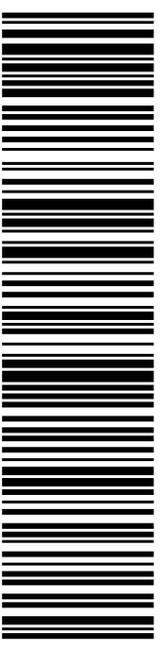
0024

Carrier -- Leave if No Response

C066

SHIP MAYOR MARCIA LECLERC
 TO: TOWN OF EAST HARTFORD
 740 MAIN ST
 CC: JEFFREY CORMIER - TOWN PLANNER
 EAST HARTFORD CT 06108-3140

USPS TRACKING #



9405 5036 9930 0120 2732 08

Electronic Rate Approved #038555749



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Instructions

1. Each Click-N-Ship® label is unique. Labels are to be used as printed and used only once. DO NOT PHOTO COPY OR ALTER LABEL.
2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

USPS TRACKING # :
9405 5036 9930 0120 2732 08

Trans. #: 473274652	Priority Mail® Postage: \$7.35
Print Date: 09/25/2019	Total: \$7.35
Ship Date: 09/28/2019	
Expected Delivery Date: 09/30/2019	

From: MARK J ROBERTS
 QC DEVELOPMENT
 PO BOX 916
 STORRS CT 06268-0916

To: MAYOR MARCIA LECLERC
 TOWN OF EAST HARTFORD
 740 MAIN ST
 CC: JEFFREY CORMIER - TOWN PLANNER
 EAST HARTFORD CT 06108-3140

* Retail Pricing Priority Mail rates apply. There is no fee for USPS Tracking® service on Priority Mail service with use of this electronic rate shipping label. Refunds for unused postage paid labels can be requested online 30 days from the print date.



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09/28/2019 Mailed from 06268 062S0000001301

PRIORITY MAIL 2-DAY™

Expected Delivery Date: 09/30/19

MARK J ROBERTS
 QC DEVELOPMENT
 PO BOX 916
 STORRS CT 06268-0916

0004

C004

SHIP TO: HARTFORD EAST ASSOCIATION
 954 WARWICK AVE
 ATTN MR PETER WOLOOHOJIAN
 WARWICK RI 02888-3650

USPS TRACKING #



9405 5036 9930 0120 2732 15

Electronic Rate Approved #038555749



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Instructions

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2. Place your label so it does not wrap around the edge of the package.
3. Adhere your label to the package. A self-adhesive label is recommended. If tape or glue is used, DO NOT TAPE OVER BARCODE. Be sure all edges are secure.
4. To mail your package with PC Postage®, you may schedule a Package Pickup online, hand to your letter carrier, take to a Post Office™, or drop in a USPS collection box.
5. Mail your package on the "Ship Date" you selected when creating this label.

Click-N-Ship® Label Record

USPS TRACKING # :
9405 5036 9930 0120 2732 15

Trans. #: 473274652	Priority Mail® Postage: \$7.35
Print Date: 09/25/2019	Total: \$7.35
Ship Date: 09/28/2019	
Expected Delivery Date: 09/30/2019	

From: MARK J ROBERTS
 QC DEVELOPMENT
 PO BOX 916
 STORRS CT 06268-0916

To: HARTFORD EAST ASSOCIATION
 954 WARWICK AVE
 ATTN MR PETER WOLOOHOJIAN
 WARWICK RI 02888-3650

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 Check the status of your shipment on the USPS Tracking® page at usps.com



Shipment Confirmation Acceptance Notice

A. Mailer Action

Note To Mailer: The labels and volume associated to this form online, **must** match the labeled packages being presented to the USPS® employee with this form.

Shipment Date: 09/25/19

Shipped From:

MARK J ROBERTS
QC DEVELOPMENT
PO BOX 916
STORRS CT 06268-0916

Type of Mail	Volume
Priority Mail®	2
Priority Mail Express™*	0
International Mail*	0
Other	0
Total Volume	2

*Start time for products with service guarantees will begin when mail arrives at the local Post Office™ and items receive individual processing and acceptance scans.

B. USPS Action

- USPS EMPLOYEE: Please scan upon pickup or receipt of mail. Leave form with customer or in customer's mail receptacle.
- Employee verifies the package volume count on the Package Pickup Carrier Manifest.
 - If the volume on the manifest matches the volume being collected from the customer, the employee should make the **1:YES** selection by pressing the number 1 on the keypad of the handheld scanner, or on the keyboard of the POS ONE terminal.
 - If the volume on the manifest does not match the volume being collected from the customer, the employee should make the **2:NO** selection. The mail should still be collected and dispatched as normal.

USPS SCAN



9475 7036 9930 0327 6300 12